

Special Issue Reprint

Environmental Catalysis and Air Pollution Control

Edited by Zhiming Liu and Chi He

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Environmental Catalysis and Air Pollution Control

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Guest Editors

Zhiming Liu Chi He



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Editorial

Advances and Challenges in Environmental Catalysis and Air Pollution Control

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Air quality is closely related to human health, and the control of air pollution through environmental catalysis has garnered increasing attention. This Special Issue features one review article and ten research papers, each addressing critical aspects of environmental catalysis and air pollution control. The review article highlights the application and future potential of stable isotope techniques in tracing the sources of atmospheric NOx and nitrate. Among the research contributions, three papers focus on the catalytic removal of volatile organic compounds (VOCs), including formaldehyde, toluene, and 1,2-dichloroethane. Two papers explore the catalytic oxidation of NO and passive NOx adsorption (PNA), while three others investigate CO oxidation, soot oxidation, and SO₂ adsorption. Additionally, the simultaneous removal of CO and toluene, as well as NOx and VOCs, is reported in detail.

Beyond traditional catalytic methods, this issue also delves into innovative approaches such as the integration of catalysis with plasma technology, and the combination of catalysis with ozone (O_3) . These studies collectively address a wide range of catalysts and catalytic techniques, offering insights into their design, efficiency, and application in air pollution control.

This Special Issue aims to illuminate recent advancements and emerging challenges in the field of environmental catalysis and air pollution control. We hope that the findings presented here will inspire the development of more active, selective, and durable environmental catalysts. Furthermore, we anticipate that the integration of catalysis with other physical methods will significantly enhance the efficiency of air pollution control, paving the way for a cleaner and healthier environment.

Conflicts of Interest: The authors declare no conflicts of interest.

List of Contributions:

- Zhen, S.; Luo, M.; Shao, Y.; Xu, D.; Ma, L. Application of Stable Isotope Techniques in Tracing the Sources of Atmospheric NOx and Nitrate. *Processes* 2022, 10, 2549. https://doi.org/10.339 0/pr10122549.
- Huang, Y.; Fang, S.; Tian, M.; Jiang, Z.; Wu, Y.; He, C. Chlorine-Resistant Hollow Nanosphere-Like VOx/CeO₂ Catalysts for Highly Selective and Stable Destruction of 1,2-Dichloroethane: Byproduct Inhibition and Reaction Mechanism. *Processes* 2021, 9, 119. https://doi.org/10.3390/ pr9010119.
- 3. Peng, P.; Li, J.; Mo, S.; Zhang, Q.; Shen, T.; Xie, Q. Bimetallic Pt-Co Nanoparticle Deposited on Alumina for Simultaneous CO and Toluene Oxidation in the Presence of Moisture. *Processes* **2021**, *9*, 230. https://doi.org/10.3390/pr9020230.

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- 4. Wang, H.; Hao, R.; Gao, M.; Zhang, Z.; Hao, Z. High Temperature Adsorption of SO₂ on Mixed Oxides Derived from CaAl Hydrotalcite-Like Compounds. *Processes* **2021**, *9*, 325. https://doi.org/10.3390/pr9020325.
- Zhang, C.; Yu, D.; Peng, C.; Wang, L.; Fan, X.; Yu, X.; Zhao, Z. Preparation of K Modified Three-Dimensionally Ordered Macroporous MnCeOx/Ti_{0.7}Si_{0.3}O₂ Catalysts and Their Catalytic Performance for Soot Combustion. *Processes* 2021, 9, 1149. https://doi.org/10.3390/pr9071149.
- 6. Luo, Y.; Li, Y.; Wang, C.; Wang, J.; Liu, W.; Peng, H.; Wu, D. Highly Active CuO/KCC-1 Catalysts for Low-Temperature CO Oxidation. *Processes* **2022**, *10*, 145. https://doi.org/10.3390/pr10010145.
- 7. Fan, C.; Mi, J.; Wu, Q.; Chen, J.; Li, J. Deactivation of Pd/SSZ-13 by Potassium and Water for Passive NOx Adsorption. *Processes* **2022**, *10*, 222. https://doi.org/10.3390/pr10020222.
- 8. Shen, H.; Tang, Z.; Xiao, X.; Wu, H.; Zhou, H.; Fang, P.; Zhu, D.; Ge, J. Catalytic Oxidation of NO by Ozone over Mn-Ce/Al₂O₃/TiO₂ Catalyst. *Processes* **2022**, *10*, 1946. https://doi.org/10.3 390/pr10101946.
- 9. An, C.; Jiang, X.; Hong, W.; Sun, Y.; Zhu, T. To Promote the Catalytic Ozonation of Typical VOCs by Modifying NiO with Cetyltrimethylammonium Bromide. *Processes* **2023**, *11*, 1893. https://doi.org/10.3390/pr11071893.
- 10. Chen, Y.; Zhao, S.; Gao, F.; Yu, Q.; Zhou, Y.; Tang, X.; Yi, H. The Promoting Effect of Metal Vacancy on CoAl Hydrotalcite-Derived Oxides for the Catalytic Oxidation of Formaldehyde. *Processes* **2023**, *11*, 2154. https://doi.org/10.3390/pr11072154.
- Li, J.; Zhao, R.; Sun, M.; Shi, Q.; Zhao, M.; Zhang, J.; Liu, Y.; Jia, J. Collaborative Effect of In-Plasma Catalysis with Sequential Na₂SO₃ Wet Scrubbing on Co-Elimination of NOx and VOCs from Simulated Sinter Flue Gas. *Processes* 2023, 11, 2916. https://doi.org/10.3390/pr11102916.

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Article

Chlorine-Resistant Hollow Nanosphere-Like VO_x/CeO₂ Catalysts for Highly Selective and Stable Destruction of 1,2-Dichloroethane: Byproduct Inhibition and Reaction Mechanism

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Abstract: Developing economical and robust catalysts for the highly selective and stable destruction of chlorinated volatile organic compounds (CVOCs) is a great challenge. Here, hollow nanosphere-like VO_x/CeO_2 catalysts with different V/Ce molar ratios were fabricated and adopted for the destruction of1,2–dichloroethane (1,2–DCE). The $V_{0.05}Ce$ catalyst possessed superior catalytic activity, reaction selectivity, and chlorine resistance owing to a large number of oxygen vacancies, excellent low-temperature redox ability, and chemically adsorbed oxygen (O $^-$ and O $_2^-$) species mobility. Typical chlorinated byproducts (CHCl $_3$, CCl $_4$, C $_2$ HCl $_3$, and C $_2$ H $_3$ Cl $_3$) derived from the cleavage of C–Cl and C–C bonds of 1,2–DCE were detected, which could be effectively inhibited by the abundant acid sites and the strong interactions of VO $_x$ species with CeO $_2$. The presence of water vapor benefited the activation and deep destruction of 1,2–DCE over V $_{0.05}$ Ce owing to the efficient removal of Cl species from the catalyst surface.

Keywords: catalytic destruction; 1,2–dichloroethane; VO_x/CeO₂; chlorinated byproduct inhibition; reaction mechanism

1. Introduction

Chlorinated volatile organic compounds (CVOCs) mainly originate from industrial processes and result in great hazards to public health and the natural environment because of their long durability, poor reactivity, and high toxicity [1–3]. So far, several methods including absorption, photocatalytic degradation, catalytic oxidation, and biological processes have been used for CVOC elimination [4]. Among them, catalytic oxidation has been identified as the most efficient treatment measure due to its significant energy saving, adjustable reaction selectivity, low operation temperature, and green environment effect [5,6]. Up to now, various catalysts including transition metal oxides, zeolites/modified zeolites, and supported noble metals have been studied for CVOC destruction. Supported noble—metal catalysts exhibit outstanding catalytic performance, whereas their widespread application is greatly limited by their susceptibility to chlorine poisoning, the formation of chlorinated byproducts, and their high cost [7,8]. Although zeolites/modified zeolites exhibit good catalytic performance, they more easily suffer deactivation due to chlorine poisoning and coke deposition during the oxidation process [9,10].

Comparatively, transition metal oxides (e.g., Cr₂O₃, MnO_x, and V₂O₅) are considered as a category of desired candidates to destroy CVOCs owing to their considerable catalytic performance, high availability, and low cost [6,11–13]. For example, VO_x catalysts are usually used for CVOC destruction due to their excellent resistance to chlorine poisoning [13,14]. Recently, CeO₂ catalysts attracted much attention for CVOC destruction attributed to their higher oxygen mobility, superior redox ability, and abundant oxygen vacancies. However, CeO₂ catalysts are easily deactivated because of the strong adsorption of Cl species onto their active sites. Generally, the introduction of transition metal oxides is advantageous for promoting activity and stability. Dai et al. [15] presented that a 6 wt.% VO_x/CeO₂ catalyst displayed superior catalytic activity for 1,2–dichloroethane (1,2–DCE) degradation owing to the strong interaction of VO_x species with CeO₂ and the high valence of VO_x. It was observed that the stability of VO_x/CeO₂ materials was significantly improved, attributed to the VO_x species preventing Cl species from exchanging the surface lattice oxygen of CeO₂ during chlorobenzene destruction [16]. Although VO_x/CeO₂ catalysts have made certain progress in CVOC destruction, there are many issues that should be further solved and clarified; for instance, the role of VO_x and/or the synergistic effect of VO_x/CeO₂ in the production of chlorinated byproducts requires an in-depth study, as well as the effect of water vapor on catalytic performance and chlorinated byproduct distributions over VO_x/CeO₂ catalysts. It was reported that CeO₂ material with a hollow nanosphere structure (CeO₂–HS) had abundant oxygen vacancies and a large surface area, which is favorable for VOC oxidation [17]. Meanwhile, CeO₂-HS with high stability and water resistance is a potential carrier for fabricating effective CVOC oxidation materials.

Herein, hollow nanosphere–like VOx/CeO $_2$ catalysts with well–dispersed VO $_x$ species, abundant surface acid sites, and outstanding low–temperature reducibility were fabricated via a simple wetness impregnation process. The structural properties, reducibility, oxygen mobility, and acidity of prepared materials were deeply analyzed using various techniques such as field emission scanning electron microscopy (FE–SEM), high-resolution transmission electron microscopy (HR–TEM), the hydrogen temperature programmed reduction (H $_2$ –TPR), X-ray photoelectron spectroscopy (XPS), the temperature programmed desorption of O $_2$ (O $_2$ –TPD) and the temperature programmed desorption of NH $_3$ (NH $_3$ –TPD). Catalytic activity and stability, yields of CO and CO $_2$, and the distribution of chlorinated byproducts over prepared materials were studied in detail. In particular, the influence of water vapor on catalytic performance and the vital factors inhibiting the generation of chlorinated byproducts were explored. Accordingly, the destruction mechanism of 1,2–DCE over VO $_x$ /CeO $_2$ samples was further proposed.

