

Special Issue Reprint

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# Innovative Catalytic Materials for Environmental Remediation and Energy Applications

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Edited by  
Georgios Bampos, Athanasia Petala and Zacharias Frontistis

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# **Innovative Catalytic Materials for Environmental Remediation and Energy Applications**



# **Innovative Catalytic Materials for Environmental Remediation and Energy Applications**

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# Contents

**Georgios Bampos, Athanasia Petala and Zacharias Frontistis**

Innovative Catalytic Materials for Environmental Remediation and Energy Applications

Reprinted from: *Catalysts* **2024**, *14*, 102, <https://doi.org/10.3390/catal14020102> . . . . . 1

**Alexandros Safakas, Vasileios Ch. Kournoutis, Georgios Bampos and Symeon Bebelis**

CO and Propane Combustion on  $\text{La}_{0.8}\text{Sr}_{0.2}\text{Co}_x\text{Fe}_{1-x}\text{O}_{3-\delta}$  Perovskites: Effect of Fe-to-Co Ratio on Catalytic Activity

Reprinted from: *Catalysts* **2023**, *13*, 1342, <https://doi.org/10.3390/catal13101342> . . . . . 5

**Avik Chowdhury, Sudip Bhattacharjee, Sayantan Chongdar, Bhabani Malakar, Anindita Maity and Asim Bhaumik**

A New Mixed-Metal Phosphate as an Efficient Heterogeneous Catalyst for Knoevenagel Condensation Reaction

Reprinted from: *Catalysts* **2023**, *13*, 1053, <https://doi.org/10.3390/catal13071053> . . . . . 25

**Nikoleta Kokkinou, Fotios Xydas, Susanne Brosda, Georgios Kyriakou and Alexandros Katsaounis**

Electrochemical Promotion of  $\text{CO}_2$  Hydrogenation Using Rh Catalysts Supported on  $\text{O}^{2-}$ -Conducting Solid Electrolyte

Reprinted from: *Catalysts* **2023**, *13*, 1014, <https://doi.org/10.3390/catal13061014> . . . . . 40

**Oleg A. Shlyakhtin, Grigoriy M. Timofeev, Sergey A. Malyshev, Alexey S. Loktev, Galina N. Mazo, Tatiana Shatalova, Veronika Arkhipova, Ilya V. Roslyakov and Alexey G. Dedov**

$\text{Nd}_{2-x}\text{Sr}_x\text{NiO}_4$  Solid Solutions: Synthesis, Structure and Enhanced Catalytic Properties of Their Reduction Products in the Dry Reforming of Methane

Reprinted from: *Catalysts* **2023**, *13*, 966, <https://doi.org/10.3390/catal13060966> . . . . . 56

**Basmah H. Alshammari, Humayra Begum, Fatma A. Ibrahim, Mohamed S. Hamdy, Tahamida A. Oyshi, Nazia Khatun and Mohammad A. Hasnat**

Electrocatalytic Hydrogen Evolution Reaction from Acetic Acid over Gold Immobilized Glassy Carbon Surface

Reprinted from: *Catalysts* **2023**, *13*, 744, <https://doi.org/10.3390/catal13040744> . . . . . 68

**Athanasios Lampropoulos, Stamatia A. Karakoulia, Georgios Varvoutis, Stavros Spyridakos, Vassilios Binas, Leila Zouridi, et al.**

The Combined Impact of Ni-Based Catalysts and a Binary Carbonate Salts Mixture on the  $\text{CO}_2$  Gasification Performance of Olive Kernel Biomass Fuel

Reprinted from: *Catalysts* **2023**, *13*, 596, <https://doi.org/10.3390/catal13030596> . . . . . 81

**Haiou Zhang, Yixin Zhang, Huikang Song, Yan Cui, Yingying Xue, Cai-e Wu, et al.**

Transition Metal ( $\text{Fe}_2\text{O}_3$ ,  $\text{Co}_3\text{O}_4$  and  $\text{NiO}$ )-Promoted  $\text{CuO}$ -Based  $\alpha\text{-MnO}_2$  Nanowire Catalysts for Low-Temperature CO Oxidation

Reprinted from: *Catalysts* **2023**, *13*, 588, <https://doi.org/10.3390/catal13030588> . . . . . 101

**Wenhui Zhu and Ali Reza Kamali**

Molten Salt-Assisted Catalytic Preparation of  $\text{MoS}_2/\alpha\text{-MoO}_3$ /Graphene as High-Performance Anode of Li-Ion Battery

Reprinted from: *Catalysts* **2023**, *13*, 499, <https://doi.org/10.3390/catal13030499> . . . . . 119

**Tzoulia Kraia, Georgios Varvoutis, George E. Marnellos and Michalis Konsolakis**

Unveiling the Role of In Situ Sulfidation and  $\text{H}_2\text{O}$  Excess on  $\text{H}_2\text{S}$  Decomposition to Carbon-Free  $\text{H}_2$  over Cobalt/Ceria Catalysts

Reprinted from: *Catalysts* **2023**, *13*, 504, <https://doi.org/10.3390/catal13030504> . . . . . 141

<b>Natarajan Chidhambaram, Samuel Jasmine Jecintha Kay, Saravanan Priyadharshini, Rajakantham Meenakshi, Pandurengan Sakthivel, Shanmugasundar Dhanbalan, et al.</b> Magnetic Nanomaterials as Catalysts for Syngas Production and Conversion Reprinted from: <i>Catalysts</i> <b>2023</b> , <i>13</i> , 440, <a href="https://doi.org/10.3390/catal13020440">https://doi.org/10.3390/catal13020440</a> . . . . .	<b>159</b>
<b>Andreas Kouroumlidis, Georgios Bampos, Paraskevi Panagiotopoulou and Dimitris I. Kondarides</b> Performance of Particulate and Structured Pt/TiO <sub>2</sub> -Based Catalysts for the WGS Reaction under Realistic High- and Low-Temperature Shift Conditions Reprinted from: <i>Catalysts</i> <b>2023</b> , <i>13</i> , 372, <a href="https://doi.org/10.3390/catal13020372">https://doi.org/10.3390/catal13020372</a> . . . . .	<b>195</b>

# Innovative Catalytic Materials for Environmental Remediation and Energy Applications

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## 1. Introduction

The need for low-cost and environmentally friendly energy is greater than ever nowadays due to the global population growth as well as the modern lifestyle. Considering this, research has focused on the development of novel cost-effective, eco-friendly technologies with high performance for power production and energy storage in addition to conventional technology. The reforming processes for hydrogen or syn-gas production [1,2], fuel cells producing electrical power [3–5] or chemical energy (H<sub>2</sub>, CH<sub>4</sub>, etc.) [6,7], various types of batteries [8,9] and supercapacitors [10–12] are listed among them. Environmental remediation technologies have also experienced tremendous growth over the last few decades in order to effectively remove organic contaminants from wastewater [13–15]. The activation of persulfate [16,17] and a Fenton-like process [18,19] are some indicatively advanced oxidation processes (AOPs) typically applied for the degradation of organic contaminants. The common ground for most of the abovementioned technologies, considering both energy production and storage and environmental management, is that they are based on catalytic processes. Therefore, the design and synthesis of innovative and economically affordable catalytic materials for various catalytic processes are of particular importance for their potential application. The present Special Issue includes ten research articles and one review article highlighting new perspectives on the design and implementation of innovative catalytic materials for a series of processes. The materials studied in the presented works are related to both catalytic and electrocatalytic processes, thus applying to a wide range of researchers.

## 2. Overview of Published Articles

Investigating the development of electrocatalytic materials, Zhu and Kamali (contribution 1) introduced the synthesis of the  $\alpha$ -MoO<sub>3</sub> nanoribbon structure, which is incorporated into MoS<sub>2</sub> and graphene nanosheets derived from natural graphite and MoS<sub>2</sub> minerals. They implement a rapid preparation method in order to harvest its storage properties as potential electrode material for Li-ion batteries. The proposed preparation method resulted in the formation of a molybdenum oxycarbide layer in the electrode/electrolyte interface, which can facilitate the charge and ion transfer and significantly reduces the electrochemical resistance of the electrode, thus favoring the Li-ion storage capacity (773.5 mAh g<sup>−1</sup>) compared to that obtained from the bare MoS<sub>2</sub> (176.8 mAh g<sup>−1</sup>). Next, the unique significance of the hydrogen production from the acetic acid (AA) process is underscored by Alshammari et al. (contribution 2) since it provides clean hydrogen fuel compared to reforming processes while also contributing to agricultural waste management. For this purpose, they studied the hydrogen evolution reaction (HER) over glassy carbon decorated with Au (Au/GCE) using a neutral KCl electrolyte solution in the presence of AA in a three-compartment cell, implementing the rotating disk electrode (RDE) technique. The

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proton reduction was observed at a lower overpotential ( $-0.2$  V vs. RHE), exhibiting higher current values in employed Au/GCE electrodes compared to the bare GCE electrode.

Kokkinou et al. investigated the electrochemical promotion of  $\text{CO}_2$  hydrogenation over Rh-based catalysts deposited on an  $\text{O}^{2-}$ -conducting  $\text{Y}_2\text{O}_3$ -stabilized  $\text{ZrO}_2$  (YSZ) solid electrolyte (contribution 3). This exceptionally detailed study is among the few works related to the  $\text{CO}_2$  hydrogenation reaction for  $\text{CH}_4$  production over Rh/YSZ at the laboratory scale in such narrow  $\text{CO}_2/\text{H}_2$  ratios. It was found that applying a positive or negative potential or current to the electrode acted beneficially on the electrocatalytic performance towards the  $\text{CH}_4$  production rate, thus confirming the electrochemical promotion of the catalysis (EPOC) theory.

The dry reforming of methane (DRM) towards syngas ( $\text{CO}$  and  $\text{H}_2$ ) was studied over  $\text{Nd}_{2-x}\text{Sr}_x\text{NiO}_{4\pm\delta}$  ( $0 \leq x \leq 1.4$ ) solid solutions with a  $\text{K}_2\text{NiF}_4$  structure synthesized via a freeze-drying method by Shlyakhtin et al. (contribution 4). Enhanced DRM activity was exhibited by samples with  $x = 0$  and  $x > 1$ . These two peaks observed in the DRM performance were attributed to the contribution of  $\text{Nd}_2\text{O}_3$  and  $\text{SrCO}_3$ , respectively. Hydrogen production was also investigated through the decomposition of  $\text{H}_2\text{S}$ , employing  $\text{Co}_3\text{O}_4/\text{CeO}_2$  catalytic systems (contribution 5). Kraia et al. studied the hydrogen disulfide decomposition under water in an effort to simulate the concentration of  $\text{H}_2\text{S}$  in deep water layers of the Black Sea. The significance of this work is two-fold since it combines the production of chemical energy with the environmental management of the topical ecosystem, producing multiple benefits for coastal countries. The 30 wt.%  $\text{Co}_3\text{O}_4/\text{CeO}_2$  catalyst exhibited the highest performance, which was attributed to the in situ sulfidation of cobalt species forming stable phases ( $\text{Co}_3\text{S}_4$ ,  $\text{CoS}$ ).

The purification of the  $\text{H}_2$ -rich gas stream obtained from the various reforming processes (mostly steam reforming of hydrocarbons) was conducted via a series of processes, including water gas shift (WGS) reaction, methanation reaction,  $\text{CO}$  oxidation, etc.. Kouroumliadis et al. investigated the WGS reaction at high (HT) and low temperatures (LT) over a series of modified particulates and structure Pt/ $\text{TiO}_2$  catalytic systems (contribution 6). The modification of the  $\text{TiO}_2$  support was performed with alkali- or alkaline earth metals (Na, Cs, Ca, Sr), whereas, in another series, the metal phase of Pt (0.5 wt.%) was enriched with another metal (namely Ru, Cr, Fe, Cu). Among all the tested samples, 0.5 wt.% Pt/ $\text{TiO}_2$ (Ca) exhibited the best performance and was tested further in the form of pellets and monoliths. Its high WGS activity was attributed to metal support interaction effects.

Innovative  $\text{La}_{0.8}\text{Sr}_{0.2}\text{Co}_x\text{Fe}_{1-x}\text{O}_{3-\delta}$  perovskite oxides, with a varying Co to Fe ratio ( $x = 0, 0.1, 0.2, 0.4, 0.6, 0.8, 0.9, 1$ ), were synthesized in the form of powders via the in situ combustion synthesis method and were tested via  $\text{CO}$  and propane combustion for  $\text{CO}_2$  production by Safakas et al. (contribution 7). Increasing the Co/Fe ratio resulted in an increase in the catalytic performance of both reactions, which was attributed to the occurrence of the interfacial redox mechanism. The latter was due to the enhancement of the number of catalytically active sites, strongly related to oxygen-vacant sites neighboring the Co sites, as well as to the lower redox stability of Co cations compared to Fe ones.  $\text{CO}$  oxidation was also studied over a series of transition metal oxides—this was performed on  $\text{CuO}$ -based catalytic systems, which were supported on an  $\alpha\text{-MnO}_2$  nanowire structure employing the precipitation synthesis method (contribution 8). Specifically, in this detailed work, Zhang et al. examined the effect on the catalytic performance of the type of transition metal oxide used ( $\text{Fe}_2\text{O}_3$ ,  $\text{Co}_3\text{O}_4$ ,  $\text{NiO}$ ), the loading wt.% of the oxide and the calcination temperature. The highest performance in terms of  $\text{CO}$  conversion was found for the 3 wt.%  $\text{Co}_3\text{O}_4$ —10 wt.%  $\text{CuO}/\alpha\text{-MnO}_2$  catalytic system which was calcined at  $400^\circ\text{C}$ . This enhanced catalytic activity was related to its high specific surface area, which resulted in an increase in oxygen vacancies, thus favoring the  $\text{CO}$  oxidation on the basis of the Mars–van Krevelen mechanism.

The beneficial effect of the combination of Ni-based catalytic systems with molten salt on the olive kernel– $\text{CO}_2$  gasification was thoroughly studied by Lampropoulos et al. (contribution 9). The gasification of biomass feedstock is a process of high significance since it enhances the total amount of renewable energy, whereas the exploitation of olive kernel as

feedstock is a step towards the energy independence of Mediterranean countries. The presence of molten salt improved the mass and heat transport properties, thus favoring catalytic activity.

The production of  $\alpha,\beta$ -unsaturated compounds via condensation between an aldehyde or a ketone with an active hydrogen compound (Knoevenagel reaction) employing a basic catalytic system is a very important process towards the synthesis of various chemical compounds. Chowdhury et al. investigated Knoevenagel condensation over a porous magnesium–aluminum mixed-metal phosphate, which was prepared via a hydrothermal method (contribution 10). The basic sites of the synthesized catalyst were found to enhance its efficiency towards the condensation reaction, whereas its remarkable recyclability highlighted its potential application as a catalytic system for similar reactions.

Syngas conversion reactions are very important for the production of various chemicals. The recent trends of the unique role of magnetic nanomaterials as catalytic systems for syngas production and conversion were discussed in the review article authored by Chidambaram et al. (contribution 11). Various synthesis methods and experimental parameters are discussed in detail in this very informative review paper, highlighting the role of the applied magnetic field and the beneficial effect of the addition of various modifiers.

### 3. Conclusions

Considering the published works in the current Special Issue, it is concluded that various technologies based on catalytic processes were investigated. New insights concerning both novel synthesis methods and innovative materials are revealed, paving the way for further developing power-producing and storage technologies as well as purification processes.

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### List of Contributions

1. Zhu, W.; Kamali, A.R. Molten Salt-Assisted Catalytic Preparation of  $\text{MoS}_2/\alpha\text{-MoO}_3/\text{Graphene}$  as High-Performance Anode of Li-Ion Battery. *Catalysts* **2023**, *13*, 499.
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## Article

# CO and Propane Combustion on $\text{La}_{0.8}\text{Sr}_{0.2}\text{Co}_x\text{Fe}_{1-x}\text{O}_{3-\delta}$ Perovskites: Effect of Fe-to-Co Ratio on Catalytic Activity

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**Abstract:** Perovskites are promising alternative catalysts for oxidation reactions due to their lower cost compared to noble metals, and their greater thermal stability. The catalytic oxidation of CO is essential in order to control CO emissions in a series of applications whereas the catalytic combustion of propane is considered an economical and environmentally acceptable solution for energy production and gaseous pollutant management, since propane is among the organic compounds involved in photochemical reactions. This work concerns the effect of the Co/Fe ratio in the B-sites of a series of eight  $\text{La}_{0.8}\text{Sr}_{0.2}\text{Co}_x\text{Fe}_{1-x}\text{O}_{3-\delta}$  perovskites, with  $x$  ranging from 0 to 1, on the catalytic activity towards CO and  $\text{C}_3\text{H}_8$  oxidation. The perovskite oxides were synthesized using the combustion synthesis method and characterized with respect to their specific surface areas, structures, and reduction properties. Increasing the Co/Fe ratio resulted in an increase in CO and propane conversion under both oxidative and stoichiometric conditions. The increase in Co content is considered to facilitate the formation of oxygen vacancies due to the lower redox stability of the cobalt cations compared to iron cations, favoring oxygen ion mobility and oxygen exchange between the gas phase and the oxide surface, thus enhancing the catalytic performance.

**Keywords:** CO combustion; propane combustion; CO oxidation; propane oxidation; perovskites;  $\text{La}_{0.8}\text{Sr}_{0.2}\text{Co}_x\text{Fe}_{1-x}\text{O}_{3-\delta}$ ; lanthanum strontium cobaltite ferrite

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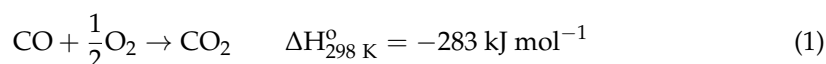
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## 1. Introduction

Increasing energy demands, mostly attributed to rising global population, result in an increase in the use of internal combustion engine vehicles that are considered as the main source of emissions of CO as well as other toxic compounds, such as  $\text{NO}_x$ , due to incomplete fossil fuel combustion [1]. These exhaust emissions are strongly related to a series of health issues and environmental problems [2,3]. The exhaust gas harmful components are reduced via oxidation in catalytic converters, using, typically, expensive noble metals as catalysts [4]. The oxidation of CO is described by the following equation [5]:



So far, the use of hybrid technology vehicles combining internal combustion engines with electric motors powered by batteries, and of electrical vehicles, powered exclusively by batteries or fuel cells with zero pollutant emissions [6], has not managed to reduce CO emissions to the desired levels, since the vast majority of human population does not have access to these advanced technologies. Nonetheless, the use of the aforementioned environmentally friendly technologies includes processes where CO production is inevitable. An indicative example is the production of significant amounts of CO in the hydrocarbons reforming processes for  $\text{H}_2$  production to feed  $\text{H}_2$ -fuelled proton exchange membrane fuel cells (PEMFCs) [7,8]. The reduction in CO concentration to the required level (<50 ppm) to



avoid poisoning of the Pt-based electrocatalysts typically used in PEMFCs is achieved via the water–gas shift reaction, followed by preferential oxidation of CO in the presence of  $H_2$  [9].

Considering the above, the catalytic CO oxidation is essential in both conventional and alternative power applications. Catalysts typically used for CO oxidation are noble metal-based materials [10], which are characterized by high cost and low resistance to high CO concentration [11]. Towards addressing these issues, the development of alternative catalytic materials with enhanced resistance to CO poisoning, low cost, and similar activity to that of noble metal-based catalysts has attracted significant research interest [11,12].

Perovskite oxides of the  $ABO_3$  type, where A-sites are occupied by alkaline earth or alkali metal cations and B-sites by transition metal cations, are considered as alternative catalytic materials for CO oxidation, exhibiting good activity and resistance to poisoning [12–14]. The chemical composition and structure of perovskite oxides play a crucial role in their catalytic performance [12–16], as they affect their redox [17,18] and/or acid–base [19] properties. The catalytic activity of a perovskite depends primarily on the transition metals occupying the B-sites, whereas A-sites are considered to play a secondary role in catalytic performance [12,13,20]. Perovskitic oxides with La or other rare earth metals in the A-sites and Co, Fe, Ni, or Mn in the B-sites have been reported as the most active for CO oxidation [12,16]. In addition to parameters that typically affect catalytic activity, such as the nature of the metal cations and the catalytic surface area [20], their enhanced catalytic performance has been attributed to structural defects and rapid surface oxygen exchange [12].

CO oxidation, as well as other oxidation reactions, on perovskite oxides can proceed via two different catalytic mechanisms, namely, the “suprafacial” and “intrafacial” mechanisms [12,14–16], which can also operate concurrently [21]. According to the suprafacial mechanism, CO or an organic molecule is oxidized by oxygen adsorbed on the catalytic surface from the gas phase, whereas the perovskite surface acts as a fixed template providing atomic orbitals with suitable energy and symmetry to facilitate the adsorption and surface reaction of the reactants. A Langmuir–Hinshelwood or an Eley–Rideal kinetic model can be used in this case, depending on whether the oxidized reactant is adsorbed or reacts directly from the gas phase. According to the intrafacial mechanism, which resembles the Mars–van Krevelen surface redox model [22], the lattice oxygen of the perovskite oxide participates in the CO or organic molecule oxidation step, and the reaction is carried out via a redox cycle where the consumed lattice oxygen is afterwards replenished by incorporation in the resultant surface oxygen vacancies of oxygen from the gas phase in the rate determining step. Provided that they have sufficient mobility, oxygen anions migrating from the bulk can also fill in the surface oxygen vacancies, thus virtually participating in the oxidation process, contrary to the suprafacial mechanism where only surface oxygen species participate in the reaction [14,16]. In general, the suprafacial mechanism is expected for low-temperature processes in which removal/incorporation of oxygen from/into the perovskite lattice is much slower than adsorption/desorption and reactions between adsorbed surface species [14–16]. The intrafacial mechanism, on the other hand, is preferably followed at relatively higher temperatures, where the mobility of lattice oxygen and the surface oxygen exchange are favored [14–16].

Partial substitution of the metal cations at the A- and B-sites with metal cations of different oxidation numbers results in alteration of the oxygen sub-stoichiometry with parallel formation of vacant lattice sites or/and change in the oxidation state of the transition metal ions at the B-sites or/and formation of positively charged holes in order to maintain overall electro-neutrality, while the perovskitic structure remains stable [5,14]. This modification can enhance the catalytic performance of the perovskite oxide. For example, in  $La_{1-x}Sr_xMnO_3$  perovskites, the  $La^{3+}$  cations are partially substituted by  $Sr^{+2}$  cations at the A-sites, causing a deviation from the electro-neutrality, which is counterbalanced by partial transformation of  $Mn^{3+}$  to  $Mn^{4+}$  at the B-sites [5]. On the other hand, in  $La_{1-x}Sr_xFeO_3$  perovskites, partial substitution of lanthanum by strontium at the A-sites is

followed by the formation of oxygen vacancies as the main mechanism to maintain overall electro-neutrality [23,24]. In general, partial substitution of both A- and B-sites in a  $\text{ABO}_3$  perovskite by an alkaline earth metal  $\text{A}'$  and another transition metal  $\text{B}'$ , respectively, to form a  $\text{AA'BB'O}_3$  type perovskite, results both in change in the oxidation state of the metal ions at the B-sites and in the formation of lattice oxygen vacancies, facilitating oxygen dissociation on the surface, increasing lattice oxygen anion mobility, and improving the ionic conductivity of the parent material [14,25].

Combining two catalytically active transition metals at the B-sites of a perovskitic oxide can result in enhanced catalytic activity owing to a synergistic effect between the two metals, which alters the adsorptive properties of the perovskite [5]. Co, Mn, and Fe cations are typically found at the B-sites of the perovskite catalysts [5]. It is generally accepted that the co-presence of cations of two different transition metals at the B-sites facilitates electron transfer in the redox catalytic cycle, which enhances the reducibility of the perovskite oxide and improves its catalytic performance [5]. Zhang et al. [26] used oxygen temperature-programmed desorption ( $\text{O}_2$ -TPD) to study the effect of partial substitution of La by Sr and Co by Fe at the A- and B-sites, respectively, on the desorption properties of the perovskite  $\text{La}_{1-x}\text{Sr}_x\text{Co}_{1-y}\text{Fe}_y\text{O}_3$ . They found that coexistence of Co and Fe was beneficial for the oxygen adsorption/desorption properties of the perovskite, thus enhancing its catalytic activity towards n-butane complete oxidation. Oxygen adsorption/desorption at temperatures lower than  $300^\circ\text{C}$  was favored whereas partial substitution of La by Sr at the A-sites significantly enhanced the activity of the perovskite. Scott et al. [27] studied the effect of temperature, chemical composition, and oxygen partial pressure on oxygen sub-stoichiometry  $\delta$  of  $\text{La}_{1-x}\text{Sr}_x\text{Co}_{1-y}\text{Fe}_y\text{O}_{3-\delta}$ . They found that  $\delta$  increased with increasing temperature, decreasing oxygen partial pressure, and increasing Sr and Co content at the A- and B-sites, respectively. Lankhorst and ten Elshof [28] investigated the effect of partial substitution of Co by Fe at the B-sites of  $\text{La}_{0.2}\text{Sr}_{0.8}\text{Co}_{1-y}\text{Fe}_y\text{O}_{3-\delta}$  ( $y = 0\text{--}0.6$ ) on oxygen sub-stoichiometry  $\delta$  and found that the  $\delta$  value decreased with increasing Fe/Co ratio. This was attributed to an increase in the binding energy of  $\text{O}^{2-}$  in the perovskite lattice, which favors the formation of holes over oxygen vacancies [28].

Levasseur and Kaliaguine [29] studied the effect of the Co/Fe ratio at the B-sites of  $\text{La}_{1-x}\text{Ce}_x\text{Co}_{1-y}\text{Fe}_y\text{O}_3$  ( $x = 1, 0.9$  and  $y = 0, 0.2, 0.4, 1$ ) on catalytic activity for methanol, CO, and  $\text{CH}_4$  oxidation. Partial substitution of La by Ce at the A-sites caused an enhancement of the catalytic performance. Increasing Fe content resulted in a decrease in the catalytic activity and in a decrease in the  $\beta$ -oxygen peak in the  $\text{O}_2$ -TPD curves, accompanied by a shift in the desorption peaks of all oxygen species to higher temperatures. Moreover, decreasing the Co/Fe ratio resulted in an increase in the reduction temperature of  $\text{Co}^{3+}$  and  $\text{Co}^{2+}$  species to  $\text{Co}^{2+}$  and  $\text{Co}^0$  species, respectively, as manifested by  $\text{H}_2$  temperature-programmed reduction measurements. Therefore, it was concluded that an increase in the Fe content reduces the redox activity of the B-sites and decreases the lattice oxygen mobility. Similar results were reported by Tanaka et al. [30] concerning the catalytic activity towards the oxidation of a mixture of hydrocarbons, NO, and CO over  $\text{La}_{0.9}\text{Ce}_{0.1}\text{Co}_{1-y}\text{Fe}_y\text{O}_3$  ( $y = 0, 0.2, 0.4, 0.6, 0.8, 1$ ). Isupova et al. [31] observed a maximum CO oxidation activity of  $\text{La}_{0.7}\text{Sr}_{0.3}\text{Co}_{1-y}\text{Fe}_y\text{O}_3$  ( $y = 0, 0.05, 0.1, 0.7$ ) for a Co/Fe atomic ratio equal to 0.95/0.05. This behavior was attributed to an increase in the number of structural defects which in turn resulted in an increase in the density of surface defects, thus favoring CO oxidation reaction on the basis of its mechanism.

Catalytic combustion of propane, described by Equation (2), is also a reaction of significant research interest, both for energy production, especially in areas where there is no access to natural gas, and for management of air pollutants since propane belongs to volatile organic compounds (VOCs) [32].



Noble metal-based catalysts are considered highly efficient towards propane combustion and have been extensively studied [33–38]. However, the high cost of noble metals has motivated the development of alternative noble metal-free catalytic systems. Ma et al. [39]

investigated propane oxidation on  $\text{Co}_3\text{O}_4$  nanorods, as alternative to  $\text{Pt}/\text{Al}_2\text{O}_3$ . They highlighted the differences in propane combustion mechanism over the two catalysts, reporting a Langmuir–Hinshelwood mechanism for  $\text{Co}_3\text{O}_4$  nanorods and an Eley–Rideal mechanism for  $\text{Pt}/\text{Al}_2\text{O}_3$ . Perovskites have also been used as catalysts for propane combustion, although the corresponding studies are significantly fewer than those concerning CO oxidation [14]. Klvana et al. [40] investigated the effect of the synthesis method of  $\text{La}_{0.66}\text{Sr}_{0.34}\text{Co}_{0.2}\text{Fe}_{0.8}\text{O}_3$  and specific surface area on its activity for propane combustion. Kinetic experiments over a wide range of gas phase compositions indicated a Mars–van Krevelen mechanism [22,40,41]. Alifanti et al. [42] compared methane and propane oxidation on  $\text{La}_{1-x}\text{Sr}_x\text{M}_{1-y}\text{M}'_y\text{O}_{3-\delta}$  (M: Mn, Cu, Ni, Co and M': Ni, Fe), focusing on the relative role of specific surface area and oxygen mobility. The effect of partial substitution of La by Sr, Ce, and Ca at the A-sites has been studied in propane oxidation on  $\text{La}_{1-x}\text{Sr}_x\text{CoO}_3$  [43], on  $\text{La}_{1-x}\text{Sr}_x\text{FeO}_3$ ,  $\text{La}_{1-x}\text{Ce}_x\text{FeO}_3$  and  $\text{La}_{1-x}\text{Ce}_x\text{CoO}_3$  [44], and on  $\text{La}_{1-x}\text{Ca}_x\text{CoO}_3$  [25]. Merino et al. [45] studied the effect of the partial substitution of Co by Fe at the B-sites in propane combustion on  $\text{LaCo}_{1-y}\text{Fe}_y\text{O}_{3\pm\lambda}$  ( $y = 0, 0.1, 0.3, 0.5$ ). Partial substitution of Co by Fe by 10% ( $y = 0.1$ ) was found to favor the catalytic performance, whereas a further increase in the Fe content resulted in a gradual reduction in the catalytic activity [45]. Song et al. [46] investigated the kinetics of propane oxidation on  $\text{La}_{0.66}\text{Sr}_{0.34}\text{Ni}_{0.3}\text{Co}_{0.7}\text{O}_3$  and proposed an extended Mars–van Krevelen kinetic model, taking also into account the inhibiting effect of adsorbed  $\text{CO}_2$  and  $\text{H}_2\text{O}$  products.

Considering the abovementioned studies of CO and propane combustion on perovskite oxides, it can be concluded that relevant research interest has been mainly focused on the investigation of the catalytic effect of the transition metals occupying the B-sites, with particular interest in Co and Fe. Along this direction, eight (8) perovskite oxides  $\text{La}_{0.8}\text{Sr}_{0.2}\text{Co}_x\text{Fe}_{1-x}\text{O}_{3-\delta}$ , with a fixed La/Sr ratio at the A-sites and a varying Co and Fe content at the B-sites ( $x = 0, 0.1, 0.2, 0.4, 0.6, 0.8, 0.9, 1$ ) were synthesized via the combustion synthesis method and tested for their catalytic activity towards CO and propane combustion. The synthesized oxides were characterized as it concerns their specific surface area, structure, and reducibility in  $\text{H}_2$  atmosphere. The observed differences in catalytic activity among the tested perovskites were mainly correlated with differences in oxygen vacancies, surface oxygen exchange, and oxygen ion mobility induced by changing the relative content of Co and Fe at the B-sites. The novelty of the present work lies on the fact that, to the best of our knowledge, it is the first systematic study of the effect of the Co/Fe ratio on the catalytic performance of La-Sr-Co-Fe perovskites for both CO and propane total oxidation, two reactions of significant environmental and technological interest, allowing comparison of the activity trends for the two reactions.

## 2. Results

### 2.1. Physicochemical and Structural Characterization

The composition, the notation, and the measured via  $\text{N}_2$  physical adsorption (BET method) SSA values of the synthesized perovskites are shown in Table 1. No significant differences were observed between their nominal composition and their stoichiometry determined via inductively coupled plasma optical emission spectroscopy (ICP-OES). The SSA varied from  $4.1 \text{ m}^2 \text{ g}^{-1}$  for LSCF\_8291 to  $7.9 \text{ m}^2 \text{ g}^{-1}$  for LSCF\_8219. The low SSAs are attributed to the elevated calcination temperature ( $900^\circ\text{C}$ ) used to obtain the perovskite structure [47].

The XRD spectra of the eight synthesized perovskites are presented in Figure 1. Six of them (LSC, LSCF\_8282, LSCF\_8264, LSCF\_8246, LSCF\_8228, and LSF) have been already presented in a previous work of our group [47]. After identification of the formed phases using ICDD data files, the formation of the perovskite phase was confirmed (main peak at  $2\theta$  between  $32^\circ$  and  $34^\circ$ ) without the presence of secondary phases at detectable levels. A gradual shift in all XRD peaks towards lower  $2\theta$  values was observed with increasing partial substitution of Co by Fe (Figure 1b). This shift was accompanied by a change in the main peak from doublet ( $0.4 \leq x \leq 1$ ) to single ( $x = 0, 0.1, 0.2$ ), indicating a change in the  $\text{La}_{0.8}\text{Sr}_{0.2}\text{Co}_x\text{Fe}_{1-x}\text{O}_{3-\delta}$  perovskite structure from rhombohedral to orthorhombic [25,48,49].

This is in accordance with the results of Tai et al. [49] for  $\text{La}_{0.8}\text{Sr}_{0.2}\text{Co}_{1-y}\text{Fe}_y\text{O}_3$  ( $0 \leq y \leq 1$ ) sintered in air at 1250 to 1350 °C, who reported that partial substitution of Co by Fe to an iron percentage of 80% or higher ( $y = 0.8, 0.9, 1$ ) resulted in a change in the perovskite unit cell from rhombohedral to orthorhombic. Similarly, Natile et al. [48] reported a change from rhombohedral to orthorhombic structure for  $\text{La}_{0.6}\text{Sr}_{0.4}\text{Co}_{1-y}\text{Fe}_y\text{O}_{3-\delta}$  perovskites ( $y = 0.2, 0.5, 0.8$ ) calcined at 800 °C, but for a lower Fe content ( $y \geq 0.5$ ), which implies that the La/Sr ratio at the A-sites and, possibly, the thermal treatment conditions can affect the Co/Fe ratio for which the aforementioned change in unit cell geometry occurs. The observed gradual shift in the XRD peaks towards higher  $2\theta$  values with increasing partial substitution of Fe by Co (Figure 1) indicates a contraction of the perovskite unit cell, which can be attributed to the substitution of  $\text{Fe}^{3+}$  by  $\text{Co}^{3+}$ , the latter having a smaller ionic radius [45,48,50]. Moreover, this shift becomes relatively smaller with increasing Co content (Figure 1b), which implies a smaller reduction in the unit cell size [47]. This behavior has also been reported for  $\text{LaCo}_x\text{Fe}_{1-x}\text{O}_{3-\delta}$ , associated with changes in the relative number of  $\text{Co}^{2+}$  to  $\text{Co}^{3+}$  and  $\text{Fe}^{4+}$  to  $\text{Fe}^{3+}$  accompanying the substitution of  $\text{Fe}^{3+}$  by  $\text{Co}^{3+}$  [50].

**Table 1.** Composition, notation, specific surface area (SSA), and average crystallite size of the synthesized perovskites  $\text{La}_{0.8}\text{Sr}_{0.2}\text{Co}_x\text{Fe}_{1-x}\text{O}_{3-\delta}$ .

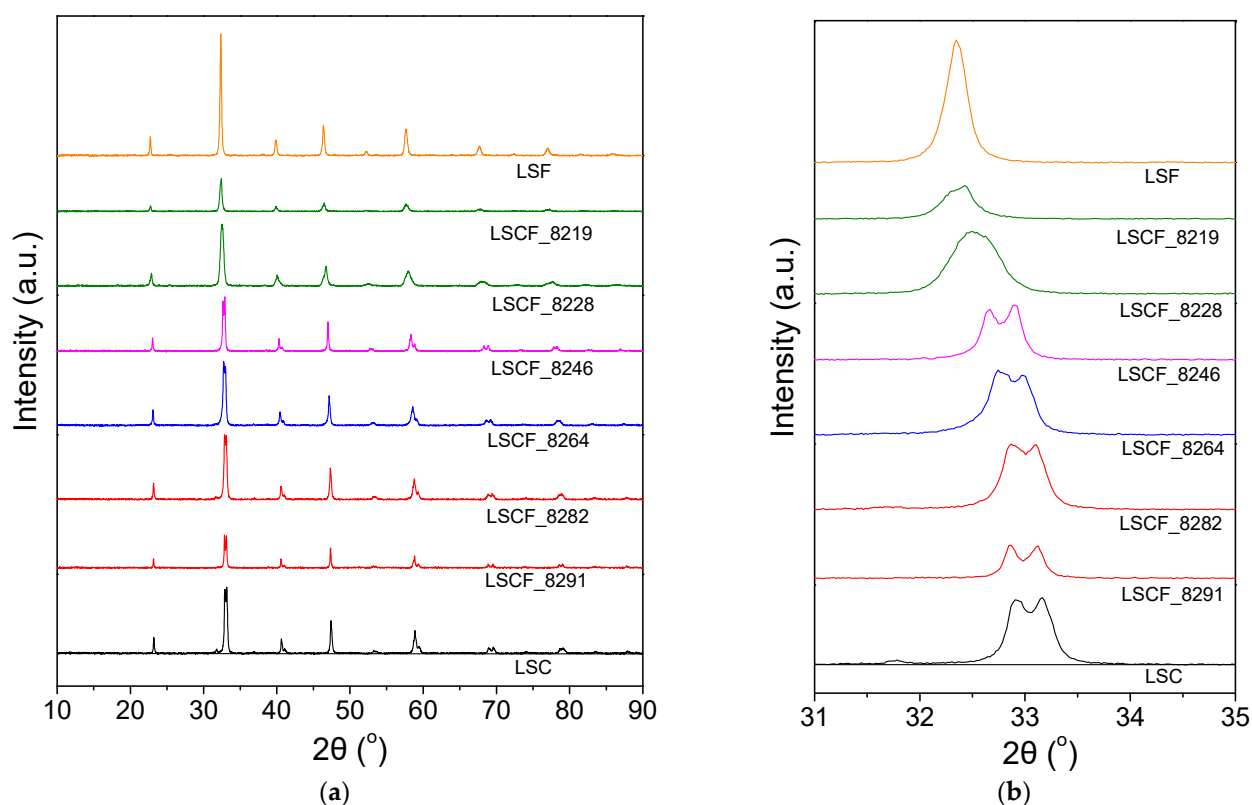
Perovskite	Notation	SSA ( $\text{m}^2 \text{g}^{-1}$ )	Crystallite Size (nm)
$\text{La}_{0.8}\text{Sr}_{0.2}\text{FeO}_{3-\delta}$	LSF	7.2 <sup>1</sup>	29.1
$\text{La}_{0.8}\text{Sr}_{0.2}\text{Co}_{0.1}\text{Fe}_{0.9}\text{O}_{3-\delta}$	LSCF_8219	7.9	19.7
$\text{La}_{0.8}\text{Sr}_{0.2}\text{Co}_{0.2}\text{Fe}_{0.8}\text{O}_{3-\delta}$	LSCF_8228	5.6 <sup>1</sup>	16.9
$\text{La}_{0.8}\text{Sr}_{0.2}\text{Co}_{0.4}\text{Fe}_{0.6}\text{O}_{3-\delta}$	LSCF_8246	4.7 <sup>1</sup>	50.2
$\text{La}_{0.8}\text{Sr}_{0.2}\text{Co}_{0.6}\text{Fe}_{0.4}\text{O}_{3-\delta}$	LSCF_8264	6.8 <sup>1</sup>	32.5
$\text{La}_{0.8}\text{Sr}_{0.2}\text{Co}_{0.8}\text{Fe}_{0.2}\text{O}_{3-\delta}$	LSCF_8282	5.5 <sup>1</sup>	32.5
$\text{La}_{0.8}\text{Sr}_{0.2}\text{Co}_{0.9}\text{Fe}_{0.1}\text{O}_{3-\delta}$	LSCF_8291	4.1	60.2
$\text{La}_{0.8}\text{Sr}_{0.2}\text{CoO}_{3-\delta}$	LSC	5.7 <sup>1</sup>	34.2

<sup>1</sup> ref. [47].

The average crystallite size, estimated via application of the Scherrer equation [51,52] for the XRD peak located at  $2\theta$  between 46° and 48°, revealed a significant difference among the synthesized materials (Table 1). The largest crystallite size, equal to 60.2 nm, was calculated for LSCF\_8291, whereas the smallest, equal to 16.9 nm, was calculated for LSCF\_8228. Although no clear trend was observed, it could be argued that increasing the Fe content results in an increase in the SSA and a decrease in the average crystallite size, as also reported for  $\text{La}_{0.6}\text{Sr}_{0.4}\text{Co}_{1-y}\text{Fe}_y\text{O}_{3-\delta}$  by Natile et al. [48]. The observed changes in the crystallite size were accompanied by changes in the lattice strain,  $\epsilon$  (%), which was calculated using the Williamson–Hall method [52,53]. Specifically, the calculated lattice strain values for the synthesized perovskites follow the increasing order, LSCF\_8291 (0.14%) < LSCF\_8246 (0.15%) < LSC (0.24%) < LSCF\_8282 (0.25%) < LSCF\_8264 (0.26%) < LSF (0.28%) < LSCF\_8219 (0.38%) < LSCF\_8228 (0.4%), which corresponds to a decreasing order of crystallite size (Table 1).

## 2.2. Investigation of the Perovskite Reducibility

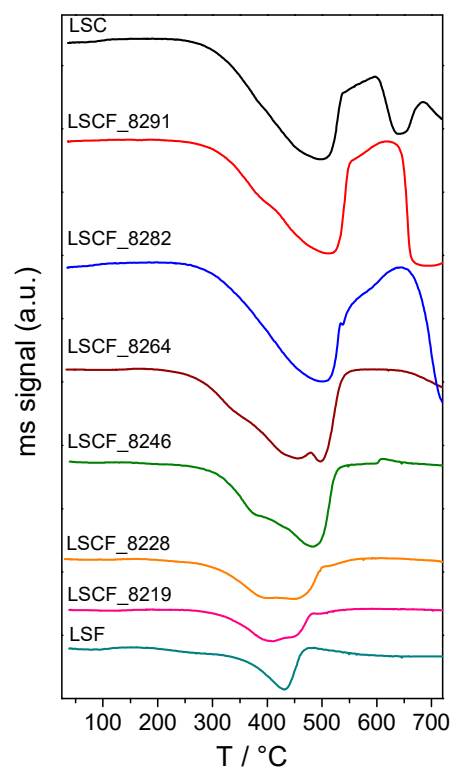
The synthesized perovskites were characterized with respect to their reducibility using  $\text{H}_2$  temperature-programmed reduction ( $\text{H}_2$ -TPR). The recorded mass spectrometer signal (ms signal) for  $\text{H}_2$  ( $m/z = 2$ ) as a function of temperature (TPR profile) is shown in Figure 2 for all tested samples. The main feature of the TPR curves is a broad inverse peak that starts to develop at temperatures between ca. 200 °C and 250 °C depending on the perovskite composition and which seems to consist of more than one peak, clearly for Co/Fe ratio in the range 6/4 to 1/9. For Co/Fe ratios larger than 6/4, additional reduction features appear at temperatures higher than ca. 595 °C that were not completed due to limitations of the experimental setup, with the exception of a peak located between ca. 595 °C and 685 °C in the TPR profile of the LSC oxide.



**Figure 1.** (a) XRD patterns of the synthesized perovskite oxides. (b) Detailed view of the XRD patterns in the  $2\theta$  range from  $31^\circ$  to  $35^\circ$ .

Interpretation of the  $H_2$ -TPR features of LSCF perovskite oxides depends on the temperature range of their appearance. The reduction of Fe is typically performed in two consecutive steps, i.e., reduction of  $Fe^{4+}$  to  $Fe^{3+}$  at  $350$  to  $450^\circ C$  and subsequent reduction of  $Fe^{3+}$  to  $Fe^{2+}$  and possibly further reduction to metallic  $Fe^0$ , at temperatures higher than  $500^\circ C$  [54]. The reduction of cobalt cations is also carried out in two steps,  $Co^{3+}$  being reduced to  $Co^{2+}$  and  $Co^{2+}$  to  $Co^0$  at temperatures lower and higher than  $500^\circ C$ , respectively [54]. However, according to García-López et al. [55], the reduction of  $Fe^{3+}$  to  $Fe^{2+}$  can take place at temperatures lower than  $400^\circ C$  or in the temperature range where reduction of  $Co^{3+}$  occurs, resulting in overlapping of the corresponding TPR peaks. Merino et al. [45] also observed, in TPR profiles of  $LaCo_{1-y}Fe_yO_3$  oxides, the appearance of a peak in the temperature range  $355$ – $385^\circ C$ , which they attributed to the reduction of the  $Fe^{4+}$  species.

In the present work, broad reduction peaks were recorded for all tested perovskites that could be explained by the potential participation of the bulk lattice oxygen in the reduction reactions, since the surface oxygen is consumed rapidly with increasing temperature. As shown in Figure 2, the increase in the Co/Fe ratio (from LSF to LSC) was accompanied by a shift in the onset reduction temperature to lower values. This can be attributed to the facilitation of the surface lattice oxygen release, associated with the lower redox stability of cobalt cations in LSCF compared to iron cations [56,57]. Moreover, the parallel increase in the number of oxygen ion vacancies and oxygen ion mobility [12,14,58] facilitates the bulk lattice oxygen diffusion to the oxide surface, thus favoring the reaction with hydrogen. The appearance of a doublet peak for LSCF\_8219 to LSCF\_8264 can be associated with the onset of the reduction of  $Co^{3+}$  to  $Co^{2+}$ , occurring parallel to the reduction of  $Fe^{4+}$  to  $Fe^{3+}$  [45]. For LSCF\_8282 and LSCF\_8291, the peak associated with the reduction of  $Fe^{4+}$  to  $Fe^{3+}$  is not discernible, as it is presumably overlapped by the dominant peak associated with the reduction of  $Co^{3+}$  to  $Co^{2+}$  [45].

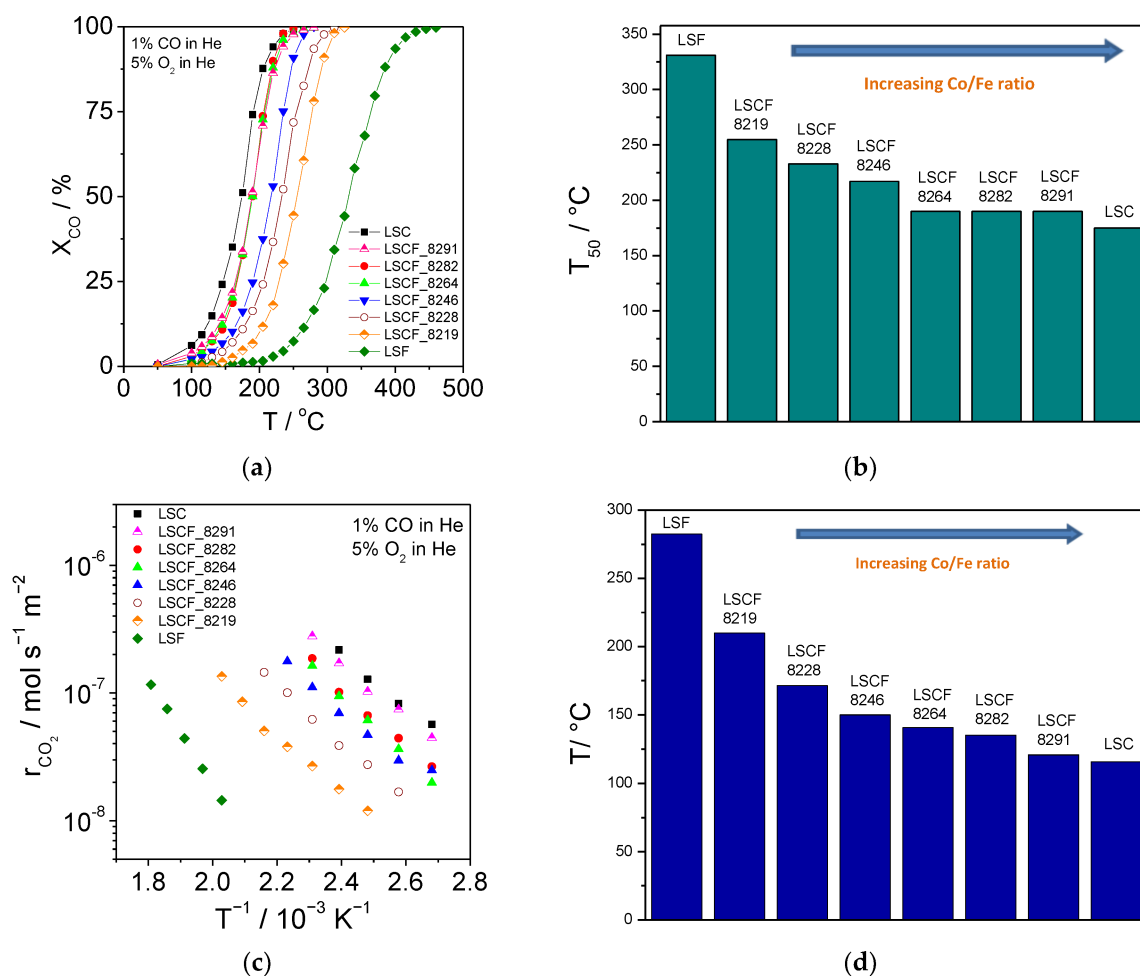


**Figure 2.** H<sub>2</sub> temperature-programmed reduction profiles of the synthesized perovskites.

### 2.3. Catalytic Activity for CO Combustion

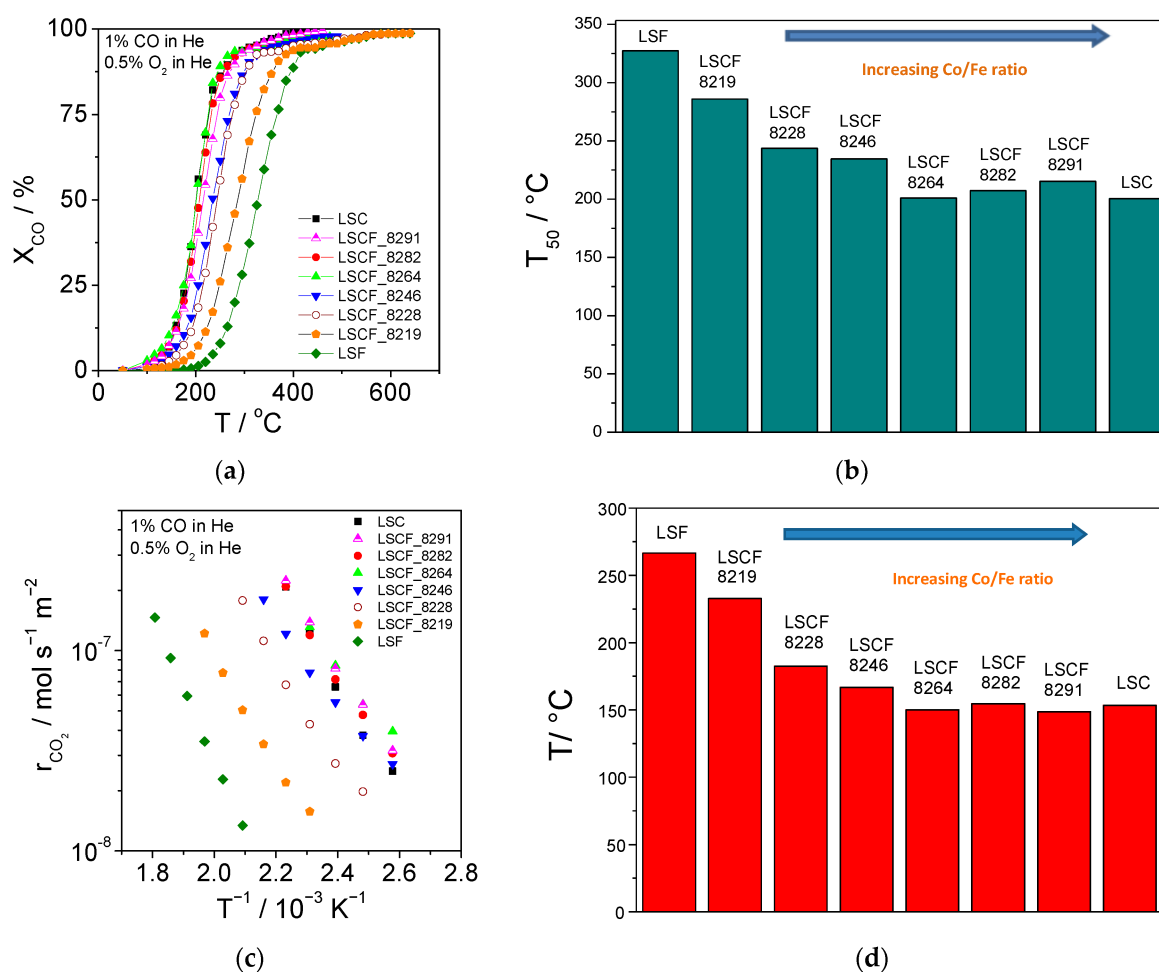
In Figure 3a, the CO conversion ( $X_{CO}$ ) vs. temperature curves obtained under oxidative conditions (feed composition: 1% CO/5% O<sub>2</sub>/balance He) for the synthesized perovskites are presented. As shown in the figure, complete CO conversion was achieved for all oxides in the temperature range between 265 °C and 460 °C, whereas at each temperature conversion increased with increasing Co/Fe ratio at the B-sites. In Figure 3b, the light-off temperatures  $T_{50}$  for the tested materials, i.e., the temperatures corresponding to a CO conversion equal to 50%, are compared. Increasing the Co/Fe ratio resulted in a gradual decrease in  $T_{50}$ , which was more pronounced for Co/Fe ratios equal or smaller than 6/4. As shown in the figure, the  $T_{50}$  value was practically the same for the LSCF\_8264, LSCF\_8282, and LSCF\_8291 perovskites, which is also evident by comparing the corresponding CO conversion curves (Figure 3a).

Figure 3c shows, in the form of Arrhenius plots, the temperature dependence of the CO<sub>2</sub> production rate  $r_{CO_2}$  for the tested perovskites, under oxidative conditions. The CO<sub>2</sub> production rate was measured under practically differential conditions and was normalized to the SSA of each sample to take into account the existing differences in the specific surface area of the tested catalysts (Table 1) and compare their intrinsic activity, assuming that the change in the number of active sites follows the change in SSA. By increasing the Co/Fe ratio, the same  $r_{CO_2}$  was achieved at lower temperatures, which implies enhancement of the intrinsic catalytic activity. In order to highlight the differences in the intrinsic catalytic activity of the tested perovskites, the temperatures corresponding to  $r_{CO_2}$  equal to  $10^{-7}$  mol s<sup>-1</sup> m<sup>-2</sup> (Figure 3c) are compared in Figure 3d. As shown in the figure, this temperature decreased from 283 °C for LSF to 116 °C for LSC, indicating that among the tested perovskites (Table 1) LSC and LSF were the most active and the less active, respectively, for CO oxidation in terms of intrinsic activity, in agreement with the conclusions drawn by comparing the  $T_{50}$  values (Figure 3b).



**Figure 3.** CO combustion on  $\text{La}_{0.8}\text{Sr}_{0.2}\text{Co}_x\text{Fe}_{1-x}\text{O}_{3-\delta}$  perovskites for oxidative feed conditions (1%CO/5% $\text{O}_2$ /balance He): (a) CO conversion,  $X_{\text{CO}}$ , as a function of temperature, and (b) comparison of the corresponding light-off temperatures,  $T_{50}$ . (c) Temperature dependence of the  $\text{CO}_2$  production rate,  $r_{\text{CO}_2}$  (Arrhenius plots), measured under practically differential conditions, and (d) comparison of the temperatures corresponding to  $r_{\text{CO}_2}$  equal to  $10^{-7} \text{mol s}^{-1} \text{m}^{-2}$ .

In Figure 4, the catalytic performance of the synthesized  $\text{La}_{0.8}\text{Sr}_{0.2}\text{Co}_x\text{Fe}_{1-x}\text{O}_{3-\delta}$  perovskites for CO combustion under stoichiometric feed conditions (1% CO/0.5%  $\text{O}_2$ /balance He) is compared. Figure 4a shows the dependence of CO conversion ( $X_{\text{CO}}$ ) on temperature. As shown in the figure, complete conversion of CO is reached for temperatures ranging between ca. 430  $^\circ\text{C}$  and 640  $^\circ\text{C}$ , which are considerably higher than the corresponding ones for oxidative feed conditions (Figure 3a). This difference implies a positive reaction order with respect to oxygen, considering the much lower percentage of  $\text{O}_2$  in the feed under stoichiometric conditions (0.5%) compared to that under oxidative conditions (5%). As in the latter case, decreasing the Fe content at the B-sites of the LSCF perovskites resulted in an increase in the CO conversion for the same temperature for  $\text{Co/Fe} \leq 6/4$ , whereas for higher Co/Fe ratios, the differences in CO conversion were small (Figure 4a). Similarly, as shown in Figure 4b,  $T_{50}$  decreased from ca. 325  $^\circ\text{C}$  for the LSF to ca. 200  $^\circ\text{C}$  for the LSCF\_8264 and remained practically constant by further decreasing the Fe content (with parallel increase in the Co content) to zero (LSC sample).



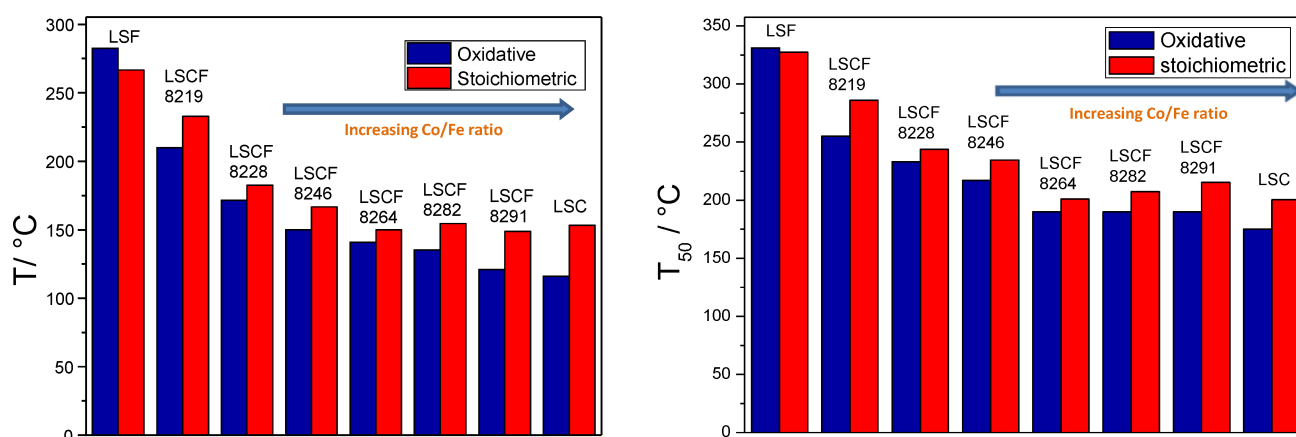
**Figure 4.** CO combustion on  $\text{La}_{0.8}\text{Sr}_{0.2}\text{Co}_x\text{Fe}_{1-x}\text{O}_{3-\delta}$  perovskites for stoichiometric feed conditions (1% CO/0.5%  $\text{O}_2$ /balance He): (a) CO conversion,  $X_{\text{CO}}$ , as a function of temperature, and (b) comparison of the corresponding light-off temperatures,  $T_{50}$ . (c) Temperature dependence of the  $\text{CO}_2$  production rate,  $r_{\text{CO}_2}$  (Arrhenius plots), measured under practically differential conditions, and (d) comparison of the temperatures corresponding to  $r_{\text{CO}_2}$  equal to  $10^{-7} \text{mol s}^{-1} \text{m}^{-2}$ .

Figure 4c shows, in the form of Arrhenius plots, the temperature dependence of  $r_{\text{CO}_2}$  for the tested perovskites, as measured under practically differential conditions and for a stoichiometric CO/ $\text{O}_2$  ratio in the feed (1% CO/0.5%  $\text{O}_2$ /balance He). By increasing the Co/Fe ratio up to 6/4, the same  $r_{\text{CO}_2}$  was obtained at lower temperatures, indicating an increase in the intrinsic catalytic activity, whereas for higher Co/Fe ratios, the effect was not significant (Figure 4c). This is clearly shown in Figure 4d, where the temperatures corresponding to  $r_{\text{CO}_2}$  equal to  $10^{-7} \text{mol s}^{-1} \text{m}^{-2}$  are presented. As shown in the figure, this rate value was obtained at  $267^{\circ}\text{C}$  for LSF and at  $150^{\circ}\text{C}$  for LSCF\_8264, whereas for the perovskite oxides with higher Co/Fe ratios, the corresponding temperature remained practically constant, varying between 150 and  $154^{\circ}\text{C}$  (Figure 4d).

In Figure 5, the catalytic performance for CO combustion of the synthesized  $\text{La}_{0.8}\text{Sr}_{0.2}\text{Co}_x\text{Fe}_{1-x}\text{O}_{3-\delta}$  perovskites under oxidative and stoichiometric conditions is compared on the basis of the temperature required to obtain a  $r_{\text{CO}_2}$  equal to  $10^{-7} \text{mol s}^{-1} \text{m}^{-2}$  (Figure 5a) and on the basis of the light-off temperature,  $T_{50}$  (Figure 5b). As shown in Figure 5a, the temperature corresponding to a  $\text{CO}_2$  production rate of  $10^{-7} \text{mol s}^{-1} \text{m}^{-2}$  decreased with increasing Co/Fe ratio under oxidative feed conditions over the entire range of Co/Fe ratios (LSF to LSC), whereas under stoichiometric feed conditions it decreased up to a Co/Fe ratio equal to 6/4, remaining practically the same for higher Co content. The same trend was observed concerning the  $T_{50}$  values (Figure 5b). Moreover,



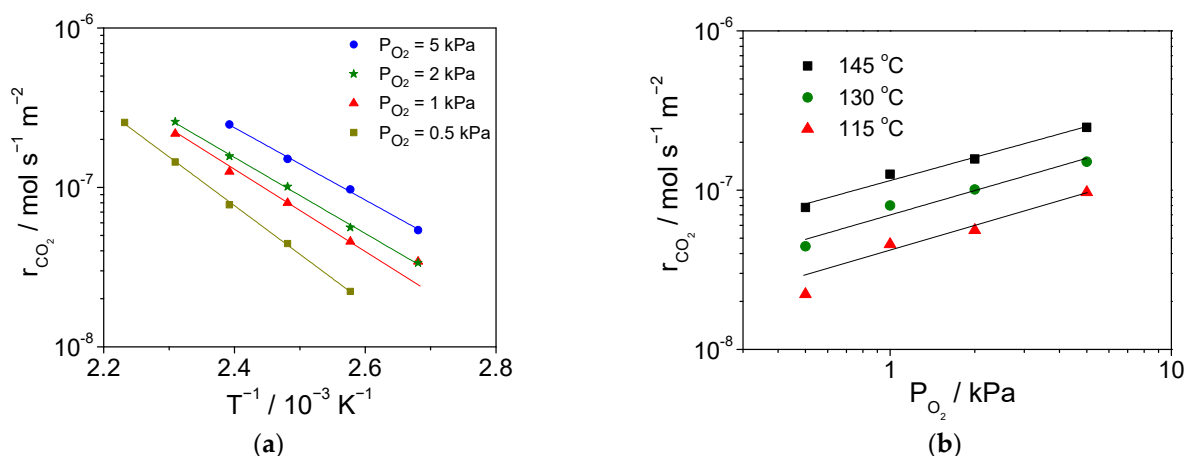
with the exception of the less active LSF oxide, both the temperature corresponding to  $r_{\text{CO}_2}$  equal to  $10^{-7} \text{ mol s}^{-1} \text{ m}^{-2}$  and  $T_{50}$  for each of the tested perovskites were lower under oxidative conditions compared to stoichiometric conditions, implying a higher catalytic performance in the former case. Considering the above observations, it can be concluded that the catalytic activity for CO oxidation, under both oxidative and stoichiometric feed conditions, depends strongly on the relative content of Co and Fe at the B-sites of the  $\text{La}_{0.8}\text{Sr}_{0.2}\text{Co}_x\text{Fe}_{1-x}\text{O}_{3-\delta}$  perovskite oxides. Increasing the Co/Fe ratio results in an increase in the catalytic activity for CO combustion, more pronounced under oxidative reaction conditions. The lowest and highest activities among the tested materials were exhibited by the LSF and the LSC perovskites, respectively.



**Figure 5.** CO combustion on  $\text{La}_{0.8}\text{Sr}_{0.2}\text{Co}_x\text{Fe}_{1-x}\text{O}_{3-\delta}$  perovskites under oxidative (1% CO/5%  $\text{O}_2$ /balance He) and stoichiometric (1% CO/0.5%  $\text{O}_2$ /balance He) feed conditions: (a) Temperatures corresponding to a  $\text{CO}_2$  production rate of  $10^{-7} \text{ mol s}^{-1} \text{ m}^{-2}$ , measured under practically differential conditions and (b) light-off temperatures,  $T_{50}$ .

Kinetic measurements with varying  $\text{O}_2$  partial pressures were conducted for the most active LSC catalyst, under practically differential conditions. Figure 6a shows, in the form of Arrhenius plot, the temperature dependence of the  $\text{CO}_2$  production rate ( $r_{\text{CO}_2}$ ), normalized to the SSA, for four different  $\text{O}_2$  partial pressures  $P_{\text{O}_2}$  (0.5, 1, 2 and 5 kPa) and a constant CO partial pressure,  $P_{\text{CO}}$ , equal to 1 kPa. As expected, for all oxygen partial pressures, the  $\text{CO}_2$  production rate increased exponentially with increasing temperature, whereas the apparent activation energy that was determined from the slopes of the Arrhenius plots ranged between  $9.8 \text{ kcal mol}^{-1}$  for  $P_{\text{O}_2} = 0.5 \text{ kPa}$  and  $13.1 \text{ kcal mol}^{-1}$  for  $P_{\text{O}_2} = 5 \text{ kPa}$ . Moreover, at each temperature,  $r_{\text{CO}_2}$  was found to increase with increasing  $\text{O}_2$  partial pressure, which implies a positive order of the reaction with respect to  $\text{O}_2$ , in agreement with the higher activity observed under oxidative conditions compared to stoichiometric conditions (Figure 5). The latter behavior was observed for all tested perovskites; thus, it can be assumed that CO combustion is positive order with respect to  $\text{O}_2$  on all of them.

The positive order of CO combustion with respect to  $\text{O}_2$  is more clearly shown in Figure 6b, where is presented in the form of logarithmic plot the dependence of the  $\text{CO}_2$  production rate on  $\text{O}_2$  partial pressure at three different temperatures (115, 130, and  $145^\circ\text{C}$ ), for constant CO partial pressure equal to 1 kPa. The slopes of the plots for the three temperatures do not differ significantly, corresponding to an apparent reaction order in oxygen of ca. 0.5.

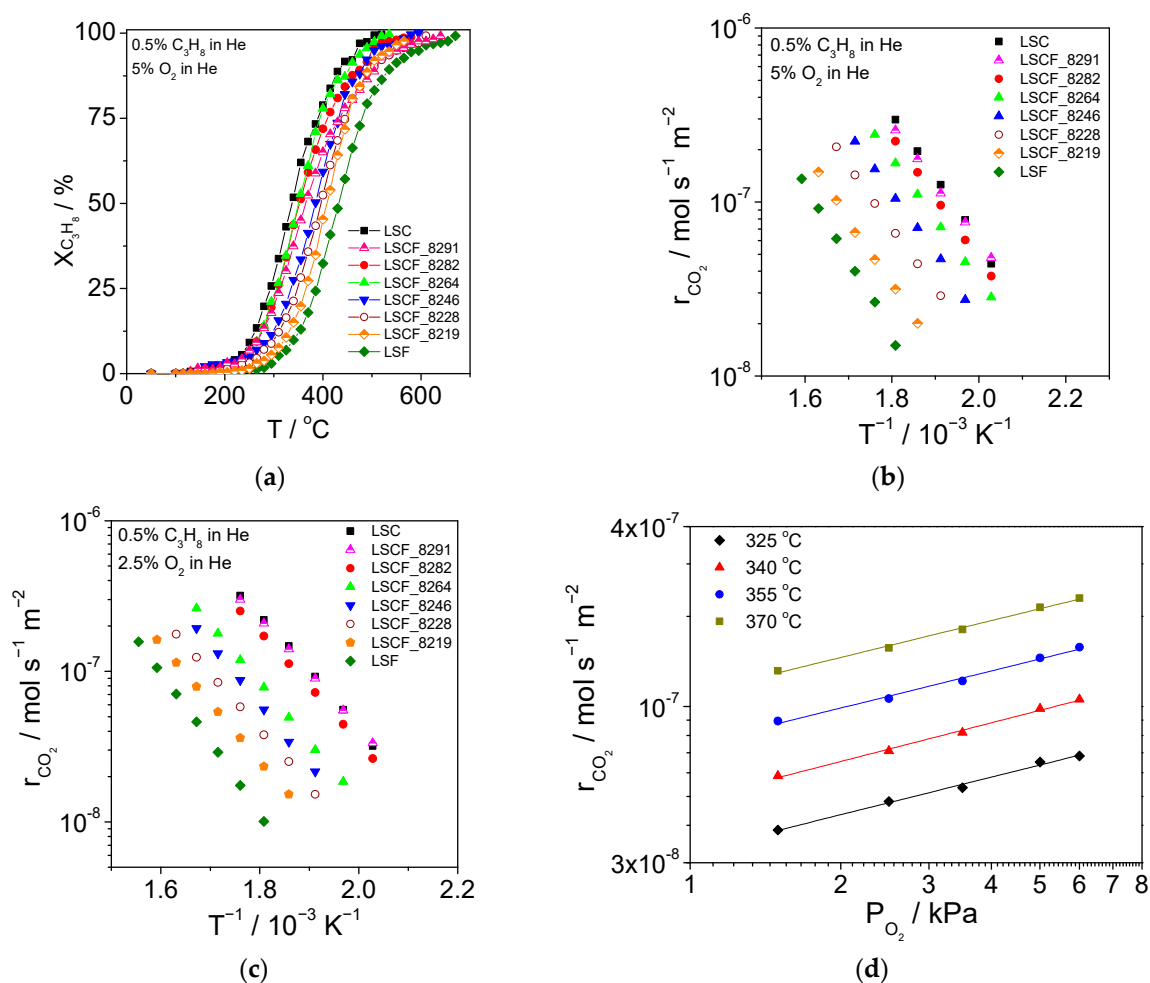


**Figure 6.** CO combustion on LSC. (a) Temperature dependence of the CO<sub>2</sub> production rate (Arrhenius plots) for four different O<sub>2</sub> partial pressures ( $P_{\text{O}_2}$ : 0.5, 1, 2 and 5 kPa) and  $P_{\text{CO}} = 1$  kPa. (b) Effect of  $P_{\text{O}_2}$  on the CO<sub>2</sub> production rate, at constant  $P_{\text{CO}} = 1$  kPa, for three different temperatures (115, 130, and 145 °C).

#### 2.4. Catalytic Activity for Propane Combustion

The synthesized  $\text{La}_{0.8}\text{Sr}_{0.2}\text{Co}_x\text{Fe}_{1-x}\text{O}_{3-\delta}$  perovskites were also tested as catalysts for complete oxidation of propane under oxidative and stoichiometric conditions. Figure 7a shows, for all synthesized perovskites, the dependence of propane conversion ( $X_{\text{C}_3\text{H}_8}$ ) on temperature, under oxidative feed conditions (0.5%  $\text{C}_3\text{H}_8$ /5%  $\text{O}_2$ /balance He). For all tested perovskite oxides, complete conversion of propane was achieved at temperatures ranging between 520 °C and 670 °C, which are higher than the corresponding ones for CO oxidation (Figure 3a). For the same temperature, increasing the Co/Fe ratio was accompanied by an increase in propane conversion, more pronounced for Co/Fe ratios up to 6/4 (Figure 7a). Equivalently, the light-off temperature ( $T_{50}$ ) decreased with increasing Co/Fe ratio. Considering the above, it is concluded that the dependence of catalytic activity of  $\text{La}_{0.8}\text{Sr}_{0.2}\text{Co}_x\text{Fe}_{1-x}\text{O}_{3-\delta}$  perovskites on the Co/Fe ratio is similar for both CO and propane combustion, i.e., the activity is reduced with increasing Fe and decreasing Co content at the B-sites. The higher temperatures required for complete conversion of propane compared to CO (Figures 3a and 7a), under oxidative feed conditions, are expected since propane is a more complex molecule compared to CO.

Figure 7b,c present for all tested perovskites, in the form of Arrhenius plots, the temperature dependence of the CO<sub>2</sub> production rate ( $r_{\text{CO}_2}$ ) in propane combustion under oxidative (0.5%  $\text{C}_3\text{H}_8$ /5%  $\text{O}_2$ /balance He) and stoichiometric (0.5%  $\text{C}_3\text{H}_8$ /2.5%  $\text{O}_2$ /balance He) feed conditions, respectively, with the rate being determined under practically differential conditions and normalized to SSA. As shown in Figure 7b, for oxidative conditions, with increasing Co content the same  $r_{\text{CO}_2}$  was obtained at lower temperature, more clearly for Co/Fe  $\leq 6/4$ , which implies an increase in the catalytic activity for propane combustion. The temperature corresponding to a CO<sub>2</sub> production rate of  $10^{-7} \text{ mol s}^{-1} \text{ m}^{-2}$  was equal to 345 °C and 244 °C for the less active (LSF) and the most active (LSC) perovskite catalysts, respectively. As shown in Figure 7c, practically the same behavior was observed for propane combustion under stoichiometric conditions, i.e., the same  $r_{\text{CO}_2}$  value was achieved at lower temperatures with increasing Co/Fe ratio, the effect being clearer for Co/Fe ratios up to 6/4. In this case, the temperature corresponding to a CO<sub>2</sub> production rate of  $10^{-7} \text{ mol s}^{-1} \text{ m}^{-2}$  was 355 °C for the LSF and 255 °C for the LSC perovskites (Figure 7c). Also, the comparison of the data shown in Figure 7b,c reveals that the temperatures corresponding to a specific  $r_{\text{CO}_2}$  value, for example,  $10^{-7} \text{ mol s}^{-1} \text{ m}^{-2}$ , were lower under oxidative conditions compared to stoichiometric conditions for all the tested perovskites, which, similar to CO combustion, indicates a higher catalytic activity under oxidative conditions.



**Figure 7.** Propane combustion on  $La_{0.8}Sr_{0.2}Co_xFe_{1-x}O_{3-\delta}$  perovskites: (a)  $C_3H_8$  conversion as a function of temperature under oxidative feed conditions (0.5%  $C_3H_8$ /5%  $O_2$ /He), (b) temperature dependence of the  $CO_2$  production rate under oxidative feed conditions (0.5%  $C_3H_8$ /5%  $O_2$ /balance He), (c) temperature dependence of the  $CO_2$  production rate under stoichiometric feed conditions (0.5%  $C_3H_8$ /2.5%  $O_2$ /balance He), and (d) effect of oxygen partial pressure ( $P_{O_2}$ ) on the  $CO_2$  production rate, for the LSC catalyst, at constant propane partial pressure  $P_{C_3H_8} = 0.5$  kPa and for four different temperatures (325 °C, 340 °C, 355 °C, and 370 °C).

Kinetic measurements were performed for propane combustion on the most active LSC perovskite. Figure 7d shows, in the form of logarithmic plots, the dependence of the  $CO_2$  production rate on  $O_2$  partial pressure at four different temperatures (325, 340, 355, and 370 °C), for constant propane partial pressure equal to 0.5 kPa. A positive order with respect to  $O_2$  is observed, practically the same for all tested temperatures. This can explain the higher activity for propane combustion observed for LSC under oxidative conditions compared to stoichiometric conditions. As the same behavior was observed for the other tested perovskites, it can be assumed that also for them propane combustion is positive order with respect to  $O_2$  (close to 0.5) in agreement with the observed higher activity under oxidative conditions.

### 3. Discussion

Oxygen adsorption on perovskites is a complex process, considered to occur mainly at the vicinity of B-sites of perovskite catalysts [13,59,60]. Adler et al. [61] assumed that two neighboring vacant surface lattice sites, similar to those in the bulk of the oxide, are involved in the dissociative adsorption of oxygen and surface oxygen exchange. Royer et al. in their review work [16] highlight the significant role of the oxidation state of the B-site

cations and of oxygen vacancies (created by partial substitution of the cations at the A- and/or B-sites) on the perovskite surface oxygen exchange and transport properties, which are also affected by the material microstructure. CO is chemisorbed molecularly on many transition metal oxides, via donation of electron density towards the metal cations, whereas the chemisorption of alkanes on transition metal oxides is generally dissociative [62]. Rhee and Lee [60] refer to two different adsorption states of CO on the surface of  $\text{LaCoO}_3$  depending on temperature, namely, CO adsorbed in the form of carbonyl species on  $\text{Co}^{3+}$  cations at 167 °C and CO in the form of bidentate complexes with the lattice oxygen or/and with the surface adsorbed oxygen at 360 °C. It has also been reported that the main CO adsorption site on  $\text{LaCoO}_3$  perovskite surface is provided by surface lattice oxygen, with formation of surface carbonate species [59,63]. Propane has been reported to adsorb dissociatively on unsubstituted and P-doped  $\text{LaCoO}_3$  with the surface  $\text{Co}^{3+}$  sites acting as active sites for initial cleavage of a C-H bond and formation of an adsorbed alkyl radical [64]. Promotion of propane adsorption and dissociation has been also reported for  $\text{LaCoO}_3$  perovskites with increased defect content, synthesized via a defect engineering route, being attributed to an increase in the number of  $\text{Co}^{3+}$  on the surface combined with an increase in lattice oxygen mobility and surface oxygen capacity, as also corroborated using DFT calculations [65]. Such calculations have been also used to study propane adsorption on macroporous  $\text{La}_{0.8}\text{Sr}_{0.2}\text{CoO}_3$  perovskite oxides [66].

As mentioned in the Introduction section, two oxidation mechanisms are considered as dominant in  $\text{AA}'\text{BB}'\text{O}_3$  perovskites, namely, the suprafacial mechanism, which involves only surface oxygen species, and the intrafacial mechanism, corresponding to a redox cycle involving surface lattice oxygen with possible participation of oxygen species originating from the bulk of the perovskite oxide, the prevailing reaction mechanism depending strongly on the perovskite composition and the reaction [12,14–16]. CO oxidation catalyzed by substituted  $\text{AA}'\text{BO}_3$  and  $\text{AA}'\text{BB}'\text{O}_3$  perovskites, with Co and Fe at the B and B'-sites, is considered to proceed via the intrafacial mechanism due to their higher ionic conductivity compared to other perovskites, associated mainly with their high lattice oxygen mobility [14]. This agrees with the observed high surface exchange in oxygen between the gas phase and the lattice structure of  $\text{La}_{1-x}\text{Sr}_x\text{CoO}_3$  ( $x$ : 0 – 0.6) at low temperatures ( $T < 300$  °C) [67] at which  $\text{ABO}_3$  type perovskites tend to follow the suprafacial mechanism [14,15].

In the present study, a similar trend in the catalytic activity of  $\text{La}_{0.8}\text{Sr}_{0.2}\text{Co}_x\text{Fe}_{1-x}\text{O}_{3-\delta}$  for both CO and propane combustion was observed as  $x$  varied from 0 (LSF) to 1 (LSC). This indicates that the intrafacial mechanism is probably prevailing, as in this case the rate determining step would be the surface lattice oxygen replenishment for both reactions. The prevalence of the intrafacial mechanism is also corroborated by the fact that, as mentioned above, the tested perovskites exhibit a higher number of oxygen ion vacancies, an improved reducibility of the B-site ions, and a higher surface oxygen exchange as well as a higher mobility of oxygen ions compared to  $\text{LaFeO}_3$  and  $\text{LaCoO}_3$  [5,12,14,44,58,67] for which a suprafacial mechanism for CO oxidation at temperatures below 350 °C has been suggested [5,12,14,15]. In this respect, the observed increase in catalytic activity with increasing substitution of iron by cobalt at the B-sites can be mainly attributed to the induced change in the number of lattice oxygen vacancies associated with the easier alteration of the redox state of the Co cations compared to Fe cations [56–58], which increases lattice oxygen anion mobility and enhances surface oxygen exchange [14,54,58], thus favoring the aforementioned redox cycle corresponding to the intrafacial mechanism. The easier release of oxygen from the perovskite oxides with increasing Co/Fe ratio (from LSF to LSC) is corroborated by the observed shift in the onset reduction temperature to lower values in the  $\text{H}_2$ -TRP profiles (Figure 2). The preferential release of oxygen from oxygen sites in the vicinity of Co rather than Fe sites, as a result of the easier reduction of Co cations compared to Fe cations, has also been observed by Itoh et al. [68] for  $\text{La}_{0.6}\text{Sr}_{0.4}\text{Co}_{0.2}\text{Fe}_{0.8}\text{O}_{3-\delta}$  using in situ X-ray absorption spectroscopy. The increase in oxygen non-stoichiometry, or equivalently in the number of oxygen vacancies, induced by substitution of Fe by Co at the

B-sites of  $\text{La}_{1-x}\text{Sr}_x\text{Co}_{1-y}\text{Fe}_y\text{O}_{3-\delta}$  perovskites has been demonstrated by Scott et al. [27] using solid electrolyte coulometry and CO-TPR measurements. Similarly, Lankhorst and ten Elshof [28] using coulometric titration at 650–950 °C reported a decrease in the oxygen non-stoichiometry in  $\text{La}_{0.6}\text{Sr}_{0.4}\text{Co}_{1-y}\text{Fe}_y\text{O}_{3-\delta}$  with increasing Fe content at the B-sites (changing  $y$  from 0 to 0.6), which they associated with an increase in the  $\text{O}^{2-}$  binding energy in the lattice and with the preferential formation of holes over oxygen vacancies.

The results of the present study are in agreement with the reported by Levasseur and Kaliaguine [29] decrease in the catalytic activity of  $\text{La}_{1-y}\text{Ce}_y\text{Co}_{1-x}\text{Fe}_x\text{O}_3$  for CO combustion with partial substitution of Co by Fe at the B-sites, which they attributed to a decrease in the reducibility of the B-site cations and in the mobility of oxygen in the perovskite bulk. These results also agree with the observed by Tanaka et al. [30] increase in the catalytic activity for propane combustion of  $\text{La}_{0.9}\text{Ce}_{0.1}\text{Co}_{1-x}\text{Fe}_x\text{O}_3$  ( $x$ : 0 to 1) with increasing Co content and with the reported by Merino et al. [45] increase in the catalytic activity of  $\text{LaCo}_{1-y}\text{Fe}_y\text{O}_{3\pm\lambda}$  ( $y$  = 0.1, 0.5, 1) for the same reaction with decreasing  $y$  (partial substitution of Fe by Co).

It is noted that the observed variation in catalytic activity of the tested perovskites for CO and propane combustion with changing Fe/Co ratio could be also attributed, to a lesser extent, to the observed changes in their structural characteristics (Section 2.1), which are associated with the surface electronic structure and, thus, may affect the chemisorptive bond strengths of the reactants [16,31,48,50].

## 4. Materials and Methods

### 4.1. Synthesis of the Perovskite Oxides

The synthesis method of the perovskite oxides affects significantly their physical properties, including particle size, porosity, and specific surface area (SSA). Synthesis of a perovskite material with high SSA and porosity is expected to enhance its catalytic or electrocatalytic performance. Therefore, the perovskite synthesis methods reported in the literature focus on fine-tuning of the aforementioned physical properties for specific applications [69]. In the present work, the in situ combustion method, with citric acid as fuel, was applied for synthesis of the tested  $\text{La}_{0.8}\text{Sr}_{0.2}\text{Co}_x\text{Fe}_{1-x}\text{O}_{3-\delta}$  perovskites, as described in detail in a previous study of our group [47].

The following metal nitrates, in the form of solutions in triple-distilled water, were used as metal precursors:  $\text{La}(\text{NO}_3)_3 \cdot 6\text{H}_2\text{O}$  (99.9% REO, Alfa Aesar, Karlsruhe, Germany),  $\text{Sr}(\text{NO}_3)_2$  (99+%, ACS reagent, Sigma-Aldrich Chemie, Steinheim, Germany),  $\text{Fe}(\text{NO}_3)_3 \cdot 9\text{H}_2\text{O}$  ( $\geq 99.0\%$ , Merck, Darmstadt, Germany), and  $\text{Co}(\text{NO}_3)_2 \cdot 6\text{H}_2\text{O}$  ( $\geq 99.0\%$  KT, ACS reagent, Sigma-Aldrich Chemie, Steinheim, Germany). Citric acid monohydrate ( $\text{C}_6\text{H}_8\text{O}_7 \cdot \text{H}_2\text{O}$ , 99.5–100.5% assay, Merck, Darmstadt, Germany) and ammonium nitrate ( $\text{NH}_4\text{NO}_3$ ,  $\geq 99.0\%$ , Sigma-Aldrich, St. Louis, MO, USA) were used as fuel and extra oxidant, respectively [47]. Citric acid was diluted in triple-distilled water to form a 1.7 M solution, and an appropriate amount of this solution was added under continuous stirring to the metal precursors solution to obtain a citric acid-to-metal ions molar ratio equal to 2:1 [47,70]. An amount of  $\text{NH}_4\text{NO}_3$  was also added to obtain a molar ratio of  $\text{NH}_4\text{NO}_3$ -to-metal ions equal to 1:1 [47]. The presence of ammonium nitrate, which does not affect the chemical composition of the synthesized perovskite, both accelerates the combustion, reducing sintering time after the formation of the perovskite, and yields in the production of extra amount of gasses that have a dilatative effect on the microstructure of the material, which results in an increase in the SSA of the oxide [71]. An appropriate amount of ammonia solution (30 wt.%, Carlo Erba) was then added dropwise until reaching a pH value of ca. 9 [47,70] in order to neutralize the excess citric acid and form a colloidal solution (sol) [72]. This solution was heated under magnetic stirring on a hot plate until evaporation of  $\text{H}_2\text{O}$ . The resulting slurry was then heated up to ca. 400 °C, using a heat gun, in order to initiate ignition and form a thin crust. The powder, which resulted from shattering the crust, was calcined at 900 °C for 5 h in stagnant air to form the crystalline perovskite phase, and, finally, was finely grounded in a mortar [47].

#### 4.2. Physicochemical Characterization of the Perovskite Oxides (BET, XRD, and ICP-OES)

The specific surface areas (SSAs) of the synthesized perovskite powders were determined via nitrogen physisorption at liquid N<sub>2</sub> temperature (BET method), using a TriStar 3000 surface area and porosimetry analyzer (Micromeritics, Norcross, GA, USA) preceded by degassing of the perovskite samples under vacuum at 300 °C for 1 h [47].

X-ray diffraction (XRD) measurements were performed in order to determine the structural characteristics of the synthesized perovskite materials. XRD spectra were obtained for  $2\theta$  values ranging from 10° to 90° at a rate of 0.04 ° s<sup>-1</sup>, using a Bruker AXS D8 Advance diffractometer, which was equipped with a Cu-K $\alpha$  lamp ( $\lambda$  = 1.54062 Å) and a Ni filter [47]. The identification and analysis of the observed phases were performed using the EVA software (Bruker AXS, Karlsruhe, Germany).

After previous acid digestion of the perovskite powders, their exact stoichiometry was determined with inductively coupled plasma optical emission spectroscopy (ICP-OES) in an Optima 7000 DV ICP-OES system (Perkin Elmer, Waltham, MA, USA) [47].

#### 4.3. H<sub>2</sub> Temperature-Programmed Reduction Characterization

H<sub>2</sub> temperature-programmed reduction measurements were performed in order to assess and compare the reducibility of the synthesized perovskites. The apparatus used for the experiments consisted of a gas flow system, a quartz reactor positioned in an open-ended vertical electric furnace, and an Omnistar<sup>TM</sup> GSD301 O1 quadrupole mass spectrometer (Pfeiffer Vacuum, Asslar, Germany) interfaced to a personal computer for on-line monitoring of the TPR effluent gas, using the Quadstar 32-bit (version 7.03) software (Pfeiffer Vacuum, Asslar, Germany). The perovskite mass used in each experiment was 150 mg. The sample was placed in the reactor in the form of a fixed bed deposited on quartz wool and was initially heat treated under He flow at 500 °C for 15 min to remove any adsorbed species [73]. Heat treatment continued under flow of 21% O<sub>2</sub>/He mixture at the same temperature for 30 min, followed by free cooling to room temperature (ca. 25 °C). Then, the feed was sequentially switched to He for 15 min and to 3.9% H<sub>2</sub>/He mixture for 10 min. Afterwards, the TPR experiment was started by linearly increasing the temperature of the sample up to 720 °C at a rate of 30 °C min<sup>-1</sup>, using a Eurotherm 815 controller/programmer, and simultaneously monitoring hydrogen in the reactor effluent by recording the transient mass spectrometer signal at mass-to-charge ratio  $m/z$  = 2. The temperature of the sample was measured by means of a type-K thermocouple. The gas feed flow rate was equal to 30 cm<sup>3</sup> min<sup>-1</sup> in all the above steps.

#### 4.4. Catalytic Oxidation Measurements

The experimental apparatus used for the CO and propane combustion measurements consisted of a fixed-bed quartz tube reactor positioned in an open-ended vertical electric furnace, a gas flow system, and an analysis system. The composition and flow rate of the gas mixture fed to the reactor in down-flow mode were adjusted using three electronic mass flow controllers (Aera FC-7700C connected to a ROD-4 operating unit, Advanced Energy Industries, Inc., Fort Collins, CO, USA). Reaction gases were high purity O<sub>2</sub>/He, CO or C<sub>3</sub>H<sub>8</sub>/He mixtures, and He. The perovskite powder (120 mg) was placed on quartz wool in the middle of the quartz tube reactor (8 mm internal diameter). The temperature of the perovskite catalyst was measured in the middle of the catalyst bed using a K-type thermocouple enclosed in a quartz tube entering the upper part of the reactor through a tee connection and was controlled using a Eurotherm 2216e temperature controller. The analysis system consisted of a non-dispersive infrared CO-CO<sub>2</sub> analyzer (BINOS<sup>®</sup> 100, Rosemount Analytical/Emerson Process Management, Hasselroth, Germany), for continuous monitoring of CO and CO<sub>2</sub> concentration, and a gas chromatograph (TRACE<sup>TM</sup> CG Ultra, Thermo Fischer Scientific, Inc., Waltham, MA, USA) equipped with a thermal conductivity detector (TCD) and a 6-port sampling valve (VICI Valco). A Carbosieve SII 80/100 (1.8" O.D. × 8 ft) stainless steel packed column operating at 120 °C was used for analysis of the reaction mixture in CO combustion, whereas a cascade of a 23% SP<sup>®</sup>-1700

on 80/100 Chromosorb P AW (1.8"O.D.  $\times$  8 ft) and a 10% TCEP on 100/120 Chromosorb P AW (1.8"O.D.  $\times$  8 ft) stainless steel packed columns, operating at 40 °C, were used for analysis of the reaction mixture in propane combustion, using He as carrier gas in both cases. Analysis of the reactor feed was possible by bypassing the reactor using a 4-port valve (VICI Valco). The experiments were carried out under practically atmospheric pressure in the temperature range 50–670 °C, using a total feed flow rate of 100 cm<sup>3</sup> min<sup>−1</sup>. For this flow rate, the pressure drop across the catalyst fixed-bed reactor, as measured using a manometer, was negligible (less than 0.01 atm). The gas hourly space velocity (GHSV) was equal to 27,500 h<sup>−1</sup>, as calculated using a measured bulk catalyst bed density value of 0.55 g cm<sup>−3</sup>. Oxidative (1% CO–5% O<sub>2</sub> and 0.5% C<sub>3</sub>H<sub>8</sub>–5% O<sub>2</sub>) and stoichiometric (1% CO–0.5% O<sub>2</sub> and 0.5% C<sub>3</sub>H<sub>8</sub>–2.5% O<sub>2</sub>) feed compositions were used, with He as balance gas. All measurements were performed after previous establishment of steady-state conditions. No indication of catalyst deactivation due to the produced H<sub>2</sub>O(g) was observed during the catalytic measurements concerning propane combustion.

## 5. Conclusions

In the present work, a series of eight La<sub>0.8</sub>Sr<sub>0.2</sub>Co<sub>x</sub>Fe<sub>1−x</sub>O<sub>3−δ</sub> perovskites, with  $x = 0, 0.1, 0.2, 0.4, 0.6, 0.8, 0.9$ , and 1, were synthesized via the in situ combustion synthesis method, and their catalytic activities for CO and C<sub>3</sub>H<sub>8</sub> combustion were compared. The perovskite powders were characterized with respect to their specific surface area (SSA), structure, and reducibility via N<sub>2</sub> physisorption (BET method), XRD, and H<sub>2</sub>-TPR, respectively, while their chemical composition was determined via ICP-OES.

Their SSA values ranged between 4.1 (La<sub>0.8</sub>Sr<sub>0.2</sub>Co<sub>0.9</sub>Fe<sub>0.1</sub>O<sub>3−δ</sub>) and 7.9 m<sup>2</sup> g<sup>−1</sup> (La<sub>0.8</sub>Sr<sub>0.2</sub>Co<sub>0.1</sub>Fe<sub>0.9</sub>O<sub>3−δ</sub>). XRD confirmed the formation of the perovskite structure for all synthesized materials and the absence of secondary phases. A shift in the XRD peaks to higher  $2\theta$  was observed with increasing partial substitution of Fe by Co at the B-sites, indicating a contraction of the perovskite unit cell. This shift was accompanied by a gradual change in the main peak (located at  $2\theta$  between 32 and 33°) from single to doublet, implying a change in the perovskite symmetry from orthorhombic to rhombohedral.

The H<sub>2</sub>-TPR profiles of all synthesized perovskites were characterized by the presence of a broad main reduction peak that can be attributed to the reaction of hydrogen with surface oxygen partly replenished by lattice oxygen migrating from the oxide bulk as the temperature increased. The onset temperature of the reduction process was shifted towards lower values with increasing Co/Fe ratio accompanied by an increase in the main reduction peak, clearly for Co/Fe  $\leq 6/4$ . This indicates an easier release of the surface lattice oxygen species and an easier transport of oxygen from the oxide bulk with increasing Co/Fe ratio, which can be mainly associated with the more facile change in the oxidation state of the cobalt cations compared to iron cations.

The catalytic performance of the synthesized La<sub>0.8</sub>Sr<sub>0.2</sub>Co<sub>x</sub>Fe<sub>1−x</sub>O<sub>3−δ</sub> perovskites for CO and propane combustion was investigated in a fixed bed reactor under oxidative and stoichiometric feed conditions. Increase in the Co/Fe ratio, from La<sub>0.8</sub>Sr<sub>0.2</sub>FeO<sub>3−δ</sub> (LSF) to La<sub>0.8</sub>Sr<sub>0.2</sub>CoO<sub>3−δ</sub> (LSC), resulted in an enhancement of the catalytic activity for both CO and propane combustion, as concluded both from conversion vs. temperature curves and from CO<sub>2</sub> production rate measurements under practically differential conditions. For CO combustion, the effect of changing the relative content of Co and Fe at the B-sites on catalytic activity was more pronounced under oxidative feed conditions (1% CO/5% O<sub>2</sub>/balance He), whereas under stoichiometric feed conditions (1% CO/0.5% O<sub>2</sub>/balance He) it was more significant for Co/Fe  $\leq 6/4$ . A higher activity of the tested catalytic materials was observed under oxidative reaction conditions compared to stoichiometric conditions, which can be attributed to positive order kinetics with respect to oxygen. The latter was confirmed with kinetic measurements performed for both CO and propane oxidation using La<sub>0.8</sub>Sr<sub>0.2</sub>CoO<sub>3−δ</sub> as catalyst.

The observed enhancement of the catalytic activity of La<sub>0.8</sub>Sr<sub>0.2</sub>Co<sub>x</sub>Fe<sub>1−x</sub>O<sub>3−δ</sub> perovskites for CO and propane combustion with increasing Co/Fe ratio can be mainly

explained on the basis of a prevailing redox catalytic cycle (intrafacial mechanism), considering that the increase in the Co content at the expense of iron induces an increase in the number of catalytically active sites, as they are related to oxygen vacancies at the vicinity of the Co B-sites, and enhances oxygen surface exchange kinetics, due to the lower redox stability of cobalt cations compared iron cations, as also corroborated by the results of the H<sub>2</sub>-TPR experiments.

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## Article

# A New Mixed-Metal Phosphate as an Efficient Heterogeneous Catalyst for Knoevenagel Condensation Reaction

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**Abstract:** The escalating demand for the cost-effective synthesis of valuable fine chemicals has fueled the search for sustainable heterogeneous catalysts. Among these catalytic reactions, Knoevenagel condensation has emerged as a very demanding reaction due to its involvement in the synthesis of new C–C bond formation. Porous metal phosphates have attracted significant attention in catalysis due to their unique surface properties. In this study, we report the synthesis of a novel porous magnesium aluminum phosphate (MALPO) material through a hydrothermal template-free approach. MALPO exhibited very promising specific surface area and hierarchical porosity. Moreover, the plate-like morphology of the material can enhance the exposure of the catalytic sites located at the surfaces, leading to enhanced catalytic activity. MALPO demonstrated excellent catalytic performance, yielding a series of Knoevenagel products with up to 99% yield. Notably, the catalyst displayed remarkable recyclability, retaining its structural integrity throughout multiple reaction cycles. The findings highlight the potential of porous mixed-metal phosphates, exemplified by MALPO, as sustainable and efficient base catalyst for the synthesis of value-added chemicals, contributing to the growing demand of the chemical industry. Further investigations are warranted to explore their catalytic potential in diverse chemical transformations and optimize their performance for large-scale operations.