2. Materials and Methods

2.1. Catalyst Preparation

Hollow nanosphere–like CeO $_2$ was prepared using a hydrothermal route [18]. Specifically, 5.0 g of Ce(NO $_3$) $_3\cdot6H_2O$ and 5 mL of CH $_3$ COOH (36 wt.%) were added into 150 mL of a mixed solution (ethylene glycol (100 mL) and deionized water (50 mL)) under vigorous stirring for 0.5 h. After that, 4.0 g of polyvinyl pyrrolidone (PVP; K–30) was added, with continued stirring at 60 °C for 1 h. The solution was then placed into a 200 mL Teflon–lined stainless–steel autoclave and kept at 180 °C for 6 h. Finally, the precursor was centrifuged, washed, dried, and calcined at 500 °C for 4 h in air.

Hollow nanosphere–like VO_x/CeO_2 materials were prepared via a wetness impregnation approach. Typically, 3.0 g of the above–prepared CeO_2 was dispersed into 150 mL of deionized water, and an appropriate amount of NH_4VO_3 with the molar ratio of nNH_4VO_3 : $nCeO_2 = 0.025:1$, 0.05:1, 0.1:1, or 0.2:1 was then mixed in the above solution. Subsequently, the corresponding molar amount of oxalic acid with the molar ratio of nNH_4VO_3 :noxalic acid = 1:2 was added to the suspension of CeO_2 . After that, the solution was vigorously stirred at 80 °C until excess deionized water was completely evaporated.

The final products were treated under the same conditions as for CeO_2 preparation. The obtained materials were designated as $V_{0.025}Ce$, $V_{0.05}Ce$, $V_{0.1}Ce$, and $V_{0.2}Ce$, respectively.

In comparison, VO_x was also prepared using a hydrothermal method [19]. The prepared powder was also treated as in the CeO_2 preparation process to obtain the bulk VO_x . Additionally, commercial CeO_2 (Aladdin Reagent Co., Ltd., Shanghai, China, 99.5%) named CeO_2 –C was also investigated for 1,2–DCE oxidation.

2.2. Catalyst Characterizations

The prepared materials were characterized by X-ray diffraction (XRD), Fourier transform infrared spectra (FT–IR), low–temperature N_2 adsorption/desorption, FE–SEM, HR–TEM, XPS, H_2 –TPR, O_2 –TPD, NH_3 –TPD, FT–IR spectra of NH_3 adsorption (NH_3 –IR), and in situ diffuse reflectance infrared spectroscopy (DRIFTS). The detailed information can be found in the Supplementary Materials.

2.3. Catalytic Activity

The 1,2–DCE destruction experiments were employed in a continuous–flow fixed–bed quartz tube reactor with 10.0 mm inner diameter. Typically, the prepared catalyst (500 mg; 40–60 mesh) was loaded into the isothermal region of the tube reactor. The reactant mixture containing 1000 ppm of 1,2–DCE, 79% N₂, and 21% O₂, with a total flow rate of 250 mL·min⁻¹ (gas hourly space velocity (GHSV) = 30,000 mL·g⁻¹·h⁻¹) was obtained through the reactor. The concentrations of 1,2–DCE, chlorinated byproducts, and CO_x (CO and CO₂) were measured using an online gas chromatograph (GC9890, China) with Electron Capture Detector (ECD). Furthermore, an online Cl₂ and HCl detector (PN–2000, China) was used to analyze the concentrations of Cl₂ and HCl.

The 1,2–DCE conversion $(X_{1,2-DCE})$ was calculated using Equation (1).

$$X_{1,2\text{-DCE}} = \frac{C_{\text{in}} - C_{\text{out}}}{C_{\text{in}}} \times 100\%,$$
 (1)

where C_{in} and C_{out} refer to the inlet and outlet 1,2–DCE concentrations, respectively.

The CO and CO_2 yields (Y_{CO} and Y_{CO2}) were calculated using Equations (2) and (3), respectively.

$$Y_{\rm CO} = \frac{C_{\rm CO}}{2C_{\rm in}} \times 100\%,$$
 (2)

$$Y_{\text{CO}_2} = \frac{C_{\text{CO}_2}}{2C_{\text{in}}} \times 100\%,\tag{3}$$

where C_{CO} and C_{CO2} refer to the outlet concentrations of CO and CO₂, respectively.

The stability of the prepared catalysts was evaluated at different temperatures corresponding to 90% conversion of 1,2–DCE under the same conditions as the activity experiments. Moreover, the stability of the highest–activity $V_{0.05}$ Ce sample for 1,2–DCE oxidation was studied in the absence and presence of water vapor. Different concentrations of water vapor (1, 2, and 5 vol.%) were injected into the reactant mixture containing 1000 ppm of 1,2–DCE using an automatic sample injector.

3. Results

3.1. Structural and Textural Properties

Figure 1a and Figure S1 (Supplementary Materials) exhibit the XRD patterns of prepared catalysts. The peaks located at 28.4° , 33.1° , 47.4° , 56.3° , 59.1° , 69.6° , 76.6° , and 79.2° were attributed to the (111), (200), (220), (311), (222), (400), (331), and (420) crystal planes of CeO₂, respectively [20]. The characteristic peaks of VO_x (V₂O₅) were located at 15.3° , 20.2° , 21.7° , 26.1° , 31.0° , 32.4° , 34.3° , and 47.4° [21]. Notably, no characteristic peaks corresponding to VO_x and CeVO₄ species ($2\theta = 24.0^{\circ}$ and 32.5°) could be detected over VO_x/CeO₂ catalysts, suggesting that VO_x species were highly dispersed on the surface or in the form of a solid solution [15,22]. The position of the main peak of CeO₂ (ca. 28.4°)

was well maintained over VO_x/CeO_2 materials, suggesting that VO_x neither altered the CeO_2 crystallization nor was incorporated into the CeO_2 crystalline phase, forming a solid solution [15,23]. Hence, VO_x species existed in a highly dispersed form.

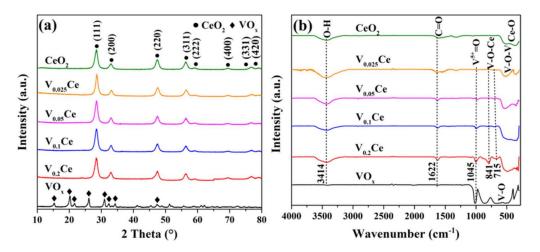


Figure 1. (a) X-ray diffraction (XRD) profiles and (b) Fourier transform infrared spectra (FT–IR) of prepared catalysts.

As shown in Figure 1b, the broad IR peaks over all catalysts between 3500 and $3000~\rm cm^{-1}$ corresponded to the stretching vibration of surface hydroxyl groups, while the peaks presented at $1622~\rm cm^{-1}$ were indexed as C=O stretching vibration [24]. For CeO₂, the peaks located at wavenumbers lower than $1000~\rm cm^{-1}$ were associated with the vibration of Ce–O [25]. For VO_x, the peaks located in the 1100– $400~\rm cm^{-1}$ region were related to the V–O stretching vibration [26]. The peaks centered at $1045~\rm and~841~\rm cm^{-1}$ were consistent with the symmetric stretching vibration of V⁵⁺=O and stretching vibration of O–(V)₃, respectively. It can be observed that V⁵⁺=O vibration located at $1045~\rm cm^{-1}$ was detected over VO_x and VO_x/CeO₂ catalysts [26]. The two peaks over VO_x/CeO₂ catalysts at 715 and 841 cm⁻¹ could be regarded as the V–O–Ce modes [27]. In addition, the symmetric and antisymmetric stretching vibration of V–O–V could be detected in the 700– $400~\rm cm^{-1}$ range over VO_x and VO_x/CeO₂ catalysts [26].

FE-SEM images of prepared catalysts are shown in Figure 2a–x. CeO₂ exhibited a regular nanosphere-like morphology with different diameters (ca. 245-600 nm), as displayed in Figure 2a,b. The V_{0.05}Ce catalyst was made up of nanospheres with a diameter of ca. 100–200 nm (Figure 2e,f). Compared with the $V_{0.05}$ Ce catalyst, $V_{0.025}$ Ce (Figure 2c,d), V_{0.1}Ce (Figure 2g,h) and V_{0.2}Ce catalysts (Figure 2i,j) consisted of larger nanospherelike particles with a diameter of ca. 300–400 nm. Moreover, VO_x showed an irregular nanosphere-like morphology with size varying from ca. 200 to 300 nm (Figure 2k,l). Figure 2m-x and Figure S2 (Supplementary Materials) exhibit the transmission electron microscope (TEM) and high-angle annular dark-field imaging in scanning transmission electron microscopy (HAADF-STEM) images of prepared catalysts. It was revealed that CeO₂ and VO_x/CeO₂ catalysts possessed a well-defined hollow nanosphere-like structure with diameter in the range of ca. 200-400 nm, in agreement with the FE-SEM results. The results exhibited that VO_x species were highly dispersed and did not change CeO₂ morphology [28]. VO_x had an irregular nanosphere–like morphology with a lattice spacing of 0.34 nm, ascribed to the (101) plane of V₂O₅ (Figure 2w,x) [29]. The measured lattice distances of 0.31, 0.27, and 0.19 nm were ascribed to the (111), (200), and (220) lattice planes of CeO₂ nanospheres (JCPDS #34–0394), respectively (Figure 2n). Figure 2p,r,t and Figure S2 (Supplementary Materials) show that V_{0.025}Ce, V_{0.05}Ce, V_{0.1}Ce, and CeO₂–C catalysts possessed the (200) and (111) lattice planes of CeO₂ with lattice spacings of 0.27 and 0.31 nm, respectively. For $V_{0.2}$ Ce, the lattice spacings of 0.27 and 0.19 nm were associated with the (200) and (220) crystal planes of CeO₂, respectively (Figure 2v). No VO_x species on the VO_x/CeO_2 catalysts could be detected in HAADF–STEM images (Figure 2p,r,t,v), which could be attributed to the rough surface of CeO_2 or the generation of VO_x films from the layer structure [15].