**Keywords:** porous metal phosphate; heterogeneous catalysis; Knoevenagel condensation; base catalysis

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## 1. Introduction

In the midst of a relentless surge for the green chemical synthesis, the chemical industry experiences an extraordinary upswing in the demand for suitable heterogeneous catalysts. Thus, the search for sustainable and cost-effective catalytic routes for synthesizing value-added chemicals has become a major concern for scientists worldwide. Knoevenagel condensation has been one of the most famous reactions in organic synthesis since its discovery (1890) [1] due to its massive importance in synthesizing valuable reactive organic building blocks [2,3]. In a typical Knoevenagel reaction a carbonyl compound reacts with active methylene groups to generate a new C–C bonds [4,5]. The reaction is found to be highly applicable for synthesizing various fine chemicals [6], hetero-Diels–Alder reactions [7,8], and carbocyclic as well as heterocyclic compounds with significant bio-active behavior [9]. Furthermore, the various kinds of intermediates, such as  $\alpha$ ,  $\beta$ -unsaturated esters;  $\alpha$ -cyanocinnamates [10];  $\alpha$ ,  $\beta$ -unsaturated nitriles; and cinnamic acid, involved in the Knoevenagel reaction are considered to be the major platform chemicals [11] for the pharmaceutical industry, the cosmetic industry, the production of perfumes, and the antihypertensive and polymer industries [12,13]. The Knoevenagel condensation reaction can proceed through an acid- or base-catalyzed pathway. So far, several attempts have been

made to understand the mechanistic pathway for this reaction. Initially, the methodologies were developed via homogeneous routes [14,15], but in the context of the long-term usage of catalysts, the homogeneous approach has serious shortcomings. In this context, the heterogeneous path is considered to be the most convenient due to the scope of the recyclability of catalyst, the ease of catalyst separation, and the cost-effectiveness of the process. Several heterogeneous catalysts displayed good performances in Knoevenagel condensation reactions such as the surfactant–mesoporous silica composite [16], functionalized MCM-41 [17], indium-doped AlMCM-41 [18], mesoporous carbon nitride [19], zeolites [20,21], porous organic polymers [22], metal–organic framework [2], phosphate complexes [23], coordination polymers [24], etc. However, use of these materials as catalysts may often lead to metal contamination in the final product.

Today, porous nanomaterials play a very crucial role in the field of heterogeneous catalysis due to their enhanced surface activity, pore size tunability, and ease of surface modifications. Previously, Gascon et al. reported AlMIL-53-NH<sub>2</sub> and IRMOF-3 in the Knoevenagel condensation of benzaldehyde with ethyl cyanoacetate [25]. On the other hand, Fischer et al. identified catalytic activities on several functionalized porous materials like Fe-MIL-101-NH<sub>2</sub>, CAU-1-NH<sub>2</sub>, and Al-MIL-101-NH<sub>2</sub> catalysts in the Knoevenagel condensation reaction of benzaldehyde with malononitrile and ethyl cyanoacetate [26]. Porous metal phosphates have emerged as a captivating class of materials [27] that has garnered significant interest within the realm of material science and engineering. These unique materials embody the fusion of advantageous properties exhibited by metals and phosphates, offering a broad spectrum of applications across diverse industries. Active catalytic sites in these porous metal phosphates are located at the surface of the interconnected pores [28] and can thus offer impressive catalytic activities.

Since the discovery of the aluminophosphate molecular sieve in 1982 by Wilson and coworkers [29], significant attention has been paid to the development of microporous aluminum phosphate molecular sieves [30–32]. Aluminum phosphate, a crystalline inorganic compound, is widely recognized for its diverse applications. Its similarities with zeolite make it a promising material in fields like gas separation [31], sensing, and heterogeneous catalysis. The framework of ALPO composed of AlO<sub>4</sub> and PO<sub>4</sub> moieties, due to the electronically neutral skeleton and the lack of sufficient acidic sites results in a very weak catalytic activity [33]. Over the past few years, significant strides have been made in the synthesis and characterization of porous metal phosphates. Advanced techniques, including solvothermal and hydrothermal methods [34,35], have been harnessed to produce materials with well-defined porosity and desirable properties. Moreover, researchers have focused their efforts on designing and modifying these materials to enhance their performance and expand their potential applications. Significant focus is directed towards the development of highly active ALPO materials, while considerable attention has been dedicated to the synthesis of ALPO materials incorporating different metal ions [36].

Over the past few decades, porous metal phosphates containing transition metals have garnered significant attention due to the high catalytic activity associated with the metal sites. The low-cost synthetic approach, as well as easiness in bulk synthesis, followed by significant reproducibility, make this class of materials a promising contender among the other members of the porous material family. Thus, immense effort is paying off in the fabrication of these materials, both in academia and industry. So far, a large number of different metal-incorporating aluminum phosphate catalysts have been reported. Acid properties can be significantly affected by introducing Ga, Si, and Co in the ALPO framework [37–39]. Generally, the synthesis of porous nanomaterials involves the use of structure directing agents (SDA) like amines or ionic/nonionic surfactants [38,40,41]. However, the removal of SDA can sometimes be very challenging, as the calcination process requires high temperatures, which often result in the collapse of the porous framework. Moreover, the emission of toxic gas during the calcination process is hazardous to nature. Thus, the template-free synthesis of surface-active porous metal phosphates has garnered significant attention in recent times. The scientific community is highly focused on the controlled

fabrication of crystalline porous frameworks with specific morphologies. This approach holds great promise due to the wide availability of active sites, resulting in remarkable outcomes. Researchers are actively exploring the synthetic process, recognizing its potential and the immense interest associated with it. Thus, the pursuit of morphology-controlled fabrication and the accessibility of active sites in transition metal phosphates have become a subject of immense scientific interest and investigation.

Herein, we report the synthesis of a new magnesium aluminum phosphate (MALPO) through a template-free hydrothermal synthesis approach. The resulting catalyst, MALPO, exhibited a good BET surface area and hierarchical porosity. The electron microscopic analysis revealed the plate-like morphology of the material, which facilitated enhanced surface exposure and improved catalytic activity. MALPO has been employed as a heterogeneous catalyst for the Knoevenagel condensation reaction under mild reaction conditions. Remarkably, MALPO demonstrated excellent catalytic performance, resulting in high yields of the desired products and significantly reduced reaction times. Moreover, the catalyst exhibited exceptional recyclability, retaining its structural integrity throughout multiple reaction cycles. These findings highlight significant potential of MALPO as a valuable catalyst for efficient and sustainable synthesis of organic value added chemicals. The further exploration and optimization of MALPO's catalytic properties are warranted to unlock its full potential for various chemical transformations and large-scale applications.

## 2. Results

Herein, we have synthesized porous magnesium aluminum phosphate (MALPO) using a template-free hydrothermal approach. The material was thoroughly characterized via different experimental tools. The bonding connectivity inside the material network was evaluated by carrying out a Fourier transform infrared (FTIR) spectroscopic analysis in a solid state by preparing the sample in the KBr pallet. The FTIR spectrum shown in Figure 1 indicates the presence of different bonding inside the material architecture. The peak at  $3425\text{ cm}^{-1}$  could be attributed to the O–H stretching vibration [42]. On the other hand, peaks at the region of  $1700\text{--}1550\text{ cm}^{-1}$  ( $1705$ ,  $1655$ ,  $1580\text{ cm}^{-1}$ ) could be assigned to different H–O–H bending vibrations. The signals at  $982$ ,  $1017$ , and  $1053\text{ cm}^{-1}$  indicate the presence of phosphate groups. The  $769$  and  $717\text{ cm}^{-1}$  peaks indicate the presence of metal oxygen bonds in the material [43,44].

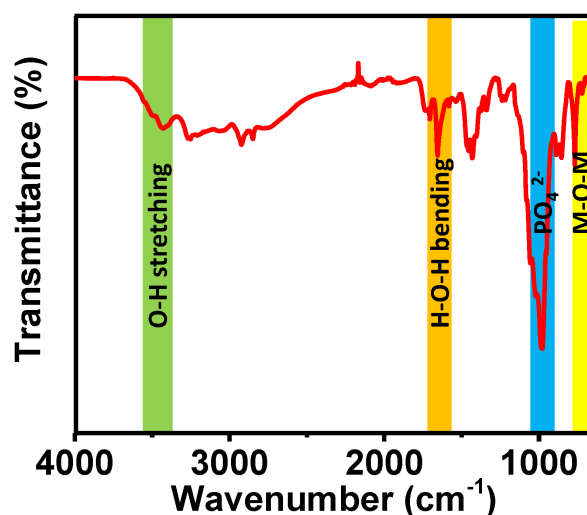
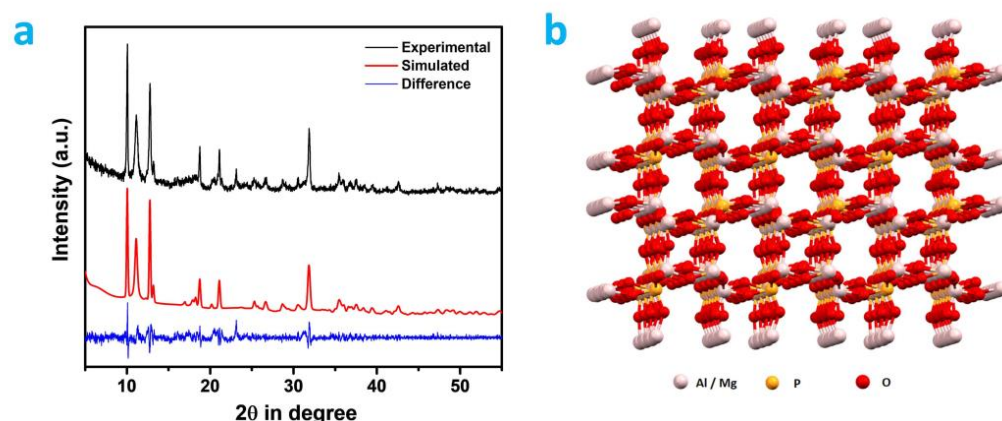


Figure 1. FTIR spectrum of MALPO.

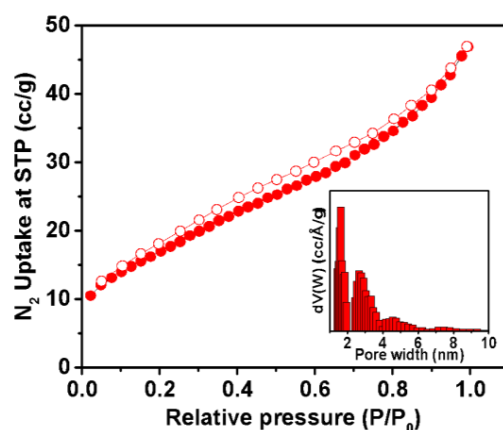
The unit cell parameters and the crystalline phase of the MALPO was evaluated using the powder X-ray diffraction (PXRD) analysis. Prominent sharp crystalline peaks are observed at  $10.08$ ,  $11.04$ ,  $12.77$ ,  $13.21$ ,  $18.96$ ,  $21.12$ ,  $23.13$ ,  $25.29$ ,  $26.72$ ,  $28.79$ ,  $30.56$ ,  $31.88$ ,  $35.48$ ,  $37.53$ , and  $42.58$  degrees of  $2\theta$  (Figure 2a). These aforementioned peaks were indexed

using the Expo2014 software [45], and these are assigned as 001, 101, 201, 210, 311, 30-2, 020, 021, 51-2, 711, 003, 91-1, 82-1, 812, and 31-4 planes, respectively (Table S1, ESI). The corresponding unit cell parameters of this phase of MALPO were  $a = 27.652 \text{ \AA}$ ,  $b = 7.683 \text{ \AA}$ ,  $c = 8.866 \text{ \AA}$ ,  $\alpha = 90.00^\circ$ ,  $\beta = 98.56^\circ$ , and  $\gamma = 90.00^\circ$ . The unit cell volume of MALPO was calculated as  $1862.59 \text{ \AA}^3$ . The space group of this triclinic phase was assigned to  $P1(1)$ . A structural model of MALPO (Figure 2b) was developed using VESTA 4.5.0 software [46] in order to understand the connectivity and porosity in the framework. The refined simulated PXRD of the model was generated, which matched well with the experimental PXRD pattern with a low ESD value of 0.072.



**Figure 2.** (a) Wide-angle powder XRD patterns: experimental (black), simulated (red), and difference (blue). (b) Ball and stick model of MALPO.

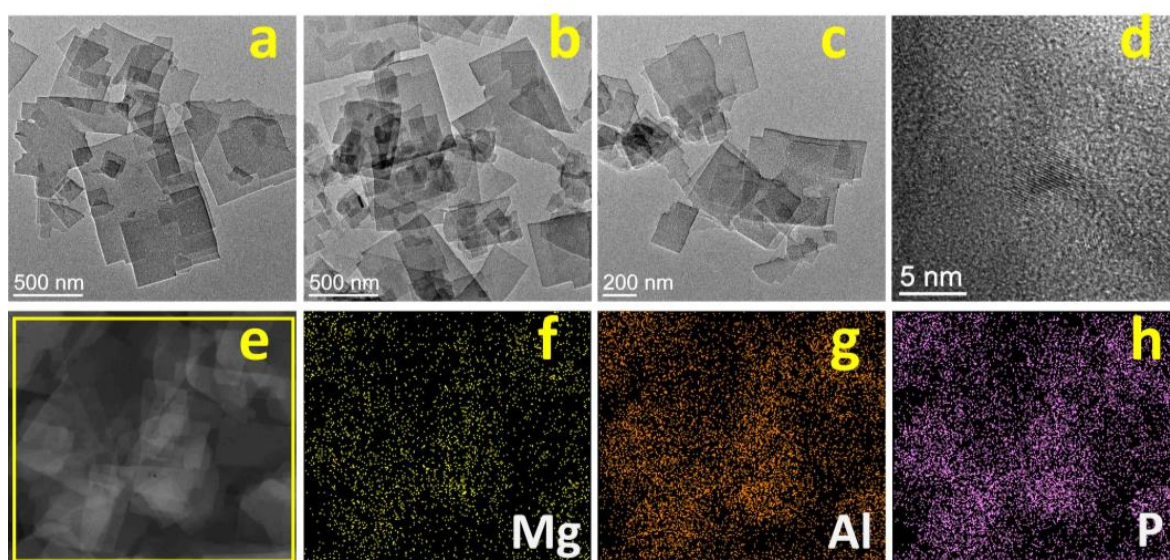
In order to investigate the porous nature of the as-prepared sample, nitrogen adsorption–desorption analysis was carried out at 77 K. The result is displayed in Figure 3. The isotherm indicated a mixture of type I and type IV isotherms, according to IUPAC convention [47]. A small rise in low pressure indicates the presence of microporosity and a steady rise in the  $N_2$  uptake, along with a mild desorption hysteresis in the relative pressure region of 0.4 to 0.8 reflects the presence of mesoporosity. The pore size distribution, as observed in the inset Figure 3, obtained through non-local density functional theory analysis (NLDFT), reveals the presence of maximum pores with diameters of 1.6 to 2.6 nm. This finding suggests the existence of a dominant pore size within this range. The calculated BET surface area is measured to be  $71 \text{ m}^2\text{g}^{-1}$ . This  $N_2$  sorption result indicates the significance of these specific pore sizes in the material, potentially influencing its properties and applications. Further investigation and characterization is warranted to explore the implications of this pore size distribution on the overall behavior and performance of the material.



**Figure 3.** Nitrogen adsorption–desorption isotherm; pore size distribution curve (inset).



The MALPO's morphological characteristics were meticulously assessed utilizing ultra-high resolution transmission electron microscopy (UHR-TEM). The acquired TEM images, obtained at different resolutions, unveiled a compelling plate-like morphology exhibited by MALPO. Notably, Figure 4 vividly depicts the presence of rectangular sheets [48] in varying sizes, effectively highlighting the material's intricate structure. Remarkably, upon closer examination at a high resolution (Figure 4d), the TEM image uncovers the presence of crystalline fringes, aligning impeccably with the expected outcomes from its corresponding X-ray diffraction pattern. This observation strongly suggests the presence of a well-defined crystal lattice within the material, underscoring its inherent structural integrity. The identified two-dimensional (2D) morphological feature holds tremendous potential for enhanced surface activity [49], primarily attributable to the significantly augmented surface exposure that it offers. This unique characteristic opens up exciting prospects for applications where improved [50] surface reactivity and accessibility are critical factors.



**Figure 4.** Transmission electron microscopy images of MALPO at different magnifications (a–d), selected area image under elemental mapping (e), elemental mapping of MALPO and the distribution of magnesium (Mg, (f)), aluminum (Al, (g)) and phosphorus (P, (h)).

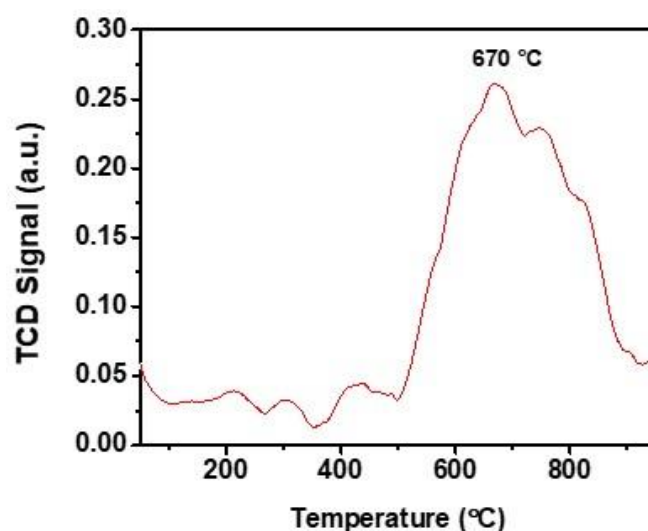
In addition to the morphological evaluation, an elemental distribution (Figure 4f–h) analysis was performed using energy-dispersive X-ray spectroscopy (EDAX) on the TEM images. Notably, the results obtained demonstrate that a strikingly uniform presence of elements throughout MALPO.  $\text{CO}_2$ -TPD analysis was carried out under an inert He gas flow, and the corresponding  $\text{CO}_2$  desorption profile of MALPO is shown in Figure 5. As can be seen from this  $\text{CO}_2$ -TPD profile, a broad  $\text{CO}_2$  desorption peak with maxima at a very high temperature of  $670^\circ\text{C}$  can be observed. The presence of no significant  $\text{CO}_2$  desorption peaks at lower temperatures suggests that  $\text{CO}_2$  molecules are strongly bound at the MALPO surface. The observed total basicity was  $3.15\ \mu\text{mol g}^{-1}$ . On the other hand, to measure the surface acidity of MALPO, we performed acid–base titration (see the Supporting Information), which suggested a total acidity of  $0.71\ \text{mmol g}^{-1}$ . The presence of defect phosphate groups are responsible for this surface acidity in MALPO.

#### Catalytic Activity of MALPO

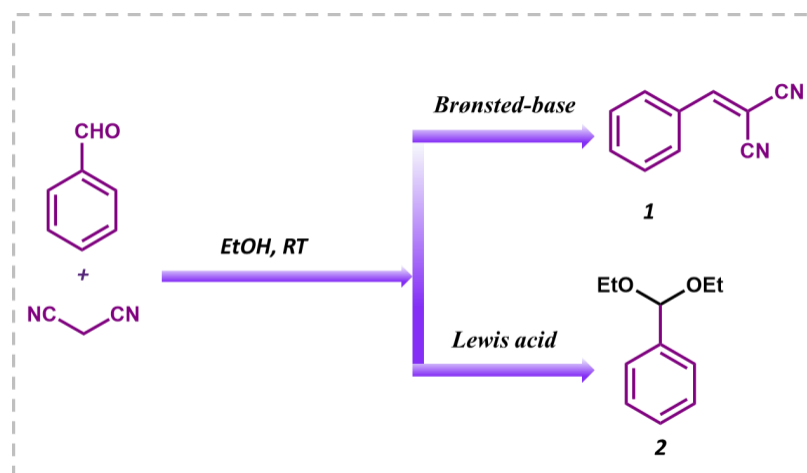
Knoevenagel condensation is a classical organic transformation in which an active methylene molecule reacts with a carbonyl compound to produce an  $\alpha,\beta$ -conjugated enone. As these intermediates are extensively used in perfumes, polymers, fine chemicals, cosmetics, medicines, and pharmaceuticals, many research groups are concentrating on developing heterogeneous solid catalysts for this organic reaction to generate relevant products. Basic



or acidic nature-based catalysts are often used to carry out the condensation reaction, but this requires high reaction temperatures or microwave irradiation [51,52]. Although many catalytic systems have been reported for this reaction, it is very challenging to develop a catalyst which can promote this reaction without the formation of by-products due to the consecutive self-condensation and oligomerization reactions of the primary reaction product [53,54]. The type of catalyst used has a significant impact on product selectivity. In the presence of a Brønsted-base, it results in benzylidene malononitrile, while in presence of Lewis's acid, benzaldehyde reacts with ethanol solvent to produce the desired product (Figure 6). To investigate the catalytic activity of the MALPO, the Knoevenagel condensation reaction was performed by taking benzaldehyde and malononitrile as model substrates in ethanol as the solvent. The reaction yielded the desired benzylidene malononitrile through the activation of a methylene group followed by aldol condensation under the present experimental conditions. As previously discussed, ethanol is considered as the best solvent when compared to MeCN, benzene, toluene, and DCM; thus, we performed our reaction with ethanol [55]. Before confirming the catalytic activity, a blank test was performed without using catalyst, which did not provide the suitable results after 2 h of reaction (17% conversion) in ethanol at room temperature.

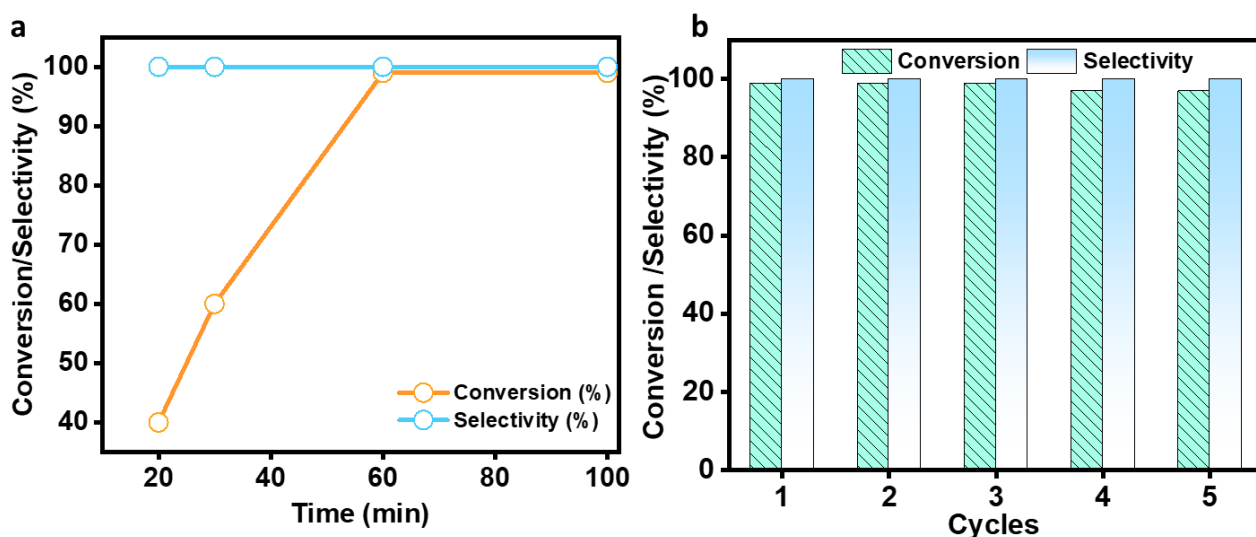


**Figure 5.** Temperature programmed desorption of  $\text{CO}_2$  profile of MALPO in the temperature range 50–875 °C.



**Figure 6.** Knoevenagel condensation reaction between benzaldehyde and malononitrile in ethanol as the solvent to obtain benzylidene malononitrile (1) and the undesired by-product benzaldehyde diethyl acetal (2).

In the same experimental conditions, a 99% conversion of benzaldehyde was accomplished using MALPO in ethanol at room temperature after only 100 min. The results clearly reveal the contribution of catalysts towards the activation of this reaction. As we observed that the reaction proceeds smoothly in ethanol within 100 min, we further identified the actual required time for this conversion. Then, we performed the reaction at different time intervals, which is shown in Figure 7a, and while it was observed for 100 min, the reaction was completed within 60 min.

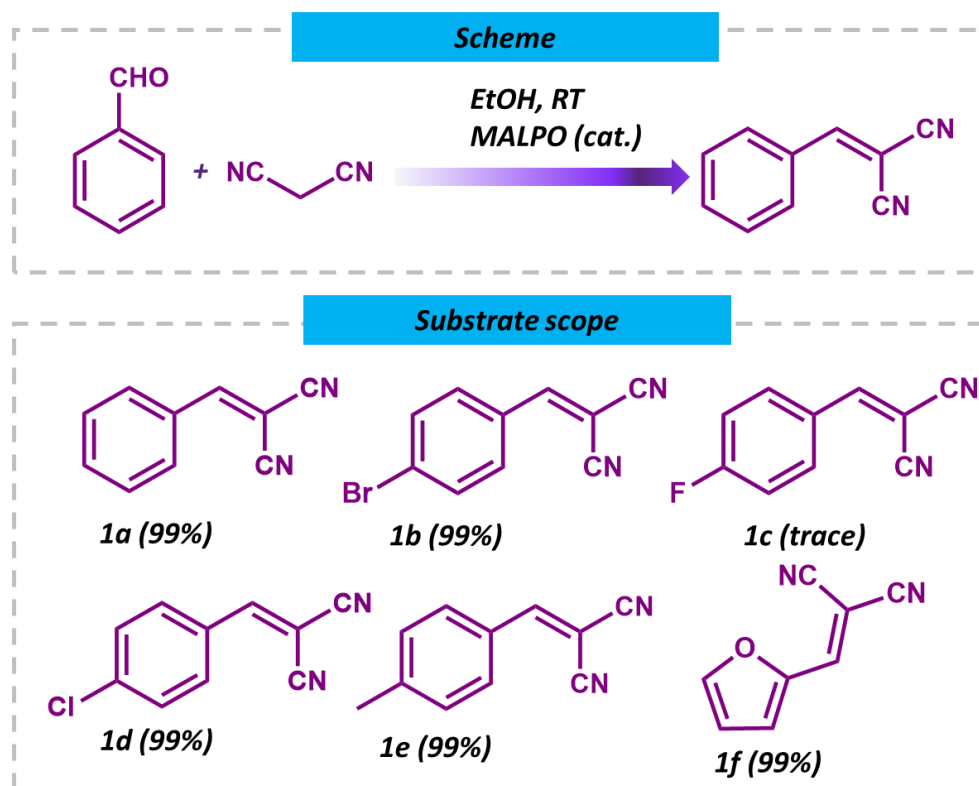


**Figure 7.** Conversion/selectivity plot with respect to the time (a) and the recyclability experiment (b).

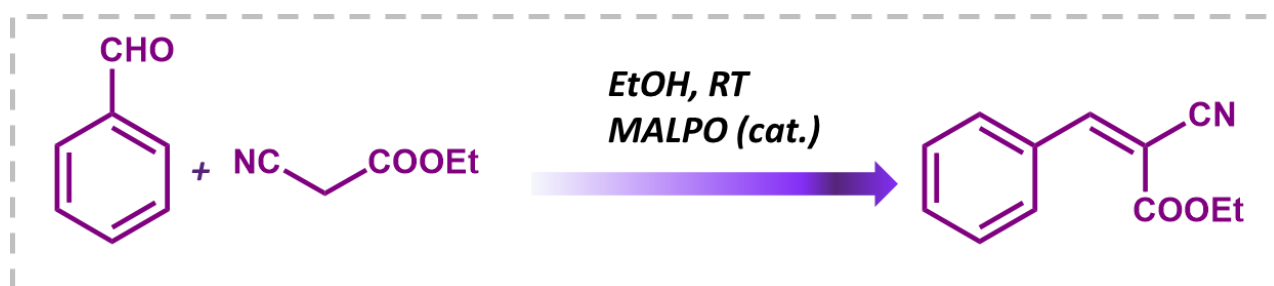
To verify that the observed reaction was solely stimulated by a solid catalyst and not due to active sites leaching into the solution, a leaching experiment was conducted under identical conditions. Specifically, the benzaldehyde and malononitrile reaction was initiated in the presence of MALPO under the same circumstances. After 30 min, an aliquot was extracted from the reaction mixture and filtered in order to eliminate the solid catalyst, allowing the resulting solution to continue reacting for an additional 30 min. The outcomes of this leaching experiment are presented in Figure S1 of the Supplementary Materials, which clearly demonstrate that the reaction rate experienced a substantial reduction in the absence of the catalyst following the filtration step. These results indicate that the presence of MALPO exclusively catalyzes the reaction, without any active sites leaching from the solid catalyst into the solution. However, the slight increase in the conversion of benzaldehyde after the catalyst's removal may be attributed to the contribution from the blank reaction, as indicated.

Having observed that the MALPO catalyst achieves an impressive 99% conversion of benzaldehyde to benzylidene malononitrile at room temperature, further experimentation at higher temperatures was deemed unnecessary. Subsequently, upon successfully optimizing the catalytic performance of MALPO for the Knoevenagel reaction, the scope of substrates was expanded to include aromatic-substituted aldehydes (Figure 8, 1a–1e) and biomass-derived heterocyclic aldehydes (Figure 8, 1f). Notably, the catalyst demonstrated the efficient conversion of various substrates, including those with electron-withdrawing groups in the para position and furfural, yielding their corresponding derivatives with high efficiency. However, para-fluoro benzaldehyde (Figure 8, 1c) proved to be an exception, as it did not undergo conversion under the same reaction conditions. The catalyst was also probed for a different active methylene group, such as ethyl cyanoacetate with benzaldehyde (Scheme 1), which showed a 94% conversion (Figure S6, ESI) regarding the condensation reaction under refluxing conditions. These findings highlight the unique catalytic prowess of MALPO and its broad substrate compatibility, thereby showcasing its

potential for diverse synthetic applications, ranging from aromatic substituted aldehydes to biomass-derived heterocyclic aldehydes.



**Figure 8.** Scheme and substrate scopes and reaction conditions for the Knoevenagel condensation reactions for MALPO.

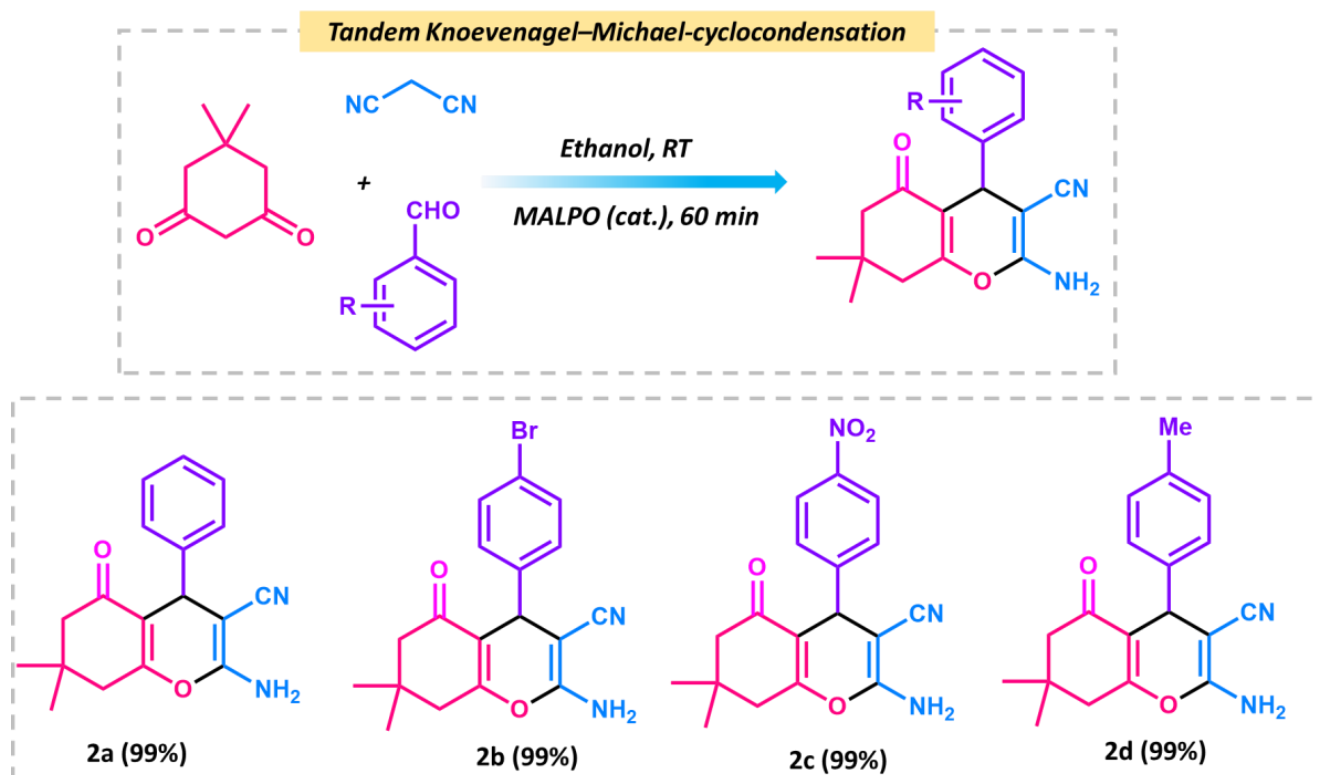


**Scheme 1.** Schematic representation of the Knoevenagel condensation of ethylcyanoacetate and benzaldehyde.

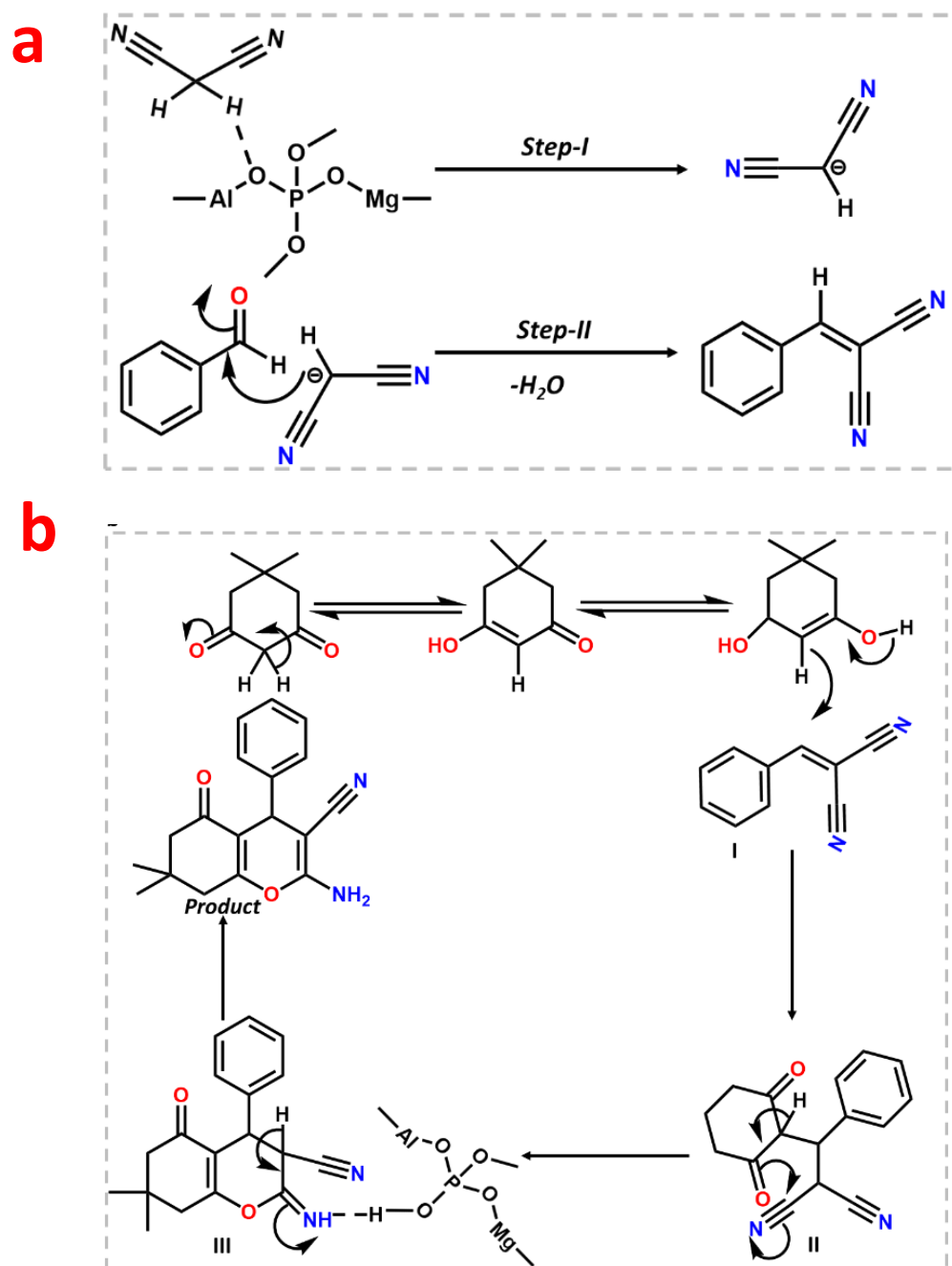
After the initial experiment, we ran a recyclability test for consecutive fourth cycle to verify the heterogeneity of the catalyst. The catalyst was collected after each cycle, properly washed with methanol, and activated at 120 °C for two hours to conduct the recyclability test. The catalyst was utilized for four successive cycles after it had been activated, and the conversion/selectivity plot is shown in Figure 7b. Up to the fourth cycle, no discernible difference in conversion or  $O_2$  at acid–base paired sites on the catalyst surface that effectively catalyze the deprotonating aldol–dehydration processes was observed. The powdered X-ray diffraction pattern was taken after the fourth cycle (Figure S8, ESI) to assess the stability of the MALPO, and it reveals that there was no structural change. According to Figure 8a, the high catalytic activity of MALPO could be attributed to the basic sites, which promote the abstraction of the protons and activate the malononitrile. This active

methylene attacks the  $-C=O$  bond of benzaldehyde, which further eliminate the water via aldol condensation, resulting in the final benzylidene malononitrile product.

After the Knoevenagel reaction, we further extended the procedure to produce tetrahydrobenzo[*b*]pyrans. This is a good example of tandem Knoevenagel–Michael cyclocondensation [56] reaction (Scheme 2). To perform the reaction, we chose malononitrile, aromatic aldehyde, and dimedone as model substrates in ethanol. The overall reaction was carried at room temperature, which resulted in a 99% conversion after 1 h of reaction. The reaction follows the same pathway, which follows the Knoevenagel in the first step and further reacts with dimedone to form the pyran derivative via cyclo condensation. The plausible mechanism is shown in Figure 9. In the first step, the MALPO catalyst activates the malononitrile to form the active methylene group, which reacts with the carbonyl group of the aldehyde to form the intermediate **I** via the removal of one molecule of  $H_2O$ . On the other hand, dimedone favors the enol form after tautomerization, which attacks the cyano-olefin compound **I** and which behave as a Michael acceptor to produce intermediate **II**. After the formation of intermediates **II**, it follows the cyclo-condensation via the bond shifting of  $-C=O$  to the corresponding nitrile group to form intermediate **III**. This intermediate **III** gives the final product by abstracting protons from the reaction mixture. After the successful conversion of the pyran derivatives of benzaldehyde, we examined the catalytic activity on the substrate scope for *p*-bromo derivatives, which provide 99% conversion. *p*-nitro derivatives also give higher yields. From the above mentioned results, it can be concluded that the catalyst is very efficient for both types of Knoevenagel condensation reactions as well as Knoevenagel–Michael cyclo-condensation. The higher activity of MALPO is due to the presence of basic sites as well as acidic sites in the framework.



**Scheme 2.** Schematic representation of tandem Knoevenagel–Michael cyclocondensation reactions between dimedone, benzaldehyde, and malononitrile.



**Figure 9.** Probable mechanistic pathway for the Knoevenagel condensation reaction (a) and Knoevenagel–Michael cyclo-condensation (b).

### 3. Experimental

#### 3.1. Characterizations

The bonding connectivity in the as-synthesized MALPO was analyzed using Fourier transform infrared (FTIR) spectroscopy and a Spectrum 100 spectrophotometer was used for the FTIR analysis (PerkinElmer, Cambridge, MA, USA). The crystalline nature of the phosphate materials was investigated using a Bruker D8 advance X-ray diffractometer, with  $\text{Cu K}\alpha$  ( $\lambda = 0.154 \text{ nm}$ ) is used as an X-ray source (Bruker AXS, Karlsruhe, Germany). The surface area of the material was investigated by analyzing the Brunauer–Emmett–Teller (BET) surface through  $\text{N}_2$  sorption analysis at 77 K using a Quantachrome Autosorb iQ surface area analyzer (Quantachrome Inc., Boynton Beach, FL, USA). In order to analyze

the data, the samples were activated in a hot air oven at 80 °C, followed by the gassing of the materials at 120 °C under continuous vacuum for 3 h. The pore size distribution was investigated using the non-local density functional theory (NLDFT) method. The morphological analysis of the materials was investigated by analyzing the images obtained from ultrahigh resolution transmission electron microscopy (UHR-TEM, JEOL, Tokyo, Japan). The conformation of the catalytic products was evaluated through nuclear magnetic resonance (NMR) spectroscopy using a Bruker Avance NMR spectrometer (Bruker AXS, Germany). The elemental distribution in the material architecture was analyzed using the elemental distribution images obtained through energy dispersive spectroscopy (EDS). The JEOL 2010 TEM (JEOL, Japan), operated at 200 kV, was utilized to capture ultrahigh-resolution transmission emission microscopy (UHR-TEM) images. For the TEM analysis, the sample was dispersed in methanol and then drop-cast onto a copper grid coated with a carbon polymer. For the temperature programmed desorption analysis of CO<sub>2</sub> (CO<sub>2</sub>-TPD), the MALPO sample was activated at 250 °C under a He flow of 2 h. Then, after cooling the sample to room temperature, CO<sub>2</sub> was purged in the absence of a carrier gas flow for 30 min. Then, the sample temperature was raised in a step-wise manner with a heating rate of 10 °C min<sup>-1</sup>. The desorbed CO<sub>2</sub> in the temperature range 50 to 875 °C was analyzed using a thermal conductivity detector fitted in a AMI-300 Chemisorption Analyzer (Altamira Instruments, Pittsburgh, PA, USA).

### 3.2. Chemicals

Magnesium nitrate hexahydrate (Mg(OH)<sub>2</sub> 6H<sub>2</sub>O) (Spectrochem, Mumbai, India), and aluminum nitrate nonahydrate (Al(NO<sub>3</sub>)<sub>3</sub> 9H<sub>2</sub>O) and 28% ammonium hydroxide solutions were purchased from Merck, Bengaluru, India. Phosphoric acid (H<sub>3</sub>PO<sub>4</sub>) was purchased from TCI Chemicals, India. Benzaldehyde was purchased from Spectrochem, India, Furfural was purchased from Sigma-Aldrich (St. Louis, MO, USA), and 4-chlorobenzaldehyde and 4-bromobenzaldehyde were purchased from Merck, India. Dimedone and malononitrile were purchased from Sigma-Aldrich (USA). Of the solvents, ethanol was purchased from Bengal Chemicals (Kolkata, India); acetone and methanol were purchased from Finar Chemicals (Mumbai, India); and the NMR solvent CDCl<sub>3</sub> was purchased from Sigma-Aldrich (USA). All the reagents and solvents were used without any further purification.

### 3.3. Synthesis of MALP

Magnesium aluminum phosphate was synthesized via a typical hydrothermal [39] method. In the synthetic procedure, 1.54 g of phosphoric acid was dissolved in 10 mL of distilled water, 1.28 g of magnesium nitrate hexahydrate (Mg(NO<sub>3</sub>)<sub>2</sub> 6H<sub>2</sub>O; 0.005 mmol) and 1.87 g of aluminum nitrate nonahydrate (Al(NO<sub>3</sub>)<sub>3</sub> 9H<sub>2</sub>O, 0.005 mol) were separately placed in 5 mL distilled water. The metal precursor solutions were added simultaneously drop-wise, followed by the addition of 28% ammonium hydroxide solution (NH<sub>4</sub>OH) in order to maintain a fixed pH of 7. The final solution was kept under vigorous stirring at room temperature for another 3 h. Finally, the solution was transferred to a stainless steel hydrothermal autoclave and kept static for 72 h at 180 °C in a hot air oven. After that, the white precipitate obtained was filtered, followed by washing with water, methanol, and tetrahydrofuran. Finally, the product was dried at 80 °C under vacuum. The material was then characterized using X-ray diffraction, Fourier-transform infrared spectroscopy, transmission electron microscopy, and nitrogen sorption isotherm analysis.

### 3.4. Catalytic Activity of MALPO

In order to conduct the catalytic activity test for the Knoevenagel condensation reaction, we carried out the following experiment. A total of 2 mmol of aromatic aldehydes was placed in a 50 mL round-bottomed flask. Then, 2 mmol of malononitrile was added, along with the pre-activated catalyst MALPO (10 mg), followed by the addition of 10 mL ethanol. The reaction mixture was then stirred at 400 rpm for the desired time and monitored via thin-layer chromatography (TLC). After the completion of the reaction, the reaction mixture

was filtered in order to separate out the solid catalyst. Thereafter, the liquid was dried under reduced pressure to obtain solid product. The conformation of the product was evaluated via  $^1\text{H}$  NMR spectroscopy, where  $\text{CDCl}_3$  was used as an NMR solvent.

### 3.5. Catalyst Recyclability Experiment

To assess the reusability of MALPO, we performed catalytic recyclability tests. After the catalytic performance, the MALPO material was recovered via filtration. The catalyst was then subjected to a series of washes using distilled water, methanol, and ethanol, followed by vacuum drying. This process regenerated the catalyst, allowing us to employ it for up to four consecutive catalytic cycles. Through this evaluation, we aimed to determine the extent to which MALPO could be reused as a catalyst, providing valuable insights into its potential for sustainable and efficient applications.

## 4. Conclusions

In summary, herein, we successfully synthesized porous magnesium aluminum mixed-metal phosphate MALPO using ortho phosphoric acid as a phosphate source. MALPO synthesized through a template free approach was found to possess a high specific surface area and a novel triclinic crystal structure. The basic sites present in the material make it a very efficient catalyst for the heterogeneous Knoevenagel condensation reaction. The series of substrates investigated result in excellent product yields of up to 99%. Furthermore, the recyclability test carried out demonstrated the enhanced recyclability of MALPO without any loss of structural integrity, which further concludes the long term applicability of the material towards heterogeneous catalysis. In conclusion, our investigation reveals that the novel mixed-metal phosphate material MALPO holds promise as a potential catalyst for facilitating the Knoevenagel condensation reaction. This observation suggests that MALPO exhibits favorable catalytic properties and could play a crucial role in meeting the growing demand for the synthesis of value-added chemicals, involving a new C–C bond. By offering enhanced catalytic efficiency, MALPO has the potential to contribute significantly to the development and validation of advanced chemical synthesis strategies in the near future. Further research and exploration are warranted in order to fully exploit the capabilities of MALPO and optimize its performance when catalyzing the Knoevenagel condensation reaction.

**Supplementary Materials:** The following supporting information can be downloaded at: <https://www.mdpi.com/article/10.3390/catal13071053/s1>, Figure S1: Leaching experiment indicating no leaching of active sites during catalysis, Figure S2:  $^1\text{H}$  NMR of 2-benzylidenemalononitrile, Figure S3:  $^1\text{H}$  NMR of 2-(4-chlorobenzylidene)malononitrile, Figure S4:  $^1\text{H}$  NMR of 2-(furan-2-ylmethylene)malononitrile, Figure S5:  $^1\text{H}$  NMR of 2-(4-bromobenzylidene)malononitrile, Figure S6:  $^1\text{H}$  NMR of ethyl (*E*)-2-cyano-3-phenylacrylate, Figure S7:  $^1\text{H}$  NMR of 2-amino-7,7-dimethyl-5-oxo-4-((*p*-tolyl)-5,6,7,8-tetrahydro-4(*H*)-chromene-3-carbonitrile, Figure S8: PXRD pattern of recycled catalyst, Figure S9: (a) TEM image of MALPO; (b) distribution of oxygen in MALPO. Table S1: Indexing of triclinic phase of MALPO with space group P1.

**Author Contributions:** Experiments, investigation, and formal analysis were carried out by A.C. and S.B. S.C. was involved in the crystal structure analysis. B.M. and A.M. were involved in the formal analysis of the catalysts and products. A.B. provided the resources, investigation, and overall supervision of this project. A.C. wrote the draft manuscript with the help of A.B. All authors have read and agreed to the published version of the manuscript.

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## Article

# Electrochemical Promotion of CO<sub>2</sub> Hydrogenation Using Rh Catalysts Supported on O<sup>2−</sup> Conducting Solid Electrolyte

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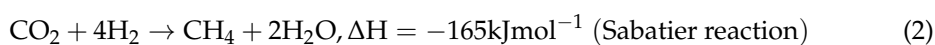
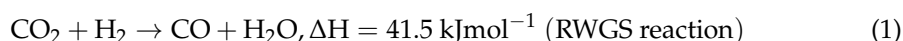
**Abstract:** Electrochemical promotion was used to modify the activity and selectivity of a Rh catalyst electrode in the CO<sub>2</sub> hydrogenation reaction. The experiments were carried out in a temperature range of 350–430 °C at ambient pressure and at different CO<sub>2</sub> to H<sub>2</sub> gas feeding ratios (1:2 to 4:1). The only reaction products observed were CO and CH<sub>4</sub>, both under open- and closed-circuit conditions. The CH<sub>4</sub> formation rate was found to increase with both positive and negative potential or current application. The CO formation rate followed the opposite trend. The selectivity to CH<sub>4</sub> increased under high values of hydrogen partial pressure and decreased at high pressures of CO<sub>2</sub>. The results demonstrate how electrochemical promotion can be used to finely tune activity and selectivity for a reaction of high technical and environmental importance.

**Keywords:** electrochemical promotion of catalysis (EPOC); non-faradaic electrochemical modification of catalytic activity (NEMCA); CO<sub>2</sub> hydrogenation; rhodium (Rh); YSZ; XPS

## 1. Introduction

Carbon dioxide (CO<sub>2</sub>) is the most abundant greenhouse gas in our atmosphere with its concentration drastically increasing over time due to anthropogenic activities, most crucially the extensive use of fossil fuels for transport and power generation purposes. The ever-increasing CO<sub>2</sub> emissions in the atmosphere have gradually led to climate change, which is strongly associated with global warming, extreme weather conditions, and other major environmental threats [1–4]. In this regard, it is of foremost importance to globally minimize the use of fossil fuels, and accordingly, develop the necessary technologies for capturing and utilizing CO<sub>2</sub> to produce fuels, bulk chemicals, and value-added products. It is widely accepted that CO<sub>2</sub> hydrogenation may offer a relatively economic and effective way of controlling and making use of the CO<sub>2</sub> excess atmospheric levels [5–7].

Most studies of the catalytic hydrogenation of CO<sub>2</sub> have been performed in fixed-bed reactors using mainly metal catalysts (e.g., Rh, Pd, Ru, Cu, Fe, Co, Ni, Au, Ag) supported over a wide range of metal oxides (e.g., Nb<sub>2</sub>O<sub>3</sub>, ZrO<sub>2</sub>, Al<sub>2</sub>O<sub>3</sub>, SiO<sub>2</sub>) [8–37] and utilizing high pressures (5–70 atm) [12–15,17,24–28,30] which shift the thermodynamic equilibrium towards methanol and light hydrocarbon production. Under atmospheric pressure, CO<sub>2</sub> can be reduced by hydrogen to form methane (Sabatier reaction) and/or carbon monoxide (reverse water gas shift, RWGS, reaction) according to the following equations:



The RWGS reaction is endothermic and is thermodynamically favored at high operating temperatures. Contrary to this, the Sabatier reaction leads to the formation of methane, which is an exothermic reaction and is favored at low operation temperatures. However, the low operation temperatures limit the activity and the kinetics of the reactions as well.

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Therefore, it is essential to develop active and selective low temperature catalytic processes, operating at high CO<sub>2</sub> to H<sub>2</sub> feed ratios and atmospheric pressure.

The electrochemical promotion of CO<sub>2</sub> hydrogenation has been studied in recent years over different catalytic films including noble and non-noble metals (Ru [7,38–43] and Rh [44,45], and Ni, Co, Fe [46,47], respectively) supported on a variety of solid electrolytes including yttria-stabilized-zirconia (YSZ, an O<sup>2−</sup> conductor [7,38,44,45]), H<sup>+</sup> conductors [40,43,46], and alkali ion conductors such as Na-β"-Al<sub>2</sub>O<sub>3</sub> [40]. Under open circuit conditions, the non-promoted catalytic reaction takes place on the catalyst-working electrode. Application of a potential or current, between the catalyst film (working electrode) and a counter electrode, leads to changes of the conversion rate and product selectivity [7,38,48–56]. These non-Faradaic changes are evoked by the formation of an effective double layer due to the migration of promoting species (e.g., O<sup>2−</sup> in the case of YSZ) migrating from the solid electrolyte to the metal–gas interface [7,38,49,57–59].

The CO<sub>2</sub> hydrogenation reaction on Rh catalyst-electrodes deposited on YSZ has been rarely investigated and mainly under conditions of excess of hydrogen (regarding Equation (1)) and cathodic polarizations. The study of the reaction in a single chamber reactor by Bebelis et al. [44] led to CO and CH<sub>4</sub> formation at temperatures of 346–477 °C. It was found that the rate of CH<sub>4</sub> formation is enhanced with positive potentials (electrophobic behavior) while the rate of CO formation is enhanced with negative potentials (electrophilic behavior). The maximum selectivity to CH<sub>4</sub> was up to 35%. Using a monolithic electro-promoted reactor (MEPR) [45], the reaction of CO<sub>2</sub> hydrogenation was studied on 22 thin Rh/YSZ/Pt plate cells at temperatures between 220 and 380 °C. The only products observed were, again, CO and CH<sub>4</sub>. The rates of both reactions were significantly affected during polarization, while the selectivity to CH<sub>4</sub> remained always below 12%.

The pronounced catalytic activity of Rh-based catalysts, supported on O<sup>2−</sup> conductors, under electro-promoted conditions have been associated in earlier studies with the decomposition of the rhodium oxide to metallic rhodium, which is more active especially under oxidation reaction conditions [57–59].

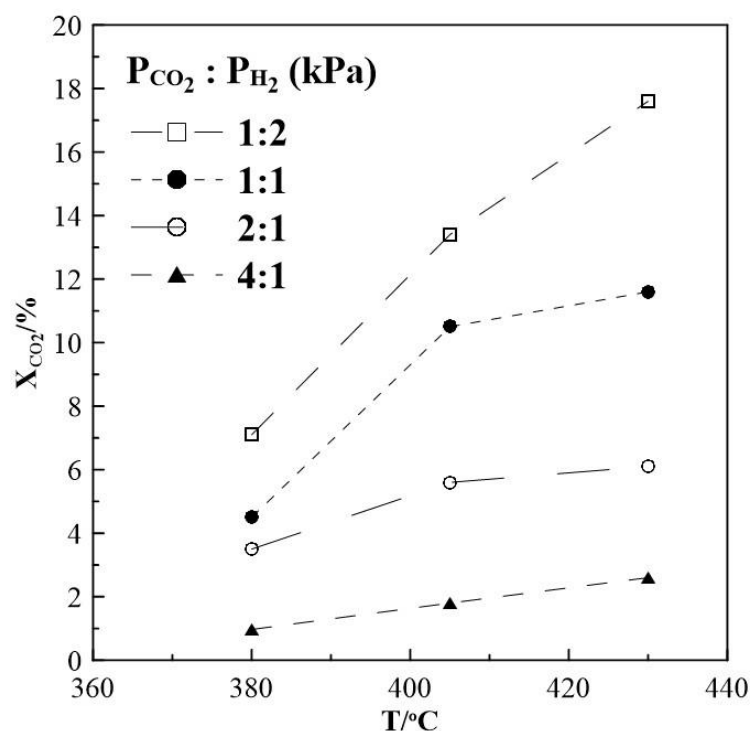
In the present study, the electrochemical promotion of CO<sub>2</sub> hydrogenation reaction was studied over a Rh catalyst-electrode deposited on an O<sup>2−</sup> solid electrolyte conductor, YSZ, at atmospheric pressure, and for the first time, in a continuous single pellet flow reactor. The main scopes were in contrast to earlier studies: to perform CO<sub>2</sub> hydrogenation at a lower temperature range of 350–430 °C and at different CO<sub>2</sub> to H<sub>2</sub> cofeeding ratios.

## 2. Results and Discussion

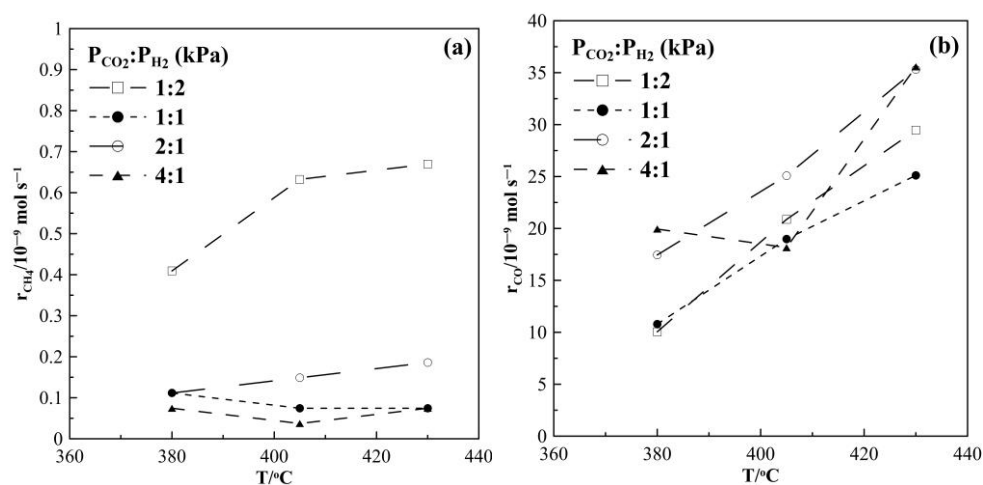
### 2.1. Hydrogenation Activity Measurements

The steady-state-CO<sub>2</sub> conversion as a function of temperature for different CO<sub>2</sub> to H<sub>2</sub> ratios was first investigated. The results displayed in Figure 1 show that the conversion of CO<sub>2</sub> increases with increasing temperature reaching a maximum of 17.6% under reaction conditions of CO<sub>2</sub> to H<sub>2</sub> feeding ratio of 1:2. Under conditions of CO<sub>2</sub> to H<sub>2</sub> of 1:1 the conversion drops to 12% and is smallest with 6% and 2% at CO<sub>2</sub> to H<sub>2</sub> ratios of 2:1 and 4:1, respectively.

Figure 2 shows the CH<sub>4</sub> and CO production rates at steady state as a function of temperature. The rate of the methanation reaction was found to be highest for a gas feed ratio of CO<sub>2</sub> to H<sub>2</sub> of 1:2. With increasing CO<sub>2</sub> partial pressure in the reaction mixture, i.e., a CO<sub>2</sub> to H<sub>2</sub> ratio of 1:1, 2:1 and 4:1, the observed CH<sub>4</sub> formation rate is very low and almost independent of temperature. Figure 2b suggests that the RWGS reaction prevails over the Sabatier reaction. Moreover, as shown in Figure 3, CO appears to be the main product under all feeding CO<sub>2</sub> to H<sub>2</sub> ratios of this study and its selectivity is higher than 96%, while CH<sub>4</sub> selectivity is smaller than 4%. The reaction rate values of the RWGS reaction are more than one order of magnitude higher than those of the methanation one.



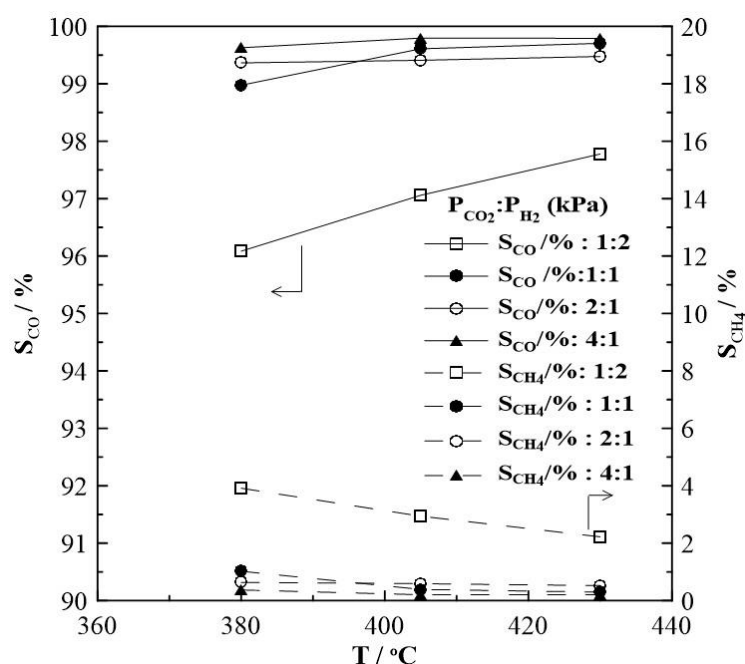
**Figure 1.** Steady-state effect of temperature on CO<sub>2</sub> conversion. Different gas feeding ratios of CO<sub>2</sub> to H<sub>2</sub>.  $F_T = 50 \text{ cm}^3 \text{ min}^{-1}$ .



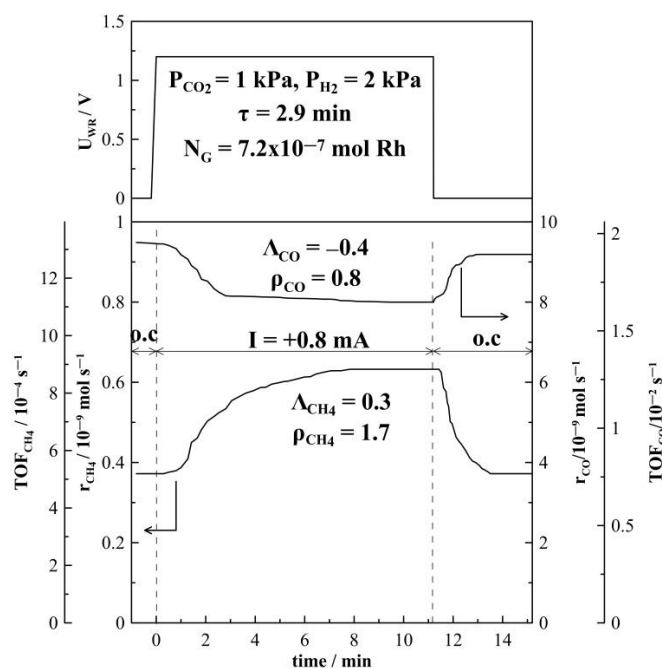
**Figure 2.** Steady-state effect of temperature on (a) CH<sub>4</sub> formation rate and (b) CO formation rate. Different gas feeding ratios of CO<sub>2</sub> to H<sub>2</sub>.  $F_T = 50 \text{ cm}^3 \text{ min}^{-1}$ .

Figures 4 and 5 depict the transient effect of constant applied positive (Figure 4) and negative (Figure 5) current on the catalytic rate and turnover frequency (TOF) for the formation of CH<sub>4</sub> and CO at a CO<sub>2</sub> to H<sub>2</sub> ratio of 1:2 at 380 °C. Initially, as presented in Figure 4, at  $t < 0$ , the circuit is open and the steady-state formation rates of CH<sub>4</sub> and of CO are equal to  $0.38 \times 10^{-9} \text{ mol s}^{-1}$  and  $9.2 \times 10^{-9} \text{ mol s}^{-1}$  respectively. At  $t = 0$ , a constant anodic current ( $I = +0.8 \text{ mA}$ ) is applied between the catalyst and counter electrode, which causes an applied potential of  $U_{WR} = +1.2 \text{ V}$ . Oxygen ions,  $\text{O}^{2-}$ , are transferred from the YSZ support to the Rh catalyst-electrode at a rate of  $I/2F$  equal to approximately  $10^{-3} \text{ s}^{-1}$ . The rate of CH<sub>4</sub> increases and approaches a new steady-state value ( $r_{\text{CH}_4} = 0.62 \times 10^{-9} \text{ mol s}^{-1}$ ). This increase of the CH<sub>4</sub> catalytic rate ( $\Delta r = 0.24 \times 10^{-9} \text{ mol s}^{-1}$ ) is 1.7 times greater than the initial rate achieved under open circuit conditions. The CO formation rate decreases under anodic current application to  $8.0 \times 10^{-9} \text{ mol s}^{-1}$ , resulting in a rate enhancement

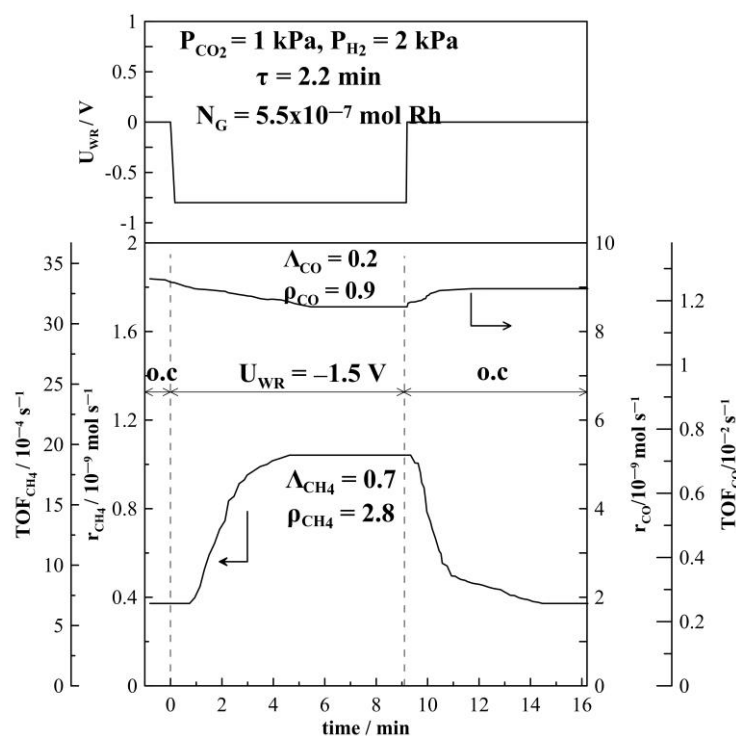
value of  $\rho = 0.84$ . After current interruption, the  $\text{CH}_4$  rate of formation returns to its initial open circuit value (reversible behavior), while the  $\text{CO}$  formation rate returns only to a value above the initial open circuit rate (non-reversible behavior). A very similar trend is observed under cathodic current application, as shown in Figure 5. The decrease in  $\text{CO}$  formation rate is less pronounced with a rate enhancement ratio,  $\rho$ , (see Equation (5) in Section 3.3) equal to 0.94. After current interruption, the rate does not return to its initial open circuit value. Under cathodic current application,  $\text{CH}_4$  formation rate is increased and a rate enhancement  $\rho$ -value of 2.7 is estimated.



**Figure 3.** Steady-state effect of temperature on the selectivity to  $\text{CO}$  and  $\text{CH}_4$  formation under open circuit conditions and at different gas feeding ratios of  $\text{CO}_2$  to  $\text{H}_2$ .  $F_T = 50 \text{ cm}^3 \text{ min}^{-1}$ .



**Figure 4.** Transient effect of constant applied current ( $I = +0.8 \text{ mA}$ ) on the formation rate of  $\text{CH}_4$  and  $\text{CO}$  at  $T = 380 \text{ °C}$  and  $\text{CO}_2$  to  $\text{H}_2$  ratio of 1:2.  $F_T = 50 \text{ cm}^3 \text{ min}^{-1}$ .



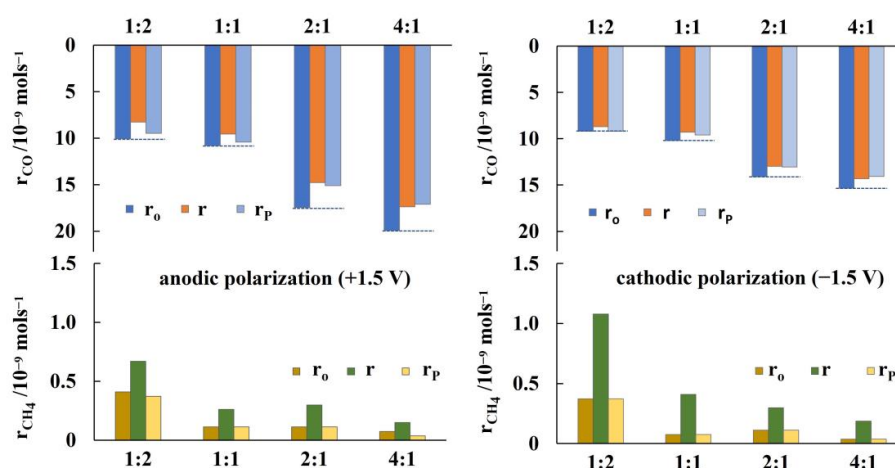
**Figure 5.** Transient effect of constant applied current ( $I = -0.8$  mA) on the formation rate of  $\text{CH}_4$  and CO at  $T = 380$  °C and  $\text{CO}_2$  to  $\text{H}_2$  ratio of 1:2.

The time constant,  $\tau$ , given in both Figures 4 and 5, is defined as the time required for the rate increase  $\Delta r$  to reach 63% of its new steady-state value during a galvanostatic transient [38,59]. When an  $\text{O}^{2-}$  ion conductor is used, the magnitude of  $\tau$  can be generally predicted by

$$\tau \approx \frac{2FN_G}{I} \quad (3)$$

where  $N_G$  (mol) is the reactive oxygen uptake on the metal catalyst. The time constant  $\tau$  expresses the time required to form a monolayer of  $\text{O}^{\delta-}$  on the metal surface, while  $N_G$  expresses, approximately, the surface mols of metal—here, Rh. The average active catalyst surface area,  $N_G$ , which is equal to  $7.62 \times 10^{-7}$  mol Rh, has been calculated based on 6 galvanostatic transients. The estimated value of  $N_G$  agrees well with the values found in previous studies of Rh catalyst electrodes supported on YSZ [44,45,56,59]. The average  $N_G$  value obtained was used to calculate turnover frequencies (TOFs) for  $\text{CH}_4$  and CO formation. TOFs for  $\text{CH}_4$  formation are found to be small and in the order of  $10^{-4} \text{ s}^{-1}$ , which is in good agreement with the literature data [21].

The non-reversible behavior of CO formation has been further investigated by repeated current and/or potential application, which have generally shown that upon current and/or potential interruption the rate of CO formation does not return to its initial open circuit value. Figure 6 summarizes the results for potentiostatic transient operation at different  $\text{CO}_2$  to  $\text{H}_2$  feed ratios. The bottom part of the figure shows that the increase in  $\text{CH}_4$  formation rate under anodic and cathodic polarization (+ and  $-1.5$  V), which is more pronounced at high  $\text{H}_2$  to  $\text{CO}_2$  feeding ratios, is reversible. However, the CO formation rate, as shown in the top part of Figure 6, exhibits a “permanent”, non-reversible NEMCA behavior [60,61]. The guide (dotted) lines clearly show that this non-reversible effect of current and/or potential application is more pronounced at higher  $\text{CO}_2$  to  $\text{H}_2$  feed ratios.

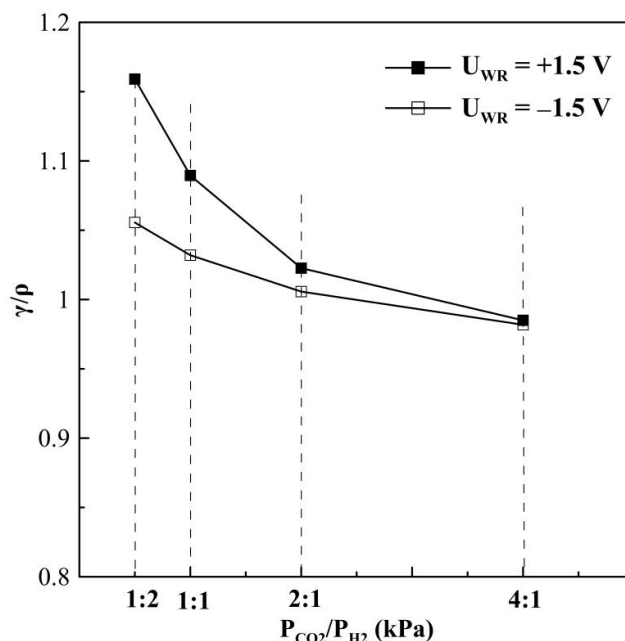


**Figure 6.** Transient effect of constant applied potential (left +1.5 V, right −1.5 V) on the formation rates of CH<sub>4</sub> and CO at T = 380 °C and at different ratios of CO<sub>2</sub> to H<sub>2</sub>. Dotted lines in the sketch for the CO formation rates point guidance for the non-reversible behavior of the open circuit rate after potential interruption, for details see text. F<sub>T</sub> = 50 cm<sup>3</sup> min<sup>−1</sup>. R<sub>o</sub> is the formation rate under open circuit conditions, r is the formation rate under potentiostatic polarization, and r<sub>p</sub> corresponds to the formation rate after potential interruption.

The “permanent” rate enhancement ratio  $\gamma$ , was defined for the first time by Comninellis et al. [61] as

$$\gamma = r_p / r_o \quad (4)$$

where  $r_p$  is the “permanent” promoted catalytic rate after current or potential interruption, and  $r_o$  is the unpromoted rate (i.e., the open-circuit catalytic rate). Figure 7 displays the non-reversibility magnitude of CO formation for different gas feed ratios. Under reaction conditions of a CO<sub>2</sub> to H<sub>2</sub> ratio of 1:2, the  $\gamma/\rho$  ratio is higher than 1, expressing, that the CO formation rate observed under potential application partially returns to its initial open circuit value. However,  $\gamma/\rho$  ratio equals to 1 for a reaction mixture with a CO<sub>2</sub> to H<sub>2</sub> ratio of 4:1 and a significant “permanent” NEMCA behavior is observed.

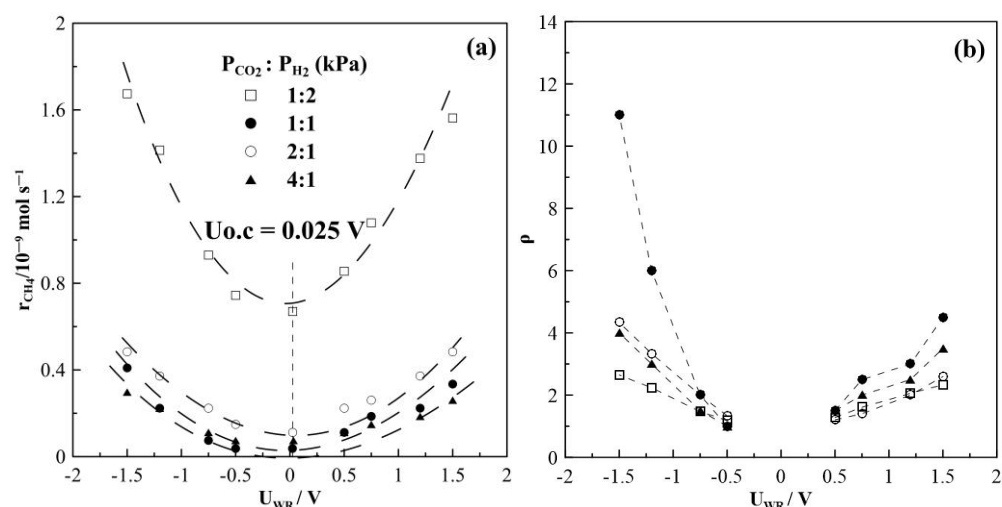


**Figure 7.** Ratio of “permanent” rate enhancement  $\gamma$  to rate enhancement  $\rho$  for CO formation at different gas feeding ratios, T = 380 °C.



In the general case of an oxidation reaction on catalysts deposited on  $O^{2-}$  conductors, like YSZ, the ionic species migrating in the solid electrolyte is participating in the electrochemical reaction leading to distinct values of apparent Faradaic efficiency,  $|\Lambda| > 1$  (see Equations (6)–(8), Section 3.3). In the present case, however, in which oxygen is not a reactant, any positive current or positive potential-induced catalytic rate change denotes electrochemical promotion, even when  $|\Lambda| < 1$  [39].

Figure 8 summarizes the results of steady-state potential application on the rate of  $CH_4$  formation at  $T = 430^\circ C$ , for which the highest rate enhancement ratio,  $\rho$  has been found. The observed currents do not depend on gas feed conditions, which means they are almost equal at a given potential and do not depend on the  $CO_2$  to  $H_2$  ratios. This observation is one of the very first hints that the overall oxidation state of the film remains relatively unchanged during the course of the reaction. The rate of  $CH_4$  production displays an inverted volcano type behavior, i.e., it increases with increasing and decreasing catalyst potential as shown in Figure 8a. Maximum changes in the  $CH_4$  rate are observed under reaction conditions of a  $CO_2$  to  $H_2$  ratio of 1:2, but the highest rate enhancement ratios are achieved at conditions of  $CO_2:H_2 = 1:1$ , with  $\rho$  reaching values of up to 11. If the partial pressure of  $CO_2$  is further increased, i.e.,  $CO_2$  to  $H_2$  ratios of 2:1 and 4:1, methane formation is found to be small with values below  $0.6 \times 10^{-9} \text{ mol s}^{-1}$ . Despite this, however, methane formation can be electrochemically promoted with  $\rho$ -values of up to 5. Product selectivity towards  $CH_4$  is electrochemically promoted under anodic and cathodic polarization; furthermore, it is highest under reaction conditions of a  $CO_2$  to  $H_2$  ratio of 1:2, but does not exceed 10%, as seen in Figure 9.



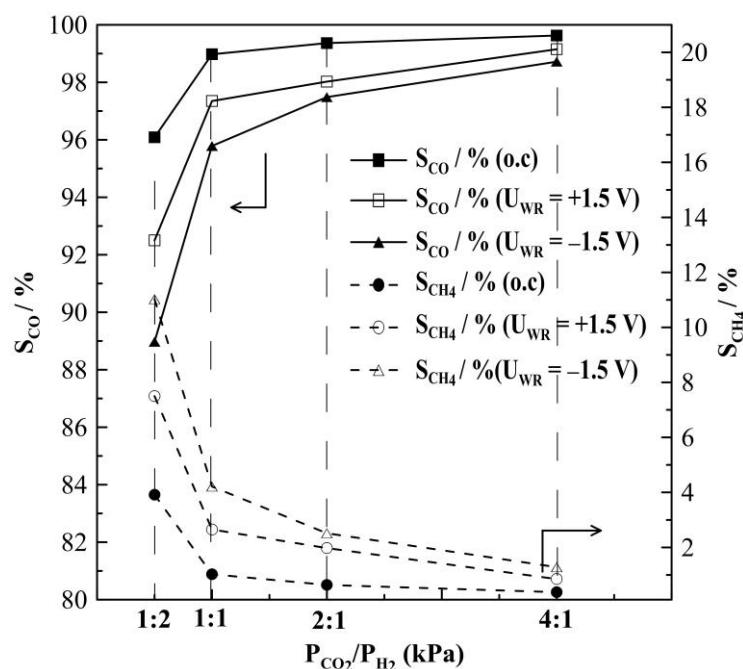
**Figure 8.** Steady-state effect of potential on (a)  $CH_4$  formation rate and (b) the corresponding rate enhancement ratio,  $T = 430^\circ C$ , different gas feeding ratios,  $F_T = 50 \text{ cm}^3 \text{ min}^{-1}$ .

## 2.2. Catalyst Characterization

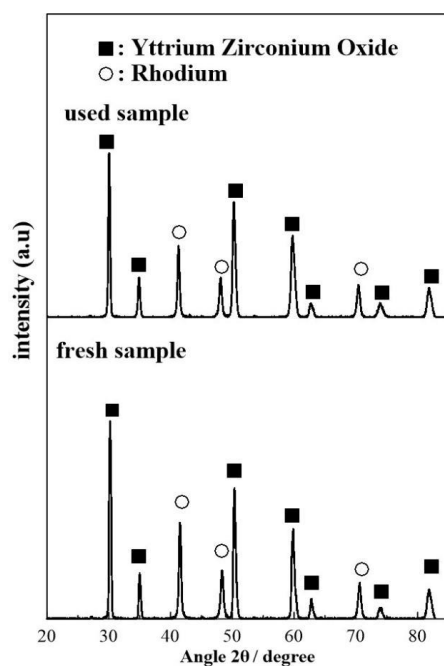
The morphology and chemical state of the Rh/YSZ film was assessed with XRD (X-ray diffraction), SEM (scanning electron microscopy) and XPS (X-ray photoelectron spectroscopy). The characterization studies were carried out on 2 different samples, designated as fresh and used, which correspond to the freshly reduced (i.e., after treatment in 15%  $H_2$  in He) and a post-experiment (i.e., after exposure to different  $CO_2 : H_2$  gas feed compositions) Rh/YSZ catalyst electrode, respectively.

The diffractograms displayed in Figure 10 show no major differences in the phase distribution of the fresh and used sample. More specifically both diffractograms show clear reflections at  $2\theta = 30.3^\circ, 35.0^\circ, 50.4^\circ, 59.9^\circ, 62.9^\circ, 74.1^\circ$ , and  $81.9^\circ$ , which correspond to the (111), (200), (220), (311), (222), (400), (331) planes of YSZ [62–67]. In addition, both diffractograms show clear reflections at  $41.5^\circ, 48.4^\circ$ , and  $70.7^\circ$  which correspond to the (111), (200), and (220) phases Rh particles in their metallic ( $Rh^0$ ) state [66]. No reflections

corresponding to  $\text{RhO}_2$  or  $\text{Rh}_2\text{O}_3$  were detected in the XRD measurements, suggesting that the chemical state of the Rh film is mostly metallic before and after use.



**Figure 9.** Steady-state effect of gas feeding ratios of  $\text{CO}_2$  to  $\text{H}_2$  on the selectivity to  $\text{CO}$  and  $\text{CH}_4$  formation on Rh catalyst under open and closed-circuit conditions,  $T = 380^\circ\text{C}$ .

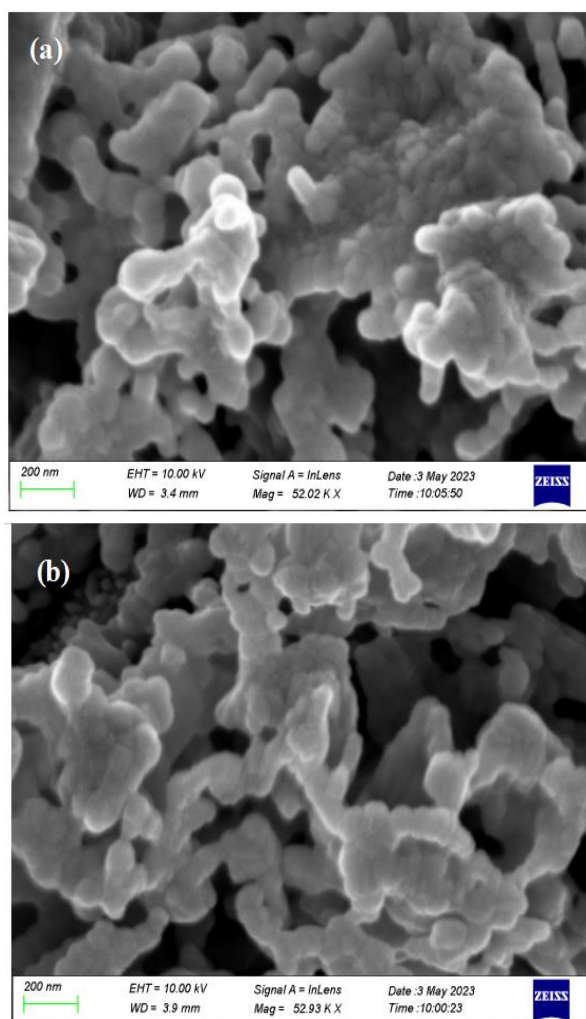


**Figure 10.** XRD patterns of the freshly reduced and used (after exposing to experimental operating conditions) sample.

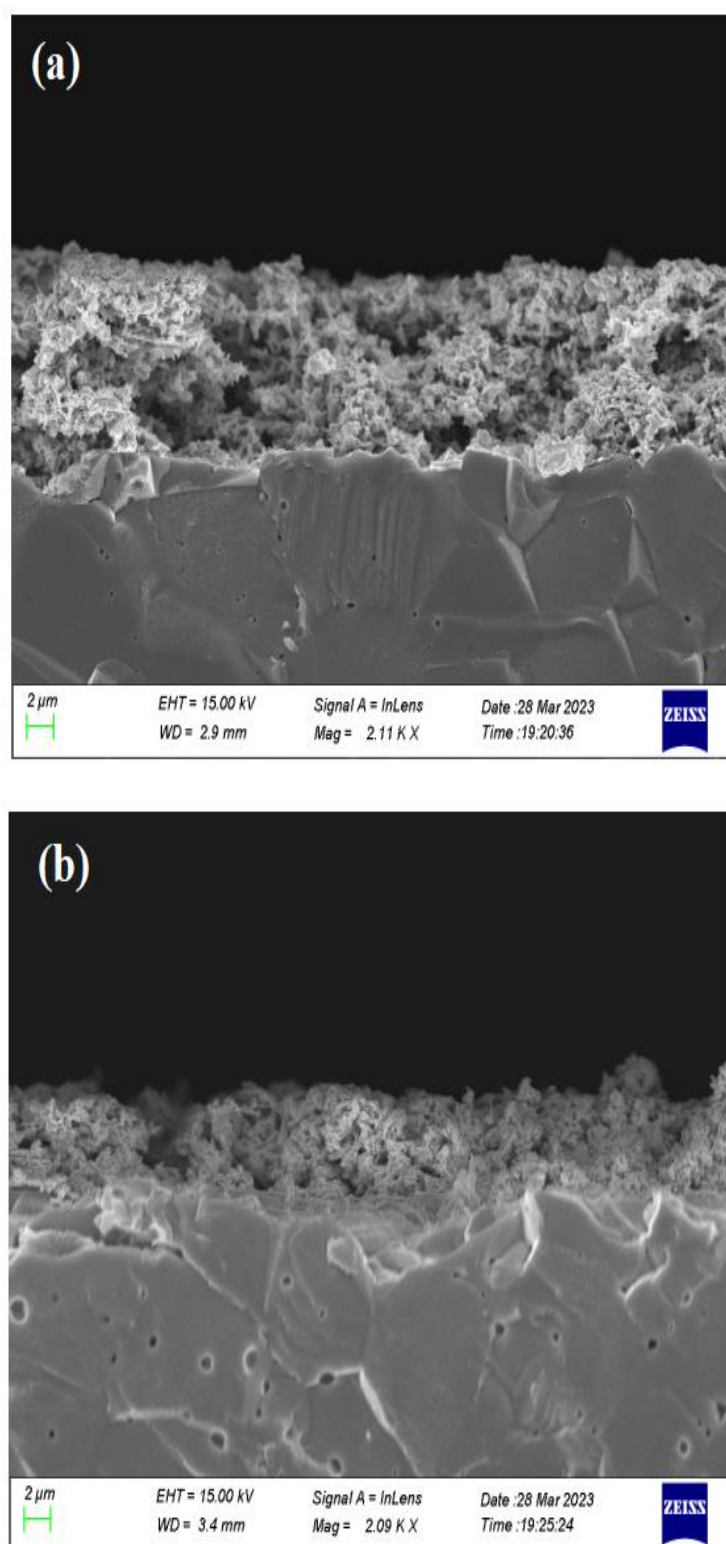
The mean Rh crystallite size of the fresh and used samples were calculated by means of the Scherrer equation [65] by assuming a spherical crystallite shape and averaging the crystalline domain diameter obtained for the (111), (200), and (220) reflections. The size of the Rh crystallites in the fresh sample ( $19.9 \pm 0.8\text{ nm}$ ) was found to be slightly smaller as compared to the used sample ( $24 \pm 1\text{ nm}$ ), which suggests that some degree of crystallite size increase during the course of the electrocatalytic reaction due to agglomeration.

Previous XRD studies on Rh/YSZ systems have shown that after reduction and prior to experimental measurements the metallic phase of Rh is mainly present in the sample with only tracers of metal oxides being detectable [66]. Using metalorganic paste (Engelhard 8826) as a precursor, Jimenez et al. reported rhodium crystallite sizes equal to  $58.5 \pm 0.3$  nm, calculated by the XRD patterns of the reduced sample [66]. The observed size variation and the Rh<sup>0</sup>: Rh oxide ratio were attributed to the different conditions of calcination and reduction conditions of the working Rh-catalyst electrode.

Top view and cross section SEM images of the fresh and used catalyst film are shown in Figures 11 and 12, respectively. Overall, the sample preparation method followed in this work has led to a continuous rhodium film, sufficiently porous which facilitates the efficient access of both reactants and products on the Rh active sites, and well attached to the YSZ support to ensure an electrochemically active interface. The apparent average particle size is estimated to be 40 nm, which is roughly twice the crystallite size calculated from the XRD spectra. It is worth mentioning here that particle size estimation from the SEM images is limited by the resolution of the instrument. Both the morphology and structure of the Rh film appears to be unchanged comparing the images from the sample prior experiment and after exposing it to reaction conditions. The thickness of the catalyst film was estimated from the cross-section micrograph and was found to be in the range of 6.5–10  $\mu\text{m}$ , which is a common thickness for films prepared by applying metalorganic pastes [38].



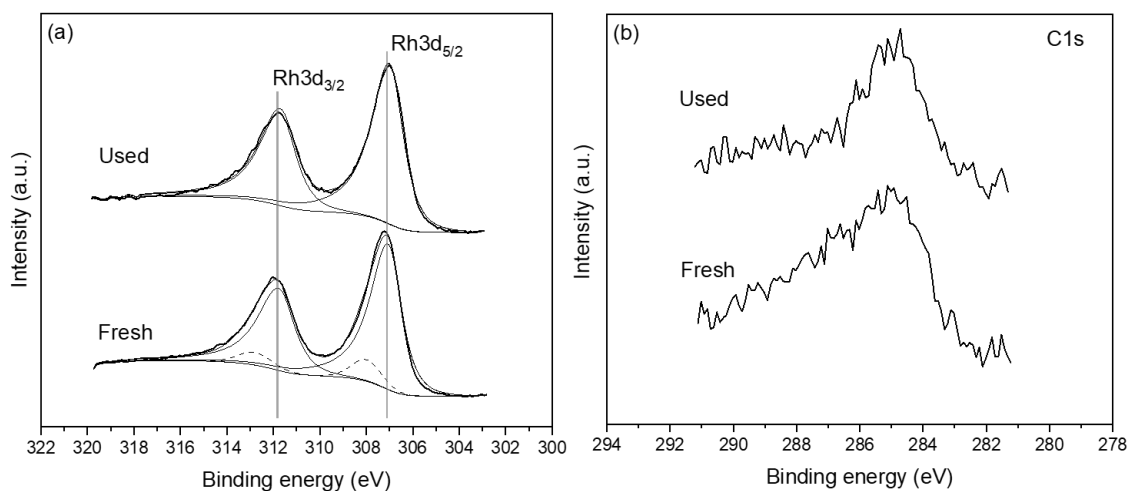
**Figure 11.** SEM micrographs of Rh/YSZ from top view (a) fresh sample and (b) used sample.



**Figure 12.** SEM micrographs of Rh/YSZ from cross section (a) fresh sample and (b) used sample.

Figure 13a shows the Rh 3d spectra of the freshly reduced and post-reaction (used) sample. The Rh 3d<sub>5/2</sub> peak of the fresh sample is centred at approximately 307.2 eV, which indicates that the Rh catalyst film is mostly in the metallic state, without excluding the possibility of some minor Rh oxide quantities being also present [66]. The post-reaction data suggest that the surface chemical state of the Rh electrocatalyst film has not changed significantly. A rather small shift of ~0.2 eV towards lower binding energy is observed

suggesting that a minor oxide component may be present in the fresh sample which has been reduced after reaction leading to the apparent shift. To clarify this point, the raw Rh3d spectra were deconvoluted using an asymmetric peak shape for the metallic state and Gaussian–Lorentzian peak shape for the oxidized state. Figure 13a shows that the metallic Rh3d<sub>5/2</sub> component (solid line) is centred at ~307 eV while the oxidized Rh3d<sub>5/2</sub> component (dashed line) is centred at ~308 eV. The ratio of metallic Rh to oxidized Rh is 1:9, confirming that Rh film is nearly metallic both before and after reaction. It is worth noting here that the post-reaction spectra have been acquired after testing the catalyst under reaction conditions of CO<sub>2</sub> to H<sub>2</sub> of 1:4. The XPS results are in close agreement with the XRD data presented above (Figure 10), with the two techniques suggesting the absence of any substantial quantity of Rh oxide on the surface or bulk of the Rh film. Minor quantities of carbon were present on both the fresh and used samples (Figure 13b). More crucially, the amount of carbon was not found to increase in the post-reaction sample, which indicates that there is no carbon deposition on the catalyst surface during the reaction, especially under feed conditions of P<sub>CO2</sub>:P<sub>H2</sub> ratios of 4:1.



**Figure 13.** XPS measurements of the freshly reduced and post-reaction used catalyst sample. (a) Rh 3d and (b) C 1s regions.

### 3. Experimental

#### 3.1. Catalyst Preparation

A disc of 8% mol Y<sub>2</sub>O<sub>3</sub>-stabilized ZrO<sub>2</sub> (YSZ), with 17 mm diameter and 1.5 mm thickness, respectively, was utilized as solid electrolyte. Gold (Au) reference and counter electrodes were deposited on one side of the electrolyte, using Au paste (Metalor, AU 201 Gold Resinate, Birmingham, UK) and calcination at 450 °C for 30 min following a sintering at 700 °C for 1 h, with a heating rate of 10 °C min<sup>−1</sup>.

The working electrode (Rh catalyst electrode) was deposited on the opposite side of the YSZ solid electrolyte by application of thin coatings of Rh paste (Engelhard Rhodium Resinate 8826, Cinderford, UK). Calcination was carried out in air at 550 °C for 3 h with a heating rate of 10 °C min<sup>−1</sup>. Prior electrochemical experiments, the Rh catalyst electrode was reduced at 440 °C for 2 h under a flow of 15% H<sub>2</sub> in He. The total mass of the Rh catalyst electrode was 1.8 mg.

#### 3.2. Reactor Operation

The electrocatalytic experiments were carried out in a continuous single pellet flow reactor, which has been discussed previously [38–40]. The feed gas composition and total flow rates were controlled by a set of electronic flow meters (Brooks Instrument, Hatfield, PA, USA). Reactants were certified standards of 5% CO<sub>2</sub> in He and 15% H<sub>2</sub> in He. Pure He (99.999%) was fed to further adjust the total flow rate and the inlet gas composition at the

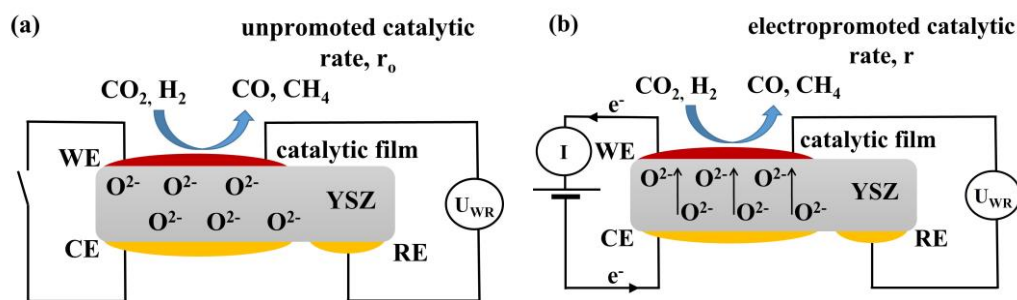
desired values. Electrochemical experiments were performed at ambient pressure. Feed reactant partial pressure was varied between 1 to 4 kPa CO<sub>2</sub> and 1 to 7 kPa H<sub>2</sub>.

The concentrations of reactants and products were analyzed with an IR CO<sub>2</sub>-CO-CH<sub>4</sub> gas analyzer (Futzi Electric ZRE, Shinagawa City, Tokyo, Japan). Constant currents and potentials were applied using an AMEL 2053 galvanostat-potentiostat. CO<sub>2</sub>, CO, and CH<sub>4</sub> were further analyzed by gas chromatography (Gas Chromatographer, Shimadzu 2014, Kyoto, Japan) with TCD and FID detectors, using a Porapak QS packed column.