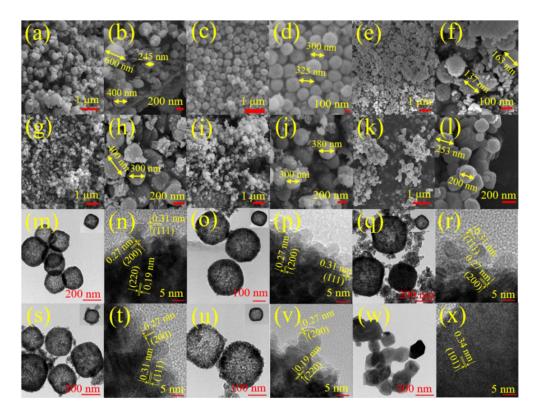


Figure 2. Field emission scanning electron microscopy (FE–SEM) images of (**a**,**b**) CeO₂, (**c**,**d**) $V_{0.025}$ Ce, (**e**,**f**) $V_{0.05}$ Ce, (**g**,**h**) $V_{0.1}$ Ce, (**i**,**j**) $V_{0.2}$ Ce, and (**k**,**l**) $V_{0.2}$ Ce, igh-resolution transmission electron microscopy (HR–TEM) patterns of (**m**,**n**) CeO₂, (**o**,**p**) $V_{0.025}$ Ce, (**q**,**r**) $V_{0.05}$ Ce, (**s**,**t**) $V_{0.1}$ Ce, (**u**,**v**) $V_{0.2}$ Ce, and (**w**,**x**) $V_{0.2}$ Ce,

N₂ adsorption/desorption isotherms of the prepared materials are presented in Figure 3. CeO₂ and VO_x/CeO₂ catalysts showed a type II isotherm curve with H3-type hysteresis loops at the relative pressure (P/P_0) range of 0.7–1.0 (Figure 3a), indicating that meso- and macropore structures co-existed in CeO₂ and VO_x/CeO₂ catalysts [30,31]. VO_x exhibited a type III isotherm curve with H3-type hysteresis loops ($P/P_0 = 0.9$ -1.0), illustrating that the presence of textural pores facilitated the filling of interparticle spaces. It was demonstrated that the pore size distribution of prepared catalysts was centered at approximately 25.4, 11.7, 19.4, 37.6, 27.0, and 17.4 nm, respectively (Figure 3b), indicating that all catalysts possessed a large number of mesopores. The pore size distribution of materials in the 100-500 nm region could be attributed to the existence of a macroporous structure. The specific surface area, average pore diameter, and pore volume of materials are documented in Table 1, and the average pore diameter followed the order of VO_x (63.1 nm) > $V_{0.1}Ce$ (30.1 nm) > $V_{0.025}Ce$ (18.0 nm) > $V_{0.2}Ce$ (14.8 nm) > CeO_2 (13.2 nm) > $V_{0.05}Ce$ (10.7 nm). The specific surface area of CeO_2 and VO_x/CeO_2 was much higher than that of VO_x , which obeyed the sequence of CeO_2 (110.9 m²·g⁻¹) $> V_{0.025}$ Ce (101.0 m²·g⁻¹) $> V_{0.05}$ Ce (98.6 m²·g⁻¹) $> V_{0.1}$ Ce (93.4 m²·g⁻¹) $> V_{0.2}$ Ce (76.1 $m^2 \cdot g^{-1}$) >> VO_x (11.3 $m^2 \cdot g^{-1}$). It was revealed that the specific surface area of VO_x/CeO_2 catalysts decreased along with the increase in VO_x loading because of the partial blockage of CeO₂poresby VO_x species [28].

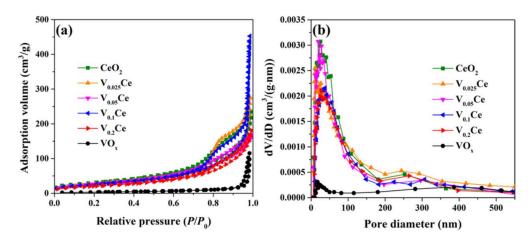


Figure 3. (a) Nitrogen adsorption/desorption isotherms and (b) pore size distribution of prepared catalysts.

Table 1. Textural properties and catalytic performance of prepared catalysts.

Sample	$S_{ m BET}$ a (m ² ·g ⁻¹)	$V_{\rm t}^{\rm \ b} \ (imes 10^{-2}, \ { m cm}^3 \cdot { m g}^{-1})$	$D_{\mathrm{p}}^{\ \mathrm{c}}$ (nm)	T ₅₀ ^d (°C)	T ₉₀ ^d (°C)
CeO ₂	110.9	36.54	13.2	328	381
$V_{0.025}Ce$	101.0	45. 46	18.0	299	367
$V_{0.05}Ce$	98.6	26. 43	10.7	281	347
$V_{0.1}Ce$	93.4	30.46	30.1	294	356
$V_{0.2}Ce$	76.1	28.18	14.8	307	413
VO_x	11.3	17.92	63.1	/	/

^a Specific surface area obtained at $P/P_0 = 0.05$ –0.30 by the Brunauer–Emmett–Teller (BET) method; ^b total pore volume estimated at $P/P_0 = 0.99$; ^c pore diameter calculated from the N₂ desorption branch by the Barrett–Joyner–Halenda (BJH) method; ^d temperatures at which 50% and 90% conversion of 1,2–dichloroethane (1,2–DCE) occurred.

3.2. Surface Composition and Element Status

The surface elemental composition and oxidation status of prepared materials were characterized through XPS, as illustrated in Figure 4 and Table 2. The C 1s, O 1s, V 2p, and Ce 3d peaks of prepared materials could be detected, as shown in Figure 4a. As shown in Figure 4b, O 1s XPS spectra were classified into three sub-peaks centered at 529.3-529.9, 531.5-531.9, and 533.0-533.4 eV, which were attributed to lattice oxygen $(O_{\alpha}; O^{2-})$, surface oxygen species adsorbed on oxygen vacancies $(O_{\beta}; O_{2}^{2-}, O^{-}, OH^{-}, OH^{-})$ and CO_3^{2-}), and carbonates and/or water (O_γ) , respectively [32,33]. The $O_\beta/(O_\alpha + O_\beta)$ ratios of prepared catalysts followed the sequence of $V_{0.05}$ Ce (0.61) > $V_{0.1}$ Ce (0.57) > $V_{0.025}$ Ce $(0.54) > CeO_2$ $(0.48) > V_{0.2}$ Ce $(0.46) > VO_x$ (0.45) (Table 2), suggesting that the $V_{0.05}$ Ce catalyst possessed the largest number of surface oxygen species, facilitating the destruction of 1,2–DCE [5]. Figure 4c shows the V 2p XPS spectra of VO_x and VO_x/CeO₂ catalysts. Only V⁵⁺ species could be detected over VO_x, corresponding to the presence of the V_2O_5 phase. The peaks at 517.1–517.4 and 515.0–515.4 eV represented V^{5+} and V^{4+} , respectively, suggesting that V⁵⁺ and V⁴⁺ species co–existed on VO_x/CeO₂ catalysts [34]. Moreover, the peak–fitting results demonstrated that VO_x/CeO₂ catalysts were mainly composed of V^{5+} species corresponding to the V_2O_5 phase [21,34]. As shown in Table 2, the ratios of $V^{5+}/(V^{4+}+V^{5+})$ for $V_{0.025}$ Ce, $V_{0.05}$ Ce, $V_{0.1}$ Ce, and $V_{0.2}$ Ce catalysts were 0.84, 0.87, 0.85, and 0.83, respectively, indicating that the $V_{0.05}$ Ce material possessed high ratios of $V^{5+}/(V^{4+}+V^{5+})$, favorable for 1,2–DCE oxidation. The Ce 3d XPS spectra were split into eight sub-peaks, as depicted in Figure 4d. Six peaks of Ce 3d labeled by V, V'', V''', U, U'', and U''' were assigned to Ce^{4+} species and the other two peaks labeled by U' and V' belonged to Ce^{3+} species [34]. The $Ce^{3+}/(Ce^{3+} + Ce^{4+})$ ratios of prepared

catalysts were calculated according to the corresponding peak areas, as documented in Table 2. Generally, surface oxygen vacancies were formed by the removal of lattice oxygen species (O_{α}) in CeO₂, causing the formation of Ce³⁺ species (Ce⁴⁺ + e⁻ \rightarrow Ce³⁺ + \diamond) [35]. According to Table 2, Ce³⁺/(Ce³⁺ + Ce⁴⁺) ratios of prepared materials followed the order of V_{0.05}Ce (0.19) > V_{0.1}Ce (0.18) > V_{0.025}Ce (0.17) > CeO₂(0.15) > V_{0.2}Ce (0.13), suggesting that V_{0.05}Ce owned the largest amount of Ce³⁺ species. It was reported that a large amount of Ce³⁺ species contributes to the formation of oxygen vacancies, which can effectively accelerate the mobility of active oxygen species and consequently promote the catalytic activity [35]. This result also suggested that VO_x species interaction with CeO₂ was strongest over V_{0.05}Ce, leading to the formation of more low–valence Ce³⁺ species [28].

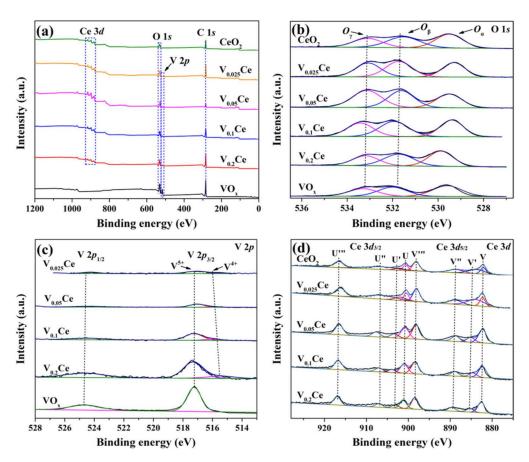


Figure 4. X-ray photoelectron spectroscopy (XPS) spectra of prepared catalysts: (**a**) C 1*s*, (**b**) O 1*s*, (**c**) V 2*p*, and (**d**) Ce 3*d*.

Binding Energy (eV) **Molar Ratio** Sample v^{4+} $O_{\beta}^{\ b}$ $V^{5+}/(V^{5+} + V^{4+})$ V^{5+} O_{α} a O_{γ} c $O_{\beta}/(O_{\alpha} + O_{\beta})$ $Ce^{3+}/(Ce^{3+} + Ce^{4+})$ 529.5 531.5 533.2 0.48 0.15 CeO₂ 515.2 517.1 529.3 531.7 0.54 0.84 0.17 $V_{0.025}$ Ce 533.0 $V_{0.05}Ce$ 515.4 517.2 529.5 531.6 533.1 0.87 0.19 0.61 517.2 531.9 $V_{0.1}Ce$ 515.0 529.4 533.4 0.57 0.85 0.18 $V_{0.2}Ce$ 515.4 517.4 529.9 531.8 533.3 0.46 0.83 0.13 VO_x 517.2 529.6 531.9 533.3 0.45

Table 2. XPS results of prepared catalysts.

^a Lattice oxygen species; ^b surface oxygen species; ^c adsorbed oxygen species from hydroxyl and adsorbed water on the surface.

3.3. Reducibility and Oxygen Species Mobility

An H₂-TPR experiment was employed to test the redox properties of all samples, as depicted in Figure 5a. For CeO₂, the reduction peaks presented at ca. 524 and 785 °C were respectively associated with the reduction of surface Ce⁴⁺ to Ce³⁺ and bulk CeO₂ [28]. The introduction of VO_x could effectively enhance the redox capacity of CeO₂. For VO_x/CeO₂ catalysts, the reduction peaks located at 518, 500, 507, and 526 °C were indexed to the reduction of VO_x species ($V^{5+} \rightarrow V^{4+}$), while the peaks at 436, 454, 466, and 492 °C were indexed to the reduction of surface CeO_2 ($Ce^{4+} \rightarrow Ce^{3+}$) [22,28], indicating the co-existence of Ce^{4+}/Ce^{3+} and V^{5+}/V^{4+} species, in accordance with the XPS results (Figure 4). It is illustrated that the reduction temperature of VO_x species in VO_x /CeO₂ (except $V_{0.025}$ Ce) catalysts apparently shifted to higher temperatures along with the increase in VO_x loading due to the CeO₂ interaction with VO_x species affecting the redox performance of surface CeO₂ [22]. The total H₂ consumption of prepared materials below 600 °C followed the order of $V_{0.05}$ Ce (9.86 mmol·g⁻¹) > $V_{0.1}$ Ce (9.53 mmol·g⁻¹) > $V_{0.025}$ Ce (8.64 mmol·g⁻¹) >CeO₂ (8.02 mmol·g⁻¹) > V_{0.2}Ce (7.63 mmol·g⁻¹), suggesting that V_{0.05}Ce possessed superior reducibility (Table 3). Additionally, the initial H₂ consumption (less than 25% H₂ consumption for the first reduction peak) rate was also employed to evaluate the low-temperature reducibility of all catalysts [24]. Figure 5b shows that the initial H₂ consumption rates of the catalysts followed the sequence of $V_{0.05}Ce > V_{0.1}Ce > V_{0.025}Ce >$ CeO₂> V_{0.2}Ce, suggesting that V_{0.05}Ce had superior low-temperature reducibility.

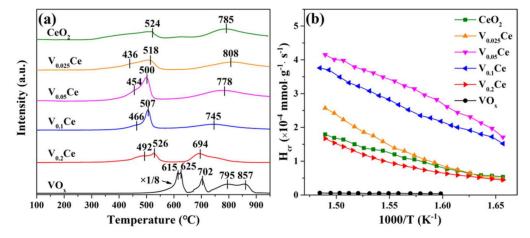


Figure 5. (a) Hydrogen temperature programmed reduction (H₂-TPR) and (b) the initial H₂ consumption rate of prepared catalysts.

	_	 	
Sample	H_2 Consumption (mmol·g ⁻¹)	O ₂ Desorption Peaks	N

Table 3. H₂–TPR, O₂–TPD, and NH₃–TPD results of prepared catalysts.

Sample	H_2 Consumption (mmol·g ⁻¹)	О ₂ Г	esorption I	NH ₃ Desorption Peaks	
	P ^a	P_1^{b}	P_2 c	P_3 d	P e
CeO ₂	8.02	25,200	7190	5029	231.78
$V_{0.025}Ce$	8.64	40,000	9423	11,700	250.55
$V_{0.05}Ce$	9.86	30,700	13,700	26,900	257.03
$V_{0.1}Ce$	9.53	27,800	12,256	56,600	244.76
$V_{0.2}Ce$	7.63	8536	2551	59,100	223.09
VO_x	/	/	/	26,700	83.87

^a Hydrogen consumption at 100–600 °C; ^b areas of physically adsorbed oxygen species; ^c chemically adsorbed oxygen (O⁻ and O₂⁻) species; ^d weak surface lattice oxygen (O²⁻) species; ^e total area of NH₃ desorption peaks.

The O₂-TPD results of prepared materials are displayed in Figure 6. Generally, the peaks located at <250, 250–550, and 550–750 °C could be regarded as the physically adsorbed oxygen species, chemically adsorbed oxygen (O $^-$ and O $_2^-$) species, and weak surface lattice oxygen (O 2) (bulk lattice oxygen at above 750 °C), respectively [36,37]. For CeO $_2$ and VO $_x$ /CeO $_2$ catalysts, the desorption peaks located at 169, 160, 187, 193, and 176 °C were assigned to the physically adsorbed oxygen (O $^-$ and O $_2^-$) species. The desorption peaks in the region of 250–550 °C corresponded to the chemically adsorbed oxygen species. Additionally, the desorption peaks located at 642, 747, 706, 644, and 565 °C could be associated with the weak surface lattice oxygen (O 2) [16,38]. Generally, the lattice oxygen diffused from bulk to surface, which further promoted the reduction of V 5 + to V 4 + and Ce 4 + to Ce 3 + [38]. For the VO $_x$ catalyst, the desorption peaks presented at 629 and 684 °C were consistent with the weak surface lattice oxygen (O 2). As displayed in Table 3, the desorption amount of chemically adsorbed oxygen (O 2 and O $_2$) species followed the sequence of V $_{0.05}$ Ce > V $_{0.1}$ Ce > V $_{0.025}$ Ce > CeO $_2$ > V $_{0.2}$ Ce, suggesting that V $_{0.05}$ Ce possessed excellent chemically adsorbed oxygen (O $^-$ and O $_2$) species mobility, favorable for 1,2–DCE oxidation.

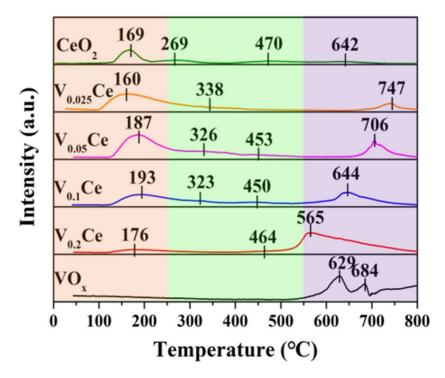


Figure 6. Temperature programmed desorption of O₂ (O₂–TPD) profiles of prepared catalysts.

3.4. Surface Acidity

The acidity properties of the prepared catalysts were investigated through NH₃–TPD, as displayed in Figure 7a. Generally, the NH₃desorption spectra of prepared catalysts were divided into three peaks corresponding to weak acidity (<200 °C), moderate acidity (200–400 °C), and strong acidity (>400 °C) [24]. CeO₂ displayed two peaks presented at 198 and 365 °C, which were related to the weak and moderate acid sites, respectively. The broad peaks over V_{0.05}Ce (232 °C) and V_{0.1}Ce (246 °C) catalysts were attributed to the moderate acid sites. Similarly, V_{0.025}Ce, V_{0.2}Ce, and VO_x catalysts also exhibited wide peaks at 160, 187, and 157 °C, which corresponded to the weak acid sites. The total NH₃desorption amount of the prepared catalysts followed the order of V_{0.05}Ce > V_{0.1}Ce > V_{0.025}Ce > CeO₂ > V_{0.2}Ce >> VO_x (Table 3), which revealed that the opportune introduction of VO_x could enhance the total acidity of CeO₂. V_{0.05}Ce possessed the largest number of acid sites, crucial for promoting the adsorption and activation of 1,2–DCE molecules [39].

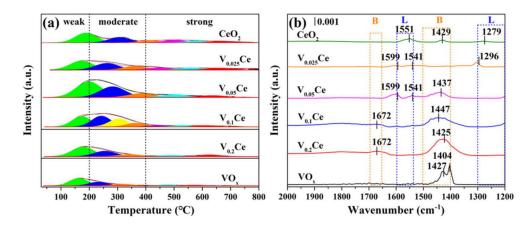


Figure 7. (a) Temperature programmed desorption of NH_3 (NH_3 –TPD) and (b) FT–IR spectra of NH_3 adsorption (NH_3 –IR) profiles of prepared catalysts.

An NH₃-IR analysis of prepared catalysts was further conducted to characterize the acid site types, as shown in Figure 7b. Generally, the bands in the regions of 1500–1400 and 1690–1660 cm⁻¹ were associated with the symmetric and antisymmetric stretching vibrations of NH₄⁺ species adsorbed on Brønsted acid (designed as B) sites [40,41]. The bands at 1300-1200 and 1600-1540 cm⁻¹ were related to the symmetric and antisymmetric stretching vibration of NH₃ adsorbed on Lewis acid (designed as L) sites [30,40]. For CeO₂, the band located at 1429 cm⁻¹ was related to the B acid sites, and the bands centered at 1279 and 1551 cm⁻¹ could be connected to the L acid sites. The bands at 1296, 1541, and 1599 cm $^{-1}$ associated with L acid sites over $V_{0.025}$ Ce could be detected. For $V_{0.05}$ Ce, the band located at 1437 cm $^{-1}$ corresponded to the B acid sites, while the bands centered at 1541 and 1599 cm $^{-1}$ corresponded to the L acid sites. Compared with CeO₂, more B and L acid sites could be observed over $V_{0.05}$ Ce. For $V_{0.1}$ Ce and $V_{0.2}$ Ce, the bands at 1404, 1427, and 1672 cm⁻¹ could be ascribed to the B acid sites. However, no L acid sites could be detected over V_{0.1}Ce and V_{0.2}Ce catalysts, indicating that more L acid sites were occupied with the increase in V loading [30]. The bands at 1404 and 1427 cm⁻¹ over VO_x corresponded to the B acid sites.