Blank experiments have been carried out to confirm the non-catalytic behavior of the Au counter and reference electrodes under open- and closed-circuit conditions. For this purpose, an electrochemical cell of the type Au/YSZ/Au (replacing the Rh working electrode with Au) was investigated under reaction conditions of this study ( $T = 400\text{ }^{\circ}\text{C}$ ,  $F_T = 100\text{ cm}^3\text{ min}^{-1}$  and different H<sub>2</sub> to CO<sub>2</sub> gas feeding ratios). The obtained CO formation rate on Au was small with values of  $r_{\text{CO}} < 10^{-9}\text{ mols}^{-1}$  and it was not affected by potential application. CH<sub>4</sub> formation on Au was not observed.

### 3.3. Electrochemical Promotion Parameters Computation

Figure 14 shows a schematic representation of the (Rh | YSZ | Au) electrochemical cell under (a) open circuit and (b) closed circuit conditions. WE correspond to the working electrode (Rh deposited catalytic active film), CE to the counter, and RE to the reference electrodes both made out of Au in order to be catalytically inactive. All 3 electrodes are deposited on yttria-stabilized zirconia (YSZ) which serves as a solid O<sup>2-</sup> ion conductor at operating temperatures of 380 to 430 °C. Under open circuit conditions (i.e., no current passing through the cell), H<sub>2</sub> and CO<sub>2</sub> are co-fed over the conductive catalyst film leading to the formation of CO and CH<sub>4</sub>, expressed by the unpromoted catalytic rate,  $r_0$ . Under, for example, anodic polarization, the application of a positive potential between the counter and working electrode, O<sup>2-</sup> ions from the solid electrolyte are migrating to the catalyst-film forming at the metal gas interface an effective double layer, that alters the catalytic activity, and leading to the electropromoted rate,  $r$ .



**Figure 14.** Schematic presentation of the electrochemical cell under (a) open and (b) closed circuit conditions, WE corresponds to the working electrode, CE to counter, and RE to reference electrode.

The non-Faradaic behavior is defined by two basic parameters, the rate enhancement ratio,  $\rho$ ,

$$\rho = \frac{r}{r_0} \quad (5)$$

where  $r$  is the electropromoted catalytic rate under polarization and  $r_0$  is the unpromoted rate (i.e., the open-circuit catalytic rate). The apparent Faradaic efficiency,  $\Lambda$ , defined from:

$$\Lambda = \frac{\Delta r}{I/nF} \quad (6)$$

where  $\Delta r$  is the current- or potential-induced observed change in catalytic rate ( $\Delta r = r - r_0$ ),  $I$  is the applied current,  $n$  is the number of exchanged electrons, and  $F$  is Faraday's constant.

In this study, where CH<sub>4</sub> and CO were the only products of the CO<sub>2</sub> hydrogenation reaction, the Faradaic efficiency for each formation reaction can be defined from the follow equations:

$$\Lambda_{\text{CO}} = \frac{2\Delta r_{\text{CO}} \left( \text{in } \frac{\text{mol}}{\text{s}} \right)}{I/F} \quad (7)$$

$$\Lambda_{\text{CH}_4} = \frac{8\Delta r_{\text{CH}_4} \left( \text{in } \frac{\text{mol}}{\text{s}} \right)}{I/F} \quad (8)$$

### 3.4. Catalyst Characterization

Wide-angle X-ray diffraction (XRD) patterns were recorded using a Bruker D8 Advance system equipped with Cu-K $\alpha$  radiation ( $\lambda = 1.5418 \text{ \AA}$ ). The voltage and lamp current were adjusted to 40 kV and 40 mA, respectively. The angle range  $2\theta$  was  $20\text{--}90^\circ$  and scan speed was 0.3 s/step (Siemens D-500, Frankfurt, Germany).

High resolution field-emission scanning electron microscopy (FE-SEM) was employed using a Zeiss SUPRA 35VP system operating at 10–15 kV voltage range (Carl Zeiss AG, Jena, Germany).

Ex situ X-ray photoelectron spectroscopy (XPS) measurements of the fresh Rh catalyst sample (after H<sub>2</sub> reduction) and post-experiment sample were carried out in an ultrahigh-vacuum (UHV) system described in detail elsewhere [68]. Measurements were carried out using non-monochromatic AlK $\alpha$  radiation (1486.6 eV) and a Leybold LH EA11 energy analyzer (Leybold, Germany), which was operated at a constant pass energy (100 eV). The analyzed sample area was a  $2 \times 5 \text{ mm}^2$  rectangle. All spectra were corrected for charge transfer using the C1s peak at 284.8 eV for adventitious carbon

## 4. Conclusions

In this work, the electrochemical promotion of CO<sub>2</sub> hydrogenation was studied over a Rh/YSZ electrode in a continuous single pellet flow reactor for P<sub>CO<sub>2</sub></sub>/P<sub>H<sub>2</sub></sub> gas feed mixtures ranging from 1:2 to 4:1. Despite the large body of literature on the use of Rh/YSZ electrodes for other reactions such as NO reduction and ethylene oxidation under various experimental set-ups, CO<sub>2</sub> hydrogenation has been rarely investigated on Rh/YSZ using laboratory reactors. There are only a couple of references discussing data under reaction conditions of a narrow CO<sub>2</sub> to H<sub>2</sub> ratio of 1–1.5 or 1:1.8 and cathodic polarizations. The results of the present study show that potential or current application can strongly affect the CO<sub>2</sub> hydrogenation reaction, both in regard to the catalytic rates obtained but also selectivity to reactions products. In the temperature range of 350 to 430 °C, under atmospheric total pressure and with a total flowrate of  $F_T = 50 \text{ cm}^3 \text{ min}^{-1}$ , the only products found were CH<sub>4</sub> and CO. Increasing or decreasing the catalyst potential by up to 1.5 V leads to an inverted volcano type behavior of the methanation rate (the formation rate increases with anodic and cathodic polarization), while the rate of CO production follows a volcano type behavior (the formation rate decreases with anodic and cathodic polarization). The observed trends are confirmed by kinetic measurements and agree with the rules governing the EPOC phenomenon as described in bibliography.

The observed rate changes were non-faradaic and after current interruption, the catalytic rate of CH<sub>4</sub> formation returned to its initial open circuit value, demonstrating the reversibility of the phenomenon. However, the CO formation rate, exhibited a partial non-reversible behavior, which is more pronounced under a gas feed composition of CO<sub>2</sub> to H<sub>2</sub> ratio of 4:1, i.e., in excess of CO<sub>2</sub>. Permanent EPOC behavior was discussed in view of the stabilization of the Rh metallic phase under anodic polarization. Our preliminary XPS studies show that for pre- and post-reaction samples the Rh metal phase is mainly present, even after exposing the Rh film to higher CO<sub>2</sub> to H<sub>2</sub> ratios. This confirms that, at first glance, the partially permanent EPOC behavior in our case is due to the electrochemically induced stabilization of the Rh metallic phase.

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## Article

# Nd<sub>2–x</sub>Sr<sub>x</sub>NiO<sub>4</sub> Solid Solutions: Synthesis, Structure and Enhanced Catalytic Properties of Their Reduction Products in the Dry Reforming of Methane

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**Abstract:** Solid solutions Nd<sub>2–x</sub>Sr<sub>x</sub>NiO<sub>4±δ</sub> (x = 0, 0.5, 1, 1.2, 1.4) with a K<sub>2</sub>NiF<sub>4</sub> structure can be obtained from freeze-dried precursors. The end members of this series can be obtained at T ≥ 1000 °C only, while complex oxides with x = 1; 1.5 are formed at T ≥ 700 °C. Thermal analysis revealed the two stages of Nd<sub>2–x</sub>Sr<sub>x</sub>NiO<sub>4±δ</sub> thermal reduction in a 10%H<sub>2</sub>/Ar gas mixture that was completed at 900 °C. For x < 0.2, the reduction products demonstrated an exsolution-like morphology with Ni nanoparticles allocated at the surface of oxide grains. As-obtained nanocomposites with x = 0 and x > 1 revealed the outstanding catalytic activity and selectivity in the dry reforming of the methane (DRM) reaction at 800 °C with CH<sub>4</sub> conversion close to the thermodynamic values. The appearance of two different maxima of the catalytic properties of Ni/(Nd<sub>2</sub>O<sub>3</sub>,SrCO<sub>3</sub>) nanocomposites could be affiliated with the domination of the positive contributions of Nd<sub>2</sub>O<sub>3</sub> and SrCO<sub>3</sub>, respectively.

**Keywords:** metal–oxide nanocomposites; multicomponent catalysts; complex oxide precursors; K<sub>2</sub>NiF<sub>4</sub> structure; high temperature reduction; exsolution; dry reforming of methane

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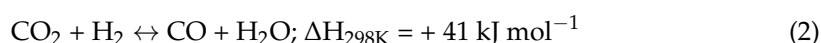
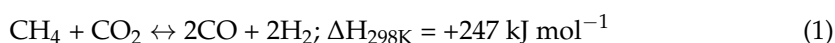


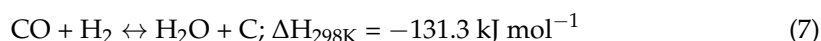
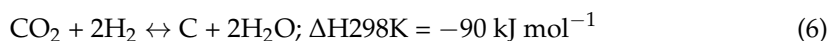
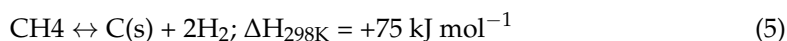
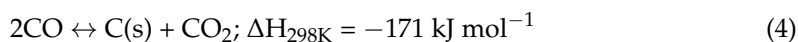
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## 1. Introduction

Through the dry reforming of methane (DRM), the reaction of methane with CO<sub>2</sub> is one of the most prospective methods of methane conversion into synthesis gas and is a useful raw material for the large-scale chemical industry. The advantage of DRM in the steam reforming of methane currently available on large-scale deals with a more balanced composition of Syngas is that it allows its direct processing into petrochemical products. Another advantage of DRM is that it deals with the utilization of significant amounts of CO<sub>2</sub> byproducts which are often formed in other petrochemical and other industrial processes. In addition, more and more attention is being paid to the dry reforming of methane to a synthesis gas as an effective way to utilize these two main greenhouse gases [1–5]. The DRM process is also rather beneficial for utilization and conversion into value-added products with the growing amounts of biogas consisting mostly of CH<sub>4</sub> and CO<sub>2</sub> [6,7].

The main processes that occurred during DRM is shown as follows [1,2,8–10]:





The main reaction (1) of the DRM process was strongly endothermic due to the large amount of energy necessary to break down methane and  $\text{CO}_2$ . According to thermodynamic calculations, the equilibrium was shifted to CO and  $\text{H}_2$  at  $T > 640^\circ\text{C}$ . The amount of these reaction products increased with the temperature and in the lack of catalyst approaches 100% at  $T = 1000\text{--}1100^\circ\text{C}$ . The actual composition of the reaction mixture depended on the reaction rate and the contribution of the side reactions (2)–(5). The amount of hydrogen in the reaction products could be reduced by a reverse water-gas shift reaction (2). The reaction of methane and  $\text{CO}_2$  could also cause the formation of hydrocarbons through a reaction (3) through one of the main obstacles to the large-scale application of DRM were reactions (4) and (5) and, to a lesser extent, (6) and (7), which caused the formation of coke at the surface of the catalysts and resulted in their deterioration [11].

Due to these features, DRM is usually performed as a catalytic process; the possibility of realizing it with a high yield of products at reasonable temperatures depends greatly on the selection of efficient catalysts. This selection deals with features of the DRM reaction mechanism at the atomic level. According to the existing models, the DRM reaction in the catalytic mode could be divided into four elementary steps: (1) the dissociative adsorption of methane at the metal surface and fast desorption of  $\text{H}_2$ ; (2) the dissociative adsorption of  $\text{CO}_2$  at the metal and metal–oxide interface and fast desorption of CO; (3) formation of the surface hydroxyl groups by hydrogen and oxygen spillover at the surface of the catalyst; (4) the oxidation of methyl-like  $\text{CH}_x$  groups by the surface oxygen and hydroxyls, resulting in the formation and desorption of CO and  $\text{H}_2$  [10,12,13].

The highest activity and selectivity in DRM among the base metals was demonstrated by the nickel catalysts, especially at  $T < 900^\circ\text{C}$ . The main problem with their industrial application is related to intense coking which results in the progressive deactivation of the catalyst. However, recent studies of the coking processes demonstrated that their intensity could be significantly reduced by the particle size control and selection of oxide substrates. Taking into account the atomic scale model of the DRM process, the oxide substrate is now considered one of the key elements of metal–oxide composite catalysts, as the sorption and activation of  $\text{CO}_2$  usually occur at the oxide components of catalysts. It was found that the surface acidity/basicity of the oxide components was rather important for this process, which made it preferable to the application of alkaline earth and rare earth oxides, such as the elements of DRM catalysts [8]. Several other, more complex metal–oxide interactions could also be important in DRM catalysis. It was found, for example, that the methane activation barriers were drastically different for Co and Ni surfaces of pure metals and for  $\text{Co/CeO}_{2-x}$  (111) and  $\text{Ni/CeO}_{2-x}$  (111) surfaces [10,14,15]. These features make the processes of metal–oxide interaction in the catalytic systems one of the hottest topics in modern studies of heterogeneous catalysts.

Until now, most of the metal–oxide catalysts have been prepared by the incipient wetness technique when the porous oxide substrate is soaked with a solution containing active metal, followed by drying, thermal decomposition, and the chemical reduction in the metal-containing component. This method ensures the relatively uniform distribution of catalytically active components across the surface of the supporting material. Along

with the preferences for their chemical composition described before, these materials should possess a high surface area, extended porosity, and excellent thermal stability. A significant interaction of the active metal with the oxide surface is considered a positive factor here, as the anchoring of active particles to the surface of the supporting material promotes the prevention of sintering the nanoparticles of active metals in the reaction environment which is the second most important reason for catalyst deactivation. However, this method is really efficient when the composite metal-oxide catalyst consists of a single active component and a single supporting material only [11].

Due to the multistage mechanism of the DRM process, the modern Ni-based DRM catalysts usually consist of several components promoting the most efficient realization of the particular stages of the process [10]. To implement the efficient transport of the adsorbed reaction species between these components, it is necessary to provide a number of tight multiphase contacts of the various catalyst components. One of the best ways to ensure that multiphase contacts are based on a reduction in the complex oxide precursors containing all the necessary cations. The application of single oxide precursors ensures the reproducibility not only of the phase composition but also the morphology of the catalyst [1].

Currently, the most often used precursors are complex oxides with *q* perovskite structure, though, in the case of nickel-based catalysts, the number of suitable perovskites is rather limited. The largest number of studies in this field deal with  $\text{LaNiO}_3$  and its solid solutions. The preliminary chemical reduction in this complex oxide, often called the activation of the catalyst, results in the formation of a  $\text{Ni/La}_2\text{O}_3$  nanocomposite when the nanoparticles of the Ni metal are allocated at the surface of lanthanum oxide. The processing of native  $\text{LaNiO}_3$  at DRM conditions also results in the fast decomposition of  $\text{LaNiO}_3$ , which usually occurs through the formation of the  $\text{La}_2\text{O}_2\text{CO}_3$  intermediate. Despite the same phase composition of reduction products in both cases, different reaction routes cause a different Ni particle size and a different character of its spatial distribution. Taking into account the reversibility of  $\text{La}_2\text{O}_2\text{CO}_3$  decomposition and the closeness of its decomposition temperature and usual processing conditions of the DRM process ( $T = 700\text{--}800\text{ }^\circ\text{C}$ ;  $\text{CO}_2$ -containing atmosphere), the actual composition of the nanocomposite catalyst, in this case, is rather  $\text{Ni/La}_2\text{O}_2\text{CO}_3$  than  $\text{Ni/La}_2\text{O}_3$ . The temperature of the reductive decomposition of  $\text{LaNiO}_3$  and, hence, the morphology of its decomposition products could be substantially modified by the cationic substitution both to La- and to Ni-sublattices of the perovskite structure by Ca, Sr, Ce, and by Fe, Mn, respectively. The easy resynthesis of  $\text{LaNiO}_3$  from the spent catalyst at moderate temperatures in the air promotes its oxidative regeneration, followed by its further reduction to  $\text{Ni}/(\text{La}_2\text{O}_3, \text{La}_2\text{O}_2\text{CO}_3)$  nanocomposites [16,17].

The number of the available Ni-containing complex oxides with the  $\text{K}_2\text{NiF}_4$  structure is much larger, which opens a broader selection of the possible metal-oxide compositions that can be obtained by their thermal reduction [18]. Our previous studies demonstrated the efficiency of the metal-oxide nanocomposites obtained by the thermal reduction of  $(\text{Ln,Ca})_2(\text{Ni,Co})\text{O}_4$  as catalysts for the partial oxidation and dry reforming of methane [19–21]. The essential morphological feature of as-obtained composites is the formation of the Ni metal nanoparticles at the surface of larger agglomerates of the oxide-based reduction products. This type of composite is usually observed before in the course of several processes of a partial reduction in complex oxides (redox exsolution) and is characterized by the enhanced strength of the metal particle connection with a surface of oxide particle [22–24]. The DRM catalysts based on these composites and obtained by both a partial or complete reduction in oxides were found prone not only to the sintering of active metal particles in the course of the DRM process but also to intense coking at their surface: one of the main reasons for the deactivation of DRM catalysts [25,26].

The best catalysts of the DRM at  $T < 800\text{ }^\circ\text{C}$  among these products were the  $\text{Ni}/(\text{Nd}_2\text{O}_3, \text{CaO})$  nanocomposites obtained by the thermal reduction of  $(\text{Nd,Ca})_2\text{NiO}_4$  [20]. To find the most efficient one among them, it was necessary to vary their composition and compare their properties. However, the homogeneity range of these solid solutions was found to

be rather limited ( $0 < x < 0.5$ ), which, in turn, limited the variation range of these metal–oxide composites by the Nd/Ca ratio. It is known that the variation range was wider for  $\text{Nd}_{2-x}\text{Sr}_x\text{NiO}_4$  solid solutions [27], and their reduction products were also expected to be good DRM catalysts. Similarly to  $\text{LaNiO}_3$ -derived catalysts, SrO in the  $\text{Ni}/(\text{Nd}_2\text{O}_3, \text{SrO})$  composite could transform into  $\text{SrCO}_3$  in the DRM environment. Apart from  $\text{La}_2\text{O}_2\text{CO}_3$ , the information on the  $\text{SrCO}_3$  effect on the properties of DRM catalysts was rather limited. However, the high thermal stability of  $\text{SrCO}_3$ , especially in a  $\text{CO}_2$ -containing DRM environment, could promote the morphological stabilization of the composite  $\text{Ni}/(\text{Nd}_2\text{O}_3, \text{SrCO}_3)$  catalyst at elevated temperatures.

Due to these reasons, the present study was aimed at the synthesis of  $\text{Nd}_{2-x}\text{Sr}_x\text{NiO}_4$  complex oxides, the refinement of the homogeneity ranges of these solid solutions with  $\text{K}_2\text{NiF}_4$  structure in the air, the study of their thermal reduction processes, an analysis of the composition and morphology of their reduction products and evaluation of their catalytic properties in the DRM reaction.

## 2. Results and Discussion

In order to investigate the thermal decomposition features of the freeze-dried precursors, TG measurements with a simultaneous DSC signal detection were carried out for two samples of significantly different compositions. It was observed that both  $\text{Nd}_2\text{NiO}_4$  and  $\text{Nd}_{0.6}\text{Sr}_{1.4}\text{NiO}_4$  precursors exhibited rather similar behavior in the course of their TG-DSC examination (Figures S1 and S2). Their TG profiles contained three distinct temperature ranges that likely corresponded to the different chemical reactions that occurred in precursors. The first step at  $\sim 150\text{--}250^\circ\text{C}$  could be attributed to the elimination of chemically bound water presented as  $-\text{OH}$  species or  $\text{H}_2\text{O}$  molecules incorporated into the structure of inorganic hydrates. The second step at  $250\text{--}400^\circ\text{C}$  corresponded to the decomposition of Nd, Sr, and Ni nitrates, and the last step was likely to be the complete combustion of PVA fragments by atmospheric  $\text{O}_2$  or/and active oxygen species released during the decomposition of nitrates at temperatures near the combustion reaction. The combustion nature of this process was confirmed by a strong exothermic effect at  $400\text{--}450^\circ\text{C}$ , which was detected by the DSC method. No effects at temperatures above  $500^\circ\text{C}$  were observed in the TG-DSC profiles except a slight mass loss at  $850\text{--}900^\circ\text{C}$  for the  $\text{Nd}_{0.6}\text{Sr}_{1.4}\text{NiO}_4$  precursor. This could have been elucidated by the decomposition of the minor amount of  $\text{SrCO}_3$  formed by the partial interaction of SrO with  $\text{CO}_2$  gas released in the course of PVA combustion. Thus, the intensive formation of the target  $\text{K}_2\text{NiF}_4$  complex oxides under isothermal temperature conditions was expected at  $T > 500\text{--}600^\circ\text{C}$  after the completion of all decomposition/combustion processes in freeze-dried precursors.

To study the complex oxide formation, the thermal decomposition of the freeze-dried precursors was performed in the air at  $T = 600\text{--}1200^\circ\text{C}$  for 6 h. A careful comparison of the XRD patterns of the decomposition products revealed the considerable dependence of the phase formation conditions on the  $\text{Nd}_{2-x}\text{Sr}_x\text{NiO}_4$  composition (Figure 1 and Figures S3–S7).

In the case of  $\text{Nd}_2\text{NiO}_4$ , the samples obtained at  $600\text{--}700^\circ\text{C}$  consisted of a mixture of cubic  $\text{Nd}_2\text{O}_3$  and  $\text{NdNiO}_3$  with an orthorhombic perovskite structure. These observations were in good accordance with the fact that neodymium-nickel perovskite can be obtained at lower temperatures under an air atmosphere [28]. Further heating provided a solid-state interaction between  $\text{Nd}_2\text{O}_3$  and  $\text{NdNiO}_3$ , forming the target  $\text{Nd}_2\text{NiO}_4$  compound at  $T > 900^\circ\text{C}$ .

In the case of  $\text{Nd}_{1.5}\text{Sr}_{0.5}\text{NiO}_4$  and  $\text{NdSrNiO}_4$  compositions, the thermal decomposition of the freeze-dried precursors led to the intense dominant formation of the target  $\text{K}_2\text{NiF}_4$  phases even at  $600\text{--}700^\circ\text{C}$ ; only trace amounts of the  $\text{SrCO}_3$  carbonate was observed by XRD. All the samples obtained at  $T \geq 800^\circ\text{C}$  were single-phase complex nickelates. Such low temperatures demanded  $\text{Nd}_{1.5}\text{Sr}_{0.5}\text{NiO}_4$  and  $\text{NdSrNiO}_4$  formation to be explained by the drastic stabilization of the  $\text{K}_2\text{NiF}_4$  structure due to the substitution of  $\text{Nd}^{3+}$  with a larger  $\text{Sr}^{2+}$  cation.

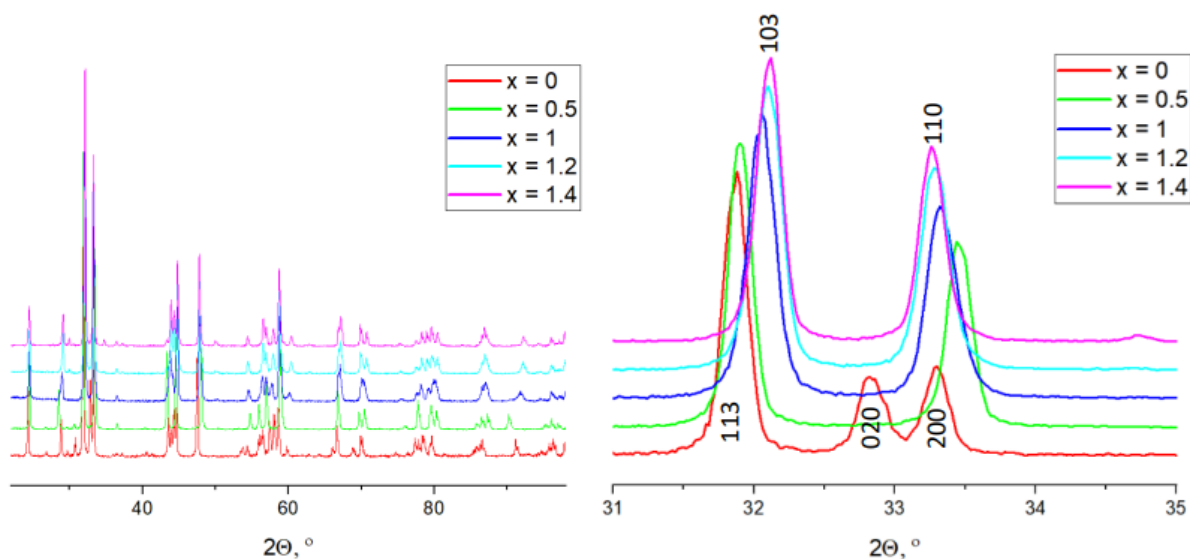
	$\text{Nd}_2\text{NiO}_4$	$\text{Nd}_{1.5}\text{Sr}_{0.5}\text{NiO}_4$	$\text{NdSrNiO}_4$	$\text{Nd}_{0.8}\text{Sr}_{1.2}\text{NiO}_4$	$\text{Nd}_{0.6}\text{Sr}_{1.4}\text{NiO}_4$
1100 °C	$\text{Nd}_2\text{NiO}_4$	$\text{Nd}_{1.5}\text{Sr}_{0.5}\text{NiO}_4$	$\text{NdSrNiO}_4$	$\text{Nd}_{0.8}\text{Sr}_{1.2}\text{NiO}_4$	$\text{Nd}_{0.6}\text{Sr}_{1.4}\text{NiO}_4$
1000 °C	$\text{Nd}_2\text{NiO}_4$	$\text{Nd}_{1.5}\text{Sr}_{0.5}\text{NiO}_4$	$\text{NdSrNiO}_4$	$\text{Nd}_{0.8}\text{Sr}_{1.2}\text{NiO}_4$	$\text{Nd}_{0.6}\text{Sr}_{1.4}\text{NiO}_4$
900 °C	$\text{Nd}_2\text{NiO}_4$	$\text{Nd}_{1.5}\text{Sr}_{0.5}\text{NiO}_4$	$\text{NdSrNiO}_4$	$\text{Nd}_{0.8}\text{Sr}_{1.2}\text{NiO}_4$	RP P
800 °C	RP c- $\text{Nd}_2\text{O}_3$ P	$\text{Nd}_{1.5}\text{Sr}_{0.5}\text{NiO}_4$	$\text{NdSrNiO}_4$	RP $\text{SrCO}_3$	RP P
700 °C	P c- $\text{Nd}_2\text{O}_3$	$\text{Nd}_{1.5}\text{Sr}_{0.5}\text{NiO}_4$	RP $\text{SrCO}_3$	RP $\text{SrCO}_3$	RP $\text{SrCO}_3$
600 °C	P c- $\text{Nd}_2\text{O}_3$	RP $\text{SrCO}_3$	RP $\text{SrCO}_3$	RP $\text{SrCO}_3$	RP $\text{SrCO}_3$

**Figure 1.** The phase composition of  $\text{Nd}_{2-x}\text{Sr}_x\text{NiO}_4$  samples obtained at various temperatures; RP—oxide with  $\text{K}_2\text{NiF}_4$  structure, P—oxide with perovskite structure.

According to the XRD data, the thermolysis products at 600–700 °C contained phases with a  $\text{K}_2\text{NiF}_4$  structure mixed with considerable amounts of strontium carbonate. Apparently, these  $\text{K}_2\text{NiF}_4$  products were stable complex nickelates with a moderate Sr content; the excess of the last one was presented as a  $\text{SrCO}_3$  phase. Interestingly, further heating to 800–900 °C led to the formation of mixtures of  $\text{K}_2\text{NiF}_4$  and orthorhombic perovskite phases. A similar feature was observed for Nd-Ca cobaltite in [29], where the formation of the target  $\text{K}_2\text{NiF}_4$  complex oxide at moderate temperatures was accompanied by the kinetically controlled formation of an intermediate phase with a perovskite structure. For Nd-Sr nickelates, the observed features could be explained by the formation of Sr-rich (Nd,Sr) $\text{NiO}_3$  perovskites with a Ni oxidation state close to +3 followed by their solid state interaction with the “low temperature” Nd-rich (Nd,Sr) $_2\text{NiO}_4$  phases at 900–1000 °C, resulting in the target  $\text{Nd}_{0.8}\text{Sr}_{0.2}\text{NiO}_4$  and  $\text{Nd}_{0.6}\text{Sr}_{1.4}\text{NiO}_4$  nickelates.

Thus, despite such diverse solid-state reaction pathways, all the discussed nickelates could be securely synthesized by the freeze-drying method at  $T = 1000\text{--}1200$  °C in the air. In order to ensure a high level of crystallographic ordering in such multicomponent solid solutions and to make a reliable comparison between the samples with various Sr content, a series of  $\text{Nd}_{2-x}\text{Sr}_x\text{NiO}_4$  samples ( $x = 0; 0.5; 1; 1.2; 1.4$ ) obtained at 1200 °C was chosen for further investigation. According to the XRD study, their crystal structure was reliably assigned to the perovskite-related  $\text{K}_2\text{NiF}_4$  type. Similarly to [20], the orthorhombically distorted Fmmm structure was observed for  $\text{Nd}_2\text{NiO}_4$  ( $x = 0$ ); no additional reflections of the other  $\text{K}_2\text{NiF}_4$  polymorphs were observed. On the other hand, for the Sr-containing solid solutions ( $0.5 \leq x \leq 1.4$ ), a tetragonal I4/mmm structure was verified (Figure 2). It clearly indicated the stabilization effect. A profile analysis of these complex oxides was performed by the Le Bail method from powder XRD data; the resulting unit cell parameters are given in Table 1.

The variation in the  $\text{K}_2\text{NiF}_4$  lattice parameters values on the Sr content was found similar to that found in [27]. It is noteworthy that the observed changes could be attributed to both Nd/Sr and O stoichiometry which provided a notable deviation from the linear Vegard’s rule (Figure S8). The absence of these changes for the sample with  $x > 1.4$  corresponded quite well with the previous conclusion on the allocation of the limit of the  $\text{Nd}_{2-x}\text{Sr}_x\text{NiO}_{4+\delta}$  homogeneity range at  $1.4 < x < 1.6$ .



**Figure 2.** XRD patterns of  $\text{Nd}_{2-x}\text{Sr}_x\text{NiO}_4$  obtained at  $T = 1200^\circ\text{C}$ .

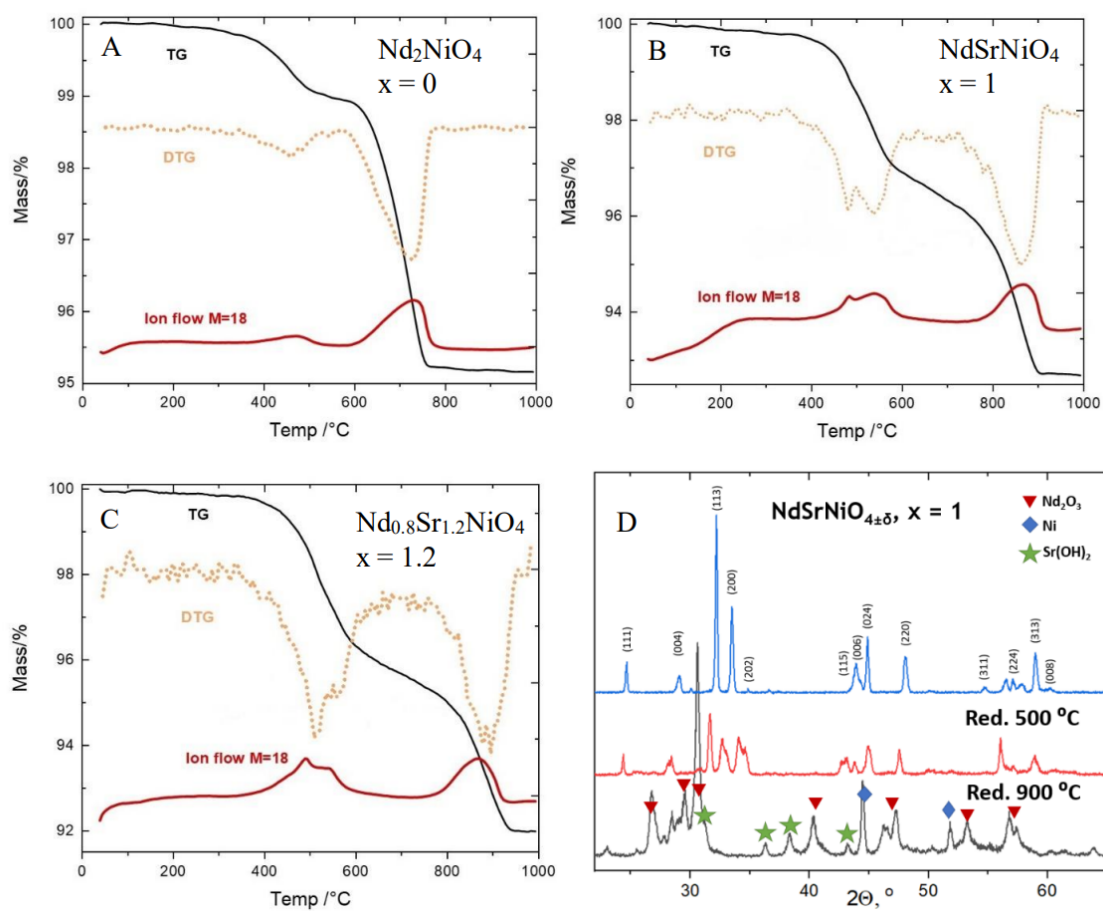
**Table 1.** The unit cell parameters of  $\text{Nd}_{2-x}\text{Sr}_x\text{NiO}_{4\pm\delta}$ .

Composition	Space Group	a, Å	b, Å	c, Å	V, Å <sup>3</sup>
$\text{Nd}_2\text{NiO}_{4\pm\delta}$	Fmmm	5.3789(3)	5.4514(3)	12.3724(8)	362.79(5)
$\text{Nd}_{1.5}\text{Sr}_{0.5}\text{NiO}_{4\pm\delta}$	I4/mmm	3.776(2)	3.776(2)	12.482(1)	177.9(2)
$\text{NdSrNiO}_{4\pm\delta}$	I4/mmm	3.7886(2)	3.7886(2)	12.320(1)	176.8(2)
$\text{Nd}_{0.8}\text{Sr}_{1.2}\text{NiO}_{4\pm\delta}$	I4/mmm	3.798(2)	3.798(2)	12.261(1)	176.8(2)
$\text{Nd}_{0.6}\text{Sr}_{1.4}\text{NiO}_{4\pm\delta}$	I4/mmm	3.804(2)	3.804(2)	12.252(6)	177.3(2)
$\text{Nd}_{0.4}\text{Sr}_{1.6}\text{NiO}_{4\pm\delta}$	I4/mmm	3.8027(3)	3.8027(3)	12.266(11)	177.38(3)

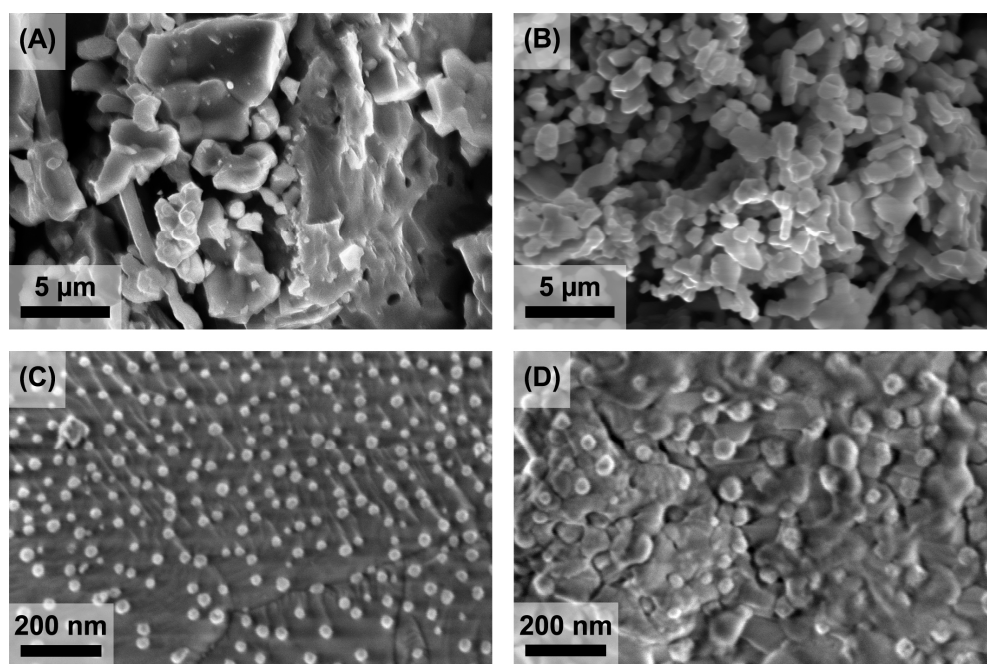
The thermal analysis of the reduction processes of the as-obtained complex oxides in the  $\text{Ar}/\text{H}_2$  mixture revealed two different stages of this process for all samples in the study (Figure 3A–C), as it was observed before for other  $\text{K}_2\text{NiF}_4$  complex oxides [19–21]. According to the XRD analysis results of the reduction products, the partial reduction in the complex oxide precursor at the first stage caused its transformation into another complex oxide with an individual crystal structure. The detection of the  $\text{Ni}^0$  phase possibly formed during its reduction was complicated by the strong overlapping of its reflections with the reflections of complex oxide structures. Complete decomposition of this intermediate at the second stage of the reduction resulted in the formation of  $\text{Ni}^0$ ,  $\text{Nd}_2\text{O}_3$ , and  $\text{SrO}$ , which could be transformed into  $\text{Sr}(\text{OH})_2$  during further cooling in the air (Figure 3D). An increase in the Sr content in the initial complex oxide was accompanied by a systematic increase in the complete reduction temperature.

The microstructure of the complete reduction products of  $\text{Nd}_{2-x}\text{Sr}_x\text{NiO}_{4\pm\delta}$  was similar to the microstructure in the reduction products of their Ca-substituted counterparts, as studied in more detail before. According to [19,20], the coarser grains were likely formed by Nd and Sr oxides that were coated with spherical nanoparticles of the Ni metal. Due to a wider range of Sr substitution in  $\text{Nd}_2\text{NiO}_4$  compared to Ca, it was possible to observe in this case that the increase in Sr content was accompanied by a significant coarsening of the exsolved Ni particles from ~20 nm for  $x = 0$  to 40–60 nm for  $x \geq 1$ , probably due to a higher reduction temperature (Figure 4C,D).





**Figure 3.** TG, DTG, and H<sub>2</sub>O evolution curves for the reduction of Nd<sub>2</sub>NiO<sub>4</sub> (A), NdSrNiO<sub>4</sub> (B), Nd<sub>0.8</sub>Sr<sub>1.2</sub>NiO<sub>4</sub> (C) in Ar/H<sub>2</sub> mixture; XRD patterns of NdSrNiO<sub>4</sub> and its reduction products at 500 °C and 900 °C (D).



**Figure 4.** SEM micrographs of Nd<sub>2</sub>NiO<sub>4</sub> (A), NdSrNiO<sub>4</sub> (B), and the products of their thermal reduction at 900 °C ((C,D), respectively).

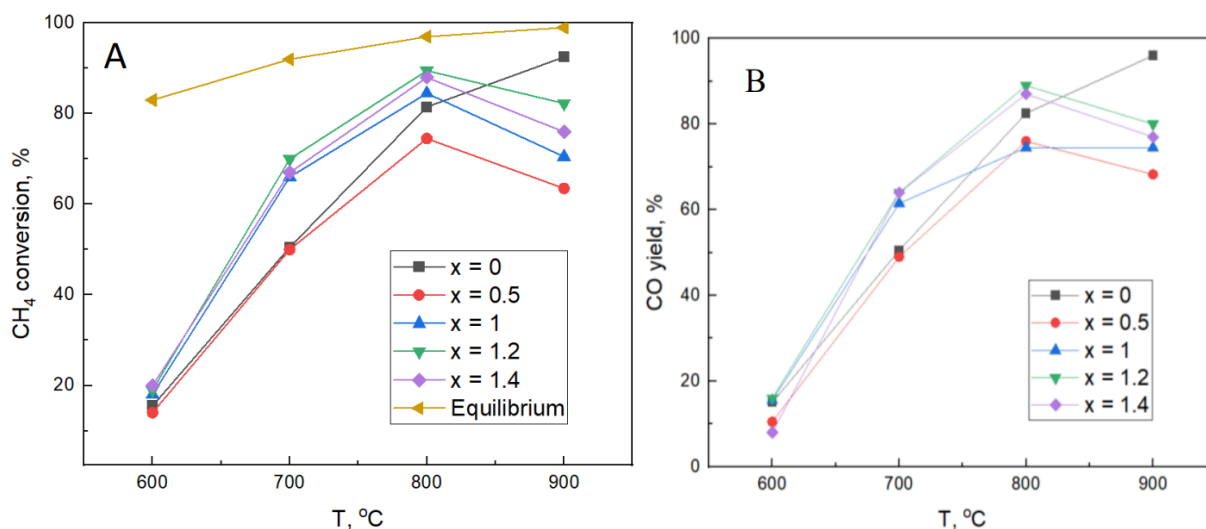
Taking into account the results of our previous studies, it was expected that the reduction products of  $\text{Nd}_{2-x}\text{Sr}_x\text{NiO}_{4\pm\delta}$  with the morphology described before would demonstrate significant catalytic properties in the DRM process. Due to the similarity of the catalytic processes, the DRM catalysts often demonstrated significant catalytic activity and selectivity in the partial oxidation of the methane (POM) reaction: another widely discussed alternative to the currently applied steam reforming process [2,19–21]. However, the production of syngas by DRM at  $T = 700\text{--}800\text{ }^\circ\text{C}$  over the Ni-based catalysts could be more efficient than POM. According to [20], a lower CO yielded in POM at  $T < 800\text{ }^\circ\text{C}$  over Ni/( $\text{Nd}_2\text{O}_3$ , CaO) nanocomposites dealt with Ni oxidation to NiO, the catalyst of the total oxidation of methane and CO to  $\text{CO}_2$ . The oxidation of the part of methane to  $\text{CO}_2$  led to a notable decrease in syngas selectivity. Similar processes were expected to be obtained in  $\text{Nd}_{2-x}\text{Sr}_x\text{NiO}_{4\pm\delta}$ -derived nanocomposites in the POM environment, but their appearance during DRM was less probable due to the lack of oxidants.

An experimental evaluation of their catalytic performance confirmed a considerable catalytic activity and selectivity in DRM for all metal–oxide composites in a study at  $T \geq 700\text{ }^\circ\text{C}$  (Figure 5, Figures S9 and S10). However, the catalytic behavior of these composites demonstrated several important anomalies. Similar metal–oxide composites obtained from  $\text{K}_2\text{NiF}_4$ -like precursors usually demonstrate a monotonous dependence of their catalytic properties in DRM both on the temperature and on the rare earth to alkaline earth ratio in the composite [19,20]. In the present case, the samples in the study could be divided into two different groups according to the behavior of their catalytic properties—Sr-free and Sr-containing composites. The catalytic activity and selectivity of the only member of the first group, the  $\text{Nd}_2\text{NiO}_4$  reduction product ( $x = 0$ ), similarly to [19,20], increased monotonously with the temperature demonstrating maximum values at the maximum temperature of the study ( $T = 900\text{ }^\circ\text{C}$ ) and approaching their thermodynamic limits (Figure 5A and Figure S9B). Meanwhile, the maximum values of activity and selectivity in all the Sr-containing composites ( $0.5 \leq x \leq 1.4$ ) were observed at  $T = 800\text{ }^\circ\text{C}$  while further heating to  $T = 900\text{ }^\circ\text{C}$ , contrary to the thermodynamically predicted behavior, caused a considerable decrease in their catalytic performance. Another unusual feature in this series of composites dealt with a significant drop in catalytic activity at  $0 < x \leq 0.5$ . However, the further substitution of Nd with Sr resulted in the systematic recovery of the catalytic activity and selectivity of composites with their maximal values at  $T = 800\text{ }^\circ\text{C}$  for the samples with  $x = 1.2\text{--}1.4$ .

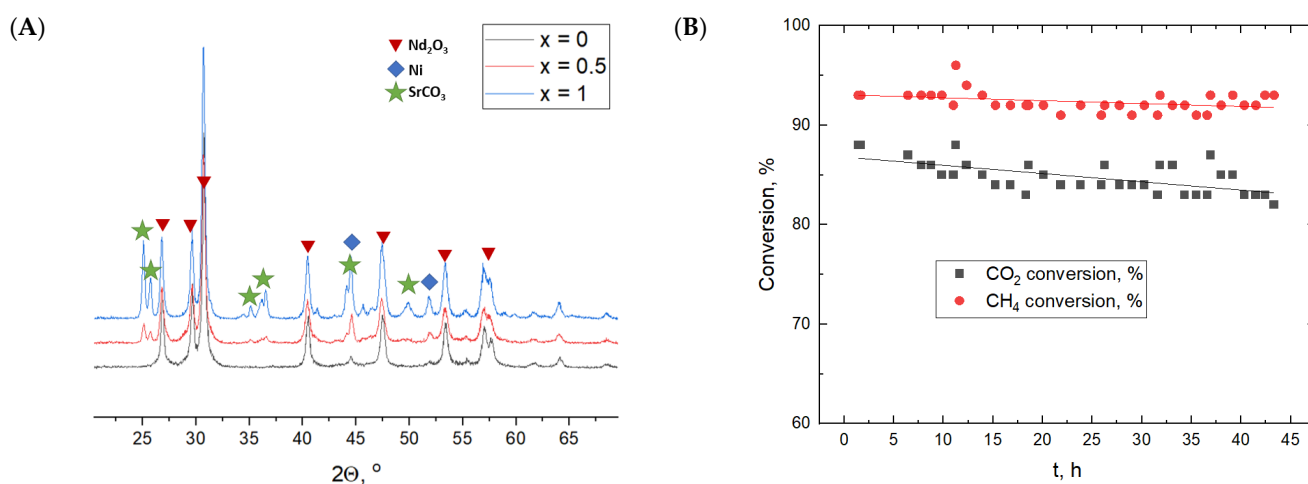
The XRD analysis of spent catalysts revealed that they consisted of Ni and  $\text{Nd}_2\text{O}_3$  for  $x = 0$  and Ni,  $\text{Nd}_2\text{O}_3$ , and  $\text{SrCO}_3$  in all other cases (Figure 6A), as SrO converted easily into  $\text{SrCO}_3$  in the DRM reaction environment [30]. Hence, the most probable reasons for the different behaviors of these two types of DRM catalysts were likely affiliated with the appearance of  $\text{SrCO}_3$  in the composite catalysts and with specific properties of strontium carbonate. According to the existing models of DRM catalysis, the catalytic properties of the  $\text{Nd}_2\text{NiO}_4$  reduction products were determined by the combination of the methane sorption and catalytic activity of nickel metal and the  $\text{CO}_2$  sorption activity of the neodymium oxide. As the amount of Ni metal was almost the same in all samples in the study, the higher catalytic activity of the composites with a larger Sr content could be affiliated with more intense  $\text{CO}_2$  sorption due to a higher basicity catalyst surface. However, a decrease in the sorption activity at higher temperatures was likely more pronounced for  $\text{SrCO}_3$  than for  $\text{Nd}_2\text{O}_3$ , thus promoting a definite decrease in the other catalytic properties of Sr-containing composites at  $T > 800\text{ }^\circ\text{C}$ .

The reasons for the observed drop in the catalytic properties at  $0 < x \leq 0.5$  and, in general, the non-monotonous dependence of the catalytic properties of Ni/( $\text{Nd}_{2-x}\text{Sr}_x$ )Oy composites on  $x$  were likely due to a competition between the two catalytic pathways, via  $\text{Nd}_2\text{O}_3$  and via  $\text{SrCO}_3$ . It should also be noted that the catalytic activity of samples ( $x = 1.2\text{--}1.4$ ) with a larger size of Ni particles was the same or even higher than the corresponding activity of the Sr-free ( $x = 0$ ) sample with much smaller Ni exclusions (Figure 4C,D). It appeared contradictory to the common trend of the better catalytic perfor-

mance of the smaller particles of a catalyst. This discrepancy could also be affiliated with different mechanisms of the DRM catalysis on  $\text{Nd}_2\text{O}_3$  and  $\text{SrCO}_3$  substrates when more efficient  $\text{CO}_2$  activation with  $\text{SrCO}_3$  became more important than the smaller activity of coarser Ni particles on the  $\text{SrCO}_3$  substrate.



**Figure 5.** CH<sub>4</sub> conversion (A) and CO yield (B) over the reduction products of various composites. The calculated values of CH<sub>4</sub> conversion are given according to [13,31–33].



**Figure 6.** XRD patterns of spent catalysts (A) and the results of the stability test of the metal-oxide nanocomposite with  $x = 1.4$  at  $T = 800$  °C (B).

These interesting and unusual features demanded more detailed studies using modern instrumental methods. It should be noted, however, that the values of the activity and selectivity of as-obtained DRM catalysts were comparable with the results obtained by other groups [3,4,10,30,31]. An essential feature of the  $\text{Nd}_{2-x}\text{Sr}_x\text{NiO}_{4\pm\delta}$  reduction products was good reproducibility (Figure S10) and the enhanced stability of their catalytic properties in the DRM environment. This was illustrated by the results of the 45h stability test, which revealed only the minimum variation in the catalytic properties (Figure 6B). This stability could be affiliated with an absence of significant coking at the surface for the catalyst as one of the main reasons of catalyst deactivation during the DRM process (Figure S11).

### 3. Materials and Methods

$\text{Nd}_{2-x}\text{Sr}_x\text{NiO}_4$  ( $x = 0 \div 1.4$ ) samples were obtained by the modified freeze-drying synthesis technique. To obtain multicomponent starting solutions, preliminarily calcined  $\text{Nd}_2\text{O}_3$  and  $\text{SrCO}_3$  were dissolved in the warm diluted acetic acid, then a  $\text{Ni}(\text{NO}_3)_2 \cdot 6\text{H}_2\text{O}$  aqueous solution was added. To stabilize the frozen solution during freeze drying, an aqueous solution (5 wt. %) of polyvinyl alcohol was added to all solutions under intense stirring. The freeze-drying of flash-frozen solutions was performed at  $P = 0.7$  mbar for 2 days. The thermal decomposition of the freeze-dried precursors was performed in the air at  $800\text{--}1200$  °C for 6 h. A reduction in as-obtained  $\text{Nd}_{2-x}\text{Sr}_x\text{NiO}_4$  powders was performed in an  $\text{H}_2:\text{Ar} = 1:10$  gas mixture at different temperatures for 1 h, followed by slow cooling to room temperature under a reducing atmosphere.

XRD analysis of the powders was performed using a Rigaku D/MAX-2500PC diffractometer (Rigaku, Tokyo, Japan) with  $\text{Cu K}\alpha$  radiation generated on a rotating Cu anode (40 kV, 250 mA). The profile analysis of the powder XRD data was carried out by the Le Bail method using the Jana 2006 program package. The TG-DSC thermal analysis of samples combined with a simultaneous QMS evolved gas analysis was performed in the air or in a 10%  $\text{H}_2/\text{Ar}$  gas mixture by STA 409PC/PG (NETZSCH) at  $T = 40$  °C  $\div$  1000 °C and a 10 K/min heating rate. The morphology of the powders was studied using a Carl Zeiss NVision 40 scanning electron microscope (Carl Zeiss SMT AG, Oberkochen, Germany).

The catalytic tests of the DRM reaction were carried out in a quartz glass flow fixed-bed reactor (18 mm internal diameter, 300 mm length) with a 0.2 g sample of the catalyst (100–250 mesh fraction) at atmospheric pressure in the absence of dilution with inert gas. This catalyst was first heated in a hydrogen flow at 10 K/min to 900 °C. Then, the gas stream was switched to a mixture of  $\text{CH}_4/\text{CO}_2 = 1/1$  at GHSV values of 16 L/g h. No dilution in the feed flow by the inert gas was applied. The catalytic experiments were performed consecutively at 900, 800, 700, and 600 °C by holding at the preselected temperatures for 1–5 h at a steady state. After the analysis, the furnace was switched off, and the catalyst was cooled to room temperature over 3–4 h in pure  $\text{N}_2$ . The details of the testing technique and GC analysis can be found elsewhere [34].

The methane conversion (X), product selectivity (S), and yield (Y) of the products were defined as follows:

$$X(\text{CH}_4, \%) = \frac{\text{moles of CH}_4 \text{ converted}}{\text{moles of CH}_4 \text{ in feed}} \times 100 \quad (8)$$

$$S(\text{CO}, \%) = \frac{\text{moles of CO in products}}{\text{moles of CH}_4 + \text{CO}_2 \text{ converted}} \times 100 \quad (9)$$

$$S(\text{H}_2, \%) = \frac{\text{moles of H}_2 \text{ produced}}{2 \times \text{moles of CH}_4 \text{ converted}} \times 100 \quad (10)$$

$$Y(\text{products}, \%) = \frac{X(\text{CH}_4, \%) \times S(\text{products}, \%)}{100} \quad (11)$$

$$\text{C balance } (\%) = \frac{\text{moles of C in products}}{\text{moles of C in feed}} \times 100 \quad (12)$$

The number of moles in the feed gases and gaseous products of the reactions was calculated based on the measured volumetric velocity of the feed gases and the products formed, as well as chromatography data, which made it possible to fully take into account the stoichiometry of the reaction and the corresponding volume expansion of the reacted gas mixture.

### 4. Conclusions

A full scale of the solid solutions  $\text{Nd}_{2-x}\text{Sr}_x\text{NiO}_{4+\delta}$  ( $0 \leq x \leq 1.4$ ) was obtained during these studies; the boundaries of their homogeneity ranged by the Nd/Sr ratio were refined.

The processes of a high-temperature reduction in these complex oxides were investigated; the composition and the morphology of as-obtained metal-oxide nanocomposites were determined. It was found that several Ni/(Nd<sub>2</sub>O<sub>3</sub>,SrCO<sub>3</sub>) nanocomposites demonstrated outstanding activity and selectivity in the DRM process at T = 800 °C and the significant stability of their catalytic properties on stream. A positive effect of SrCO<sub>3</sub> on the catalytic properties of Ni/(Nd<sub>2</sub>O<sub>3</sub>,SrCO<sub>3</sub>) nanocomposites was detected.

**Supplementary Materials:** The following supporting information can be downloaded at: <https://www.mdpi.com/article/10.3390/catal13060966/s1>. Figure S1: TG (green) and DSC (blue) profiles of freeze-dried Nd<sub>2</sub>NiO<sub>4</sub> precursor, Figure S2: TG (green) and DSC (blue) profiles of freeze-dried Nd<sub>0.6</sub>Sr<sub>1.4</sub>NiO<sub>4</sub> precursor, Figure S3: XRD patterns of thermal decomposition products of Nd<sub>2</sub>NiO<sub>4</sub> (x = 0) precursors at different temperatures, Figure S4: XRD patterns of thermal decomposition products of Nd<sub>1.5</sub>Sr<sub>0.5</sub>NiO<sub>4</sub> (x = 0.5) precursors at different temperatures, Figure S5: XRD patterns of thermal decomposition products of NdSrNiO<sub>4</sub> (x = 1) precursors at different temperatures, Figure S6: XRD patterns of thermal decomposition products of Nd<sub>0.8</sub>Sr<sub>1.2</sub>NiO<sub>4</sub> (x = 1.2) precursors at different temperatures, Figure S7: XRD patterns of thermal decomposition products of Nd<sub>0.6</sub>Sr<sub>1.4</sub>NiO<sub>4</sub> (x = 1.4) precursors at different temperatures, Figure S8: The dependence of Nd<sub>2-x</sub>Sr<sub>x</sub>NiO<sub>4±δ</sub> lattice parameters on Sr content, Figure S9: CO<sub>2</sub> conversion (A) and H<sub>2</sub> yield (B) over the reduction products of various composites. The calculated values of H<sub>2</sub> yield are given according to [13,31–33], Figure S10: The results of testing the composites with various Sr content in the DRM process, Figure S11: SEM micrographs of the spent catalyst (x = 1.4).

**Author Contributions:** Conceptualization, O.A.S. and A.G.D.; methodology, O.A.S., S.A.M., A.S.L. and G.N.M.; validation, O.A.S., A.S.L. and G.N.M.; investigation, S.A.M., G.M.T., V.A., T.S. and I.V.R.; data curation, S.A.M. and A.S.L.; formal analysis, S.A.M., A.S.L.; software, S.A.M. and G.M.T.; resources, O.A.S. and A.S.L.; writing—original draft, O.A.S. and G.M.T.; Writing—review and editing, O.A.S., S.A.M., G.N.M. and A.S.L.; visualization, S.A.M. and G.M.T.; project administration, O.A.S. and A.G.D.; funding acquisition, O.A.S.; supervision, A.G.D. All authors have read and agreed to the published version of the manuscript.

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**Data Availability Statement:** The data presented in this study are available in the present paper and supplementary materials.

**Conflicts of Interest:** The authors declare no conflict of interest.

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## Article

# Electrocatalytic Hydrogen Evolution Reaction from Acetic Acid over Gold Immobilized Glassy Carbon Surface

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**Abstract:** A hydrogen fuel cell is a highly promising alternative to fossil fuel sources owing to the emission of harmless byproducts. However, the operation of hydrogen fuel cells requires a constant supply of highly pure hydrogen gas. The scarcity of sustainable methods of producing such clean hydrogen hinders its global availability. In this work, a noble Au-atom-decorated glassy carbon electrode (Au/GCE) was prepared via a conventional electrodeposition technique and used to investigate the generation of hydrogen from acetic acid (AA) in a neutral electrolyte using 0.1 M KCl as the supporting electrolyte. Electrochemical impedance spectroscopy (EIS), open circuit potential measurement, cyclic voltammetry (CV), and rotating disk electrode voltammetry (RDE) were performed for the characterization and investigation of the catalytic properties. The constructed catalyst was able to produce hydrogen from acetic acid at a potential of approximately  $-0.2$  V vs. RHE, which is much lower than a bare GCE surface. According to estimates, the Tafel slope and exchange current density are  $178$  mV dec<sup>-1</sup> and  $7.90 \times 10^{-6}$  A cm<sup>-2</sup>, respectively. Furthermore, it was revealed that the hydrogen evolution reaction from acetic acid has a turnover frequency (TOF) of approximately  $0.11$  s<sup>-1</sup>.

**Keywords:** acetic acid; hydrogen evolution reaction; hydrogen fuel cell; rotating disk voltammetry; gold electrode; turnover frequency

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## 1. Introduction

Energy demand is surging due to population expansion and the introduction of technological conveniences. It is predicted that by 2040, the energy demand will increase by 30%. Most of this energy is produced from fossil fuels, which are non-renewable and detrimental to the environment due to the release of harmful gasses. The existing fossil fuel reserve is already under strain due to the rising energy demand, which is leading it to be exhausted more quickly and release more harmful polluting gases into the atmosphere. As a result, developing environmentally benign as well as self-sustainable fuel sources is crucial and therefore has grown to become one of the most alluring research areas in the present era. In this regard, many alternative energy sources have been reported, including solar energy, ocean energy, hydroelectric power, and wind energy, but none of them have the potential to completely supplant fossil fuel [1–4]. Moreover, the complete utilization of these fuel sources is limited by their uneven distribution.

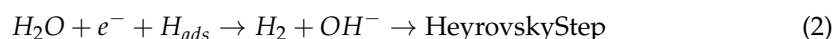
The conversion of chemical energy to electric energy in an electrochemical fuel cell has been considered a promising technique for providing an alternative fuel source due to its eco-friendliness, lower toxicity, and ability to produce electricity with zero carbon



dioxide emission [5]. In an electrochemical fuel cell, the chemical energy of fuel materials such as hydrogen, methanol, and oxygen is converted to electrical energy via a pair of redox reactions. Potential applications range from operating large-scale power stations to small-scale laptops, mobiles, and other electrical devices. In particular, hydrogen has demonstrated great potential as an energy carrier owing to its ability to have a high energy density, greater than almost all hydrocarbons, as well as its ability to produce harmless byproducts (only water) [6–8]. The challenge for the widespread application of hydrogen fuel cells is the availability of highly pure hydrogen. Commercially, hydrogen is obtained from the steam reforming process in which natural gas is heated with steam where hydrogen gas is produced along with toxic carbon monoxide [9,10]. This process utilizes fossil fuel sources for heating and releases toxic gases into the environment. Moreover, the steam reforming process does not produce hydrogen in a pure state but generates a mixture of gasses including CO<sub>2</sub>, CH<sub>4</sub>, etc. [11]. Although the hydrogenase enzyme can produce hydrogen using earth-abundant metals such as iron and nickel, its commercial application is limited due to the low stability of the enzymes outside their native environment and the complex preparation of the catalysts [12]. Two other alternative techniques for generating hydrogen in a highly pure state are photochemical and electrochemical water-splitting reactions [13–15]. However, photochemical water splitting requires a comparatively larger electrode area than electrochemical water splitting, imposing restrictions on choosing viable catalysts with desirable construction sites. Due to its greater adaptability and flexibility, electrochemical water splitting is more desirable. Once more, hydrogen evolution can be driven by electrochemical water splitting because water is renewable and abundant [16,17]. Until now, Pt has been the most efficient catalyst for HER due to its ability to reduce protons at a low overpotential [18–22]. The widespread use of hydrogen fuel cells has remained unexplored even decades after its invention due to the high cost and scarcity of Pt.

Thus, it is exceedingly necessary to develop cost-effective, efficient, and green catalysts for HER. For this purpose, metal phosphides, chalcogenides, carbides, borides, and nitrides have been investigated extensively, yet the problems of high metal content, convoluted operation, and long-term durability have not been overcome yet [23–28]. On the other hand, various nanostructures, heterostructures, and carbon composites have shown interesting activity, but the preparation procedure is still complex [29–32].

The majority of hydrogen evolution reactions have been reported in acidic and alkaline media, while the study of HER in neutral media is very limited [33–35]. However, extreme pH conditions are not only harmful to fuel cell components but also degrade the electrocatalysts. Moreover, since the pH of the natural water reserves on our planet, including the ocean and rivers, is close to neutral, the development of HER in neutral media would be helpful for powering devices sailing in seawater. HER in a neutral media occurs as follows [36,37]:



Nevertheless, due to the low proton concentration in a neutral solution, HER follows sluggish kinetics compared to those of acidic and alkaline media, and water molecules must act as a reactant. Several catalysts such as amorphous MoS<sub>x</sub>, CoP, and FeP have been shown to exhibit good activity for HER in neutral media, but the synthesis procedure of that catalyst is still difficult [38–40].

Pyrolysis of biomass from agricultural waste produces bio-oil in which acetic acid is a major component, constituting around 25% [41]. Furthermore, acetic acid is a great hydrogen carrier that is inflammable and safer than other types of hydrocarbons. The generation of hydrogen from acetic acid can be of great significance, as it not only provides clean fuel but also assists in recycling agricultural waste. Previously, V.S Thoi et al. reported



a molecular catalyst for the generation of hydrogen from acetic acid using non-aqueous media [42]. The preparation of molecular catalysts is a complex procedure and the use of organic media during electrolysis is a convoluted process.

Here, we have investigated a green method for the generation of hydrogen from acetic acid in a KCl medium using a Au-modified glassy carbon electrode. To make the catalysts cost-effective, we have decorated the glassy carbon surface with an extremely thin layer of gold. To the best of our knowledge, no one has ever produced hydrogen from acetic acid using gold-modified glassy carbon, despite substantial research on HER in gold electrodes using H<sub>2</sub>SO<sub>4</sub> being available.

## 2. Experimental Section

### 2.1. Chemicals

Analytical-grade chemicals were purchased and used as received without additional purification. KCl salt was obtained from Merck, Darmstadt, Germany. Alumina powder, sulfuric acid, acetic acid, and tetra chloroauric acid (HAuCl<sub>4</sub>) were purchased from Sigma-Aldrich. All the solutions were prepared using Millipore Milli-Q water (resistivity < 18 MΩ cm and micro-organic concentration < 3 ppb). All the experiments were conducted in clean and N<sub>2</sub>-saturated conditions.

### 2.2. Fabrication of Electrode and Electrochemical Measurements

All electrochemical experiments, such as cyclic voltammetry (CV), open circuit potential (OCP) measurements and electrochemical impedance (EIS) measurements, were conducted with PGSTAT 128N (Autolab, Utrecht, The Netherlands) and CHI 660 (Bee Cave, TX, USA) potentiostats using a typical three-electrode arrangement. In the case of EIS measurements, the frequency range was maintained from 0.1 MHz to 0.1 Hz, with 50 measuring points.

A glassy carbon electrode (GCE) with an exposed geometric surface area of ca. 0.0314 cm<sup>2</sup> was cleaned and modified with Au atoms using the electrodeposition technique. Ag/AgCl saturated with KCl and Pt wire electrodes were used as reference and counter electrodes, respectively. The GCE surface was first polished mechanically with fine alumina powder (down to 0.3 μm) until it turned a shiny black. Then, the polished electrode was rinsed with water and sonicated in ethanol and water for 10 min each to remove the adsorbed particles. Finally, the GCE surface was subjected to electrochemical cleaning in a N<sub>2</sub>-saturated 0.1 M H<sub>2</sub>SO<sub>4</sub> solution from 0.1 to +1.0 V at a scan rate of 0.1 V s<sup>−1</sup> for 50 cycles. The clean electrode was then modified with Au by cycling the potential in a 0.01 M HAuCl<sub>4</sub> solution from 0 V to −1.0 V with a scan rate of 0.1 V s<sup>−1</sup> for two cycles.

To unveil the catalysis of the hydrogen evolution reaction, cyclic voltammograms were recorded at potentials lower than the open circuit potential in a KCl medium by varying the acetic acid concentration (1–7 mM) and scan rate.

The hydrodynamic analysis and linear sweep voltammograms (LSVs) were recorded in a 0.1 M KCl solution with 5 mM acetic acid at a 0.05 V s<sup>−1</sup> scan rate at different rotation rates (400–1200 rpm) using a Modulated Speed Rotator (PINE Incorp., Los Angeles, CA, USA).

In this article, all the potentials were converted into a reversible hydrogen electrode (RHE) using the following expression (4):

$$E_{RHE} = E_{Ag/AgCl} + E^0_{Ag/AgCl} + (0.059 \times pH) \quad (4)$$

where  $E^0_{Ag/AgCl} = 0.1976$  V.

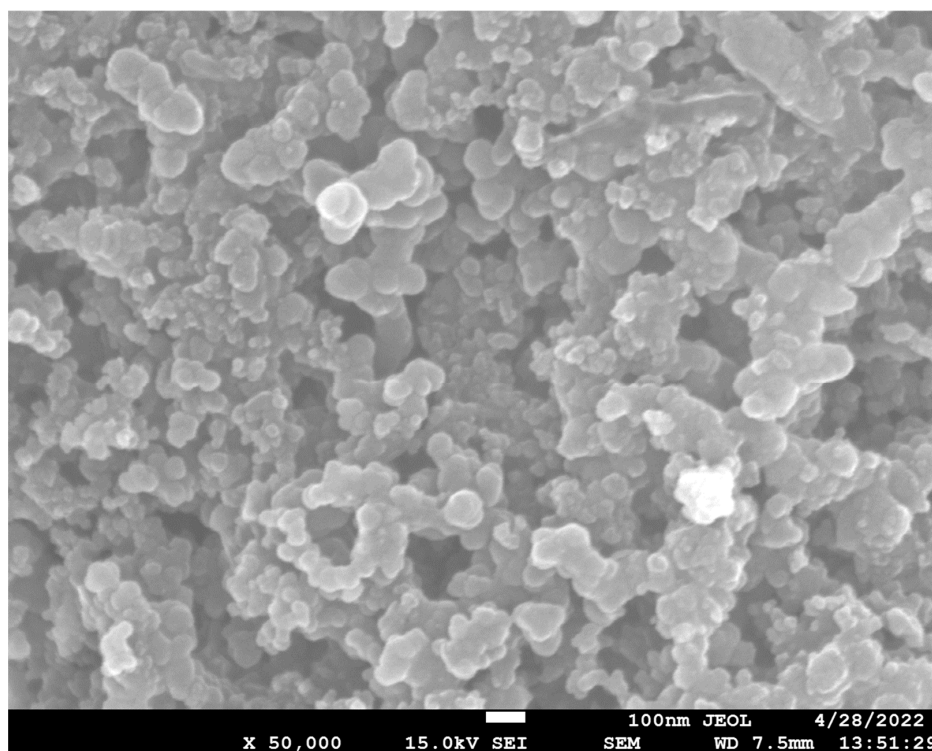
The prepared Au/GCE surface was morphologically characterized using a scanning electron microscope (SEM) (JSM-7610F, JEOL Ltd., Tokyo, Japan). The X-ray photoelectron spectroscopy (XPS)-related analysis was executed using a Thermo Scientific (Waltham, MA, USA) K-Alpha KA1066 spectrometer to unveil the composition of the Au/GCE surface. A monochromatic AlKα X-ray radiation source was used as the excitation source, where the beam-spot size was kept at 300.0 μm. The spectra were recorded in terms of fixed analyzer

transmission mode, where the pass energy was kept at 200.0 eV. The recording of the XPS spectra was executed at pressures of less than  $10^{-8}$  Torr.

### 3. Results and Discussion

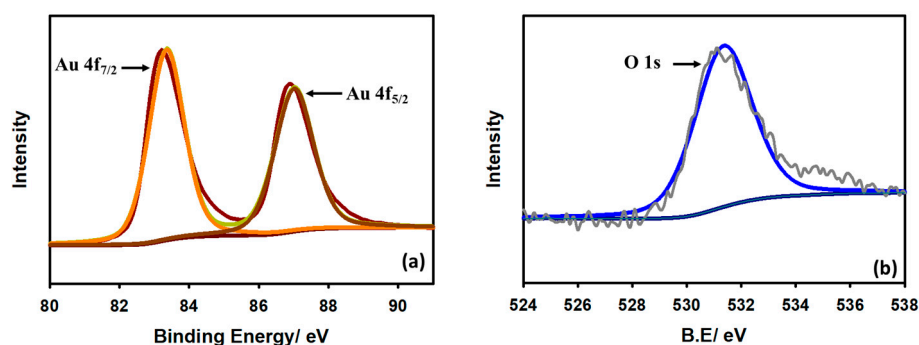
#### 3.1. Surface Characterization

To reveal the surface feature of the Au/GCE electrode, a field-emission scanning electron microscopic (SEM) image was recorded. Figure 1 depicts the SEM image of the Au/GCE surface, which indicates that the Au particles were deposited successfully on the GCE surface. Additionally, the Au particles present on the surface are in a globular shape.



**Figure 1.** SEM image of the Au/GCE surface.

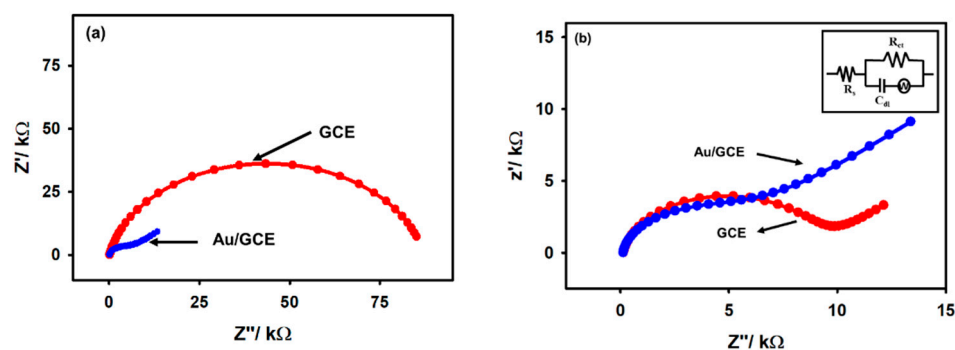
To understand the characteristics of the modified Au/GCE electrode, X-ray photoelectron spectroscopy (XPS) was conducted. Figure 2 depicts the XPS spectrum of Au on the GCE surface. In Figure 2a, the two intense peaks at 83.34 eV and 87.05 eV represent Au 4f<sub>7/2</sub> and Au 4f<sub>5/2</sub>, respectively. The difference between the peaks is noted to be 3.71 eV, which suggests that the surface-located Au particles are metallic. Figure 2b demonstrates that the O 1s spectrum of the modified electrode at approximately 531.34 eV is due to the existence of oxygen in the environment.



**Figure 2.** XPS spectra of Au on GCE surface (a) Au 4f and (b) O 1s.

### 3.2. Electrochemical Characterization

The electrochemical characterization of the Au/GCE electrode was performed by electrochemical impedance spectroscopy (EIS) and open circuit potential (OCP) measurements. Furthermore, the results were compared with those of unmodified GCE electrodes in a similar experimental condition. From the comparative analysis, the modification of GCE with the gold film was confirmed. The conventional display of Nyquist plots recorded using GCE and Au/GCE electrodes is shown in Figure 3 with 5 mM acetic acid in 0.1 M KCl at ca.  $-0.2$  V and  $-0.6$  V. It can be noted from Figure 3a that at  $-0.2$  V in the Nyquist plot with bare GCE, there is a distorted semicircle with an extremely high charge transfer resistance, while in Au/GCE, the Nyquist plot exhibits a Warburg impedance curve. On the other hand, both figures show a Warburg impedance at  $-0.6$  V, indicating that the reduction process is diffusion controlled (Figure 3b). The charge transfer resistance is lower in the case of Au/GCE compared to that of a bare GCE at each potential, indicating that the reduction process is more feasible on the Au/GCE surface than on the bare GCE surface. An Au/GCE electrode was perhaps naturally more negative than a GCE, hence the Au/GCE electrode could attract positively charged protons toward the electrode surface due to Coulombic attraction. The equivalent circuit is shown in the inset of Figure 3b and the charge transfer resistances in each electrode are compared in Table 1.



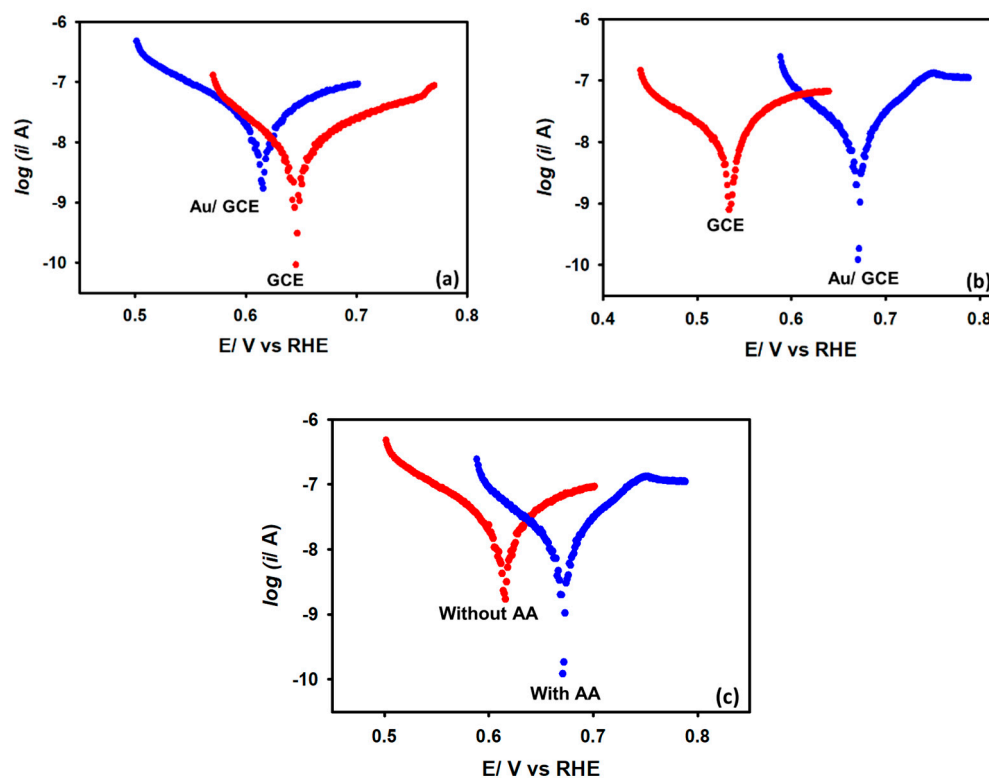
**Figure 3.** The comparative EIS spectra of bare GCE and Au/GCE at the potentials (a)  $-0.2$  V and (b)  $-0.6$  V recorded with 5 mM acetic acid in a 0.1 M KCl  $N_2$ -saturated solution; inset shows the equivalent circuit.

**Table 1.** Values of OCP and charge transfer resistance of a bare GCE and Au/GCE electrode recorded in a  $N_2$ -saturated 0.1 M KCl solution.

Electrode	OCP/V		$R_s/\Omega$	$R_{ct}/k\Omega$
	Without AA	With 5 mM AA		
GCE	0.651	0.542	126	9.78
Au/GCE	0.622	0.675	130	4.70

Next, to justify the OCP observation, the linear polarization curves were recorded with both GCE and Au/GCE electrodes in the presence and absence of 5 mM acetic acid in a KCl medium. It can be noted from Figure 4a that in the absence of acetic acid, the Au/GCE electrode's OCP value is less positive compared to a bare GCE electrode. This observation shows that the Au/GCE electrode has greater capability to attract positively charged cations due to Coulombic interactions. This fact is also consistent with the results obtained from the EIS experiments. However, when the linear polarization curve was recorded in the presence of 5 mM acetic acid, it was observed that the Au/GCE surface became more positive than that of the bare GCE surface (Figure 4b). Thus, it can be assumed that, in the presence of acetic acid, the negatively charged Au/GCE surface provides electrons to reduce the positively charged protons and becomes more positive itself. The OCP values are summarized in Table 1. Figure 4c compares only Au/GCE electrodes with and without

acetic acid. The shifting of the OCP value towards more positive potential in the presence of acetic acid also supports the above argument.

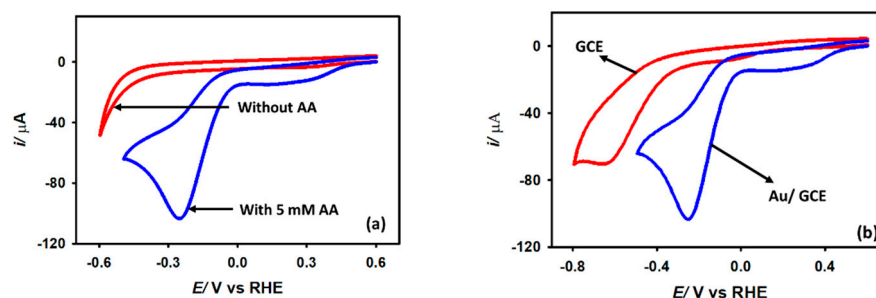


**Figure 4.** Linear polarization curves were recorded with (a) bare GCE and Au/GCE electrodes without AA, (b) bare GCE and Au/GCE electrodes with 5 mM AA, and (c) a Au/GCE electrode with and without AA in a  $N_2$ -saturated KCl solution. Scan rate:  $0.1 \text{ V s}^{-1}$ .

### 3.3. HER Studies

#### 3.3.1. Catalysis

Figure 5a depicts the cyclic voltammograms recorded in a 0.1 M KCl solution with and without 5 mM acetic acid at a  $0.1 \text{ V s}^{-1}$  scan rate with a Au/GCE electrode. As shown, no reduction peak is seen between the potential range of 0 V and  $-0.5 \text{ V}$  when acetic acid is not present. The reduction peak beyond  $-0.5 \text{ V}$  is due to the hydrogen evolution from water. When 5 mM acetic acid is added to the electrolyte solution, an intense reduction peak is obtained at  $-0.2 \text{ V}$ . Thus, this reduction peak is attributed to the reduction of acetic acid. Two reasons can be assumed for the occurrence of this wave: (1) the reduction of acetic acid to aldehyde or alcohol, or (2) the reduction of the proton to generate hydrogen. To confirm the identity of this peak, 5 mM sodium acetate is added to the KCl solution, but no such peak is found at this region. The peak is therefore proven to be related to proton reduction or hydrogen generation from acetic acid, not the reduction of the acetate ion. This is also evident from the appearance of small bubbles at the electrode surface during the CV measurement. Note that in bare GCE, proton reduction from acetic acid occurs at  $-0.6 \text{ V}$ , while in Au/GCE the potential shifted to  $-0.2 \text{ V}$  with an almost 48% higher current. This positive shift of potential is very important as it indicates that less energy is required to generate hydrogen from acetic acid with Au/GCE than that of bare GCE. After it is confirmed that the reduction wave is from proton reduction, some kinetics analysis is performed with the Au/GCE electrode.



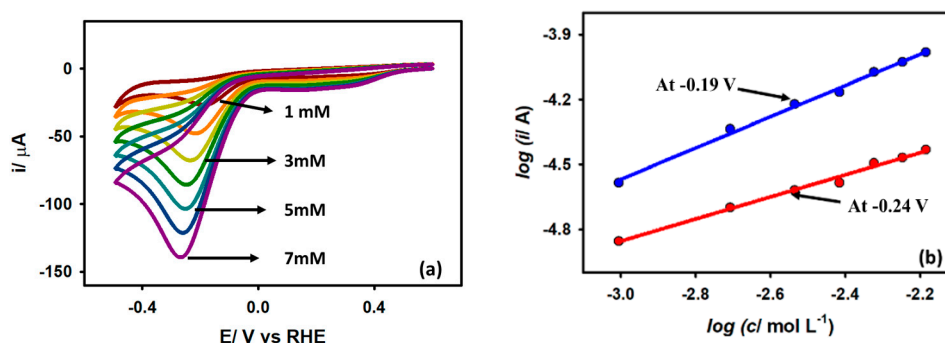
**Figure 5.** Cyclic voltammograms of (a) Au/GCE surface in KCl solution in the presence and absence of 5 mM  $\text{CH}_3\text{COOH}$  (b) bare GCE and Au/GCE surface in presence of 5 mM acetic acid at  $0.1 \text{ V s}^{-1}$  scan rate.

The experiment was repeated using a Au electrode. It was found that a gold electrode reduces protons under the same experimental conditions with insignificant activity (Figure S1, Supplementary information) in the KCl medium. Significant  $\text{H}^+$  reduction performance was obtained in a 0.1 M KCl medium while a Au/GCE electrode was employed. It was prepared by depositing Au particles on the GCE surface from a 0.01 M  $\text{HAuCl}_4$  solution by potential cycling between 0 and  $-1.0 \text{ V}$  (vs.  $\text{Ag}/\text{AgCl}$  (sat. KCl)) two times with a scan rate of  $0.1 \text{ V s}^{-1}$  (Figure S2, Supplementary Information). The Au/GCE electrode prepared with more than two cycles produces large capacitive currents without a significant improvement in Faradaic currents. Hence, all the rest of the experiments were performed by fabricating a Au/GCE electrode with controlled Au deposition on the GCE surface for two potential cycles only.

### 3.3.2. Effect of Acetic Acid Concentration

The variation of peak current ( $i_p$ ) and peak potential ( $E_p$ ) against the concentration of acetic acid at the Au/GCE electrode is shown in Figure 6a. The plot shows that as the AA concentration rises, the peak current progressively increases, and the peak potential slightly shifts in the negative direction. This is due to the concentration overpotential resulting from the increased AA concentration. The kinetic order ( $\beta$ ) of the reaction is often used to disclose the mechanistic route of an electrochemical process. The value of  $\beta$  can be computed from the dependencies of peak currents on the concentration of the electro-active species with the assumption that at the peak potentials, the  $\log i_p$  vs.  $\log C$  curve gives straight lines as per Equation (5):

$$\log i = \log k + \beta \log [C] \rightarrow \quad (5)$$



**Figure 6.** (a) CVs of Au/GCE electrode with varying concentration of acetic acid at  $0.1 \text{ V s}^{-1}$  scan rate. (b) Linear regression plots of  $\log i_p$  vs.  $\log C$  on Au/GCE electrode at  $-0.19 \text{ V}$  and  $-0.24 \text{ V}$ .

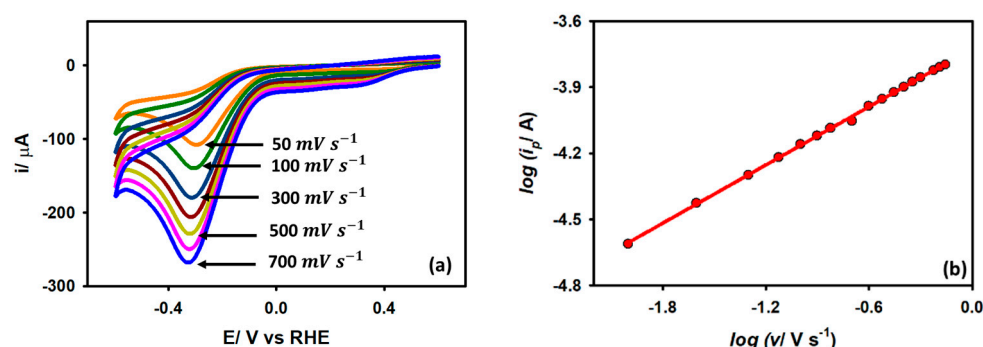
Here,  $k$  is the reaction rate constant. From Figure 6b, using Equation (5) the order of the reaction was found to be 0.56 and 0.62 for Au/GCE at potentials  $-0.19$  V and  $-0.24$  V, respectively, which means that the reaction followed half-order kinetics.

### 3.3.3. Effect of Scan Rate

Cyclic voltammograms were obtained for a Au/GCE electrode in a 0.1 M KCl medium with 5 mM acetic acid with variable scan rates in order to further study the kinetics. It is observed from Figure 7a that when the scan rate is raised from  $0.05$  V s $^{-1}$  to  $0.7$  V s $^{-1}$ , the peak current also increases with a shift of potential toward a slightly negative value. The enhancement of the peak current with an increased scan rate is due to the thinning of the diffusion layer at a higher scan rate. For an irreversible diffusion-controlled reaction, the peak current is linearly dependent on the square root of the scan rate as per the following expression (6):

$$i_p = 2.99 \times 10^5 n A C \alpha^{1/2} D_0^{1/2} v^{1/2} \quad (6)$$

where  $C$  is the bulk acetic acid concentration,  $n$  is the number of heterogeneous electron transfers,  $\alpha$  is the cathodic transfer coefficient,  $A$  is the effective surface area of the working electrode,  $v$  is the scan rate, and  $D_0$  is the diffusion coefficient of acetic acid. The peak current and square root of the scan rate showed a linear connection with a slope value of 0.48, indicating a diffusion control process, which is also compatible with the EIS results.



**Figure 7.** (a) CVs of Au/GCE electrode in 0.1 M KCl medium with 5 mM acetic acid at various scan rates. (b) Linear regression plots of  $\log i_p$  vs.  $\log v$ .

### 3.3.4. Tafel Analysis

The cathodic transfer coefficient,  $\alpha$ , was calculated between 0.42 and 0.48 when the scan rate was raised from  $0.05$  V s $^{-1}$  to  $0.5$  V s $^{-1}$  according to the following formula (7):

$$\alpha = \frac{1.857RT}{F|E_p - E_p^0|} \quad (7)$$

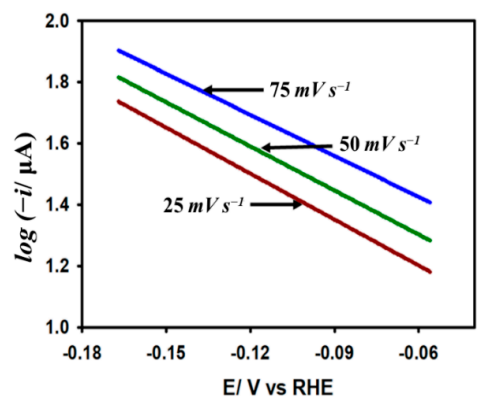
The fairly constant nature of  $\alpha$  at the current maxima indicates that the reaction follows B-V kinetics. In this regard, the Tafel slope is evaluated to understand the insight into the kinetic process of HER on the catalyst surface. Note that the Tafel slope is defined as the slope of the linear region of the plot  $\log(\text{current})$  vs. potential around the activation region of the current potential region as per Equation (8):

$$\ln i = \ln i_0 - \frac{\alpha F}{RT} (E - E^0) \quad (8)$$

Here,  $i$  is the kinetic current,  $i_0$  is the exchange current, and  $-\frac{2.303RT}{F}$  is the Tafel slope. We estimated the Tafel slope to determine the kinetic feasibility of the HER on the Au/GCE surface. Figure 8 demonstrates the Tafel plots obtained from the LSV curves with respect to HER originating from 5 mM acetic acid at 0.025, 0.05, and 0.075 V s $^{-1}$  scan rates. The average slope at three different scan rates is found to be 178 mV dec $^{-1}$ , which outranks



many other metals reported previously for HER [43]. Note that the transfer coefficient equivalent to 0.33 obtained from the Tafel slope is smaller than that acquired at the peak region by Equation (7). This observation suggests that the electron transfer rate is slower at the activation region compared to the diffusional region, which is a highly general feature for most irreversible processes.

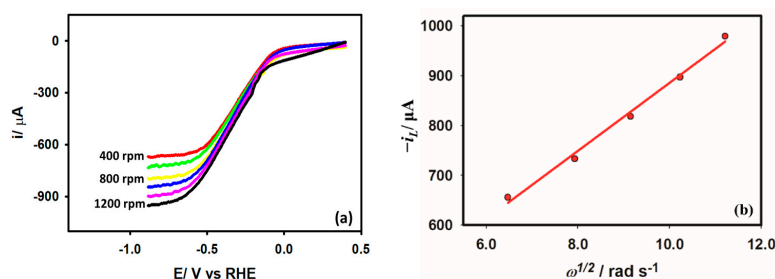


**Figure 8.** Variation of  $\log(i)$  with the applied potential at  $0.025 \text{ V s}^{-1}$ ,  $0.05 \text{ V s}^{-1}$ , and  $0.075 \text{ V s}^{-1}$  scan rates on Au/GCE electrode in  $0.1 \text{ M KCl}$  solution with  $5 \text{ mM AA}$ .

Another important parameter for understanding the HER kinetics is the exchange current density ( $j_0$ ) which depends on the electrode material, electrode surface state, electrolytic composition, and experimental temperature. This current parameter can be derived by extrapolating the Tafel plots to the Y-axis as per Equation (8). It should be noted that  $j_0$  is proportional to the catalytic surface area. The large  $j_0$  value indicates a larger surface area, fast electron transfer, and favorable HER kinetics. From Figure 8, the value of  $j_0$  was calculated to be  $7.90 \times 10^{-6} \text{ A cm}^{-2}$ , which is consistent with other metals found in the literature [17,44].

### 3.3.5. Diffusion Coefficient

Rotating disk electrode voltammetry (RDE) is employed to study the hydrodynamics of the HER from acetic acid. A steady-state concentration profile, and consequently a steady-state current, is produced at the electrode surface when the electrode is rotated at a fixed rate, transporting the electroactive species in the bulk solution to the electrode surface at a fixed rate. Figure 9a depicts the RDE voltammograms of the Au/GCE electrode in a  $0.1 \text{ M KCl}$  medium in the presence of  $5 \text{ mM}$  acetic acid at a  $0.05 \text{ V s}^{-1}$  scan rate. Acetic acid's diffusion coefficient is calculated using the change in steady-state current as a function of the rotation rate provided by the Levich equation. The diffusion coefficient of acetic acid according to Equation (9) is found to be  $6.47 \times 10^{-5} \text{ cm}^2 \text{ s}^{-1}$ , which is consistent with the value of the following literature [42].



**Figure 9.** (a) Rotating disk voltammogram obtained with Au/GCE electrode in  $0.1 \text{ M KCl}$  solution with  $5 \text{ mM}$  acetic acid at  $0.05 \text{ V s}^{-1}$  scan rate. (b) Linear dependency of the limiting current on the square root of the rotation rate.

$$i_L = \frac{0.62nAFD^{2/3}\omega^{1/2}}{v^{1/6}} \quad (9)$$

### 3.3.6. Turnover Frequency

Turnover frequency (TOF) has become one of the crucial parameters in evaluating HER kinetics. It is defined by the transformation of reactive molecules per unit site at a unit time. A higher value of TOF characterizes the efficiency of a catalytic material pertaining to a specific reaction. A common method for estimating the TOF is based on the following two steps: (1) evaluation of the catalytic active sites and (2) calculation of the TOF value according to Equation (10) [45]:

$$TOF = \frac{jA}{2Fm} \quad (10)$$

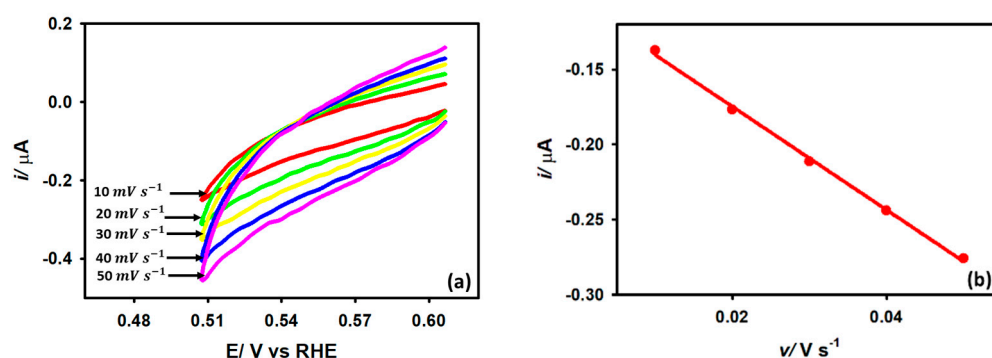
Here,  $j$  is the current density at a defined overpotential,  $A$  is the geometric surface area of the electrode, 2 denotes the number of electron transfers during hydrogen formation,  $F$  is the Faraday constant, and  $m$  is the number of active sites.

The determination of the actual active surface area ( $A$ ) in the catalytic surface is an extremely challenging task. The easiest approach is determining the capacitance ( $C_{dl}$ ) in the double-layer region using Equation (11), which denotes the relationship between capacitive currents and scan rate. The value of  $C_{dl}$  fairly represents the active surface area.

$$i = C_{dl} \times \frac{dV}{dt} \quad (11)$$

The voltammograms concerning capacitive currents in the double-layer region as a function of scan rate are shown in Figure 10 for the Au/GCE electrode in a 0.1 M KCl solution. From the slope of Figure 10b, the  $C_{dl}$  value with respect to the Au/GCE electrode was determined to be  $2.55 \mu\text{F cm}^{-2}$ . By comparing the  $C_{dl}$  value ( $0.65 \mu\text{F cm}^{-2}$ ) obtained for a pure GCE surface in 0.1 M KCl with respect to its area of  $0.0314 \text{ cm}^2$ , the active area of the modified electrode (Au/GCE) was determined to be approximately  $0.12 \text{ cm}^2$  using Equation (12).

$$A_{Au/GCE} = \frac{C_{dl(Au/GCE)}}{C_{dl(GCE)}} \times A_{GCE} \quad (12)$$



**Figure 10.** (a) CVs recorded with Au/GCE electrode in 0.1 M KCl at various scan rates. (b) Linear relation of the current vs. scan rate plot.

By setting the value of  $A_{Au/GCE}$  and equating the slope of the  $i$  vs.  $v$  relationship (Equation (13)) with that obtained from the slope of the peak current vs. scan rate plot (w.r.t Figure 7a), the value of ' $m$ ' was determined to be  $5.76 \times 10^{-9} \text{ mol cm}^{-2}$ .

$$i = \frac{n^2 F^2 A_{Au/GCE} m}{4RT} v \quad (13)$$



Inserting the value of 'm' in Equation (10) with respect to the peak potential of the CV obtained for 5 mM acetic acid, the TOF value was obtained to be  $0.11 \text{ s}^{-1}$ .

Thus, this work has demonstrated a green method for generating clean fuel hydrogen from acetic acid which can be obtained from agricultural waste.

#### 4. Conclusions

A green methodology for the generation of hydrogen from acetic acid was demonstrated using a Au/GCE electrode. The electrode was prepared using a simple and straightforward electrodeposition technique and the electrokinetic investigations were carried out with CV, RDE, OCP, and EIS measurements. EIS and OCP measurements confirmed the successful modification of the GCE surface with Au and revealed the greater feasibility of the Au/GCE surface for proton reduction than that of the bare GCE surface. Cyclic voltammograms show a low overpotential ( $-0.2 \text{ V}$  vs. RHE) for proton reduction in Au/GCE electrodes with around 48% higher current than that of the bare GCE surface. The Tafel slope and exchange current density were estimated to be  $178 \text{ mV dec}^{-1}$  and  $7.90 \times 10^{-6} \text{ A cm}^{-2}$ , respectively, while the diffusion coefficient of AA in KCl was estimated to be  $6.47 \times 10^{-5} \text{ cm}^2 \text{ s}^{-1}$ . Moreover, a high TOF for proton reduction was also observed with Au/GCE electrodes in neutral media. This work not only demonstrates a green approach to clean energy production, but also proposes a recycling method for agricultural waste products.

**Supplementary Materials:** The following supporting information can be downloaded at: <https://www.mdpi.com/article/10.3390/catal13040744/s1>, Figure S1: HER observation from 5 mM acetic acid in 0.1 M KCl using Au, GCE and Au/GCE electrodes obtained scan rate of  $0.1 \text{ V s}^{-1}$ ; Figure S2: Optimization of Au deposition on GCE for HER from 5 mM acetic acid in 0.1 M KCl. The electrodes having different amount of Au deposition was executed by cycling the potential in 0.01 M HAuCl<sub>4</sub> solution from 0 V to  $-1.0 \text{ V}$  with a scan rate of  $0.1 \text{ V s}^{-1}$  for different number of cycles.