4. Discussion

4.1. Catalytic Activity and Stability

All prepared materials were evaluated in 1,2-DCE destruction, as exhibited in Figure 8a. According to T_{90} (the temperature for 90% conversion of 1,2–DCE), the activity sequence of synthesized materials was in the order of $V_{0.05}$ Ce (347 °C) > $V_{0.1}$ Ce (356 $^{\circ}$ C) > $V_{0.025}$ Ce (367 $^{\circ}$ C) > CeO₂ (381 $^{\circ}$ C) > $V_{0.2}$ Ce (413 $^{\circ}$ C) > CeO₂-C (> 450 $^{\circ}$ C) >> VO_x . The catalytic activity of CeO₂–C was significantly lower than that of hollow nanosphere– like CeO₂, indicating that the designed hollow nanosphere structure for CeO₂ had an advantage in 1,2-DCE degradation. Furthermore, it could be found that the activity of all catalysts increased slowly (<240 $^{\circ}$ C) and then enhanced rapidly with the increase in temperature as 1,2-DCE was firstly adsorbed at relatively low temperature and then activated with increasing temperature. Compared with CeO₂, the activity of V_{0.025}Ce, $V_{0.05}$ Ce, and $V_{0.1}$ Ce catalysts was obviously improved because the strong interaction of VO_x species with CeO₂ could promote the efficient removal of Cl species on the catalyst surface [16]. On the other hand, the catalytic activity of $V_{0.2}$ Ce was lower than that of CeO₂, which was related to the excessive VO_x content covering some oxygen vacancies or active sites of CeO₂ and inhibiting the removal of Cl species [42]. According to the XPS results in Figure 4d, $V_{0.05}$ Ce possessed the highest amount of Ce³⁺, indicating the presence of more oxygen vacancies in CeO₂, which could be advantageous to improving the mobility of active oxygen species and further promoting the oxidation of 1,2-DCE. According to H₂-TPR and O₂/NH₃-TPD results (Figures 5-7), it was demonstrated that $V_{0.05}$ Ce possessed superior low–temperature reducibility, excellent chemically adsorbed oxygen (O⁻ and O₂⁻) species mobility, and a large number of acid sites, facilitating the adsorption and oxidation of 1,2–DCE. Moreover, the strong interaction of VO_x species with CeO₂ could also efficiently enhance the activity of $V_{0.05}$ Ce.

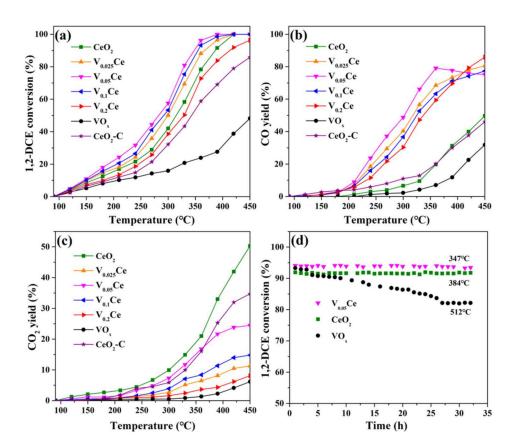


Figure 8. (a) Catalytic activity, (b) CO yield, (c) CO₂ yield, and (d) stability of prepared catalysts for 1,2–DCE destruction.

The yields of CO and CO₂ as a function of temperature were analyzed in Figure 8b,c. It was revealed that the yields of CO and CO₂ over CeO₂ and CeO₂–C catalysts increased with increasing temperature; however, much different behaviors could be found over VO_x/CeO₂. The yields of CO and CO₂ over CeO₂ only had a tiny gap and could reach approximately 50% at 450 °C, whereas the yields of CO (46%) and CO₂ (35%) over CeO₂–C were lower than that of hollow nanosphere–like CeO₂. It could be found that the yield of CO significantly increased when VO_x species were loaded on the surface of CeO₂. In addition, the yields of CO and CO₂ over V_{0.025}Ce, V_{0.1}Ce, and V_{0.2}Ce catalysts increased with increasing temperature. However, the yield of CO over V_{0.05}Ce catalyst initially increased and then decreased with increasing temperature, attributed to the further oxidation of CO (>360 °C). It was reported that the final product mainly containing carbon species is CO over VO_x/CeO₂ catalysts during 1,2–DCE destruction, and the high yield of CO is presumed to be connected to the surface lattice oxygen of VO_x [15].

Reaction stability is one of the most important indices to evaluate the application prospect of a catalyst. The stabilities of $V_{0.05}Ce$, CeO_2 , and VO_x were studied at approximately T_{90} temperatures, as shown in Figure 8d. The $V_{0.05}Ce$ catalyst possessed outstanding catalytic stability and resistance to chlorine poisoning, maintaining approximately 94% of 1,2–DCE conversion at 347 °C for 32 h. Similarly, the catalytic stability of CeO_2 was maintained at approximately 92% at 384 °C in 32 h. However, the conversion of 1,2–DCE over VO_x decreased distinctly from 93% to 83% in the first 27 h, which could be ascribed to the attack of Cl species, leading to the loss of active sites.

4.2. Chlorinated Intermediate Species Distribution and Proposed Reaction Mechanism

 CO_2 , CO, HCl, and Cl_2 are the ideal products for CVOC destruction; however, chlorinated byproducts are usually inevitably formed. In this work, 1,1,2–trichloroethane $(C_2H_3Cl_3)$, vinyl chloride (C_2H_3Cl) , trichloroethylene (C_2HCl_3) , dichloromethane (CH_2Cl_2) , trichloromethane $(CHCl_3)$, and perchloromethane (CCl_4) were observed during the oxidation of 1,2–DCE. CCl_4 , $CHCl_3$, C_2HCl_3 , and $C_2H_3Cl_3$ as primary chlorinated byproducts collected at different reaction temperatures. Figure 9 presents the remarkable differences in the concentration of chlorinated byproducts detected over all catalysts. The concentrations of CCl_4 , $CHCl_3$, C_2HCl_3 , and $C_2H_3Cl_3$ over VO_x/CeO_2 catalysts were obviously lower than those over CeO_2 and VO_x . Additionally, it was observed that the concentrations of chlorinated byproducts over CeO_2 and VO_x/CeO_2 catalysts firstly increased and then decreased with increasing test temperature (>250 °C). The appropriate introduction of VO_x species ($V_{0.025}Ce$, $V_{0.05}Ce$, and $V_{0.1}Ce$) in CeO_2 was advantageous for the catalytic activity of CeO_2 and remarkably inhibited the formation of chlorinated byproducts, ascribed to the strong interaction between VO_x species and CeO_2 and the superior removal ability of Cl species during 1,2-DCE oxidation [30,43].

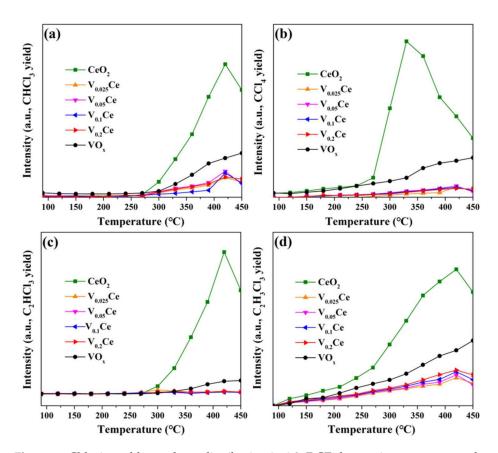


Figure 9. Chlorinated byproducts distribution in 1,2–DCE destruction over prepared catalysts: (a) $CHCl_3$, (b) CCl_4 , (c) C_2HCl_3 , and (d) $C_2H_3Cl_3$.

The reaction process of 1,2-DCE over prepared materials was deeply studied using an in situ DRIFTS experiment, as displayed in Figure 10. The broad bands presented at 3100–4000 cm $^{-1}$ were indexed to the stretching vibrations of hydrogen–bonded OH [15,44]. Additionally, no bands corresponding to VO_x species were detected over VO_x/CeO_2 catalysts because of the highly dispersed VO_x species on the CeO_2 surface [44].

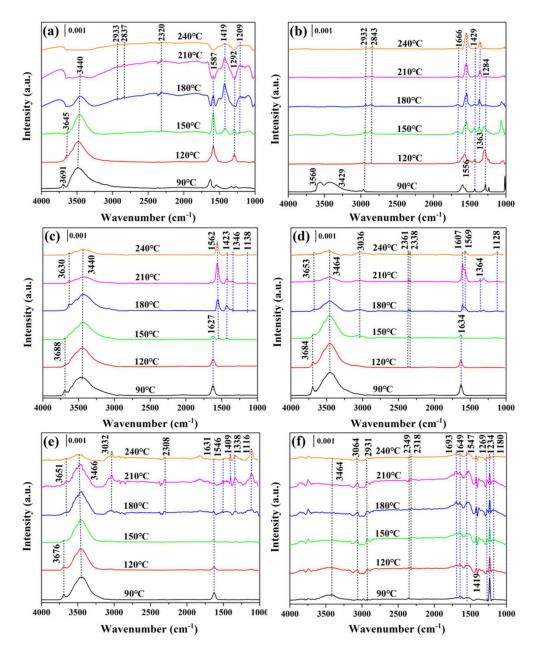


Figure 10. In situ diffuse reflectance infrared spectroscopy (DRIFTS) of 1,2–DCE catalytic oxidation: (a) CeO_2 , (b) $V_{0.025}Ce$, (c) $V_{0.05}Ce$, (d) $V_{0.1}Ce$, (e) $V_{0.2}Ce$, and (f) VO_x .

The bands presented at 2932–2933 and 2837–2843 cm $^{-1}$ attributed to the asymmetric and symmetric stretching of methyl (CH₃–) could be observed over CeO₂ and V_{0.025}Ce, respectively, which was attributed to the generation of CH₃CHO and CH₃COOH intermediates during the 1,2–DCE oxidation process [45]. On the other hand, no bands could be detected over the V_{0.05}Ce catalyst in the above wavenumber range. The weak bands located at 3036–3032 cm $^{-1}$ were detected over V_{0.1}Ce (>150 °C) and V_{0.2}Ce (>180 °C) catalysts, which corresponded with the asymmetric stretching of methylene species (–CH₂–) [15,45]. VO_x exhibited two weak bands at 3064 and 2931 cm $^{-1}$ corresponding to antisymmetric stretching of methylene species and antisymmetric stretching of methyl (CH₂–), respectively [45]. Generally, the vibration of –CH– stretching (v(CH), such as CH₂– and CH₃– groups) is related to the adsorption of 1,2–DCE on the catalyst surface [46]. The bands present between 2400 and 2300 cm $^{-1}$ were associated withCO₂ adsorption, while the bands located in the 2300–2000 cm $^{-1}$ region were indexed to CO adsorption [15,43]. As shown in Figure 10b,c, no bands corresponding to adsorbed CO₂ were detected over

 $V_{0.025}$ Ce and $V_{0.05}$ Ce catalysts, and the bands corresponding to adsorbed CO could not be observed in all catalysts. The bands at 1700–1200 cm⁻¹ could be classified as the vibration of surface formates, carbonate species, and hydrocarbons, which were associated with the formation of CO₂ and CO during 1,2–DCE oxidation [24].