**Author Contributions:** B.H.A.: Writing; H.B.: Experimental & draft writing; F.A.I.: editing; M.S.H.: editing, T.A.O.: Editing; N.K.: Surface analysis; M.A.H.: overall supervision. All authors have read and agreed to the published version of the manuscript.

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**Data Availability Statement:** Not applicable.

**Conflicts of Interest:** The author declares no conflict of interest.

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## Article

# The Combined Impact of Ni-Based Catalysts and a Binary Carbonate Salts Mixture on the CO<sub>2</sub> Gasification Performance of Olive Kernel Biomass Fuel

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**Abstract:** In the present work, the individual or synergistic effect of Ni-based catalysts (Ni/CeO<sub>2</sub>, Ni/Al<sub>2</sub>O<sub>3</sub>) and an eutectic carbonate salt mixture (MS) on the CO<sub>2</sub> gasification performance of olive kernels was investigated. It was found that the Ni/CeO<sub>2</sub> catalyst presented a relatively superior instant gasification reaction rate (Rco) compared to Ni/Al<sub>2</sub>O<sub>3</sub>, in line with the significant redox capability of CeO<sub>2</sub>. On the other hand, the use of the binary eutectic carbonate salt mixture (MS) lowered the onset and maximum CO<sub>2</sub> gasification temperatures, resulting in a notably higher carbon conversion efficiency (81%) compared to the individual Ni-based catalysts and non-catalytic gasification tests (60%). Interestingly, a synergetic catalyst-carbonate salt mixture effect was revealed in the low and intermediate CO<sub>2</sub> gasification temperature regimes, boosting the instant gasification reaction rate (Rco). In fact, in the temperature range of 300 to 550 °C, the maximum Rco value for both MS-Ni/Al<sub>2</sub>O<sub>3</sub> and MS-Ni/CeO<sub>2</sub> systems were four times higher ( $4 \times 10^{-3} \text{ min}^{-1}$  at 460 °C) compared to the individual counterparts. The present results demonstrated for the first time the combined effect of two different Ni-based catalysts and an eutectic carbonate salt mixture towards enhancing the CO production rate during CO<sub>2</sub> gasification of olive kernel biomass fuel, especially in the devolatilization and tar cracking/reforming zones. On the basis of a systematic characterization study and lab-scale gasification experiments, the beneficial role of catalysts and molten carbonate salts on the gasification process was revealed, which can be ascribed to the catalytic activity as well as the improved mass and heat transport properties offered by the molten carbonate salts.

**Keywords:** olive kernel; CO<sub>2</sub> gasification; Ni/CeO<sub>2</sub>; Ni/Al<sub>2</sub>O<sub>3</sub>; molten carbonates salt (MS); instant gasification rate; carbon conversion

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## 1. Introduction

The increasing demand for more energy worldwide, along with the rising concerns on climate change, are forcing humanity to speed up defossilization and prioritize the clean transition of the energy mix [1]. However, the wide deployment of intermittent renewables, such as solar and wind power, requires the development of energy and cost efficient large-scale seasonal energy storage technologies to balance electricity grids and avoid costly curtailments, which has not yet been convincingly achieved nowadays [2]. On the other hand, if logistics are resolved, the use of bioenergy potential could sufficiently meet the energy demand and decarbonize our economies. In specific, the thermochemical

exploitation of biomass (combustion, pyrolysis, gasification, etc.) is expected to notably suppress greenhouse gas (GHG) emissions due to the carbon neutral nature of biomass [1,3,4]. According to Di Gulliano et al. [5], biomass-based power plants accompanied by CO<sub>2</sub> capture can achieve negative CO<sub>2</sub> emissions, leading to an estimated CO<sub>2</sub> sequestration potential of 2.0–12.0 Gt CO<sub>2</sub> by 2050.

Agricultural and agro-industrial activities are the main sources of residual biomass that could be used as renewable feedstock in thermochemical cycles, thus enhancing local economies and minimizing waste handling problems [6–10]. Greece possesses large quantities of animal manure and agricultural and agro-industrial residues that are equal to 50 Mt/year [11]. Olive oil industry residues (tree pruning, leaves, pits, kernel and pomace) represent 20% of the total annual residual biomass in Greece, which is the third largest olive oil industry worldwide (350 ktons/year) [12,13]. Specifically, olive kernel accounts for 15% of the total residues resulting as by-products from the olive oil extraction process [14,15]. Among other residues, olive kernel exhibits the lowest moisture content (5–15%), and is thus considered a saleable fuel without further treatment [14–16]. Assuming an average lower heating value (LHV) of olive-based biomass residues equal to 16–18 MJ/kg [17–21] and an electrical efficiency of 25–35% [22–24], the thermochemical exploitation of the total annual quantity of olive oil-industry residues in Greece (10 Mt) could potentially produce around 14–15 GWh/year of energy. However, uncertainties associated with the Greek institutional framework towards biomass-based power plants are slowing down practical applications at larger scales [25–27].

Converting biomass to heat, electrical power, biofuels, and chemicals via the gasification process is of paramount importance in achieving energy independence and increasing the share of renewables in the energy mix. In principle, gasification process includes two main consecutive steps: (a) a relatively fast step ( $t < 60\text{ s}$  @  $300\text{--}700\text{ }^{\circ}\text{C}$ ), involving the thermal decomposition of volatile components to gaseous products, tars (condensable hydrocarbon compounds), and a solid char residue, and (b) a slower step ( $t > 3300\text{ s}$  @  $T > 700\text{ }^{\circ}\text{C}$ ), including the gasification of the pyrolyzed char (gas-solid reactions) along with other gas-phase reforming reactions [28]. Suitable gasifying agents (air, steam, CO<sub>2</sub>, or their mixture) can benefit the gasification reaction of the remaining char [4,29,30]. Apart from the gasifying agent, from a process system perspective, the main factors affecting syngas quality and quantity are the employed operating temperature and pressure, gasifier design and heating mode, the addition of catalysts, and the feedstock composition [31,32].

Despite the advantages of biomass exploitation through the gasification process, there are specific challenges that seriously affect the gasification performance in terms of the as-produced syngas quantity and quality. Syngas clean-up from impurities such as tars and water is of high priority towards producing a final product suitable for several downstream processes, i.e., in high-temperature fuel cells for the co-generation of heat and power or in catalytic reactors for the production of synthetic fuels and/or chemicals [33–35]. Mechanical separation methods for the removal of particulate matter (wet scrubber, cyclone, filter, and electrostatic precipitator), along with tar thermal cracking, have been widely used for syngas clean-up and conditioning [36–38]. However, the relatively high capital cost and the formation of small, complex tar structures restrict the commercialization of gasification technology [38]. In this regard, the use of highly active catalysts, in situ or outside the gasifier, has been proposed to reform tars, generating additional syngas with negligible impurities. Moreover, the use of catalysts in gasification leads to faster kinetics at decreased temperatures, further enhancing its efficiency [33,34,39]. Numerous studies [40–43] highlighted the main criteria for a good catalyst selection, which include the decrease of energy activation for tar cracking, gas-solid and gas-phase reactions, the reduced supply of gasifying agents, and the generation of high-value chemicals.

In general, catalysts used in biomass gasification can be divided into three major categories: (a) natural mineral catalysts (dolomite, olivine, zeolites, alumina), (b) alkali and alkaline Earth metal catalysts, AAEMs (Li, Na, K, Mg, Ca, and Rb), and (c) transition metal catalysts [44,45]. Among all of the transition metals (group VIII), Ni-based catalysts

have been widely reported in the literature [28,44,46–50]. This can be attributed to their remarkable role on tar removal, steam reforming, and water gas shift (WGS) reactions, for H<sub>2</sub>-rich syngas production [44,45]. For instance, Baker et al. [51] and Li et al. [52] investigated the performance of commercial nickel catalysts in fluidized bed gasifiers in the temperature range of 700–800 °C during sawdust and pine flakes steam gasification. They both noticed the pronounced role of Ni catalysts during steam gasification in terms of gaseous product yield and tar elimination. However, in both studies, the catalysts suffered from rapid deactivation (<5 h) due to carbon deposition on the catalyst surface and nickel particles sintering. In this regard, numerous studies investigated and proposed alternative routes to modify Ni based catalysts, including the use of different supporting materials and/or aliovalent doping (Fe, Co, La Ce, Mg, etc.) [46–50,53–62]. Several types of supporting materials have been examined in the literature, involving metal oxides, among others [44,45]. Metal oxides (CeO<sub>2</sub>, Al<sub>2</sub>O<sub>3</sub>, ZrO<sub>2</sub>), natural minerals (olivine, dolomite), and zeolites can provide mechanical strength, improved textural properties, and adsorption ability if they are employed as supports in Ni-based catalysts [63,64].

In addition to the use of catalysts, molten alkali carbonate (MAC) salts have been extensively studied in biomass gasification for tar elimination and enhanced syngas production [65–67]. In general, MAC salts (Li<sub>2</sub>CO<sub>3</sub>, Na<sub>2</sub>CO<sub>3</sub>, K<sub>2</sub>CO<sub>3</sub>, etc.) in eutectic compositions can be utilized as excellent industrial fluids in a wide range of high temperature operating technologies (solar power applications, waste oxidation, direct carbon fuel cells, and catalytic biomass gasification) [66]. A well-established application of MAC salts is as heating carriers, since they exhibit a dual function as solar heat storage and heat transfer media [65]. Unlike the use of solar-heated MACs as an indirect heating medium for pyrolysis and/or gasification processes, the direct contact of molten salts and biomass particles can lead to an enhanced gasification rate and syngas production. This enhancement can be attributed to the facilitation of mass and heat transfer phenomena induced by MACs in conjunction with their alkali-based catalytic nature [66].

Various studies have been devoted to interpreting the gasification mechanism of solid fuels in the presence of MAC salts [68–74]. Notably, the majority of works are dealing with pure carbon and coal/biomass chars. For instance, McKee and co-investigators [68] concluded that the catalytic gasification of coal char over K<sub>2</sub>CO<sub>3</sub> involves the following steps: (a) melting of K<sub>2</sub>CO<sub>3</sub> salt, (b) its precipitation at the char surface area (pores), and (c) the formation of a thin layer favoring the carbon-catalyst interaction.

Gasifying agents notably affect the overall reaction network and, in turn, the syngas formation reaction rate. Strong gasifying agents (pure oxygen and steam) can affect the thermal stability of MAC salts [75], whereas the formation of hydroxide intermediates (MOH) and salt oxides (M<sub>2</sub>O<sub>2</sub>) may lead to fouling and plugging of the reactor and pipeline system [28,76]. However, CO<sub>2</sub> is expected to be a suitable gasifying agent for biomass gasification in the presence of MAC catalysts since it can maintain MACs' stability at high temperatures [28]. Taking into account the efforts towards CO<sub>2</sub> mitigation, CO<sub>2</sub> biomass gasification over MAC salts can be a promising route towards producing biofuels and high value products with negative CO<sub>2</sub> emissions [77–80]. In the light of the above aspects, the majority of the studies regarding biomass gasification over MAC salts are restricted to the use of CO<sub>2</sub> as a gasifying agent [28,81–87].

As mentioned above, the char-CO<sub>2</sub> gasification reaction requires more energy compared to other gasifying agents (air, oxygen, and steam) and can be considered the rate-determining step of the overall reaction network [88]. Interestingly, catalyst addition to MACs could synergistically lead to enhanced tar-free syngas production, sufficiently simplify gas clean-up steps, and render the whole process less complex and economically feasible for large-scale applications [28]. As extensively mentioned above, commercial nickel and modified Ni-based catalysts can facilitate biomass gasification, tar cracking, and reforming reactions. In fact, Ni-based catalysts are both selective for hydrogen production and highly efficient towards carbon conversion. Very few works have reported on the combination of Ni-based catalysts and molten alkali carbonate salts during biomass

gasification [28,76]. Specifically, Sakhon Ratchahat and co-workers [28,76] investigated the catalytic effect of a combined Ni/Al<sub>2</sub>O<sub>3</sub> and ternary carbonate salt (Li<sub>2</sub>-K<sub>2</sub>-Na<sub>2</sub>-CO<sub>3</sub>) catalytic system on the pyrolysis and CO<sub>2</sub> gasification of different biomass wastes.

In this context, the present work aims for the first time to systematically explore the combined impact of different Ni-based catalysts (Ni/CeO<sub>2</sub> and Ni/Al<sub>2</sub>O<sub>3</sub>) and an eutectic binary carbonate salt mixture (Li<sub>2</sub>CO<sub>3</sub>-K<sub>2</sub>CO<sub>3</sub> molten salt, MS) on the CO<sub>2</sub> gasification performance of olive kernels under non-isothermal operating conditions in a lab-scale fixed-bed reactor. Various characterization techniques (H<sub>2</sub>-TPR, SEM, HR/SEM\_EDS, TEM, HR/TEM, and XRD) were applied to investigate the morphological and structural properties of these catalysts. It was disclosed that the type of commercial metal oxide used as support (Al<sub>2</sub>O<sub>3</sub> or CeO<sub>2</sub>) does not significantly affect the activity of Ni catalysts towards CO<sub>2</sub> gasification. However, the addition of the binary eutectic carbonate mixture (MS) resulted in a notably favorable performance during olive kernel-CO<sub>2</sub> gasification tests, leading to a high CO yield and carbon conversion efficiency. More interestingly, a synergistic MS-Ni medium effect in the low-temperature CO<sub>2</sub> gasification zone was revealed, boosting carbon monoxide production yields and carbon conversion efficiency.

## 2. Results and Discussion

### 2.1. Structural Characterization (XRD Analysis)

Figure 1 shows the XRD patterns of Ni/CeO<sub>2</sub>, Ni/Al<sub>2</sub>O<sub>3</sub> and their blends with the binary carbonate salt mixture. All catalysts exhibited the characteristic peaks of cubic NiO at 2θ angles of ca. 37, 43, 63, 76, and 79.5° (PDF #73-1519). No characteristic peaks of precursor Ni(NO<sub>3</sub>)<sub>3</sub> or of other nitrates were detected, indicating that nickel nitrate was totally utilized and decomposed during the catalysts' preparation procedure. Furthermore, the d-spacing (d) values of as-prepared catalysts, calculated by Bragg's law, along with the corresponding lattice parameters (α), are summarized in Table 1. In addition, by applying the Scherrer equation [89], the primary crystallite sizes (D<sub>XRD</sub>) of ceria and alumina were found to be 54.92 and 73.22 nm, respectively (Table 1). Moreover, the crystallite size (D<sub>XRD</sub>) of the NiO particles on both the alumina and ceria supports was calculated at ca. 40 nm (37.22 and 42.83, respectively, in Table 1), in accordance with HR-SEM observations (Section 2.2). Both MS-Ni catalysts exhibited characteristic peaks at 2θ angles of 28–35, 40, and 47°, which are attributed to Li<sub>2</sub>CO<sub>3</sub>-K<sub>2</sub>CO<sub>3</sub> carbonates (Figure 1).

Notably, the characteristic peaks attributed to NiO and carbonates phases present lower intensities in the case of CeO<sub>2</sub>-containing samples, ascribed to the higher crystallinity of ceria compared to that of alumina. However, in the case of Ni/Al and MS-Ni/Al catalysts, the high-intensity characteristic peaks at 2θ = 37 and 43° can be ascribed to the co-existence of NiO, Al<sub>2</sub>O<sub>3</sub>, NiAl<sub>2</sub>O<sub>4</sub> and carbonates phases. Interestingly, it should be noticed that small shoulder peaks standing for NiAl<sub>2</sub>O<sub>4</sub> spinel oxide (#77-1877) can be found at 2θ = 37, 45, and 65°, indicating its formation, which has also been confirmed by H<sub>2</sub>-TPR (see in Section 2.3). In particular, under high calcination temperatures (above 700 °C), nickel ions are migrating into the alumina lattice, forming the spinel structure (NiAl<sub>2</sub>O<sub>4</sub>), through the solid-solid interaction of NiO with Al<sub>2</sub>O<sub>3</sub>.

### 2.2. Morphological Characterization (SEM, HR-SEM, EDS Mapping, and TEM)

Figure 2 illustrates the SEM images of the fresh samples prior to gasification experiments. It can be observed from Figure 2a,b that both Ni/Al<sub>2</sub>O<sub>3</sub> and Ni/CeO<sub>2</sub> catalysts display an irregular morphology consisting of nano-sized particles. Additionally, micro-scaled agglomerates are present on both catalysts, attributed to the high calcination temperature, which presumably leads to the sintering of NiO particles and/or supporting materials [44,45].

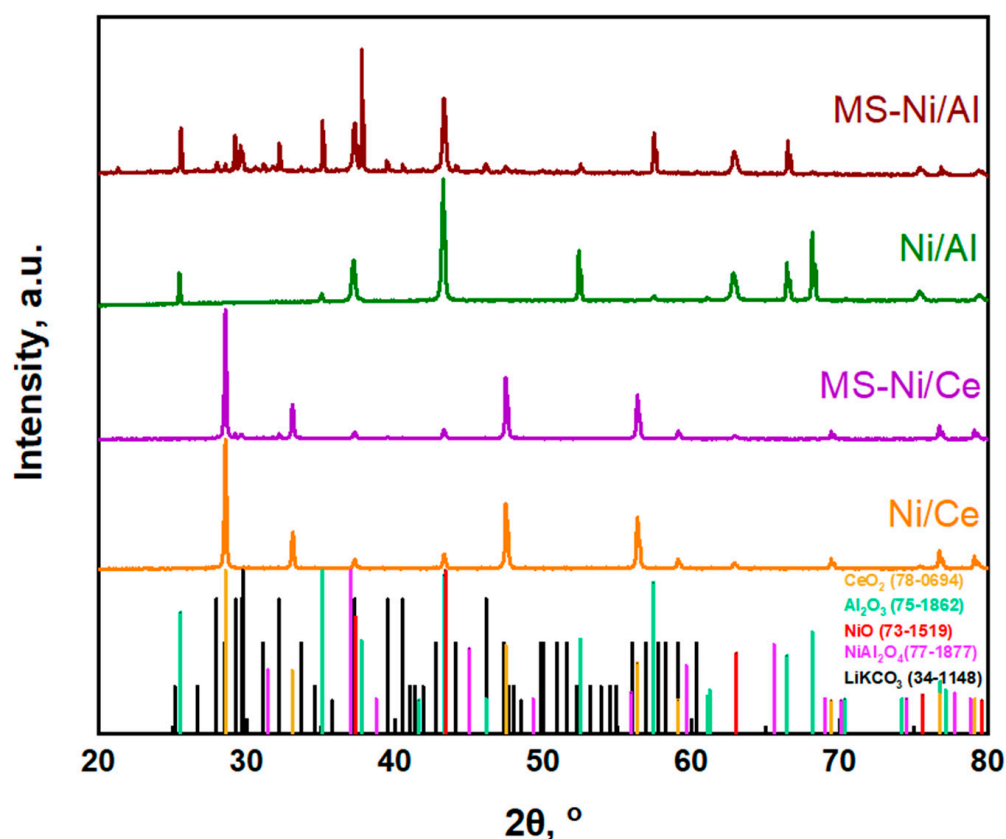


Figure 1. XRD patterns of Ni-based and MS-Ni-based catalysts.

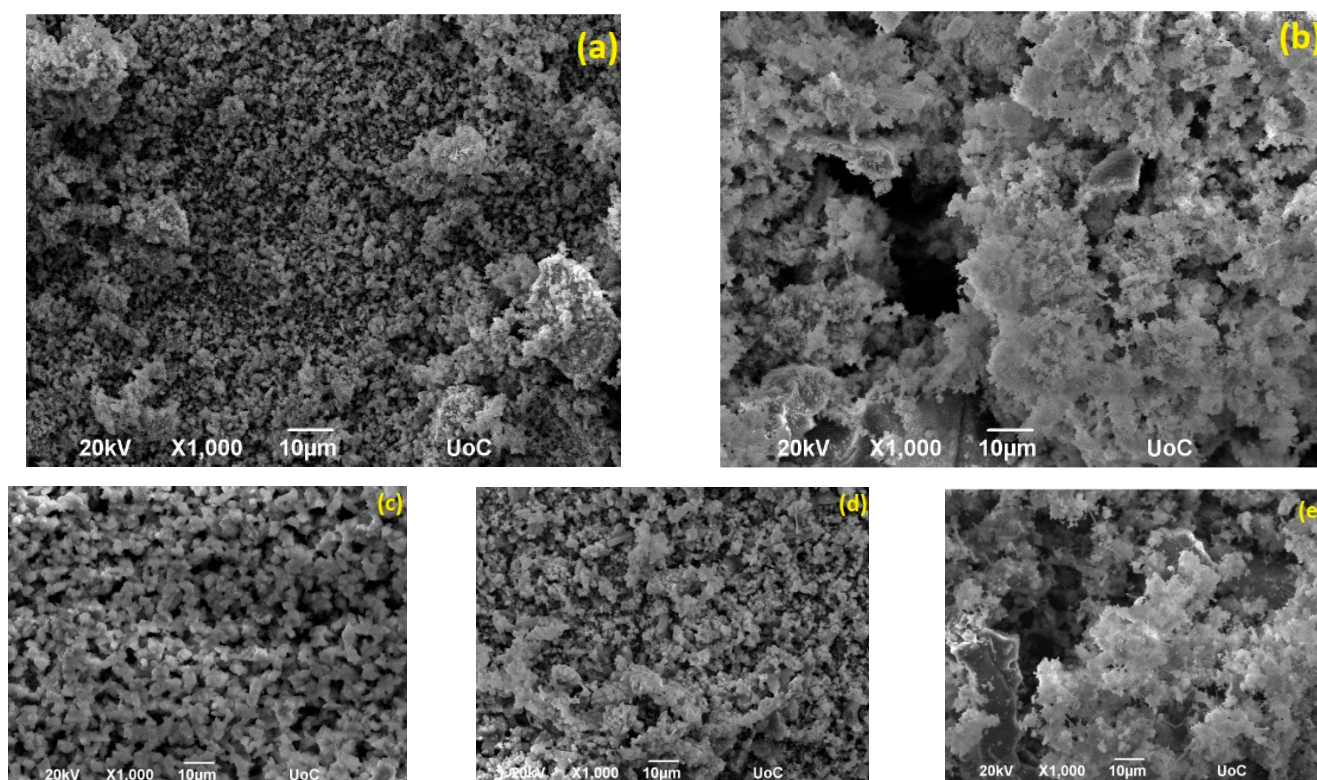
Table 1. XRD and TEM results for the as-prepared Ni/CeO<sub>2</sub> and Ni/Al<sub>2</sub>O<sub>3</sub> catalysts.

Sample		XRD					TEM
Ni/CeO <sub>2</sub>	CeO <sub>2</sub> (111)			NiO (200)			NiO mean particle size
	D <sub>XRD</sub> (nm) <sup>1</sup>	d (nm) <sup>2</sup>	a (nm)	D <sub>XRD</sub> (nm) <sup>1</sup>	d (nm) <sup>2</sup>	a (nm)	
	54.92	0.31	0.54	42.83	0.21	0.42	38.1 ± 8.5
Ni/Al <sub>2</sub> O <sub>3</sub>	Al <sub>2</sub> O <sub>3</sub> (113)			NiO (200)			NiO mean particle size
	D <sub>XRD</sub> (nm) <sup>1</sup>	d (nm) <sup>2</sup>	a (nm)	D <sub>XRD</sub> (nm) <sup>1</sup>	d (nm) <sup>2</sup>	a (nm)	
	73.22	0.21	n/a *	37.22	0.21	0.42	37.7 ± 9.0

\* Aluminum forms a rhombohedral crystal lattice, not a cubic lattice such as CeO<sub>2</sub> and NiO. <sup>1</sup> Calculated applying Scherrer's equation. <sup>2</sup> Calculated by Bragg's law.

Figure 2c illustrates a uniform surface for the binary molten salt carbonate mixture (MS) with particle sizes less than 10 μm, confirming that the preparation protocol resulted in a relatively homogeneous blend. In the case of MS/catalyst mixtures (Figure 2d,e), the catalytic particles retained their irregular shape together with the presence of certain agglomerates due to the calcination pretreatment. At the same time, EDS analysis (not shown for the sake of brevity) demonstrates that Ni loading is practically equal to the nominal one (ca. 15 wt.%) in the case of Ni/CeO<sub>2</sub>, whereas a slightly lower value was revealed for Ni/Al<sub>2</sub>O<sub>3</sub> (13 wt.%).





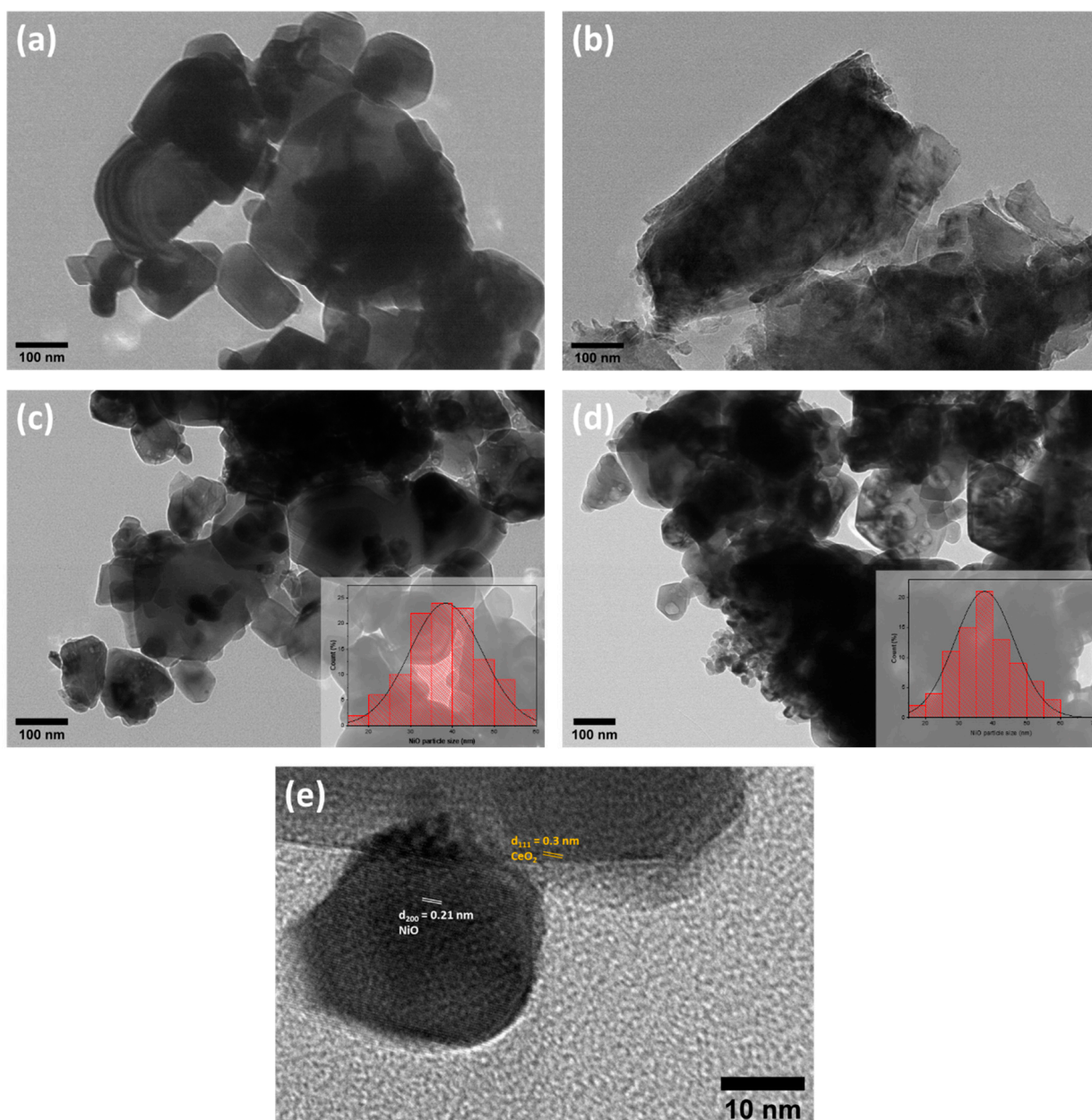
**Figure 2.** SEM images of the as-prepared samples: (a) Ni/CeO<sub>2</sub>; (b) Ni/Al<sub>2</sub>O<sub>3</sub>; (c) MS (d) MS-Ni/CeO<sub>2</sub>; and (e) MS-Ni/Al<sub>2</sub>O<sub>3</sub>.

TEM analysis was applied to gain further insight into the morphological features of the samples (Figure 3). The bare support materials are presented in Figure 3a,b, while Ni/CeO<sub>2</sub> and Ni/Al<sub>2</sub>O<sub>3</sub> are shown in Figure 3c,d. In the case of both Ni/CeO<sub>2</sub> and Ni/Al<sub>2</sub>O<sub>3</sub>, the mean particle size of NiO was ca. 40 nm, verifying the XRD findings, as shown in Table 1. It is worth noting that the wet-impregnation method and calcination at 850 °C resulted in similar NiO particle sizes. Given the inherent difficulties in distinguishing between commercial CeO<sub>2</sub> and NiO particles, the lattice fringes of NiO and CeO<sub>2</sub> were identified, which are reflective of the crystallinity of the samples. In particular, for the Ni/CeO<sub>2</sub> sample, the distinction was established by the calculation of the d-spacing values in an indicative HR-TEM image (Figure 3e). The lattice spacing for the phases of NiO and CeO<sub>2</sub> were 0.2 and 0.3 nm, respectively, which confirms the presence of NiO particles by exposing (200) planes that are in contact with CeO<sub>2</sub> (111), further confirming the results from XRD. In addition, it can be clearly seen that NiO cluster particles are semi-submerged upon the CeO<sub>2</sub> support and are characterized by a quasi-spherical shape.

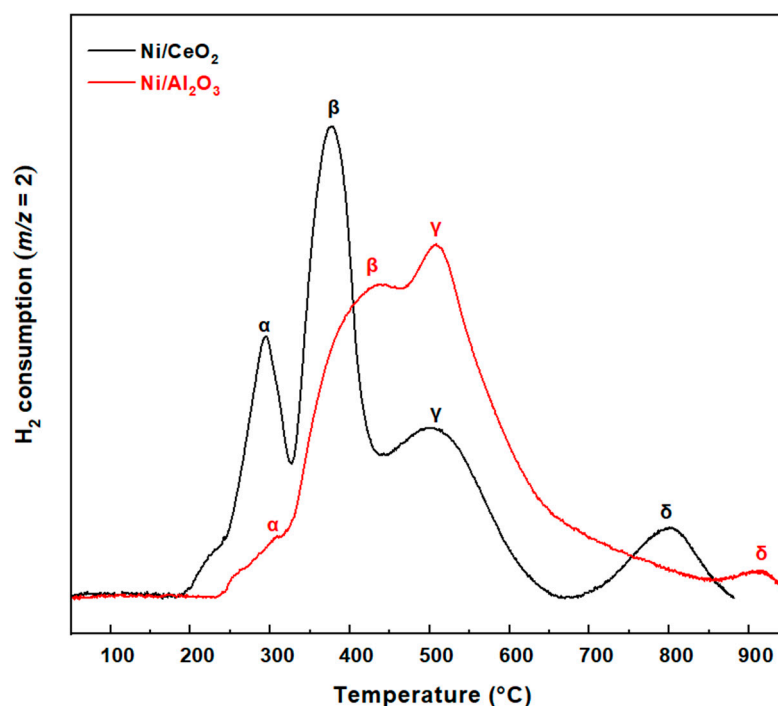
### 2.3. Redox Behavior (H<sub>2</sub>-TPR Analysis)

The reduction profiles (H<sub>2</sub>-TPR) of Ni/CeO<sub>2</sub> and Ni/Al<sub>2</sub>O<sub>3</sub> samples are compared in Figure 4. Four major H<sub>2</sub> consumption peaks were observed for both Ni-based catalysts. Notably, for Ni/CeO<sub>2</sub>, the onset reduction temperature is around 180 °C, whereas for Ni/Al<sub>2</sub>O<sub>3</sub>, this temperature is significantly higher (ca. 235 °C), implying the beneficial effect of ceria in the low-temperature reducibility [58,90–92]. Specifically, a low-temperature peak at 295 °C (peak α) and a prominent medium-temperature peak at 376 °C (peak β) can be distinguished in the low-temperature region (below 500 °C) for the Ni/CeO<sub>2</sub> catalyst. These peaks can be associated with the reduction of NiO species strongly interacting with the CeO<sub>2</sub> support [46,50,91,93–96]. Notably, a shoulder at 242 °C can be in addition observed, which can be ascribed to the reduction of the loosely bound NiO species and/or to surface-absorbed O<sup>2−</sup>/O<sup>−</sup> species (oxygen vacancies associated with the formation of the Ni-O-Ce structure) [97,98]. The peak at 502 °C (peak γ) corresponds to the reduction of

bulk NiO species. Lastly, the low intensity reduction peak above 750 °C (peak  $\delta$ ) can be attributed to the reduction of the CeO<sub>2</sub> bulk [46,50,91,93]. For the Ni/Al<sub>2</sub>O<sub>3</sub> catalyst, one smaller and two major reduction peaks were observed at 310, 436, and 507 °C, respectively. The first peak (peak  $\alpha$ ) is assigned to the reduction of the loosely bound NiO species, whereas the two peaks at 436 and 507 °C (peaks  $\beta$ ,  $\gamma$ ) are attributed to the NiO species interacting with the Al<sub>2</sub>O<sub>3</sub> support [91–93]. Finally, the last reduction feature (peak  $\delta$ ) at the high temperature zone (above 900 °C) corresponds to the reduction of NiAl<sub>2</sub>O<sub>4</sub> spinel phases, suggesting a strong interaction between NiO and Al<sub>2</sub>O<sub>3</sub> species, in good agreement with the XRD findings and relevant literature studies [50,91,93,97,98].



**Figure 3.** (a) TEM image of CeO<sub>2</sub>; (b) TEM image of Al<sub>2</sub>O<sub>3</sub>; (c,d) TEM images and NiO particle size distribution (PSD histograms) of the as-prepared Ni/CeO<sub>2</sub> and Ni/Al<sub>2</sub>O<sub>3</sub>, respectively; (e) HRTEM image of Ni/CeO<sub>2</sub>.



**Figure 4.** H<sub>2</sub>-TPR profiles of the as-prepared Ni/CeO<sub>2</sub> and Ni/Al<sub>2</sub>O<sub>3</sub> catalysts.

Quantitative analysis of the H<sub>2</sub>-TPR profiles was also carried out by calculating the H<sub>2</sub> uptake (mmol H<sub>2</sub>/g) of each peak (Table 2). As expected, regarding the reducibility of the samples in the low-temperature region ( $T < 500$  °C), the calculated H<sub>2</sub> consumption values were almost identical for both Ni/CeO<sub>2</sub> and Ni/Al<sub>2</sub>O<sub>3</sub> catalysts (2.5 mmol/g<sub>cat</sub>). However, H<sub>2</sub> is consumed at relatively lower temperatures in the case of the Ni/CeO<sub>2</sub> catalyst, indicative of the superior reducibility of ceria-based oxides, facilitated by metal-support interactions [46,90,97,99]. Moreover, the total hydrogen consumption in the case of Ni/Al<sub>2</sub>O<sub>3</sub> catalyst (2.65 mmol H<sub>2</sub>/g<sub>cat</sub>), which almost coincides with the theoretical amount of H<sub>2</sub> required for the complete reduction of NiO to metallic Ni<sup>0</sup> (~2.5 mmol H<sub>2</sub>/g<sub>cat</sub>), implies a complete reduction of NiO species. On the other hand, in the case of the Ni/CeO<sub>2</sub> catalyst, the relatively higher H<sub>2</sub> consumption (compared to the theoretical one) can be presumably attributed to the reduction of surface oxygen species of CeO<sub>2</sub>, which is facilitated by nickel-ceria interactions. To summarize, the results show that both Ni catalysts present a redox ability at the lower (250–400 °C) and intermediate (400–600 °C) temperature regimes. This can be an indication that more labile oxygen species could be involved in the primary and secondary tar cracking and/or reforming reactions, effectively reducing the tar content in the as-produced syngas [100]. Moreover, the peak observed at 800 °C and attributed to the reduction of bulk CeO<sub>2</sub> species may lead to additional syngas production by the oxidation of the remaining char and/or formatted carbon on the catalyst's surface (carbon deposition) [99].

**Table 2.** Redox properties of the Ni/CeO<sub>2</sub> and Ni/Al<sub>2</sub>O<sub>3</sub> samples.

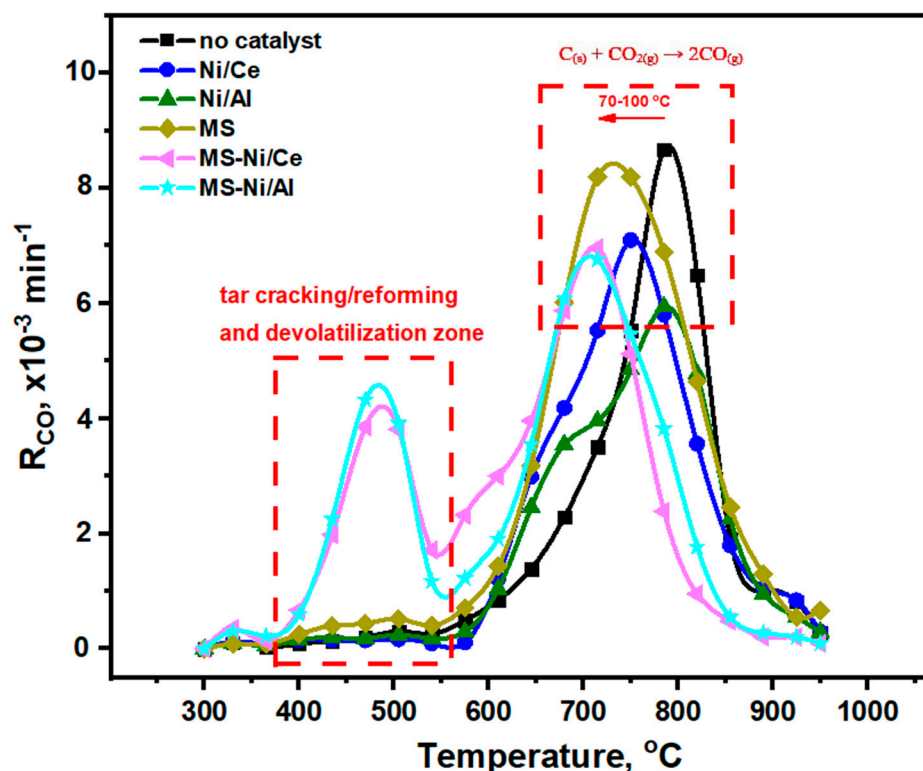
	Total H <sub>2</sub> Uptake (mmol H <sub>2</sub> /g)	α	β	γ	δ
Ni/CeO <sub>2</sub>	2.85	0.69 (295 °C)	1.10 (376 °C)	0.70 (502 °C)	0.35 (802 °C)
Ni/Al <sub>2</sub> O <sub>3</sub>	2.65	0.04 (310 °C)	1.33 (436 °C)	1.21 (507 °C)	0.06 (916 °C)

#### 2.4. Catalyst-Aided CO<sub>2</sub> Gasification Experiments under Batch Mode of Operation

Figures 5 and 6 depict the instant CO production rate,  $R_{CO}$  (min<sup>−1</sup>), and carbon to CO conversion efficiency,  $X_{CO}$ , as a function of temperature during the batch non-isothermal



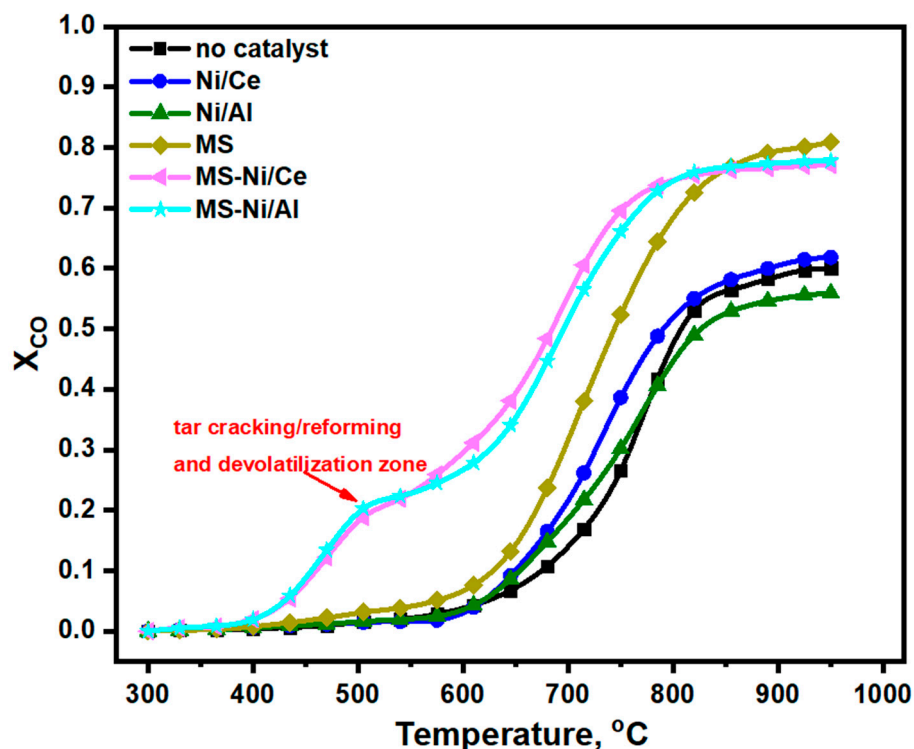
CO<sub>2</sub> catalytic gasification tests over the different catalytic systems examined (Ni/CeO<sub>2</sub>, Ni/Al<sub>2</sub>O<sub>3</sub>, MS, and MS-Ni systems). For comparison purposes, the catalyst-free gasification experiments are also included. The CO<sub>2</sub> gasification process includes two consecutive steps (Table 3): the volatile decomposition and tar cracking/reforming reactions (R1–R6,) in the temperature range of 300–600 °C (step 1), and the reaction of the remaining char with CO<sub>2</sub> (R9) along with other solid and/or gas-phase reactions (R7, R8), denoted as step 2 [36].



**Figure 5.** Effect of temperature and catalyst addition on the instant CO production rate ( $R_{CO}$ ) during non-isothermal CO<sub>2</sub> gasification experiments. Gasifying agent flowrate = 30 cm<sup>3</sup>/min of 20 vol.% CO<sub>2</sub> in Helium.

In this regard,  $X_{CO}$  (Equation (1) in Section 3.4) involves a first term standing for the CO production during the tar cracking and devolatilization stage and a second term corresponding to the CO formation associated with the Boudouard reaction (R9) during the gasification stage [81,101]. In all cases, carbon monoxide was the principal product of gasification, appearing at different temperature regimes depending on the presence and the of catalyst. CO production, which is favored with temperature due to the endothermic reaction R9 [77], reaches its maximum and then gradually decreases until fuel depletion. During the olive kernel non-catalytic CO<sub>2</sub> gasification, a maximum  $R_{CO}$  value ( $8.5 \times 10^{-3} \text{ min}^{-1}$ ) was observed at a temperature of 785 °C. Both Ni/CeO<sub>2</sub> and Ni/Al<sub>2</sub>O<sub>3</sub> catalysts did not reveal any significant effect on the CO production rate. However, a slight reduction in the onset and peak gasification temperature was noticed in the case of the Ni/CeO<sub>2</sub> catalyst. Indeed, the maximum  $R_{CO}$  value for Ni/CeO<sub>2</sub> sample (ca.  $7 \times 10^{-3} \text{ min}^{-1}$ ) was attained at 750 °C, which is 35 °C lower compared to the non-catalytic gasification. On the other hand, Ni/Al<sub>2</sub>O<sub>3</sub> exhibited a maximum  $R_{CO}$  value equal to  $6 \times 10^{-3} \text{ min}^{-1}$  at 780 °C, a slightly lower temperature compared to the un-catalyzed reaction (795 °C). The lower  $R_{CO}$  values obtained during the Ni-based catalytic CO<sub>2</sub> gasification reaction as compared to the non-catalytic process ( $8.5 \times 10^{-3} \text{ min}^{-1}$ ) can possibly be attributed to the faster fuel depletion in conjunction with the favorable conditions for the endothermic Boudouard reaction (R9), since the gasification process takes place at lower temperatures. However, in the temperature regime of 600–750 °C, the  $R_{CO}$  values for the Ni-based catalysts were higher compared to those obtained during the uncatalyzed gasification reaction. Apart from the

CO generated via the endothermic R9 reaction, Sakhon Ratchahat and co-investigators [28] proposed a different pathway for CO production. In brief, solid carbon atoms react with the adsorbed oxygen on a support surface, resulting from the CO<sub>2</sub> dissociation on Ni active sites, leading to additional CO production (carbon cleavage reaction on Ni active sites). Notably, for the Ni/Al<sub>2</sub>O<sub>3</sub> catalytic gasification, at temperatures above 650–700 °C, the R<sub>co</sub> values present a pronounced descending trend compared to the Ni/CeO<sub>2</sub> catalyst. This can presumably be attributed to two different phenomena that take place during the high temperature char-gasification stage: (a) the inhibiting role of NiAl<sub>2</sub>O<sub>4</sub> spinel species observed in XRD and H<sub>2</sub>-TPR tests on catalytic gasification performance [102–104], and (b) the coke/carbon formation through the thermal and catalytic decomposition of carbonaceous intermediates and/or undesired gas phase side reactions. Indeed, since NiAl<sub>2</sub>O<sub>4</sub> cannot be easily reduced to Ni<sup>0</sup>, its formation probably lowers the amount of active Ni sites, thus leading to a reduced catalytic activity [102]. On the other hand, a superior gasification rate is observed for Ni/CeO<sub>2</sub> sample up to 800 °C, which can be related to the high catalytic activity of Ni/CeO<sub>2</sub> catalyst and its tolerance toward carbon formation. CeO<sub>2</sub>-based catalysts present a significant redox ability by releasing and up-taking oxygen through the reversible reaction,  $\text{CeO}_2 \leftrightarrow \text{CeO}_{2-x} + \text{O}_x$ , where O<sub>x</sub> stands for the lattice oxygen at CeO<sub>2</sub> [33,34]. This lattice oxygen possibly enhances the catalytic gasification performance via two different pathways. The first one is by the reaction of CO with CeO<sub>2</sub> lattice oxygen, resulting in CO<sub>2</sub> formation ( $\text{CO} + \text{O}_x \rightarrow \text{CO}_2 + \text{O}_{x-1}$ ). The second one is related to the oxidation of the remaining solid char/carbon which could be facilitated by CeO<sub>2</sub>. Indeed, as a supplier of lattice oxygen, CeO<sub>2</sub> may oxidize solid carbon ( $\text{C}_{(s)} + \text{O}_x \rightarrow \text{CO} + \text{O}_{x-1}$ ) towards additional CO formation. These induced effects are in line with the enhanced Ni/CeO<sub>2</sub> reducibility results (Figure 4, Table 2); the peak observed at 800 °C and attributed to the reduction of bulk CeO<sub>2</sub> species confirms the presence of lattice oxygen at such high temperatures, which can further oxidize the remaining carbon species [99].



**Figure 6.** Effect of temperature and catalyst addition on the conversion of carbon to CO during non-isothermal CO<sub>2</sub> gasification experiments. Gasifying agent flowrate = 30 cm<sup>3</sup>/min of 20 vol.% CO<sub>2</sub> in Helium.

**Table 3.** The main reaction network during biomass CO<sub>2</sub> gasification.

	Reaction	No
Tar thermal cracking	$\text{Tar (C}_m\text{H}_n) \rightarrow \text{Smaller Tar (C}_q\text{H}_q) + \text{H}_{2(g)}$	R1
Tar dry reforming	$\text{Tar (C}_m\text{H}_n) + m\text{CO}_{2(g)} \rightarrow 2m\text{CO}_{2(g)} + (n/2)\text{H}_{2(g)}$	R2
Tar dry reforming	$\text{Tar (C}_m\text{H}_n) + (m + n/2)\text{CO}_{2(g)} \rightarrow (2m + n/2)\text{CO}_{(g)} + (n/2)\text{H}_{2(g)}$	R3
Tar steam cracking	$\text{Tar (C}_m\text{H}_n) + m\text{H}_2\text{O}_{(g)} \rightarrow m\text{CO}_{(g)} + (m + n/2)\text{H}_{2(g)}$	R4
Tar steam cracking	$\text{Tar (C}_m\text{H}_n) + 2m\text{H}_2\text{O}_{(g)} \rightarrow m\text{CO}_{2(g)} + (2m + n/2)\text{H}_{2(g)}$	R5
Tar partial oxidation	$\text{Tar (C}_m\text{H}_n) + (n/2)\text{O}_{2(g)} \rightarrow m\text{CO}_{(g)} + (n/2)\text{H}_{2(g)}$	R6
Carbon-steam reforming	$\text{C}_{(s)} + \text{H}_2\text{O}_{(g)} \leftrightarrow \text{CO}_{(g)} + \text{H}_{2(g)}$	R7
Water gas shift	$\text{CO}_{(g)} + \text{H}_2\text{O}_{(g)} \leftrightarrow \text{CO}_{2(g)} + \text{H}_{2(g)}$	R8
Boudouard reaction	$\text{C}_{(s)} + \text{CO}_{2(g)} \leftrightarrow 2\text{CO}_{(g)}$	R9

In the case of the molten carbonate salt mixture (MS), the instant gasification rate approached its maximum value ( $8.3 \times 10^{-3} \text{ min}^{-1}$ ) at ca. 55 °C lower compared to non-catalytic CO<sub>2</sub> gasification experiments. Moreover, the Rco values obtained during MS-assisted gasification were significantly higher, compared to non-catalytic and Ni-assisted catalytic gasification, in the temperature range of 600–800 °C. This remarkable result is in agreement with relevant studies on the MS-assisted CO<sub>2</sub> gasification of various biomass fuels [28,71,81,86,105]. Obviously, MS favors CO production at lower gasification temperatures due to its ability to improve mass and heat transfer phenomena in conjunction with the catalytic role of contained alkali metals in the three-cyclic-step Boudouard reaction (Table 4) [65–67].

**Table 4.** Mechanism of the alkali carbonate-assisted carbon CO<sub>2</sub> gasification.

Reaction	No
$\text{M}_2\text{CO}_3 + 2\text{C} \rightarrow 2\text{M}^* + 3\text{CO}$	R11
$2\text{M}^* + \text{CO}_2 \rightarrow \text{M}_2\text{O} + \text{CO}$	R12
$\text{M}_2\text{O} + \text{CO}_2 \rightarrow \text{M}_2\text{CO}_3$	R13
$\text{C}_{(s)} + \text{CO}_{2(g)} \rightarrow 2\text{CO}_{(g)}$	R14

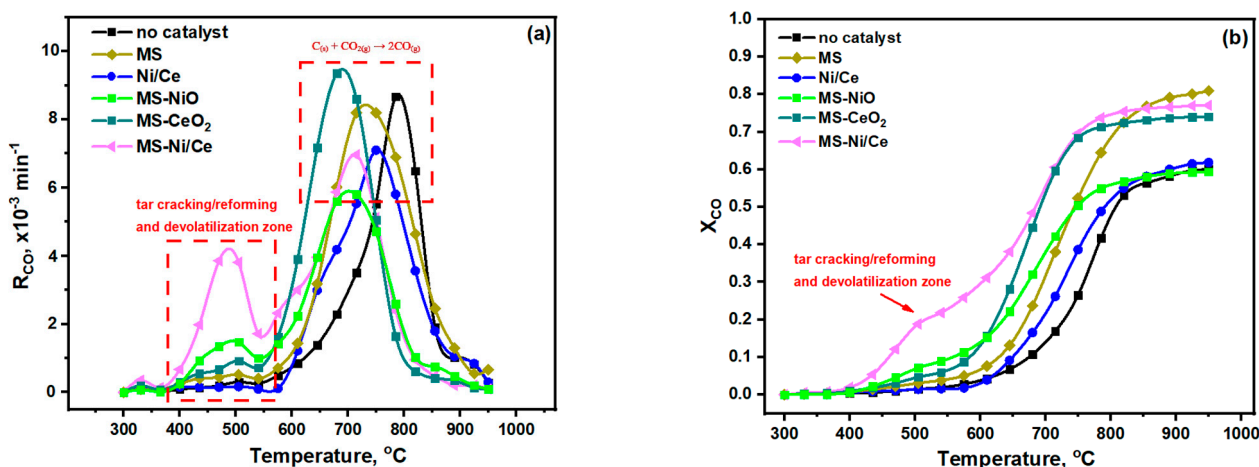
\* M stands for the alkali metal.

Notably, the CO production rate maxima for the combined MS-Ni/X (X: CeO<sub>2</sub>, Al<sub>2</sub>O<sub>3</sub>) medium was shifted to 15, 40, and 70 °C lower compared to MS and Ni catalysts and non-catalytic gasification tests, respectively. Most importantly, the mixed MS-Ni/CeO<sub>2</sub> and MS-Ni/Al<sub>2</sub>O<sub>3</sub> composites revealed an excellent synergy regarding their beneficial role in the devolatilization and tar cracking/reforming zones. Indeed, in the temperature range of 300 to 550 °C, the maximum Rco value for both MS-Ni systems was four times higher ( $4 \times 10^{-3} \text{ min}^{-1}$ , 460 °C) compared to their counterparts. This can be attributed to the combined catalytic effect of both Ni catalysts and MS on tar/volatiles' thermal and/or dry cracking/reforming reactions, as well as on the oxidation of the dissociated carbon on nickel active sites [44,45]. Interestingly, the additional CO formation at this temperature regime coincides with the melting point of the MS (Li<sub>2</sub>CO<sub>3</sub>-K<sub>2</sub>CO<sub>3</sub>) which is ca. 490 °C [65]. As the salt mixture melts, it forms a thin layer that favors the carbon-MS contact [68,70]. This in turn facilitates the tar oxidation reaction (R6) at the carbon-catalyst interface through the labile oxygen species in the low temperature region (see H<sub>2</sub>-TPR analysis above).

To further shed light on the CO<sub>2</sub> gasification performance, the carbon to CO conversion efficiency, Xco (Figure 6), was calculated via Equation 1. Notably, there are three distinct temperature regimes. At temperatures up to 600 °C, where tar and volatiles' cracking/reforming reactions prevail, the combined MS-Ni systems lead to a carbon to CO conversion of ca. 0.3, in complete contrast to the bare constituents (Ni catalysts or MS), which are almost inactive. This further verifies the synergy between the Ni-based catalysts and MS towards tar and volatile dry cracking/reforming reactions. At the temperature range between 600 and 800 °C, the CO production is mainly ascribed to the endothermic Boudouard reaction (R9). In this temperature regime, the Xco values for the MS-Ni systems are higher compared to their individual counterparts, highlighting the syner-

getic combination of the MS-induced mass/heat transfer phenomena and catalytic activity towards the Boudouard reaction (R9), along with the Ni ability to favor the C-C bond cleavage reaction into an additional CO formation. At 800 °C, the  $X_{CO}$  follows the order: MS-Ni/Ce  $\approx$  MS-Ni/Al (0.75) > MS (0.68) > Ni/Ce (0.51) > Ni/Al  $\approx$  no catalyst (ca. 0.45). At temperatures higher than 800 °C, the carbon to CO conversion for the combined MS-Ni samples reached a plateau ( $X_{CO} = 0.78$ ) due to fuel depletion above this temperature. The  $X_{CO}$  for the MS-assisted gasification tests reached the highest value (0.81 at 950 °C), highlighting the pronounced effect of MS at higher temperatures.

To further explore the synergetic role between NiO and CeO<sub>2</sub> in combination with molten carbonate salt (MS) in the low/intermediate tar cracking/reforming temperature regime, the effect of MS-NiO and MS-CeO<sub>2</sub> systems on the CO<sub>2</sub> gasification reaction rate and carbon to CO conversion was examined (Figure 7). It is evident that the presence of all the catalyst's components is necessary to achieve high gasification performance at temperatures below 700 °C. This coincides with the well-established hydrocarbon (tar) dissociation and dehydrogenation on Ni active sites, the enhanced CeO<sub>2</sub> redox properties in the low/intermediate temperature regime, and the key role of MS on the decomposition of volatiles during steam and/or dry reforming reactions [44,45].



**Figure 7.** Effect of temperature and catalyst components on the instant CO production rate,  $R_{CO}$  (a), and carbon to CO conversion (b) during non-isothermal CO<sub>2</sub> gasification experiments. Gasifying agent flowrate = 30 cm<sup>3</sup>/min of 20 vol.% CO<sub>2</sub> in Helium.

### 3. Materials and Methods

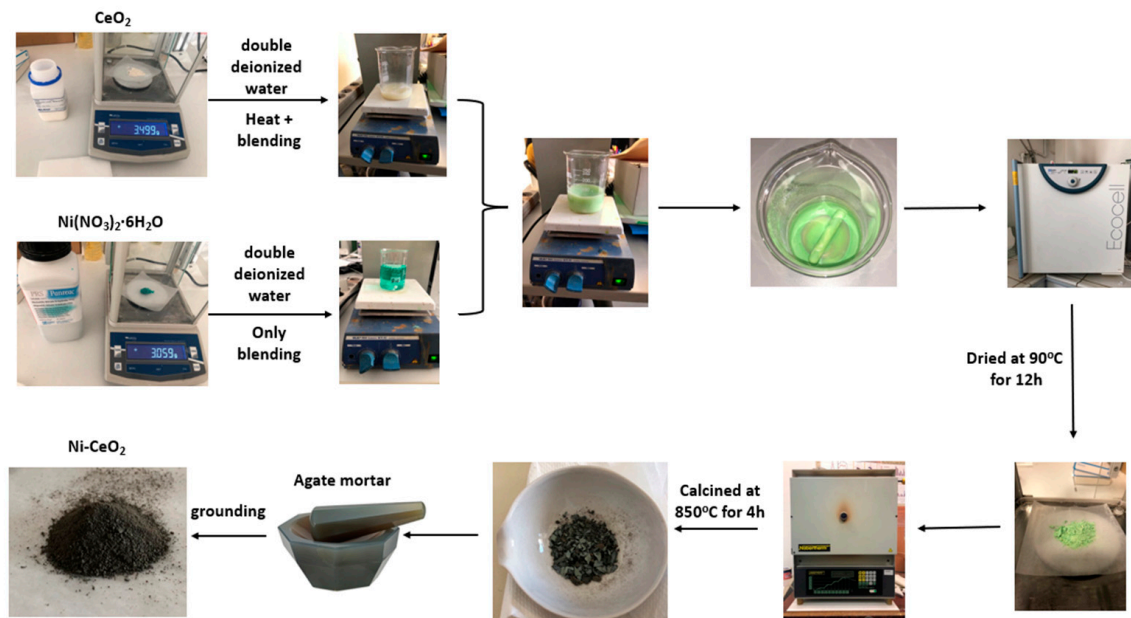
#### 3.1. Fuel Feedstock

Olive kernel (OK) from Cretan olive tree cultures was selected as raw fuel. OK was initially crushed to a particle size between 1–3 mm using a jaw crusher. Then, part of this fraction was milled to 100–200 µm using an agate mortar (Retsch RM200) producing a large amount (ca. 70 wt.%) of fines (<100 µm). The elemental and proximate analysis of olive kernel fuel has been presented in our previous work [31], following a typical pattern for lignocellulosic residual biomass with negligible nitrogen, sulfur, and chlorine contents. Moreover, the proximate analysis revealed the high volatile matter content (75.8 wt.%) and low ash concentration (2.9 wt.%) of olive kernel biomass.

#### 3.2. Catalyst Preparation

Ni-based catalysts were prepared using the wet impregnation method. Commercial aluminum oxide ( $\alpha$ -Al<sub>2</sub>O<sub>3</sub>, ~100 mesh, 99.9% purity, Aldrich) and cerium oxide (CeO<sub>2</sub>, 99.9% purity) were used as catalyst supports. In brief, Ni/Al<sub>2</sub>O<sub>3</sub> and Ni/CeO<sub>2</sub> catalysts were prepared by the aqueous impregnation of nickel nitrate precursor salt (Ni(NO<sub>3</sub>)<sub>2</sub>·6H<sub>2</sub>O) in commercial  $\alpha$ -Al<sub>2</sub>O<sub>3</sub> and CeO<sub>2</sub> by vigorously agitating at ca. 80 °C for about 3 h until a green slurry was obtained. The slurry was dried at 90 °C for 12 h and

then calcined in an air flow at 850 °C for 4 h. The nominal loading of Ni over Al<sub>2</sub>O<sub>3</sub> and CeO<sub>2</sub> was set at 15 wt.% based on relevant literature studies and reviews [33,39]. For sake of brevity, the Ni-based catalysts will be noted as Ni/Ce and Ni/Al, with the procedure followed to synthesize the former sample being illustrated in Figure 8.



**Figure 8.** Illustrated procedure for the synthesis of the 15 wt.% Ni/CeO<sub>2</sub> sample.

The molten salts used for preparing the eutectic carbonates mixture were Li<sub>2</sub>CO<sub>3</sub> and K<sub>2</sub>CO<sub>3</sub> (Sigma Aldrich, Munich, Germany) with a molar ratio of 62/38 mol.%, respectively. The salts were firstly rolled and milled at ca. 200 rpm for approximately 12 h. The melting point of the binary carbonates eutectic mixture (MS) is approximately 498 °C, thus it could be utilized as a mass and heat transfer medium for the gasification of solid fuels [65]. Then the Li<sub>2</sub>-K<sub>2</sub>/CO<sub>3</sub> mixture (MS) was placed on a hot plate at 60 °C so as to evaporate the liquid carrier (ethanol) used during the roll milling process [65]. Finally, the molten salts were cooled to room temperature, crushed, and finely ground in an agate mortar.

The combined Ni/M<sub>x</sub>O<sub>y</sub> (M: Al, Ce) and MS blends were prepared by homogeneously mixing the individual counterparts in an agate mortar.

### 3.3. Experimental Apparatus for the Olive Kernel Catalytic Gasification Studies

Figure 9 schematically illustrates the experimental setup for the olive kernel catalytic gasification tests, which were performed under a batch mode of operation. The experimental apparatus and conditions are described in detail in our previous work [31]. In brief, a mixture of fuel feedstock (0.1 g) and MS or MS-Ni catalyst was loaded into an Inox, U-tube, fixed bed reactor. The employed catalyst-to-biomass weight ratio was fixed at 0.5:1 for the MS-OK experiments, 2.5:1 for the Ni-aided gasification tests, and 0.5:2:1 for the ternary MS-Ni catalyst/OK mixtures. The mass ratio of the employed catalysts to OK was fixed at 2.5, while the MS to OK weight ratio was set at 0.5. The feedstock mixtures were prepared by physically mixing the olive kernel with the examined catalyst composites in an agate mortar. The flowrate of 20 vol.% CO<sub>2</sub>/He, used as gasifying agent mixture, was set at 30 cm<sup>3</sup>/min. After passing through a cooling trap (ice bath) to collect tars, the gaseous products were driven to a gas chromatograph (Shimadzu GC-14B) to monitor the effluent's gas composition in the temperature range of 300–950 °C, by increasing the temperature at a constant rate of 2 °C/min. In order to obtain reliable and accurate results, all gasification tests were repeated at least twice.



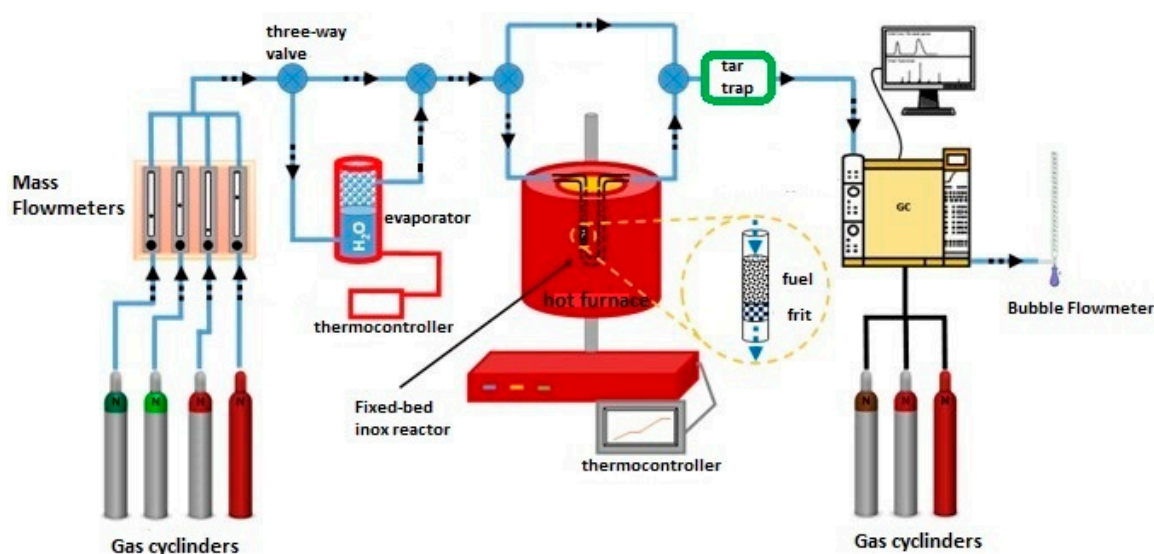


Figure 9. Experimental apparatus of the lab-scale CO<sub>2</sub>-gasification experiments.

Here, it should be noted that non-isothermal gasification studies provide a more reliable overview on the gasification performance in the whole operational range since the gasification temperature often varies along the gasifier in real applications. Moreover, lower heating rates result in more accurate studies since higher ones may lead to the formation of larger temperature gradients within the sample, leading to higher temperature differences inside the fuel bed [106].

### 3.4. Gasification Performance Indicators

In the case of the non-isothermal catalytic CO<sub>2</sub>-gasification experiments, since CO was practically the main product during gasification, the catalysts' activity was evaluated through the calculation of two performance parameters:  $X_{CO}$  expressing the carbon to CO conversion; and  $R_{CO}$  (min<sup>−1</sup>) standing for the instant CO production rate, as described in our previous work [107]:

$$X_{CO} = \frac{\sum_{t=0}^{t_{step1}} y_{CO,t} \times 12}{m \times w_c} + \frac{\sum_{t_{step1}}^{t_f} y_{CO,t} \times 12}{2 \times m \times w_c} \quad (1)$$

$$R_{CO} = \frac{dX_{CO}}{dt} \quad (2)$$

where  $y_{CO,t}$  corresponds to the cumulative CO production moles in time  $t$ ,  $m$  is the initial mass of fuel sample (gr), and  $w_c$  is the elemental carbon content of the olive kernel biomass fuel. It should be noted that the first term in Equation (1) stands for the CO production during the devolatilization stage, whereas the second term corresponds to the CO formation associated with the Boudouard reaction ( $C + CO_2 \rightarrow 2 CO$ ) during the gasification stage. The same expression has also been employed in relevant studies in the literature to estimate the CO<sub>2</sub> gasification conversion of various coal fuels [81,101].

### 3.5. Physicochemical Characterizations

X-ray diffraction patterns of powdered samples were obtained by a Bruker AXS D8 Advance copper anode diffractometer (CuK $\alpha$  radiation) equipped with a nickel foil monochromator, operating at 40 kV and 40 mA over the  $2\theta$  collection range of 10–80° at a scan rate of 0.05° s<sup>−1</sup>.

The d-spacing was calculated by applying the Bragg's law:

$$2d \sin\theta_B = n \lambda \quad (3)$$

where  $\lambda$  is the X-ray wavelength,  $d$  is the spacing of the diffraction planes, and  $\theta_B$  is the angle between the incident rays and the diffracting planes, otherwise known as the Bragg angle. For  $\text{CeO}_2$  and  $\text{NiO}$ , which are both crystallized in cubic form ( $a = b = c$ ,  $\alpha = \beta = \gamma = 90^\circ$ ), the lattice parameters can be calculated by the following equation:

$$1/d^2 = (h^2 + k^2 + l^2)/a^2 \quad (4)$$

The morphological analysis of the samples was performed by scanning electron microscopy (SEM, JEOL JSM-6390LV, JEOL Ltd., Akishima, Tokyo, Japan) operating at 20 keV. Elemental analysis/mapping and morphological observation were obtained by high-resolution scanning electron microscopy (HR-SEM) using a JS-IT700HR (JEOL, Tokyo, Japan) instrument at 20 kV. Transmission electron microscopy (TEM) was performed using a JEM-2100 instrument (JEOL, Tokyo, Japan) equipped with a LaB6 filament, working at 200 kV. Specimens for TEM were prepared by the deposition of dispersed powder samples after ultrasonication.

The reducibility of the Ni/Ce and Ni/Al catalysts was examined by temperature-programmed reduction with  $\text{H}_2$  (TPR- $\text{H}_2$ ). In a typical experiment, 0.1 g of the catalyst sample was loaded in a fixed-bed quartz reactor and pretreated at 500 °C for one hour under helium flow (50 mL/min). The catalyst was then cooled down to 35–40 °C, and TPR- $\text{H}_2$  analysis was carried out from 40 to 920 °C at a heating rate of 10 °C/min in a 5 v/v%  $\text{H}_2/\text{He}$  flow (50 mL/min). The composition of the exit gas was monitored online with a quadrupole mass analyzer (Omnistar, Balzer). The  $m/z$  fragments registered were as follows:  $\text{H}_2 = 2$ ,  $\text{H}_2\text{O} = 18$ , and  $\text{He} = 4$ . The quantitative analysis of the consumed/desorbed  $\text{H}_2$  was based on  $m/z = 2$ .

#### 4. Conclusions

The main objective of this work was to explore the impact of catalyst addition (Ni/ $\text{CeO}_2$ , Ni/ $\text{Al}_2\text{O}_3$ ) and/or carbonates (eutectic binary mixture of carbonate salts, MS) on the  $\text{CO}_2$  gasification of olive kernel biomass fuel. It was found that Ni/ $\text{CeO}_2$  and Ni/ $\text{Al}_2\text{O}_3$  catalysts demonstrated a beneficial role on  $\text{CO}_2$  gasification performance by slightly reducing the onset and peak  $\text{CO}_2$  gasification temperatures. Interestingly, the Ni/ $\text{CeO}_2$  catalyst presented an enhanced instant gasification reaction rate for temperatures up to 800 °C, in line with the significant redox capability of  $\text{CeO}_2$ . In the presence of MS, the instant gasification rate approached its maximum value ( $8.3 \times 10^{-3} \text{ min}^{-1}$ ) at ca. 55 °C lower compared to the non-catalytic gasification tests. The pronounced effect of MS at higher temperatures was also reflected in the high carbon to CO conversion value ( $X_{\text{CO}} = 0.81$  at 950 °C). More importantly, the combined use of MS with Ni catalysts notably enhances the  $\text{CO}_2$  gasification performance, specifically on the devolatilization and tar cracking/reforming zones. Indeed, in the temperature range of 300 to 550 °C, the maximum  $R_{\text{CO}}$  and  $X_{\text{CO}}$  values for both MS-Ni systems were notably higher ( $4 \times 10^{-3} \text{ min}^{-1}$  and 0.25 at 460 °C) compared to the insignificant corresponding performance ( $R_{\text{CO}} < 0.5 \times 10^{-3} \text{ min}^{-1}$ ) obtained by the individual catalyst counterparts. Collectively, the synergistic combination of molten salt and nickel-based catalysts can provide an innovative approach to enhance biomass  $\text{CO}_2$  gasification and, in parallel, improve syngas quality for downstream processes, substantially reducing syngas cleaning requirements and system costs.

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## Article

# Transition Metal ( $\text{Fe}_2\text{O}_3$ , $\text{Co}_3\text{O}_4$ and $\text{NiO}$ )-Promoted $\text{CuO}$ -Based $\alpha\text{-MnO}_2$ Nanowire Catalysts for Low-Temperature CO Oxidation

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**Abstract:** As a toxic pollutant, carbon monoxide (CO) usually causes harmful effects on human health. Therefore, the thermally catalytic oxidation of CO has received extensive attention in recent years. The  $\text{CuO}$ -based catalysts have been widely investigated due to their availability. In this study, a series of transition metal oxides ( $\text{Fe}_2\text{O}_3$ ,  $\text{Co}_3\text{O}_4$  and  $\text{NiO}$ ) promoted  $\text{CuO}$ -based catalysts supported on the  $\alpha\text{-MnO}_2$  nanowire catalysts were prepared by the deposition precipitation method for catalytic CO oxidation reactions. The effects of the loaded transition metal type, the loading amount, and the calcination temperature on the catalytic performances were systematically investigated. Further catalyst characterization showed that the  $\text{CuO}/\alpha\text{-MnO}_2$  catalyst modified with 3 wt%  $\text{Co}_3\text{O}_4$  and calcined at 400 °C performed the highest CO catalytic activity ( $T_{90} = 75$  °C) among the investigated catalysts. It was supposed that the loading of the  $\text{Co}_3\text{O}_4$  dopant not only increased the content of oxygen vacancies in the catalyst but also increased the specific surface area and pore volume of the  $\text{CuO}/\alpha\text{-MnO}_2$  nanowire catalyst, which would further enhance the catalytic activity. The  $\text{CuO}/\alpha\text{-MnO}_2$  catalyst modified with 3 wt%  $\text{NiO}$  and calcined at 400 °C exhibited the highest surface adsorbed oxygen content and the best normalized reaction rate, but the specific surface area limited its activity. Therefore, the appropriate loading of the  $\text{Co}_3\text{O}_4$  modifier could greatly enhance the activity of  $\text{CuO}/\alpha\text{-MnO}_2$ . This research could provide a reference method for constructing efficient low-temperature CO oxidation catalysts.

**Keywords:** transition metal oxides;  $\text{CuO}$ -based catalysts;  $\text{Co}_3\text{O}_4$  modification;  $\alpha\text{-MnO}_2$  nanowire; catalytic oxidation of CO

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## 1. Introduction

As a toxic pollutant in the atmosphere, carbon monoxide (CO) has widely received public attention in recent years [1]. CO is not only mainly produced during the incomplete combustion of fossil fuels and motor vehicle emissions [2], but it is also a precursor of the ozone pollution [3], which can be harmful even at low concentrations. In recent years, scientists around the world have employed different methods for the removal of CO, such as photocatalysis [4], thermocatalysis oxidation [5], etc. Thermocatalysis oxidation is the most commonly used method for the oxidation of CO. The noble metal-based catalysts (such as Au [6,7], Pt [8–10], Pd [11], Ru [12,13], Rh [14] and Ag [15]), transition metal oxide based catalysts (such as  $\text{MnO}_2$  [16],  $\text{CeO}_2$  [17],  $\text{ZrO}_2$  [18],  $\text{Co}_3\text{O}_4$  [16]), and metal



hybrid catalysts (such as  $\text{MnCo}_2\text{O}_4$  spinel [19], Ce-Zr solid solution [20]) can be used for the thermocatalytic oxidation of CO at low temperatures without generating the secondary contaminants [16]. Transition metal-based catalysts have good potential for application due to their low cost, high stability, and good activity [21,22]. Among the transition metal oxides, manganese dioxide ( $\text{MnO}_2$ ) has many advantages, such as a low price, being environmentally friendly, and abundance in nature [2,23]. As is well known,  $\text{MnO}_2$  usually exists in different crystalline phases with different structures, such as the  $\alpha$ -,  $\beta$ -, and  $\gamma$ -types of the one-dimensional pore structure, the  $\delta$ -type of the two-dimensional pore structure, and the  $\lambda$ -type of the three-dimensional network structure [24], which greatly depend on the different connectivity (corner-edge sharing) exhibited by the  $[\text{MnO}_6]$  octahedra [25–28]. Liang et al. [28] prepared  $\text{MnO}_2$  nanorods with four different crystalline phases for the oxidation of CO. It was found that the order of oxidation activity of different crystalline phases with the same nanorod morphology was greatly different, in decreasing order from  $\alpha$ -  $\approx$   $\delta$ -  $>$   $\gamma$ -  $>$   $\beta$ - $\text{MnO}_2$  (The temperature at which the conversion of CO on  $\alpha$ - $\text{MnO}_2$  reached 100% was approximately 130 °C). This indicated that the oxidation activity of CO significantly depended on the phase structure and channel structure of the  $\text{MnO}_2$ . Tian et al. [29] investigated the effects of the crystalline phases of  $\text{MnO}_2$  ( $\alpha$ -,  $\beta$ -, and  $\varepsilon$ - $\text{MnO}_2$ ) on the performances of the oxidation of CO and toluene. It was found that the  $\beta$ - $\text{MnO}_2$  performed the highest activity for CO oxidation ( $T_{90} = 75$  °C) among the three crystalline phases of  $\text{MnO}_2$ , and the  $\alpha$ - $\text{MnO}_2$  behaved with the lowest activity for CO oxidation ( $T_{90} = 118$  °C). The content of oxygen vacancy in the catalyst was also determined by in situ EPR spectra and the results showed that the catalytic activity of the catalyst was proportional to the concentration of oxygen vacancies, which were regarded as the active sites for the adsorption and dissociation of oxygen molecules. It was believed that the catalytic activity of  $\text{MnO}_2$  was greatly related to the oxygen vacancy activity [29]. As is well known, the  $\alpha$ - $\text{MnO}_2$  is provided with the 1D ( $1 \times 1$ ) ( $2 \times 2$ ) tunnel structures, which are attributed to the tetragonal crystal system [30].

CuO has been widely used as the active site of the low-temperature catalytic oxidation of CO due to its excellent activity and abundant availability [31]. For example, Raziye Jökar et al. [31] used CuO/ $\alpha$ - $\text{MnO}_2$  as the catalyst of the preferential oxidation of CO in the hydrogen-rich gas stream and investigated the interaction between the  $\text{MnO}_2$  and CuO ( $T_{97} = 130$  °C), the superior activity of the catalyst due to the beneficial synergistic interaction between CuO and  $\alpha$ - $\text{MnO}_2$ . Meanwhile, the catalytic activity was also influenced by several factors, such as specific surface area, crystallinity, oxygen vacancies, and redox properties. Qian et al. [32] prepared a series of CuO/ $\text{MnO}_2$  catalysts with different CuO loading amounts by the incipient wetness impregnation method for the oxidation of CO. The catalyst activity was almost the same for the CuO loadings, from 1% to 40%. Sun et al. [33] prepared a CuO/ $\text{Cu}_{1.5}\text{Mn}_{1.5}\text{O}_4$  spinel-type composite oxide for synergistic catalysis of CO oxidation. It was found that the synergistic effect between  $\text{Cu}_{1.5}\text{Mn}_{1.5}\text{O}_4$  spinel and CuO can promote the oxidation of CO, and CuO- $\text{Cu}_{1.5}\text{Mn}_{1.5}\text{O}_4$  had the best oxidation activity for CO ( $T_{100} = 177$  °C).

Nowadays, for the modification of transition metal oxide-based catalysts, in addition to the carrier and active site, the promoter also plays an active role in the improvement of catalytic performance [34]. Gao et al. [35] doped transition metals (Fe, Co, Ni, and Cu) with a 1:10 molar ratio on  $\alpha$ - $\text{MnO}_2$  nanowires by a one-step hydrothermal method to oxidize CO. Among the four transition metals,  $\text{Cu}_{0.1}\text{MnO}_x$  had the best oxidation activity for CO ( $T_{100} \sim 120$  °C). Krasimir et al. [36] investigated the effects of different molar ratios of chemical compositions on the  $\gamma$ - $\text{Al}_2\text{O}_3$ -supported CuO/ $\text{MnO}_2$ / $\text{Cr}_2\text{O}_3$  catalysts for the oxidation of CO, dimethyl ether (DME), and methanol. The results showed that the Cu-Mn-Cr/ $\gamma$ - $\text{Al}_2\text{O}_3$  catalyst, which Cu/(Mn + Cr) has a molar ratio of 2:1 and a Mn/Cr molar ratio of 0.25, can achieve the complete oxidation of CO at 200 °C.

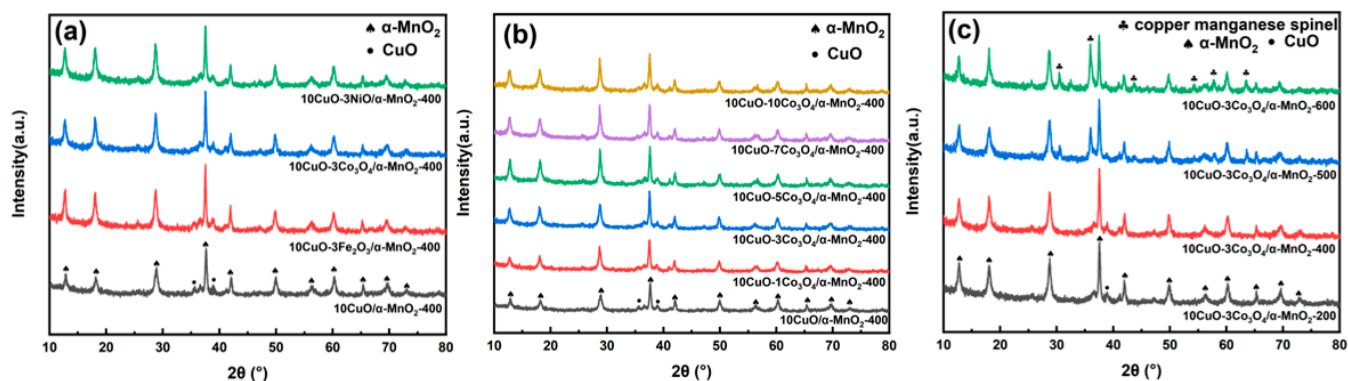
In order to further investigate the contribution of promoters to the catalytic performance of CuO/ $\text{MnO}_2$  catalysts in the oxidation of CO, in this work, the  $\alpha$ - $\text{MnO}_2$  nanowire was successfully prepared by the hydrothermal method and used as the support for the

CuO-based catalysts. A series of the transition metal oxides ( $\text{Fe}_2\text{O}_3$ ,  $\text{Co}_3\text{O}_4$ , and  $\text{NiO}$ ) promoted CuO-based  $\alpha\text{-MnO}_2$  nanowire catalysts were prepared by the deposition precipitation method. The effects of the type, the loading amount, and the calcination temperature of three transition metal oxides on the performance of the catalytic oxidation of CO were systematically studied. The obtained catalysts were carefully characterized by X-ray diffraction (XRD), scanning electron microscopy (SEM), nitrogen physisorption, X-ray photoelectron spectroscopy (XPS), and  $\text{H}_2$  temperature-programmed reduction ( $\text{H}_2$ -TPR). These catalysts were evaluated for their catalytic performances in the oxidation of CO. The results show that the  $\text{Co}_3\text{O}_4$  (3 wt.%) promoted 10 wt.% CuO/ $\alpha\text{-MnO}_2$  catalyst calcined at  $400^\circ\text{C}$  performed the greatest CO reactivity ( $T_{90} = 75^\circ\text{C}$ ).

## 2. Results and Discussion

### 2.1. XRD Analysis

The crystalline phase structures of the catalysts were obtained using X-ray diffraction (XRD) analysis. The results of XRD are shown in the Figure 1. Figure 1a shows the XRD patterns of the transition metal oxide ( $\text{MOx} = \text{Fe}_2\text{O}_3$ ,  $\text{Co}_3\text{O}_4$ ,  $\text{NiO}$ ) doped catalysts and the pristine 10CuO/ $\alpha\text{-MnO}_2$ -400 catalyst. It can be observed in Figure 1a that all the catalysts show wide and clear diffraction peaks at  $2\theta = 12.78^\circ$ ,  $18.11^\circ$ ,  $25.71^\circ$ ,  $37.52^\circ$ ,  $41.97^\circ$ ,  $49.86^\circ$ ,  $56.37^\circ$ ,  $65.11^\circ$ , and  $69.71^\circ$ , which could be conformed to the characteristic peaks of the  $\alpha\text{-MnO}_2$  (PDF#44-0141). It could be observed that the intensity of the diffraction peaks of  $\text{MnO}_2$  increased after the loading of the second transition metal oxides, especially over the 10CuO-3 $\text{Co}_3\text{O}_4$ / $\alpha\text{-MnO}_2$  catalyst. This phenomenon suggests that the crystallinity of the catalysts increased after loading the transition metal oxides, especially for the catalyst loading  $\text{Co}_3\text{O}_4$ . Meanwhile, two weak diffraction peaks could be detected at  $2\theta = 35.5^\circ$  and  $38.8^\circ$ , which corresponded to the characteristic peaks of CuO, according to the standard card of PDF#05-0661. The diffraction peak intensity of CuO became weaker after the addition of the transition metal to the catalyst, indicating that the addition of the transition metal promoted the dispersion of CuO.



**Figure 1.** Powder XRD patterns of the (a) 10CuO-3MOx/ $\alpha\text{-MnO}_2$ -400 catalysts doped with different transition metals ( $\text{MOx} = \text{Fe}_2\text{O}_3$ ,  $\text{Co}_3\text{O}_4$ ,  $\text{NiO}$ ); (b) 10CuO- $y\text{Co}_3\text{O}_4$ / $\alpha\text{-MnO}_2$ -400 catalysts doped with different contents of  $\text{Co}_3\text{O}_4$  ( $y = 1, 3, 5, 7, 10$ ); (c) 10CuO-3 $\text{Co}_3\text{O}_4$ / $\alpha\text{-MnO}_2$ -T catalysts calcined at different temperatures ( $T = 200, 400, 500, 600^\circ\text{C}$ ).

The XRD patterns of the 10CuO- $y\text{Co}_3\text{O}_4$ / $\alpha\text{-MnO}_2$ -400 catalysts with different contents of  $\text{Co}_3\text{O}_4$  are shown in the Figure 1b. It can be observed that the diffraction peaks of CuO are very clear over the pristine 10CuO/ $\alpha\text{-MnO}_2$ -400 catalyst without  $\text{Co}_3\text{O}_4$  loading. However, it can be observed that the diffraction peaks of CuO became blurry after loading  $\text{Co}_3\text{O}_4$  from 1 wt.% to 10 wt.%. The possible reason accounting for this phenomenon was that the appropriate loading amount of  $\text{Co}_3\text{O}_4$  could greatly enhance the dispersion of CuO on the surface of  $\alpha\text{-MnO}_2$  nanowire catalyst. Nevertheless, the characteristic peaks of  $\text{Co}_3\text{O}_4$  could be not observed in the catalysts due to the good dispersion of  $\text{Co}_3\text{O}_4$ .

The XRD patterns of 10CuO-3Co<sub>3</sub>O<sub>4</sub>/α-MnO<sub>2</sub> catalysts calcined at different temperatures are shown in the Figure 1c. It can be recognized that the intensity of the diffraction peaks of α-MnO<sub>2</sub> became weak at high calcination temperatures. The reason might be due to the formation of a copper manganese spinel (JCPDS No.70-0260) [37]. Only a diffraction peak of CuO was observed at 38.8°. Meanwhile, the intensity of the diffraction peaks of CuO became sharp with the increase of the calcination temperature (only from 200 °C to 400 °C). This indicated that the dispersion of CuO on the catalyst surface gradually deteriorated and the crystal size of CuO nanoparticles grew due to the finite surface area of the MnO<sub>2</sub> nanowire from 200 °C to 400 °C. As the calcination temperature rose from 400 °C to 600 °C, the diffraction peak strength of copper manganese spinel increased. The diffraction peak strength of CuO decreased, indicating that the dispersion of CuO increased.

## 2.2. SEM Observation

The morphologies of the 10CuO-3MO<sub>x</sub>/α-MnO<sub>2</sub>-400 catalysts loaded with different transition metal oxides (MO<sub>x</sub> = Fe<sub>2</sub>O<sub>3</sub>, Co<sub>3</sub>O<sub>4</sub>, NiO) and the pristine 10CuO/α-MnO<sub>2</sub>-400 catalyst were characterized by SEM (Figure 2). It can be observed that the morphology of the α-MnO<sub>2</sub> nanowire support greatly changed after loading the CuO active sites and the transition metal oxides. Specifically, the length to diameter ratio of the α-MnO<sub>2</sub> nanowire significantly decreased compared to the pristine α-MnO<sub>2</sub> nanowire. This was caused by the high loading contents of the CuO and transition metal oxides. In addition, the α-MnO<sub>2</sub> nanowire support might experience thermal sintering and self-assemble at high calcination temperatures. The spatial distribution of the elements over the one-dimensional 10CuO-3MO<sub>x</sub>/α-MnO<sub>2</sub>-400 (MO<sub>x</sub> = Fe<sub>2</sub>O<sub>3</sub>, Co<sub>3</sub>O<sub>4</sub>, NiO) nanowire catalyst was studied by energy dispersive X-ray spectroscopy mapping (EDS-mapping). As shown in Figure 2, the Cu and the doped Fe/Co/Ni elements were homogeneously distributed over these investigated catalysts. This indicated that the great dispersion of the CuO and the doped transition metal oxides on the surface of the α-MnO<sub>2</sub> nanowire supports could be easily achieved by the precipitation deposition method.

## 2.3. BET Analysis

In order to further investigate the structural properties of the catalysts, the specific surface areas, pore volumes, and pore size distributions of the catalysts were measured by nitrogen physisorption measurements. As shown in Figure 3a, all catalysts show IV isotherms with H3-shaped hysteresis loops. These results prove the presence of mesopores with a narrow slit-shape in the catalyst [38]. It is also interesting to find that the 10CuO-3MO<sub>x</sub>/α-MnO<sub>2</sub> catalysts still possess the similar mesoporous structure to the 10CuO/α-MnO<sub>2</sub> nanowire catalysts after loading different transition metal oxides. This demonstrates that the 10CuO/α-MnO<sub>2</sub> nanowire catalyst was provided with good thermal stability. The pore size distribution curves of the corresponding catalysts are shown in Figure 3b. The pore diameter of the catalysts is in the range of 2–15 nm after loading with transition metals. Moreover, the specific parameters of the structural properties of these catalysts are shown in Table 1. It can be observed that the specific surface areas of both the 10CuO-3Fe<sub>2</sub>O<sub>3</sub>/α-MnO<sub>2</sub> and 10CuO-3NiO/α-MnO<sub>2</sub> catalysts decreased after the loading of transition metals. On the contrary, the specific surface area of the 10CuO-3Co<sub>3</sub>O<sub>4</sub>/α-MnO<sub>2</sub> catalysts increased substantially. This indicates that the Co<sub>3</sub>O<sub>4</sub> on the α-MnO<sub>2</sub> nanowire support surface was highly dispersed. Meanwhile, the average pore sizes of all the 10CuO-3MO<sub>x</sub>/α-MnO<sub>2</sub> (MO<sub>x</sub> = Fe<sub>2</sub>O<sub>3</sub>, Co<sub>3</sub>O<sub>4</sub>, NiO) catalysts are very similar to the pristine 10CuO/α-MnO<sub>2</sub> nanowire. Specifically, the 10CuO-3Fe<sub>2</sub>O<sub>3</sub>/α-MnO<sub>2</sub> catalyst has a similar pore size distribution as the 10CuO/α-MnO<sub>2</sub> catalyst. This indicates that their mesoporous structures are not sharply impaired by the loaded metal oxides. In addition, the pore capacities of all 10CuO-3MO<sub>x</sub>/α-MnO<sub>2</sub> (MO<sub>x</sub> = Fe<sub>2</sub>O<sub>3</sub>, Co<sub>3</sub>O<sub>4</sub>, NiO) catalysts are enhanced compared to the pristine 10CuO/α-MnO<sub>2</sub>. As for the 10CuO-3Co<sub>3</sub>O<sub>4</sub>/α-MnO<sub>2</sub> catalyst, its surface area was twice as large as the pristine 10CuO/α-MnO<sub>2</sub> catalyst. The higher specific surface area is beneficial for the catalyst to expose more active sites, and the larger pore

volume helps the reactant accelerate the reactant mass diffusion and has a better adsorption ability to the reactant [39].

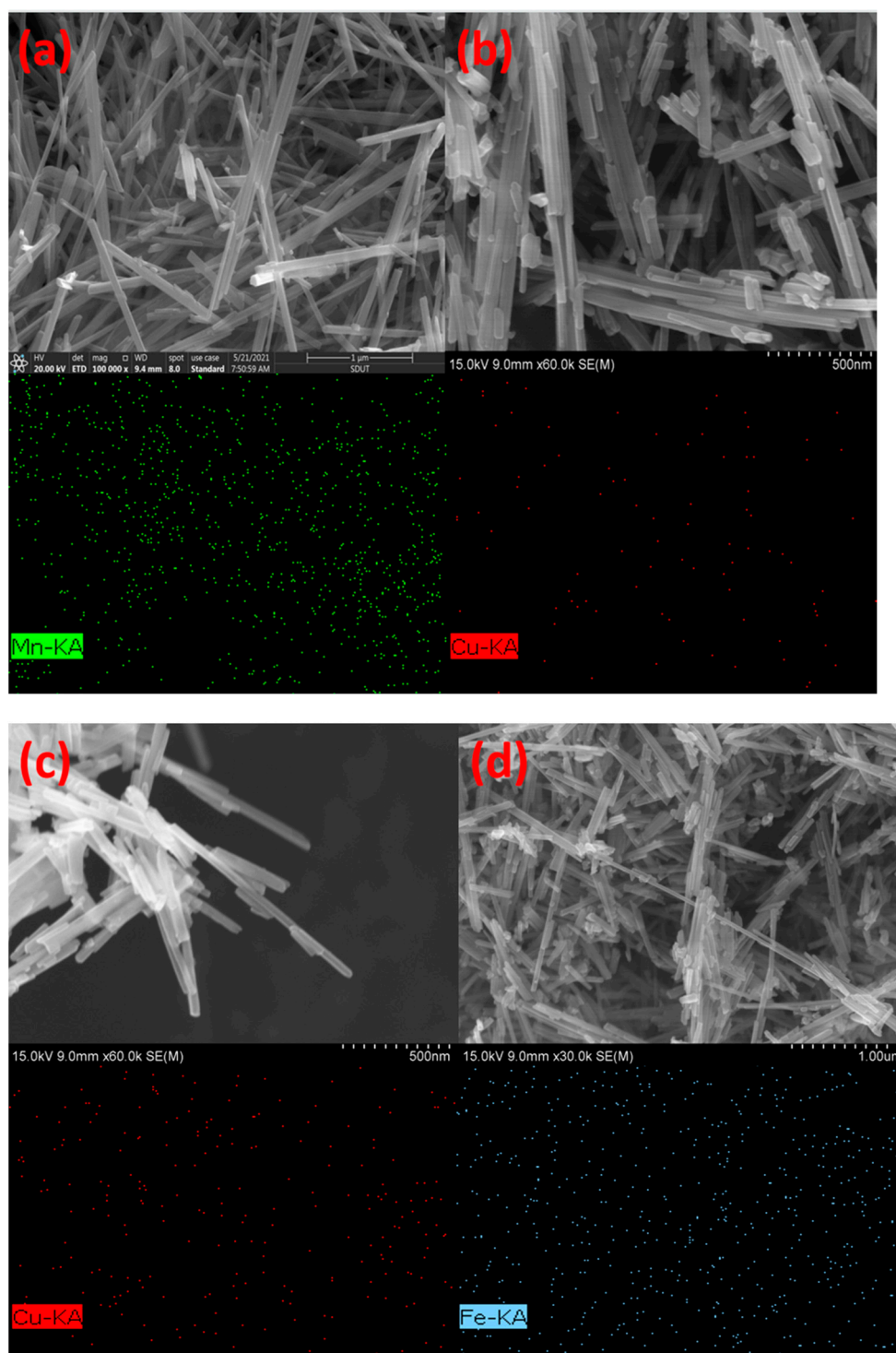
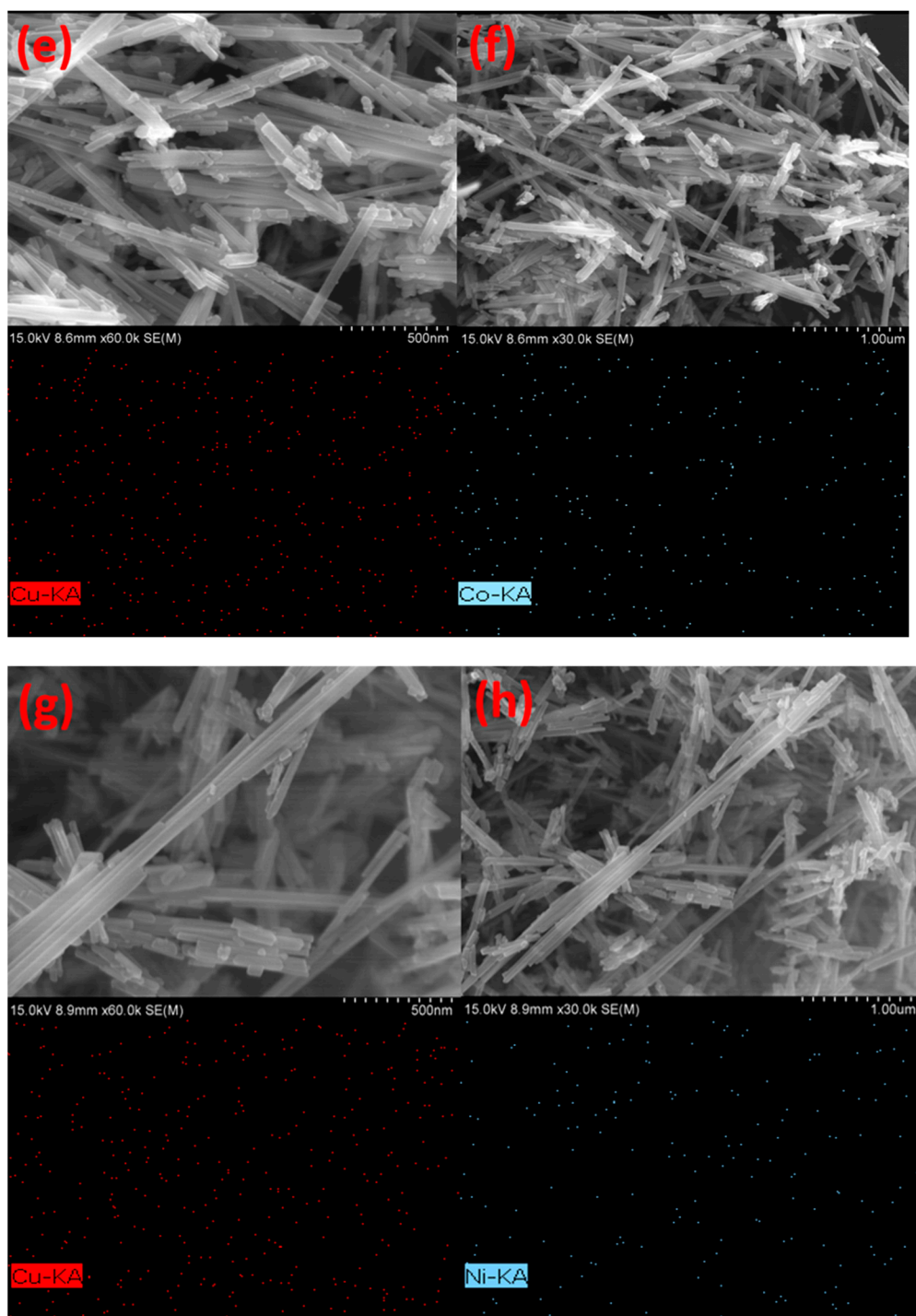
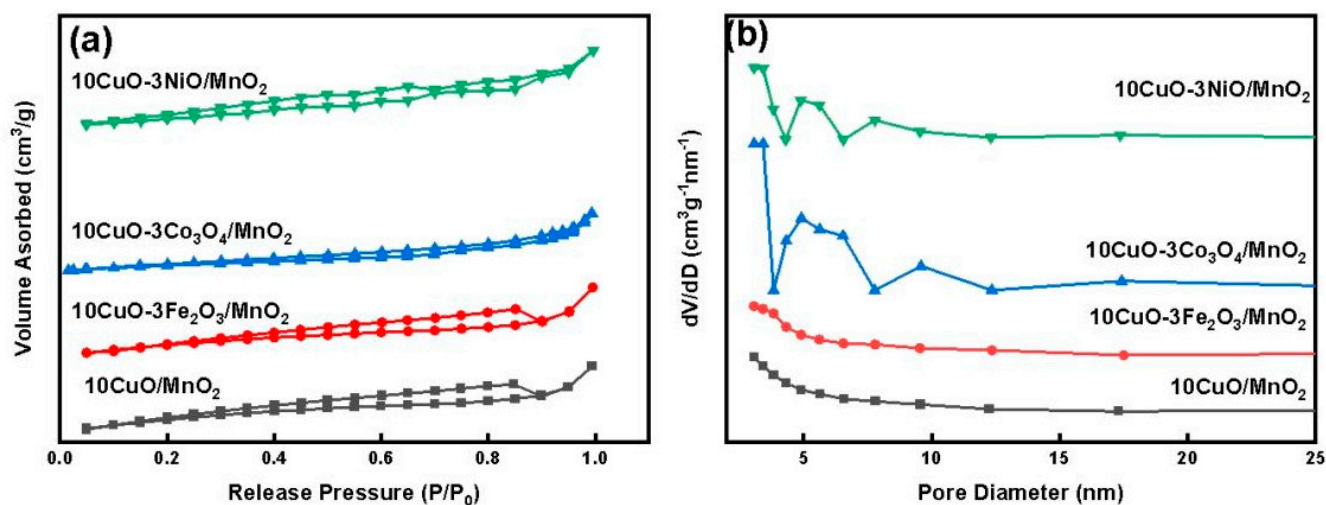


Figure 2. Cont.



**Figure 2.** SEM-EDS images of the (a) α-MnO<sub>2</sub> nanowire, (b) 10CuO/α-MnO<sub>2</sub>-400, (c,d) 10CuO-3Fe<sub>2</sub>O<sub>3</sub>/α-MnO<sub>2</sub>-400, (e,f) 10CuO-3Co<sub>3</sub>O<sub>4</sub>/α-MnO<sub>2</sub>-400, and (g,h) 10CuO-3NiO/α-MnO<sub>2</sub>-400.





**Figure 3.** (a) Nitrogen adsorption-desorption isotherms and (b) BJH pore size distribution of the 10CuO/ $\alpha$ -MnO<sub>2</sub>-400 and 10CuO-3MOx/ $\alpha$ -MnO<sub>2</sub>-400 (MOx = Fe<sub>2</sub>O<sub>3</sub>, Co<sub>3</sub>O<sub>4</sub>, NiO) catalysts.

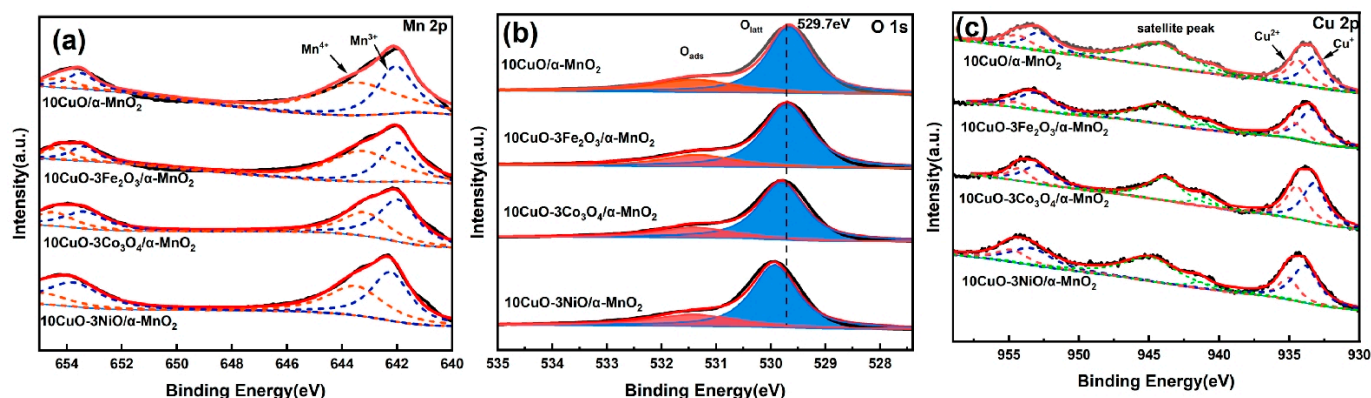
**Table 1.** Structural properties of the 10CuO/ $\alpha$ -MnO<sub>2</sub>-400 and 10CuO-3MOx/ $\alpha$ -MnO<sub>2</sub>-400 (MOx = Fe<sub>2</sub>O<sub>3</sub>, Co<sub>3</sub>O<sub>4</sub>, NiO) catalysts.

Catalyst	Specific Surface Area (m <sup>2</sup> /g)	Pore Volume (cm <sup>3</sup> /g)	Average Pore Diameter (nm)	Isotherm Type
10CuO/MnO <sub>2</sub>	72	0.09	3.1	IV H3
10CuO-3Fe <sub>2</sub> O <sub>3</sub> /MnO <sub>2</sub>	64	0.10	3.1	IV H3
10CuO-3Co <sub>3</sub> O <sub>4</sub> /MnO <sub>2</sub>	84	0.18	3.1	IV H3
10CuO-3NiO/MnO <sub>2</sub>	52	0.10	3.1	IV H3

#### 2.4. XPS Analysis

The coordination, composition, and valence state of the elements over the catalyst surface were investigated by X-ray photoelectron spectroscopy (XPS). The XPS of Mn 2p, O 1s, and Cu 2p of the 10CuO/ $\alpha$ -MnO<sub>2</sub>-400 and the 10CuO-3MOx/ $\alpha$ -MnO<sub>2</sub>-400 (MOx = Fe<sub>2</sub>O<sub>3</sub>, Co<sub>3</sub>O<sub>4</sub>, NiO) are shown in Figure 4. It can be observed in Figure 4a that 10CuO/ $\alpha$ -MnO<sub>2</sub>-400 had two main peaks around 654.0 eV and 642.0 eV, which could be attributed to the binding energies of the Mn 2p<sub>1/2</sub> at BE = 654.0 eV and Mn 2p<sub>3/2</sub> at BE = 642.0 eV, respectively. The two main peaks were divided into four peaks after the peak fitting. The fitted peaks of Mn 2p<sub>3/2</sub> at 642.0 eV and 643.5 eV indicate the existence of Mn<sup>3+</sup> and Mn<sup>4+</sup> in the 10CuO-3MOx/ $\alpha$ -MnO<sub>2</sub>-400 catalyst [40–44]. The ratios of the Mn<sup>3+</sup>/(Mn<sup>3+</sup> + Mn<sup>4+</sup>) over different catalysts followed the below order: 10CuO-3Co<sub>3</sub>O<sub>4</sub>/ $\alpha$ -MnO<sub>2</sub> (0.606) > 10CuO-3NiO/ $\alpha$ -MnO<sub>2</sub> (0.541) > 10CuO/ $\alpha$ -MnO<sub>2</sub> (0.414) > 10CuO-3Fe<sub>2</sub>O<sub>3</sub>/ $\alpha$ -MnO<sub>2</sub> (0.406). The redox electron pair in Cu-Mn oxide was the -Cu<sup>2+</sup>-O<sup>2-</sup>-Mn<sup>4+</sup>-→-Cu<sup>+</sup>-□-Mn<sup>3+</sup>- + 1/2O<sub>2</sub> (□ indicates the oxygen vacancy) [45]. The content of Mn<sup>3+</sup> and oxygen vacancies are proportional, or indirectly proportional, to the oxidation capacity of the catalyst [25,29,46,47]. The Mn<sup>3+</sup> may cause the Jahn-Teller effect, which could prolong the Mn-O bond in [MnO<sub>6</sub>] [48,49], thereby prolonging the distance between the oxygen pairs and causing the stretching of the Mn-O bond length [48]. As a result, the Mn-O bond was easier to break, and the mobility of oxygen became higher. Therefore, the released surface oxygen atoms are more likely to participate in the reaction and thus promote the catalytic performance. The XPS of O 1s of 10CuO-3MOx/ $\alpha$ -MnO<sub>2</sub>-400 was measured to elucidate the nature of the oxygen species over the 10CuO-3MOx/ $\alpha$ -MnO<sub>2</sub>-400 catalysts. As shown in Figure 4b, all the samples show double peaks of different oxygen species. Specifically, the BEs at around 529.8 eV and 531.4 eV could be ascribable to the surface lattice oxygen (O<sub>latt</sub>) and surface adsorbed oxygen (O<sub>ads</sub>) species [50,51], respectively. The ratios of the

$O_{ads}/O_{latt}$  are also summarized in Table 2. It can be observed that the binding energy of surface lattice oxygen ( $O_{latt}$ ) shifted to a higher binding energy with the addition of transition metals. The surface oxidation states of the Cu species were also investigated to show the redox properties of the as-prepared catalysts. As shown in Figure 4c, all the catalysts displayed two main peaks of Cu  $2p_{1/2}$  (953.6 eV) and Cu  $2p_{3/2}$  (933.7 eV) [43]. The Cu  $2p_{3/2}$  orbitals with binding energy in the range of 930.0–935.0 eV, could be divided into two peaks. Specifically, the binding energy peak at 933.4 eV was attributed to  $Cu^+$ , and the peak at 934.4 eV was attributed to  $Cu^{2+}$  [43]. Furthermore, it is worth noting that the Cu  $2p_{3/2}$  peak is accompanied by the vibrating satellite peaks in the range of 940.0–944.0 eV [52]. Combined with the results of the Mn 2p spectrum, the catalysts formed redox pairs of  $Cu^+/Cu^{2+}$  and  $Mn^{3+}/Mn^{4+}$ , which would promote the charge transference to generate more oxygen defects [37,53].



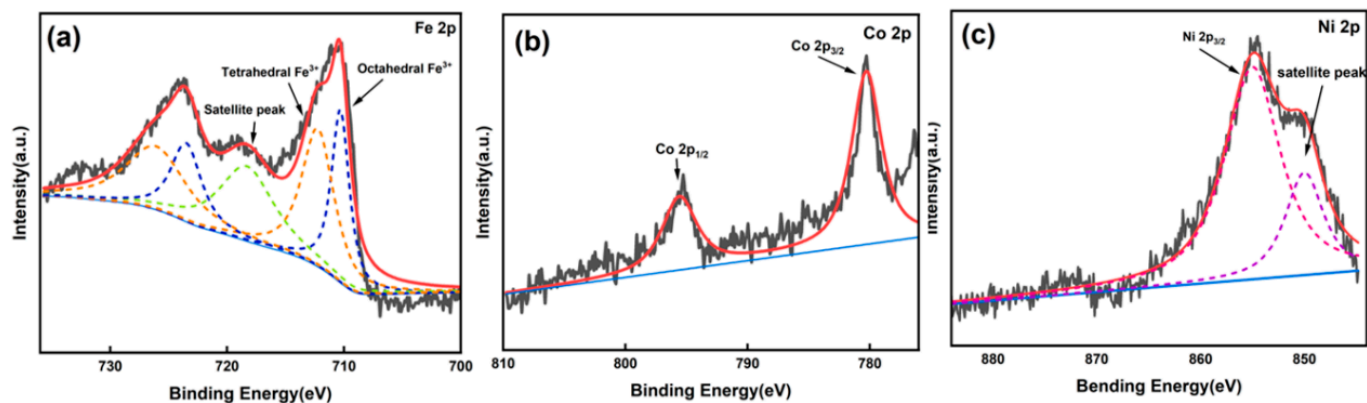
**Figure 4.** (a) Mn 2p spectra, (b) O 1s spectra, and (c) Cu 2p spectra of the 10CuO/ $\alpha$ -MnO<sub>2</sub>, 10CuO-3Fe<sub>2</sub>O<sub>3</sub>/ $\alpha$ -MnO<sub>2</sub>, 10CuO-3Co<sub>3</sub>O<sub>4</sub>/ $\alpha$ -MnO<sub>2</sub>, and 10CuO-3NiO/ $\alpha$ -MnO<sub>2</sub> (T = 400 °C) catalysts.

**Table 2.** The ratio of  $Mn^{3+}/(Mn^{3+} + Mn^{4+})$ ,  $O_{ads}/O_{latt}$ , and  $Cu^+/(Cu^{2+} + Cu^+)$  of the 10CuO-3MOx/ $\alpha$ -MnO<sub>2</sub> (MOx = Fe<sub>2</sub>O<sub>3</sub>, Co<sub>3</sub>O<sub>4</sub>, NiO) and the 10CuO/ $\alpha$ -MnO<sub>2</sub> catalyst.

Sample	$Mn^{3+}/(Mn^{3+} + Mn^{4+})$	$O_{ads}/O_{latt}$	$Cu^+/(Cu^{2+} + Cu^+)$
10CuO/ $\alpha$ -MnO <sub>2</sub>	0.414	0.324	0.551
10CuO-3Fe <sub>2</sub> O <sub>3</sub> / $\alpha$ -MnO <sub>2</sub>	0.406	0.283	0.644
10CuO-3Co <sub>3</sub> O <sub>4</sub> / $\alpha$ -MnO <sub>2</sub>	0.606	0.300	0.563
10CuO-3NiO/ $\alpha$ -MnO <sub>2</sub>	0.541	0.352	0.688

To determine the valence state of the transition metals loaded on the catalyst, the XPS spectra of Fe 2p, Co 2p, and Ni 2p are determined. The XPS profile of Fe 2p over the 10CuO-3Fe<sub>2</sub>O<sub>3</sub>/ $\alpha$ -MnO<sub>2</sub>-400 catalyst is shown in Figure 5a. The binding energies at 710.4 eV and 725.1 eV are ascribed to Fe  $2p_{3/2}$  and Fe  $2p_{1/2}$ , respectively [54,55]. The peak of Fe  $2p_{3/2}$  can be divided into two peaks (710.3 eV and 712.5 eV) [56]. In addition, a satellite peak was observed at about 718.3 eV. This indicates that the iron species existed in the form of Fe<sup>3+</sup> on the surface of the 10CuO-3Fe<sub>2</sub>O<sub>3</sub>/ $\alpha$ -MnO<sub>2</sub>-400 [54,56]. The XPS of Co 2p over the 10CuO-3Co<sub>3</sub>O<sub>4</sub>/ $\alpha$ -MnO<sub>2</sub>-400 catalyst is shown in Figure 5b. The binding energies at 780.0 eV are ascribed to the Co  $2p_{3/2}$  [57]. Meanwhile, there was no significant satellite shake-up intensity at 786 eV, indicating the dominance of Co<sup>3+</sup> on the surface of Co<sub>3</sub>O<sub>4</sub> [57]. The XPS of Ni 2p over the 10CuO-3NiO/ $\alpha$ -MnO<sub>2</sub>-400 catalyst is shown in Figure 5c. The binding energies at 855.1 eV are ascribed to the Ni  $2p_{3/2}$  [58]. The peak of Ni  $2p_{3/2}$  of metallic Ni was basically at 852.6 eV, and the binding energy of NiO is about 1 eV higher than that of Ni<sup>0</sup> [58]. The peak of NiO  $2p_{3/2}$  is lower than that of Ni  $2p_{3/2}$  in this work (854.8 eV). Therefore, the oxidation state of the indicated Ni element is mainly in the form of Ni<sup>2+</sup>. The higher binding energy compared to pure NiO binding energy indicates that NiO did not exist in the free form. The strong interaction was formed between the

Ni and the support. The results indicate that  $\text{Fe}_2\text{O}_3$ ,  $\text{Co}_3\text{O}_4$ , and  $\text{NiO}$  were successfully loaded on the catalyst. The XPS electronic binding energies of the surface elements of the  $10\text{CuO}-3\text{MOx}/\alpha\text{-MnO}_2-400$  ( $\text{MOx} = \text{Fe}_2\text{O}_3$ ,  $\text{Co}_3\text{O}_4$ ,  $\text{NiO}$ ) are summarized in Table 3.



**Figure 5.** (a) Fe 2p, (b) Co 2p, and (c) Ni 2p spectra of the  $10\text{CuO}-3\text{MOx}/\alpha\text{-MnO}_2-400$  ( $\text{MOx} = \text{Fe}_2\text{O}_3$ ,  $\text{Co}_3\text{O}_4$ ,  $\text{NiO}$ ) catalysts.

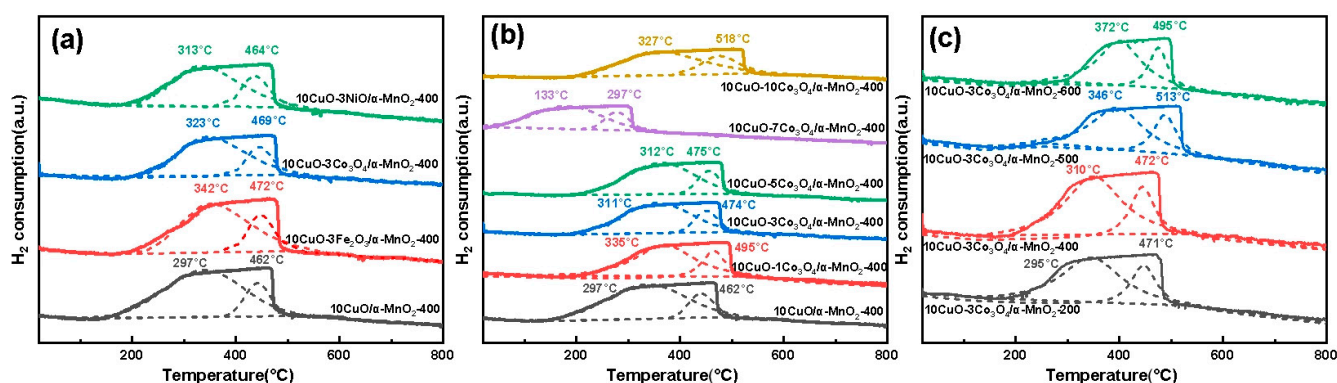
**Table 3.** XPS electronic binding energies of surface elements of the  $10\text{CuO}-3\text{MOx}/\alpha\text{-MnO}_2-400$  ( $\text{MOx} = \text{Fe}_2\text{O}_3$ ,  $\text{Co}_3\text{O}_4$ ,  $\text{NiO}$ ) catalysts.

Sample	Cu 2p <sub>3/2</sub>	O 1s	Mn 2p <sub>3/2</sub>
10CuO/ $\alpha\text{-MnO}_2$	933.6	529.7	642.1
10CuO-3Fe <sub>2</sub> O <sub>3</sub> / $\alpha\text{-MnO}_2$	933.7	529.7	642.1
10CuO-3Co <sub>3</sub> O <sub>4</sub> / $\alpha\text{-MnO}_2$	933.7	529.8	642.3
10CuO-3NiO/ $\alpha\text{-MnO}_2$	934.2	529.9	642.4

### 2.5. H<sub>2</sub>-TPR

The H<sub>2</sub>-TPR profiles of  $10\text{CuO}-3\text{MOx}/\alpha\text{-MnO}_2-400$  ( $\text{MOx} = \text{Fe}_2\text{O}_3$ ,  $\text{Co}_3\text{O}_4$ ,  $\text{NiO}$ ),  $10\text{CuO}-y\text{Co}_3\text{O}_4/\alpha\text{-MnO}_2-400$  ( $y = 0, 1, 3, 5, 7, 10$ ), and  $10\text{CuO}-3\text{Co}_3\text{O}_4/\alpha\text{-MnO}_2-T$  ( $T = 200, 400, 500, 600$  °C) are shown in Figure 6. It can be observed that both the  $10\text{CuO}-3\text{MOx}/\alpha\text{-MnO}_2-400$  catalyst and the  $10\text{CuO}/\alpha\text{-MnO}_2-400$  catalyst show similar hydrogen consumption peaks in strength and shape in Figure 6a. Specifically, there were two sets of peaks in the range of 297–342 °C and 462–472 °C, which might be attributed to the hydrogen consumption derived from the gradual reduction of the  $\alpha\text{-MnO}_2$  nanowire ( $\text{MnO}_2 \rightarrow \text{Mn}_2\text{O}_3 \rightarrow \text{Mn}_3\text{O}_4$ ), according to the pioneer report [31]. Meanwhile, it is worth noting that the loading of the transition metal oxides on the  $10\text{CuO}/\alpha\text{-MnO}_2$  support changed the reduction behavior of the  $10\text{CuO}/\alpha\text{-MnO}_2$  catalyst. Specifically, the reduction of  $10\text{CuO}/\alpha\text{-MnO}_2$  nanowires shifted to higher temperatures after loading the transition metal oxides. In general, the reducibility of the  $10\text{CuO}/\alpha\text{-MnO}_2$  catalyst decreases with the addition of transition metal oxides. The H<sub>2</sub>-TPR profiles of the  $10\text{CuO}-y\text{Co}_3\text{O}_4/\alpha\text{-MnO}_2-400$  catalysts with different  $\text{Co}_3\text{O}_4$  loading amounts are shown in Figure 6b. It is of great interest to find that the positions of the reduction peaks gradually shifted to the high-temperature region with the  $\text{Co}_3\text{O}_4$  loading amount increasing from 1 wt% to 10 wt%. This illustrated that the reducibility of the catalysts also gradually decreases. Therefore, the reduction temperatures of the  $10\text{CuO}-y\text{Co}_3\text{O}_4/\alpha\text{-MnO}_2-400$  catalyst were significantly higher than that of the  $10\text{CuO}/\alpha\text{-MnO}_2$  catalyst, except for the  $10\text{CuO}-7\text{Co}_3\text{O}_4/\alpha\text{-MnO}_2-400$  catalyst. The H<sub>2</sub>-TPR profiles of the  $10\text{CuO}-3\text{MOx}/\alpha\text{-MnO}_2-T$  catalyst with different calcination temperatures is shown in Figure 6c. It can be observed that the reduction temperature of the  $10\text{CuO}-3\text{Co}_3\text{O}_4/\alpha\text{-MnO}_2-T$  catalyst gradually shifted to a higher reduction temperature with the increase of the calcination temperature from 200 °C to 600 °C. The positions of the two reduction peaks became closer. This suggests that the interaction between the CuO and the  $\alpha\text{-MnO}_2$  nanowire support became stronger at higher temperatures.



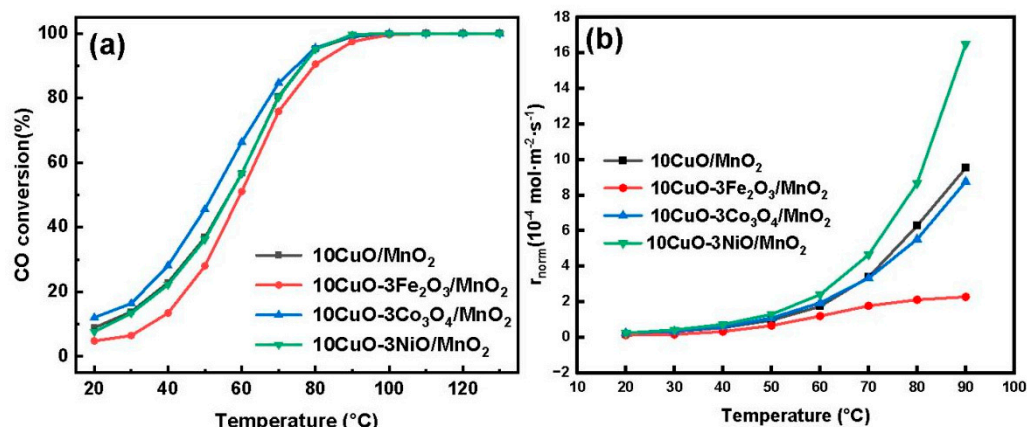


**Figure 6.** H<sub>2</sub>-TPR profiles of the (a) 10CuO-3MOx/α-MnO<sub>2</sub>-400 (MOx = Fe<sub>2</sub>O<sub>3</sub>, Co<sub>3</sub>O<sub>4</sub>, NiO), (b) 10CuO-yCo<sub>3</sub>O<sub>4</sub>/α-MnO<sub>2</sub>-400 (y = 0, 1, 3, 5, 7, 10), and (c) 10CuO-3Co<sub>3</sub>O<sub>4</sub>/α-MnO<sub>2</sub>-T (T = 200, 400, 500, 600 °C) catalysts.

## 2.6. Catalytic Performance of the CO Oxidation

### 2.6.1. The Effect of the Transition Metal Oxides (MOx) on the Activities

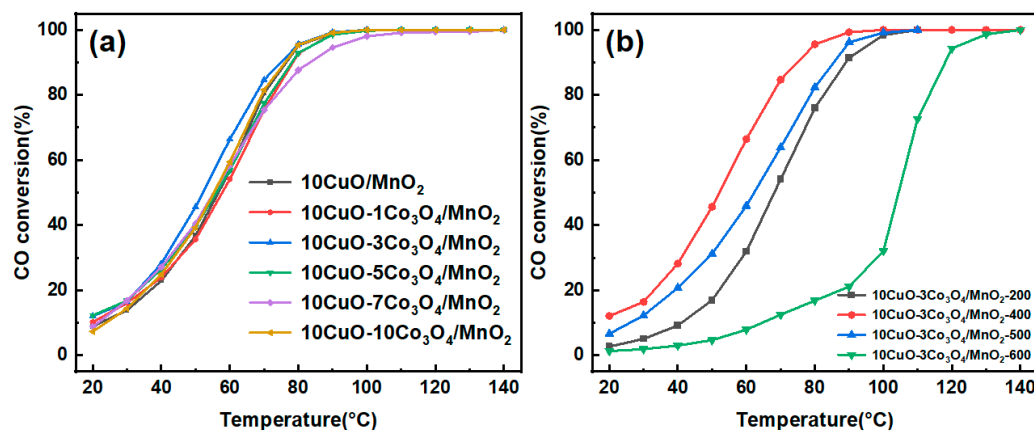
The catalytic CO oxidation activities of the 10CuO-3MOx/α-MnO<sub>2</sub>-400 (MOx = Fe<sub>2</sub>O<sub>3</sub>, Co<sub>3</sub>O<sub>4</sub>, NiO) catalysts were studied to investigate the effect of the dual loading of transition metals and CuO on the catalytic activity. As shown in Figure 7a, it can be observed that the CO conversion gradually increases with the increase of the reaction temperature until it reached 100%. As can be observed, the temperature of the 90% CO conversion over the 10CuO-3Co<sub>3</sub>O<sub>4</sub>/α-MnO<sub>2</sub>-400 catalyst was 75 °C. The activity of the 10CuO-3NiO/α-MnO<sub>2</sub>-400 catalyst basically shows a similar catalytic activity to that of the pristine 10CuO/α-MnO<sub>2</sub>-400 catalyst without modification ( $T_{90}$  = 77 °C). However, the CO oxidation activity of the 10CuO-3Fe<sub>2</sub>O<sub>3</sub>/α-MnO<sub>2</sub>-400 catalyst ( $T_{90}$  = 80 °C) was even worse than that of the pristine 10CuO/α-MnO<sub>2</sub>-400 catalyst. Therefore, only the catalytic activity of the 10CuO-3Co<sub>3</sub>O<sub>4</sub>/α-MnO<sub>2</sub>-400 was significantly improved compared with the pristine 10CuO/α-MnO<sub>2</sub>-400 catalyst. The reason for this might be that the loading of Cu and Co could generate more oxygen vacancies and active sites to the α-MnO<sub>2</sub> nanowire. From the order of catalyst activity, it can be observed that the catalytic activity of the catalyst increases with the increase in of Mn<sup>3+</sup> content. Meanwhile, the loading of Co<sub>3</sub>O<sub>4</sub> increased the specific surface area and pore volume of the catalyst, providing more active sites for the reaction. The ratio of  $O_{ads}/O_{latt}$  was not exactly the same as the catalytic activity of the catalyst. The reasons for this phenomenon were stated in the discussion. The CO oxidation activity was significantly improved over the 10CuO-3Co<sub>3</sub>O<sub>4</sub>/α-MnO<sub>2</sub>-400 catalyst. This result was well consistent with the Mn 2p XPS analysis. The results of the normalized reaction rates of the four catalysts are shown in Figure 7b. It can be observed that the normalized reaction rates gradually increase with the increase of the reaction temperature. The order of reaction rates of the catalysts per surface area was 10CuO-3NiO/MnO<sub>2</sub> > 10CuO/MnO<sub>2</sub> > 10CuO-3Co<sub>3</sub>O<sub>4</sub>/MnO<sub>2</sub> > 10CuO-3Fe<sub>2</sub>O<sub>3</sub>/MnO<sub>2</sub>. The normalized reaction rates excluded the effect of specific surface area on catalytic activity and expressed the intrinsic catalytic activity of the catalysts. The order of the  $O_{ads}/O_{latt}$  ratios was consistent with the order of the normalized reaction rates.



**Figure 7.** (a) CO conversions and (b) normalized reaction rates over the 10CuO-3MO<sub>x</sub>/α-MnO<sub>2</sub>-400 (MO<sub>x</sub> = Fe<sub>2</sub>O<sub>3</sub>, Co<sub>3</sub>O<sub>4</sub>, NiO) catalysts under the reaction conditions: CO/O<sub>2</sub>/N<sub>2</sub> = 1/20/79, GHSV = 12,000 mL·g<sup>-1</sup>·h<sup>-1</sup>, 1 atm.

### 2.6.2. The Effect of the Co<sub>3</sub>O<sub>4</sub> Loading Amount on the Activities

The effect of Co<sub>3</sub>O<sub>4</sub> loading on the catalytic activity of the CO oxidation was investigated, and the profiles of the CO conversion are shown in Figure 8a. It could be noticed that the Co<sub>3</sub>O<sub>4</sub> loading amount in the range of 0 wt.%–10 wt.% had little effect on the CO oxidation activity of the 10CuO/α-MnO<sub>2</sub> catalyst. The order of CO catalytic activity of the catalysts is 10CuO-3Co<sub>3</sub>O<sub>4</sub>/α-MnO<sub>2</sub>-400 (T<sub>90</sub> = 75 °C) > 10CuO-10Co<sub>3</sub>O<sub>4</sub>/α-MnO<sub>2</sub>-400 (T<sub>90</sub> = 77 °C) ≈ 10CuO/α-MnO<sub>2</sub>-400 > 10CuO-1Co<sub>3</sub>O<sub>4</sub>/α-MnO<sub>2</sub>-400 (T<sub>90</sub> = 79 °C) ≈ 10CuO-5Co<sub>3</sub>O<sub>4</sub>/α-MnO<sub>2</sub>-400 > 10CuO-7Co<sub>3</sub>O<sub>4</sub>/α-MnO<sub>2</sub>-400 (T<sub>90</sub> = 84 °C). The 10CuO-3Co<sub>3</sub>O<sub>4</sub>/α-MnO<sub>2</sub>-400 catalyst performed the highest activity in the low temperature region. It is shown that a certain increase in the loading of Co<sub>3</sub>O<sub>4</sub> was beneficial to the catalytic activity of the catalyst.



**Figure 8.** CO conversions over the (a) 10CuO-*y*Co<sub>3</sub>O<sub>4</sub>/α-MnO<sub>2</sub>-400 (*y* = 0, 1, 3, 5, 7, 10), and (b) 10CuO-3Co<sub>3</sub>O<sub>4</sub>/α-MnO<sub>2</sub>-*T* (*T* = 200, 400, 500, 600 °C) catalysts under the reaction conditions: CO/O<sub>2</sub>/N<sub>2</sub> = 1/20/79, GHSV = 12,000 mL·g<sup>-1</sup>·h<sup>-1</sup>, 1 atm.

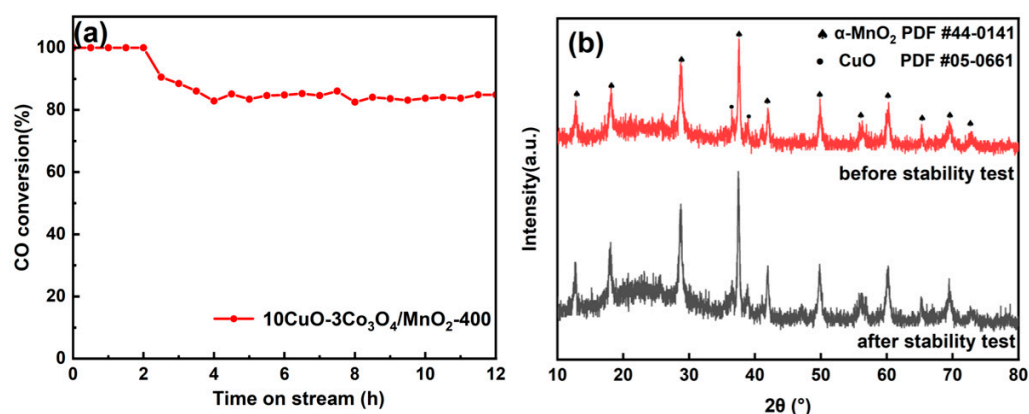
### 2.6.3. The Effect of the Calcination Temperature on the Activities

The catalytic CO oxidation of the 10CuO-3Co<sub>3</sub>O<sub>4</sub>/α-MnO<sub>2</sub>-*T* (*T* = 200, 400, 500, 600 °C) catalyst was conducted to study the influence of the calcination temperature on catalytic activity, and the CO conversion profiles are shown in Figure 8b. The order of CO catalytic activity of catalysts is 10CuO-3Co<sub>3</sub>O<sub>4</sub>/α-MnO<sub>2</sub>-400 (T<sub>90</sub> = 75 °C) > 10CuO-3Co<sub>3</sub>O<sub>4</sub>/α-MnO<sub>2</sub>-500 (T<sub>90</sub> = 86 °C) > 10CuO-3Co<sub>3</sub>O<sub>4</sub>/α-MnO<sub>2</sub>-200 (T<sub>90</sub> = 89 °C) > 10CuO-3Co<sub>3</sub>O<sub>4</sub>/α-MnO<sub>2</sub>-600 (T<sub>90</sub> = 118 °C). It can be observed that catalytic activity has significantly decreased with the increase of the calcination temperature from 400 °C to 600 °C, especially over

the 10CuO-3Co<sub>3</sub>O<sub>4</sub>/α-MnO<sub>2</sub>-600 catalyst. Specifically, the 10CuO-3Co<sub>3</sub>O<sub>4</sub>/α-MnO<sub>2</sub>-600 catalyst had low activity of CO oxidation in the low temperature region. The possible reason is that the formation of a copper manganese spinel in the catalyst after calcination at high temperatures led to the significant decrease in the CO adsorption and oxidation capacities of the catalysts. This result is consistent with the XRD analysis. The 10CuO-3Co<sub>3</sub>O<sub>4</sub>/α-MnO<sub>2</sub>-200 catalyst was also prepared for comparison. The results show that the catalytic activity of the 10CuO-3Co<sub>3</sub>O<sub>4</sub>/α-MnO<sub>2</sub>-200 catalyst was significantly lower than that of the 10CuO-3Co<sub>3</sub>O<sub>4</sub>/α-MnO<sub>2</sub>-400 catalyst. The possible reason is that the precursor of the Co<sub>3</sub>O<sub>4</sub> could not be completely decomposed at 200 °C.

#### 2.6.4. Stability Tests

The 12 h stability measurement was conducted over the 10CuO-3Co<sub>3</sub>O<sub>4</sub>/α-MnO<sub>2</sub>-400 catalyst under the specific conditions (80 °C, CO/O<sub>2</sub>/N<sub>2</sub> = 1/20/79, GHSV = 12,000 mL·g<sup>-1</sup>·h<sup>-1</sup>, 1 atm), and the result is shown in Figure 9a. It can be observed that the initial activity of the 10CuO-3Co<sub>3</sub>O<sub>4</sub>/α-MnO<sub>2</sub>-400 catalyst can achieve 100% CO conversion in the first 2 h. Then, the CO conversion gradually decreased from 100% to 80% in the subsequent 2 h test. This indicates that the catalyst began to deactivate. However, the CO conversion could remain stable in the subsequent 8 h. This suggests that the 10CuO-3Co<sub>3</sub>O<sub>4</sub>/α-MnO<sub>2</sub>-400 catalyst was provided with relatively good stability to some degree.



**Figure 9.** (a) The 12 h stability test of CO oxidation over the 10CuO-3Co<sub>3</sub>O<sub>4</sub>/α-MnO<sub>2</sub>-400 catalyst under the conditions: 80 °C, CO/O<sub>2</sub>/N<sub>2</sub> = 1/20/79, GHSV = 12,000 mL·g<sup>-1</sup>·h<sup>-1</sup>, 1 atm; (b) The XRD patterns of the fresh and the spent 10CuO-3Co<sub>3</sub>O<sub>4</sub>/α-MnO<sub>2</sub>-400 catalysts before and after the stability test.

The XRD pattern of the 10CuO-3Co<sub>3</sub>O<sub>4</sub>/α-MnO<sub>2</sub>-400 catalyst after the 12 h stability test is shown in Figure 9b. It can be observed that the diffraction peaks of the spent 10CuO-3Co<sub>3</sub>O<sub>4</sub>/α-MnO<sub>2</sub>-400 catalyst after the 12 h stability test were a bit narrower and sharper than the fresh catalyst before the stability test. The possible reason is that the 10CuO-3Co<sub>3</sub>O<sub>4</sub>/α-MnO<sub>2</sub>-400 catalyst underwent a bit of thermal agglomeration of the CuO active sites and the α-MnO<sub>2</sub> nanowire support during the catalytic process due to the hot spots of the catalyst bed, which could partly reduce the stability of the catalyst.

### 3. Discussion

The oxidation of CO on Cu-doped MnO<sub>2</sub> follows the Mars–van Krevelen (MvK) mechanism [35]. The reaction is divided into two parts: CO is first adsorbed on the catalyst surface and then reacts with surface-active oxygen on the catalyst surface to produce CO<sub>2</sub>, which then generates oxygen vacancies on the catalyst surface. O<sub>2</sub> replenishes the depleted surface-active oxygen. After these two processes, the reaction completes a cycle [59]. There are redox electron pairs in the Cu-doped MnO<sub>2</sub> catalyst: -Cu<sup>2+</sup>-O<sup>2-</sup>-Mn<sup>4+</sup>- → -Cu<sup>+</sup>-□-Mn<sup>3+</sup>- + 1/2O<sub>2</sub> (□ indicates the oxygen vacancy) [45]. The content of Mn<sup>3+</sup> on the MnO<sub>2</sub> catalyst is higher, presumably with more oxygen vacancies on the MnO<sub>2</sub> [60].

The order of the oxygen vacancy content of the catalysts is  $10\text{CuO}-3\text{Co}_3\text{O}_4/\alpha\text{-MnO}_2 > 10\text{CuO}-3\text{NiO}/\alpha\text{-MnO}_2 > 10\text{CuO}/\alpha\text{-MnO}_2 > 10\text{CuO}-3\text{Fe}_2\text{O}_3/\alpha\text{-MnO}_2$ . The oxygen vacancy content is consistent with the  $\text{Mn}^{3+}$  content and catalyst activity.  $\text{O}_2$  is commonly activated near the oxygen vacancy, producing surface active oxygen species ( $\text{O}_{\text{sur}}$ ) [61]. It is well known that the higher the surface oxygen vacancy, the more easily  $\text{O}_2$  is activated to reactive oxygen species [50]. However, the XPS spectra of O 1s showed that the order of the  $\text{O}_{\text{ads}}/\text{O}_{\text{latt}}$  ratios was not consistent with the oxygen vacancy content and catalyst activity. To evaluate the intrinsic activity of the catalysts, the surface area normalized reaction rates are determined. The results of the surface area normalized reaction rates show that the loading of NiO has the greatest effect on the intrinsic activity of the catalyst. The  $10\text{CuO}-3\text{NiO}/\alpha\text{-MnO}_2$  catalyst did not exhibit superior catalytic activity because the specific surface area of the catalyst after NiO loading was reduced, and the effect of specific surface area on the activity of the CO oxidation reaction could not be ignored. The  $10\text{CuO}-3\text{NiO}/\alpha\text{-MnO}_2$  catalyst has the most surface adsorbed oxygen and reaction rates per unit surface area, but the small specific surface area results in the catalytic activity being similar to that of the pristine  $10\text{CuO}/\alpha\text{-MnO}_2$ -400 catalyst. The order of the intrinsic activity of the catalyst is consistent with the order of the  $\text{O}_{\text{ads}}/\text{O}_{\text{latt}}$  ratio ( $10\text{CuO}-3\text{NiO}/\alpha\text{-MnO}_2 > 10\text{CuO}/\alpha\text{-MnO}_2 > 10\text{CuO}-3\text{Co}_3\text{O}_4/\alpha\text{-MnO}_2 > 10\text{CuO}-3\text{Fe}_2\text{O}_3/\alpha\text{-MnO}_2$ ). This suggests that the surface-adsorbed oxygen is the reactive oxygen species involved in the oxidation of CO.  $\text{CO}_2$  was produced by CO reacting with surface-adsorbed oxygen species [62,63]. After loading different transition metals, the catalysts form different types of oxygen vacancies, which have different electron densities and affect the production of reactive oxygen species [39]. The oxygen vacancies of  $10\text{CuO}-3\text{Co}_3\text{O}_4/\alpha\text{-MnO}_2$  did not activate  $\text{O}_2$  as well, and the  $10\text{CuO}-3\text{Co}_3\text{O}_4/\alpha\text{-MnO}_2$  catalyst did not form more surface adsorbed oxygen. This might be the cause of the  $10\text{CuO}-3\text{Co}_3\text{O}_4/\alpha\text{-MnO}_2$  catalyst providing the highest oxygen vacancy but poor surface-adsorbed oxygen. Although the normalized reaction rate of the  $10\text{CuO}-3\text{Co}_3\text{O}_4/\alpha\text{-MnO}_2$  catalyst is not the highest, its high specific surface area allows for a greater number of oxygen vacancies. The large number of oxygen vacancies of the  $10\text{CuO}-3\text{Co}_3\text{O}_4/\alpha\text{-MnO}_2$  catalyst counteracted the low activity of the oxygen vacancies and performed the high catalytic activity of CO oxidation. Therefore, the  $10\text{CuO}-3\text{Co}_3\text{O}_4/\alpha\text{-MnO}_2$  catalyst exhibited the highest activity owing to its maximum specific surface area. The activity of the  $10\text{CuO}-3\text{Co}_3\text{O}_4/\alpha\text{-MnO}_2$  catalyst was slightly higher than that of the  $10\text{CuO}-3\text{NiO}/\alpha\text{-MnO}_2$  catalyst.

#### 4. Materials and Method

##### 4.1. Synthesis of $\alpha\text{-MnO}_2$ Nanowire Supports

The  $\alpha\text{-MnO}_2$  nanowire support was facilely prepared via the typical hydrothermal method. Typically, 2 mmol  $\text{KMnO}_4$  (Sinopharm Chemical Reagent Co., Ltd., Shanghai, China, AR, >99.5%) and 3 mmol  $\text{MnSO}_4 \cdot \text{H}_2\text{O}$  (Shanghai Aladdin Biochemical Technology Co., Ltd., Shanghai, China, AR, 99%) were absolutely dissolved in 40 mL deionized water and vigorously stirred for 5 min, respectively. Then, these two solutions were mixed together by adding the  $\text{KMnO}_4$  solution into the  $\text{MnSO}_4$  solution. After stirring for 30 min, the obtained suspension was transferred to the 100 mL Teflon-lined stainless-steel autoclave. The autoclave was kept at  $160^\circ\text{C}$  for 12 h. The obtained precipitate after the hydrothermal reaction was separated by the centrifuge and washed with ethanol (Sinopharm Chemical Reagent Co., Ltd., Shanghai, China, AR) and deionized water for three times. Then, the final powder was dried in the  $100^\circ\text{C}$  oven overnight after the centrifugation. The obtained  $\alpha\text{-MnO}_2$  was used as a support for subsequent experiments.

##### 4.2. The Preparation of the Transition Metal Oxide ( $\text{Fe}_2\text{O}_3$ , $\text{Co}_3\text{O}_4$ , $\text{NiO}$ )-Doped CuO-Based Catalysts Supported on the $\alpha\text{-MnO}_2$ Nanowire

The transition metal oxides promoted CuO-based  $\alpha\text{-MnO}_2$  nanowire supported catalysts were prepared by the deposition precipitation method as reported in our previous work [64]. The weight percentages of the CuO and transition metal oxides were controlled

at  $x\%$  and  $y\%$  ( $x\% = m_{\text{CuO}} / (m_{\text{CuO}} + m_{\text{MOx}} + m_{\text{support}}) \times 100\%$ ;  $y\% = m_{\text{MOx}} / (m_{\text{CuO}} + m_{\text{MOx}} + m_{\text{support}}) \times 100\%$ ) by using the  $\text{Cu}(\text{NO}_3)_2 \cdot 6\text{H}_2\text{O}$  (Shanghai Xinbao Fine Chemical Industry Factory, Shanghai, China, AR, >99.5%),  $\text{Fe}(\text{NO}_3)_3 \cdot 9\text{H}_2\text{O}$  (Shanghai Macklin Bio-Chem Co., Ltd., Shanghai, China, AR, 98.5%),  $\text{Co}(\text{NO}_3)_2 \cdot 6\text{H}_2\text{O}$  (Shanghai Macklin Bio-Chem Co., Ltd., Shanghai, China, AR, 99%),  $\text{Ni}(\text{NO}_3)_2 \cdot 6\text{H}_2\text{O}$  (Sinopharm Chemical Reagent Co., Ltd., Shanghai, China, AR, 99%) as the precursors. For the specific procedure, the  $\alpha\text{-MnO}_2$  nanowire was firstly dispersed in a  $\text{Cu}(\text{NO}_3)_2 \cdot 6\text{H}_2\text{O}$  and  $\text{Fe}(\text{NO}_3)_3 \cdot 9\text{H}_2\text{O} / \text{Co}(\text{NO}_3)_2 \cdot 6\text{H}_2\text{O} / \text{Ni}(\text{NO}_3)_2 \cdot 6\text{H}_2\text{O}$  aqueous solution. Then, the  $\text{Na}_2\text{CO}_3$  (0.01M, Shanghai Ling Feng Chemical Reagent Co., Ltd., Shanghai, China, AR, >99.8%) solution was added by droplet into the above solution to adjust the pH to 8–9 under vigorously stirring. The resultant solution was stirred for 30 min and then kept still for 1 h. The solid powder was separated by filtration and washed by the deionized water. The obtained catalyst was dried at  $120^\circ\text{C}$  in an oven overnight and then calcinated at  $400^\circ\text{C}$  for 5 h with a heating rate of  $2^\circ\text{C}/\text{min}$ . The  $\alpha\text{-MnO}_2$  nanowire-supported catalysts with 10 wt.% CuO and 3 wt.% MOx (MOx =  $\text{Fe}_2\text{O}_3$ ,  $\text{Co}_3\text{O}_4$ , NiO) were denoted as the  $10\text{CuO-3MOx}/\alpha\text{-MnO}_2$  (MOx =  $\text{Fe}_2\text{O}_3$ ,  $\text{Co}_3\text{O}_4$ , NiO). Meanwhile, the loading amount of the  $\text{Co}_3\text{O}_4$  (wt.%) was subsequently changed in the same way. The obtained catalysts with loading amounts of 10 wt.% CuO and  $y$  wt.%  $\text{Co}_3\text{O}_4$  were denoted as the  $10\text{CuO-}y\text{Co}_3\text{O}_4/\alpha\text{-MnO}_2$  ( $y = 0, 1, 3, 5, 7, 10$ ). As for the influence of the calcination temperature, the catalysts with loading of the 10 wt.% CuO and 3 wt.%  $\text{Co}_3\text{O}_4$  were calcinated at different temperatures and named  $10\text{CuO-3Co}_3\text{O}_4/\alpha\text{-MnO}_2\text{-T}$  ( $T = 200, 400, 500, 600^\circ\text{C}$ ).

#### 4.3. Catalyst Characterizations

The X-ray diffraction (XRD) patterns of the catalysts were recorded on an X-ray power diffractometer (XRD-6100) from the Shimadzu Corporation by using the Cu K $\alpha$  rays (0.15046 nm), 40 KV tube voltage, and 40 mA tube current. The  $2\theta$  scanning range was from  $10^\circ$  to  $80^\circ$ , and the scanning speed was controlled at  $3^\circ/\text{min}$ . The scanning electron microscope (SEM) images were taken on an Apreo S Hivac instrument (Thermo Fisher Science, Waltham, MA, USA) with the accelerating voltage of 5 kV. The nitrogen physisorption was performed on an Autosorb-iQ-AG-MP instrument (Quantachrome, Boynton Beach, FL, USA) at liquid nitrogen temperature ( $-196^\circ\text{C}$ ). The samples were degassed at  $300^\circ\text{C}$  for 3 h to remove the surface-adsorbed water and impurities before the regular test. The specific surface areas of the catalysts were calculated by the Brunauer-Emmett-Teller (BET) method, and the pore size distribution and pore volume were calculated from the adsorption branch of the isotherm by the Barrett-Joyner-Halenda (BJH) method in the range of 0–1.0 P/P $_0$ . The X-ray photoelectron spectroscopy (XPS) measurements were performed on a Thermo Science K-Alpha + spectrometer (Thermo Fisher Science, Waltham, MA, USA). For the XPS measurement, the penetration depth of each catalyst was about 1–2 nm. The binding energy (BE) was calibrated by using C 1s = 284.8 eV as the standard. A fixed-bed reactor was used to conduct the hydrogen temperature-programmed reduction ( $\text{H}_2\text{-TPR}$ ) experiment. The hydrogen consumption profile was recorded and analyzed with the online LC-D200 mass spectrometer (TILON GRP TECHNOLOGY LIMITED, Shanghai, China). The mixture of  $\text{H}_2$  (1.2 mL/min) and Ar (23.7 mL/min) was introduced into the reactor. For each test, 100 mg of catalyst was loaded. After the hydrogen signal baseline line ( $m/z = 2$ ) was stabilized, the  $\text{H}_2\text{-TPR}$  test was performed with a heating rate of  $20^\circ\text{C}/\text{min}$  from room temperature to  $800^\circ\text{C}$ .

#### 4.4. Catalyst Evaluation

The activity of the catalysts was evaluated in a fixed-bed reactor equipped with a quartz tube (i.d. = 8.00 mm). For each test, 100 mg catalyst was placed in the center of the quartz tube. The reactant gases, with a composition of 1%  $\text{CO}$ , 21%  $\text{O}_2$ , 79%  $\text{N}_2$  (20 mL/min), were introduced into the reactor with the gas hourly space velocity (GHSV) of  $12,000 \text{ mL} \cdot \text{g}^{-1} \cdot \text{h}^{-1}$ . The catalytic activities of CO oxidation over different catalysts were tested in the specified temperature range. Each catalyst was tested three times at each

temperature. The outlet gases were analyzed online by using the GC-680 Perkin Elmer gas chromatograph equipped with the thermal conductivity detector (TCD). The 24 h stability tests of catalysts were carried out at 80 °C with the GHSV of 12,000 mL·g<sup>-1</sup>·h<sup>-1</sup>.

The catalytic performances of CO oxidation over these catalysts were stated in the form of the CO conversion. The calculated formula is listed below:

$$X_{\text{CO}} = (C_{\text{CO, Inlet}} - C_{\text{CO, Outlet}}) / C_{\text{CO, Inlet}} \times 100\% \quad (1)$$

where  $X_{\text{CO}}$  is the conversion rate of CO; and  $C_{\text{CO, Inlet}}$  (ppm), and  $C_{\text{CO, Outlet}}$  (ppm) are CO flowing into and out of the reactor, respectively.

In order to evaluate the intrinsic rate of CO oxidation on these catalysts, the calculated formula of the specific surface area normalization reaction rate is listed below [25]:

$$r_{\text{norm}} \left( \text{mol} \cdot \text{m}^{-2} \cdot \text{s}^{-1} \right) = \frac{C_{\text{inlet}} \cdot F}{m_{\text{cat}} \cdot S_{\text{BET}}} \cdot \ln \left( \frac{1}{1 - X_{\text{CO}}} \right) \quad (2)$$

where  $r_{\text{norm}}$  (mol·m<sup>-2</sup>·s<sup>-1</sup>) is the normalized reaction rate,  $F$  (mol·s<sup>-1</sup>) is the CO flow rate,  $m_{\text{cat}}$  (g) is the mass of catalyst, and  $S_{\text{BET}}$  (m<sup>2</sup>·g<sup>-1</sup>) is the BET surface area.

## 5. Conclusions

In this work, the novel  $\alpha$ -MnO<sub>2</sub> nanowire was prepared by the one-step hydrothermal method. A series of transition metal oxides (Fe<sub>2</sub>O<sub>3</sub>, Co<sub>3</sub>O<sub>4</sub>, NiO) promoted the CuO-based catalyst supported on the  $\alpha$ -MnO<sub>2</sub> nanowire and were synthesized by the co-precipitation method for the CO oxidation reaction. The effects of the transition metal oxide type, the loading amount, and the calcination temperature on the CO oxidation reaction had been systematically investigated. It was found that the 10CuO-3Co<sub>3</sub>O<sub>4</sub>/α-MnO<sub>2</sub>-400 catalyst showed the highest reactivity with  $T_{90} = 75$  °C. It was found that the 10CuO-3Co<sub>3</sub>O<sub>4</sub>/α-MnO<sub>2</sub>-400 catalyst possessed the largest specific surface area and exposed more active sites, which could further enhance the catalytic activity. The 10CuO-3NiO/α-MnO<sub>2</sub>-400 catalyst had the highest surface-adsorbed oxygen content and normalized reaction rate. This indicated that the surface-adsorbed oxygen was the surface-active oxygen involved in the oxidation of CO. It was found that the 10CuO-3Co<sub>3</sub>O<sub>4</sub>/α-MnO<sub>2</sub>-400 catalyst suffered from some deactivation during the 12 h stability test, which might be caused by the thermal sintering and agglomeration of the CuO active sites and α-MnO<sub>2</sub> nanowire support. This should be the key consideration when designing the CuO-based CO oxidation catalyst in the future.

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**Conflicts of Interest:** The authors declare no conflict of interest.



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## Article

# Molten Salt-Assisted Catalytic Preparation of MoS<sub>2</sub>/α-MoO<sub>3</sub>/Graphene as High-Performance Anode of Li-Ion Battery

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**Abstract:** We report on the facile and scalable catalytic conversion of natural graphite and MoS<sub>2</sub> minerals into α-MoO<sub>3</sub> nanoribbons incorporated into hexagonal MoS<sub>2</sub> and graphene nanosheets, and evaluate the structural, morphological and electrochemical performances of the hybrid nanostructured material obtained. Mechanochemical treatment of raw materials, followed by catalytic molten salt treatment leads to the formation of nanostructures with promising electrochemical performances. We examined the effect of processing temperature on the electrochemical performance of the products. At 1100 °C, an excellent Li-ion storage capacity of 773.5 mAh g<sup>−1</sup> is obtained after 180 cycles, considerably greater than that of MoS<sub>2</sub> (176.8 mAh g<sup>−1</sup>). The enhanced capacity and the rate performance of this electrode are attributed to the well-integrated components, characterized by the formation of interfacial molybdenum oxycarbide layer during the synthesis process, contributing to the reduced electrical/electrochemical resistance of the sample. This unique morphology promotes the charge and ions transfer through the reduction of the Li-ion diffusion coefficient ( $1.2 \times 10^{-18}$  cm<sup>2</sup> s<sup>−1</sup>), enhancing the pseudocapacitive performance of the electrode; 59.3% at the scan rate of 0.5 mV s<sup>−1</sup>. This article provides a green and low-cost route to convert highly available natural graphite and MoS<sub>2</sub> minerals into nanostructured hybrid materials with promising Li-ion storage performance.

**Keywords:** natural graphite; MoS<sub>2</sub>; molten NaCl; graphene; MoO<sub>3</sub>; molybdenum oxycarbide

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## 1. Introduction

The development of efficient and low-cost energy storage devices is a key towards the electrification of various sectors, including the transportation and grid services [1–3], supporting the sustainable development goals. Lithium-ion battery (LIB) is the state of the art energy storage device in a wide variety applications and, therefore, its modifications in terms of performance, cost and availability of raw materials are of great importance [4–6]. Graphite, including synthetic graphite (SG) and modified natural graphite (NG) is a commonly used material for the fabrication of the anode of LIBs, due to its modest theoretical capacity of 372 mAh g<sup>−1</sup> and high cycle stability [7,8]. SG is made by the graphitization of carbonaceous material at extremely high temperatures ( $\approx 3000$  °C) [9], which is an extremely energy-intensive approach. NG originating from carbon-rich organics formed through the prolonged geological interactions [9] is considered as a promising alternative anode material mainly due to its high availability and low cost [10–12]. In fact, the world's NG reserves are huge, exceeding 800 million tons of recoverable graphite [13], with a typical low price of around USD 750 per metric ton ( $\approx 94\%$  purity) [11] making NG highly attractive for energy applications. Despite these advantages, however, NG minerals often undergo expensive, energy intensive and time-consuming processes, including high-temperature treatments ( $>2300$  °C), and/or treatment with hazardous chemicals such as HF [13–15]. Therefore, the direct application of NG minerals for the fabrication of anode materials

without going through expensive/environmentally problematic processes is required in order to appropriately utilize NG for future developments of LIBs.

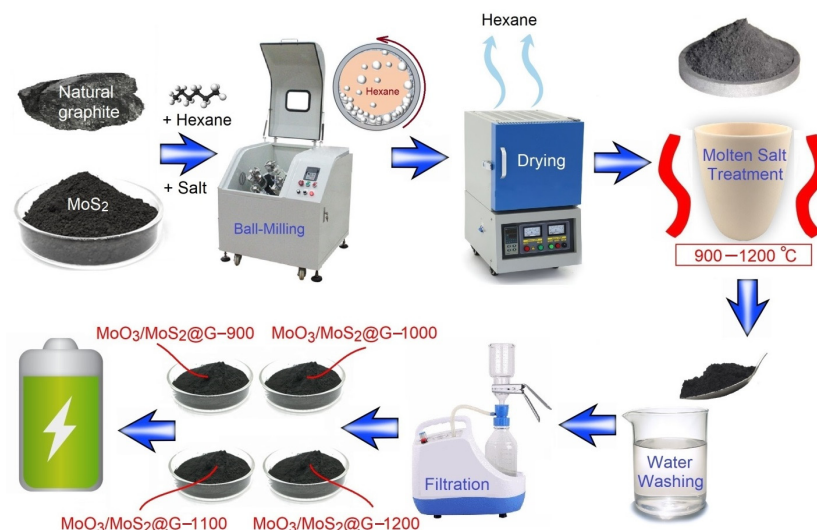
Apart from NG, other naturally available materials such as molybdenum disulfide ( $\text{MoS}_2$ ) have also attracted attentions due to their high availability and low-cost. In particular, the theoretical Li-ion storage capacity of  $\text{MoS}_2$  is approximately three times greater than that of commercial graphite anodes [16,17]. Despite its potential capability, the application of  $\text{MoS}_2$  as the anode of LIBs is challenging due to the low reversible capacity of the material at large cycle numbers. In contrast to  $\text{MoS}_2$ , other molybdenum compounds such as molybdenum trioxide ( $\text{MoO}_3$ ) have also been evaluated as the anode of LIBs. However, the cycling performance of  $\text{MoO}_3$  is not satisfactory due to the low conductivity of the compound, and its disintegration during discharge/charge cycles [18–20]. These issues might be reduced by combining  $\text{MoO}_3$  and  $\text{MoS}_2$  so that the latter can enhance the conductivity of the nanocomposite and prevents the rapid disintegration [21–23]. The methods suggested for the synthesis of  $\text{MoS}_2/\text{MoO}_3$  nanocomposites comprise of chemical vapor deposition [24], hydrothermal methods [25,26], in-situ growth [23], sulfur transfer [27], anion-exchange [28], and annealing treatment [29] using the precursor materials such as  $(\text{NH}_4)_6\text{Mo}_7\text{O}_{24}$  and thiourea [23,28], organic amine, and  $\text{MoO}_3$  [24], Mo metal powder and  $\text{H}_2\text{O}_2$  [27] as well as  $\text{MoO}_3$  powders, sulfur and  $\text{N}_2$  [29]. These synthesis methods are typically complicated and require long processing periods involving expensive and/or environmentally problematic raw materials, limiting their capability at large scales.

With this background, the clean and facile preparation  $\text{MoS}_2/\text{MoO}_3$  nanocomposites with enhanced Li-ion storage performance using low-cost and highly available minerals is an interesting goal. In a recent work, we suggested the mechanochemical–molten salt treatment of pure synthetic graphite with  $\text{MoS}_2$  as a possible green way of producing nanostructures with promising Li-ion storage performance [30]. However, the application of pure synthetic graphite would greatly influence the economic and sustainability of the process. In this study, we show that the wet high-energy ball-milling of commercial  $\text{MoS}_2$ , non-purified natural graphite and NaCl, followed by a heat-treatment at temperatures above the melting point of NaCl leads to the formation of well-integrated nanostructured hybrid materials, in which  $\text{MoO}_3$  nanoribbons are incorporated with hexagonal  $\text{MoS}_2$  and graphene nanosheets. We further study on the effect of heating regime on the microstructural evolution of the nanocomposite materials, and find out that at 1100 °C, the nanocomposite contains the highest amount of well-integrated  $\alpha\text{-MoO}_3$  nanoribbons providing a promising Li-ion storage performance of 773.5 mAh g<sup>−1</sup> after 180 charge/discharge cycles, considerably greater than that of  $\text{MoS}_2$  (176.8 mAh g<sup>−1</sup>). We suggest the formation of interfacial molybdenum oxycarbide that reduces the internal impedance, and promotes the ion/electron transfer within the nanostructured material, and its interface with the electrolyte. Furthermore, this article reports on the molten salt synthesis of hexagonal  $\text{MoS}_2$  nanosheets, which are well incorporated into the nanocomposite and contribute to the high performance of the electrode by improving the electron and ion transportation across the material. The formation of hexagonal  $\text{MoS}_2$  nanosheets, presented here, is in contrast with alternative techniques reported in the literature for the fabrication of such  $\text{MoS}_2$  morphologies based on prolonged sulfurization of  $(\text{NH}_4)_2\text{MoS}_4$  using  $\text{H}_2\text{S}$  at 800 °C [31,32]. Other techniques reported on the preparation of hexagonal  $\text{WS}_2$  nanoflakes include thermal conversion of  $\text{W}_x\text{O}_y$  nanorods in the presence of S at 750 °C (6 h) under high-vacuum [33], and the electrochemical exfoliation of  $\text{WS}_2$  in  $\text{Na}_2\text{SO}_4$  [34]. Also, the preparation of hexagonal nanosheets of  $\text{CdI}_2$  [35] and  $\text{SnS}_2$  [36] have been reported using chemical vapor deposition and steam vapor etching. In this paper, we report on the facile preparation of hexagonally-shaped  $\text{MoS}_2$  nanosheets incorporated with  $\text{MoO}_3$  nanoribbons and graphene nanosheets ( $\text{MoO}_3/\text{MoS}_2@\text{Graphene}$ ) by a simple mechanochemical–molten salt approach using natural graphite and  $\text{MoS}_2$  minerals, with promising Li-ion storage performance. The mechanism involved in the preparation and the electrochemical performance of the nanostructured materials are investigated.

## 2. Results

### 2.1. Preparation of Materials

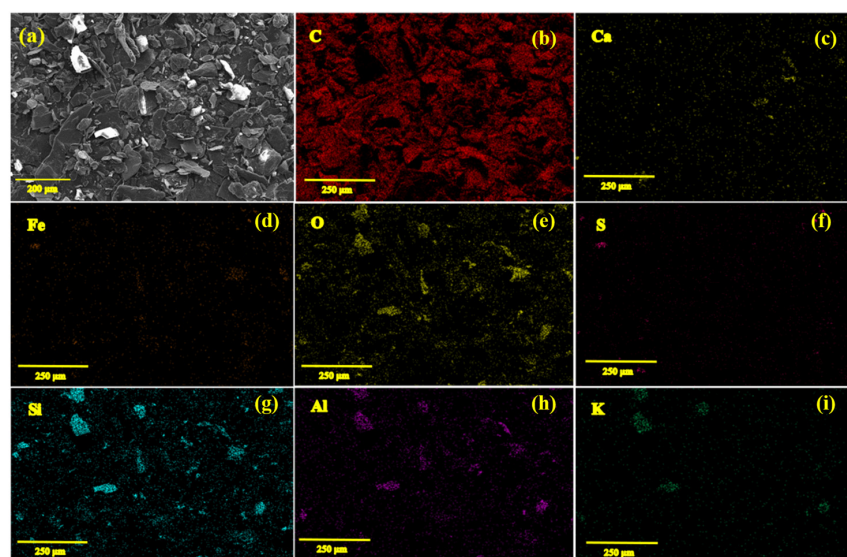
In this work,  $\text{MoO}_3/\text{MoS}_2@\text{Graphene}$  samples were prepared using natural graphite mineral without conducting extensive modification/purification processes which are often performed to fabricate battery-grade materials. The details of the process are mentioned in “Materials and Methods” and summarized in Figure 1.



**Figure 1.** The process employed to convert natural graphite mineral and commercially available  $\text{MoS}_2$  into nanostructured materials for energy-storage application.

### 2.2. Characterization of the Natural Graphite Mineral

It is useful to provide insights on to the chemical and microchemical composition of the NG used as the raw material in this research. Figure 2 shows the SEM/EDS element mapping analysis recorded on the sample. As can be seen from Figure 2a, the material contains graphitic flakes with lateral dimensions typically larger than  $20\ \mu\text{m}$ . According to the EDS analysis, in addition to carbon, other elements comprising Ca, Fe, O, S, Si, Al, and K could also be detected, indicating the impurity of the natural graphite material.



**Figure 2.** (a) SEM micrograph of the non-purified natural graphite material, and (b–i) corresponding elemental EDS mapping analysis exhibiting the distribution of various elements.

The presence of oxide impurities can clearly be recognized from the EDS analysis. The data obtained could be confirmed by the X-ray fluorescence (XRF) quantitative analysis recorded on the natural graphite sample, as exhibited in Table 1. The analysis performed shows that the carbon content of the material is 74.3 wt%. Other components include SiO<sub>2</sub> (9.27 wt%), Al<sub>2</sub>O<sub>3</sub> (6.92 wt%), CaO (2.97 wt%), Fe<sub>2</sub>O<sub>3</sub> (2.29 wt%), K<sub>2</sub>O (2.17 wt%) and S (2.08 wt%). The natural graphite mineral was employed for the synthesis of MoO<sub>3</sub>/MoS<sub>2</sub>@graphene samples without purification, as explained in the next section.

**Table 1.** Quantitative XRF analysis of the natural graphite material (wt%).

C	SiO <sub>2</sub>	Al <sub>2</sub> O <sub>3</sub>	CaO	Fe <sub>2</sub> O <sub>3</sub>	K <sub>2</sub> O	S
74.3	9.27	6.92	2.97	2.29	2.17	2.08

### 2.3. Catalytic Phase Transitions during the Molten Salt Treatment

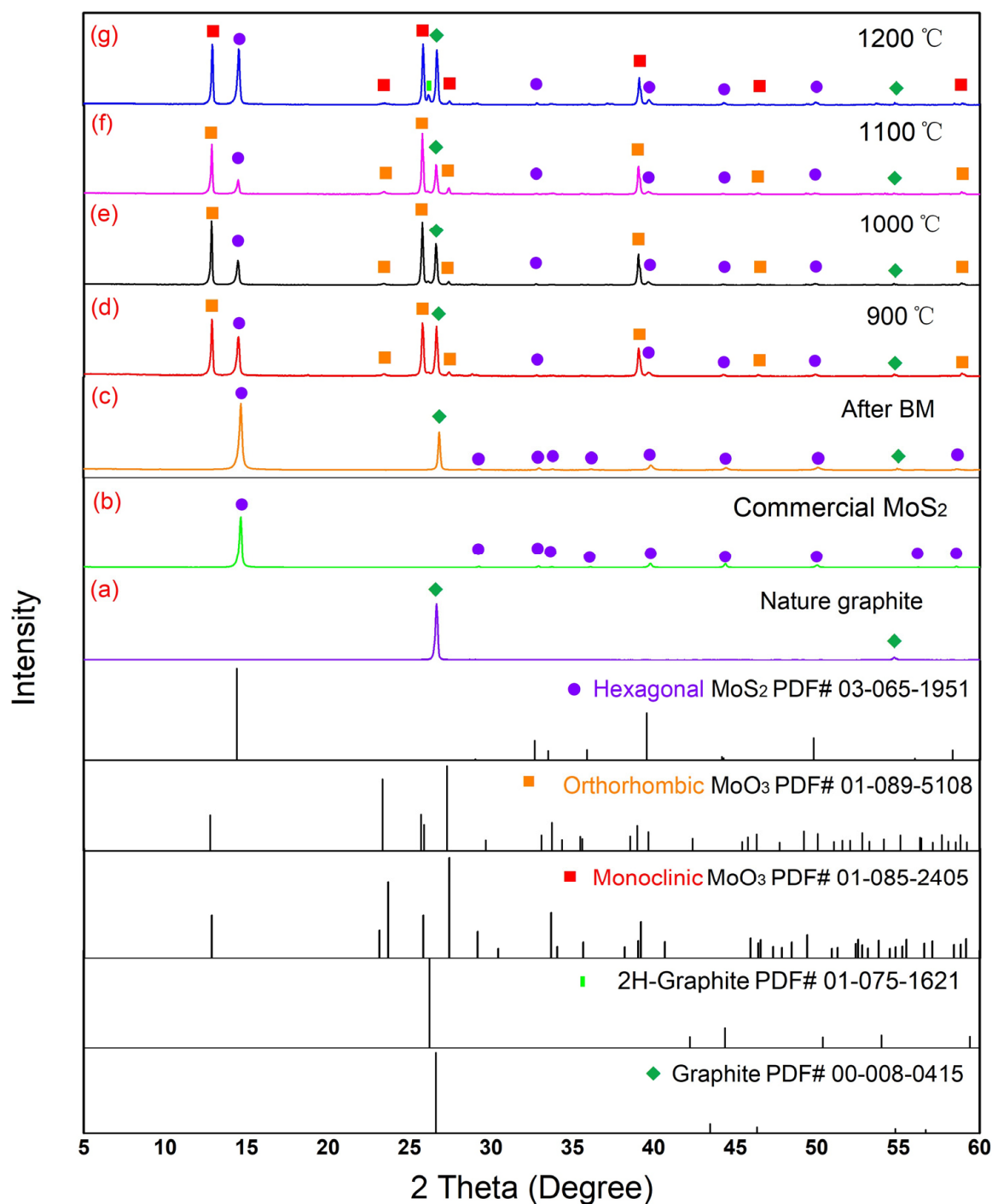
MoS<sub>2</sub> and natural graphite precursors were subjected to a ball-milling process (2 h) in the presence of hexane, and the BMed samples were heat treated with NaCl at 900, 1000, 1100 and 1200 °C in air for 20 min. These temperatures are greater than the melting point of NaCl (~800 °C), causing the progress of the reactions in a molten salt environment. This simple molten salt process led to the formation of MoS<sub>2</sub>/MoO<sub>3</sub>@Graphene nanocomposites, as can be realized from Figure 1, and the XRD patterns of Figure 3. Moreover, the XRF quantitative analysis of various samples, namely MoO<sub>3</sub>/MoS<sub>2</sub>@G-900, MoO<sub>3</sub>/MoS<sub>2</sub>@G-1000, MoO<sub>3</sub>/MoS<sub>2</sub>@G-1100 and MoO<sub>3</sub>/MoS<sub>2</sub>@G-1200 are shown in Table 2. From the XRD patterns, the graphite and MoS<sub>2</sub> materials do not show any change of crystalline structure after ball milling, while a reduction in the thickness of their flakes can be expected under the influence of the shear forces applied during the ball milling process. However, various phases can be detected in products obtained after the heat-treatment process at different temperatures, namely MoS<sub>2</sub> (PDF#03-065-0160), orthorhombic-MoO<sub>3</sub> (PDF#01-089-5108), monoclinic-MoO<sub>3</sub> (PDF#01-085-2405) and graphite (PDF# 01-075-2078).

Figures S1–S3 show high resolution XRD patterns of diffraction peaks corresponding to monoclinic and orthorhombic MoO<sub>3</sub> which are close to each other. In addition, Table S1 shows the intensity ratios of various phases in MoO<sub>3</sub>/MoS<sub>2</sub>@G-900, MoO<sub>3</sub>/MoS<sub>2</sub>@G-1000, MoO<sub>3</sub>/MoS<sub>2</sub>@G-1100 and MoO<sub>3</sub>/MoS<sub>2</sub>@G-1200. One observation from Figure 3 and Figures S1–S3 is that the monoclinic-MoO<sub>3</sub> (PDF#01-085-2405) could be formed only at 1200 °C. Moreover, the combination of Table S1 and Table 2 can lead to the conclusion that the amounts of sulfur, molybdenum, carbon and other elements in the samples heated at 900 and 1000 °C are nearly similar. In the samples heated at 1100 °C, however, the amount of sulfur is less, but the contents of other elements are more than those in the samples prepared at 900 and 1000 °C. Therefore, the amount of sulfur reaches to its maximum in the sample prepared at 1200 °C, while the proportions of other elements in this sample are the lowest among all samples.

Based on the observations mentioned above, it can be concluded that the content of MoS<sub>2</sub> gradually decreases, while the temperature is increased from 900 to 1100 °C. On the contrary, the content of MoO<sub>3</sub> gradually increases upon the temperature increase. When the temperature exceeds 1100 °C, the content of MoS<sub>2</sub> increases, leading to the assumption that MoO<sub>3</sub> would further transform into MoS<sub>2</sub>. The mechanism involved in this phase transition will be discussed in this paper. As the result, the maximum amount of MoO<sub>3</sub> could be achieved at the heating temperature of 1100 °C.

Further characterization of samples was performed using Raman spectroscopy, and the results are shown in Figure S4. For C-MoS<sub>2</sub>, the Raman spectrum shows two major  $E_{2g}^1$  (380 cm<sup>-1</sup>) and  $A_{1g}$  (406 cm<sup>-1</sup>) activation modes.  $E_{2g}^1$  is due to the in-plane vibration of S and Mo atoms, and  $A_{1g}$  is attributed to the relative vibration of S atoms in the out of plane direction. The other two relatively weak peaks observed at 285 and 450 cm<sup>-1</sup> belong to  $E_{1g}$  and longitudinal acoustic phonon mode in C-MoS<sub>2</sub>, respectively, as shown in Figure S4a. After the ball milling process, the  $E_{1g}$  peak of C-MoS<sub>2</sub> disappears, and the  $A_{1g}$ -LA (M)

peak is promoted. However, the structure of C-MoS<sub>2</sub> and natural graphite phase has no significant change, as shown in Figure S4a. The Raman spectra of the products obtained at various temperatures are shown in Figure S4b. As can be seen from Figure S4b, in addition to peaks related to graphite and MoS<sub>2</sub>, there are also peaks related to MoO<sub>3</sub>, which are marked with red asterisks on the spectrum of the sample prepared at 1100 °C. Therefore, Raman spectra confirm the formation of MoO<sub>3</sub>/MoS<sub>2</sub>@Graphene.



**Figure 3.** XRD patterns of various precursor materials and products: (a) the non-purified natural graphite material, (b) the commercial MoS<sub>2</sub>, (c) the mixture after ball milling; and (d–g) nanostructured materials obtained at various temperatures.

**Table 2.** XRF quantitative analysis of the MoO<sub>3</sub>/MoS<sub>2</sub>@G samples prepared at various temperatures.

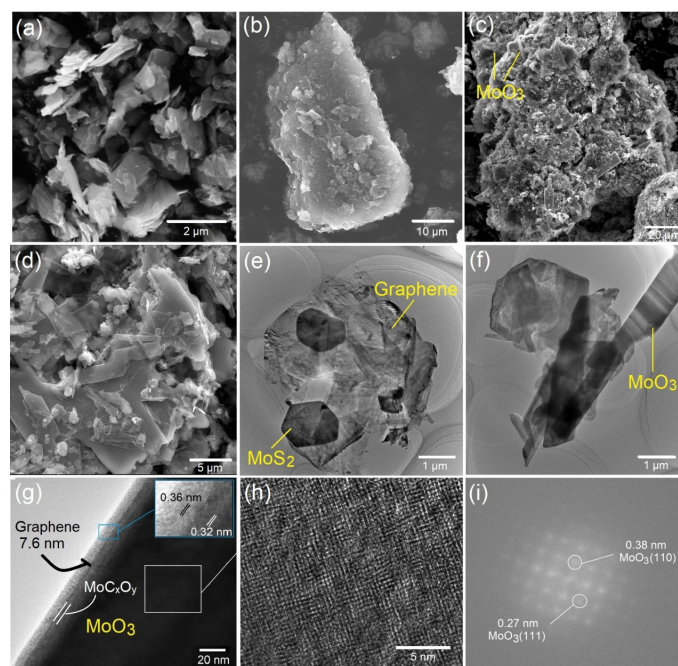
Sample	S	Mo	C	Si	Al	Fe	Ca	O
MoO <sub>3</sub> /MoS <sub>2</sub> @G-900	5.78	44.33	22.6	5.15	1.92	1.65	1.69	16.88
MoO <sub>3</sub> /MoS <sub>2</sub> @G-1000	5.59	45.18	23.3	6.36	2.42	1.15	1.74	14.26
MoO <sub>3</sub> /MoS <sub>2</sub> @G-1100	2.72	46.01	17.8	6.78	2.48	1.56	1.65	21.00
MoO <sub>3</sub> /MoS <sub>2</sub> @G-1200	10.2	48.48	15.6	5.96	2.07	1.82	1.18	14.69

On the other hand, the band gap energy indicates the energy required for the excitation of an electron to be moved from the valence band up to the conduction band. The Tauc method of evaluating the band gap using UV Vis spectroscopy was used to measure the values of the band gap, as shown in Figures S5 and S6 and Table S2. It can be concluded that the values of band gap energy gradually increase with the increase of the content of molybdenum trioxide. The reason behind this variation is based on the fact that MoO<sub>3</sub> is an n-type wide band gap ( $\approx 3$  eV) semiconductor [37], so the value of energy band gap in the sample produced in 1100 °C is the largest.

#### 2.4. SEM Characterization

To investigate the effects of the processing temperature on the morphology and microstructure of the nanocomposite materials prepared in this study, SEM characterization was carried out on commercial molybdenum disulfide (C-MoS<sub>2</sub>), natural graphite and products comprising of MoO<sub>3</sub>/MoS<sub>2</sub>@G-900, 1000, 1100, and 1200. The results are shown in Figure S7 and Figure 4. The SEM micrograph of C-MoS<sub>2</sub> is shown in Figure 4a, indicating that the material consists of irregularly-shaped flakes with the sizes of typically around 2  $\mu$ m. SEM micrograph of natural graphite (Figure 4b) shows the sample is made of agglomerated flakes with typical sizes of several tens of micrometers. These two materials in combination with NaCl were used to fabricate MoO<sub>3</sub>/MoS<sub>2</sub>@G samples. As shown in Figure S7b–g, the morphology of the synthesized materials is different from those of starting material due to the formation of molybdenum oxides, hexagonal MoS<sub>2</sub> and graphene nanosheets. In MoO<sub>3</sub>/MoS<sub>2</sub>@G-900, the presence of orthorhombic-MoO<sub>3</sub> was already confirmed based on XRD analysis of Figure 3c. The oxide phase can be distinguished in Figure S7b as crystals with sizes of around 1  $\mu$ m, scattered within natural graphite and MoS<sub>2</sub> flakes. The presence of orthorhombic-MoO<sub>3</sub> is attributed to the partial oxidation of MoS<sub>2</sub>, leading to the formation of the molybdenum oxide and gaseous sulfur dioxide, under the influence of atmospheric air. According to Figure 2, as the temperature increases to 1000 °C, MoS<sub>2</sub> is almost fully oxidized into orthorhombic-MoO<sub>3</sub>. Moreover, the dimensions of resulting oxide are increased to form rod-like particles with dimensions in range of around 5–30  $\mu$ m, as shown in Figure S7c. The directional growth of orthorhombic-MoO<sub>3</sub> particles may lie on the preferential growth occurred along the-(001) direction in the orthorhombic structure of MoO<sub>3</sub>, as further observed in TEM micrograph of Figure S8. By increasing the temperature to 1100 °C, the MoO<sub>3</sub> nanoribbons could grow even further, to form sheet-like particles with dimensions of around 50  $\mu$ m, as shown in Figure S7d and Figure 4c,d. This observation suggests that at 1100 °C, other crystallographic directions in the orthorhombic lattice of MoO<sub>3</sub> nanoribbons contribute to the growth phenomenon observed, forming sheet-like particles, which is in contrast to the rod-like particles observed in Figure S7c.

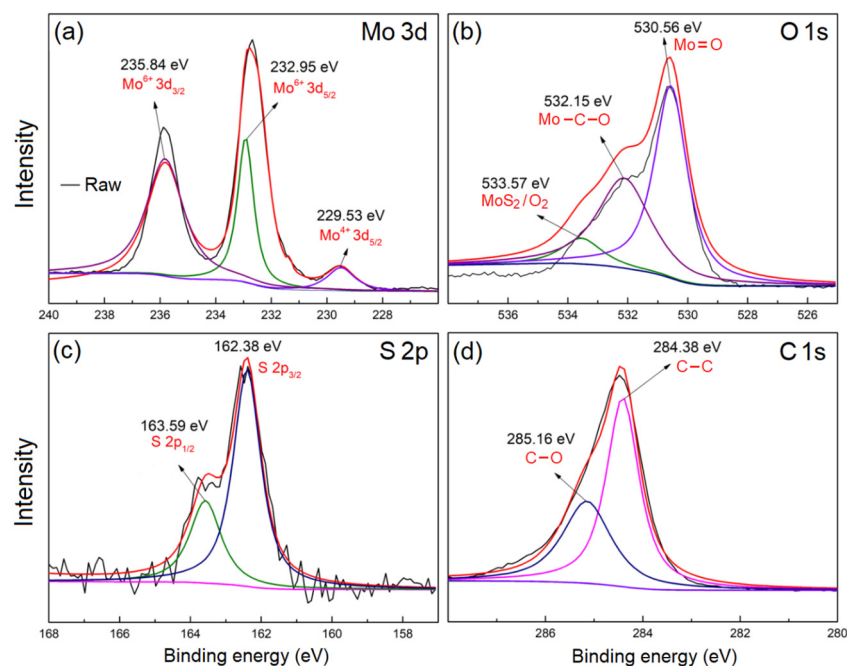




**Figure 4.** SEM micrographs of (a) commercial  $\text{MoS}_2$ , (b) natural graphite, and (c,d)  $\text{MoO}_3/\text{MoS}_2@\text{G-1100}$ . (e–h) TEM micrographs of  $\text{MoO}_3/\text{MoS}_2@\text{G-1100}$ . (i) FFT pattern recorded on the micrograph (h).

According to Figure S7e,f, by raising the temperature to 1200 °C, large-sized  $\text{MoO}_3$  crystals observed in Figure S7d disappear, and instead, a large number of hexagonally-shaped  $\text{MoS}_2$  crystals form. This morphological evolution may be described based on the possible reaction between the natural graphite flakes and sulfur dioxide released by the oxidation of the original  $\text{MoS}_2$  flakes, leading to the formation of elemental sulfur. Then, sulfur formed reacts on the surface of  $\text{MoO}_3$  nanoribbons particles to form hexagonal  $\text{MoS}_2$  nanosheets. As exhibited from Figure S7f, the hexagonal  $\text{MoS}_2$  nanosheets grow from the surface of the  $\text{MoO}_3$  nanoribbons particles, possibly, by replacing the oxygen of  $\text{MoO}_3$  with S [28]. The size of hexagonal  $\text{MoS}_2$  nanosheets is typically less than around 2  $\mu\text{m}$ , as shown in the high-magnification image of Figure S8g. Figure S7h shows the EDS analysis recorded on the hexagonal  $\text{MoS}_2$  nanosheet shown in Figure 5, providing further evidence for the nature of such hexagonal crystals.

The in-situ formation of hexagonal  $\text{MoS}_2$  nanosheets on the surfaces of  $\text{MoO}_3$  nanoribbons leads to the disintegration of the  $\text{MoO}_3$  into smaller particles, as can be observed in SEM micrographs of Figure S7e,f. This phenomenon also causes the phase transition of  $\text{MoO}_3$  from the orthorhombic crystalline structure ( $\alpha\text{-MoO}_3$ ) to the monoclinic modification ( $\beta\text{-MoO}_3$ ), as shown in Figure 2f. This hypothesized mechanism will be discussed further in next sections in this article. The combination of XRD and XRF analyses suggested that the  $\text{MoO}_3$  content of the samples reaches its maximum value at 1100 °C. This behavior can be related to the action of molten NaCl to protect the  $\text{MoO}_3$  particles from being excessively converted into hexagonal- $\text{MoS}_2$  nanosheets at 1100 °C, while this temperature allows the maximum oxidation of the original  $\text{MoS}_2$  into  $\text{MoO}_3$  nanoribbons. Considering the higher contentment of  $\text{MoO}_3$  in the sample prepared at 1100 °C, the Li-ion storage capacity of this sample is expected to be greater than other samples, and this will be shortly discussed later in this article.



**Figure 5.** High resolution XPS spectra of MoO<sub>3</sub>/MoS<sub>2</sub>@G-1100, around (a) Mo 3d, (b) O 1s, (c) S 2p, and (d) C 1s peaks.

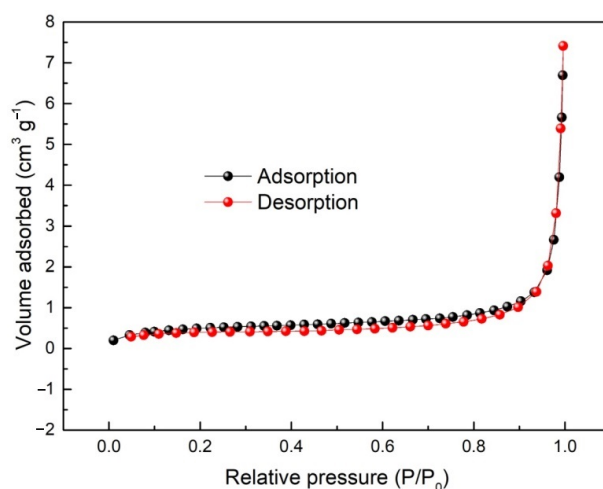
### 2.5. TEM Characterization

As observed in Figure 4c,d, the SEM morphology of MoS<sub>2</sub>-MoO<sub>3</sub>@G-1100 could be characterized by the presence of agglomerated nano-entities. TEM studies were performed to further investigate this morphology, and the results are shown in Figure 4e–i, where the presence of hexagonal MoS<sub>2</sub> nanoflakes ( $\approx 1 \mu\text{m}$ ), graphene nanosheets and  $\alpha$ -MoO<sub>3</sub> nanoribbons ( $W \approx 400\text{--}800 \text{ nm}$ ;  $L > 10 \mu\text{m}$ ) can be realized. The formation of such nanoribbons can be related to the presence of oxygen vacancies on the surface of MoO<sub>3</sub> crystals, providing the driving force for the solid-phase growth of oxides into nanoribbons [38,39]. The MoO<sub>3</sub> nanoribbons appears to be formed as the result of dominant crystal growth along the [001] direction, as shown in Figure S8. In TEM images, the presence of graphene nanosheets (originating from the natural graphite material) combined with hexagonal MoS<sub>2</sub> nanoflakes and MoO<sub>3</sub> nanoribbons is evident. Figure 4g–i provide further insights into the interface between graphene and MoO<sub>3</sub>. Figure 4g shows a MoO<sub>3</sub> nanoribbon, where the presence of a graphene layer with the thickness of around 7.6 nm on its surface can be seen. The high magnification TEM image shown as the inset of Figure 4g shows the presence graphene layers with the interlayer spacing of 0.36 nm, representing (002) planes of hexagonal carbon. In addition, toward the bulk of sample, the interlayer spacing of 0.32 nm can be assigned to the (021) crystalline planes of orthorhombic-MoO<sub>3</sub>. Moreover, there is an amorphous interface between the graphene nanosheets and MoO<sub>3</sub> which could be assigned to molybdenum oxycarbide formed during the molten salt processing of the sample. Formation of this interfacial phase will be further discussed by XPS analysis in this article. Figure 4h shows a high resolution TEM micrograph recorded on the MoO<sub>3</sub> nanoribbons, where the crystalline structure of the materials can clearly be observed. Figure 4i exhibits the fast Fourier transform (FFT) recorded on the micrograph of Figure 4h, where the spots related to the crystalline planes of orthorhombic-MoO<sub>3</sub> are indexed. Overall, XRD, SEM and TEM analyses suggest the formation of nanostructured MoO<sub>3</sub>/MoS<sub>2</sub>@G-1100, in which orthorhombic-MoO<sub>3</sub> nanoribbons, hexagonal MoS<sub>2</sub> nanoflakes and graphene nanosheets are well-integrated. The presence of interfacial molybdenum oxycarbide was also suggested.

## 2.6. Surface Characterization

The structural and microstructural characterizations mentioned above could demonstrate the formation of MoO<sub>3</sub> nanoribbons incorporated into hexagonal MoS<sub>2</sub> and graphene. The Li-ion storage performance of the products will be evaluated shortly in this article. However, before that, it would be interesting to shed light on to nature of the interface between the above mentioned phases. This was examined using XPS analysis, as shown in Figure 5. As can be observed, the characteristic peaks of Mo, O, S and C are debatable in the XPS spectrum of MoO<sub>3</sub>/MoS<sub>2</sub>@G-1100. High-resolution XPS spectra obtained on Mo 3d, O 1s and S 2p peaks are exhibited Figure 5a–c. As observed, the strong peak at 229.53 eV corresponds to Mo<sup>4+</sup> 3d<sub>3/2</sub>, and peaks at about 163.1 eV and 161.5 eV to S 2p<sub>1/2</sub> and S 2p<sub>3/2</sub>, respectively, revealing the existence of MoS<sub>2</sub> [40,41]. On the other hand, the peaks located at 235.79, 232.95, 530.56 and 532.15 eV correspond to the Mo<sup>6+</sup> 3d<sub>3/2</sub>, Mo<sup>6+</sup> 3d<sub>5/2</sub>. These peaks together with that appeared at 530.65 eV (corresponding to O1s components) indicate the presence of MoO<sub>3</sub> [27]. Moreover, the C 1s core level shown in Figure 5d could be deconvoluted into two peaks at 284.38 and 285.16 eV, which originate from the C–C and C–O bonds, respectively [41]. The presence of C–C bond is related to the graphene nanosheets, and C–O bond to the local interaction between graphene nanosheets and MoO<sub>3</sub>.

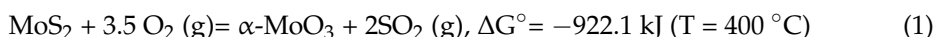
Moreover, the presence of peak at 532.15 eV in Figure 5b indicates the presence of Mo–O–C [42] corresponding to the formation of interfacial molybdenum oxycarbide (MoC<sub>x</sub>O<sub>y</sub>) at the interface between MoO<sub>3</sub> and graphene nanosheets, as also suggested by the TEM micrograph of Figure 4g. Density functional theory calculations have confirmed the possibility of formation of molybdenum oxycarbide by reacting between zeolite-supported Mo and CO<sub>2</sub> [43]. Zhu et al. [42] suggested that MoO<sub>x</sub>C<sub>y</sub> can be formed from MoO<sub>3</sub>, when vacancies available on the surface of MoO<sub>3</sub> are filled by carbon atoms. In our case, MoO<sub>3</sub> nanoribbons are wrapped with graphene nanosheets (Figure 4). Under this condition, the diffusion of carbon atoms into the surface of MoO<sub>3</sub> at high-temperatures such as 1100 °C is possible, leading to the formation of interfacial MoO<sub>x</sub>C<sub>y</sub>. It should be mentioned that molybdenum oxycarbide is generally considered to possess low electrical resistivity of 3 μΩm at room temperature [44]. The interfacial molybdenum oxycarbide is likely to promote the electrochemical performances of the nanostructured materials. This will be discussed later in this article. The well-incorporated phases in MoO<sub>3</sub>/MoS<sub>2</sub>@G-1100, and the possible presence of interfacial molybdenum oxycarbide, can lead to the reduced specific surface area (1.74 m<sup>2</sup> g<sup>−1</sup>) and pore volume (0.008 cm<sup>3</sup> g<sup>−1</sup>). In agreement with these observations, the nitrogen adsorption–desorption isotherms of MoO<sub>3</sub>/MoS<sub>2</sub>@G-1100, shown in Figure 6, provide features corresponding to the type III isotherms, characteristic of the non-porous materials [45].



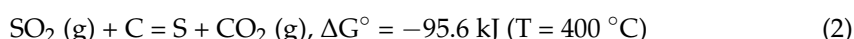
**Figure 6.** Nitrogen adsorption–desorption isotherms of MoO<sub>3</sub>/MoS<sub>2</sub>@G-1100.

## 2.7. Catalytic Formation of Hexagonal MoS<sub>2</sub> Nanocrystals and $\alpha$ -MoO<sub>3</sub>

In this research, commercially-available MoS<sub>2</sub> flakes and natural graphite mineral were utilized as the initial material, and the product contained hexagonal MoS<sub>2</sub> nanocrystals. The conversion of flake MoS<sub>2</sub> into hexagonal nanocrystals is an interesting phenomenon discussed in this section. It is known that MoS<sub>2</sub> flakes start to oxidize at around 400 °C, leading to the formation of orthorhombic molybdenum trioxide ( $\alpha$ -MoO<sub>3</sub>) [46]. Therefore, the thermochemical reactions occurred in the process initiates with the formation of  $\alpha$ -MoO<sub>3</sub> through the involvement of oxygen from the atmosphere:



In the presence of graphite, the SO<sub>2</sub> gas formed based on the reaction (1) is likely to be fixed by graphite flakes to generate elemental sulfur and carbon dioxide gas, as shown in Equation (2).



The combination of reactions (1) and (2) can lead to the reaction (3):



The generated elemental sulfur adhered to the surface of MoO<sub>3</sub> is likely to in-situ reduce the MoO<sub>3</sub> into hexagonal MoS<sub>2</sub> nanocrystals:



The reactions (1)–(4) demonstrates the thermodynamic possibility of the formation of  $\alpha$ -MoO<sub>3</sub> and hexagonally shaped MoS<sub>2</sub> at temperatures greater than 400 °C initiating with the oxidation of MoS<sub>2</sub>. In this research, the heating process was performed at temperatures above the melting point of NaCl. Therefore, the molten salt is likely to exfoliate the graphite flakes [47,48]. The formation of graphene nanosheets is evident from the TEM micrographs of Figure 4 and Figure S7. Figure S13 illustrates the possible mechanism involved in the catalytic formation of hexagonal MoS<sub>2</sub> nanocrystals and MoO<sub>3</sub> observed in this study.