For all catalysts, the bands present at 1666–1610 cm⁻¹ were considered as C=C stretching vibration [30]. The intensity of the stretching vibration of C=C over V_{0.1}Ce and V_{0.2}Ce catalysts gradually decreased with increasing temperature and finally disappeared at relative high temperature. The band deemed as C=O stretching vibration (ca. 1693 cm $^{-1}$) could be found over VO_x [43]. The characteristic bands appearing at 1587–1532 cm $^{-1}$ corresponding to the carboxylate $v(COO^{-})$ asymmetric stretching of acetate species could be detected over all catalysts [47]. The bands located at 1429–1409 cm⁻¹ associated with the formation of -CH₂- and -CH- groups (e.g., δ (CH₂Cl), δ (HCCl), and δ (CCH)) could be detected over all catalysts (except V_{0.1}Ce), illustrating that 1,2-DCE was adsorbed and activated [15,43]. The intensity of bands over these catalysts primarily increased and then decreased with escalating temperature, inferring that 1,2-DCE oxidation occurred [15]. Bands located at 1332–1364 cm⁻¹ over VO_x/CeO₂ catalysts could be detected, which were ascribed to the partial oxidized surface species as acetates, maleate species, and formats [47]. The bands presented at 1138–1120 cm⁻¹ were indexed to the vibration stretching of -CH-. The bands at 1284–1292 cm⁻¹ over CeO₂ and $V_{0.025}$ Ce catalysts could be attributed to -CH- vibration groups [48]. The band present at 1209 cm⁻¹ could be indexed to phenolate (v(CH)/v(CO)) over CeO_2 . Moreover, the bands over VO_X located at 1269, 1234, and 1180 cm⁻¹ could be identified as the formation of $-CH_2$ and -CHgroups, suggesting that 1,2-DCE was adsorbed and activated over the catalyst.

Combining the results of in situ DRIFTS and byproduct distribution (Figures 9 and 10), a destruction mechanism of 1,2–DCE over prepared materials was proposed, as shown in Scheme 1. Generally, the catalytic oxidation of chlorinated alkanes (CA) proceeds according to the procedure of CA adsorption \rightarrow Cl dissociation \rightarrow C-C/C-Cl cleavage →Cl desorption/accumulation [49,50]. As such, 1,2–DCE is initially adsorbed on the surface of catalysts, which is mainly ascribed with the adsorption and dissociated of Cl bonds on Lewis acid sites ($V^{5+/4+}$ and $Ce^{4+/3+}$) [15]; The C-Cl (Path 1) and C-C (Path 2) bonds in 1,2-DCE are activated and cleaved, forming chloroethane, vinyl chloride, and chloromethane intermediates. Afterward, the polychlorinated byproducts (CHCl₃, CCl₄, C₂HCl₃, and C₂H₃Cl₃) are mainly produced via dehydrochlorination and chlorination. Then, the reaction of dissociative Cl from polychlorinated byproducts and surface hydroxy groups can form HCl, and HCl would be partially oxidized to form Cl₂ (the Deacon reaction) [15,49]. Additionally, the intermediate acetaldehyde (from the activation of the C-H bond and the transformation of hydrogen species on VO_x species [15]) would be easily and rapidly oxidized to oxygenate species (carbonate bidentate) and partially oxidized to maleates, acetates, formates, and so on, which are usually considered the main source for the generation of CO and CO₂ [24,51]. The above oxygenate species are further oxidized to form the final products (CO, CO₂, Cl₂, and HCl).



Scheme 1. Proposed 1,2–DCE destruction mechanism over prepared catalysts.

4.3. Effect of Water Vapor

It is of great importance to study the influence of water vapor on the reaction activity of samples for CVOC destruction. Here, water vapor with different concentrations (1–5 vol.%) was introduced to study the influence of water vapor on the activity of the $V_{0.05}$ Ce catalyst in 1,2-DCE oxidation (Figure 11a). The conversion of 1,2-DCE was maintained at approximately 94% without water vapor. Interestingly, when 1, 2, or 5 vol.% of water vapor was injected into the atmosphere, 1,2-DCE conversion over the V_{0.05}Ce catalyst increased slightly and was maintained at approximately 97%, 96%, or 95%, respectively, owing to that low concentration of water molecules efficiently removing Cl species from the catalyst surface [52]. However, the promotion effect of water vapor gradually decreased with increasing concentration because of the competitive adsorption or blockage of water molecules on active sites [17,52]. In addition, the catalytic activity of $V_{0.05}$ Ce was restored to the initial level when water vapor was removed from the reaction atmosphere, indicating that the $V_{0.05}$ Ce catalyst had good water resistance and stability under the conditions with/without water vapor during 1,2-DCE destruction. The effect of water vapor on chlorinated byproduct distribution over the $V_{0.05}$ Ce catalyst was further investigated, as exhibited in Figure 10b-d. It was found that the presence of water vapor did not change the type of chlorinated byproducts; however, the yields of CHCl₃, CCl₄, and C_2HCl_3 over the $V_{0.05}Ce$ catalyst were apparently lower than those in the absence of water vapor because the reactivity of Cl₂ was inhibited by water molecules as a hydrogen source [7,49]. Moreover, the yield of chlorinated byproducts decreased with increasing water vapor concentration, suggesting that the presence of water vapor could efficiently inhibit the generation of chlorinated byproducts during 1,2–DCE oxidation.

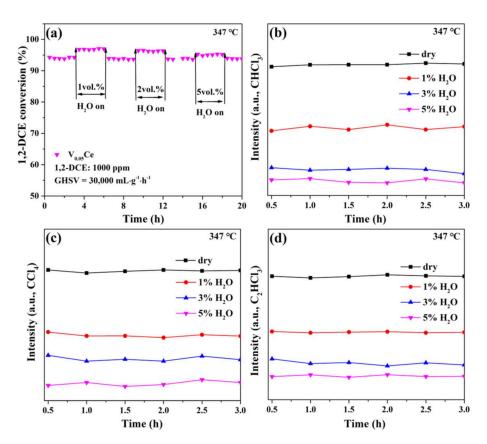


Figure 11. (a) Effects of water on 1,2–DCE conversion over $V_{0.05}$ Ce catalyst; (b) CHCl₃, (c) CCl₄, and (d) C_2 HCl₃ distribution during the stability test.

4.4. Key Factors Inhibiting the Formation of Chlorinated Intermediate Species

Figure 9 reveals that the yields of chlorinated byproducts (CHCl₃, CCl₄, C₂HCl₃. and C₂H₃Cl₃) over VO_x/CeO₂ were significantly lower than those of CeO₂ and VO_x during the 1,2–DCE oxidation process, ascribed to the high surface Cl removal ability of composite catalysts. Feng et al. [24] reported that the CoCrO_x catalyst can effectively inhibit the yield of chlorinated byproducts during 1,2–DCE destruction, and it possesses better product selectivity than Cr₂O₃ and Co₃O₄ due to the abundant B and L acid sites and higher acid strength. Therefore, the relationship between chlorinated byproducts yield and total acidity over VO_x/CeO₂ catalysts was analyzed. As shown in Figure 12a, CHCl₃, CCl₄, C₂HCl₃, and C₂H₃Cl₃ yields versus total acidity maintained linear relationships ($R^2 = 0.996$, 0.991, 0.993, and 0.997, respectively). Compared with $V_{0.025}Ce$, V_{0.1}Ce, and V_{0.2}Ce catalysts, V_{0.05}Ce possessed higher total acidity and lower chlorinated byproduct (CHCl₃, CCl₄, C₂HCl₃, and C₂H₃Cl₃) yields, indicating that the yields of chlorinated byproducts decreased with increasing total acidity, which apparently reduced the occurrence of the chlorination reaction [53]. In addition, the catalytic activity of VO_x/CeO_2 catalysts (T_{90}) versus total acidity maintained a good linear relationship (R^2 = 0.995), as shown in Figure 12b. The above results indicate that the total acidity of catalysts played a vital role in inhibiting the production of chlorinated byproducts. Therefore, it can be reasonably explained that the low chlorinated byproduct yields could be ascribed to the higher total acidity and good synergy between CeO2 and VOx species during the 1,2–DCE oxidation process.

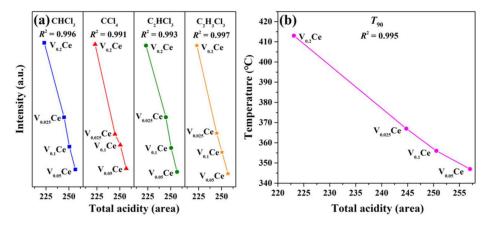


Figure 12. (a) Relationship between chlorinated byproduct yields and total acidity over VO_x/CeO_2 catalysts; (b) relationship between T_{90} of VO_x/CeO_2 catalysts and total acidity.

4.5. Characterization of the Used Catalysts

XRD and XPS analyses of the used $V_{0.05}$ Ce catalyst were carried out, and the results are summarized in Figure 13 and Table S1 (Supplementary Materials). Compared to the fresh $V_{0.05}$ Ce catalyst, the crystal phase of CeO_2 of the used $V_{0.05}$ Ce catalyst remained unchanged, indicating that the phase of CeO_2 was not destroyed by the attack of Cl species, further confirming that the $V_{0.05}$ Ce catalyst possessed excellent resistance to chlorine poisoning (Figure 13a). Figure 13b shows that the lattice oxygen (O_α) species abundance of the used $V_{0.05}$ Ce catalyst was lower than that of the fresh $V_{0.05}$ Ce catalyst, indicating that a large number of lattice oxygen species were removed, giving rise to the greater formation of Ce^{3+} species (Table S1, Supplementary Materials) [35]. We discovered that the Ce^{3+} species abundance of the used $V_{0.05}$ Ce catalyst was remarkably higher than that of the fresh $V_{0.05}$ Ce catalyst, confirming that the lattice oxygen species was removed leading to the greater formation of Ce^{3+} species (Figure 13c and Table S1, Supplementary Materials). Additionally, greater Ce^{3+} species abundance led to greater formation of surface oxygen vacancies, with surface oxygen species being adsorbed onto oxygen vacancies over time, showing that the $V_{0.05}$ Ce catalyst owned superior catalytic

performance (Figure 13b and Table S1, Supplementary Materials). No V^{4+} species over the used $V_{0.05}Ce$ catalyst could be detected, suggesting that the V^{4+} species were completely transformed into V^{5+} species ($V^{4+} \rightarrow V^{5+}$), accelerating the oxidation of 1,2–DCE (Figure 13d). According to the above results, it was confirmed that the Ce^{3+} species and surface oxygen (O_{β}) species are important factors in improving the catalytic performance of the $V_{0.05}Ce$ catalyst.