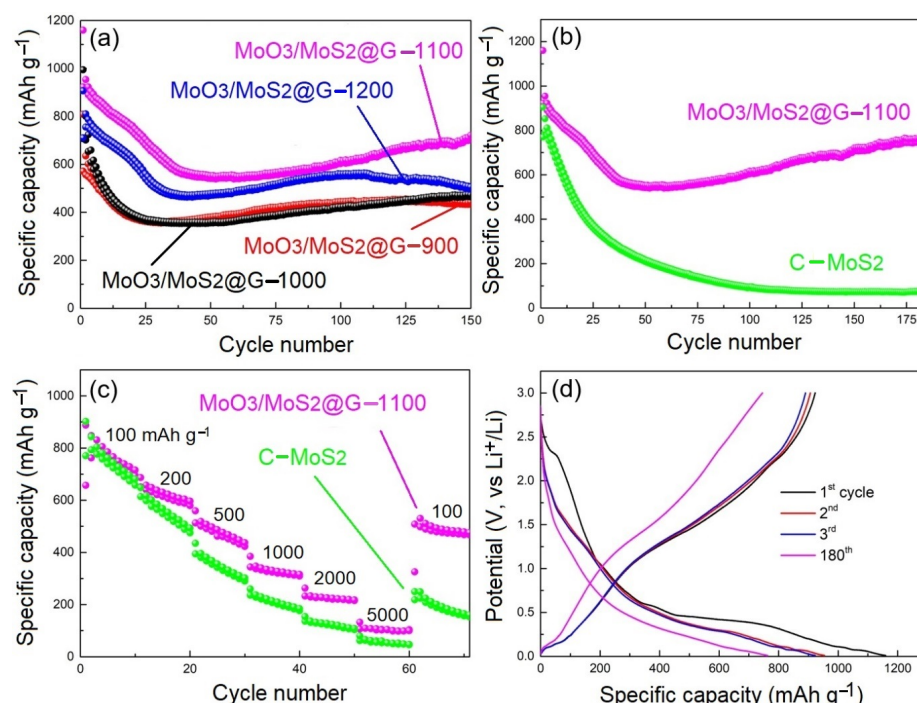
To highlight the role of NaCl in the process, the sample prepared at 1100 °C was washed to remove its NaCl content, and the product (MoO<sub>3</sub>/MoS<sub>2</sub>@G-1100) was heated to 1200 °C for 5 min, without the involvement of NaCl. The appearance and X-ray diffraction pattern of the resulting sample are shown in Figures S9 and S10, respectively, providing evidence that the sample heated at 1200 °C mainly contains molybdenum oxide, without the participation of molten NaCl. In this case, carbon and molybdenum disulfide content of the sample are oxidized during the heat-treatment process to form molybdenum oxide and gas species at high temperature.

It should be mentioned that oxidation in air of graphitic carbon materials typically occurs at temperatures in the range 400–800 °C, depending on their grain size, level of crystallinity and presence of impurities that can catalyze the oxidation process [49,50] leading to the formation of gashouse species and ash. It is known that the oxidation of bulk and few-layer MoS<sub>2</sub> flakes does not readily take place at ambient conditions due to the high energy barrier involved [51–54]. However, non-isothermal oxidation of MoS<sub>2</sub> flakes initiates at temperatures as low as 350 °C with a limited rate, and increases by enhancing the temperature under an apparent activation energy of  $\approx 1$  kcal/mol, representing the bulk oxidation event. The oxidation process leads to the increase of the molybdenum oxide content (typically MoO<sub>3</sub>), by increasing the temperature [55,56]. This is in agreement with our observation exhibited in Figure S10. Based on the observations mentioned above, the presence of NaCl provides an essential support toward the formation of MoO<sub>3</sub>/MoS<sub>2</sub>@G samples at high temperatures. First, molten NaCl provides an ionic environment to enhance the chemical reactions, while preventing the oxidation of species and supporting the exfoliation of graphite into graphenene nanosheets; the latter is discussed elsewhere [57].

## 2.8. Electrochemical Characterization of MoO<sub>3</sub>/MoS<sub>2</sub>@G Samples

We further investigated the Li-ion storage performances of MoO<sub>3</sub>/MoS<sub>2</sub>@G samples prepared at various temperatures, namely MoO<sub>3</sub>/MoS<sub>2</sub>@G-900, -1000, -1100 and -1200 in comparison with those of the initial commercial MoS<sub>2</sub> flakes, named as C-MoS<sub>2</sub>. In the half-cell configuration, the driving force for the Li-ion insertion/extraction into/out of the electrode during the discharge/charge processes is provided by the negative/positive polarization applied on the electrode, respectively.

The electrochemical performances of the electrodes are shown in Figure 7. The electrodes were fabricated using the water-based polystyrene acrylic-acrylate as the binder, as explained in the Experimental section. Figure 7a shows the cycle performances of MoO<sub>3</sub>/MoS<sub>2</sub>@G electrodes, and selected outcomes are summarized in Table 3. As can be seen, MoO<sub>3</sub>/MoS<sub>2</sub>@G-1100 electrode shows a greater initial coulombic efficiency (CE) of 79.58% compared with other electrodes. After 100 cycles, this electrode exhibits a reversible capacity of 616.3 mAh g<sup>-1</sup> at 100 mA g<sup>-1</sup>.



**Figure 7.** Li-ion storage performances of various electrodes. (a) Cycle performance of various electrodes. (b) Cycle performance, and (c) rate performance of C-MoS<sub>2</sub> in contrast with those of MoO<sub>3</sub>/MoS<sub>2</sub>@G-1100. (d) Potential-capacity curve of MoO<sub>3</sub>/MoS<sub>2</sub>@G-1100 electrode. All measurements were recorded at 100 mA g<sup>-1</sup>, unless indicated otherwise.

**Table 3.** The electrochemical performance of commercial MoS<sub>2</sub> (C-MoS<sub>2</sub>) in comparison with those of MoO<sub>3</sub>/MoS<sub>2</sub>@G nanostructured materials.

Electrode	Initial Coulombic Efficiency (%)	Specific Capacity after 100 Cycles (mAh/g)	Specific Capacity after 150 Cycles (mAh/g)
C-MoS <sub>2</sub>	85.13	94.8	73.5
MoO <sub>3</sub> /MoS <sub>2</sub> @G-900	70.64	444.1	442.8
MoO <sub>3</sub> /MoS <sub>2</sub> @G-1000	71.13	422.2	472.7
MoO <sub>3</sub> /MoS <sub>2</sub> @G-1100	79.58	616.3	721.2
MoO <sub>3</sub> /MoS <sub>2</sub> @G-1200	78.36	560.1	505.9



The performance MoO<sub>3</sub>/MoS<sub>2</sub>@G-1200 electrode can be evaluated to be greater than those of -900 and -1000 electrodes, but lower than that of -1100. The greater performance of MoO<sub>3</sub>/MoS<sub>2</sub>@G-1100 can be attributed to the greater amount of MoO<sub>3</sub> in this sample as realized from Figure 2 and Table 2. The other point that deserves attention is that by increasing the temperature to 1200 °C, the amount of MoO<sub>3</sub> in the sample reduces to reach its minimum among all samples, as evidenced from the relative low intensity of MoO<sub>3</sub> reflections observed in Figure 3. Despite having the minimum amount of MoO<sub>3</sub>, the performance of the electrode is greater than samples prepared at 900 and 1000 °C. This observation can be assigned to the formation of β-MoO<sub>3</sub> with monoclinic crystalline structure at 1200 °C. This is known that the metastable β-MoO<sub>3</sub> has a highly ionically conductive open-structure [41], enhancing the electrochemical performance of MoO<sub>3</sub>/MoS<sub>2</sub>@G-1200, despite the lower MoO<sub>3</sub> content of the sample.

As can be seen in Figure 7d, the first discharge/charge specific capacity of MoO<sub>3</sub>/MoS<sub>2</sub>@G-1100 is recorded at 1159.6 mAh g<sup>-1</sup>/953.8 mAh g<sup>-1</sup> (coulombic efficiency = 79.58%). This capacity loss can mostly be related to the generation of solid electrolyte interphase (SEI) layers on the electrode. The specific reversible capacity of the electrode could still be recorded at 773.5 mAh g<sup>-1</sup> after 180 cycles, as exhibited in Figure 7d. Figure S11 shows the durability of MoS<sub>2</sub>/MoO<sub>3</sub>/G-1100 sample in lithium-ion battery. As seen, the specific capacity after 400 cycles is still maintained at 240 mAh g<sup>-1</sup> under the current density of 500 mA g<sup>-1</sup>.

Figure 8 shows the CV curve of the MoO<sub>3</sub>/MoS<sub>2</sub>@G-1100 electrode, providing detailed information about the Li-ion insertion and extraction processes. During the first cathodic scan, there is a cathodic peak at 0.56 V. This cathodic event cannot be observed in the subsequent cycles, providing evidence that this peak mainly corresponds to the formation of SEI. Moreover, the presence redox peaks at 1.56/1.76 V and 1.25/1.48 V in the first cycle can be related to the lithiation and delithiation of MoO<sub>3</sub>, and to the metallization/oxidation of metallic molybdenum:

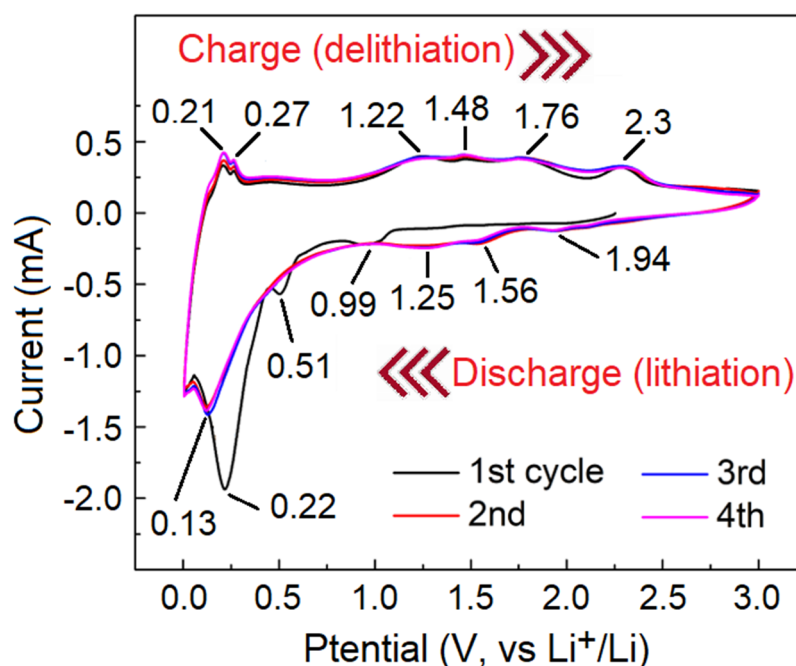
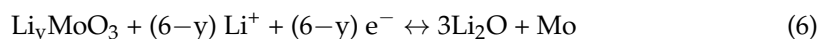
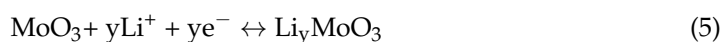
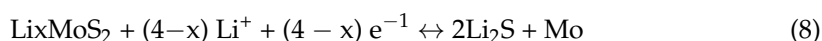
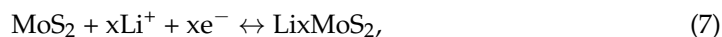


Figure 8. CV curve of MoO<sub>3</sub>/MoS<sub>2</sub>@G-1100 electrode recorded at 0.5 mV/s.

Moreover, the cathodic peak at 1.94 V might be attributed to the conversion from  $S_8$  to  $Li_2S$ , and the oxidation peak at 2.3 V to the decomposition of  $Li_2S$  [58,59]. On the other hand, the redox peaks at 0.99/1.22 V corresponded to the following electrochemical reactions [60]:



Furthermore, the reduction/oxidation peaks at 0.21/0.22 V are related to adsorption/desorption of lithium ion on the surfaced of graphene nanosheets [61]. Overall, in agreement with Figure 7d, the CV curve of Figure 8 provides evidence for the electrochemical contribution of all the components of the electrode to the Li-ion storage performance observed.

## 2.9. Impedance Spectroscopy and Electrode Kinetics

Impedance spectroscopy performed on  $MoO_3/MoS_2@G$  and C- $MoS_2$ . Figure 9a exhibits the Nyquist plots of the electrode. The plots show a semicircle in the high frequency range. The diameter of this semicircle can be related to the charge-transfer resistance ( $R_{ct}$ ). In the low frequency range, the plots also show sloping straight lines. This part reflects the diffusion characteristics of lithium ions within the electrode [62]. The electrode made of  $MoO_3/MoS_2@G-1100$  exhibits a smaller semi-circle diameter (40.71  $\Omega$ ) than other samples, namely -900, -1000, -1200 and C- $MoS_2$ ; 63.65, 53.65, 62.9 and 263.8  $\Omega$ , respectively. This indicates the higher charge transfer resistance in the latter. The smaller electrochemical resistance observed in the  $MoO_3/MoS_2@G-1100$  is consistent with the micrographs of Figure 4, indicating to the presence of integrated components with interfacial molybdenum oxycarbide that reduces the interfacial resistance across the sample.

The Li-ion diffusion ( $D_{Li}$ ) involved in the electrochemical process discussed above can be calculated as follows [63]:

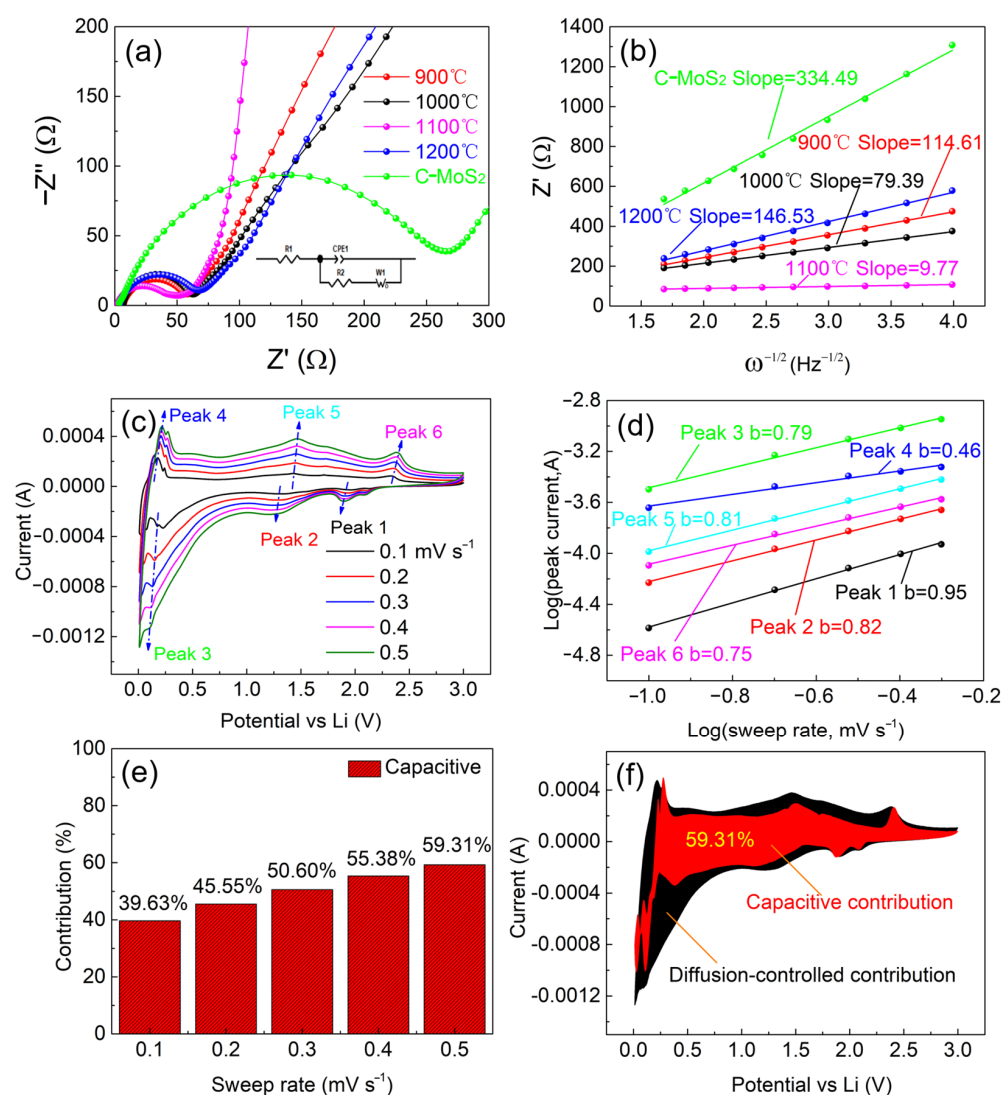
$$D_{Li} = \frac{R^2 T^2}{2A^2 n^4 F^4 C^2 \sigma^2} \quad (9)$$

Here, R and F represent the gas and Faraday constants, respectively, T is temperature (298 K) and n is the number of participating electrons ( $n = 1$ ). C represents the concentration of  $Li^+$ . The electrode surface area of the electrode (A) was calculated based on the diameter of the electrode (1.1  $cm^2$ ). Moreover,  $\sigma$  represents the Warburg factor which is determined based on the slope of the line  $Z' \sim \omega^{-1/2}$  shown in Figure 9b, considering that  $\omega = 2\pi f$  ( $f$  = frequency, Hz). The kinetic parameters of the electrode were determined from the equivalent circuit fitting of Nyquist plots (Figure 9a), and shown in Table 4. At low values of frequency, the  $MoO_3/MoS_2@G-1100$  electrode exhibits a high slope (9.77  $\Omega s^{-1/2}$ ) which demonstrates the relatively high lithium ion diffusion coefficient [64]. The lithium ion diffusion coefficient of  $MoO_3/MoS_2@G-900$ , -1000, -1100, -1200 and C- $MoS_2$  electrodes could be calculated to be  $8.7 \times 10^{-21}$ ,  $1.8 \times 10^{-20}$ ,  $1.2 \times 10^{-18}$ ,  $5.3 \times 10^{-21}$  and  $1.0 \times 10^{-21}$ , respectively. The larger  $D_{Li}$  in the earlier can be related to the shorter diffusion pathways available in the electrode, brought about by the presence of integrated hexagonal  $MoS_2$  nanocrystals and graphene nanosheets as shown in Figure 4.

**Table 4.** Electrode kinetic parameters for the  $MoO_3/MoS_2@G$  and C- $MoS_2$  electrodes.

Sample	$R_e$ ( $\Omega$ )	$R_{ct}$ ( $\Omega$ )	$\sigma$ ( $\Omega s^{-1/2}$ )	$D_{Li}$ ( $cm^2 s^{-1}$ )
$MoO_3/MoS_2@G-900$	6.90	63.65	114.61	$8.7 \times 10^{-21}$
$MoO_3/MoS_2@G-1000$	6.56	53.56	79.39	$1.8 \times 10^{-20}$
$MoO_3/MoS_2@G-1100$	2.21	40.71	9.77	$1.2 \times 10^{-18}$
$MoO_3/MoS_2@G-1200$	3.92	62.9	146.53	$5.3 \times 10^{-21}$
C- $MoS_2$	3.56	263.8	334.49	$1.0 \times 10^{-21}$





**Figure 9.** (a) AC impedance spectra of  $\text{MoO}_3/\text{MoS}_2@\text{G}$  and  $\text{C-MoS}_2$  electrodes. (b) The values of  $Z'$  vs.  $\omega^{-1/2}$  ( $\omega = 2\pi f$ ) for  $\text{MoO}_3/\text{MoS}_2@\text{G}$  and  $\text{C-MoS}_2$ . (c–f): Contribution of pseudocapacitive Li-ion storage to the total capacity of the  $\text{MoO}_3/\text{MoS}_2@\text{G-1100}$  electrode: (c) CV curves with scan rates ranging 0.1 to 0.5  $\text{mV s}^{-1}$ ; (d) the logarithmic dependence between the peak current and sweep rate; (e) contribution of pseudocapacitive and diffusion-based processes to the total current at different sweep rates, and (f) the pseudocapacitive contribution at 0.5  $\text{mV s}^{-1}$ .

## 2.10. Contribution of Diffusion- and Surface-Phenomena

We also evaluated the contribution of diffusion- and surface-phenomena to the overall Li-ion storage performance of the  $\text{MoO}_3/\text{MoS}_2@\text{G-1100}$  electrode. Figure 9c exhibits CV curves recorded on the electrode at various scan rates from 0.1 to 0.5  $\text{mV s}^{-1}$ . It should be mentioned that the current intensity ( $i$ ) and the sweep rate ( $v$ ) can be related by Equations (10) and (11) [65]:

$$i = a \times v^b \quad (10)$$

$$\log i = \log a + b \times \log v \quad (11)$$

Here,  $a$  and  $b$  are dimensionless variables. Figure 9d could be established by plotting the logarithmic dependence between the current values related to various peaks shown in Figure 9c and the corresponding values of sweep rates. Based on the results obtained, the relative contributions of pseudocapacitive (vs. the diffusion-controlled events)

to the total current could be found to be in the range 39–60% at different sweep rates, as exhibited in Figure 9e.

It can be seen that the contribution of pseudocapacitive processes to the total current is proportional to the scan rate: higher scan rate, the greater contribution. As such, the pseudocapacitive contribution can directly influence the high-rate performance of the electrode, as shown in Figure 7c. Figure 9f exhibits the pseudocapacitive contribution to the total current at  $0.5 \text{ mV s}^{-1}$ .

Moreover, in Equation (11), the  $b$  value depends on the Li-ion storage mechanism. The value of  $b = 0.5$  represents a diffusion-dominated process, while  $b = 1$  represents the pseudocapacitive processes. The  $b$  values between 0.5 and 1 represent process involving both pseudocapacitive and diffusion-based process with various contribution ratio depending of the  $b$ -value [66,67]. As can be seen from Figure 9d, the value of  $b$  for the peaks 1, 2, 3, 4, 5, and 6 are obtained to be 0.95, 0.82, 0.79, 0.46, 0.81 and 0.75, respectively. It confirms that all current peaks are mainly dominated by pseudocapacitive processes, unless the anodic peak 4 with the  $b$  value of 0.46, representing diffusion based processes. The pseudocapacitive-oriented nature of the peaks mentioned above can be explained based of the integrated nanostructure of the sample (Figure 4) that promotes the Li-ion diffusion and charge transfer the electrode/electrolyte interfaces across the electrode. In contrast, the anodic peak 4 located at 0.20 V, with the  $b$ -value of 0.46, corresponds to de-intercalation of  $\text{Li}^+$  out of the thicker graphitic flakes present in the sample.

### 3. Discussion

We have successfully developed a green, simple process for the conversion of the abundant and low-cost natural graphite and widely available  $\text{MoS}_2$  into nanostructured  $\text{MoO}_3/\text{MoS}_2@\text{Graphene}$ . In this process, the oxidation of  $\text{MoS}_2$  in the presence of graphite leads to the formation of  $\alpha\text{-MoO}_3$  with orthorhombic crystalline structure, as well as hexagonal  $\text{MoS}_2$  nanocrystals. At 900 and 1000 °C, the molten salt promotes the catalytic exfoliation of the natural graphite into graphene nanosheets, incorporated with hexagonal  $\text{MoS}_2$  crystals and  $\alpha\text{-MoO}_3$ , denoted as  $\text{MoO}_3/\text{MoS}_2@\text{G-900}$ , and -1000, respectively. The further development of  $\text{MoS}_2$  oxidation at 1100 °C, resulted in the formation of  $\text{MoO}_3/\text{MoS}_2@\text{G-1100}$ , containing the maximum amount of  $\text{MoO}_3$  among all samples. The highest amount of  $\text{MoO}_3$  in this sample combined with the presence of integrated graphene nanosheets and hexagonal  $\text{MoS}_2$  provide the sample with the greatest value of Li-ion storage capacity about  $773.5 \text{ mAh g}^{-1}$  after 180 cycles at a current density of  $100 \text{ mA g}^{-1}$ . The formation of molybdenum oxycarbide between  $\text{MoO}_3$  and graphene nanosheets was suggested as the cause of reduced charge-transfer resistance ( $53.56 \Omega$ ).

At the processing temperature of 1200 °C, the content of  $\text{MoO}_3$  is the minimum among all samples, but the electrochemical performance of the sample ( $\text{MoO}_3/\text{MoS}_2@\text{G-1200}$ ) is second only to that of the sample prepared at 1100 °C, with a Li-ion storage capacity of about  $505.9 \text{ mAh g}^{-1}$  after 180 cycles at a current density of  $100 \text{ mA g}^{-1}$  (Table 3). Interestingly, the high Li-ion storage capacity of the sample prepared at 1200 °C was corresponded to the formation of thermodynamically metastable monoclinic molybdenum trioxide ( $\beta\text{-MoO}_3$ ), instead of conventional orthorhombic  $\alpha\text{-MoO}_3$  which appears at 900–1100 °C.  $\beta\text{-MoO}_3$  is known to have a highly ionically conductive open structure [41], improving the electrochemical performance of the material. Selected number of methods employed in the literature for the preparation of molybdenum compounds, and their electrochemical performances are compared with those of  $\text{MoO}_3/\text{MoS}_2@\text{G-1100}$  in Table 5. Methods shown in this table typical use expensive and/or hazardous materials such as  $(\text{NH}_4)_6\text{Mo}_7\text{O}_{24}\cdot 4\text{H}_2\text{O}$  [27,28],  $\text{MoO}_3$  [29],  $(\text{NH}_4)_2\text{MoO}_4$  [32], and metallic Mo powders [33], in combination with materials such as  $\text{CH}_4\text{N}_2\text{S}$  [27],  $\text{HNO}_3$  [28], glacial acetic acid [29],  $\text{HCl}$  [32], and  $\text{H}_2\text{O}_2$  [33]. The excessive use of such chemicals limits the large-scale implementation of these methods. In the method reported here, ball milling is applied to incorporate natural graphite and  $\text{MoS}_2$  in the presence of hexane and  $\text{NaCl}$ . Both hexane and  $\text{NaCl}$  can be retrieved from the mixture after ball-milling, and the final washing step,

respectively. Nevertheless, the method reported here requires heating at elevated temperatures which might provide some limitations. Utilization of industrial heat waste can be an option to enhance the economic features of the method.

**Table 5.** A comparison between selected MoO<sub>3</sub>/MoS<sub>2</sub> materials extracted from the literature, and MoO<sub>3</sub>/MoS<sub>2</sub>@G-1100 prepared here, in terms of the precursor materials, preparation method, and the electrochemical performance.

Mo-Oxide Based Material	Precursor Materials	Preparation Process	Performance
			Capacity (mAh/g)/Cycle/Current Density (mA/g)
Core–sheath structured MoO <sub>3</sub> @MoS <sub>2</sub> composite [23]	Rhododendron petals, (NH <sub>4</sub> ) <sub>6</sub> Mo <sub>7</sub> O <sub>24</sub> ·4H <sub>2</sub> O, CH <sub>4</sub> N <sub>2</sub> S	In situ growth at 550 °C (2 h) + 180 °C (24 h)	400/30th/200
Ternary MoS <sub>2</sub> /MoO <sub>3</sub> /C nanosheets [24]	Organic amine, MoO <sub>3</sub>	CVD at 800 °C (3 h) under N <sub>2</sub>	961.4/120th/430
MoO <sub>3</sub> /MoS <sub>2</sub> nanoribbons [25]	Molybdic acid, glacial acetic acid	Hydrothermal treatment at 800 °C (30 min)	-
MoS <sub>2</sub> /MoO <sub>3</sub> nanosheets [26]	CdCl <sub>2</sub> , (NH <sub>4</sub> ) <sub>2</sub> CS, (NH <sub>4</sub> ) <sub>2</sub> MoO <sub>4</sub> , NH <sub>2</sub> OH.HCl	Hydrothermal treatment at 180 °C (30 h)	-
MoS <sub>2</sub> coated MoO <sub>3</sub> nanobelts [27]	Mo metal powder 10 mL H <sub>2</sub> O <sub>2</sub>	Hydrothermal treatment at 180 °C (12 h)	1400/50th/100
MoS <sub>2</sub> nanosheets on MoO <sub>3</sub> nanowires [28]	(NH <sub>4</sub> ) <sub>6</sub> Mo <sub>7</sub> O <sub>24</sub> ·4H <sub>2</sub> O, HNO <sub>3</sub> , thiourea	Hydrothermal treatment at 180 °C (24 h)	800/100th/100
Core-shell MoO <sub>3</sub> /MoS <sub>2</sub> nanowires [29]	MoO <sub>3</sub> powders, sulfur, N <sub>2</sub>	Thermal treatment at 700 °C	
MoS <sub>2</sub> /MoO <sub>3</sub> @graphene [This work]	MoS <sub>2</sub> , natural graphite, NaCl	Heating at 1100 °C (20 min)	316/40th/1000
			774/180th/100

In this research, the structural, morphological and optical properties of raw materials and products obtained at various temperatures were evaluated using a combination of various techniques, based on which the possible mechanism involved in the catalytic formation of hexagonal MoS<sub>2</sub> nanocrystals upon the thermal treatment of MoS<sub>2</sub> in the presence of natural graphite flakes in the molten salt environment was proposed. The formation of hexagonal MoS<sub>2</sub> observed in this work is interesting, in comparison with alternative methods used for the preparation of hexagonally-shaped crystals from the literature, as exhibited in Figure S12 and Table S3. These methods include high-temperature sulfidation [31,32], electrochemical exfoliation [34], and chemical vapor deposition [35,36], using chemicals such as (NH<sub>4</sub>)<sub>2</sub>MoS<sub>4</sub> [31], pure Mo and S [32], W<sub>x</sub>O<sub>y</sub> [26], and Na<sub>2</sub>SO<sub>4</sub> [34]. In contrast, this work proposes a simple and facile method for the preparation of hexagonal MoS<sub>2</sub>, and ultimately MoO<sub>3</sub>/MoS<sub>2</sub>@G samples using highly available and low-cost precursors comprising of MoS<sub>2</sub>, natural graphite minerals and NaCl, as highlighted in Tables 6 and S3. The process is rapid and requires only a short-time heating at 1100 °C. Despite the simple and clean preparation method, the electrode made of MoO<sub>3</sub>/MoS<sub>2</sub>@G-1100 exhibits a decent Li-ion storage performance. Modification of naturally available materials for energy-storage [68–70] and other demanding applications [71–73] is a viable strategy to meet the increasing green energy demand. In this research, we explored the effect of heating at various temperatures on the ball-milled natural graphite/MoS<sub>2</sub>/NaCl mixture for a short period of 20 min to demonstrate that the process of fabricating MoO<sub>3</sub>/MoS<sub>2</sub>@G samples is considerably fast. The influence of heating time on characteristics of the products needs to be explored in future studies. It should be mentioned that at 900–1200 °C, the interaction between components occurs in molten NaCl, which can effectively reduce the reaction between carbon and oxygen forming CO/CO<sub>2</sub> species. According to Figures S9 and S10, further heating of MoO<sub>3</sub>/MoS<sub>2</sub>@G-900 in the absence of NaCl to 1200 °C in air leads to the oxidation of carbon and MoS<sub>2</sub> to form CO/CO<sub>2</sub> species and MoO<sub>3</sub>, respec-

tively, highlighting the effect of NaCl. The influence of other salts on the process is worth investigation in future.

**Table 6.** Amounts of raw materials used and the resultant products obtained at various temperatures.

Raw Material	MoS <sub>2</sub> (10 g)-NaCl (100 g)-Graphite (5 g)			
Ball-milled sample	112.00 g			
Heat-treatment Temperature	900 °C	1000 °C	1100 °C	1200 °C
Sample	MoO <sub>3</sub> /MoS <sub>2</sub> @G-900	MoO <sub>3</sub> /MoS <sub>2</sub> @G-1000	MoO <sub>3</sub> /MoS <sub>2</sub> @G-1100	MoO <sub>3</sub> /MoS <sub>2</sub> @G-1200
Before heat-treatment	28.00 g	28.00 g	28.00 g	28.00 g
After washing	3.31	2.60	2.29	2.45

#### 4. Materials and Methods

##### 4.1. Synthesis of MoS<sub>2</sub>/MoO<sub>3</sub>@Graphene Nanocomposites

A simple and scalable ball-milling–molten salt strategy was used to synthesize MoS<sub>2</sub>/MoO<sub>3</sub>@Graphene nanocomposites. In a typical experiment, molybdenum disulfide (MoS<sub>2</sub> 99.5%, Aladdin CAS-1317-33-5), natural graphite powder (collected from a graphite mine in Hunan province of China) and sodium chloride (NaCl, >99%) (10:5:100 g, respectively) were thoroughly mixed, and the mixture was placed into 500 mL polymeric jars. The ball-milling was performed using zirconia balls with ball: powder weight ratio of 10:1, in the presence of *n*-hexane. The latter was employed to prevent the occurrence of agglomeration during the ball milling process [74], and partial exfoliation of the non-purified natural graphite and MoS<sub>2</sub> [75,76]. The ball milling was performed for 2 h at 230 rpm using a high-energy planetary mill (MITR QM-QX-2L). After ball milling, the samples obtained were dried at 100 °C for 5 h to remove the hexane, and heat-treated at various temperatures of 900–1200 °C for 20 min in air. The heating was performed at 6 °C min<sup>−1</sup>. The samples obtained were employed for various characterizations as described below. Figure 1 exhibits the process used to fabricate the samples. The amount of raw materials used and products obtained through the process are shown in Table 6.

##### 4.2. Morphological, Structural and Surface Characterizations

A scanning electron microscope (SEM, Zeiss Ultra Plus, Oberkochen, Germany) equipped with energy dispersive X-ray spectrometer (EDS, Oxford Instruments, High Wycombe, UK) and a transmission electron microscope (TEM, JEOL JEM-F200, Tokyo, Japan) were used for morphological studies. X-Ray diffractometry (XRD, Malvern Panalytical, Malvern, UK) and fluorescence spectrometry (XRF, ZSX Primus, Rigaku, Japan) were used for phase and chemical analysis, respectively. N<sub>2</sub> adsorption-desorption evaluation was performed using a Micrometrics Tristar II 3020 to examine the surface characteristics of the samples, where the pore size distribution was obtained using the desorption branch of the isotherms. X-ray photoelectron spectroscopy (XPS, Thermo Scientific Instrument, East Grinstead, UK) was employed for surface evaluation using Al-K<sub>α</sub> rays as the excitation source (1486.6 eV).

##### 4.3. Electrochemical Characterizations

Various electrochemical evaluations were performed on the synthesized MoS<sub>2</sub>/MoO<sub>3</sub>@Graphene samples and MoS<sub>2</sub>. Accordingly, cycling and rate performances as well as cyclic voltammetry were evaluated using two-electrode half-cells. For the fabrication of the working electrode, a mixture of active materials (MoS<sub>2</sub>/MoO<sub>3</sub>@Graphene or MoS<sub>2</sub>), C45 conductive carbon and polystyrene acrylic-acrylate (mass ratio of 7:2:1) were thoroughly ground employing water solvent. Then, the slurry was distributed uniformly onto a copper foil (200 μm). After drying at 80 °C (10 h), the electrodes with the active material mass loading of around 1.1 mg cm<sup>−2</sup> were obtained. CR-2025 coin cells were

assembled using metallic Li discs as both the reference/counter electrode. For this, the solution containing 1.0 M lithium  $\text{LiPF}_6$  in EC:DEC:EMC (1:1:1 wt%) was used as the electrolyte. In addition, Celgard 2400 films were employed as the separator. Coin cells were assembled in a glove-box (Mikrouna) under high purity Ar ( $\text{O}_2$  and  $\text{H}_2\text{O} < 0.1$  ppm). The cells were left for 10 h to equilibrate at room temperature, and subsequently evaluated using various techniques. Galvanostatic discharge/charge tests were performed within on a Land CT2001A battery testing instrument. Electrochemical impedance spectroscopy (EIS) and cyclic voltammetry at various scan rates and were conducted using a CHI 660E electrochemical interface.

## 5. Conclusions

In summary, we proposed a green and simple catalytic molten salt strategy for the conversion of commercial  $\text{MoS}_2$ , natural graphite and  $\text{NaCl}$  into  $\text{MoO}_3$  nanoribbons crystals integrated with hexagonal  $\text{MoS}_2$  nanocrystals and graphene nanosheets. The formation of interfacial molybdenum oxycarbide between graphene and  $\text{MoO}_3$  is suggested, contributing to the reduced resistance of the hybrid material. The method is simple, involving the mechanochemical processing of the precursor materials, followed by a heat treatment process at 900–1200 °C in air for the duration of 20 min. The temperature was found to have a significant influence on the composition and morphology of the products. In this process, the thermal oxidation of  $\text{MoS}_2$  causes the formation of molybdenum oxides, and also the formation of highly crystalline hexagonal  $\text{MoS}_2$  nanocrystals integrated with graphene nanosheets. The Li-ion storage performances of hybrid nanostructures fabricated at various temperatures 900–1200 °C, namely  $\text{MoO}_3/\text{MoS}_2\text{@G-900}$ , -1000, -1100 and -1200 were evaluated.  $\text{MoO}_3/\text{MoS}_2\text{@G-1100}$  was found to be capable of delivering a relatively high initial coulombic efficiency of 79.58% with a reversible capacity of  $773.5 \text{ mAh g}^{-1}$  ( $100 \text{ mA g}^{-1}$ ) after 180 cycles, outperforming other electrodes. This behavior was attributed to the highest content of  $\text{MoO}_3$  in  $\text{MoO}_3/\text{MoS}_2\text{@G-1100}$  and its unique microstructure. It was observed that  $\text{MoO}_3/\text{MoS}_2\text{@G-1200}$  has the lowest amount of  $\text{MoO}_3$  among all samples, but its Li-ion storage performance was second only to  $\text{MoO}_3/\text{MoS}_2\text{@G-1100}$ , recording at  $505.9 \text{ mAh g}^{-1}$  after 150 cycles at  $100 \text{ mAh g}^{-1}$ . The high performance of this sample was attributed to the presence  $\beta\text{-MoO}_3$  with a highly ionically conductive open-structure monoclinic crystalline structure that only formed at 1200 °C. The formation of  $\beta\text{-MoO}_3$  was concluded to contribute to the enhanced electrochemical performance of  $\text{MoO}_3/\text{MoS}_2\text{@G-1200}$ , despite its relatively low  $\text{MoO}_3$  content. Graphene generated from the natural graphite and the hexagonal  $\text{MoS}_2$  could be well-integrated, promoting both the electron and ion transportation across the electrode. Consequently, the contribution of pseudocapacitive Li-ion storage of the  $\text{MoO}_3/\text{MoS}_2\text{@G-1100}$  electrode was characterized to be high at 59.31% under the scan rate of  $0.5 \text{ mV s}^{-1}$ . This resulted in the high rate performance of the electrode, providing a capacity of  $216 \text{ mAh g}^{-1}$  after 50 cycles at  $2 \text{ A g}^{-1}$ , and  $106 \text{ mAh g}^{-1}$  after 60 cycles at  $5 \text{ A g}^{-1}$ . This paper proposes a green and low-cost synthesis route for the conversion of highly available  $\text{MoS}_2$  and non-purified natural graphite minerals into hexagonal molybdenum disulfide nanocrystals integrated with molybdenum trioxide and graphene nanosheets with enhanced Li-ion storage performance.

**Supplementary Materials:** The following supporting information can be downloaded at: <https://www.mdpi.com/article/10.3390/catal13030499/s1>, Figure S1: XRD patterns of  $\text{MoO}_3/\text{MoS}_2\text{@G-900}$ ,  $\text{MoO}_3/\text{MoS}_2\text{@G-1000}$ ,  $\text{MoO}_3/\text{MoS}_2\text{@G-1100}$  and  $\text{MoO}_3/\text{MoS}_2\text{@G-1200}$  around the (2 0 0) reflection of orthorhombic  $\text{MoO}_3$ , and the (0 0 1) reflection of monoclinic  $\text{MoO}_3$ ; Figure S2: XRD pattern of  $\text{MoO}_3/\text{MoS}_2\text{@G-900}$ ,  $\text{MoO}_3/\text{MoS}_2\text{@G-1000}$ ,  $\text{MoO}_3/\text{MoS}_2\text{@G-1100}$  and  $\text{MoO}_3/\text{MoS}_2\text{@G-1200}$ , around the (4 0 0) reflection of orthorhombic  $\text{MoO}_3$ , and the (0 0 2) reflection of monoclinic  $\text{MoO}_3$ ; Figure S3: XRD patterns of  $\text{MoO}_3/\text{MoS}_2\text{@G-900}$ ,  $\text{MoO}_3/\text{MoS}_2\text{@G-1000}$ ,  $\text{MoO}_3/\text{MoS}_2\text{@G-1100}$  and  $\text{MoO}_3/\text{MoS}_2\text{@G-1200}$ , around the (6 0 0) reflection of orthorhombic  $\text{MoO}_3$ , and the (0 0 3) reflection of monoclinic  $\text{MoO}_3$ ; Figure S4: Raman spectra of various precursor materials and products obtained at various temperatures; Figure S5: UV-vis spectra of various precursor materials and products obtained at various temperatures; Figure S6:  $(\alpha h\nu)^{1/2}$  versus  $h\nu$  plots according to UV-vis spectra of

various precursor materials and products obtained at various temperatures; Figure S7: SEM image of (a) commercial MoS<sub>2</sub> and the samples prepared at (b) 900, (c) 1000, (d) 1100, and (e–f) 1200 °C. (g) High magnification image taken of the sample prepared at 1200 °C, and (h) the EDS analysis recorded on hexagonal MoS<sub>2</sub> shown in (g).; Figure S8: TEM micrographs of rod-like MoO<sub>3</sub> observed in MoO<sub>3</sub>/MoS<sub>2</sub>@G-900; Figure S6: Summary of methods proposed for the preparation of hexagonally-shaped nanocrystals extracted from the literature; Figure S9: Appearance of MoO<sub>3</sub>/MoS<sub>2</sub>@G-1100, the same sample after heating at 1200 °C for 5 min.; Figure S10: XRD patterns of MoO<sub>3</sub>/MoS<sub>2</sub>@G-1100 and the sample obtained by heating of MoO<sub>3</sub>/MoS<sub>2</sub>@G-1100 at 1200 °C for 5 min; Figure S11: Cycling performance of MoO<sub>3</sub>/MoS<sub>2</sub>@G-1100 at 500 mA g<sup>−1</sup>; Figure S12: Summary of methods proposed for the preparation of hexagonally-shaped nanocrystals extracted from the literature; Table S1: XRD peak intensity ratio corresponding to various peaks in MoO<sub>3</sub>/MoS<sub>2</sub>@G-900, MoO<sub>3</sub>/MoS<sub>2</sub>@G-1000, MoO<sub>3</sub>/MoS<sub>2</sub>@G-1100 and MoO<sub>3</sub>/MoS<sub>2</sub>@G-1200; Table S2: Band gap values of various precursor materials and products obtained at various temperatures. and Table S3: A comparison between precursor materials and the methods used for the preparation of hexagonal crystals extracted from the literature, with those produced in the current study [31–36,77,78].

**Author Contributions:** Conceptualization, A.R.K.; methodology, A.R.K.; software, W.Z. and A.R.K.; validation, W.Z. and A.R.K.; formal analysis, W.Z. and A.R.K.; investigation, W.Z. and A.R.K.; resources, A.R.K.; data curation, W.Z. and A.R.K.; writing—original draft preparation, W.Z. and A.R.K.; writing—review and editing, A.R.K.; visualization, W.Z. and A.R.K.; supervision, A.R.K.; project administration, A.R.K.; funding acquisition, A.R.K. All authors have read and agreed to the published version of the manuscript.

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## Article

# Unveiling the Role of In Situ Sulfidation and H<sub>2</sub>O Excess on H<sub>2</sub>S Decomposition to Carbon-Free H<sub>2</sub> over Cobalt/Ceria Catalysts

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**Abstract:** The emerging energy and environmental concerns nowadays are highlighting the need to turn to clean fuels, such as hydrogen. In this regard, hydrogen sulfide (H<sub>2</sub>S), an abundant chemical compound found in several natural sources and industrial streams, can be considered a potential carbon-free H<sub>2</sub> source through its decomposition. In the present work, the H<sub>2</sub>S decomposition performance of Co<sub>3</sub>O<sub>4</sub>/CeO<sub>2</sub> mixed oxide catalysts toward hydrogen production is investigated under excess H<sub>2</sub>O conditions (1 v/v% H<sub>2</sub>S, 90 v/v% H<sub>2</sub>O, Ar as diluent), simulating the concentrated H<sub>2</sub>S-H<sub>2</sub>O inflow by the Black Sea deep waters. The effect of key operational parameters such as feed composition, temperature (550–850 °C), and cobalt loading (0–100 wt.%) on the catalytic performance of Co<sub>3</sub>O<sub>4</sub>/CeO<sub>2</sub> catalysts was systematically explored. In order to gain insight into potential structure-performance relationships, various characterization studies involving BET, XRD, SEM/EDX, and sulfur elemental analysis were performed over the fresh and spent samples. The experimental results showed that the 30 wt.% Co/CeO<sub>2</sub> catalyst demonstrated the optimum catalytic performance over the entire temperature range with a H<sub>2</sub> production rate of ca. 2.1 μmol H<sub>2</sub>·g<sup>−1</sup>·s<sup>−1</sup> at 850 °C and a stable behavior after 10 h on stream, ascribed mainly to the in-situ formation of highly active and stable cobalt sulfided phases.

**Keywords:** H<sub>2</sub>S decomposition/reforming; H<sub>2</sub>O excess conditions; carbon-free H<sub>2</sub> production; Co<sub>3</sub>O<sub>4</sub>/CeO<sub>2</sub> catalysts; cobalt sulfide phase

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## 1. Introduction

The need to mitigate climate change induced by man-made activities over the past centuries is now a global imperative, implicitly highlighted by the latest report of the Inter-governmental Panel for Climate Change [1]. To this end, commitments under the EU Green Deal strategy and the REPowerEU plan, along with the Paris and Glasgow agreements, emphasize the necessity for the transition towards zero-carbon energy vectors [2,3]. In this regard, the partial or complete replacement of fossil fuels in the future energy mix can be realized by means of an economy based on the extensive use of CO<sub>2</sub>-neutral hydrogen [4,5]. Indeed, H<sub>2</sub> is regarded as a promising energy carrier, which, depending on its origin and generation method, can be totally detached from CO<sub>2</sub> emissions and extensively utilized in a wide range of energy applications and chemical processes towards their full-scale decarbonization [6,7]. Hydrogen has been used in large quantities for well over 100 years as a non-energy feedstock in the production of fertilizers, methanol synthesis, petroleum refineries, and as an agent for the direct reduction of iron in the steel industry, while its current demand at global scale amounts to ca. 100–120 Mt H<sub>2</sub>/yr [8,9]. However, in order to sufficiently meet the ambitious goals for a carbon-neutral economy, hydrogen would

need to reach shares of around 15% of the world's energy demand by mid-century and increase its production capacity more than three-fold, to 300–350 Mt H<sub>2</sub>/yr [4].

Generally, hydrogen is the most abundant element in the universe, albeit it is only available bounded in compounds such as fossil and bio-based hydrocarbons, gases (e.g., NH<sub>3</sub>, H<sub>2</sub>S), and water. It can be produced using a number of different methods with varying efficiencies, environmental footprint, costs, and technical maturity [8–10] and is typically classified into colors depending on the method and feedstock used, ranging from fossil-fuel-based hydrogen production (grey hydrogen) combined in several occasions with carbon capture, utilization, and storage (CCUS; blue hydrogen), to electrolytic hydrogen from renewable electricity (green hydrogen) or nuclear power plants (pink hydrogen) or grid electricity (yellow hydrogen), and to biohydrogen production by photolysis (orange hydrogen) and waste thermochemical conversion, among others [9]. In an attempt to improve the sustainability and competitiveness over other alternatives, research efforts on hydrogen production are mainly directed to: (a) increase in energy efficiency (less energy consumption per MJ of recovered/produced hydrogen), (b) decrease in the capital expenditures (CAPEX) and the levelized cost of hydrogen, (c) minimization or even elimination of the use of critical raw materials in key process components such as catalysts, electrodes, etc., (d) development of new pathways from CO<sub>2</sub>-neutral or carbon-free sources and (e) leveling-up the readiness of the less matured technologies [11–13].

Among the conventional H<sub>2</sub> production pathways, an alternative route concerns the utilization of hydrogen sulfide (H<sub>2</sub>S) as a potential carbon-free source of H<sub>2</sub> [14,15]. H<sub>2</sub>S is a toxic and corrosive gas, and its concentration in the air ranges between 0.11–0.33 ppb, albeit it is found in much higher levels in several natural sources and H<sub>2</sub>S-emitting industrial activities. Hydrogen sulfide is typically emitted from a variety of industrial processes, such as petroleum refineries, crude oil and natural gas production, wastewater treatment plants, coke ovens, tanneries, and kraft paper mills [16]. Moreover, H<sub>2</sub>S is also naturally present in geothermal sources and springs [17], coal seams [18], agricultural fields [19], and marine sediments [20].

Industrially, H<sub>2</sub>S emissions are predominantly managed via the Claus technology producing elemental sulfur and water, accounting for 90–95% of the total recovered sulfur. The Claus process achieves 95–98% recovery of the hydrogen sulfide feed stream [21]. On the downside, this process is energy-intensive due to the high operational temperature, commonly above 1000 °C. Additionally, secondary pollution by the unreacted H<sub>2</sub>S and SO<sub>2</sub> species is a concern, whereas the H<sub>2</sub>O by-product is undesirable for several downstream processes [22]. Alternatively, H<sub>2</sub>S decomposition to its elemental constituents, namely H<sub>2</sub> and sulfur, could be a more alluring prospect. In this direction, the abatement of H<sub>2</sub>S is combined with the simultaneous production of valuable products. Therefore, numerous technologies have been recently investigated for H<sub>2</sub>S decomposition [23], mainly involving: thermal [24,25], catalytic [26,27], plasmochemical [28,29], electrochemical [30], and photochemical [31] decomposition. The majority of these approaches, however, present several drawbacks attributed to the particular high energy requirements and low efficiencies, rendering their practical deployment infeasible as of yet [32]. In this sense, the most commonly employed direct method is the thermal decomposition of H<sub>2</sub>S, which, however, takes place at high temperatures in order to achieve conversions exceeding 50%. This is due to the fact that the cleavage of the H<sub>2</sub>S molecule into its constituent elements requires a substantial amount of energy since the thermal decomposition of H<sub>2</sub>S is an endothermic reaction with a highly positive Gibbs free energy [33,34]. Specifically, the gas-phase H<sub>2</sub>S dissociation standard enthalpy and standard Gibbs free energy values are equal to 317.9 and 270.1 kJ/mol, respectively [14].

As mentioned above, appreciable amounts of H<sub>2</sub>S exist in aquatic sediments, with particular interest being directed in the Black Sea waters, due to their high H<sub>2</sub>S content that is replenished continuously [35–37]. Owing to the specific locational and biological characteristics of the Black Sea, a large amount of H<sub>2</sub>S lies in the anoxic deeper layers with a highly toxic character [38]. Hence, an efficient method for H<sub>2</sub>S exploitation is

actively sought. Hydrogen production from  $\text{H}_2\text{S}$  in the Black Sea deep waters could play an important role in the clean energy transition of the surrounding countries offering at the same time significant environmental benefits toward the remediation of the Black Sea ecosystem.

Apart from thermal decomposition studies, research on the conversion of  $\text{H}_2\text{S}$  from the Black Sea based on electrochemical methods has also been conducted.  $\text{H}_2$  production from  $\text{H}_2\text{S}$  contained in the Black Sea deep waters has been examined by employing a micro-structured electrochemical membrane reactor, which is assembled with optimized cell materials.  $\text{CeO}_2$ -based transition metal catalysts were employed as anode materials, with ceria-supported cobalt catalysts displaying the best performance in terms of  $\text{H}_2\text{S}$  decomposition activity and long-term stability [35,39]. In a more holistic approach, Petrov et al. [40] investigated a multistage process involving the electrochemical production of  $\text{H}_2$  and polysulfides via direct alkaline electrolysis of  $\text{H}_2\text{S}$ . Raney-nickel, graphite, platinized carbon,  $\text{CoS}$ , and perovskites were tested as catalysts, with  $\text{CoS}$  and perovskites being highly stable and efficient. Elsewhere, perovskite-type catalysts were also tested for the thermal decomposition of  $\text{H}_2\text{S}$  [41,42], with  $\text{LaSr}_{0.5}\text{Mo}_{0.5}\text{O}_3$ , in particular, displaying the highest performance at temperatures ranging from 700–850 °C.

Recently, ceria-based transition metal catalysts have gained particular attention in the field of heterogeneous catalysis due to their unique solid-state properties, mainly linked to synergistic metal–support interactions [43–45]. In this regard, in our previous work [46], we thoroughly explored the impact of metal nature on the  $\text{H}_2\text{S}$  decomposition performance of a series of  $\text{M}_x\text{O}_y/\text{CeO}_2$  oxides (M: Fe, Co, Ni, Cu) catalysts under atmospheric pressure and dry conditions (i.e., absence of  $\text{H}_2\text{O}$ ). The results clearly revealed the superiority of  $\text{Co}_3\text{O}_4/\text{CeO}_2$  composites, in terms of both activity and stability, offering  $\text{H}_2\text{S}$  conversions close to the thermodynamic predicted values (ca. 35% at 850 °C).

Motivated by these findings, the  $\text{H}_2\text{S}$  decomposition performance of  $\text{Co}_3\text{O}_4/\text{CeO}_2$  catalysts is hereby investigated under extremely excess  $\text{H}_2\text{O}$  contents (1 v/v%  $\text{H}_2\text{S}$ , 90 v/v%  $\text{H}_2\text{O}$ , Ar as diluent) to better approach Black Sea inflow conditions. The impact of various operational parameters such as the feed composition, temperature, and Co loading (0–100 wt.%) on the performance and kinetics of as-prepared cobalt oxide–ceria catalysts was systematically investigated. In addition, the physicochemical properties of both fresh and spent catalysts were assessed by complementary characterization studies to gain insight into potential structure–performance relationships. To the best of our knowledge, this is the first study on the catalyst-aided  $\text{H}_2\text{S}$  decomposition reaction under harsh reaction conditions (water content of 90 v/v%), adhering to the dual purpose of environmental mitigation and carbon-free  $\text{H}_2$  production.

## 2. Results and Discussion

### 2.1. Characterization Studies

The main textural and structural characteristics of the  $\text{Co}_3\text{O}_4/\text{CeO}_2$  catalysts with different Co loadings (0–100 wt.%) are displayed in Table 1. As expected, bare  $\text{CeO}_2$  possesses the highest BET surface area (71.5  $\text{m}^2/\text{g}$ ) and pore volume (0.27  $\text{cm}^3/\text{g}$ ). On the other hand, bare  $\text{Co}_3\text{O}_4$  exhibits the lowest surface area (2.9  $\text{m}^2/\text{g}$ ) and pore volume (0.01  $\text{cm}^3/\text{g}$ ). Cobalt oxide incorporation into ceria carrier results in a decrease in surface area and pore volume and a small increase in pore size, which could be attributed to the inferior textural characteristics of bare  $\text{Co}_3\text{O}_4$ , as shown in relevant studies [47,48] and further discussed below. However, significant pore blockage phenomena upon the addition of  $\text{Co}_3\text{O}_4$  to  $\text{CeO}_2$  carrier were excluded by means of the Weisz–Prater criterion, which was calculated by the method followed in our previous work [49].

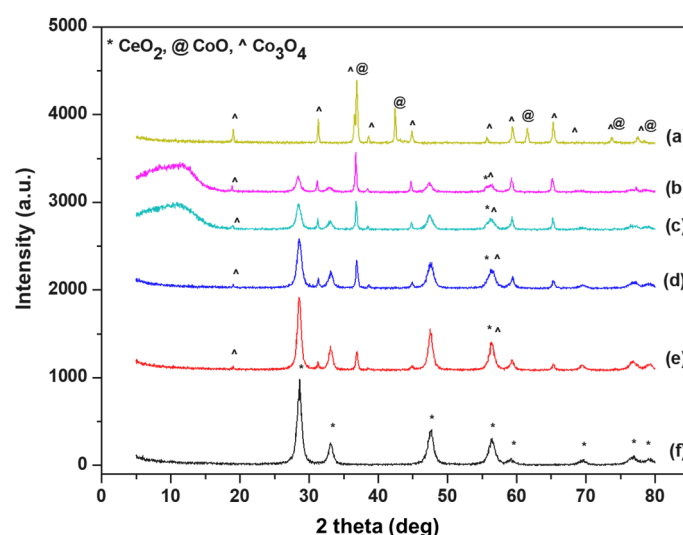
The XRD patterns of the examined materials are depicted in Figure 1, while the crystalline phases that were detected for each sample and the approximate crystallite sizes, as determined by Scherrer analysis, are provided in Table 1. In principle, all catalysts crystallized in the form of their respective oxides, while for bare cobalt oxide, both  $\text{CoO}$  and  $\text{Co}_3\text{O}_4$  phases are detected. Specifically, Co is present in the form of  $\text{Co}_3\text{O}_4$  in the mixed

oxides, with its crystallite size rising slightly upon increasing cobalt content, suggesting the partial segregation of Co metal entities. Notably, the size of bare cobalt oxide crystallites is about 4.5 times higher than CeO<sub>2</sub> (ca. 50 vs. 11 nm), implying the significant segregation of the cobalt oxide phase by the formation of large Co<sub>3</sub>O<sub>4</sub> crystallites. On the other hand, CeO<sub>2</sub> crystallite size remains practically unchanged upon increasing the loading of cobalt oxide, approximately 10–11 nm. Therefore, the progressive reduction of BET surface area of the mixed oxides upon increasing Co loading could be ascribed to the partial substitution of high-surface-area CeO<sub>2</sub> with the low-surface area Co<sub>3</sub>O<sub>4</sub>, in conjunction with the partial pore blockage by large cobalt oxide crystallites. Similar results have been reported in relevant works [50–53].

**Table 1.** Textural and structural properties of bare oxides and x-Co/CeO<sub>2</sub> catalysts.

Sample	N <sub>2</sub> Porosimetry			XRD Analysis	
	BET Surface Area (m <sup>2</sup> /g)	Pore Volume (cm <sup>3</sup> /g)	Average Pore Diameter (nm)	Crystal Phase	Crystallite Size (nm)
CeO <sub>2</sub> <sup>a</sup>	71.5	0.27	15.4	CeO <sub>2</sub>	11.0
20-Co/CeO <sub>2</sub> <sup>a</sup>	33.4	0.13	16.0	CeO <sub>2</sub>	10.2
				Co <sub>3</sub> O <sub>4</sub>	37.7
30-Co/CeO <sub>2</sub>	44.9	0.21	18.7	CeO <sub>2</sub>	10.4
				Co <sub>3</sub> O <sub>4</sub>	37.9
40-Co/CeO <sub>2</sub>	28.4	0.10	14.7	CeO <sub>2</sub>	10.5
				Co <sub>3</sub> O <sub>4</sub>	41.7
60-Co/CeO <sub>2</sub>	15.1	0.07	19.3	CeO <sub>2</sub>	10.5
				Co <sub>3</sub> O <sub>4</sub>	42.2
Co <sub>3</sub> O <sub>4</sub>	2.9	0.01	17.8	Co <sub>3</sub> O <sub>4</sub>	50.7
				CoO	52.7

<sup>a</sup> Data taken from Ref. [46].

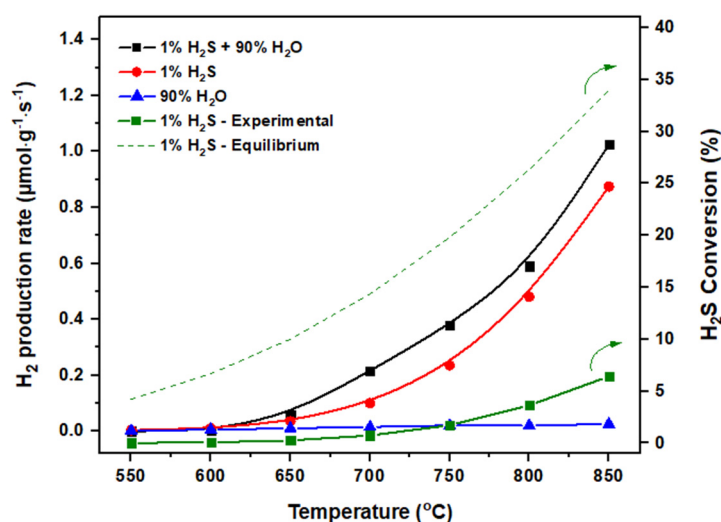


**Figure 1.** X-ray powder diffraction patterns of x-Co/CeO<sub>2</sub> catalysts with a mass Co loading of 100% (a), 60% (b), 40% (c), 30% (d), 20% (e) and 0% (f). Data for (e,f) are taken from Ref. [46].

## 2.2. Catalytic Evaluation

It should be stated first that as a point of reference, the H<sub>2</sub> production rate achieved in the absence of catalysts (blank experiments) under (i) 1 v/v% H<sub>2</sub>S and 90 v/v% H<sub>2</sub>O, (ii) 1.0 v/v% H<sub>2</sub>S and (iii) 90 v/v% H<sub>2</sub>O, balanced with Ar at the temperature range of 550–850 °C was examined. The results from these preliminary experiments, along with the corresponding experimental and equilibrium H<sub>2</sub>S conversion values for the H<sub>2</sub>S decomposition reaction in the absence of steam, are depicted in Figure 2. Clearly, the conversion of

H<sub>2</sub>O and the resulting hydrogen evolution rate are negligible for the 90 v/v% H<sub>2</sub>O feed-stock in the entire temperature range, indicating no contribution of thermal water splitting towards hydrogen generation at these experimental conditions. This is also confirmed by the corresponding equilibrium curve, which lies at very low conversion values and is not shown for brevity. Moreover, H<sub>2</sub>S conversion under dry conditions is lower than ca. 8% over the entire investigated temperature range, far below the corresponding thermodynamic values, implying the significant kinetic limitations of the homogeneous reaction, as further discussed below.



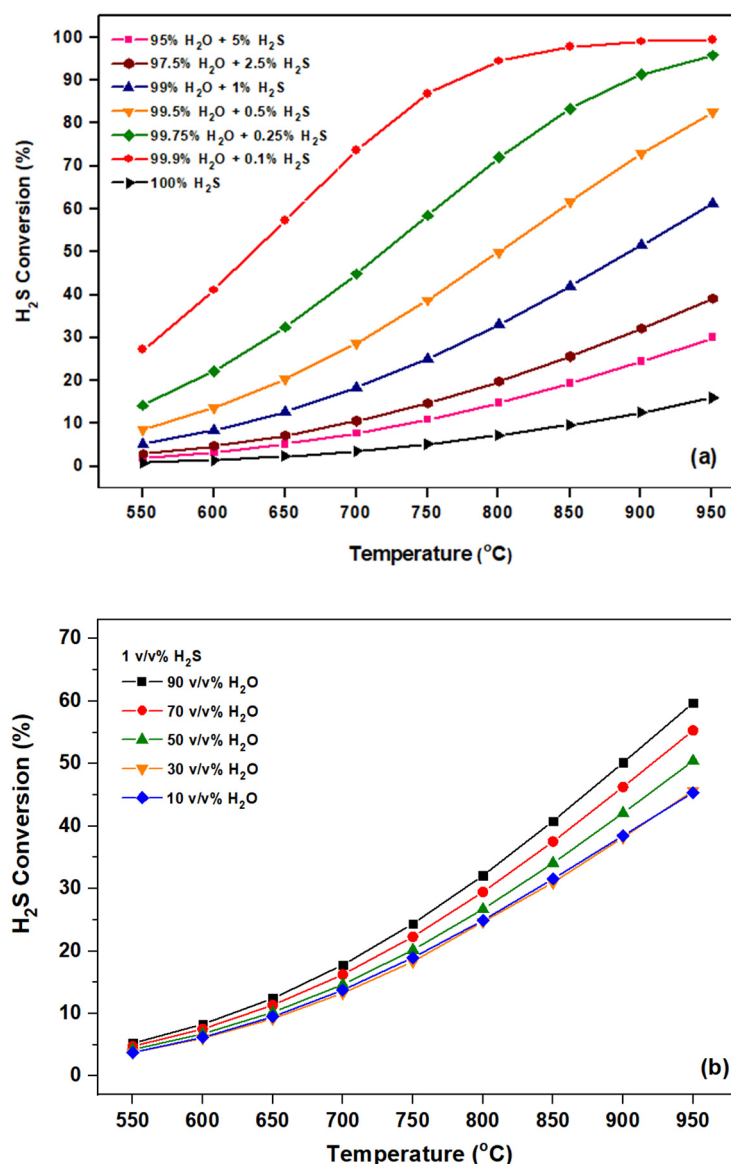
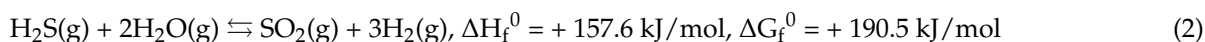
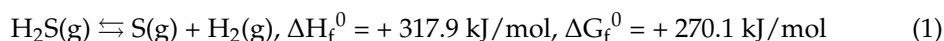
**Figure 2.** Left y-axis: Hydrogen production rate as a function of temperature and feedstock composition in the absence of catalyst (blank experiments). Right y-axis: Experimental and equilibrium H<sub>2</sub>S conversion values for the dry H<sub>2</sub>S decomposition reaction (green lines). Reaction conditions: P = 1 bar, Flowrate: 100 cm<sup>3</sup>/min.

However, in the case of H<sub>2</sub>S decomposition, significantly higher hydrogen production rates were obtained as compared to pure H<sub>2</sub>O (0.87 vs. 0.01 μmol·g<sup>−1</sup>·s<sup>−1</sup> at 850 °C, respectively). Furthermore, higher H<sub>2</sub> production rates were observed with an increase in reaction temperature attaining a maximum at 850 °C, as reported elsewhere for the non-catalytic thermal H<sub>2</sub>S decomposition [14,34,54]. This behavior is thermodynamically attributable to the endothermicity and non-spontaneity of the process, evidenced by the highly positive values of reaction enthalpy and Gibbs free energy, respectively (Equation (1)). Intriguingly, the simultaneous presence of H<sub>2</sub>S and H<sub>2</sub>O in the reaction feed (i.e., 1 v/v% H<sub>2</sub>S and 90 v/v% H<sub>2</sub>O balanced in Ar), which is originally reported in this work, resulted in the maximum H<sub>2</sub> production (ca. 1.03 μmol·g<sup>−1</sup>·s<sup>−1</sup> at 850 °C), suggesting the synergistic interaction of both H<sub>2</sub>S and H<sub>2</sub>O towards the optimal hydrogen production rate.

The above can also be corroborated by considering the thermodynamics of the gas-phase reactions of H<sub>2</sub>S decomposition (Equation (1)) and H<sub>2</sub>S steam reforming (Equation (2)). Indeed, regarding Equation (2), it was confirmed by a separate simulation in Aspen Plus that SO<sub>2</sub> and H<sub>2</sub> are by far the most favored products from the specific reacting mixture of hydrogen sulfide and steam in the relevant temperature regime, even when considering the production of elemental sulfur, SO<sub>3</sub> and/or O<sub>2</sub>. In any case, the stoichiometry of the reaction is seen in Equation (2). Moreover, whereas both reactions are endothermic and thus H<sub>2</sub>S conversion is favored with an increase in the reaction temperature, the beneficial role of steam lies predominantly in the significantly lower Gibbs free energy value in Equation (2) compared to dry H<sub>2</sub>S decomposition (Equation (1)). Thus, the presence of steam essentially provides the driving force for enhancing hydrogen formation, as the stoichiometric coefficient of H<sub>2</sub> in Equation (2) is three times higher compared to the one in Equation (1). The above is better depicted in the thermodynamic plots in Figure 3. As can be seen from Figure 3a, the conversion of H<sub>2</sub>S is thermodynamically favored over various H<sub>2</sub>S/H<sub>2</sub>O



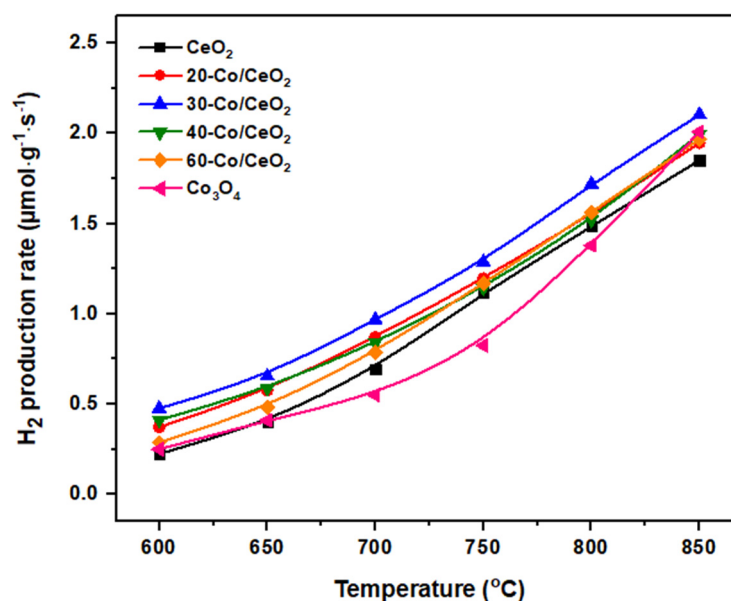
mixtures compared to  $\text{H}_2\text{S}$  decomposition in the absence of steam, whereby  $\text{H}_2\text{S}$  conversion increases monotonically with the steam excess in the feed. Furthermore, to better assess the thermodynamic tendency of the system in the employed reaction conditions, the presence of inert gas in the reactant feed is examined over a mixture of 1%  $\text{H}_2\text{S}$  in steam (Figure 3b). Evidently,  $\text{H}_2\text{S}$  conversion increases with the increased presence of water vapor in the reactor inlet.



**Figure 3.** Effect of  $\text{H}_2\text{O}$  feed concentration on the thermodynamic  $\text{H}_2\text{S}$  conversion at ambient pressure as a function of temperature in the (a) absence and (b) presence of inert Ar.

Next, the effect of Co loading on the  $\text{H}_2$  production rate under excess steam conditions was explored, and the corresponding results are shown in Figure 4. It is evident that within the selected temperature range, the  $\text{H}_2$  production rate clearly increases with increasing reaction temperature, irrespective of the cobalt loading. Furthermore, in the absence of  $\text{Co}_3\text{O}_4$  (that is, for bare  $\text{CeO}_2$  sample),  $\text{H}_2$  production is clearly lower than the respective

values for x-Co/CeO<sub>2</sub> samples, while the lowest values were attained for pure cobalt oxide. These findings point towards the fact that the synergy between ceria and cobalt oxide species is a prerequisite for optimum catalytic activity. Moreover, the 30-Co/CeO<sub>2</sub> sample exhibited the highest performance among all x-Co/CeO<sub>2</sub> catalysts, showcasing the existence of an optimal cobalt oxide loading towards the achievement of maximum hydrogen production rate. Indeed, 30-Co/CeO<sub>2</sub> outperforms its counterparts in all the examined temperatures. For instance, at 850 °C, the 30-Co/CeO<sub>2</sub> sample exhibits a H<sub>2</sub> production rate of 2.11  $\mu\text{mol}\cdot\text{g}^{-1}\cdot\text{s}^{-1}$  compared to 1.86 and 1.97  $\mu\text{mol}\cdot\text{g}^{-1}\cdot\text{s}^{-1}$  over bare CeO<sub>2</sub> and Co<sub>3</sub>O<sub>4</sub>, respectively, with the superiority of mixed oxide being even more prominent at lower reaction temperatures. It should also be stated that all catalysts exhibited far superior performance compared to blank experiments (see Figure 2), clearly revealing the decisive role of the catalyst towards the progression of hydrogen generation rates.

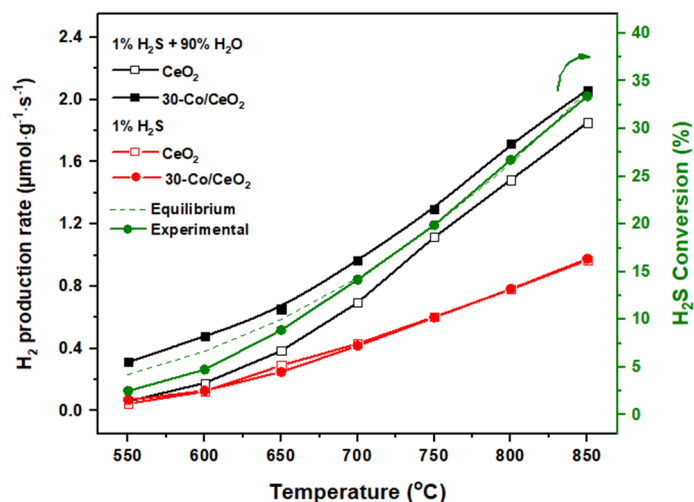


**Figure 4.** Hydrogen production rate as a function of temperature for x-Co/CeO<sub>2</sub> catalysts. Reaction conditions: 1 v/v% H<sub>2</sub>S–90 v/v% H<sub>2</sub>O, balanced with Ar, P = 1 bar, Flowrate: 100 cm<sup>3</sup>/min, Catalyst mass = 250 mg, GHSV = 13,300 h<sup>−1</sup>.

Subsequently, the H<sub>2</sub> production rate of the optimum catalyst, 30-Co/CeO<sub>2</sub>, is compared with bare ceria, both in the absence and presence of excess H<sub>2</sub>O (Figure 5). Interestingly, in the absence of H<sub>2</sub>O, both bare CeO<sub>2</sub> and Co<sub>3</sub>O<sub>4</sub>/CeO<sub>2</sub> samples exhibited almost an identical performance in terms of H<sub>2</sub> production, revealing the pivotal role of CeO<sub>2</sub> in the deH<sub>2</sub>S process [55]. Moreover, the significantly higher H<sub>2</sub>S conversion under dry conditions of the catalyst-aided process compared to the homogeneous one (Figure 2) should be noted. On the other hand, the pronounced effect of H<sub>2</sub>O excess in the feed steam is evident for both bare CeO<sub>2</sub> and x-Co/CeO<sub>2</sub> samples. The superior catalytic performance in wet conditions is in line with the thermodynamic calculations and can be attributed to the additional amount of H<sub>2</sub>, which is produced via Equation (2).

Notably, the 30-Co/CeO<sub>2</sub> sample outperforms bare ceria under wet conditions, implying a synergistic effect towards higher H<sub>2</sub> production rates in the presence of water. This synergistic interaction, however, is not perceived under dry conditions, revealing the key role of steam in conjunction with the cobalt oxide–ceria synergy. In other words, the co-existence of cobalt oxide and ceria species is required to obtain high H<sub>2</sub> production rates. The latter could be possibly ascribed to the facilitation of the H<sub>2</sub>S reforming reaction (as described by Equation (2)) at the interfacial sites, further contributing to H<sub>2</sub> production. This is additionally verified by the negligible rate of H<sub>2</sub> production during steam splitting (in the absence of H<sub>2</sub>S) over Co<sub>3</sub>O<sub>4</sub>/CeO<sub>2</sub> samples. In view of the above, the superior

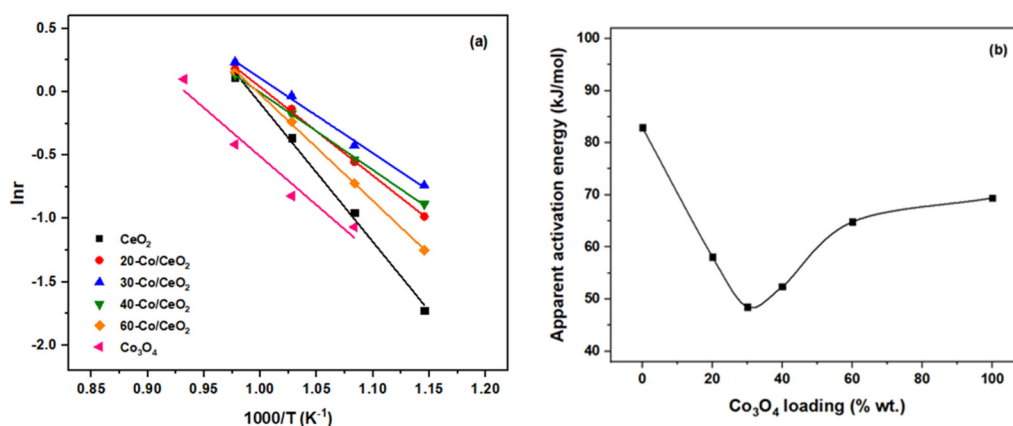
reactivity of  $\text{Co}_3\text{O}_4/\text{CeO}_2$  compared to the bare counterparts has been documented in the literature, ascribed mainly to synergistic cobalt oxide–ceria interactions [56–58].



**Figure 5.** Left y-axis:  $\text{H}_2$  production rate as a function of temperature for 30-Co/CeO<sub>2</sub> and bare CeO<sub>2</sub>. Right y-axis: Experimental and equilibrium  $\text{H}_2\text{S}$  conversion for the dry  $\text{H}_2\text{S}$  decomposition reaction over 30-Co/CeO<sub>2</sub> (green lines). Reaction conditions:  $P = 1$  bar, Flowrate:  $100 \text{ cm}^3/\text{min}$ , Catalyst mass = 250 mg, GHSV =  $13,300 \text{ h}^{-1}$ .

### 2.3. Apparent Activation Energies

For the approximate estimation of apparent activation energies, the differential method of analysis was followed. The possible contribution of internal mass transport phenomena was disregarded by means of the Weisz–Prater criterion (*vide supra*); thus, the measured apparent reaction rates were considered to be practically ascribed to the intrinsic reactivity of the catalysts. Therefore, the Arrhenius plots and the calculated activation energy values for all x-Co/CeO<sub>2</sub> catalysts are shown in Figure 6a and Figure 6b, respectively. The superior performance of the 30-Co/CeO<sub>2</sub> catalyst is again evident in terms of the apparent activation energy since it exhibits the lowest apparent activation energy value among all samples. Equally importantly, the binary cobalt oxide–ceria samples are associated with lower apparent activation energy values compared to the bare cobalt oxide and ceria, providing additional evidence of the beneficial role of the co-presence of cobalt oxide and ceria phases, which is also reflected in their catalytic activity (Figure 4).



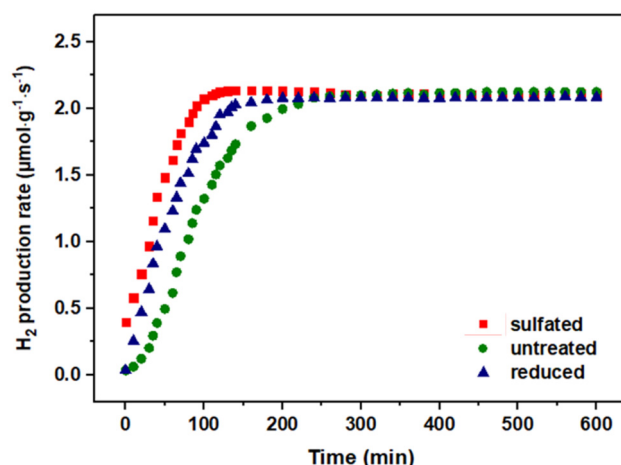
**Figure 6.** Arrhenius plots (a) and apparent activation energy values (b) for the as-prepared x-Co/CeO<sub>2</sub> catalysts. Reaction conditions: 1 v/v%  $\text{H}_2\text{S}$ –90 v/v%  $\text{H}_2\text{O}$ , balanced with Ar,  $P = 1$  bar, Flowrate:  $100 \text{ cm}^3/\text{min}$ , Catalyst mass = 250 mg, GHSV =  $13,300 \text{ h}^{-1}$ .

A more meaningful assessment of the apparent activation energy values calculated in this study cannot be made since, to the best of our knowledge, this is the first time that such values have been reported in the literature for  $\text{H}_2$  production through the decomposition of  $\text{H}_2\text{S}$  in extreme  $\text{H}_2\text{O}$  excess conditions. In any case, and in order to better showcase the beneficial synergistic role of the as-prepared cobalt oxide–ceria catalysts, the apparent activation energies for the  $\text{H}_2\text{S}$  decomposition reaction under both dry and wet conditions in the absence of catalysts were calculated (Arrhenius plots not shown for brevity). Specifically, apparent activation energy values equal to 124 and 137 kJ/mol were calculated for the non-catalytic thermal  $\text{H}_2\text{S}$  decomposition in the presence and absence of water, respectively. Not unexpectedly, these values are substantially higher compared to the respective values for all the employed catalysts and especially for the 30-Co/CeO<sub>2</sub> sample (Figure 6b). This finding showcases the significant role of catalysts, which enhance hydrogen production by offering a reaction pathway associated with a substantially decreased activation energy compared to the thermal-induced and gas-phase  $\text{H}_2\text{S}$  decomposition.

Also, with regards to the activation energy for the reaction of  $\text{H}_2\text{S}$  decomposition under dry and wet conditions for the optimum sample, i.e., 30-Co/CeO<sub>2</sub> (see Figure 5), the values were calculated to equal 66 and 49 kJ/mol, respectively. Therefore, in comparison with the respective values obtained in catalyst-free experiments (i.e., 137 and 124 kJ/mol in the absence and presence of  $\text{H}_2\text{O}$ , respectively), it is evident that the 30-Co/CeO<sub>2</sub> sample remarkably modifies the  $\text{H}_2\text{S}$  decomposition reaction pathway in the presence of water, as it decreases the apparent activation energy by a factor of 2.5. At the same time, the effect is less prominent under dry reaction conditions since the apparent activation energy in the presence of 30-Co/CeO<sub>2</sub> catalyst is decreased by a factor of 2.0 compared to the blank experiments. In all, and although the present results are not derived through a dedicated kinetic analysis, the obtained values can be considered as a reference point that can be used for comparison purposes. Therefore, they need to be refined and rigorously calculated in future work employing a more detailed kinetic methodology, also taking into account the reversibility of the reaction.

#### 2.4. Stability Tests

Motivated by the superior  $\text{H}_2\text{S}$  decomposition performance of 30-Co/CeO<sub>2</sub> under  $\text{H}_2\text{O}$  excess conditions, short-term (10 h) stability experiments were also carried out to assess its lifetime characteristics (Figure 7). Specifically, the  $\text{H}_2$  production rate was continuously monitored at  $T = 850\text{ }^\circ\text{C}$  as a function of time on stream. The fresh catalyst was first heated up to  $850\text{ }^\circ\text{C}$  ( $3\text{ }^\circ\text{C}/\text{min}$ ) under pure Ar atmosphere, kept at this temperature for 1 hr, and then at  $t = 0\text{ min}$ , the standard feed mixture used in the activity experiments ( $1\text{ v/v}\%$   $\text{H}_2\text{S}$ – $90\text{ v/v}\%$   $\text{H}_2\text{O}$ , balanced with Ar), was introduced into the reactor. Interestingly,  $\text{H}_2$  production is continuously increased for the first ca. 4 h and then stabilized to a steady-state value of ca.  $2.1\text{ }\mu\text{mol}\cdot\text{g}^{-1}\cdot\text{s}^{-1}$ . This value is similar to that obtained in the activity experiments and remained constant until the end of the experiment.



**Figure 7.** Hydrogen production rate as a function of time on stream for the “untreated”, “sulfided” and “reduced” catalysts. Reaction conditions: 1 v/v% H<sub>2</sub>S–90 v/v% H<sub>2</sub>O, balanced with Ar, P = 1 bar, T = 850 °C, Flowrate: 100 cm<sup>3</sup>/min, Catalyst mass = 250 mg, GHSV = 13,300 h<sup>−1</sup>.

In an attempt to clarify whether the initial activation period for the 30-Co/CeO<sub>2</sub> catalyst is associated with the in situ sulfidation or reduction of the sample during the reaction, two additional short-term (10 h) stability experiments were carried out employing the same catalyst at different initial states. In particular, prior to the experiment, the “untreated” 30-Co/CeO<sub>2</sub> was subjected at 850 °C to a gas stream of either 1 v/v% H<sub>2</sub>S–90 v/v% H<sub>2</sub>O for 10 h or 10 v/v% H<sub>2</sub>/Ar for 1 h in order to obtain the “sulfided” and “reduced” samples, respectively. Both the “sulfided” and “reduced” catalysts were subsequently tested under the standard reaction conditions (1 v/v% H<sub>2</sub>S–90 v/v% H<sub>2</sub>O, balance with Ar), and their hydrogen production rate profiles vs. time on stream were compared with the “untreated” sample.

The comparison between the different pretreated catalysts revealed the remarkable behavior of the “sulfided” catalyst. It was observed that the initial activation period of approximately 4 h of the “untreated” 30-Co/CeO<sub>2</sub> catalyst is reduced to less than 1.5 h for the “sulfided” sample. On the other hand, the “reduced” catalyst also demonstrated a decreased activation period (ca. 2 h) compared to the untreated material, but obviously higher compared to the “sulfided” sample.

In this point, it is worth pointing out the key role of chemisorption in the H<sub>2</sub>S decomposition process and in the observed transient nature of hydrogen generation in this work (Figure 7). Elsewhere, on a series of well-defined rhodium crystals [59], it was found that H<sub>2</sub>S adsorption on clean Rh(100) surfaces results in very rapid initial adsorption, followed by a very slow approach to saturation. This was followed by an increase in the surface S/Rh ratio, ascribed to the decomposition of H<sub>2</sub>S. Even more importantly, H<sub>2</sub> desorption follows the same trend as the S/Rh ratio, showcasing the importance of progressive in situ sulfidation. Moreover, in a more recent study examining several transition metal sulfide catalysts [60], it was shown that at higher temperatures, the reaction could proceed under a quasi-steady state, where H<sub>2</sub>S conversion and H<sub>2</sub> yield remain almost constant over elevated time on stream. Furthermore, a direct correlation between the amount of the released H<sub>2</sub> and sulfur was disclosed.

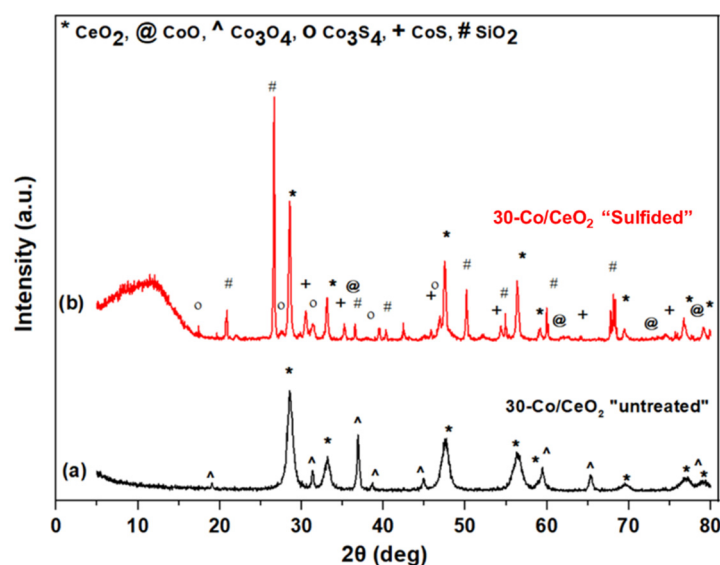
In light of the present findings, it can be deduced that the progressive activation is mainly due to the in situ sulfidation of the catalyst under the reaction atmosphere and, to a lesser extent, to H<sub>2</sub> reduction. This is better demonstrated by calculating the absolute hydrogen production (in mmol) during the activation period for each sample via the integration of the hydrogen production rate curve over the activation step. Indeed, the respective values for the “untreated”, “reduced”, and “sulfided” catalysts are equal to 288, 336, and 376 mmol H<sub>2</sub>/g, respectively, demonstrating the pronounced effect of sulfidation in the total hydrogen production. In all cases (“untreated”, “sulfided”, and “reduced”),

the H<sub>2</sub> production rate attained a stable value after a certain time period, reaching values similar to those obtained in the activity experiments and remaining stable until the end of the 10 h duration test. These findings clearly revealed the pronounced effect of in situ sulfidation, and to a lesser extent reduction, processes towards the progressive activation of cobalt oxide–ceria catalysts. Notably, irrespective of the catalyst's initial state, all samples reach the same steady state, exhibiting a remarkably stable performance after a certain time. The beneficial effect of H<sub>2</sub>S during the course of the reaction between H<sub>2</sub>S and H<sub>2</sub>O is also worth noticing, in complete contrast to the poisoning effect of H<sub>2</sub>S in several catalytic processes [61–63]. Similar observations on the positive effect of sulfidation have been reported elsewhere [64].

## 2.5. Spent Catalysts Characterization

In order to gain insight into the impact of the reaction conditions on the textural, structural, and surface features of the employed catalysts and to reveal possible structure–performance relationships, a complementary characterization study employing BET, XRD, SEM, and sulfur elemental analysis, prior (“untreated”) and after (“sulfided”) the stability experiments, was carried out. In terms of the textural characteristics, it is worth noticing that catalyst exposure to reaction conditions results in an almost complete collapse of the pore structure; the BET surface area and the pore volume of the “sulfided” catalyst decreased to about 2.4 m<sup>2</sup>/g and 0.04 cm<sup>3</sup>/g from 44.9 m<sup>2</sup>/g and 0.21 cm<sup>3</sup>/g of the “untreated” 30-Co/CeO<sub>2</sub> catalyst, respectively. Coupled with the excellent activity and stability performance of the “sulfided” catalyst, the deterioration of its porous structure clearly implies that the catalytic activity is practically independent of the textural properties.

The structural modifications induced under reaction conditions were revealed by means of XRD studies. Figure 8 depicts the XRD patterns of the “untreated” and “sulfided” catalysts. It is evident that new crystal structures were formed during the reaction, which were absent from the “untreated” samples. In particular, the XRD pattern of the “untreated” sample presents reflections that correspond to the Co<sub>3</sub>O<sub>4</sub> and CeO<sub>2</sub> oxides, implying no chemical transformations or interactions between the parent oxides up to 600 °C (calcination temperature). However, the XRD pattern of the “sulfided” catalyst is completely different; the formation of new crystalline cobalt sulfide phases, i.e., Co<sub>3</sub>S<sub>4</sub> and CoS, was clearly identified, verifying the in situ sulfidation of the catalyst under reaction conditions.

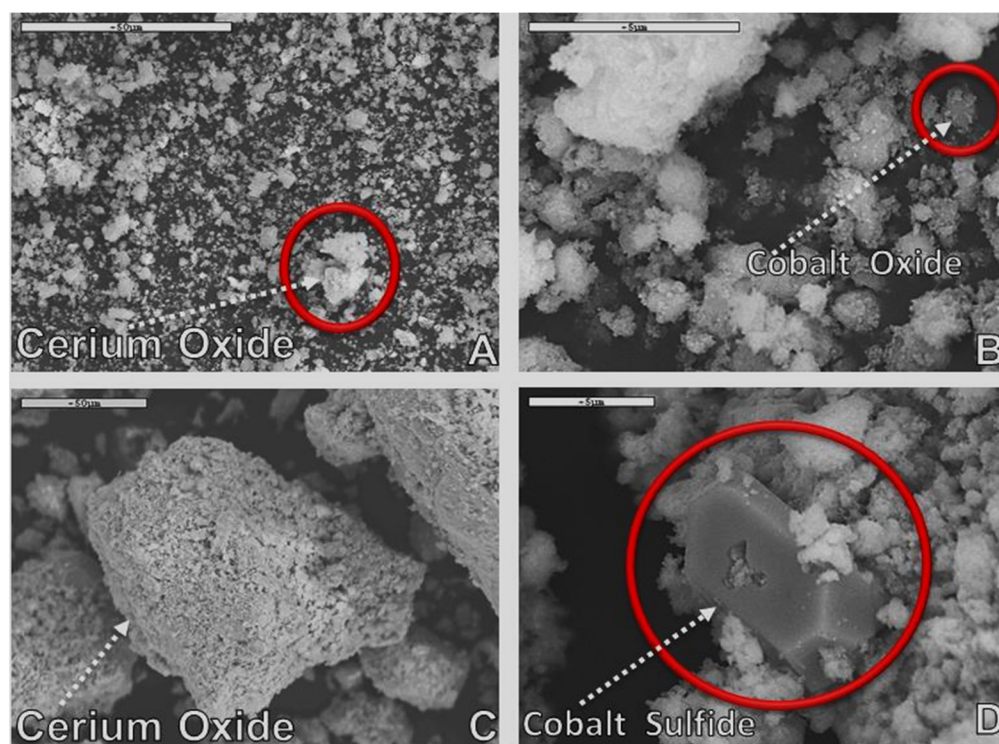


**Figure 8.** X-ray diffraction patterns of the (a) “untreated” and (b) “sulfided” catalysts. The “sulfided” catalyst was exposed for 10 h in a reaction mixture containing 1 v/v% H<sub>2</sub>S and 90 v/v% H<sub>2</sub>O, balanced in Ar, at T = 850 °C.



Surface modifications of the catalysts were further investigated by SEM/EDS analysis. Micrographs of the “untreated” and “sulfided” catalysts are presented at different magnifications in Figure 9. By comparing the SEM images of the “untreated” (Figure 9A,B) and “sulfided” (Figure 9C,D) samples, it is clear that the latter catalyst has undergone significant morphological modifications, leading to the formation of new phases, as a result of its exposure in  $\text{H}_2\text{S}/\text{H}_2\text{O}$  mixture at high temperatures. In particular, the formation of cobalt sulfide phases of polygon-like shape and cerium oxide particles of sponge-like morphology were revealed. Moreover, the average size of the cobalt-containing particles of the “sulfided” catalyst notably increased compared to the “untreated” catalyst, implying sintering under reaction conditions, in compliance with the above-discussed XRD and BET results.

In complete agreement with the identification of cobalt sulfide phases, a significant amount of sulfur (both in the form of elemental sulfur and in S-containing phases) was detected by sulfur elemental analysis of the “sulfided” sample (6.5 wt.%). However, this amount was approximately half compared to the elemental sulfur detected on the same sample when exposed to 1 v/v%  $\text{H}_2\text{S}$  balanced with an Ar feed mixture for 10 h (13.1 wt.%). The considerably lower amount of elemental sulfur in the case of wet conditions is most probably ascribed to the formation of sulfur-containing gaseous products, predominantly  $\text{SO}_2$ , as dictated by Equation (1). Notably, the relevant elemental mapping (not shown) demonstrated that sulfur formation and deposition was preferentially favored in the vicinity of Co-rich areas instead of  $\text{CeO}_2$ -rich regions.



**Figure 9.** SEM images of the “untreated” (A,B), and “sulfided” (C,D), catalysts. The “sulfided” catalyst was exposed for 10 h in a reaction mixture containing 1 v/v%  $\text{H}_2\text{S}$ –90 v/v%  $\text{H}_2\text{O}$ , balanced in Ar, at  $T = 850^\circ\text{C}$ .

In view of the above findings, the already established superiority of the 30-Co/ $\text{CeO}_2$  catalyst for the  $\text{H}_2\text{S}$  decomposition reaction under extremely wet conditions (90 v/v%  $\text{H}_2\text{O}$ ) should be mainly related to the in situ sulfidation of cobalt species (i.e.,  $\text{Co}_3\text{O}_4$  to  $\text{Co}_3\text{S}_4$  and  $\text{CoS}$ ), during its exposure to the reaction atmosphere. The previous analysis has clearly shown that during the catalytic decomposition of  $\text{H}_2\text{S}$  in the presence of  $\text{H}_2\text{O}$ , the 30-Co/ $\text{CeO}_2$  catalyst demonstrates the optimum activity performance and, at the same



time, a remarkably stable behavior. It should be therefore deduced that the produced elemental sulfur is not simply deposited on the catalyst surface but strongly interacts with the catalyst counterparts to create new active and stable phases. These promising findings could pave the way for the development of active and stable materials to be applied as heterogeneous catalysts for the thermocatalytic decomposition of  $\text{H}_2\text{S}$  in the presence of excess steam or as anode electrodes in  $\text{H}_2\text{S}$  splitting proton-conducting solid electrolyte electrochemical membrane reactors for the efficient management of  $\text{H}_2\text{S}$  emissions toward carbon-free hydrogen production.

### 3. Materials and Methods

#### 3.1. Materials Preparation

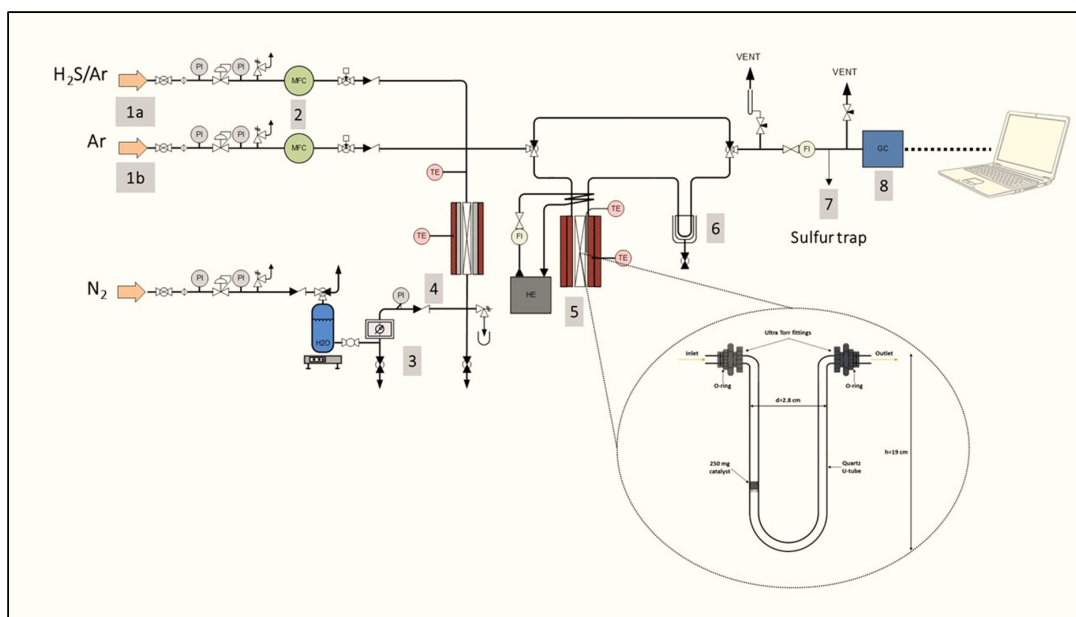
A series of  $\text{Co}_3\text{O}_4/\text{CeO}_2$  supported catalysts at different cobalt loadings (0, 20, 30, 40, 60, and 100 wt.%) was synthesized via the wet impregnation technique. The as-prepared catalysts are henceforth denoted as x-Co/ $\text{CeO}_2$  for simplicity, with x referring to the weight percentage of Co in the composite materials. The synthetic protocol followed has been described in detail elsewhere [46]. In brief, the ceria-supported cobalt oxide catalysts were prepared by impregnation of an aqueous solution with appropriate concentrations of cobalt nitrate onto the calcined  $\text{CeO}_2$  support. The resulting solutions were subsequently heated under continuous stirring and then dried at 100 °C overnight. Finally, the obtained dried samples were calcined in air at 600 °C for 2 h using a heating rate of 5 °C/min.