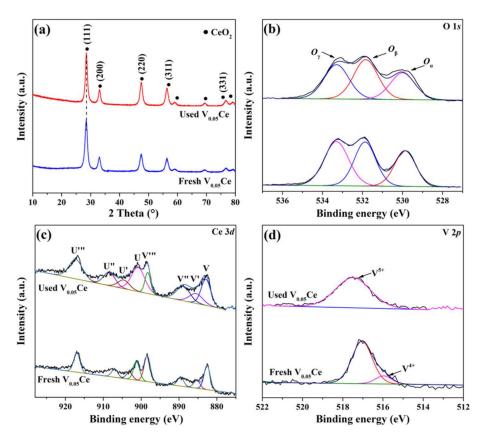


Figure 13. (a) XRD of the used $V_{0.05}$ Ce catalyst; XPS spectra of the used $V_{0.05}$ Ce catalyst: (b) O 1s, (c) Ce 3d, and (d) V 2p.

The Cl 2p spectra of all used catalysts were also further employed to investigate the chlorine deposit over catalysts, as displayed in Figure S5 (Supplementary Materials). The peaks at 198.1–198.5 eV were assigned to HCl and/or Cl₂, while the peaks at 198.1–198.5 eV were ascribed to the adsorption of 1,2–DCE on the catalyst surface [36]. It was revealed that CeO₂ had two peaks respectively ascribed to the HCl (and/or Cl₂) species and the adsorption of 1,2–DCE on the catalyst surface. However, it the adsorption peak of 1,2–DCE on the catalyst surface could not be observed over CeO₂–C. It was speculated that the 1,2–DCE did not directly contact the surface of the catalyst during the reaction process, which could explain the poor catalytic performance of the CeO₂–C catalyst. HCl (and/or Cl₂) species and the adsorption of 1,2–DCE on the catalyst surface over VO_x/CeO₂ catalysts (except V_{0.05}Ce) could be detected. Unexpectedly, no peaks could be discovered over V_{0.2}Ce and VO_x catalysts, potentially due to the formation of chlorinated oxide rather than HCl (and/or Cl₂) species.

4.6. Key Factors for 1,2-DCE Oxidation

Combining the results of the surface properties (XRD and XPS) of the used $V_{0.05}$ Ce catalyst, it was discovered that the lattice oxygen (O_{α}) species abundance of the used $V_{0.05}$ Ce catalyst was lower than that of the fresh $V_{0.05}$ Ce catalyst and the Ce³⁺ species abundance of the used $V_{0.05}$ Ce catalyst was remarkably higher than that of the fresh

 $V_{0.05}$ Ce catalyst. Moreover, the surface oxygen species abundance adsorbed on the oxygen vacancies of the $V_{0.05}$ Ce catalyst increased after the stability test. Therefore, the large number of Ce³⁺ species could enhance the formation of oxygen vacancies, which could effectively accelerate the mobility of active oxygen species and consequently promote the catalytic activity. According to the results of H₂-TPR, it was revealed that both the total H₂ consumption amount and the initial H₂ consumption rate of catalysts followed the sequence of $V_{0.05}Ce > V_{0.1}Ce > V_{0.025}Ce > CeO_2 > V_{0.2}Ce$, suggesting that $V_{0.05}Ce$ had superior low-temperature reducibility, effectively promoting the low-temperature reaction of 1,2-dichloroethane. The relationship between chlorinated byproduct yields and total acidity over VO_x/CeO₂ catalysts was also analyzed. It was found that CHCl₃, CCl₄, C₂HCl₃, and C₂H₃Cl₃ yields versus total acidity maintained linear relationships $(R^2 = 0.996, 0.991, 0.993, and 0.997, respectively)$. Compared with $V_{0.025}$ Ce, $V_{0.1}$ Ce, and V_{0.2}Ce catalysts, V_{0.05}Ce possessed higher total acidity and lower chlorinated byproduct (CHCl₃, CCl₄, C₂HCl₃, and C₂H₃Cl₃) yields, indicating that the yields of chlorinated byproducts decreased with increasing total acidity. Moreover, the catalytic activity of VO_x/CeO_2 catalysts (T_{90}) versus total acidity maintained a good linear relationship $(R^2 = 0.995)$. The above results indicated that the low chlorinated byproduct yields could be ascribed to higher total acidity during 1,2–DCE oxidation process. The influence of water vapor on the formation of chlorinated byproducts was also studied. It was displayed that the presence of water vapor did not change the type of chlorinated byproducts; however, the yields of CHCl₃, CCl₄, and C₂HCl₃ over the V_{0.05}Ce catalyst were apparently lower than those in the absence of water vapor because the reactivity of Cl₂ was inhibited by water molecules as a hydrogen source. Moreover, the yield of chlorinated byproducts decreased with increasing water vapor concentration, suggesting that the presence of water vapor could efficiently inhibit the generation of chlorinated byproducts during 1,2–DCE oxidation.

5. Conclusions

In this work, hollow nanosphere–like VO_x/CeO_2 materials were prepared using a wetness impregnation route and tested for 1,2–DCE destruction. The superior low–temperature reducibility and the mobility of O^- and O_2^- species (chemically adsorbed oxygen species) ensured the superior catalytic activity, catalytic stability, and superior resistance to chlorine poisoning of the $V_{0.05}Ce$ catalyst for 1,2–DCE oxidation. The generation of chlorinated byproducts (e.g., CHCl₃, CCl₄, C₂HCl₃, and C₂H₃Cl₃) derived from the cleavage of C–C and C–Cl bonds of 1,2–DCE was inhibited owing to the abundant acid sites and synergy between VO_x and CeO_2 . Water vapor (1–5 vol.%) had a promoting effect on the activity of $V_{0.05}Ce$, which was ascribed to the efficient removal of Cl species on the surface.

Supplementary Materials: The following are available online at https://www.mdpi.com/2227-9 717/9/1/119/s1: Figure S1. XRD profiles of CeO_2 –C catalyst; Figure S2. HAADF–STEM images of CeO_2 –C catalyst; Figure S3. Nitrogen adsorption/desorption isotherms of CeO_2 –C catalyst; Figure S4. Pore size distribution of CeO_2 –C catalyst; Figure S5. Cl 2p XPS spectra of the used catalysts; Figure S6. CO_x selectivity of prepared catalysts; Table S1. XPS results of used $V_{0.05}Ce$ catalyst.

Author Contributions: Y.H. and S.F. presided over the methodology and writing—original draft; M.T. assisted with the investigation and resources; Y.W. helped with the visualization of graphs; Z.J. was in charge of data validation; C.H. conceptualized the project and was responsible for administration and writing—review and editing. All authors read and agreed to the published version of the manuscript.

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Article

Bimetallic Pt-Co Nanoparticle Deposited on Alumina for Simultaneous CO and Toluene Oxidation in the Presence of Moisture

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Abstract: Carbon monoxide (CO) and hydrocarbons (HCs) generally have competitive adsorption on the active site of noble-metal nano-catalysts, thus developing an effective way to reduce the passivation of competitive reaction with each other is an urgent problem. In this study, we successfully synthesized transition metal-noble metal (Pt-M) alloys via introducing inexpensive metal elements (M = Ni, Co and Cu) into Pt particles and then deposited on alumina support to form Pt-based catalysts. Subsequently, we choose CO and toluene as polluting gases to evaluate the catalytic activities of Pt-M/Al₂O₃ catalysts. Introducing inexpensive metal elements (M = Ni, Co, and Cu) significantly changed the physicochemical properties and catalytic activities of these Pt-based catalysts. It can be found that the Pt-Co/Al₂O₃ catalyst exhibited outstanding catalytic activity for CO and toluene oxidation under mixed gas atmosphere, compared with other Pt-based catalysts, which is due to the higher dispersity, more surface adsorption oxygen, and well redox ability. Surprisingly, H₂O could promote the catalytic activities for CO/toluene co-oxidation over the Pt-Co/Al₂O₃ catalyst. Thus, the present synthetic strategy not only opens an avenue towards the synthesis of noble metal-based catalysts, but also provides an excellent tolerance to H₂O in the catalytic process.

Keywords: bimetallic alloy; Pt-based catalysts; catalytic oxidation; toluene; moisture

1. Introduction

In recent years, with the progress of industrial development and the increased number of vehicles, the concentration of carbon monoxide (CO) and hydrocarbons (HCs) in ambient air is on the rise, causing the frequent occurrence of photochemical smog pollution in some areas and seriously threatening people's health [1–9]. However, controlling CO and HCs exhaust emissions can be an important direction to reducing air pollution. At present, there are many technical methods for controlling volatile organic compounds (VOCs), such as adsorption, catalytic oxidation, combustion, plasma, and so on. Among them, catalytic oxidation is known as the most efficient and economical method to remove VOCs [10-14]. Besides, catalytic oxidation has also been recognized as a promising technology for reducing exhaust gases because it directly converts pollutions into CO₂ and H₂O at relatively lower temperatures and reduces the production of other atmospheric pollutants. Precious metal catalysts and non-precious metal oxide catalysts are the most studied catalytic materials for CO and VOCs oxidation, but Pt-based catalysts are the preferred candidates due to their excellent catalytic properties [15,16]. To date, the commercial 3-way (Pt-Pd-Rh) catalysts have been widely used in the after-treatment system, but the catalytic converters realize the complete removal of CO and HCs exhaust emission at a high-temperature range (300-400 °C) [17]. Significantly, CO and HCs have competitive adsorption on the active sites of catalysts, and the catalytic performance of noble metal catalysts for CO oxidation can be strongly inhibited when HCs are introduced into the mixed gas [18–21]. For example, Ye et al. [21] synthesized a series of Pt-supported catalysts (Pt-Al $_2$ O $_3$, Pt-Co $_3$ O $_4$, and Pt-CeO $_2$) for simultaneous CO and toluene oxidation. They found that CO gas was vented into the reactor. The catalytic activities of CO and toluene over the Pt-based catalysts obviously decreased compared to those under individual CO and toluene oxidation due to competitive adsorption on the same active sites. Therefore, it is still an important topic to develop effective ways to reduce the competitive reaction between CO and HCs in Pt-based catalysts.