#### 3.2. Materials Characterization

The textural, structural, and morphological characteristics of bare oxides and as-prepared cobalt oxide/ceria catalysts were determined by means of BET, XRD, and SEM/EDX methods, as previously described in detail [43]. The elemental analysis of sulfur content was conducted according to UOP 703 method on a “CHN-800” elemental analyzer (LECO Corporation, St. Joseph, MI, USA).

#### 3.3. Catalytic Evaluation

The experimental apparatus employed for the  $\text{H}_2\text{S}$  decomposition catalytic studies under excess  $\text{H}_2\text{O}$  conditions has been described in our previous work [46] and is graphically represented in Figure 10. In particular, the experimental setup is comprised of the feed, reaction, and analysis sections. The feedstock system includes the 10 v/v%  $\text{H}_2\text{S}/\text{Ar}$  (Air Liquide Hellas, Athens, Greece) and pure Ar (99.998 v/v%, Linde Hellas, Sindos, Greece) high-pressure gas cylinders, the corresponding mass flow controllers (Brooks Instruments, Hatfield, Montgomery County, PA, USA) with a range of 0–20  $\text{cm}^3/\text{min}$  for the  $\text{H}_2\text{S}/\text{Ar}$  mixture and 0–100  $\text{cm}^3/\text{min}$  for Ar at an accuracy of 1% and a digital bubble flow meter (Agilent Optiflow 520, Santa Clara, CA, USA) to regulate and monitor the volumetric gas flow rates, an HPLC 305 Pump (GILSON, Middleton, WI, USA) with a flow range between 0.14–25  $\text{cm}^3/\text{min}$  and an accuracy of 0.001  $\text{cm}^3/\text{min}$  to control the doubly distilled liquid  $\text{H}_2\text{O}$  supply into the system, the preheater for steam generation at 130 °C and the heated stainless steel pipelines to provide the desired reactant mixture to the reactor, controlled at 130 °C by a K-type thermocouple. Appropriate flows of pure Ar and 10 v/v%  $\text{H}_2\text{S}/\text{Ar}$  were mixed with steam derived by a liquid water supply of ca. 0.05  $\text{cm}^3/\text{min}$  so as to obtain the desired reactants feed mixture of 1 v/v%  $\text{H}_2\text{S}$  and 90 v/v%  $\text{H}_2\text{O}$ , balanced in Ar.



**Figure 10.** Schematic representation of the apparatus used in the catalytic experiments. Feed section: (1) (1a) 10 v/v% H<sub>2</sub>S/Ar cylinder, (1b) Pure Ar cylinder; (2) MFC: Mass Flow Controllers for H<sub>2</sub>S/Ar and Ar; (3) Doubly distilled liquid water pump; (4) Preheater for steam generation. Reaction section: (5) High-temperature furnace and U-tube quartz reactor; (6) Condenser; (7) Sulfur trap. Analysis section: (8) GC: Gas Chromatograph. PI: Pressure Indicator; FI: Flow Indicator; TE: Temperature Indicator; HE: Heat Exchanger. Adapted from Ref. [46].

A typical quartz U-tube fixed bed reactor with an internal diameter of 9.6 mm was employed for the activity and stability of H<sub>2</sub>S decomposition experiments at excess H<sub>2</sub>O conditions. In each test, the catalyst bed consisted of a mixture of 250 mg catalyst and 250 mg quartz, both in powder form, resulting in a bed volume of ~0.45 cm<sup>3</sup>. Catalytic experiments were elaborated at atmospheric pressure and total feed rate equal to 100 cm<sup>3</sup>/min, corresponding to a GHSV of ~13,300 h<sup>-1</sup>.

The analysis of the produced hydrogen was carried out by means of a gas chromatograph (Shimadzu 14B, Kyoto, Japan) involving a thermal conductivity detector (TCD) and a molecular sieve 5A separation column. Prior to gas analysis, the reactor effluent gas mixture was flowing through a sulfur scrubber involving an aqueous KOH solution for the removal of any S-containing species.

During the catalytic activity tests, the temperature was increased at intervals of 50 °C, and the reaction was carried out in the temperature range of 550–850 °C. At the initial temperature of 550 °C, the system was left to stabilize for more than 4 h, and then for each temperature step, the system was allowed to reach a steady state (~1 h) before the effluent gas analysis was performed. Short-term stability tests were also carried out isothermally at 850 °C, where the hydrogen production rate was continuously monitored. For comparison purposes, blank experiments (without catalyst) were also carried out under specified reaction conditions. In the present work, the catalytic performance of the Co<sub>3</sub>O<sub>4</sub>/CeO<sub>2</sub> mixed oxide samples is expressed in terms of hydrogen production rate (μmol H<sub>2</sub>·g<sup>-1</sup>·s<sup>-1</sup>), calculated by the following equation (Equation (3)):

$$r_{\text{H}_2} (\mu\text{mol H}_2 \cdot \text{g}^{-1} \cdot \text{s}^{-1}) = \frac{10^6 \cdot F_{\text{out}} \cdot [\text{H}_2]_{\text{out}}}{60 \cdot V_M \cdot g_{\text{cat}}} \quad (3)$$

where  $F_{\text{out}}$  (cm<sup>3</sup>/min) is the reactor outlet flowrate,  $[\text{H}_2]_{\text{out}}$  is the molar fraction of hydrogen at the reactor outlet,  $V_M$  (cm<sup>3</sup>/mol) is the molar volume of hydrogen at 1 bar and 25 °C, equal to 24,465 cm<sup>3</sup>/mol, and  $g_{\text{cat}}$  is the catalyst mass. In addition, H<sub>2</sub>S conversion under

dry reaction conditions (i.e., absence of excess H<sub>2</sub>O) was estimated on the basis of the following expression (Equation (4)):

$$X_{\text{H}_2\text{S}} (\%) = \frac{\text{moles of produced H}_2 \text{ at the outlet}}{\text{H}_2\text{S moles at the inlet}} \cdot 100 \quad (4)$$

Moreover, thermodynamic equilibrium values were calculated using an RGibbs block in Aspen Plus software. The components involved in the simulation were elemental sulfur, H<sub>2</sub>S, H<sub>2</sub>O, SO<sub>2</sub>, H<sub>2</sub>, SO<sub>3</sub>, O<sub>2</sub>, and Ar, and their thermophysical properties were obtained by applying the Peng-Robinson equation of state.

#### 4. Conclusions

In the present work, the H<sub>2</sub>S decomposition activity of a series of Co<sub>3</sub>O<sub>4</sub>/CeO<sub>2</sub> catalysts with variable cobalt loadings (0–100 wt.%) was evaluated toward carbon-free hydrogen production under extremely harsh reaction conditions employing a feed mixture comprising of 1 v/v% H<sub>2</sub>S and 90 v/v% H<sub>2</sub>O at high temperatures (550–850 °C) and atmospheric pressure. Furthermore, the analysis of the experimental results is accompanied and corroborated by thermodynamic calculations in order to gain insight into the beneficial effect of steam addition on the production rate of H<sub>2</sub>. It was revealed that the 30 wt.% Co<sub>3</sub>O<sub>4</sub>/CeO<sub>2</sub> catalyst demonstrated the optimum activity and the lower apparent activation energy, followed by remarkable stability. Notably, Co<sub>3</sub>O<sub>4</sub>/CeO<sub>2</sub> catalysts outperform bare ceria and cobalt oxide under wet conditions, implying a synergistic cobalt oxide–ceria interaction towards higher H<sub>2</sub> production rates via H<sub>2</sub>S steam reforming. The enhancement in the production of hydrogen was also assessed by comparing the performance of the optimum 30-Co/CeO<sub>2</sub> catalyst under dry and water-excess reaction conditions. Notably, significant augmentation in the H<sub>2</sub> production rate was disclosed in the presence of steam.

Equally importantly, the key role of in situ sulfidation was revealed in stability tests over 30-Co/CeO<sub>2</sub>. Intriguingly, the pretreatment of the sample with the reacting H<sub>2</sub>S–H<sub>2</sub>O–Ar mixture (“sulfided”) led to the formation of active cobalt sulfide phases that allowed the system to faster reach steady state compared to the “untreated” and “reduced” sample. A complementary characterization study over both “untreated” and “sulfided” samples revealed the complete collapse of pore structure after catalysts exposure to reaction conditions, followed, however, by the formation of new cobalt sulfided phases, such as Co<sub>3</sub>S<sub>4</sub> and CoS, which could be considered responsible for the excellent performance and stable behavior of the as-prepared cobalt oxide–ceria catalysts.

**Author Contributions:** Conceptualization, T.K. and G.E.M.; methodology, T.K.; software, G.V.; validation, G.V., G.E.M. and M.K.; formal analysis, G.V. and M.K.; investigation, T.K. and G.V.; resources, G.E.M.; data curation, G.E.M. and M.K.; writing—original draft preparation, T.K.; writing—review and editing, G.V., G.E.M. and M.K.; visualization, G.V.; supervision, G.E.M. and M.K.; project administration, G.E.M.; funding acquisition, G.E.M. All authors have read and agreed to the published version of the manuscript.

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**Data Availability Statement:** Not applicable.

**Conflicts of Interest:** The authors declare no conflict of interest.

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Review

# Magnetic Nanomaterials as Catalysts for Syngas Production and Conversion

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**Abstract:** The conversion of diverse non-petroleum carbon elements, such as coal, biomass, natural/shale gas, and even CO<sub>2</sub>, into cleaner hydrocarbon fuels and useful chemicals relies heavily on syngas, which is a combination of CO and H<sub>2</sub>. Syngas conversions, which have been around for almost a century, will probably become even more important in the production of energy and chemicals due to the rising need for liquid fuels and chemical components derived from sources of carbon other than crude oil. Although a number of syngas-based technologies, including the production of methanol, Fischer–Tropsch (FT) synthesis, and carbonylation, have been industrialized, there is still a great need for new catalysts with enhanced activity and adjustable product selectivity. New novel materials or different combinations of materials have been investigated to utilize the synergistic effect of these materials in an effective way. Magnetic materials are among the materials with magnetic properties, which provide them with extra physical characteristics compared to other carbon-based or conventional materials. Moreover, the separation of magnetic materials after the completion of a specific application could be easily performed with a magnetic separation process. In this review, we discuss the synthesis processes of various magnetic nanomaterials and their composites, which could be utilized as catalysts for syngas production and conversion. It is reported that applying an external magnetic field could influence the outcomes of any applications of magnetic nanomaterials. Here, the possible influence of the magnetic characteristics of magnetic nanomaterials with an external magnetic field is also discussed.

**Keywords:** magnetic materials; catalysts; magnetic separation; syngas; CO<sub>2</sub> conversion

## 1. Introduction

There has been a lot of scientific interest in the production of syngas (H<sub>2</sub> + CO) from biomass by gasification, a thermochemical conversion process that occurs in an oxygen-lean environment [1–3]. Syngas offers an effective alternative as a fuel for transferring energy, a raw material for creating hydrogen fuel, and a source of higher-value chemicals. Through more effective syngas-based power generation facilities and fuel cell technologies, syngas



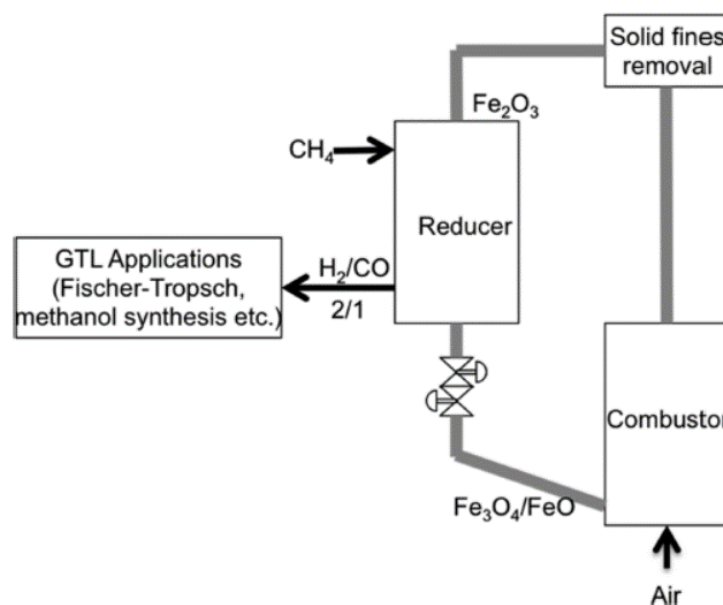
production significantly reduces greenhouse gas emissions, particularly carbon dioxide (CO<sub>2</sub>) emissions [4]. Nevertheless, it is thought that precious metal-based catalysts are the best option for producing syngas. However, significant limitations, including massive cost and unavailability, will eventually prevent their widespread use. Because of this, new non-precious metal materials have been developed as substitutes [5]. By enabling reagent adsorption and surface reactions on magnetized Fe catalysts as well as non-magnetic materials, magnetic fields can significantly improve these metals' catalytic activity. This improves selectivity to hydrocarbons and lowers apparent activation energy [6]. Although there are various metals used for syngas production using magnetic effects, Fe, Ni, and Co metals play a significant role in the production of syngas. Additionally, they have been used to generate electrically conductive materials and enhance the mechanical performance of composites. The qualities of magnetic nanoparticles include their capacity to transport other substances, their quantum characteristics, and their high surface-area-to-volume ratio. Magnetic fields can be used to alter the characteristics of magnetic nanoparticles to make them appropriate for a variety of applications, including syngas production, on a large scale. The efficiency of magnetic fields relies on the field gradient and particle magnetic moment. Based on the material, the optimum magnetic nanoparticles are between 10 and 20 nm in size as, above a certain temperature known as the blocking temperature, these particles unite into a single domain and show superparamagnetic activity [7]. However, this also leads to intrinsic instabilities over extended periods and magnetic loss because of chemically highly active bare metallic nanoparticles. The particularly attractive characteristics of spherical and cubic magnetic nanoparticles have attracted a lot of interest. It is noteworthy that these nanoparticles have been efficiently used in the pharmaceutical field for drug delivery, high-contrast MRI, DNA detection, and stem cell labeling/separation. In an initiative aimed at improving the catalytic efficiency in syngas production by using magnetic nanoparticles, it has also shown an efficient effect. This review discusses recent progress made on the effective utilization of magnetic nanomaterials for syngas production/conversion and the effective way of utilizing an external magnetic field for the synthesis of magnetic catalysts and for the adjustment of the efficiency of the synthesis/conversion process.

## 2. Magnetic Materials for Syngas Production/Conversion

Magnetic nanomaterials are found to be interesting in various applications due to their unique magnetic response behavior compared to other available nanomaterials. These materials are generally classified as magnetic and non-magnetic materials. Furthermore, they have sub-classifications, including dia, para, ferro, ferri, and antiferro, depending on the magnetic characteristics. Depending on the shape and size, their magnetic behavior is further classified as soft and hard magnetic materials. As a catalyst, transition metals are considered a support substance for the generation of syngas because of their mechanical, electrochemical, and metallic-like qualities. This may change a precious metal overlayer's catalytic characteristics. Transition metals had been synthesized using a nitriding technique that was carried out in the absence of hydrocarbons and only produced residual physisorbed N that easily desorbed as N<sub>2</sub> off the catalyst surface, in contrast to the situations of carbide and sulfide-based substrates [8]. When selecting active metals for the conversion of syngas into various sorts of products, we may be able to use the ability of CO dissociative adsorption as a guide. Due to their low adsorption heat, transition metals on the right of the periodic chart, including Cu and Pd, are not CO dissociative [9]. With the C-O bond uncleaved during CO hydrogenation, Cu and Pd are quite well-active phases for the production of methanol. However, the transition metals on the left of the periodic table, including Mo and W, exhibit a strong capacity for CO dissociative adsorption and the formation of metal carbides [10]. In contrast to Mo and W metals, Mo and W carbides are capable of activating CO differently and exhibit CO hydrogenation activity. Fe, Co, and Ru are appropriate for CO hydrogenation (Sabatier's principle) due to the moderate efficiency of CO adsorption on these metals. Rh is a promising candidate for ethanol formation from syngas because it is situated at the boundary of the CO dissociation and non-dissociation

regions. Notably, the balance between CO and H<sub>2</sub> dissociation capacities plays a crucial role in defining product selectivity. In Fischer–Tropsch (FT) synthesis, product selectivity is determined by the balance between both hydrogenation and C–C coupling abilities on metal surfaces. Typically, a catalyst with an excessively high H<sub>2</sub> dissociation or hydrogenation capacity may result in the creation of CH<sub>4</sub> with higher selectivity. Ni can be used, for instance, in the dissociation of CO. As stated earlier, the main active metals investigated for FT synthesis are Fe, Co, and Ru since they are appropriate for the synthesis of significant cumulative hydrocarbons. Ru is the most effective catalyst among these three metals for CO hydrogenation, and CO hydrogenation on Ru can take place at low temperatures. Ru has a higher affinity for long-chain hydrocarbons and a low affinity for CH<sub>4</sub>; however, due to its high cost and restricted supply, Ru cannot be used as the primary active ingredient in large-scale industrial applications. Fe and Co have so far only been used in industrial FT processes as active metals. Ru is appropriate for basic study, nevertheless, as an excellent FT active metal that can offer significant insight into the catalytic reaction mechanism. Additionally, Ru is frequently employed in FT catalysts as a stimulant to speed up the reduction of Co or Fe because it is difficult to reduce Co or Fe precursors under normal circumstances [11]. Although Fe is less expensive than Co, Co catalysts are typically more active and selective to linear long-chain hydrocarbons. Co catalysts are also frequently more water-resistant than other types of catalysts. As a result, Co catalysts have drawn a lot of interest for the production of long-chain linear hydrocarbons from syngas, such as wax and diesel fuel. In contrast, Co catalysts can only function effectively at restricted temperature ranges and H<sub>2</sub>/CO ratios, whereas Fe-based catalysts can operate under a variety of temperatures and H<sub>2</sub>/CO proportions without significantly increasing CH<sub>4</sub> preference. It is important to note that, relative to Co- or Ru-based catalysts, Fe-based catalysts demonstrate vastly greater activity for the water–gas system process. This is beneficial for converting syngas made from coal or biomass that has a lower H<sub>2</sub>/CO ratio, but it is not desired for converting H<sub>2</sub>-rich syngas made from natural gas or shale gas. For Fe catalysts to provide acceptable activity and selectivity, more substantial changes are typically needed, and quick catalytic deactivation is a major difficulty for Fe catalysts.

Solid oxygen carriers, which can be either single metal oxides or combinations of metal oxides, can be used to provide oxygen for this partial oxidation process. Zhu Xing et al. demonstrated the synthesis of syngas and hydrogen through two-step steam reforming of methane on a CeO<sub>2</sub>-Fe<sub>2</sub>O<sub>3</sub> oxygen carrier [12]. In their work, in a fixed-bed reactor, temperature-programmed interactions between methane and the oxygen carrier CeO<sub>2</sub>-Fe<sub>2</sub>O<sub>3</sub> were carried out to find the ideal temperature for the gas–solid reaction that produces syngas. They noticed that the smooth onset of CH<sub>4</sub> conversion starts at about 500 °C using temperature as a function of reaction. However, below 650 °C, the conversion is really low. The fact that conversion increases quickly with a temperature over 650 °C suggests that reaction temperature has a significant impact on methane oxidation by solid oxides and that a higher temperature is required to produce syngas through a gas–solid reaction. This might be attributed to the fact that the rate of lattice oxygen migration from the bulk to the surface accelerates with increasing temperature. On the CH<sub>4</sub> conversion curve, they also noticed a slight peak at about 600 °C. CeO<sub>2</sub>-Fe<sub>2</sub>O<sub>3</sub> has a higher CH<sub>4</sub> conversion when the temperature exceeds 800 °C. Since oxidation reactions at low temperatures are typically aided by the surface adsorption of oxygen on oxides, this is expected to be caused by the well-released bulk lattice oxygen in CeO<sub>2</sub>-Fe<sub>2</sub>O<sub>3</sub>. High-pressure experiments were carried out for the reduction and oxidation of oxygen carrier particles in a dedicated thermogravimetric analyzer as part of a study on Fe-oxide-based oxygen carriers for syngas production from methane by Niranjani Deshpande et al. [13]. The partial oxidation of CH<sub>4</sub> for syngas production using a Fe-oxide-based system is shown in Figure 1.



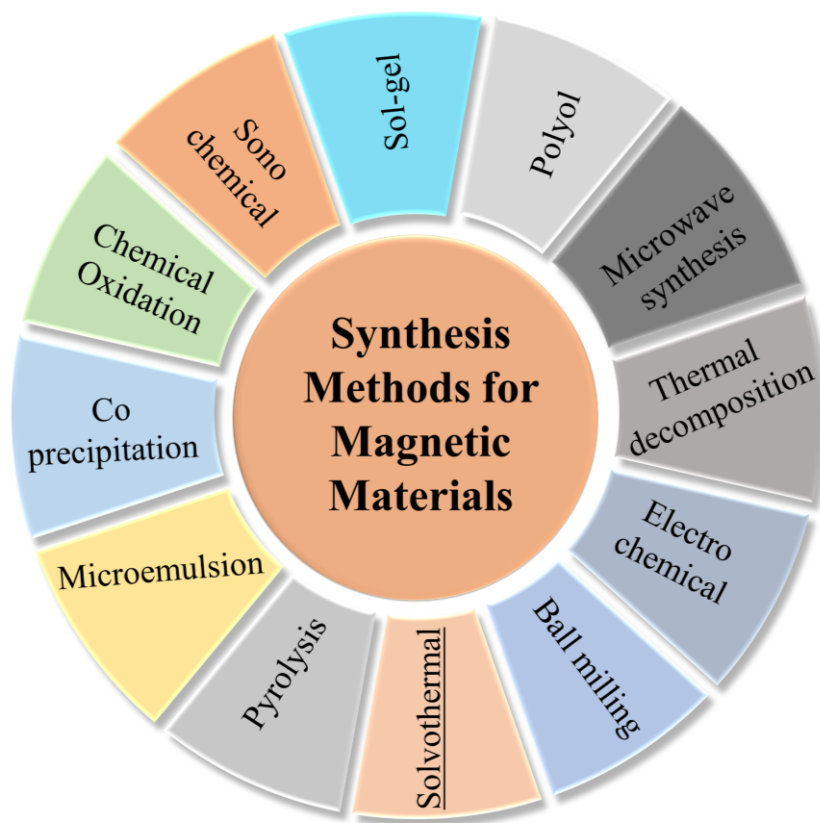
**Figure 1.** Illustration of the  $\text{CH}_4$  partial oxidation-based Fe-oxide system for producing syngas. Reprinted from [13]. Copyright (2015), with permission from the American Chemical Society.

Due to their low cost and high magnetization capability, transition metals have generated interest [14]. Nevertheless, when contrasted to their respective mono-metal counterparts, bimetallic alloys have more applications and qualities, which have made them particularly attractive to researchers. Recently, there have been various attempts to use bimetallic catalysts in catalyzed reactions [15]. Bimetallic catalysts are considered successful because they are made up of two different metals with large dispersion and active sites due to the combination of their parent metals. Additionally, the creation of a solid solution improves the physical and chemical characteristics of bimetallic catalysts. A bimetallic catalyst exhibits a greater carbon yield than a monometallic catalyst, according to Pudukudy et al. [16]. Hydrothermal, pyrolytic, Sol–gel, sonochemical, radiolytic, microwave combustion, impregnation, microemulsion, and precipitation methods are a few of the physical and chemical processes that have been used to create bimetallic alloys. Researchers are still drawn to studying the synthesis of bimetallic magnetic alloys for the synthesis of syngas production [17]. The most prominent alloys used for syngas production comprise elements such as Ni, Co, and Fe. As catalysts, alloys perform better. Siddhartha Sengupta et al. synthesized  $(\text{Ni}/\text{Al}_2\text{O}_3)$ ,  $(\text{Ni-Co}/\text{Al}_2\text{O}_3)$ , and  $(\text{Co}/\text{Al}_2\text{O}_3)$  catalysts with 15 % metal content. They observed that the initial turnover frequencies of reforming  $\text{CH}_4$  for the  $\text{Ni-Co}/\text{Al}_2\text{O}_3$  catalysts were higher than those for  $\text{Ni}/\text{Al}_2\text{O}_3$ , indicating that the Ni-Co alloy sites are more active than the Ni sites [18]. Through calcination and reduction of hydrotalcite-like compounds comprising  $\text{Ni}^{2+}$ ,  $\text{Cu}^{2+}$ ,  $\text{Mg}^{2+}$ , and  $\text{Al}^{3+}$ , Dalin Li et al. created Ni-Cu/Mg/Al bimetallic catalysts that were then tested for the steam reforming of tar developed by a low-temperature pyrolysis of biomass. Even at a low temperature of 823 K, the catalyst provided almost an complete conversion of the tar [19]. The higher metal dispersion, greater number of surface active sites, better oxygen affinity, and surface alteration brought on by the production of small Ni-Cu alloy particles all contributed to this high performance. Non-supported alloys with their distinct morphological features were synthesized by Buthainah Ali et al. and used in catalytic biogas decomposition to produce syngas and carbon bio-nanofilaments at a reaction temperature of 700 °C and 100 mL  $\text{min}^{-1}$ . The behavior of the catalysts,  $\text{CH}_4$  and  $\text{CO}_2$  conversion, and the carbon generated during the reaction were studied [17]. Irrespective of metals, alloys, and oxides, magnetic materials are selected as the better candidates for the catalyst process due the above discussed reasons, along with their magnetic characteristics. Various magnetic nanomaterials and their composites could be utilized as catalysts for syngas production/conversion. The

next section will discuss the different synthesis methods that could be utilized for the preparation of magnetic nanocatalysts.

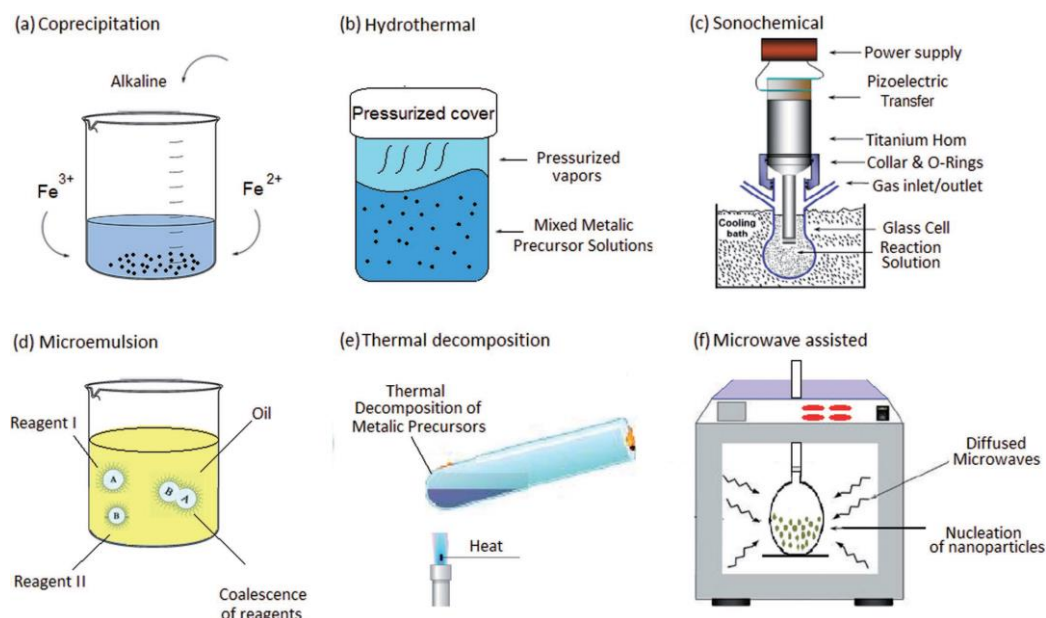
### 3. Synthesis of Magnetic Nanomaterials

To date, a variety of methods have been developed for the synthesis of magnetic nanomaterials and nanocomposites, viz. wet chemical route, microfluidic process, hydrothermal process, arc plasma discharge, chemical vapor deposition, microemulsion method, biogenic route, etc. Recently, there has been a heightened interest in synthesizing magnetic nanoparticles of uniform size for various technological applications [20]. Likewise, magnetic nanoparticle synthesis is one of the most critical challenges in tailoring particle size, shape, and crystalline structure. A wide range of magnetic nanostructures, including metals, metal alloys, oxides, and composite structures, have been synthesized using numerous techniques. Magnetic nanoparticles are prepared using three different methods, including (i) incipient wetness impregnation, (ii) precipitation, and (iii) modified sol–gel, to obtain different sizes of magnetic nanoparticles through synthesis. However, synthesis methodology plays a key role in controlling morphology, catalyst particle size, size distribution, and surface area. For example, A. Alayat et al. reported that a Fe/NS-I catalyst that was prepared using wetness impregnation and activated by CO has the highest activity and that its selectivity falls within the range of gasoline C6–C14 [21]. By contrast, the other Fe/NS catalysts show poor catalytic activity and selectivity when these Fe/NS catalysts were prepared using precipitation and modified sol–gel methods. The optimal preparation and activation methods to reach the highest catalytic activity and selectivity toward light hydrocarbons are with the Fe/NS-I catalyst activated by CO. In addition, the Fe/NS-I catalysts' selectivity favors aromatics in the C6–C14 range. In this section, we will describe some methods that provide excellent size and shape control for preparing magnetic nanomaterials, as shown in Figure 2.



**Figure 2.** Different approaches for the preparation of magnetic nanoparticles.

Wet chemistry methods, which employ macro-scale equipment to carry out the reactions, enable batch production of nanoparticles. In comparison to microfluidic and biogenic synthesis, conventional MNP synthesis uses more energy [22]. Furthermore, it is more difficult to control morphology. Wet chemical routes are divided into hydraulic and non-hydraulic techniques, as shown in Figure 3, each of which has advantages and disadvantages depending on various variables, such as reaction temperature, pH value, precursor type, ratio of precursors, and nature of the base, which are the critical parameters that influence the size of magnetic nanoparticles [23]. With increasing pH, primary magnetite nanoparticles repel each other, thus becoming smaller [24]. The stoichiometry of the final magnetic nanoparticles could be altered by adjusting the ratio of precursors. The size of magnetic nanoparticles could be controlled by introducing a surfactant or by adjusting the reaction temperature. Wet chemistry method is considered one of the low-cost and simple chemical processes as it does not require any higher-cost equipment and processing. R. A. Frimpong et al. reported that the wet coprecipitation method used to prepare iron oxide nanoparticles gives a wide size distribution of magnetic nanoparticles [25] due to their chemical stability and biocompatibility compared to other metallic magnetic properties. Therefore, many investigations have focused on the development of large-scale production methods of uniform magnetic nanoparticles.



**Figure 3.** Schematics of distinct wet-chemistry hydrolytic and non-hydrolytic strategies for the synthesis of magnetic nanoparticles, (a) co-precipitation, (b) hydrothermal, (c) sonochemical, (d) microemulsion, (e) thermal decomposition, and (f) microwave assisted process. Reprinted with permission from [23], John Wiley & Sons, Inc.

In arc plasma technology, the plasma field provides the energy and reaction environment needed for atomic excitation, collision bonding, and more rapid formation of nanophase structures [26]. Using the arc plasma technique, high-temperature (>3000 degrees Celsius) plasma is generated between closely spaced electrodes under an inert atmosphere of helium or argon using a direct current. In this process, an electrode substance is evaporated by controlling the arc discharge, and the corresponding products are obtained upon cooling down on a cathode or a vacuum chamber wall [27]. Wang et al. reported that a minimum RL of −56.3 dB at 12.1 GHz and an absorption bandwidth of 5.2 GHz are obtained in the multi-step synthesis process [26]. Arc plasma is first used to prepare magnetic metal particles, which are then combined with carbon compounds. Methane (CH<sub>4</sub>) is employed as a gaseous source of carbon in the reactor vessel.

Hydrothermal process is another easy and one-step way to develop hydrophilic magnetite nanomaterials using various precursors. There are many methods that have been used to develop magnetic metal oxide nanoparticles [28]. Hydrothermal synthesis of  $\text{Fe}_3\text{O}_4$  nanoparticles in organic solvents is an advantageous process because of the homogeneity of the procedure and its comparatively low environmental impact. In a study by Misuthani et al., an aqueous solution containing ferrous and ferric ions is used as a starting solution, followed by precipitations of ferrous hydroxide ( $\text{Fe}_3(\text{OH})_2$ ) and goethite ( $\alpha\text{-FeOOH}$ ), which are precipitated in an alkaline solution as precursors [29]. The research by Zhang et al. demonstrated parameters that cause aqueous solutions to reach a critical or supercritical state, and these parameters are of interest because they allow the almost simultaneous reduction of two metal salts at a high temperature and high pressure [30]. They used the hydrothermal synthesis route to create magnetic CoPt alloy nanowires based on this method. Komarneni et al. first reported the synthesis of crystalline unit oxides, such as  $\text{TiO}_2$ ,  $\text{ZrO}_2$ , and  $\text{Fe}_2\text{O}_3$ , as well as binary oxides, such as  $\text{KNbO}_3$  and  $\text{BaTiO}_3$ , using the microwave hydrothermal method. Using microwave-hydrothermal conditions, the influences of several factors, such as chemical concentration, duration, and temperature, on crystallization kinetics at a microwave frequency of 2.45 GHz were investigated [31]. The reaction parameters, such as reaction temperature, reaction time, ratio of the precursors, and fraction of the surfactant, could be varied to obtain magnetic nanoparticles with different morphologies.

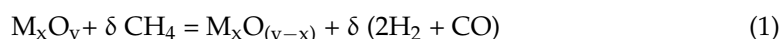
Solvothermal crystallization is one of the most consistent processes for crystal growth, and the resulting grains of magnetite have a significantly higher crystallinity than those made by other processes. The solvothermal fabrication process is similar to hydrothermal fabrication, which uses non-aqueous organic solvents. In solvothermal techniques, organic solvents, such as methanol, toluene, 1,4-butanediol, and amines, are frequently employed. Organic solvents are used as the solvents in these solvothermal processes. The solvothermal method's ability to control water-sensitive precursors is its most significant advantage. J. Li et al. simultaneously demonstrate that solvothermal techniques may be utilized in conjunction with microwaves and magnetic fields for the semicontinuous synthesis of materials with much increased repeatability and excellent quality [32].

The thermal decomposition process is another conventional process for the synthesis of various magnetic nanoparticles. However, the major disadvantage of this process is that it may require high-cost chemicals to produce magnetic nanoparticles, such as FePt, CoPt, and other related magnetic nanoparticles. A. G. Roca et al. evaluated the synthesis of monodispersed  $\text{Fe}_3\text{O}_4$  nanoparticles by focusing solely on the thermal decomposition of organometallic precursors in organic solvents at high temperatures in the presence of surfactants. They yielded nanoparticles that are not hydrophilic in nature and cannot be dispersed in water, impeding their biomedical applications [33]. Other than the above discussed methods, a few more specifically designed synthesis methods for magnetic nanomaterials have also been successfully demonstrated, namely the sol-gel auto-combustion method, polyol process, chemical oxidation methods, and different deposition processes. However, each method and process has its own advantages and disadvantages. Depending on the requirements of the targeted particle's physicochemical characteristics, one can choose an appropriate synthesis process for the development of magnetic nanomaterials. Furthermore, experimental parameters, such as reaction temperature, precursors, precursors ratio, oxidation or reduction agent fraction, surfactant or stabilizing agent, reaction time, and post-thermal treatment, could be used to alter the physicochemical characteristics of magnetic nanomaterials.

#### 4. Syngas Production and Conversion

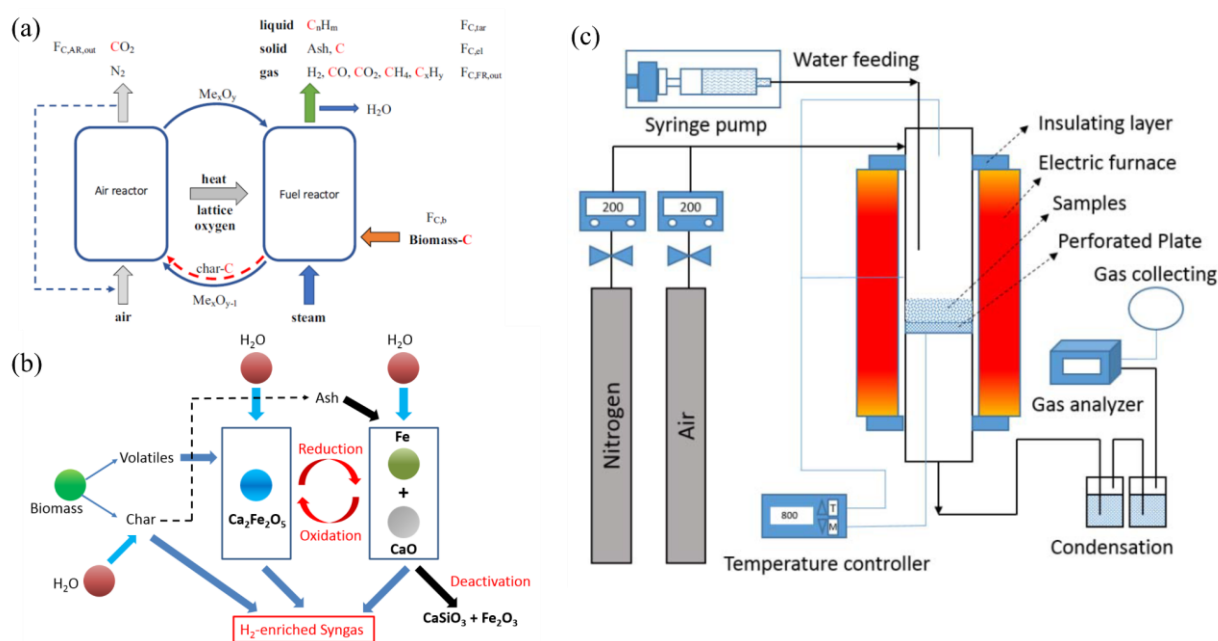
Syngas production and conversion have been the focus of recent research. Several processes have been demonstrated for the production and conversion of syngas. Syngas can be created by gasifying waste, biomass, or coal in a high-temperature atmosphere. Syngas is a gaseous fuel created when a feedstock is partially oxidized in controlled

operating conditions with a deficiency in oxygen. In a gasifier, gasification generally consists of five steps. In order to produce an incredibly clean gas at the exhaust, drying must first take place below 100 °C, with the goal of lowering the moisture content of the feedstock. The dry matter is scorched to a temperature of about 240 °C during pyrolysis as a result of the vaporization of heavy volatile chemicals (tars). In addition to hydrogen and carbon monoxide, tars contain more sophisticated compounds. A solid carbonaceous substance known as charcoal, which is composed of fixed carbon-to-carbon chains, is also produced by this process along with tar gasses. The conversion of biomass into a more useful energy form can be achieved using three main processes: (i) gasification, (ii) pyrolysis, and (iii) combustion [34]. Similar solid fuel feedstocks, such as coal, biomass, and wastes, are used in the production of syngas using traditional gasification techniques. Additionally, non-gasification technologies that employ a single reforming process or a series of catalyst-assisted reforming processes can convert liquid and gaseous feedstocks into syngas. Such procedures are anticipated to be effective in in situ syngas production techniques, as described in this section. Using chemical looping gasification in biomasses, the generation of syngas is depicted in Figure 4a. Firstly, the biomass is processed and devolatilized as it enters the fuel reactor. Additionally, there are numerous simultaneous interactions between the various pyrolysis products, the gasification agent (steam or CO<sub>2</sub>), and the oxygen carrier. When tar is gasified with steam, it generates syngas, CO, or CO<sub>2</sub>, as appropriate. Thirdly, during the pyrolysis and gasification of the biomass, redox reactions take place between both the active phases of the oxygen carrier (M<sub>x</sub>O<sub>y</sub>) and the gases that are produced. The oxygen carrier plays a vital role in the production of syngas. The oxidization of the reduced oxygen carrier and the partial combustion of the biomass yield the heat required for gasification progressions. Moreover, the oxygen carrier possesses catalytic qualities that raise syngas quality and lower tar concentration. The main material in syngas generation is an oxygen carrier containing metal oxides, which is in charge of moving heat and oxygen from the air reactor to the fuel or gasification reactor, thereby avoiding the expense of pure oxygen or significant volumes of steam [35]. Higher CO<sub>2</sub> conversion and lower carbon formation are the results of the reaction between the surface oxygen species and the surface carbon species, which can adsorb CO<sub>2</sub> molecules to create bidentate carbonate species. Fuel reduction technologies based on metal oxides, such as thermal carbon reduction, metal oxide-based selective oxidation reactions, and chemical looping processes, have been demonstrated. Chemical looping reform is a method for producing syngas that partially oxidizes methane by utilizing lattice oxygen [35]. The syngas production mechanism using metal oxides is shown in Equation (1).



Gasification is a fundamental process for converting a feedstock into synthesis gas. The process of gasification is a thermochemical conversion that uses partial oxidation of the raw material to create a gaseous mixture that is primarily composed of hydrogen and carbon monoxide [36]. There are four stages to the gasification process, depending on the type of gasifier (drying, pyrolysis, oxidation, and reduction). In Figure 4b, a graphical diagram for different Fe/Ca ratios used to synthesize Fe<sub>2</sub>O<sub>3</sub>/CaO with H<sub>2</sub>-enriched syngas conversion [37].





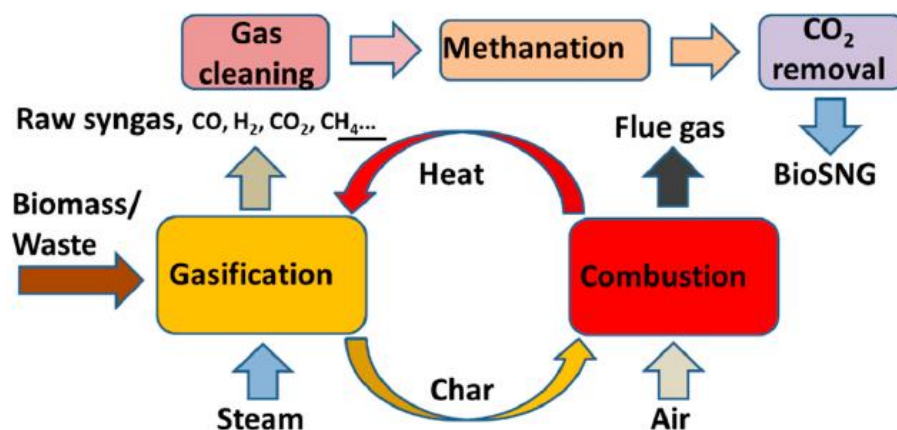
**Figure 4.** (a) The chemical looping gasification process. Reprinted from [35]. Copyright (2021), with permission from Elsevier. (b) Graphical diagram for different Fe/Ca ratios used to synthesize  $\text{Fe}_2\text{O}_3/\text{CaO}$  with  $\text{H}_2$ -enriched syngas. (c) Schematic diagram for different ratios of Fe/Ca used to synthesize  $\text{Fe}_2\text{O}_3/\text{CaO}$  with  $\text{H}_2$ -enriched syngas. Reprinted from [37]. Copyright (2020), with permission from Elsevier.

Figure 4c depicts the chemical looping gasification experimental technique, which consists of gas/water feeding, gasification reaction, condensation, syngas collection, and analysis. An electric furnace assembly with a stainless-steel tube reactor (inner diameter of 27 mm and height of 650 mm) was used as the gasification system in this experiment. Initially, the furnace was heated to a high temperature (600–900 °C). In the furnace, the stainless-steel reactor containing rice straw and OC was connected to a nitrogen flow (99.99%, 200 mL/min, and STP). A precise syringe pump was used to inject water into the reactor, and after the reactor was set up in the furnace, steam began to be produced and enter the reactor. At each run, 1 g of dried rice straw was mixed with 1 g of OC by mechanical stirring and reacted at the desired temperature for 30 min with a steam feeding rate of 0.1 g/min. The total steam was, therefore, affordable for the gasification of rice straw and the potential oxidation of reduced OCs, increasing the overall conversion efficiency. After the reaction, the solid residue was cooled down under nitrogen to room temperature and kept for further analysis. Based on this research, Quiang et al.'s study examined and compared the oxygen carrier durability, solid structure development, Fe/Ca ratio, temperature, and oxygen carrier cycling capacity to the pyrolysis and gasification processes. The trace extraction method resulted in the formation of two different kinds of calcium ferrites ( $\text{Ca}_2\text{Fe}_2\text{O}_5$  and  $\text{CaFe}_2\text{O}$ ) with various Fe/Ca ratios, with Fe and Ca being distributed equally throughout the oxygen carriers. When the Fe: Ca ratio was 1:1, the formed oxygen carrier ( $\text{Ca}_2\text{Fe}_2\text{O}_5$ ) gave the highest hydrogen yield (23.07 mmol/g biomass) at 800 °C, benefiting from the one-step reduction and oxidation properties of  $\text{Ca}_2\text{Fe}_2\text{O}_5$ . A temperature of at least 800 °C was required for the complete redox reduction of  $\text{Ca}_2\text{Fe}_2\text{O}_5$  during chemical vapor gasification. As a result, the high hydrogen selectivity of Fe: Ca = 1:1 ( $\text{Ca}_2\text{Fe}_2\text{O}_5$ ) makes it a suitable oxygen carrier candidate, but the cycling stability should be improved to make biomass chemical chain gasification conversion a better application for the production of syngas [37]. Similarly, recent research by Liu et al. examined the CLG of microalgae with calcium ferrite or modified calcium ferrite in terms of syngas production and characteristics of OCs. Their findings demonstrated that  $\text{Ca}_2\text{Fe}_2\text{O}_5$

was an appropriate material for microalgae because of its high selectivity for the production of synthesis gas [38].

Combustion is a chemical reaction between a fuel and an oxidant that makes an oxidized product. Generally, it is a reaction between hydrocarbons and oxygen to generate carbon dioxide, water, and heat. According to Zhang et al., the partial oxidation of fuel by chemical looping combustion can result in the formation of syngas [30].  $\text{CaFe}_2\text{O}_4$  and  $\text{Ca}_2\text{Fe}_2\text{O}_5$  were discovered to be the two carriers that produced partial oxidation of solid fuels, the best among the four. The investigation on charcoal, however, may indicate a limitation with the respective carriers when using raw biomass because of the presence of various minerals, depending on its source. Besides, numerous investigations have also demonstrated the successful production of syngas using chemical looping gasification technology [39]. Likewise, Luo et al. obtained pure  $\text{Fe}_2\text{O}_3/\text{MgAl}_2\text{O}_4$  and iron ore with a temperature limit of less than  $950^\circ\text{C}$  while using methane as a fuel [40].

Figure 5 illustrates the concept of indirect gasification technology with a combustion process [41]. In syngas production, a fuel mixture consisting mainly of hydrogen and carbon monoxide is burned, proving to be a promising fuel for combustion technology. According to Amin Paykani et al., the choice of base fuel, its physicochemical properties, and its physical conditions are all important factors that influence the synthesis of syngas produced by combustion systems [42]. M. Fiore et al. demonstrated that gasification is the only exothermic process and its heat release is necessary for water and carbon dioxide, as the products of several oxidation reactions are formed during this stage [43]. During cracking, carbonaceous particles become simpler molecules once they have been exposed to heat. To generate a gas compatible with an internal combustion engine, tars must first be broken down chemically. Otherwise, they could condense into sticky tars, which may cause damage to the valves. The reduction process, which assures the synthesis of hydrogen and carbon monoxide from water and carbon dioxide, is the last step. In order to achieve a high fraction of fuel gas at the exit, reduction is accomplished by passing the combustion products over a bed of extremely hot charcoal.



**Figure 5.** The concept of indirect gasification technology with the combustion process, reproduced from [41], with permission from MDPI Publisher.

Another process utilized for this purpose is pyrolysis, in which organic and plastic materials are thermally decomposed. During pyrolysis, materials undergo continuous physical and chemical changes. A wide range of applications is possible with pyrolysis technology. The chemical industry, for example, produces methanol, charcoal, and activated carbon by using this method. In addition to these, the pyrolysis process has several advantages over other energy recovery methods, such as the ability to use stone, ceramics, glass, or soil obtained during waste sorting. With this technology, a wide variety of feedstocks can be utilized. Consequently, it reduces landfill waste, landfill gas emissions, and the risk of water contamination. Moreover, building a pyrolysis plant is relatively simple [44]. Depending on the conditions associated with the process, pyrolysis can be classified into

three types: slow, fast, and flash pyrolysis. A variety of thermochemical and biological processes have been used to transform biomass into products with added value. Among those processes, pyrolysis is more convenient since it has several advantages in terms of storage, transportation, and flexibility in the solicitation. This includes engines, boilers, combustion appliances, turbines, etc. Generally, it can be divided into components that generate only heat and biochar (by using slow pyrolysis), and units that produce both biochar and bio-oils (using fast pyrolysis). Additionally, flash pyrolysis is a quick pyrolysis unit that transforms biomass into bio-oil [43,44]. Typical pyrolysis systems comprise a pyrolysis reactor, an extraction unit, and equipment for pre-processing lignocellulosic residues.

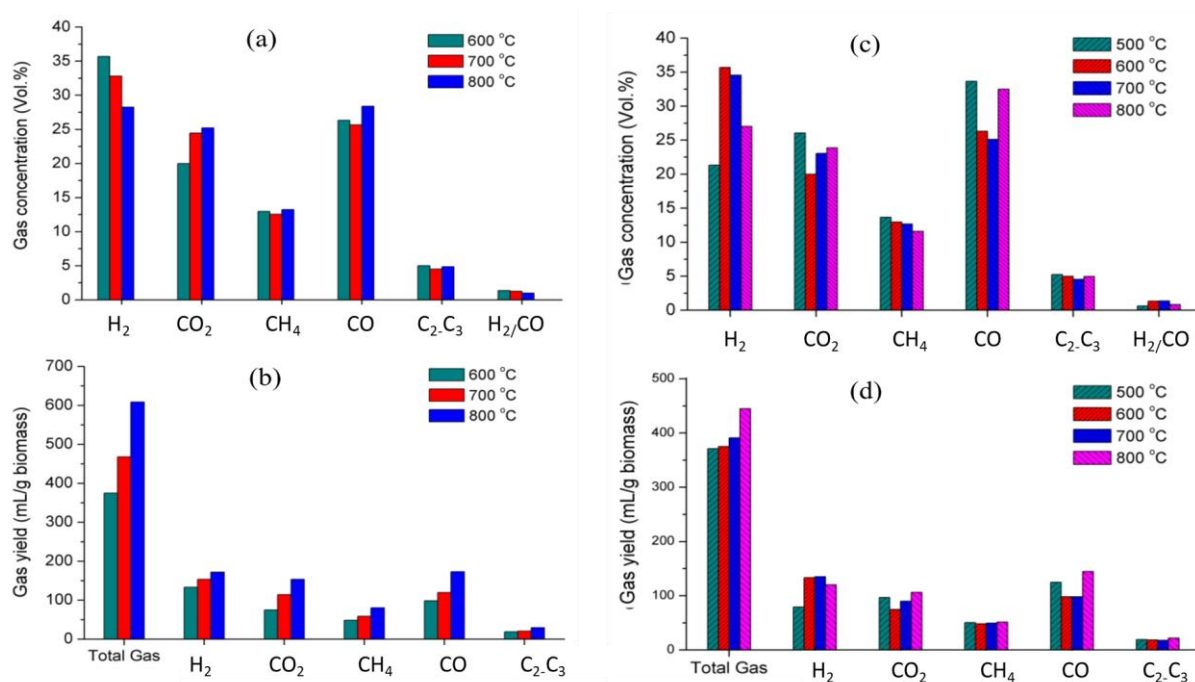
## 5. Tuning of Experimental Parameters

When developing nanocatalysts, which are employed in numerous chemical reactions to speed up the reaction and improve product efficiency, nanomaterials are frequently used because they have special catalytic capabilities. The effects of experimental factors, such as nanoparticle size, shape, distribution, and preparational methods, on their catalytic properties have been investigated by various researchers [45]. Basically, research has been conducted to comprehend the mechanism of action of nanocatalysts or the activity of catalysts, as well as the selectivity of nanocatalysts. Due to their distinctive features, nanoparticles have attracted attention as a material for advanced biofuel processes. Nevertheless, the use of nanoparticles in the production of bioethanol is still in its infancy. The morphology, physicochemical properties, and durability of nanoparticles are significantly impacted by a number of parameters throughout the synthesis process. Therefore, operational factors have a great impact on the synthesis process. The performance of nanoparticles is influenced by a variety of factors during the production of biofuel. The synthesis method, pressure, temperature, medium pH, nanoparticle size, and other variables are crucial [46].

### 5.1. Temperature

Since temperature affects the geometry of nanoparticles, comprising their size, shape, and endurance, temperature is a significant factor in the synthesis of biofuel. The metabolism and proliferation of cells are greatly influenced by temperature when using biological methods to produce syngas [47]. The solubility of CO, H<sub>2</sub>, and CO<sub>2</sub> in the fluid phase is influenced by temperature. For different microorganisms, different temperatures are ideal for syngas production. Physical and chemical techniques require temperatures higher than 300 °C, but biological methods utilize temperatures that are low to moderate (<100 °C), or even ambient. Besides this, based on the synthesis technique, the calcination temperatures for different metallic nanomaterials vary between 100 and 700 °C. The effects of temperature influence the geometry of nanoparticles, the rate of reaction during the catalytic reaction, the durability of nanoparticles, and the structure and size of nanoparticles. Reaction rate and temperature are tightly correlated, suggesting that reaction rate is slow at a relatively low temperature and speeds up as the temperature increases. Compared to nanoparticles produced at reduced temperatures, such as 25 °C, those produced at higher temperatures, such as 100 °C, are more stable and develop to their proper size. A higher temperature can speed up the production process [48]. Transesterification is a synthesis process that is used to prepare straight oils from renewable sources for biodiesel production [43,45]. When methanol or ethanol are present, transesterification processes begin at temperatures between 50 and 80 °C with sodium hydroxide (NaOH) functioning as a base catalyst. The impacts of catalyst calcination temperature and catalyst bed temperature on the constitution and productivity of syngas were studied by Shuangxia Yang et al. [49]. Their studies focused on the synthesis of hydrogen-enriched gas from biomass in a two-stage fixed-bed reaction system using a Fe/CaO catalyst formed from layered double hydroxides as the precursor. At a modest temperature range of 600 °C, the Fe/CaO catalysts displayed uniform morphological characteristics and crystalline size, and they had outstanding physicochemical characteristics, such as H<sub>2</sub> reducibility and CO<sub>2</sub> absorption capacity. This contributed to

their high catalytic performance in terms of the production of syngas, which resulted in a syngas yield of 44.6%, an H<sub>2</sub> composition of 35.7%, and an H<sub>2</sub>/CO ratio of 1.36 in the range. Although the H<sub>2</sub>/CO molar ratio decreased to 0.99 as a result of additional CO<sub>2</sub> released from the decomposition of CaCO<sub>3</sub> at higher catalytic temperatures, the syngas yield and H<sub>2</sub> yield increased up to 63.0 weight percent and 172 mL/g of biomass, respectively, as a result of the augmented supplementary cracking and realigning reactions of volatiles in the existence of the Fe/CaO-600 catalyst. The gaseous concentration and gaseous yield of the syngas conversion of biomass pyrolysis in the presence of the Fe/CaO catalysts calcined at various temperatures are shown in Figure 6.



**Figure 6.** Bar diagram of (a) gaseous concentration, (b) gaseous yield of the syngas conversion of biomass pyrolysis, effect of catalytic bed temperature on (c) concentration, and (d) yield of the syngas. Reprinted from [49]. Copyright (2017), with permission from Elsevier.

### 5.2. pH

Due to the significant role that pH variation plays in the formation of nucleation centers, pH values have an effect on the shape, size, synthesizing pace, and homogeneity of particle dispersion of nanomaterials. Small nanoparticles are evident at a pH of 6, but when the pH rises from 7.0 to 11.0, the average nanoparticle size decreases [50]. The size and form of nanoparticles are influenced by the pH of the medium: a medium with a basic pH offers a quick growth rate, faster productivity, and enhanced reduction rates, and it regulates the size, synthesizing rate, homogeneity of particle distribution, and morphology of nanomaterials. The typical size of nanoparticles drops when the pH rises from 7.0 to 11.0, while microscopic nanoparticles are evident at a pH of 6. This not only impacts the regularity of particle distribution and synthesizing speed, but it also influences the growth of nucleation sites in the morphology of the particles [50–52]. Z. Fakhroueian et al. studied the impact of the pH factor on the production of nanocatalysts, nanocomposites, and nanotubes using the hydrothermal, coprecipitation, and sputtering techniques of CuO<sub>x</sub> NiO<sub>x</sub> for syngas processes in the petroleum sector [53]. According to their research, the pH factor can alter the original texture, surface characteristics, and material properties. For instance, 25 percent of NiCo/CeAl nanocomposites at a pH of 9 can yield nanotubes and nanocomposites with the finest adaptive modulation, 99 % CH<sub>4</sub> conversion, and 91 % H<sub>2</sub> selectivity in the syngas reactions; however, at a pH of 7, it obtains a simple nano-spherical assembly, containing 98% of CH<sub>4</sub> conversion and 93.40 % of H<sub>2</sub>. The pH of the culture has

a considerable impact on aerobic metabolism, cell proliferation, and product distribution in biological processes. An effective approach to promoting the formation of syngas is a pH shift.

### 5.3. Catalyst Preparation Process

The coprecipitation method, microemulsion, thermal breakdown, hydrothermal synthesis, synthesis employing plant materials, synthesis incorporating biological organisms, and so forth are instances of nanoparticle synthesis procedures. Every method has a unique set of benefits and drawbacks [54]. Different synthesis methods have an impact on the efficiency of nanomaterials for the production of syngas. The most efficient processes for producing biodiesel are the ultrasonic reactor, batch reaction, lipase-catalyzed technique, and supercritical process. With these techniques, transesterification is used to synthetically create pure oils from renewable resources. Enzymatic hydrolysis, preprocessing, and fermentation are several steps required for the production of bioethanol. Various pretreatment techniques, including physical, chemical, physicochemical, and biological procedures, have been employed for the conversion of biomass. Different synthesis techniques play a crucial role in the performance of nanoparticles in the conversion of biomass [55]. The generation of biofuel and the effectiveness of particles are severely affected by their synthesis methods [56].

### 5.4. Pressure

In the formation of nanomaterials and biofuels, pressure is a significant factor. Typically, the reaction medium is subjected to the proper pressure in order to produce the desired geometry, size, and coalescence of nanoparticles. Particle sizes rise as a result of the high pressure. In order to regulate the levels of quick deployment and decrease, pressure can also be applied [55,57]. The effects of adding ferric chloride ( $\text{FeCl}_3$ ) to biodiesel on the performance and emission parameters of diesel engines were studied by Kannan et al. [57]. The rate of heat release and cylinder pressure were reported to have increased. While the thermal efficiency of the brakes increased by 6.3%, it was also determined that the specific fuel consumption decreased by 8.6%.

## 6. Utilization of Magnetic Nanomaterials

Magnetic nanomaterials of Fe, Ni, Co, and various combinations with other active nanomaterials and magnetic nanoparticles are found to be better candidates for use as the catalysts for syngas production/conversion process through various methods. This section discusses the progress made on magnetic nanomaterials containing Fe, Ni, and Co as the catalysts for syngas production/conversion process.

### 6.1. Fe-Based Magnetic Materials

For the synthesis of syngas, iron (Fe) is a promising active-phase material due to its lower cost than noble metal catalysts, abundance, low toxicity, and high reliability in tar breaking [58]. Due to the presence of mono-Fe and rhodium in the catalysts, conventional Rh-Fe catalysts often show greater alkane or methanol selectivity, and as a result, their specificity to higher alcohols is poor. Tong Han et al. synthesized an alternative catalyst.  $\text{YRh}_{0.5}\text{Fe}_{0.5}\text{O}_3$  with a perovskite structure was layered on  $\text{ZrO}_2$  as a solution to the conflict [59]. The homogenous and highly dispersed Rh-Fe alloys were responsible for the remarkable specificity and productivity of  $\text{YRh}_{0.5}\text{Fe}_{0.5}\text{O}_3/\text{ZrO}_2$ .  $\text{YRh}_{0.5}\text{Fe}_{0.5}\text{O}_3/\text{ZrO}_2$  demonstrated excellent stability as well. Thomas E. L. et al. examined the hydrogenation of  $\text{CO}_2$  into methanol using Ni-Fe-Ga alloys to generate  $\text{Ni}_2\text{FeGa}$ , and they observed that  $\text{Ni}_2\text{FeGa}$  performed the best out of all the evaluated catalysts in terms of methanol output. At low processing temperatures and pressures, the efficacy of the produced  $\text{Ni}_2\text{FeGa}$  yielded performance similar to commercial products, i.e.,  $\text{Cu}/\text{ZnO}/\text{Al}_2\text{O}_3/\text{MgO}$  [60].

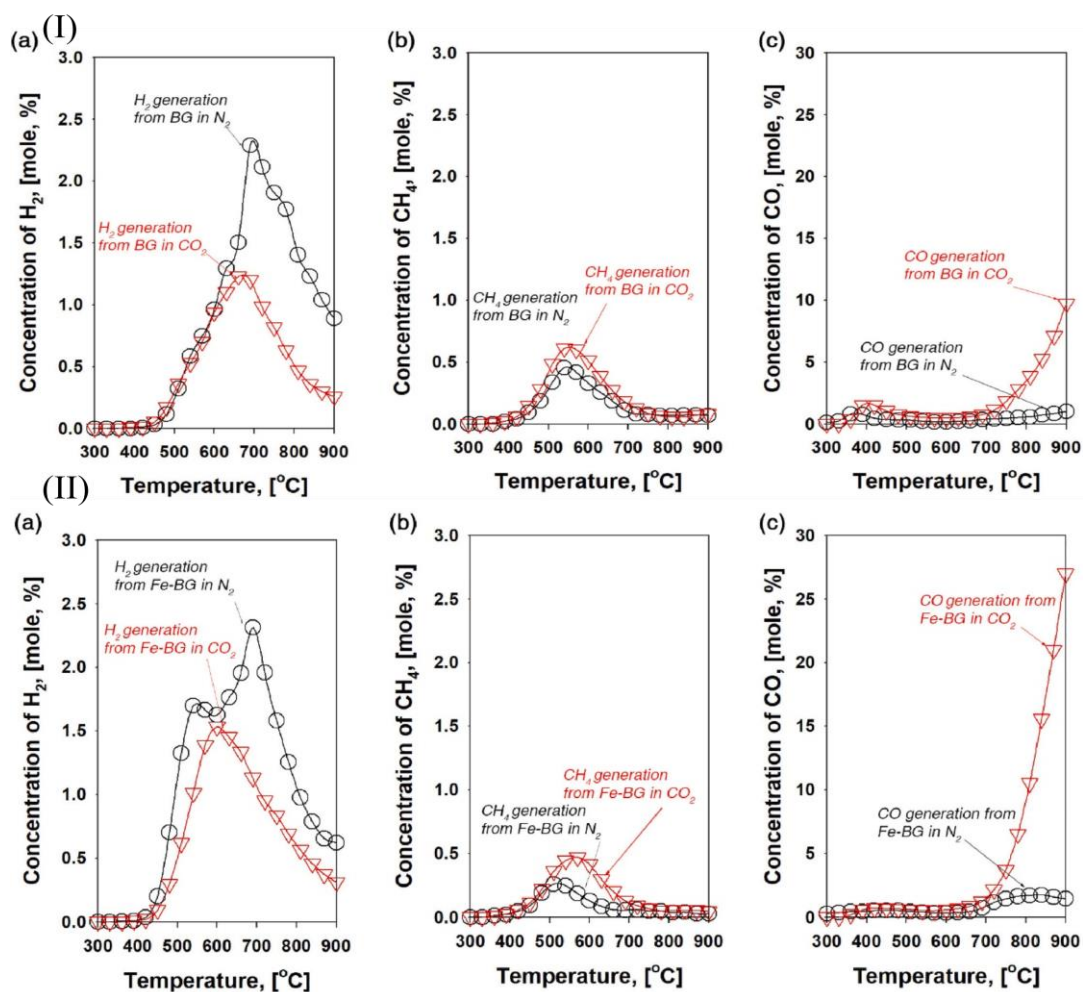
Mixing different transition-metal elements is an efficient technique to boost catalytic activity, together with nano-structuring/crystallization to raise the bulk activity. When

methane and solid oxides (oxygen carriers) combine, syngas is produced. The reduced oxygen carriers can then be replenished by a gaseous oxidant, such as water and air [61]. Chemical looping ignition is regarded as a very effective technique for capturing CO<sub>2</sub>. Since CO<sub>2</sub> segregation and capture are inherent to the process, it also offers a far lower energy penalty and cheaper cost than alternative CO<sub>2</sub> capture devices. Combustion occurs in the chemical looping process without the fuel and air coming into contact. Metal oxide (Me<sub>x</sub>O<sub>y</sub>), which is converted to Me<sub>x</sub>O<sub>y-1</sub>, delivers the ignition oxygen to the fuel reactor. Air is used to replenish the metal oxide inside a network of connected air reactors. The fuel is oxidized inside the fuel reactor to CO<sub>2</sub> and H<sub>2</sub>O [62]. Ral Pérez-Vega investigated the ignition of syngas using a Mn/Fe-based oxygen carrier and demonstrated complete fuel transformation to CO<sub>2</sub> and H<sub>2</sub>O at fuel unit temperatures exceeding 930 °C. Moreover, the CH<sub>4</sub> ignition reached the maximum burning rate of 78% at 966 °C. In addition, they reported that the fuel reactor was heated to a temperature higher than 1000 °C in order to complete CH<sub>4</sub> combustion [63].

Jiao Zhao et al. synthesized a Fe-N-C non-precious electrocatalyst, and a flow rate of 24 mL min<sup>-1</sup> of very pure CO<sub>2</sub> was delivered into the cathode chamber for 30 min prior to electrolysis [5]. At the same time, a magneton was used to agitate the electrolyte in the cathode chamber. Additionally, they stated that, compared to a resin made of carbonized melamine formaldehyde, the non-precious Fe-N-C electrocatalyst demonstrates well-pleasing movement of CO and H<sub>2</sub> generation (FE<sub>CO</sub> = 74%, FE<sub>H<sub>2</sub></sub> = 25%) at a lower overpotential of 0.6 V than others. Additionally, they reported that, compared to a resin made of carbonized melamine formaldehyde, the Fe-N-C non-precious electrocatalyst exhibits well-pleasing activity of CO and H<sub>2</sub> generation (FE<sub>CO</sub> = 74%, FE<sub>H<sub>2</sub></sub> = 25%) at a subordinate overpotential of -0.6 V, demonstrating the better selectivity of CO<sub>2</sub> reduction reactions [5]. Mesoporous titania and silica were synthesized by Claudio Cara and colleagues as support materials for the purification of H<sub>2</sub>S from syngas. Fascinatingly, it was found that both ultrasmall aspects were extremely active, sensitive to H<sub>2</sub>S, and regenerable. Under a syngas environment, the two composites' active phases differed noticeably, with the amorphous silica-based composite performing better when there were Fe infusions [64]. Aluminum magnesium spinel (MgAl<sub>2</sub>O<sub>4</sub>) was developed by G. V. Pankina et al., who employed Fe-K as the activator, and its particular surface areas were examined in relation to the physicochemical characteristics and dynamics of Fe-K [65]. They observed that syngas reduction occurs predominantly when the catalyst's magnetization is higher.

Gihoon Kwon et al. developed a Fe-impregnated bentonite, which was used as a catalyst in the CO<sub>2</sub>-assisted pyrolysis of grass cut to increase the production of syngas, quality of bio-oil, and sorptive properties of biochar. Similar to the pyrolysis of freshly grass cut, the production of hydrogen in the pyrolysis of the biochar under the N<sub>2</sub> condition begins at 500 °C (Figure 7(I)a). Yet, compared to the single pyrolysis of grass cut, it creates more H<sub>2</sub> with a maximum intensity at 700 °C, which is >2.5 times higher. Figure 7(I)b shows the concentration of CH<sub>4</sub> for the biochar. From their results, it is evident that the existence of bentonite accelerates the formation of H<sub>2</sub>, particularly between 630 and 700 °C. At the corresponding temperatures, bentonite is also found to have a similar impact on CO generation, as shown in Figure 7(I)c. Figure 7(I)d displays the outcomes of the gas investigations from the co-catalytic pyrolysis of the Fe-bentonite [66]. In the presence of N<sub>2</sub>, the pyrolysis of the Fe-bentonite produces more H<sub>2</sub> than the pyrolysis of the grass cut and biochar, with two peaks at 500 and 700 °C (Figure 7(II)a). The authors concluded that the Fe-impregnated bentonite is effective in pyrolyzing biomass to increase the generation of syngas and improves the standard of pyrogenic products.





**Figure 7.** (I) Concentrations of H<sub>2</sub> (a), CH<sub>4</sub> (b), and CO (c) formed during the pyrolysis of grass cut under the CO<sub>2</sub> and N<sub>2</sub> conditions. (II) Concentrations of H<sub>2</sub> (a), CH<sub>4</sub> (b), and CO (c) formed during the pyrolysis of Fe-bentonite under the N<sub>2</sub> and CO<sub>2</sub> conditions. Reprinted from [66]. Copyright (2022), with permission from Elsevier.

## 6.2. Ni-Based Materials

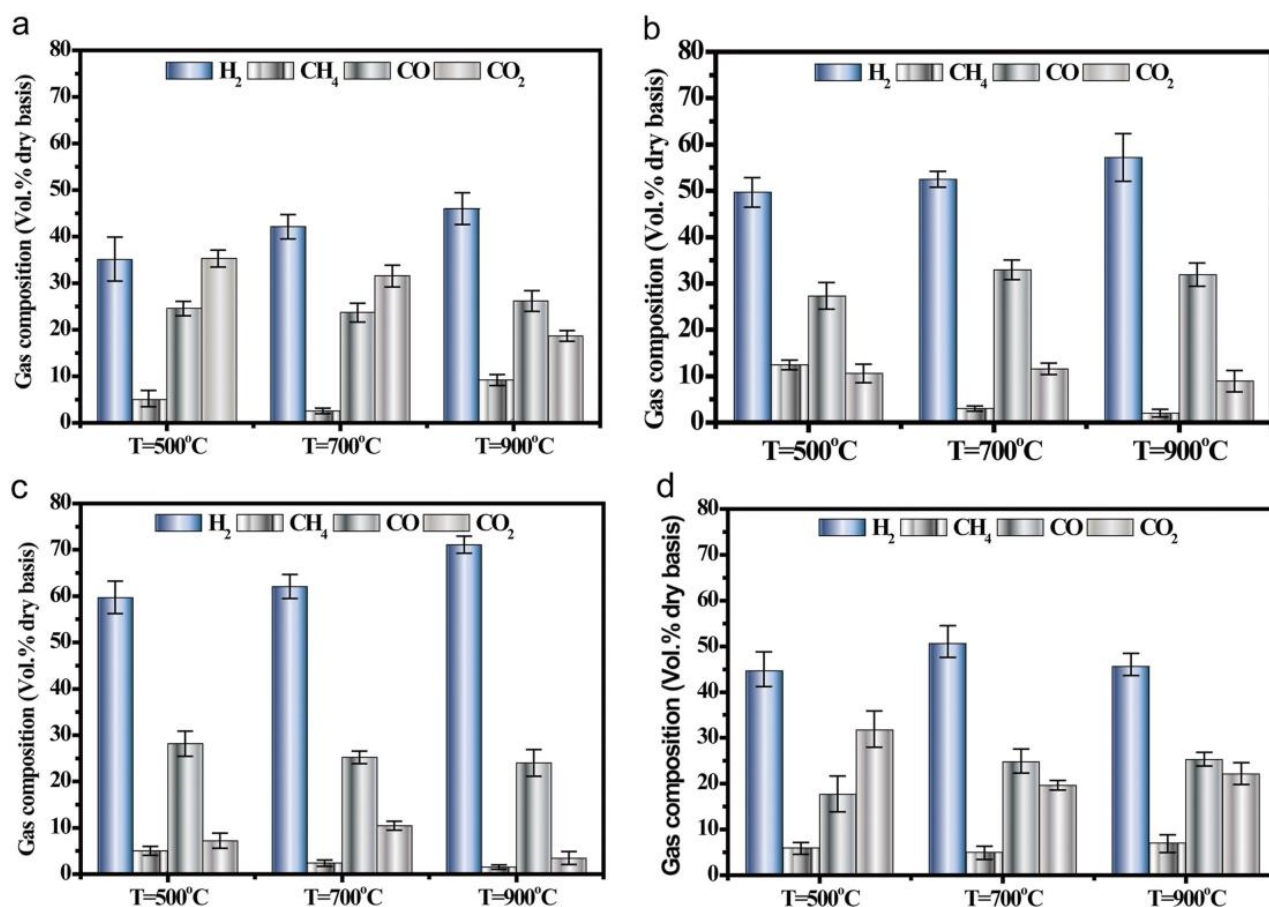
The research on nickel (Ni) has focused on enhancing reforming catalysts' durability to manufacture syngas on a large scale [67]. To improve partial oxidation, hydrogenation, dry reforming, and steam reforming, Ni-based catalysts are frequently utilized. They are favored for the reforming process due to their great stability and catalytic activity, as well as the fact that they are less expensive than noble metal catalysts [68]. On account of coke formation on catalysts and Ni sintering, Ni catalysts are known to be susceptible to deactivation. Numerous research studies have proposed that improving catalyst stability might require changing the support, adding functional metals, and using the right catalyst preparation techniques [69]. Mohammad Yusuf et al. synthesized Ni-based alloy catalysts sustained on mixed oxide (Al<sub>2</sub>O<sub>3</sub>/MgO) with the inclusion of tungsten. They noticed that a 4% by weight of tungsten loading resulted in the best performance and that the Ni-W bimetallic alloy catalyst still produced above 90% conversion of greenhouse gasses after 12 h [70]. By studying the catalytic pyrolysis of a herbal residue using a Ni-doped Fe/Ca catalyst, Jin Deng et al. demonstrated that the strong interaction between Fe and Ca produced Ca<sub>2</sub>Fe<sub>2</sub>O<sub>5</sub>, which prevented the formation of CaCO<sub>3</sub> and CO<sub>2</sub> and aided in the transition of tar and char. At 5% of the Fe-Ca catalyst, the H<sub>2</sub> output improved to 54.6 mL/g. Ni increased the dispersion of the catalyst and aided in the adsorption of alkaline ions while forming a stable Fe<sub>3</sub>Ni<sub>2</sub> alloy with Ca. The yields of H<sub>2</sub> and CO improved from



54.6 mL/g to 63.4 mL/g for 0.5% of Fe/Ca and from 70.0 mL/g to 95.5 mL/g for 0.5% of Ni-Fe/Ca, respectively [71].

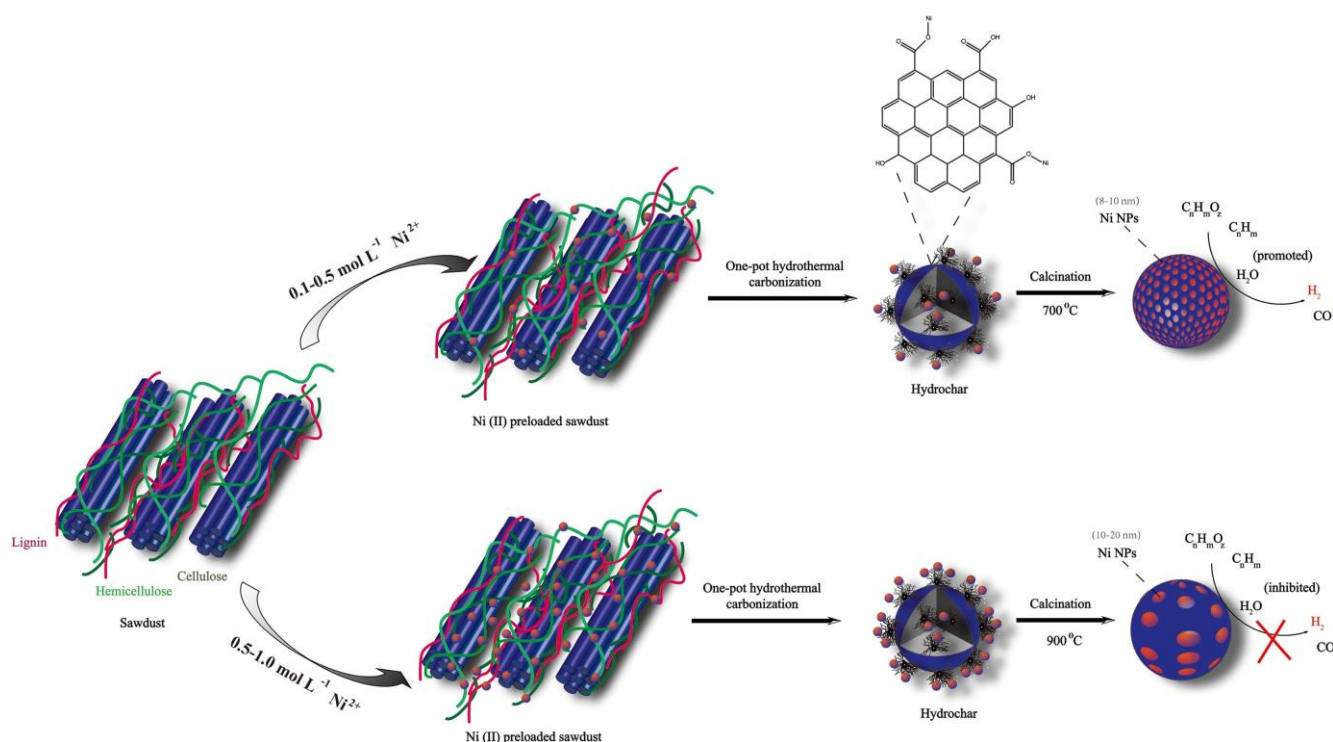
A multi-technique approach was used by L.B. Raberg et al. to investigate the potential relationship between support basicity, Ni/support activity, and stability of catalysts for the dry reforming of propane to synthesis gas. After being exposed to a magnetic field, ferrous metals retain a leftover magnetic moment at zero field; nonetheless, when the particle diameter falls below a particular size, the ferromagnetic particles transform into superparamagnetic particles [72]. The dry reformation of lignin with embedded Ni nanoparticles during microwave irradiation was prepared by M.V. Tsodikov et al., who adopted two distinct methods: impregnation and deposition [73]. In both instances, Ni particles with a size of 6 nm developed on the interface of the lignin. The dry reformation of lignin with microwave assistance was controlled by a variety of nanocatalysts. The first method's physical mixing of a carbon sorbent with a large dielectric loss factor and a specimen of lignin containing Ni was treated mechanically with a microwave, and the outcome was a 65-weight percent reformation of the lignin to synthesis gas with a H<sub>2</sub>/O ratio of 1/1. The products contained 80–90 weight percent of syngas. It was observed that the microwave treatment significantly boosted syngas yield during reforming compared to convection heating. It was found that various deposition techniques produced X-ray amorphous Ni particles with noticeably varied magnetic characteristics. Superparamagnetic NiO particles developed by metal vapor synthesis showed the highest ability for absorption using the microwave technique, which was adequate for the plasma to be derived as well as for the reforming temperature to be attained without the need for an additional sorbent; this was in contrast to the completely paramagnetic sample made from a nickel acetate solution [73]. It is quite well known that highly distributed metals with magnetic characteristics have a large absorbency in microwave assistance.

In a two-step gasification of sewage sludge at a treatment temperature of 500, 700, and 900 °C, Chao Gai et al. showed catalyst selectivity toward the primary gas components [74]. They observed that the experiments using the hydrochar without Ni nanoparticles showed lower discernment (35–46%) of total gas composition toward H<sub>2</sub> and CO<sub>2</sub> production of 19–35%. The Ni nanoparticles synthesized with the hydrochar catalysts, on the other hand, all displayed better catalytic activity and selectivity for H<sub>2</sub> production. From their report, it is demonstrated that Ni nanoparticles are useful for gasifying biomass to produce H<sub>2</sub>-enriched syngas. The authors postulate that the hydrochar-supported, evenly disseminated metallic Ni nanoparticles are responsible for the remarkable catalytic activity and selectivity toward H<sub>2</sub>. Figure 8 shows the two-stage gasification of the sewage sludge's catalyst selectivity toward the major gas components at a treatment temperature of 500, 700, and 900 °C.



**Figure 8.** The gas product selectivity from the catalytic gasification of sewage sludge using catalysts from (a) hydrochar and (b–d) nickel@hydrochar with different concentrations of nickel (0.1, 0.5, and 1.0) at different gasification temperatures from 500 to 900 °C. Reproduced from [74]. Copyright (2019), with permission from Elsevier.

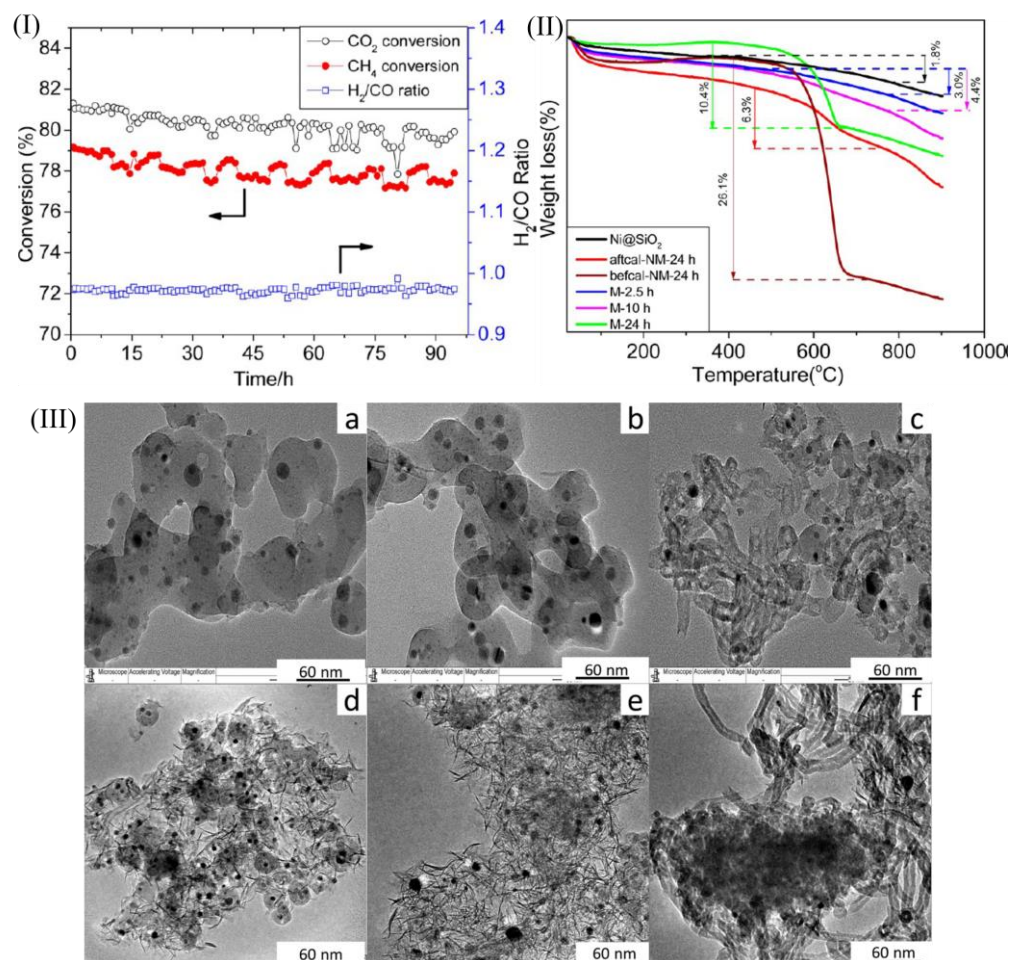
The core–shell LaMer model is largely acclaimed as being reliable, which is comprised of a hydrophobic core and a hydrophilic shell, and the model was applied by Chao Gai et al. for the synthesis of hydrochar-supported Ni nanoparticles. The interface of the hydrochar is hydrophilic with a dispersion of -OH and -C=O, such as carbonyl, hydroxyl/phenolic, and carboxylic functions. The carbonyl, hydroxyl/phenolic, and carboxylic functional groups on the surface of the hydrochar engage with Ni<sup>2+</sup> ions to absorb them when they are added to the hydrothermal liquid through ion exchange interactions [74]. Figure 9 displays a schematic illustration of the hydrochar-supported nickel nanoparticles.



**Figure 9.** Schematic illustrations of hydrochar-supported nickel nanoparticles synthesized from a lignin-rich precursor biomass. Reproduced from [74]. Copyright (2019), with permission from Elsevier.

Ziwei Li et al. fabricated Ni@Ni–Mg Phyllosilicate core/shell catalysts by treating hydrothermally Ni@SiO<sub>2</sub> with Mg(NO<sub>3</sub>)<sub>2</sub> [75]. The Ni@Ni–Mg Phyllosilicate core/shell catalyst treated for 10 h had the best catalytic performance out of all the Ni@Ni–Mg Phyllosilicate catalysts synthesized under different hydrothermal durations, with stable CO<sub>2</sub> and CH<sub>4</sub> conversions of around 81 and 78%, respectively. Its stability for the dry reforming of the methane reaction is shown in Figure 10(I). The most potent catalyst (treated for 10 h) was taken through testing for approximately 100 h, and it demonstrated conversions of CO<sub>2</sub> and CH<sub>4</sub> of 80 and 78%, respectively. The H<sub>2</sub>/CO ratio was approximately 0.96. This demonstrated the stability of the catalyst, treated for 10 h for the dry reforming of the methane process, at 700 °C. The TGA analysis for the used catalysts after a 20 h process is shown in Figure 10(II). For the 20 h testing period, there is negligible weight loss for Ni@SiO<sub>2</sub>. This may be due to the resistance influence of SiO<sub>2</sub> to Ni during sintering, which slows down the reaction of CH<sub>4</sub> breakdown. Due to the prevalence of CH<sub>4</sub> breakdown on sintered NiO, the catalyst used before calcination (befcal-NM-24 h) shows the most intense carbon deposition (26.1%). Despite being lower than that of the catalyst treated for 2.5 h (M-2.5 h) and 10 h (M-10 h), the weight loss for the after-calcination (aftcal-NM-24 h) catalyst is still higher at 6.3%. The M-2.5 h and M-10 h catalysts exhibit significantly less weight loss when compared to the befcal-NM-24 h catalysts, while having identical porosity and Ni exposures but higher basicity. Additionally, although having a weight loss of 10.4%, the catalyst treated for 24 h (M-24 h) loses 2.5 times less weight than the befcal-NM-24 h catalyst since it has a similar porosity and surface Ni exposures. These findings demonstrate the magnesium entity's potential for reducing the issue of carbon deposition, as illustrated in Figure 10(III). The authors performed a TEM analysis to examine the morphologies of the used catalysts. Following 20 h of reaction at 700 °C, cross-linking across silica shells emerges for both the Ni@SiO<sub>2</sub> and aftcal-NM-24 h catalysts, as can be seen in Figure 10(III)(a,b). This is mediated by the hydroxylation process between -(Si–O–Si)- assemblies on the silica shells, which results in the formation of three-dimensional systems when water is present. Due to the low H<sub>2</sub>/CO ratio, this water is formed through a reverse water–gas shift reaction.

From Figure 10(III)(c), a substantial amount of carbon nanotubes can be seen. This might be a result of NiO phase sintering. For the catalysts treated for 2.5 h (M-2.5 h) and 10 h (M-10 h), there is no cross-linking within the silica shells, as shown in Figure 10(III)(d,e). In the core of these two catalysts, Ni is well diffused, with the outer layer consisting of a needle-like Ni@Ni-Mg Phyllosilicate phase. Moreover, for the catalysts treated for 2.5 h (M-2.5 h), a tough outer silica shell is still discernible, whilst for the catalysts treated for 10 h (M-10 h), the majority of the porous Ni@Ni-Mg Phyllosilicate species replace the silica shell of Ni@SiO<sub>2</sub>. This makes it possible for the core portion to have great accessibility to active Ni while still limiting their sintering, which leads to strong CO<sub>2</sub> and CH<sub>4</sub> conversions and minimal carbon deposition. On the other hand, a significant number of carbon nanotubes and effective sintering of Ni /NiMg solution occur, as shown in Figure 10(III)(f), which lead to a lower catalytic activity and lower stability.



**Figure 10.** (I) Stability of the catalyst treated for 10 h and calcined at 700 °C. (II) Thermogravimetric analysis (TGA) for the utilized catalysts with various structures. (III) TEM images of the utilized catalysts after 20 h of reaction (a) Ni@SiO<sub>2</sub>, (b) aifcal-NM-24 h, (c) beifcal-NM-24 h, (d) M-2.5 h, (e) M-10 h, and (f) M-24 h. Reprinted with permission from [75]. Copyright (2014), with permission from the American Chemical Society.

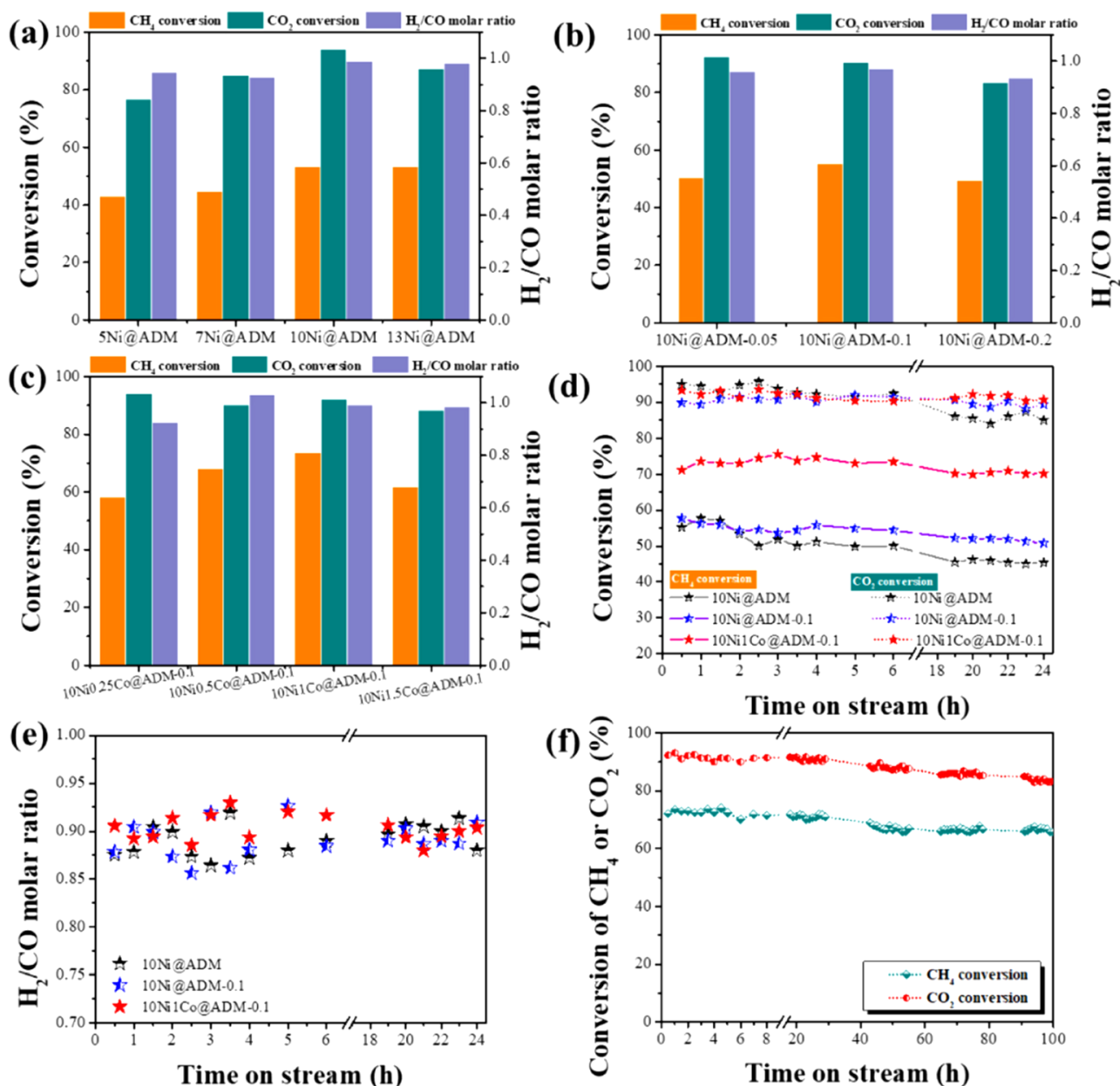
### 6.3. Co-Based MATERIALS

According to a report, Co-based alloys are efficient and have a high hydrocarbon production rate, making them a suitable material for use in syngas conversion [76]. Considerable efforts have been made to develop a range of different metal alloy materials to reduce the total cost and promote the catalytic efficiency of catalysts. Co-Cu bimetallic catalysts are regarded as the most viable catalysts due to their high affinity to higher alcohol and cheap cost. Cu-decorated Co-based catalysts and Co-decorated Cu-based catalysts are the two

forms of Co-Cu bimetallic catalysts. Through theoretical and practical research, Prieto et al. demonstrated that a Co-Cu alloy phase having Co-rich ratios is the best catalyst interface for long-chain alcohols [77]. Using a steady-state isotopic transient kinetic analysis, the results suggest that the addition of Cu into Co significantly promotes the formation of more  $C^{2+}$  oxygenates by blocking a significant fraction of Co sites for hydrocarbon synthesis [78]. Using radio-frequency magnetic fields, Hoang M. Nguyen et al. created binary (Co-Cu)- and ternary (Co-Cu-Ni)-based alloys. All prepared catalysts were stimulated under radio-frequency ignition to transform  $CO_2$  and co-reactants, such as  $H_2O$  and methane, into syngas ( $H_2$  and  $CO$ ) at a low temperature of  $400\text{ }^\circ\text{C}$  [79]. They also concluded that, in all the performance conditions, the Cu-Co sample had the best catalytic stability and performance. According to their research observations, the catalyst system's inclusion of a magnetic constituent and an electrically conductive element enables very efficient heating to occur through both hysteresis loss and Joule effect. The Cu-Co catalyst maintained its remarkable stability for about 50 h throughout the streaming test due to Joule heating. The results offer important insights into the potential of catalysts for RF-assisted chemical processes that do not require a lot of excessive input current or the usage of powerful magnetic metals to attain the optimal chemical configurations. According to Lin Chen et al., who used Co with Ni as an aerogel catalyst, the  $CH_4$  conversion in a magnetic-assisted fluidized bed reactor increased by 12 and 7%, respectively, in comparison to a fixed bed reactor and a conventional fluidized bed reactor [80]. This was due to the catalyst's better fluidization reliability. Additionally, over the course of the 50 h reaction, the catalytic performance remained quite steady. The enhanced gas–solid association in the magnetic-assisted fluidized bed reactor and the Co-Ni aerogel catalyst's better catalytic property can both serve as examples of this higher stability.

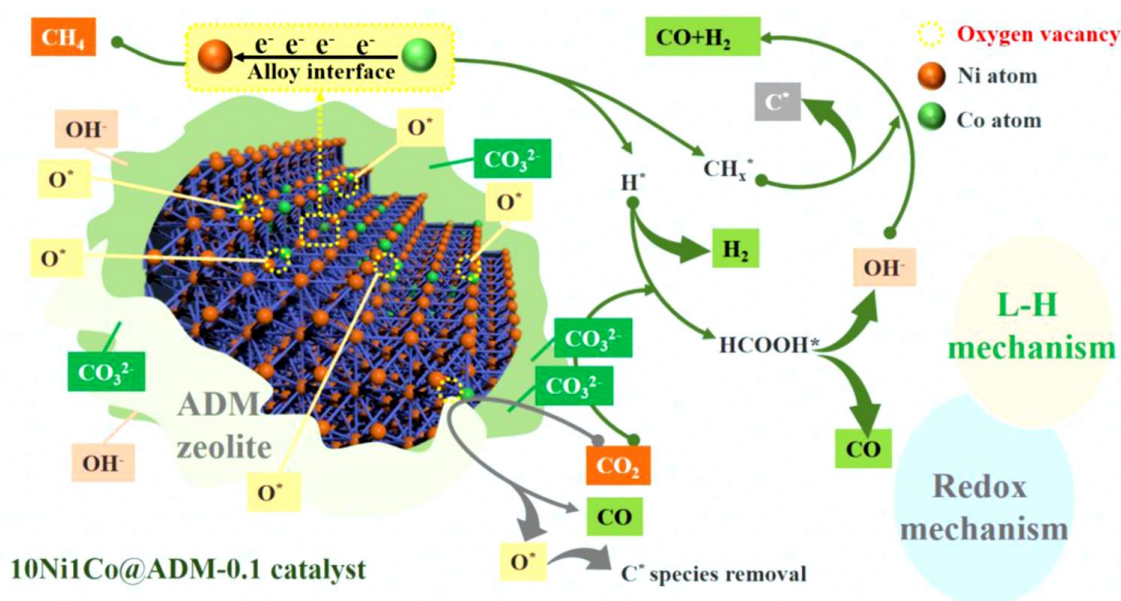
Attapulgite-derived MFI (ADM) zeolite-encased Ni-Co alloys were developed by Defang Liang et al. utilizing a one-pot technique [81]. The 24 h of dry reforming of methane effectiveness of the 10Ni@ADM, 10Ni@ADM-0.1, and 10Ni1Co@ADM-0.1 catalysts were investigated at  $700\text{ }^\circ\text{C}$  at 20/20/60 mL/min of  $CH_4/CO_2/N_2$ , and the results are displayed in Figure 11a. This investigation was performed to study the influence of the structures of ADM-encased Ni-Co alloys on catalytic stability and activity. The 10Ni1Co@ADM-0.1 catalyst has the highest dry reforming of methane activity, as shown in Figure 11a–c. The stability test results are shown in Figure 11d,e. The primary conversion of  $CH_4$  and  $CO_2$  by the 10Ni@ADM catalyst was 52 and 95%, respectively, with an  $H_2/CO$  molar ratio of 0.88. Furthermore, the 10Ni@ADM catalyst underwent a modest deactivation after 24 h of reaction, as the rates of  $CH_4$ ,  $CO_2$  conversions, and  $H_2/CO$  molar ratio declined to 45%, 85%, and 0.88, respectively. This might be a result of the catalyst being exposed to high temperatures for a long time, which caused the encased metal grains to migrate to the interface of the zeolite, causing partial metallic Ni sintering and active area loss. It was found that the initial activity of the 10Ni@ADM-0.1 catalyst and the 10Ni@ADM catalyst was related. However, once the reaction was over, the  $CH_4$  and  $CO_2$  conversions only dropped to 51% and 89%, respectively, showing that the inclusion of NaOH helped increase the catalyst's reliability. In terms of catalysts, the 10Ni1Co@ADM-0.1 catalyst showed the best catalytic performance, achieving the highest initial  $CH_4$  and  $CO_2$  conversions of 71 and 93%, respectively, and maintaining those conversions throughout the dry reforming of methane reaction. Two mechanisms, including the presence of Co as new active sites that promote  $CH_4$  activation/adsorption and the alloy interaction between Ni and Co that promotes  $CH_4$  breakdown, may be responsible for the higher initial  $CH_4$  conversion when compared to the 10Ni@ADM catalyst. In contrast to the 10Ni1Co/ADM-0.1 catalyst, as shown in Figure 11f, the 10Ni1Co@ADM-0.1 catalyst experiences little degradation over 100 h of the dry reforming of methane reaction, further demonstrating the structural resilience of the ADM zeolite-encased Ni-Co alloys.





**Figure 11.** Dry reforming of methane reactions for 4 h over the (a)  $x\text{Ni@ADM}$  ( $x = 5\text{--}13$ ), (b)  $10\text{Ni@ADM-}y$  ( $y = 0.05\text{--}0.2$ ), and (c)  $10\text{Ni}_z\text{Co@ADM-}0.1$  ( $z = 0.05\text{--}1.5$ ) catalysts. (d) Conversions of CH<sub>4</sub> and CO<sub>2</sub> and (e) H<sub>2</sub>/CO molar ratio on the attapulgite-derived MFI (ADM) zeolite-encased Ni-Co alloys. (f) Dry reforming of methane reactions for the 100 h test over the  $10\text{Ni}_1\text{Co@ADM-}0.1$  catalyst. Reproduced from [81]. Copyright (2023), with permission from Elsevier.

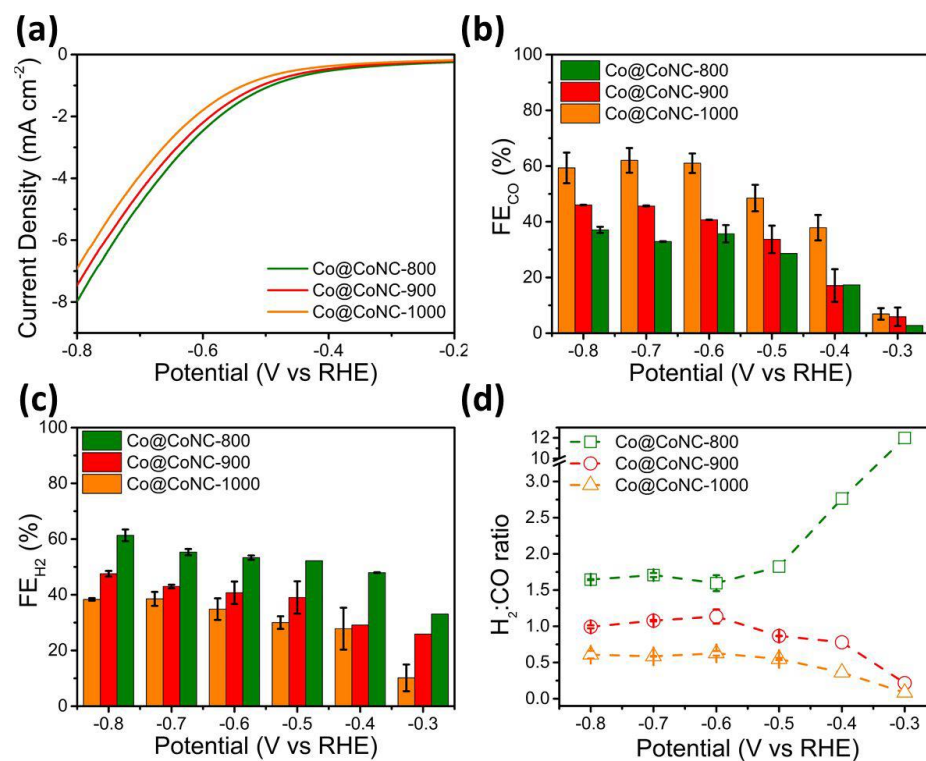
Furthermore, the mechanism for dry reforming over the  $10\text{Ni}_1\text{Co@ADM-}0.1$  catalyst was proposed by Defang Liang et al. [81]. By doping into the metallic Ni lattice of the  $10\text{Ni}_1\text{Co@ADM-}0.1$  catalyst, the inclusion of Co improved the diffusion of metallic grains and aided in the emergence of Ni-Co alloys. Additionally, the generated Ni-Co alloy interfaces promoted the transfer of electrons from Co to Ni, which aided in the production of electron-rich Ni. This led to the breakdown of C-H bonds in CH<sub>4</sub> molecules, which generated the reactive intermediaries CH<sub>x</sub><sup>\*</sup>/C<sup>\*</sup> and H<sup>\*</sup> (Figure 12).



**Figure 12.** Synergetic effect between the attapulgite-derived MFI encapsulation layers and the Ni-Co alloys for the dry reforming of methane reaction on the 10Ni1Co@ADM – 0.1 catalyst. Reproduced from [81]. Copyright (2023), with permission from Elsevier.

Rahman Daiyan et al. show that the Co@CoNC-900 electrocatalyst, which is coated with a single Co atom and enclosed in a graphitic carbon shell, can reliably produce syngas at moderate overpotentials during CO<sub>2</sub> reduction processes [82]. They examined the catalyst's linear sweep voltammetry curves and the CO<sub>2</sub> reduction process. Figure 13a,b show that as the annealing temperature is raised, and *j* marginally decreases, which may be connected to the catalyst's depleting Co-N<sub>4</sub> centers. Additionally, these findings suggest that the reaction route is not affected by the catalysts' growing surface areas (as the surface area rises when increasing the calcination temperatures). The findings of the bulk CO<sub>2</sub> electrolysis support their design strategy since an increase in the annealing temperature, i.e., from 800 °C to 1000 °C, improves FE<sub>CO</sub> (Figure 13b), while suppressing FE<sub>H<sub>2</sub></sub> (Figure 13c). The FE<sub>CO</sub> obtained with the Co@CoNC-800, Co@CoNC-900, and Co@CoNC-1000 catalysts is 36, 45, and 61%, respectively, whereas the FE<sub>H<sub>2</sub></sub> obtained with these catalysts at the same potential is 59, 43, and 40%, respectively. The combination of a decline in Co-N<sub>4</sub> moieties and the potential impact of rising defects on the CO<sub>2</sub> reaction selectivity can be used to directly correlate this enhanced selectivity with the CO<sub>2</sub> reduction reaction. The syngas ratio provides a vivid demonstration of the adjustment of reaction selectivity (Figure 13d). The authors reported H<sub>2</sub>:CO ratios of 1.5, 1, and 0.5 for the Co@CoNC-800, Co@CoNC-900, and Co@CoNC-1000 catalysts, respectively, by adjusting the annealing temperature.





**Figure 13.** Modification of syngas ratio using active site manipulation. (a) Linear sweep voltammetry, (b) FE<sub>CO</sub>, (c) FE<sub>H<sub>2</sub></sub>, and (d) H<sub>2</sub>/CO ratio with applied potential for the prepared catalysts. Reproduced from [82]. Copyright (2020), with permission from the American Chemical Society.

Some of the recent progresses on syngas production/conversion by utilizing magnetic nanomaterials are compared and shown in Table 1.

**Table 1.** Various magnetic materials and their utilization for syngas production/conversion.

Magnetic Catalysts	Preparation Process	Process	Performance	Reference
MgO/MgFe <sub>2</sub> O <sub>4</sub>	Combustion process	Biodiesel production reaction from vegetable oil	Lowest conversion is 82.4%, and maximum conversion is 91.2%.	[83]
Ni-Fe	Power-to-gas (hydrogenation method)	CO <sub>2</sub> methanation	Conversion of 80% of CO <sub>2</sub> to methane at 150 °C. CH <sub>4</sub> selectivity of CO <sub>2</sub> methanation is 95%.	[84]
(Fe, Cu, and K) and rice husk char	Pyrolysis method	Catalytic tar conversion for improving the yield of syngas	The tar conversion efficiency is obtained at 77.1% for RHC, 82.7% for K-RHC, and for 92.6% Fe-RHC at the reforming temperature of 800 °C.	[85]
FeSO <sub>4</sub>	Steam gasification and pyrolysis process	H <sub>2</sub> -rich syngas production	The maximum overall H <sub>2</sub> yield and exergy efficiency for producing H <sub>2</sub> are estimated to be 43.63%.	[86]
Ni/A-A-CFA	Biogas dry reforming method	Syngas production	It exhibits the best catalytic activity at CH <sub>4</sub> and CO <sub>2</sub> conversion rate > 95%.	[87]
Fe <sub>2</sub> O <sub>3</sub> /Al <sub>2</sub> O <sub>3</sub>	Chemical looping dry reforming process	For CO <sub>2</sub> production of hydrogen and syngas	Dry reforming stage for CH <sub>4</sub> conversion is 3.84, and syngas yield is 98.32%.	[88]

Table 1. Cont.

Magnetic Catalysts	Preparation Process	Process	Performance	Reference
TiO <sub>2</sub> /Fe	Fermentation process	For biohydrogen production	Yield increases by 24.9%.	[89]
Fe <sub>3</sub> O <sub>4</sub> and Fe <sub>5</sub> O <sub>12</sub>	Hydrolysis	Biomass production	A 90% harvesting efficiency is obtained.	[90]
Fe <sub>3</sub> O <sub>4</sub> /CuO	Coprecipitation method	Decolorization of water	A high dye removal efficiency of 94 % is achieved with 20 wt% Fe <sub>3</sub> O <sub>4</sub> /CuO composition at ambient conditions and a reaction time of 90 min.	[91]
Ni, Ni-Co, Ni-Fe, and Ni-Cu	Hydrothermal synthesis	Syngas production and carbon bio nanofilament	The highest sustainability factor (0.66) and carbon yield (424%) are obtained.	[17]
Ni/Al	Coprecipitation method	Production of hydrogen-rich syngas from biomass pyrolysis	Ni/Al-700 catalyst can increase gas yield by 30–80%.	[92]
Fe <sub>2</sub> O <sub>3</sub> and MgFe <sub>2</sub> O	Pyrolysis	Syngas production from biomass	Tar conversion efficiency reaches 94.1% with a high gas yield of 493.5 mL/g.	[93]
Fe/Ca <sub>x</sub> O	Simple precipitation method	Pyrolysis - gasification used for syngas production and tar removal	At an optimized composition of Ca/Fe 2/1, gasification yield efficiency (76.4%) is obtained.	[94]
Porous Ni, Ni-Co, Ni-Fe, and Ni-Cu	Precipitation method	Biomass decomposition to produce syngas	A high carbon yield efficiency of 36.43% is obtained.	[17]
Ni/Al	Ultrasonic-assisted incipient wetness impregnation method	Catalytic conversion of tar to syngas	With the addition of a catalyst, H <sub>2</sub> increases to 146%.	[95]
Ni-Cu/Al <sub>2</sub> O <sub>3</sub>	Impregnation method	Syngas production by methanol steam reforming	An increase in Ni content results in an increase in CO and a decrease in CO <sub>2</sub> yields.	[96]
Sc@ Ni/Fe	Pyrolysis method	Impregnation of biomass	At 600 °C, the conversion efficiency reaches 90.07%.	[97]
Fe-Ni/CNF	Pyrolysis method	Syngas production from pyrolysis gasification of biomass and plastic waste	Conversion efficiency of 87.90%.	[98]
Ni/Ru	Steam reforming process	Ru catalyst favors H <sub>2</sub> and CO production	90%	[99]

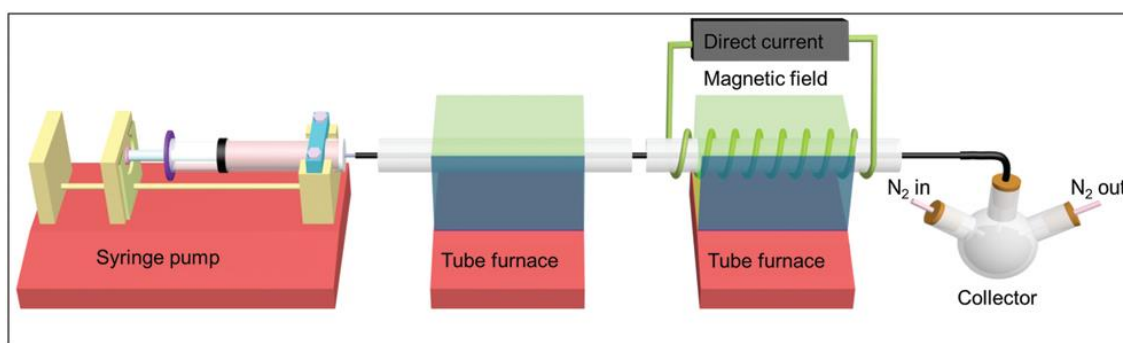
## 7. Effect of External Magnetic Field

We have discussed Fe-, Ni-, and Co-based magnetic materials for their utilization in syngas production/conversion in the previous section. This section discusses the effects of external magnetic field on magnetic nanomaterials during synthesis and applications. The effects of an external magnetic field could alter the charge transfer process during applications [100,101]. By transmitting loads of energy to the atomic and molecular dimensions of the materials, an external magnetic field can influence the microstructure and material characteristics. The production of static magnetic energy by a magnetic field affects the free energy of substances during synthesis and has an impact on their nucleation selectivity and rate, which is linked to metastable elements and innovative materials. Modern electrocatalysts can now be generated using magnetic fields, which are associated with nucleation and growth, as well as phase modulation. By enhancing the mass transfer on the working electrode, the magnetic effects of an external magnetic field, such as the magnetothermal effect, magnetohydrodynamic and micro-magnetohydrodynamic effects, Maxwell stress, and Kelvin force with spin selection effect, could indeed alter the reaction trends. This is advantageous for increasing the electrocatalytic performance of electrocatalysts with the potential utilization of external magnetic fields [102]. Various synthesis processes and

applications have proven that an external magnetic field could improve the efficiency of materials, depending on their magnetic characteristics [103,104].

An external magnetic field-coupling microfluidic synthesis process consisting of a reaction liquid preheater, a reaction-nucleation stage heating and temperature controller, a thermostat, a low-temperature abrupt termination collector, and a MF controller could be utilized for the synthesis process [105]. According to Junmei Wang et al., the synthesis of a  $\text{Fe}_2\text{Pt/C}$  catalyst under an external magnetic field has higher catalytic performance. A concurrently applied 1.4 T external magnetic field coupled with the microfluidic process results in  $\text{Fe}_2\text{Pt/C}$  nanocrystals of larger size. This method gives better catalytic performance on both ethanol and methanol oxidation reactions compared to the samples synthesized without a magnetic field [106]. Similarly, He et al. demonstrated that distinct ferric sulfide minerals, such as greigite and marcasite, have different magnetic properties, including coercive force, remnant, saturation, and magnetization. By using an in situ MF-assisted hydrothermal process to synthesize the ferric sulfide minerals, they were able to achieve this [107].

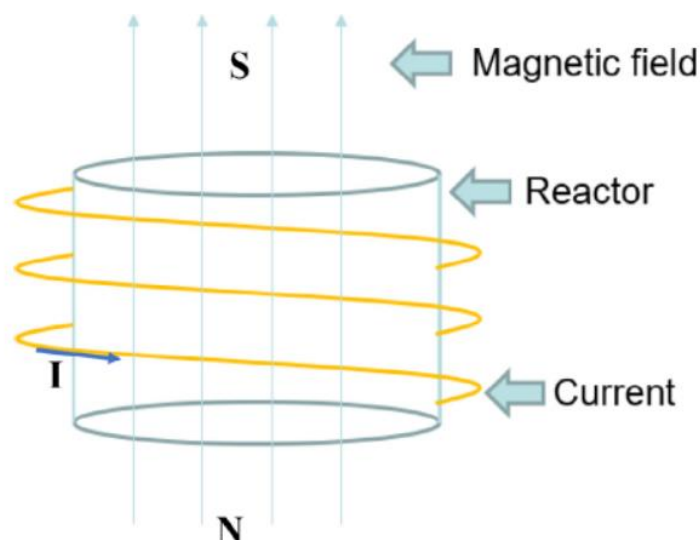
Figure 14 shows the four steps in the magnetic field-coupling microfluidic preparation process, including the preparation of the precursor, the preheating of the precursor, the nucleation of QDs, and the collection of QDs. The magnetic field along the channel was created using the solenoid electromagnet. The products were collected under  $\text{N}_2$  gas. Xiaoxiong Zhao et al. concluded that the magnetic fields had a significant impact on the nanoparticles' magnetic and optical properties. Regulation of the magnetic field was conveniently realized during the synthesis process. Co-doped ZnSe QD aggregates with a good size distribution were produced using a simplified microfluidic technique and a customizable magnetic field. These aggregates were created by numerous tiny nanoparticles (with diameters of about 4–6 nm) fusing together. Eventually, the authors insisted that by controlling the applied magnetic fields, particle sizes, and Co doping amounts, the Mr, Ms, Hc, net magnetization, and ferromagnetism of the QDs were adjusted. To alter the distinct magnetic characteristics of the QDs, one might alter the ratio of ferromagnetic to antiferromagnetic phases. It was realized that adding Co and altering the doping amount modified the band gaps of the QDs when estimating the band gap through using the UV-vis absorbance and R%.



**Figure 14.** The four steps in the magnetic field-coupling microfluidic preparation process. Used with permission from [105]; permission conveyed through Copyright Clearance Center, Inc.

Po-Wei Lan et al. investigated various Ni/Fe catalyst ratios for increased carbon dioxide methanation by employing chemical reduction with an external magnetic field, and they showed that the  $\text{Ni}_8\text{Fe}_2$  catalyst could convert more than 80% of  $\text{CO}_2$  to methane at  $150^\circ\text{C}$ . Furthermore, 95% of  $\text{CO}_2$  methanation's selectivity was for  $\text{CH}_4$  [84]. Figure 15 shows the experimental process of the magnetic field while synthesizing nanomaterials. Chemical reduction was cast off to develop a sequence of Ni/Fe catalysts with varying Fe/Ni ratios ( $\text{Ni}_9\text{Fe}_1$ ,  $\text{Ni}_8\text{Fe}_2$ , and  $\text{Ni}_7\text{Fe}_3$ ). The resulting solution was then transferred to a magnetic field reactor and heated to  $80^\circ\text{C}$  while being subjected to a 500 G magnetic field. A neodymium magnet performed well enough to harvest the generated particles,

which were subsequently purified by being washed with deionized water numerous times. Before being used, the produced Ni/Fe catalysts with various Ni/Fe ratios were dried in a desiccator.



**Figure 15.** The magnetic field reactor for Ni-Fe catalyst preparation. Reprinted from [84], Copyright (2021), with permission from Elsevier.

Due to the simultaneous endothermic  $\text{CO}_2$  reformation and exothermic partial oxidation of methane to syngas in the occurrence of oxygen, the methane-to-syngas transition process takes place in an energy-efficient manner, demanding little or no external source of energy. When Fe is injected into zeolite substances, Fe-containing acidic sites, iron oxides, and numerous paramagnetic O ions are all generated. The improved efficiency in a magnetic field is closely related to the magnetically triggered Fe ions and surface paramagnetic oxygen [108]. Methyl-functionalized silica and methyl-functionalized cobalt ferrite–silica nanoparticles were evaluated for their capacity to increase the generation of bioethanol in syngas fermentation via *Clostridium ljungdahlii* [109]. The  $\text{CoFe}_2\text{O}_4/\text{SiO}_2/\text{CH}_3$  nanoparticles demonstrated higher enhancement of syngas mass transfer when these nanoparticles were utilized to promote the syngas–water mass transfer. It was verified that the nanoparticles' ability to increase mass transfer was preserved after being recovered using a magnet and employed five more times. When utilizing both varieties of nanoparticles, the syngas fermentation process produced more biomass, ethanol, and acetic acid. Due to the increased syngas mass transfer, the  $\text{CoFe}_2\text{O}_4/\text{SiO}_2/\text{CH}_3$  nanoparticles were more successful for syngas fermentation. The inclusion of  $\text{CoFe}_2\text{O}_4/\text{SiO}_2/\text{CH}_3$  nanoparticles boosted the generation of biomass, ethanol, and acetic acid by around 228%, 214%, and 60%, respectively, compared to a control. By using recovered nanoparticles for fermentation, the nanoparticles' reusability was demonstrated, and the results clearly show the advantages of utilizing magnetic nanomaterials in syngas production.

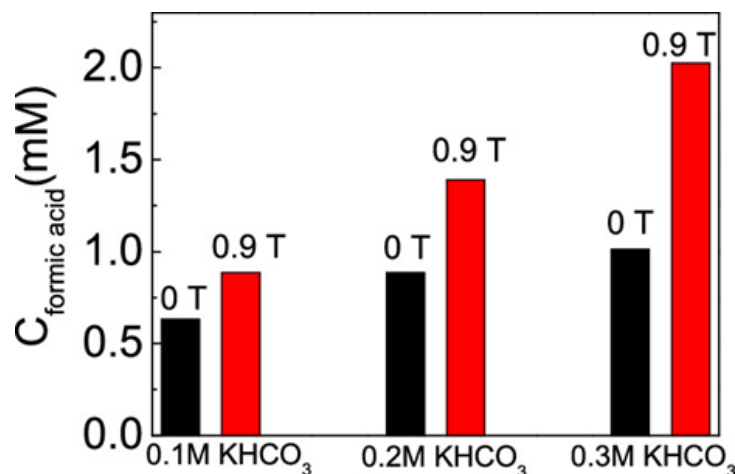
Using an external MF-coupling microfluidic method, homogeneous ultrasmall-sized  $\text{Fe}_2\text{Pt}/\text{C}$  nanocatalysts are synthesized [106]. The reactants could be controlled by the magnetizing force linked to the magnetic field gradient and the Lorentz force when an external magnetic field is applied. In turn, their catalytic performances in the electrochemical oxidation of methanol and ethanol can be considerably enhanced by controlling the size, composition, electronic status, and magnetic characteristics of the catalysts. This investigation can help us better understand how an external magnetic field influences nanocatalyst synthesis and offer us a good concept for enhancing the catalytic efficiency of electrochemical nanocatalysts. An attempt was made to determine whether it is possible to increase the catalytic performance of a Fe-based catalyst for the removal of  $\text{AsH}_3$  by using a low-energy external magnetic field [110]. With a 0.1 T magnetic field present and

a temperature of 120 °C, the catalytic performance for AsH<sub>3</sub> degradation was improved by 52%. Fe-containing acidic sites, iron oxides, and many paramagnetic O ions were all introduced when Fe was incorporated into zeolite materials. The magnetically activated Fe species and surface paramagnetic oxygen were substantially linked to the increased efficiency in a magnetic field. When a considerable magnetic field (450 mT) was introduced to the anode, electrocatalytic water oxidation in the alkaline media was revealed to be significantly strengthened by magnetism [108]. The use of an external magnetic field for water splitting investigations is suggested by the fact that magnetic enhancement works even on decorated Ni-foam electrodes with extremely high current densities, increasing their intrinsic activity by around 40% to reach over 1 A/cm<sup>2</sup> at low overpotentials. Thermal conversion investigations were carried out using magnetic field-assisted catalytic pyrolysis of biomass to produce H<sub>2</sub>-rich gases from wood sawdust [111]. The outcomes of this experiment revealed that a 10 weight percent of a Ni/CaO catalyst with adequate magnetic properties had a favorable catalytic capacity to create H<sub>2</sub> by pyrolyzing biomass. With increased magnetic field strength, the H<sub>2</sub> quantity and output increased. The H<sub>2</sub> content and output exceeded 62 vol.% and 469 mL/g, respectively, at 650 °C, 80 m T magnetic field intensity, and 10 wt.% Ni/CaO catalyst. They improved by around 10 % and 20 %, correspondingly, in comparison to the absence of a magnetic field. As a result, a promising approach for using biomass is biomass catalytic pyrolysis supported by a magnetic field.

An external magnetic field was connected with a catalytic packed bed reactor for selective generation of methanol via CO<sub>2</sub> hydrogenation over Cu and Fe loaded on highly porous ZSM-5 zeolite in an effort to address both economical and environmental concerns regarding the green generation of methanol [88,112]. It was observed that the selectivity and catalytic activity of CO<sub>2</sub> hydrogenation significantly improved with the presence of an external magnetic field. The catalyst 10Cu-10Fe/ZSM-5 showed the maximum CO<sub>2</sub> conversion at a CO<sub>2</sub>/H<sub>2</sub> molar ratio of 1:3 in the presence of an external magnetic field. At 220 °C, the external magnetic field enhanced the selectivity to methanol and the CO<sub>2</sub> conversion by factors of 1.7 and 2.24, respectively. Therefore, the use of magnetic fields promotes CO<sub>2</sub> adsorption and results in the generation of selective methanol, paving the way for the potential to introduce a green and sustainable technology in both petrochemical and chemical processes. An external magnetic field is used in an initiative to improve the catalytic efficiency of the CO<sub>2</sub> hydrogenation reaction based on green and efficient exploitation concepts [6]. Based on the activity and selectivity of Fe-based catalysts with ferro/ferrimagnetic properties, the effects of magnetic field orientation and magnetic flux density were demonstrated. In comparison to those without a magnetic field, CO<sub>2</sub> conversions were dramatically increased by 1.5–1.8 times with an external magnetic field, particularly in the north–south (N–S) direction, while activation energy was reduced by 1.1–1.15 times. When the magnetic flux density was changed, the rate of CO<sub>2</sub> conversion improved in the following order: 27.7 mT > 25.1 mT > 20.8 mT. These exceptional catalytic activities can be attributed to the magnetic field's role in facilitating reactant adsorption and surface reactions over the magnetized Fe catalysts, which reduces apparent activation energy and increases selectivity to hydrocarbons and CH<sub>3</sub>OH.

Successful demonstrations of a magnetic field's impact on CO<sub>2</sub> conversion over the Cu-ZnO/ZrO<sub>2</sub> catalyst in the hydrogenation reaction were established [113]. The maximum CO<sub>2</sub> conversions were achieved at 220 °C with a magnetic field of 20.8 mT in the SN direction, which was three times greater than the results obtained without a magnetic field. Haiping Pan et al. established efficient magnetic field adjustment of the radical-pair spin states in electrocatalytic carbon dioxide reduction [114]. This work demonstrates that applying an external magnetic field for electrocatalytic CO<sub>2</sub> reduction to formate/formic acid considerably increases the catalytic performance of tin nanoparticle catalysts. The generation of formic acid can roughly double in comparison to zero magnetic fields when a standard Sn nanoparticle electrode is used as an example, and a constant external magnetic field of about 0.9 T is utilized. Figure 16 shows the effect of the external magnetic field on the formate yield, which depends on the applied electrode potential for different molar

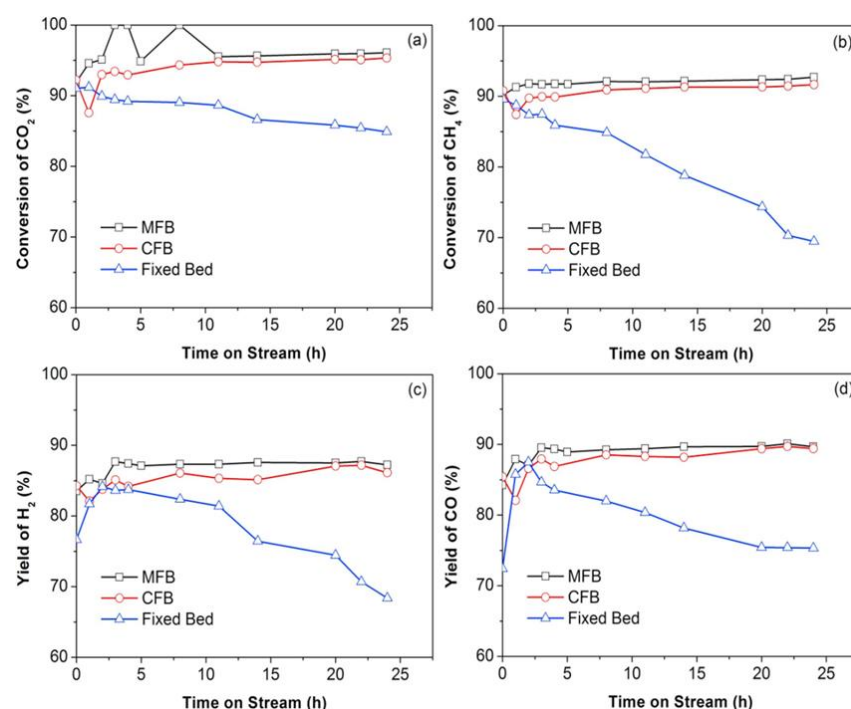
concentrations of  $\text{KHCO}_3$  electrolytes at 1.7 V (vs. Ag/AgCl). This discovery paves the path for increased formate synthesis in the electrocatalytic reduction of  $\text{CO}_2$  and points to the benefits of radical-pair spin states in the electron transfer process.



**Figure 16.** Magnetic field-dependent enhancement of formate yield (−1.7 V (vs/ Ag/AgCl)) with the same applied electrode potential for different concentrations of  $\text{KHCO}_3$  electrolytes. Reprinted with permission from [114]. Copyright (2020), with permission from the American Chemical Society.

Magnetic field-assisted acceleration of  $\text{CO}_2$  reforming of methane over an innovative hierarchical Co/MgO catalyst was performed [115]. The Co/MgO catalyst was developed through a hydrothermal precipitation route. The  $\text{CO}_2$ - $\text{CH}_4$  reforming reaction was carried out at atmospheric pressure in a bench-scale fluidized bed reactor system that included a gas feeding functionality, a fluidized bed reactor colocated with a heat furnace, and a GC analyzer. The catalyst nanoparticles were pre-reduced by utilizing  $\text{H}_2$  (100 mL/min) at 800 °C for 1 h before the experiment. Following the reduction, the feed gas was fed into the reactor to begin the  $\text{CO}_2$  reforming test, with a  $\text{CH}_4/\text{CO}_2/\text{N}_2$  molar ratio of 1:1:1. A total of 0.2 g of the nanoparticles was added to the fluidized bed reactor for the activity. Four parallel solenoids created an axial uniform magnetic field in the case of the MFB reactor, and the current of the power source could be adjusted to modulate the magnetic field's strength (H). The magnetic field employed had a 130 Oe intensity, which is equivalent to a 344W electric energy input. The calcined CoO/MgO particle has a hierarchical architecture and gyroscopic-like structure, with an average dimension of 25 nm. Many octahedral MgO nanostructures, with a crystal size of around 40 nm, self-assembled to form the particle. Figure 17 illustrates the stability test results for the Co-MgO catalyst with the MFB and CFB reactors. The first  $\text{CO}_2$ - $\text{CH}_4$  reformation performance of the Co/MgO catalyst in the CFB reactor was outstanding, with high  $\text{CO}_2$  conversion (about 92%) and  $\text{CH}_4$  conversion (nearly 90%). The conversions of  $\text{CO}_2$  and  $\text{CH}_4$  under the MFB and CFB reactors did not significantly decrease during the stability test of 24 h (Figure 17a,b). For the first three hours of the course of the reaction, the production of  $\text{H}_2$  and CO for the MFB reactor displayed a modest induction period before remaining constant (Figure 17c,d). The conversions of  $\text{CO}_2$  and  $\text{CH}_4$  were enhanced by 22% and 30%, respectively, in the magnetic-assisted fluidized bed reactor at 800 °C, with high gas at an hourly space velocity of  $15 \times 10^4$  /h. The hierarchical Co/MgO catalyst's increased activity and great resistance to coke deposition are related to the development of clusters, which exhibit a high frequency of breaking and consolidating under the influence of a magnetic field.



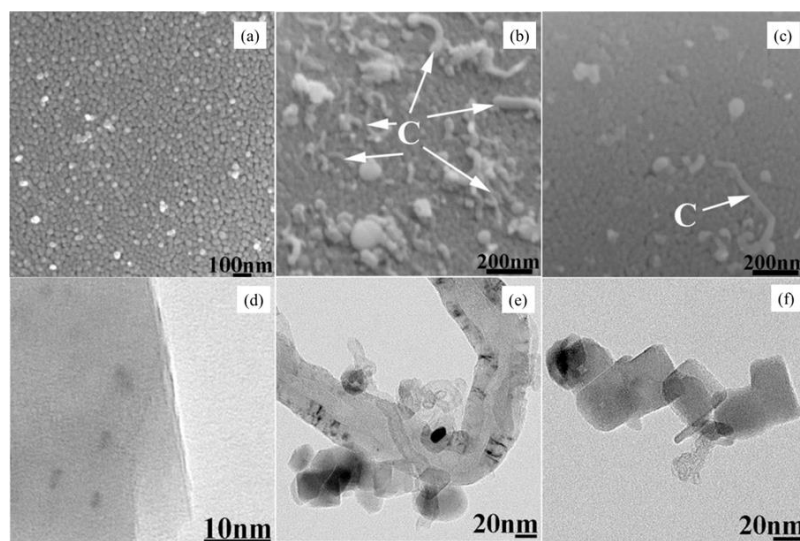


**Figure 17.** Catalytic stability experiments with GHSV of 60,000/h. Conversions of (a) CO<sub>2</sub>, (b) CH<sub>4</sub>, the yields of (c) H<sub>2</sub> and (d) CO. Reprinted from [115]. Copyright (2018), with permission from Elsevier.

In general, carbon development can originate from the Boudouard reaction below 700 °C, where CO dissociates to generate surface carbon and CO<sub>2</sub>, and CH<sub>4</sub> decomposition occurs beyond 557 °C, where CH<sub>4</sub> totally dissociates to form solid carbon on the surface of the catalyst and produce H<sub>2</sub>. After 24 h of CO<sub>2</sub>-CH<sub>4</sub> reforming at 800 °C, the used catalysts were examined by SEM and TEM to investigate the carbon deposition and changes to the catalysts' crystal size. Based on the structural examination, carbon diffraction peaks are clearly visible from the used catalysts in the CFB and MFB reactors, suggesting the presence of carbon deposition. As can be seen from the SEM image (Figure 18a–c), neither the CFB nor the MFB reactors contain any long carbon nanotubes or wires on top of the Co/MgO particles. In the conventional fluidized bed, numerous short, irregular carbon nanotubes are seen deposited on the exterior of the used catalyst in comparison to the fresh catalyst. On the catalyst that had been used up in the MFB reactor, less carbon nanotubes are seen. The fresh Co/MgO catalyst has Co NPs that are less than 5 nm in size, according to the TEM micrograph in Figure 18d. After the stability test, the average Co NP dimensions of the used Co/MgO catalysts for both the CFB and MFB reactors reveal a minor sintering compared to the fresh Co/MgO catalyst. The Co NPs after sintering show no overt response to the presence of magnetic field. This outcome contrasts with that of CO methanation in a magnetic fluidized bed reactor, where the axial magnetic field helped reduce catalyst agglomerates and prevent the sintering of NiCo particles [116]. The hierarchical Co/MgO catalyst's structure and modified particle size, which enable the hierarchical Co/MgO particle to remain an individual particle, are responsible for this variance. Following the stability test in the CFB reactor, numerous Co NPs are detached from the MgO carrier's surface and completely disseminated over the carbon nanotubes. However, due to the magnetic susceptibility of Co NPs and their interaction with one another, this transition of Co NPs is considerably diminished in the MFB reactor, as observed from the TEM micrograph in Figure 18d–f. Additional research is required to better understand the Co NPs' transition phenomena. To conclude, an axial magnetic field promotes the stability of Co particles, reduces carbon deposition, and increases the reforming rate. The suggested method successfully produces syngas via CO<sub>2</sub>-

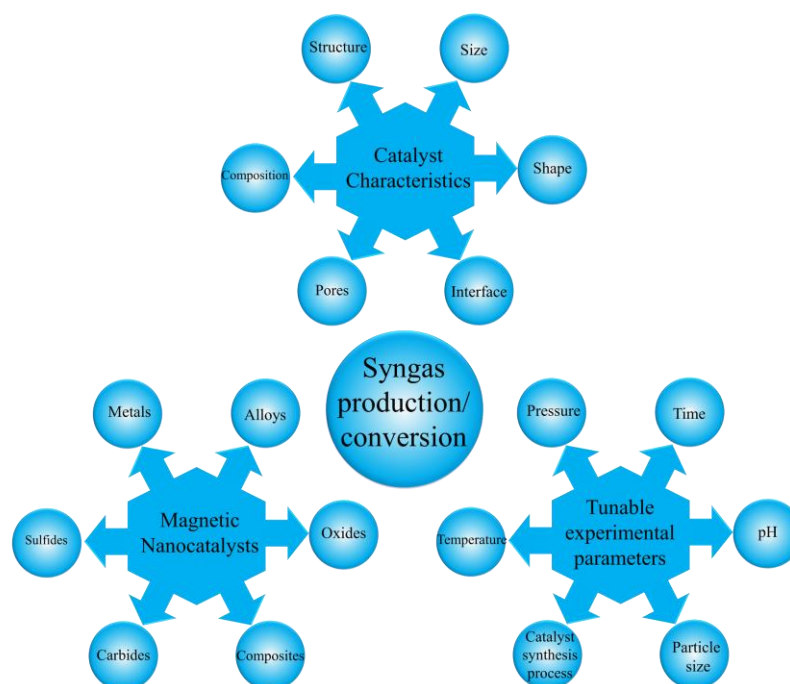


CH<sub>4</sub> reforming with improved catalytic activity through the combination of a magnetic fluidized bed and a structured nanoparticle catalyst.



**Figure 18.** (a–c) SEM and (d–f) TEM micrographs of pure Co-MgO and used Co-MgO after reforming reaction in a conventional fluidized bed reactor and a magnetic-assisted fluidized bed (MFB) reactor. Reprinted from [115]. Copyright (2018), with permission from Elsevier.

The reviewed studies suggest that there are still a lot of opportunities and challenges in the effective utilization of external magnetic fields for syngas production and conversion applications. It is important to optimize magnetic nanoparticle or nanocomposite formation as the magnetic responses to external magnetic fields mainly depend on the magnetic characteristics of the materials. Furthermore, the range of the external magnetic field for selected magnetic materials also needs an optimization to obtain a better efficiency in syngas production and conversion applications. Moreover, understanding the role of external magnetic field in syngas production and conversion is also crucial, as the magnetic field itself could alter the chemical reaction kinetics even though it does not have magnetic characteristics. We could see that a non-magnetic material could also be influenced by an external magnetic field. By considering these factors, researchers could conduct a better investigation on the effect of external magnetic field on syngas production and conversion to achieve a better efficiency. The main characteristics of magnetic nanomaterials as catalysts, the types of magnetic nanomaterials, and the experimental parameters that can be tuned to improve the performance of catalysts for syngas production/conversion is schematically shown in Figure 19.



**Figure 19.** Schematic diagram for the typical characteristics of magnetic nanomaterials, types of magnetic nanomaterials, and experimental parameters that can be tuned to improve the performance of catalysts for syngas production/conversion.

## 8. Summary and Scope

We have introduced a brief discussion of magnetic materials, and the different preparation processes for the synthesis of magnetic nanomaterials are also discussed. A brief introduction to the syngas production/conversion process and the major experimental parameters, such as temperature, pH, time, and other reaction parameters that can influence the efficiency of the process, are included. The magnetic materials that this review has mainly focused on belong to Fe-, Ni-, and Co-based materials. The last section discusses the possibility of effectively utilizing an external magnetic field for the synthesis of magnetic nanocatalysts. The role of external magnetic field on the catalysis process of syngas production/conversion process is discussed with suitable examples. The advantages of magnetic nanomaterials over other available catalysts are their magnetic characteristics. One can tune the magnetic properties of magnetic materials by tuning their stoichiometry and morphology. Furthermore, the magnetic properties could be tuned by the addition of foreign elements or materials through composite formation. The required magnetic characteristics of these magnetic materials could be achieved by employing suitable experimental parameters and a suitable surface modifier. The magnetic separation process could be used to collect used magnetic nanocatalysts, which may be used for another cyclic performance. We strongly believe that the addition of an external magnetic field to the synthesis of magnetic nanoparticles and to the catalysis process could effectively alter the efficiency of the process. However, the range of the external magnetic field should be optimized, depending on the magnetic characteristics of the magnetic nanocatalysts for better performance.

**Author Contributions:** Conceptualization, A.T. and N.C.; writing—original draft preparation, S.J.J.K. and S.P.; writing—review and editing, P.S., S.D., S.S., S.-K.K. and R.M.; supervision and writing—review and editing, A.T. and N.C. All authors have read and agreed to the published version of the manuscript.

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**Data Availability Statement:** The data presented in this study are available from the corresponding author upon request.

**Conflicts of Interest:** The authors declare no conflict of interest.

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## Article

# Performance of Particulate and Structured Pt/TiO<sub>2</sub>-Based Catalysts for the WGS Reaction under Realistic High- and Low-Temperature Shift Conditions

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**Abstract:** The water–gas shift (WGS) activity of Pt/TiO<sub>2</sub>-based powdered and structured catalysts was investigated using realistic feed compositions that are relevant to the high-temperature shift (HTS) and low-temperature shift (LTS) reaction conditions. The promotion of the TiO<sub>2</sub> support with small amounts of alkali- or alkaline earth-metals resulted in the enhancement of the WGS activity of 0.5%Pt/TiO<sub>2</sub>(X) catalysts (X = Na, Cs, Ca, Sr). The use of bimetallic (Pt–M)/TiO<sub>2</sub> catalysts (M = Ru, Cr, Fe, Cu) can also shift the CO conversion curve toward lower temperatures, but this is accompanied by the production of relatively large amounts of unwanted CH<sub>4</sub> at temperatures above ca. 300 °C. Among the powdered catalysts investigated, Pt/TiO<sub>2</sub>(Ca) exhibited the best performance under both HTS and LTS conditions. Therefore, this material was selected for the preparation of structured catalysts in the form of pellets as well as ceramic and metallic catalyst monoliths. The 0.5%Pt/TiO<sub>2</sub>(Ca) pellet catalyst exhibited comparable activity with that of a commercial WGS pellet catalyst, and its performance was further improved when the Pt loading was increased to 1.0 wt.%. Among the structured catalysts investigated, the best results were obtained for the sample coated on the metallic monolith, which exhibited excellent WGS performance in the 300–350 °C temperature range. In conclusion, proper selection of the catalyst structure and reaction parameters can shift the CO conversion curves toward sufficiently low temperatures, rendering the Pt/TiO<sub>2</sub>(Ca) catalyst suitable for practical applications.

**Keywords:** water gas shift; platinum; TiO<sub>2</sub>; promoter; structured catalysts; pellets; monoliths

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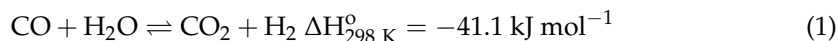
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## 1. Introduction

The water–gas shift (WGS) reaction (Equation (1)) is a well-established industrial process that is commonly used to reduce the CO concentration and increase the hydrogen content in the synthesis gas produced via reforming/partial oxidation of carbon-containing fuels [1–4].



The reaction is equilibrium-controlled and moderately exothermic and is therefore thermodynamically favored at low temperatures, and kinetically favored at high temperatures. As a result, the reaction is typically performed in industrial processes using two adiabatic reactors in sequence, with intermediate cooling. The first reactor operates at 350–450 °C using a Fe–Cr based oxide catalyst (high-temperature shift, HTS), and the second at 200–250 °C using Cu–Zn based catalysts (low-temperature shift, LTS) [1–4]. The inherent disadvantages of the classic commercial HTS catalysts (e.g., toxicity of hexavalent Cr and demanding reduction process to avoid sintering) and LTS catalysts (e.g., relatively low activity, pyrophoricity, thermal sintering, and leaching of active component) render them unsuitable for mobile and small-to-medium scale applications [2,3,5]. Therefore, efforts are currently focused on the development of alternative WGS catalysts that fulfill

the requirements for use in compact fuel processors. In this respect, metal oxide-supported noble metals have been extensively studied due to their superior kinetic performance and stability under frequent start-up/shut-down and varied duty cycle operations [1,4–6]. Among the noble metal catalysts investigated, platinum supported on partially reducible oxides such as CeO<sub>2</sub> and TiO<sub>2</sub> exhibit the highest WGS activity [1,7–9]. However, most of the above studies reported results with powder catalyst samples, which are not directly relevant to practical applications where the catalyst is in the form of pellets or monoliths. Pellets provide a high surface area of catalyst per unit reactor volume and are easy to handle and replace, whereas monolithic catalysts offer several advantages including lower pressure drop, good thermal shock resistance, robustness, and fast response to transient operation [10,11]. The competitive performance of structured noble metal-containing WGS catalysts has been investigated in several studies [6,10–17], but only a few of them have been performed under realistic reaction conditions. In our previous work, we investigated in detail the performance for the WGS reaction of noble metal catalysts (Pt, Rh, Ru, Pd) dispersed on reducible (TiO<sub>2</sub>, CeO<sub>2</sub>, La<sub>2</sub>O<sub>3</sub>, YSZ) and irreducible (Al<sub>2</sub>O<sub>3</sub>, MgO, SiO<sub>2</sub>) metal oxide supports [7,8]. Among the metal–support combinations investigated, Pt/TiO<sub>2</sub> was found to exhibit the highest WGS activity, which could be further enhanced following the promotion of TiO<sub>2</sub> with small amounts of alkali (Li, Na, K, Cs) [18] or alkaline earth metals (Mg, Ca, Sr, Ba) [19]. This has been attributed to the promoter-induced creation of dual function Pt – □<sub>s</sub> – Ti<sup>3+</sup> sites at the metal–support interface, where □<sub>s</sub> denotes an oxygen defect, which are required for the WGS reaction to proceed. The adsorption strength of these sites toward hydrogen was found to depend on the nature of the promoter and decreased with an increase in its content [18–20].

The objective of the present work was to investigate the performance of the previously developed Pt/TiO<sub>2</sub>-based catalysts under realistic reaction conditions using feed compositions that are relevant to the HTS and LTS reactions. The effects of the dispersion of a second metal (Fe, Cu, Cr, Ru) on the support were also studied. The performance of the optimized catalysts in the form of pellets or wash-coating on ceramic and metallic monoliths was further investigated under realistic conditions and was compared with that of a commercial catalyst obtained from Johnson Matthey. To the best of our knowledge, this is one of the few reports to deal with the development of structured Pt/TiO<sub>2</sub>-based catalysts and testing under HT- and LT-WGS conditions that are relevant to practical applications and can be regarded as an essential step toward the commercialization of these materials.

## 2. Results and Discussion

The powdered and structured catalysts synthesized are listed in Table 1. The composition of the Pt/TiO<sub>2</sub>(X) catalysts (X = Na, Cs, Ca, Sr) was selected based on the results of our previous studies, which showed that the WGS activity of platinum dispersed on alkali- and alkaline earth metal-promoted TiO<sub>2</sub> exhibited a volcano-type dependence on the promoter content and was maximized for samples containing 0.06 wt.% Na, 0.34 wt.% Cs, 2.0 wt.% CaO, or 1.0 wt.% SrO [18,19]. Regarding the bimetallic (Pt–M)/TiO<sub>2</sub> catalysts (M = Ru, Fe, Cr, Cu), the second metal (M) was chosen based on the well-known activity of Fe/Cr and Cu for the HTS and LTS reactions, respectively, [1–4] and the high WGS activity of Ru supported on reducible metal oxides [7,8].

**Table 1.** Physicochemical characteristics of the synthesized catalysts.

Catalyst Notation	Nominal Composition (wt.%)	Specific Surface Area (SSA) <sup>1</sup> (m <sup>2</sup> /g)	Anatase Content <sup>2</sup> (%)	Pt Dispersion <sup>3</sup> (%)	Pt Crystallite Size <sup>3</sup> (nm)
Pt/TiO <sub>2</sub>	0.5%Pt/TiO <sub>2</sub>	49	85	85	1.2
Pt/TiO <sub>2</sub> (Na)	0.5%Pt/TiO <sub>2</sub> (0.06%Na)	30	47	93	1.1
Pt/RiO <sub>2</sub> (Cs)	0.5%Pt/TiO <sub>2</sub> (0.34%Cs)	31	58	95	1.1
Pt/TiO <sub>2</sub> (Ca)	0.5%Pt/TiO <sub>2</sub> (2%CaO)	40	65	78	1.3
Pt/TiO <sub>2</sub> (Sr)	0.5%Pt/TiO <sub>2</sub> (1%SrO)	38	62	94	1.1
(Pt–Ru)/TiO <sub>2</sub>	(0.5%Pt–0.1%Ru)/TiO <sub>2</sub>	46	68	n.m. <sup>4</sup>	n.m.

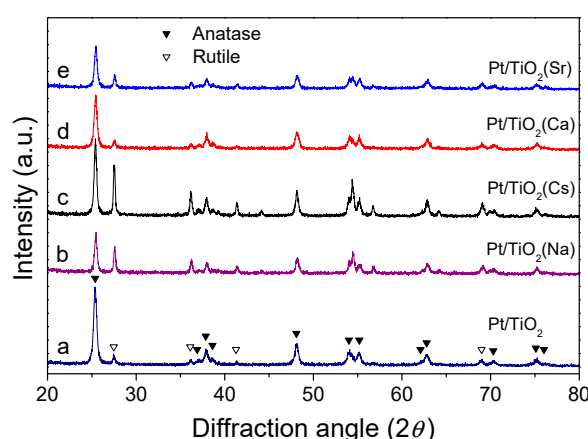
Table 1. Cont.

Catalyst Notation	Nominal Composition (wt.%)	Specific Surface Area (SSA) <sup>1</sup> (m <sup>2</sup> /g)	Anatase Content <sup>2</sup> (%)	Pt Dispersion <sup>3</sup> (%)	Pt Crystallite Size <sup>3</sup> (nm)
(Pt–Fe)/TiO <sub>2</sub>	(0.5%Pt–0.5%Fe)/TiO <sub>2</sub>	49	67	n.m.	n.m.
(Pt–Cr)/TiO <sub>2</sub>	(0.5%Pt–0.5%Cr)/TiO <sub>2</sub>	50	62	n.m.	n.m.
(Pt–Cu)/TiO <sub>2</sub>	(0.5%Pt–0.5%Cu)/TiO <sub>2</sub>	45	66	n.m.	n.m.
TiO <sub>2</sub> -P	TiO <sub>2</sub> pellets	42	n.m.	n.m.	n.m.
0.5Pt/TiO <sub>2</sub> (Ca)-P	0.5%Pt/TiO <sub>2</sub> (2%CaO) pellets	37	n.m.	90	1.1
1.0Pt/TiO <sub>2</sub> (Ca)-P	1.0%Pt/TiO <sub>2</sub> (2%CaO) pellets	38	n.m.	92	1.1
Pt/TiO <sub>2</sub> (Ca)-MM	0.5%Pt/TiO <sub>2</sub> (2%CaO) coated on metallic monolith				
Pt/TiO <sub>2</sub> (Ca)-CM	0.5%Pt/TiO <sub>2</sub> (2%CaO) coated on ceramic monolith				

<sup>1</sup> Estimated with the BET method; <sup>2</sup> Anatase content of TiO<sub>2</sub> calculated from the XRD patterns; <sup>3</sup> Estimated from the H<sub>2</sub> chemisorption measurements; <sup>4</sup> Not measured.

### 2.1. Physicochemical Characteristics of the Synthesized Catalysts

The X-ray diffraction (XRD) patterns obtained for the representative powdered catalysts are shown in Figure 1. It was observed that, in all cases, the diffractograms consisted of peaks attributable to the anatase (JCPDS Card No. 4-477) and rutile (JCPDS Card No. 21-1276) phases of TiO<sub>2</sub>. Qualitatively similar results were obtained for all of the catalyst samples investigated (not shown for brevity). The specific surface area (SSA) and anatase content of TiO<sub>2</sub> ( $x_A$ ) were considerably lower for the samples promoted with Na or Cs compared to the unpromoted Pt/TiO<sub>2</sub> (Table 1). This can be attributed to the synthesis method employed, which involved the heat treatment of the corresponding supports at 600 °C. This treatment is known to result in the partial transformation of the anatase phase of TiO<sub>2</sub> to rutile and is accompanied by particle growth and a decrease in the SSA [19]. In contrast, the SSA and anatase content were partially retained for the alkaline earth (Ca, Sr)-promoted catalysts (Table 1). This is in agreement with the results of our previous studies, which showed that the incorporation of foreign cations in the crystal matrix of TiO<sub>2</sub> resulted in an increase in the anatase-to-rutile phase transition temperature and in the stabilization of the specific surface area of the host material [19,21]. Regarding the bimetallic (Pt–M)/TiO<sub>2</sub> (M = Ru, Fe, Cr, Cu) catalysts, it was observed that their SSA and anatase content were not significantly different compared to the unpromoted Pt/TiO<sub>2</sub> sample (Table 1).

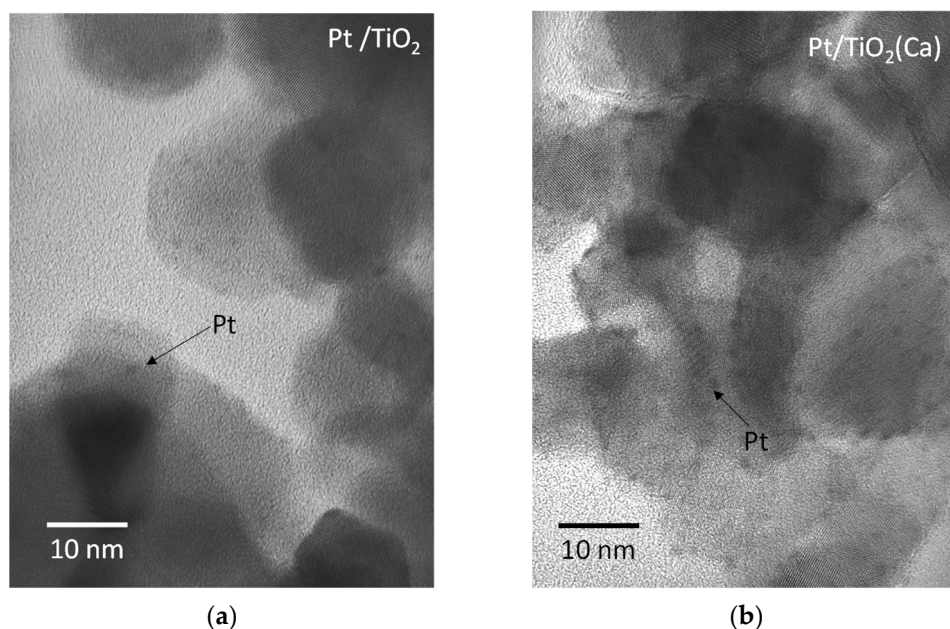


**Figure 1.** X-ray diffraction patterns of the indicated catalysts. (a) Pt/TiO<sub>2</sub>; (b) Pt/TiO<sub>2</sub>(Na); (c) Pt/TiO<sub>2</sub>(Cs); (d) Pt/TiO<sub>2</sub>(Ca); (e) Pt/TiO<sub>2</sub>(Sr).

The average crystallite size of the TiO<sub>2</sub> particles, estimated using the Scherrer equation, did not vary appreciably from one catalyst to another, taking values in the ranges of 20–26 nm for anatase and 25–35 nm for rutile for all of the samples investigated. Therefore, the observed differences in the performance of these samples should not be attributed to this parameter, which is known to affect the WGS activity of TiO<sub>2</sub>-supported Pt catalysts [7].

The Pt dispersion and average crystallite size were estimated for the monometallic catalysts from the  $H_2$  chemisorption measurements and the results obtained are listed in Table 1. It should be noted that this method could not be applied for the bimetallic (Pt–M) samples because hydrogen interacts with both metals. It was observed that Pt was very well-dispersed on all supports studied, forming crystallites with an average size in the range 1.1–1.3 nm.

Representative TEM images obtained for the Pt/TiO<sub>2</sub> and Pt/TiO<sub>2</sub>(Ca) catalysts are shown in Figure 2. It was observed that platinum was very well-dispersed on the surface of both the TiO<sub>2</sub> (Figure 2a) and TiO<sub>2</sub>(Ca) (Figure 2b) supports. The size of the Pt crystallites was in the range of 1–2 nm, in very good agreement with the results of the  $H_2$ -chemisorption measurements (Table 1). The SEM images with EDS mapping of the above two catalysts are shown in the Supplementary Materials (Figures S1 and S3). It was observed that Pt was homogeneously distributed on the surface of both catalysts (Figures S1 and S3), and the same was true for the Ca present in the TiO<sub>2</sub>(Ca) support (Figure S2).

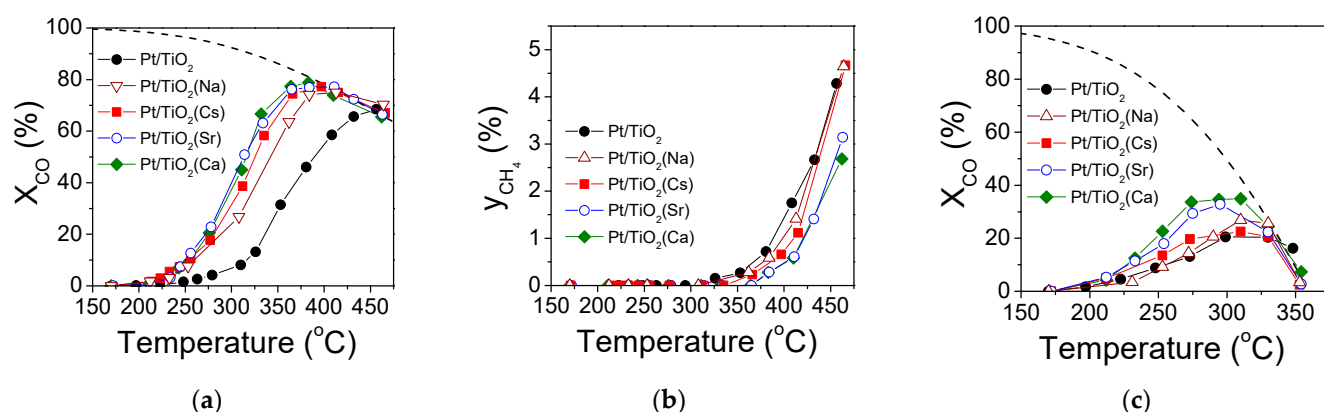


**Figure 2.** The TEM images of the (a) Pt/TiO<sub>2</sub> and (b) Pt/TiO<sub>2</sub>(Ca) powdered catalysts.

## 2.2. Performance of Particulate Catalysts

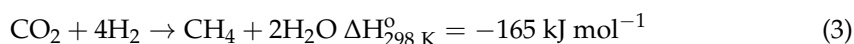
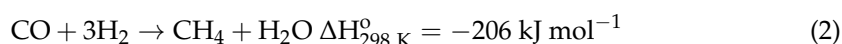
### 2.2.1. Alkali- and Alkaline Earth Metal-Promoted Catalysts

The WGS activity of the synthesized alkali- and alkaline earth-promoted Pt/TiO<sub>2</sub> catalysts was investigated using two different feed compositions, which are representative of the high temperature shift (HTS) and the low temperature shift (LTS) reaction conditions. Figure 3a shows the CO conversion curves obtained under HTS conditions. It was observed that the unpromoted Pt/TiO<sub>2</sub> catalyst became active at temperatures around 250 °C. Conversion of CO ( $X_{CO}$ ) progressively increased with the increase in the temperature and reached equilibrium at ca. 450 °C. Promotion of the TiO<sub>2</sub> support with small amounts of alkali metals resulted in a significant enhancement in the WGS activity, which was evidenced by the shift of the CO conversion curves obtained for the Pt/TiO<sub>2</sub>(Na) and Pt/TiO<sub>2</sub>(Cs) catalysts toward lower temperatures by ca. 40 °C and 50 °C, respectively, compared to the unpromoted sample. The performance of the two alkaline earth metal-promoted catalysts was even better than that of the alkali-promoted samples. Optimal results were obtained for Pt/TiO<sub>2</sub>(Ca), which achieved an equilibrium CO conversion at ca. 390 °C (Figure 3a).



**Figure 3.** Performance of the alkali- and alkaline earth metal-promoted catalysts: Effect of reaction temperature on (a) the conversion of CO and (b) the yield of CH<sub>4</sub> under HTS conditions (feed composition: 9.7%CO, 38.7%H<sub>2</sub>O, 44.8%H<sub>2</sub>, 6.8%CO<sub>2</sub>). (c) Effect of reaction temperature on the conversion of CO under LTS conditions (feed composition: 1.6%CO, 29.9%H<sub>2</sub>O, 52.2%H<sub>2</sub>, 16.3%CO<sub>2</sub>). Mass of the catalyst: 750 mg; total flow rate: 220 cm<sup>3</sup> min<sup>−1</sup>. The equilibrium CO conversion curves are shown with dashed lines.

Under the HTS conditions employed in Figure 3a, all samples catalyzed the CO/CO<sub>2</sub> methanation reactions at elevated temperatures:



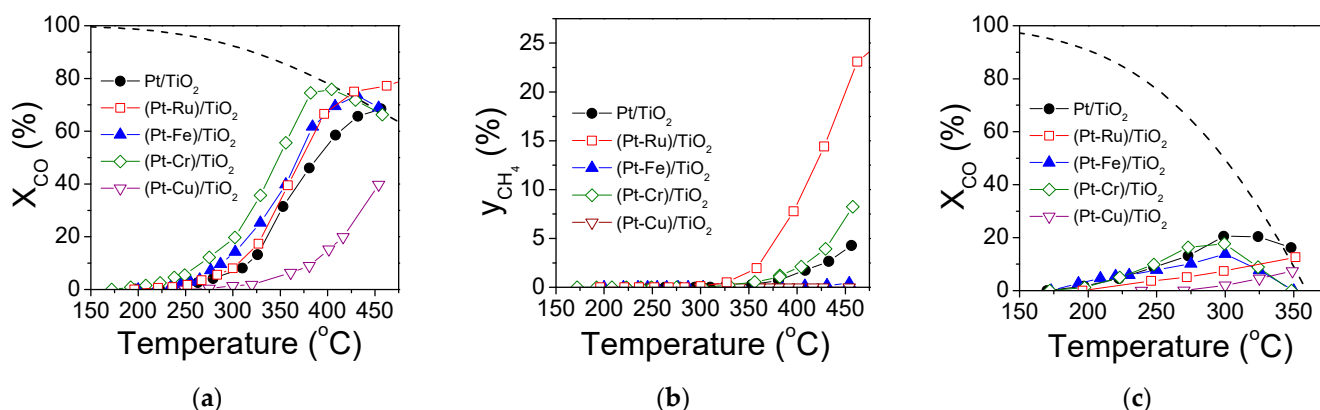
These reactions are unwanted because they reduce the yield of H<sub>2</sub> and may result in large exotherms. As shown in Figure 3b, methane formation started at ca. 320 °C and the yield of methane ( $y_{\text{CH}_4}$ ) increased considerably with the increase in the reaction temperature. Interestingly, the best performing HTS catalysts, namely, Pt/TiO<sub>2</sub>(Ca) and Pt/TiO<sub>2</sub>(Sr), produced lower amounts of methane compared to the unmodified Pt/TiO<sub>2</sub> and the alkali-promoted samples. It should be noted that the occurrence of the CO methanation reaction in parallel to the WGS reaction can explain the observation that  $X_{\text{CO}}$  slightly exceeded the equilibrium CO conversion at high temperatures under these conditions (Figure 3a).

Results of the catalytic performance tests obtained under LTS conditions are shown in Figure 3c. It was observed that catalyst ranking follows the same trend with that of the HTS experiments, with Pt/TiO<sub>2</sub>(Ca) exhibiting the highest activity. It should be noted that under the LTS conditions, only negligible amounts of CH<sub>4</sub> were detected at the reactor effluent in the temperature range investigated.

In our previous studies [18–20], the enhanced WGS activity of the alkali/alkaline earth-promoted Pt/TiO<sub>2</sub> catalysts was attributed to the creation of Pt – □<sub>s</sub> – Ti<sup>3+</sup> active sites located at the metal–support interface. The population of this type of site is expected to increase under conditions that favor the decoration of the metal crystallites by TiO<sub>x</sub> suboxides [22], in accordance with the SMSI effect [8,18,20,23–26]. It should be noted, however, that the SMSI effect is not expected to be significant under the conditions employed here. This is because the migration of suboxide species on the surface of dispersed metal crystallites is known to become important following reduction at temperatures typically higher than 500 °C and is not operable in the presence of water [23,24]. The promotion of TiO<sub>2</sub> by alkali/alkaline earth metals induces the same effect as SMSI as it also leads to the creation of □<sub>s</sub> – Ti<sup>3+</sup> defects. Moreover, this is undertaken in a controlled manner, depending on the dopant content, and is permanent. Therefore, it can be viewed as a “permanent” SMSI effect [18,20].

### 2.2.2. Bimetallic Catalysts

An attempt was made to enhance the WGS activity of the 0.5%Pt/TiO<sub>2</sub> catalyst by dispersing a second metal (M = Ru, Fe, Cr, Cu) on the support, in addition to Pt. Results obtained for the HTS reaction over the (0.5%Pt–0.5%M)/TiO<sub>2</sub> catalysts are shown in Figure 4a. It was observed that the addition of Cu, which is a component of commercial LTS catalysts [3], resulted in a significant shift in the CO conversion curve toward higher temperatures compared with the monometallic Pt/TiO<sub>2</sub> sample. On the other hand, the addition of Fe or Cr, which are components of commercial HTS catalysts [3], has a favorable effect as the X<sub>CO</sub> curves shift toward lower temperatures by ca. 10–20 °C. A similar and more pronounced beneficial effect was observed following the addition of Ru. However, the (Pt–Ru)/TiO<sub>2</sub> catalyst promotes the unwanted CO/CO<sub>2</sub> methanation reactions at elevated temperatures (Figure 4b), rendering it unsuitable for practical applications. This observation is in agreement with the results of our previous study, which showed that the CO/CO<sub>2</sub> methanation activity of Ru was higher than that of Pt, and was not significantly affected by the presence of water in the feed [27]. Regarding the activity of (Pt–M)/TiO<sub>2</sub> catalysts under LTS conditions, all samples were less active compared to the monometallic Pt/TiO<sub>2</sub> (Figure 4c).



**Figure 4.** Performance of the bimetallic catalysts: Effect of reaction temperature on (a) the conversion of CO and (b) the yield of CH<sub>4</sub> under HTS conditions. (c) Effect of reaction temperature on the conversion of CO under LTS conditions. Experimental conditions are the same as in Figure 3.

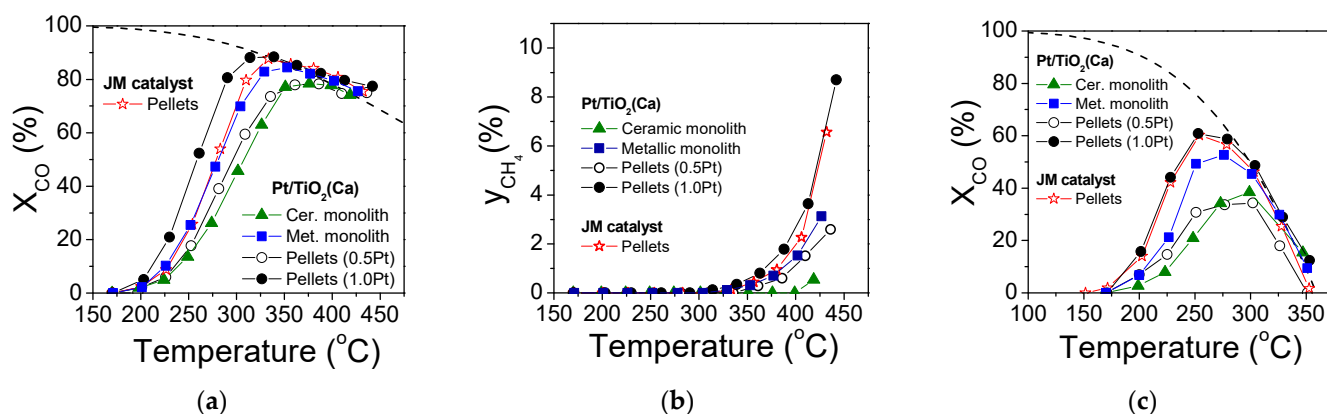
Increasing the Fe or Cr loading of the bimetallic catalysts resulted in decreased performances under both the HTS and LTS conditions. Typical results obtained over the (0.5%Pt–M)/TiO<sub>2</sub> catalysts are shown in the Supplementary Materials (Figure S4). It was observed that increasing the Fe or Cr content from 0.5% to 5.0% resulted in a shift in the CO conversion curves toward higher temperatures, which was more pronounced for (Pt–Cr)/TiO<sub>2</sub>. The yield of methane did not vary appreciably with increasing the Fe or Cr content from 0.5 to 5.0 wt.%. Furthermore, it was found that the performance of bimetallic Pt–M catalysts dispersed on the optimal TiO<sub>2</sub>(Ca) support does not result in materials with improved WGS activity, compared to the monometallic Pt/TiO<sub>2</sub>(Ca) sample (results not shown for brevity).

### 2.3. Performance of Structured Catalysts

Results presented in Figures 3 and 4 show that, among the alkali/alkaline earth metal-promoted Pt/TiO<sub>2</sub>(X) catalysts and the bimetallic (Pt–M)/TiO<sub>2</sub> catalysts investigated, 0.5%Pt/TiO<sub>2</sub>(Ca) exhibited the best performance under both the HTS and LTS reaction conditions. Therefore, this material was selected to prepare structured catalysts in the form of pellets or coatings on ceramic and metallic monoliths to investigate its performance for the WGS reaction under conditions that are more relevant to practical applications. The performance of the above structured samples was compared with that of a commercial catalyst in pellet form obtained from Johnson Matthey (JM) (Product name: W21, 10876, UK).



Results obtained over the structured catalysts with the use of the feed composition corresponding to the HTS conditions are presented in Figure 5a, where the conversion of CO is plotted as a function of the reaction temperature (measured at the exit of the catalyst bed). Regarding the 0.5%Pt/TiO<sub>2</sub>(Ca)-P catalyst (i.e., in pellet form), it was observed that  $X_{CO}$  became measurable at temperatures around 200 °C and reached equilibrium at ca. 400 °C. Comparison with the corresponding results obtained over the powdered Pt/TiO<sub>2</sub>(Ca) sample (Figure 3a) showed that the present CO conversion curve shifted toward lower temperatures (by ca. 50 °C). This was due to the larger amount of catalyst loaded in the reactor (1.8 g vs. 0.75 g) under the same experimental conditions. The performance of the Pt/TiO<sub>2</sub>(Ca)-P catalyst was considerably improved with an increase in the Pt loading from 0.5% to 1.0% (Figure 5a). This is in agreement with the results of our previous studies that showed that the CO conversion curve over TiO<sub>2</sub>-supported noble metal catalysts shifted monotonically toward lower temperatures with an increase in the metal loading from 0.1 to 5.0 wt.% [7,8]. It should be noted, however, that the specific activity (TOF) did not vary appreciably with metal loading, indicating that the WGS is a structure insensitive reaction [7,8]. It is of interest to note that the 1.0%Pt/TiO<sub>2</sub>(Ca) pellet catalyst achieved equilibrium CO conversion at a temperature around 330 °C and was more active than the commercial JM catalyst across the whole temperature range investigated (Figure 5a).



**Figure 5.** Performance of the structured Pt/TiO<sub>2</sub>(Ca) catalysts in the form of pellets or coatings in the channels of ceramic and metallic monoliths in comparison with that of a commercial catalyst (Johnson Matthey, JM): Effect of reaction temperature on (a) the conversion of CO and (b) the yield of CH<sub>4</sub> under HTS conditions. (c) Effect of the reaction temperature on the conversion of CO under LTS conditions. Mass of the synthesized and JM catalyst pellets and the monolith coatings: 1.8 g. Other experimental conditions were the same as in Figure 3.

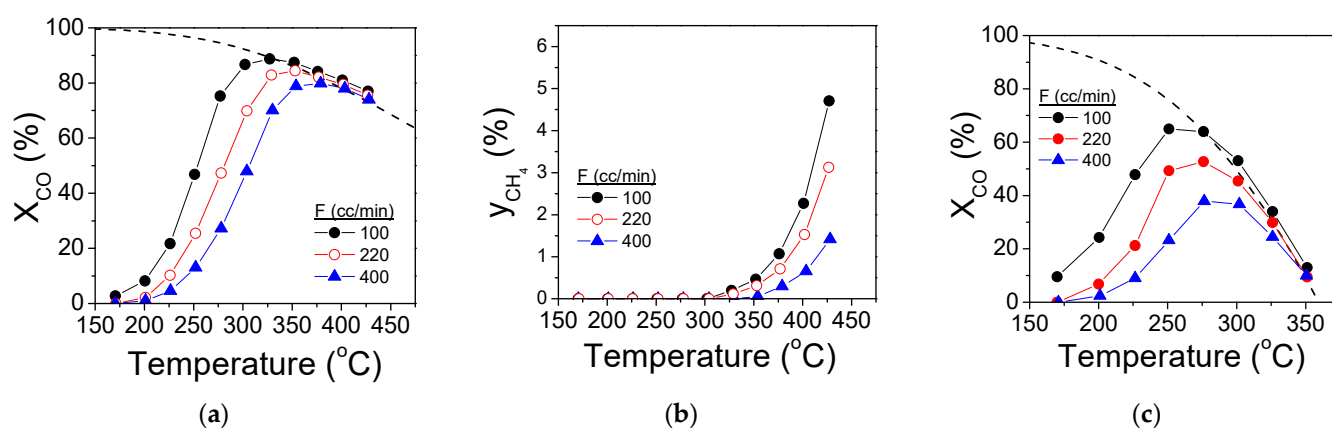
The CO conversion curve obtained for the ceramic monolith coated with 1.8 g of Pt/TiO<sub>2</sub>(Ca) shifted toward slightly higher temperatures (ca. 10 °C) compared to the catalyst in the form of pellets (Figure 5a). On the other hand, the metallic monolith catalyst exhibited improved performance compared to the previous two samples, as the CO conversion reached equilibrium at ca. 350 °C. It is of interest to note that the performance of the latter sample was comparable to that of the commercial JM pellet catalyst. Under the experimental conditions in Figure 5a, all of the structured catalysts investigated produced methane at temperatures above ca. 320 °C (Figure 5b). The yield of methane followed the same trend as that of the WGS activity (i.e., it was lowest for Pt/TiO<sub>2</sub>(Ca)-CM and highest for the 1.0Pt/TiO<sub>2</sub>(Ca)-P and JM samples in the whole temperature range investigated) (Figure 5b).

The performance of the structured catalysts under the LTS conditions is shown in Figure 5c. It was observed that the best performing sample was 1.0%Pt/TiO<sub>2</sub>(Ca)-P, which exhibited a similar performance with the commercial JM catalyst. Regarding the structured catalysts of the same Pt content (0.5 wt.%), the most active one was Pt/TiO<sub>2</sub>(Ca)-MM. It



should be noted that the blank experiments performed over the bare ceramic and metallic monoliths did not show measurable CO conversion under the HTS and LTS conditions employed here.

The effects of the total flow rate (space velocity) on the WGS performance of the best-performing Pt/TiO<sub>2</sub>(Ca)-MM catalyst are shown in Figure 6. Results of similar experiments performed over the cordierite monolithic catalyst are presented in the Supplementary Materials (Figure S5). As expected, an increase in the flow rate from 220 to 400 cm<sup>3</sup> min<sup>−1</sup> resulted in a shift in the CO conversion curves toward higher temperatures under both the HTS and LTS conditions. On the other hand, the X<sub>CO</sub> curves shifted toward lower temperatures upon decreasing the total flow rate to 100 cm<sup>3</sup> min<sup>−1</sup>. It is of interest to note that under these conditions and the use of the HTS feed, the Pt/TiO<sub>2</sub>(Ca)-MM catalyst achieved equilibrium CO conversion at around 320 °C (Figure 6a), where the production of CH<sub>4</sub> is negligible (Figure 6b). The catalyst also performed well under LTS conditions, where equilibrium CO conversion was achieved at ca. 270 °C (Figure 6c).



**Figure 6.** Effects of the total flow rate (*F*) on the performance of the Pt/TiO<sub>2</sub>(Ca) catalyst coated on the channels of the metallic monolith: (a) Conversion of CO and (b) yield of CH<sub>4</sub> under HTS conditions. (c) Conversion of CO under LTS conditions. Other experimental conditions are the same as in Figure 5.

It should be noted that the temperature profile along the Pt/TiO<sub>2</sub>(Ca)-MM catalyst was practically uniform under both the HTS and the LTS conditions employed here (see Supplementary Materials, Figure S6). In contrast, the temperature along the ceramic monolithic catalyst was found to increase toward the exit of the reactor (Figure S7). This was more pronounced under HTS conditions, elevated temperatures, and higher flow rates, where the CO conversion was also higher. This can be explained considering that metallic monoliths present high thermal conductivities and improved heat transfer characteristics compared to, for example, ceramic monoliths [15,28,29]. This advantage, combined with the easy fabrication and superior mechanical shock resistance of metallic monoliths, makes them suitable for practical applications.

The results presented in Figure 6a show that the Pt/TiO<sub>2</sub>(Ca)-MM catalyst has the potential to be used in a single-step, medium temperature shift reactor operating in the 300–350 °C range to reduce the CO content in the reformed gas to ca. 1%, which can be tolerated by preferential oxidation (PROX) catalysts [1]. Replacing the two HTS and LTS reactors by a single medium-temperature reactor is highly desirable, especially for small-scale and mobile applications where volume/weight and ruggedness become more important [30,31]. The WGS performance of this catalyst may be further improved by optimizing the catalyst loading, washcoat thickness, and cell density of the monolithic substrate as well as by using novel multi-shelled and core-shell nano/microstructured catalyst formulations [32,33], the study of which was beyond the scope of the present work and may be the subject of our future investigation.

### 3. Materials and Methods

#### 3.1. Catalyst Preparation

##### 3.1.1. Powdered Catalysts

Titanium dioxide supports promoted with small amounts of alkali or alkaline earth metals, denoted as  $\text{TiO}_2(\text{X})$  ( $\text{X} = \text{Na}, \text{Cs}, \text{Ca}, \text{Sr}$ ), were prepared following the procedures described in detail elsewhere [18–20]. In a typical synthesis, a pre-weighed amount of commercial  $\text{TiO}_2$  powder (Degussa P25) is added under continuous stirring in an aqueous solution containing the appropriate amount of the corresponding promoter salt, namely,  $\text{NaNO}_3$ ,  $\text{CsNO}_3$ ,  $\text{Sr}(\text{NO}_3)_2$ , or  $\text{CaO}$  (Alfa Aesar), the latter diluted in  $\text{HNO}_3$  at  $\text{pH} = 1$ . The resulting dispersion was heated at  $70\text{ }^\circ\text{C}$  and maintained at that temperature until nearly all the water had evaporated. The solid residue was dried overnight at  $110\text{ }^\circ\text{C}$  and then calcined in stagnant air at  $600\text{ }^\circ\text{C}$  for 5 h. The nominal contents (wt.%) of the promoters in the samples thus prepared were 0.06% for Na, 0.34% for Cs, 2.0% for CaO, and 1.0% for SrO (Table 1) and were selected based on their optimal concentrations derived in our previous studies [18–20].

Platinum catalysts dispersed on the pristine  $\text{TiO}_2$  and the promoted  $\text{TiO}_2(\text{X})$  supports were prepared via the wet impregnation method [7]. Briefly, a pre-weighed amount of the respective support was added under continuous stirring into an aqueous solution of  $(\text{NH}_3)_2\text{Pt}(\text{NO}_2)_2$  (Alfa Aesar) followed by heating at  $70\text{ }^\circ\text{C}$  to evaporate water, drying at  $110\text{ }^\circ\text{C}$  overnight, and subsequent reduction under flowing  $\text{H}_2$  at  $300\text{ }^\circ\text{C}$  for 2 h. The nominal Pt loading of the catalysts thus prepared was 0.5 wt.%.

The bimetallic  $(\text{Pt}-\text{M})/\text{TiO}_2$  catalysts ( $\text{M} = \text{Fe}, \text{Cu}, \text{Cr}, \text{Ru}$ ) were synthesized by employing a two-step procedure. In the first step, the metal M (0.5 or 5.0 wt.%) was first deposited on the support following the impregnation of  $\text{TiO}_2$  (P25) in an aqueous solution of the corresponding metal precursor salt, namely,  $(\text{Fe}(\text{NO}_3)_3 \cdot 9\text{H}_2\text{O})$ ,  $(\text{Cu}(\text{NO}_3)_2 \cdot 3\text{H}_2\text{O})$ ,  $(\text{Cr}(\text{NO}_3)_3 \cdot 9\text{H}_2\text{O})$ , or  $(\text{Ru}(\text{NO})(\text{NO}_3)_3)$  (Alfa Aesar). This was followed by the evaporation of water at  $70\text{ }^\circ\text{C}$ , drying overnight at  $110\text{ }^\circ\text{C}$ , and subsequent calcination in stagnant air at  $300\text{ }^\circ\text{C}$  for 3 h. Platinum (0.5 wt.%) was then added onto the resulting materials following the procedure described above.

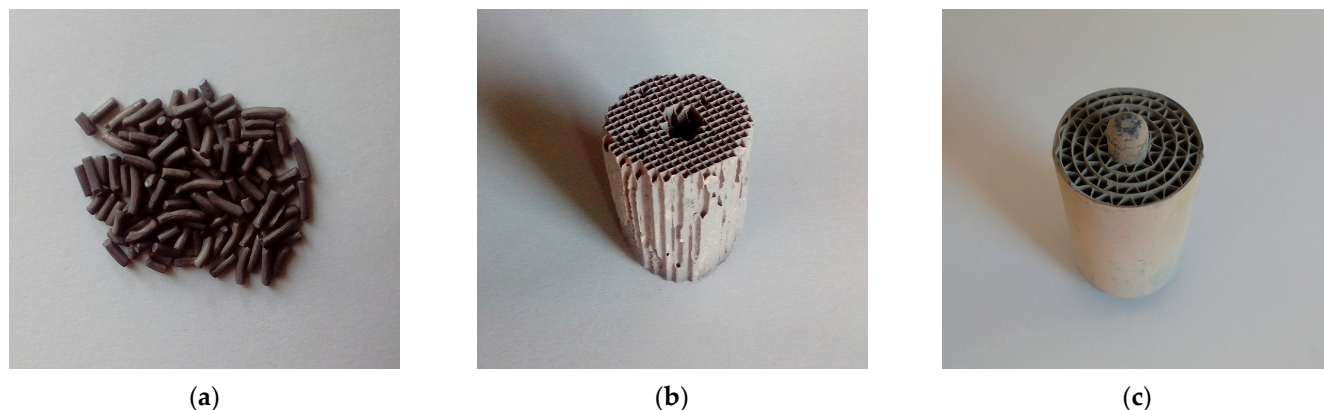
##### 3.1.2. Structured Catalysts

The best performing  $\text{Pt}/\text{TiO}_2(\text{Ca})$  catalyst was prepared in the form of pellets as well as in the form of coating on ceramic and metallic monoliths (Figure 7). Two pellet catalyst samples with different Pt loadings (0.5 and 1.0 wt.%) were synthesized as follows: An appropriate amount of  $\text{CaO}$  was diluted in an aqueous solution of  $\text{HNO}_3$  ( $\text{pH} = 1$ ) in a BUCHI beaker followed by the addition of  $\text{TiO}_2$  pellets (Aerolyst 7711, 1/16"). The beaker was adjusted in a Rotavapor to remove water under vacuum at  $40\text{ }^\circ\text{C}$ . The pellets were then dried at  $110\text{ }^\circ\text{C}$  overnight and subsequently calcined at  $600\text{ }^\circ\text{C}$  for 5 h in stagnant air. The  $\text{CaO}$ -promoted  $\text{TiO}_2$  pellets thus obtained were added in an aqueous  $(\text{NH}_3)_2\text{Pt}(\text{NO}_2)_2$  solution contained in a BUCHI beaker adjusted to a Rotavapor. After the removal of water under vacuum at  $40\text{ }^\circ\text{C}$ , the pellets were dried overnight at  $110\text{ }^\circ\text{C}$  and finally reduced under flowing  $\text{H}_2$  at  $300\text{ }^\circ\text{C}$  for 2 h.

The commercial catalyst used as the reference was supplied by Johnson Matthey and was in the form of 1/16" pellets (Product name: 205 W21, 10876, UK). No detailed information is available regarding the composition of this catalyst except that it contains a mixture of  $\text{Al}_2\text{O}_3$  ( $\geq 90\%$ ) and  $\text{CeZrO}_4$  ( $\leq 10\%$ ).

The ceramic monolithic catalyst was prepared by coating the  $\text{Pt}/\text{TiO}_2(\text{Ca})$  powder (see Section 3.1.1) in the channels of a cordierite monolith (400 cell per square inch, cpsi) of a cylindrical shape with a diameter of 2.4 cm and length of 3.6 cm. A hole was drilled at the center of the monolith (Figure 7b) to place a 1/16" quartz tube with a K-type thermocouple running throughout it to allow the temperature profile along the monolith to be monitored during the catalytic performance tests. The catalyst sample was first pulverized in a mortar and the resulting powder ( $d < 63\text{ }\mu\text{m}$ ) was suspended under continuous stirring in triple-distilled water at a concentration of 0.33 g/mL. The monolith was then immersed in the

catalyst suspension, blown with compressed air to remove the excess slurry left in the channels, dried at 110 °C overnight, and subsequently calcined at 300 °C for 3 h in stagnant air. The amount of catalyst loaded was determined by weighing the monolith before and after the catalyst deposition. This procedure (immersion, drying, calcination, weighing) was repeated until the desired amount of catalyst (1.8 g) was deposited in the channels of the monolith.



**Figure 7.** Photographs of the structured catalysts: (a) 1/16" pellets; (b) ceramic monolith; (c) metallic monolith.

A metallic monolith (custom made by rolling a corrugated Fe-Cr-Al alloy film, 300 cpsi) with the same dimensions as the ceramic monolith (diameter: 2.4 cm; length: 3.6 cm) was coated with the Pt/TiO<sub>2</sub>(Ca) catalyst using the same technique. The total amount of catalyst deposited was 1.8 g.

### 3.2. Physicochemical Characterization

The specific surface areas (SSAs) of the synthesized catalysts were determined by employing the N<sub>2</sub> physisorption method at the temperature of liquid nitrogen (−196 °C) (BET method) on a Micromeritics (Gemini III 2375) instrument. Powder X-ray diffraction patterns were obtained in the 2θ range between 20° and 80° (scan rate 0.01° s<sup>−1</sup>) on a Bruker D8 Advance (Cu Kα) apparatus operated at 40 kV and 40 mA, and were analyzed using JCPDS data files. The anatase content of TiO<sub>2</sub> in the catalyst samples was estimated from the following equation [7].

$$x_A = [1 + 1.26(I_R/I_A)]^{-1} \quad (4)$$

where  $I_A$  and  $I_R$  are the integral intensities of the anatase (101) and rutile (110) reflections, respectively.

Hydrogen chemisorption measurements were performed at 25 °C on a modified Fisons Instruments (Sorptomatic 1900) apparatus and the results were used to estimate the Pt dispersion and average crystallite size. Details of the experimental procedure and methods employed can be found elsewhere [7].

Transmission electron microscopy (TEM) images were recorded on a JEOL JEM-2100 apparatus (JEOL, Tokyo, Japan) operated at 200 kV (point resolution 0.23 nm) by means of an Erlangshen CCD Camera (Gatan Model 782 ES500W, Pleasanton, CA 94588, United States). SEM images were obtained using a JEOL 6300 scanning electron microscope (Akishima, Tokyo, Japan) equipped with an energy dispersive spectrometer (EDS, ISIS Link 300, Oxford Instruments, UK).

### 3.3. Catalytic Performance Tests

The experimental setup employed for the investigation of the WGS activity of the synthesized catalysts consisted of a flow system, a down-flow reactor, and an analysis

system. The flow system was equipped with mass flow controllers to adjust the flow of gases (He, CO, CO<sub>2</sub>, H<sub>2</sub>) and an HPLC pump (Marathon II) for feeding H<sub>2</sub>O. Water was pumped into an evaporator operating at 170 °C and then mixed with the gas coming from the mass flow controllers. The resulting mixture was fed into the reactor through insulated stainless-steel tubing heated at 170 °C. The reactor consisted of a quartz tube (6 mm OD) with an expansion in its upper part (12 mm in the case of powdered samples; 20 mm in the case of pellets and 32 mm in the case of monoliths) where the catalyst sample was placed. The monoliths were wrapped with quartz wool to avoid by-pass flow. The oven temperature was controlled using a K-type thermocouple located between the oven walls and the reactor. The temperature profile at the catalyst bed was measured with a mobile K-type thermocouple placed in a thin quartz tube (1/16") running through the reactor. The reactor effluent passed through a condenser to trap unreacted H<sub>2</sub>O and was then introduced to the analysis system, which consisted of a gas chromatograph (Shimadzu GC 14B) operating with He as the carrier gas, equipped with two columns (Porapak Q and Carbosieve) and two detectors (TCD and FID). Porapak Q was used for the separation of CH<sub>4</sub>, C<sub>2</sub>H<sub>4</sub>, C<sub>2</sub>H<sub>6</sub>, C<sub>3</sub>H<sub>6</sub>, and C<sub>3</sub>H<sub>8</sub> whereas Carbosieve was used for the separation of CO, CO<sub>2</sub>, and CH<sub>4</sub>.

Catalytic performance tests were performed at near atmospheric pressure in the temperature range of 170–450 °C using two different feed compositions: one corresponding to the HTS conditions (9.7%CO, 38.7%H<sub>2</sub>O, 44.8%H<sub>2</sub>, 6.8%CO<sub>2</sub>) and one corresponding to the LTS conditions (1.6%CO, 29.9%H<sub>2</sub>O, 52.2%H<sub>2</sub>, 16.3%CO<sub>2</sub>), which are relevant to practical applications [1]. Unless otherwise indicated, the total flow rate was 220 cm<sup>3</sup> min<sup>−1</sup>. The amount of catalyst used for the powdered samples (0.18 < *d* < 0.25 mm) was 750 mg, which corresponds to a space velocity of ca. 10,000 h<sup>−1</sup>. For the structured samples, the amount of catalyst in the form of pellets or coating on the monoliths was 1.8 g (W/F = 0.5 g s cm<sup>−3</sup>). In a typical experiment, the catalyst was heated under He flow at 300 °C where the sample was in situ reduced under H<sub>2</sub> flow (60 cm<sup>3</sup> min<sup>−1</sup>) for 1 h. The temperature was then increased to 450 °C under He flow and the feed was switched to the reaction mixture. Measurements were recorded after conditioning of the catalyst for 1 h-on-stream. The reaction temperature was then stepwise decreased under the flowing reaction mixture and similar measurements were obtained. The CO conversion (*X*<sub>CO</sub>) was calculated by employing the following equation:

$$X_{\text{CO}} = \frac{[\text{CO}]^{\text{in}} - [\text{CO}]^{\text{out}}}{[\text{CO}]^{\text{in}}} \times 100 \quad (5)$$

where  $[\text{CO}]^{\text{in}}$  and  $[\text{CO}]^{\text{out}}$  are the inlet and outlet concentrations of CO, respectively. The yield of methane (*y*<sub>CH<sub>4</sub></sub>), which was formed at elevated temperatures via the methanation of CO (Equation (2)) and/or CO<sub>2</sub> (Equation (3)), was estimated using the equation:

$$y_{\text{CH}_4} = \frac{[\text{CH}_4]^{\text{out}}}{[\text{CO}]^{\text{in}} + [\text{CO}_2]^{\text{in}}} \times 100 \quad (6)$$

where  $[\text{CH}_4]^{\text{out}}$  is the outlet concentration of CH<sub>4</sub>, and  $[\text{CO}]^{\text{in}}$  and  $[\text{CO}_2]^{\text{in}}$  are the inlet concentrations of CO and CO<sub>2</sub>, respectively. All values reported are the averages of at least three measurements and correspond to the temperature measured at the outlet of the catalyst bed.

#### 4. Conclusions

The WGS performance of 0.5%Pt/TiO<sub>2</sub>(X) (X = Na, Cs, Ca, Sr) and (0.5%Pt-M)/TiO<sub>2</sub> (M = Fe, Cu, Cr, Ru) catalysts in powder form was investigated under realistic reaction conditions. The best results were obtained for the 0.5%Pt/TiO<sub>2</sub>(Ca) catalyst, which exhibited high activity and selectivity toward H<sub>2</sub> under both HTS and LTS reaction conditions. The catalytic performance of the optimized catalyst in pellet form was comparable to

that of a commercial WGS pellet catalyst provided by JM and was further enhanced by increasing the Pt content from 0.5 to 1.0 wt.%. The results obtained using a ceramic and a metallic monolithic catalyst coated with 0.5%Pt/TiO<sub>2</sub>(Ca) showed that the latter exhibited superior performance and operated under nearly isothermal conditions with the minimal production of undesired methane. The CO conversion curve could be shifted toward lower temperatures by decreasing the space velocity, demonstrating the feasibility of the metallic monolithic catalyst for small-scale and mobile applications and its potential use in a single-step, medium temperature shift reactor operating in the 300–350 °C range.

**Supplementary Materials:** The following supporting information can be downloaded at: <https://www.mdpi.com/article/10.3390/catal13020372/s1>, Figure S1: (a) SEM image of the as prepared Pt/TiO<sub>2</sub> catalyst, and EDS mapping results showing the distribution of (b) Pt, (c) O and (d) Ti elements; Figure S2: (a) SEM image of the as prepared TiO<sub>2</sub>(Ca) support, and EDS mapping results showing the distribution of (b) Ca, (c) O and (d) Ti elements; Figure S3: (a) SEM image of the Pt/TiO<sub>2</sub>(Ca) catalyst and (b) EDS mapping results showing the distribution of Pt element; Figure S4: Effects of the metal content on the performance of bimetallic (0.5%Pt- $x$ %M)/TiO<sub>2</sub> catalysts ( $x$  = 0.5 or 5.0; M = Fe or Cr) under (A) HTS and (B) LTS conditions. Experimental conditions same as in Figure 3; Figure S5: Effects of total flow rate on the performance of Pt/TiO<sub>2</sub>(Ca) catalysts coated on the channels of the ceramic monolith: (A) Conversion of CO and (B) yield of CH<sub>4</sub> under HTS conditions. (C) Conversion of CO under LTS conditions. Other experimental conditions same as in Figure 5; Figure S6: Temperature profile along the Pt/TiO<sub>2</sub>(Ca)-coated metallic monolith (inlet at  $L$  = 0) at the indicated total flow rates under the (a) HTS and (b) LTS reaction conditions shown in Figure 6; Figure S7: Temperature profile along the Pt/TiO<sub>2</sub>(Ca)-coated ceramic monolith (inlet at  $L$  = 0) at the indicated total flow rates under the (a) HTS and (b) LTS reaction conditions shown in Figure 6.

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