Recently, many studies have suggested that noble metals and other less expensive metal elements synthesize metal nanoalloys, which not only minimizes the total used amount of precious metals, but also gives rise to a superior catalytic activity due to the rearrangement of the valence electrons in the new potential fields [22–28]. For example, Yang et al. [25] reported that bimetallic Cu-Pd nanoalloys with atomic dispersion supported on aluminum oxide (Al₂O₃) substrates were applied for oxidizing benzene. The Al₂O₃-supported Cu-Pd particles with the ratio of Pd to Cu was 0.2 to 1, which exhibited the highest TOF for benzene transformation and the high dispersity of Pd in CuO. Yim et al. [27] also synthesized bimetallic Pt-based (Meso-PtM; M = Ni, Fe, Co, Cu) nanoparticles with self-supported meso-structures that showed very high redox reaction performance and durableness, in which the transition metals (M) promoted oxygen reduction reaction (ORR) activity by modulating the electronic structure and lattice strain. The commercial Pt/C and Pt black catalysts underwent a drastic activity decrease after durability tests, whereas Meso-PtNi with intermetallic phase exhibited superior activity and durability. Besides, Sato et al. [28] also prepared a γ-Al₂O₃-supported Pt-Co bimetallic catalyst [Pt(0.1)Co(1)/Al₂O₃] for purification of automotive exhaust, the electron-rich Pt and metallic Co promoted the adsorption and activation steps of the reactions with NO, CO, and hydrocarbons. Therefore, it is ideal for studying bimetallic Pt-based catalysts via introducing inexpensive metal elements for CO and toluene oxidation.

In this work, we reported a facile synthetic strategy to form bimetallic Pt-M (M = Ni, Co and Cu) catalysts for simultaneous CO and toluene oxidation, in which both transition metal and noble Pt metal were introduced onto an alumina support. The structural information of Pt-M/Al₂O₃ catalysts was further investigated by powder X-ray diffraction (XRD), transmission electron microscopy (TEM), CO-pulse chemisorption, X-ray photoelectron spectroscopy (XPS), hydrogen temperature-programmed reduction (H₂-TPR), and oxygen temperature-programmed desorption (O₂-TPD) measurement. At the same time, the effect of weight hourly space velocity (WHSV) and moisture, stability test on the catalytic performances of CO/toluene co-oxidation were further investigated. After introducing a secondary inexpensive metal, the catalytic activities over bimetallic Pt-M (M = Ni, Co, Cu) catalysts for CO/toluene oxidation were not significantly decreased. Interestingly, the catalytic activity of only Pt-Co/Al₂O₃ catalyst was better than that of Pt/Al₂O₃ catalyst for individual CO and toluene oxidation. When CO and toluene gases simultaneously exist in the reaction gases stream, the catalytic activities of these catalysts for CO and toluene oxidation decreased because of the competing adsorption in the same active sites. In addition, H₂O promoted the catalytic activities for CO/toluene oxidation over the Pt-Co/Al₂O₃ catalyst.

2. Experimental Section

Synthesis of Pt/Al₂O₃ Catalyst

The 2.0 g alumina (γ -Al₂O₃, \sim 300 m² g⁻¹, size about 200 nm) powders from Aladdin Reagents (Shanghai, China) and 1.0 mL Platinum nitrate (10.0 mg/mL Pt) were added to 250 mL of ultrapure water. The solution was heated to boiling point under vigorous magnetic stirring. Then, 11.0 mL mixed solution of 1.0 wt.% sodium citrate and 0.05 wt.% citric acid were added to the reaction system. After half a minute, 5.5 mL of a newly synthesized sodium borohydride (0.08 wt.%) solution with 1.0 wt.% sodium citrate and

0.05 wt.% citric acid were added. The above reaction solution was kept at 100 °C for 0.5 h under vigorous magnetic stirring. After the above process was finished, the solution was cooled to room temperature, washed 3 times with deionized water and ethanol under high-speed centrifugation, and dried at 80 °C for 12 h. Finally, the as-obtained products were reduced by passing 10% H_2 at 300 °C for 5 h. The nominal Pt content of Pt/Al_2O_3 is 0.5 wt.%. The as-prepared catalyst was denoted as Pt/Al_2O_3 .

Synthesis of bimetallic Pt-M/Al₂O₃ catalysts, sample characterizations, and catalytic oxidation of CO/toluene are presented in the Supplementary material.

3. Results and Discussion

3.1. XRD Analysis

The XRD patterns of as-synthesized Pt/Al₂O₃ and Pt-M/Al₂O₃ samples are shown in Figure S1. From the XRD spectra of four samples, it can be seen that each sample contains four distinct diffraction peaks at 37.6°, 45.8°, 39.5°, and 66.8°, corresponding to the (311), (222), (400), and (440) planes of γ -Al₂O₃ (JCPDS card No. 29-0063), respectively. No new diffraction peak corresponding to the Pt or PtO_x phase (approximately 33° and 44°) is observed, and there are no peaks associated with the Pt species. This may be due to the lower loading of Pt species or the high dispersion of Pt particles in the form of small particles on the alumina.

3.2. Surface Area Analysis

Figure 1 displays the N₂ sorption isotherms and pore size distributions for as-synthesized Al₂O₃, Pt/Al₂O₃, and Pt-M/Al₂O₃ catalysts. Prior to testing, these pristine samples were desorbed at 150 °C for 6.0 h under vacuum. The isotherms in Figure 1a were consistent with type IV isotherms with an H3-type hysteresis loop, indicating a mesoporous structure. The pores of these samples can be seen from the distribution of pore size in Figure 1b. It suggests that each sample is a mesoporous material. The mesoporous structure data of all the samples are summarized in Table 1. The samples have larger surface areas in the range of 205.99 \sim 303.34 m² g⁻¹. Compared to the Al₂O₃ support, it can be found that the surface areas of Pt/Al₂O₃ and Pt-M/Al₂O₃ catalysts decreased slightly, and the pore volumes also decreased slightly between $0.91 \text{ cm}^3 \text{ g}^{-1}$ and 0.73 s^{-1} cm³ g⁻¹. It is worth noting that pure Al₂O₃ possessed the largest surface area and pore volume among all the samples. The reason for this result may be that metal particles on the surface of Pt/Al₂O₃ and Pt-M/Al₂O₃ catalysts may hinder the pore channel of Al₂O₃ support. It is well known that the surface area has an effect on the catalytic activity of most reactions, and the catalysts with larger surface areas have better catalytic activity. In addition, abundant pore structure will be more favorable for the exposure of active sites, thereby facilitating the adsorption and reaction of reactants. However, for these Pt-M/Al₂O₃ catalysts, the surface area and pore structure may not be the crucial factors in the CO/toluene oxidation.

3.3. Microstructure

It is believed that the particle sizes and dispersions of Pt nanoparticles are also pivotal factors to influence the catalytic properties of these catalysts. Transmission electron microscopy (TEM) measurement was carried out to further reveal microstructures of Pt/Al₂O₃ and Pt-M/Al₂O₃ samples, as shown in Figure 2. Insets show the size distributions of Pt-based nanoparticles in Figure 2a–d, with the nanoparticles uniformly distributed on the surface of catalysts. These particles calculated from the histograms in Figure 2 have average diameters of ca. 3.5 ± 0.2 nm, ca. 3.6 ± 0.2 nm, ca. 3.5 ± 0.2 nm, and ca. 4.4 ± 0.2 nm for the Pt/Al₂O₃, Pt-Ni/Al₂O₃, Pt-Co/Al₂O₃, Pt-Cu/Al₂O₃, respectively. The representative high-resolution TEM (HRTEM) image of Pt/Al₂O₃ (Figure 2e) clearly reveals that the surface lattice spacing is measured to be 0.215 nm, which is matched well with the (111) crystal face of Pt phase. For the Pt-Ni/Al₂O₃ catalyst, the surface lattice spacing of 0.200 nm is measured in Figure 2f, which is consistent with the (111)

lattice plane of Pt. The HRTEM image of Pt-Co/Al $_2$ O $_3$ shows the surface lattice spacing in Figure 2g, and the measured d-spacing is 0.260 nm, consistent with the (200) lattice plane of Pt. For the Pt-Cu/Al $_2$ O $_3$ catalyst (Figure 2d,h), there is the surface lattice spacing with a d-spacing of 0.230 nm, which is matched well with the (200) crystal plane of the Pt phase. From the TEM/HRTEM images of all the catalysts, introducing inexpensive metal elements (M = Ni, Co, Cu) could be used to control the average size of metal Pt nanoparticles. In addition, MO $_x$ phases are not observed, which is due to the lower loading or the formation of intermetallic compounds between Pt and MO $_x$.

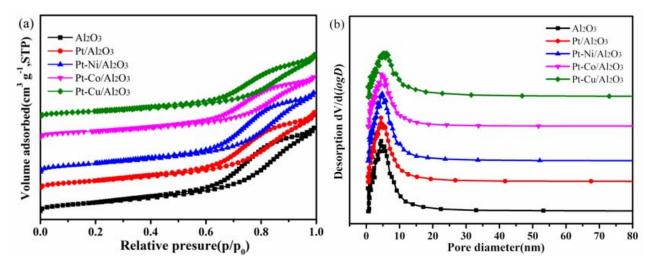


Figure 1. (a) N_2 adsorption/desorption isotherms and (b) pore-size distributions for Al_2O_3 , Pt/Al_2O_{3} , and $Pt-M/Al_2O_3$ samples.

Table 1. Elemental compositions, surface area data, and other physical-chemical parameters of Pt-Al₂O₃ and Pt/M-Al₂O₃ samples.

Sample	Pt Loading (wt.%)	M (Ni, Co and Cu) Loading (wt.%)	S _{BET} (m ² g ⁻¹)	V _{pore} (cm ³ g ⁻¹)	Pore Diameter (nm)	Pt ^a Dispersion (%)	TOF _{Pt-CO} b (10 ⁻² S ⁻¹)	TOF _{Pt-toluene} b (10 ⁻⁴ S ⁻¹)
$Pt Al_2O_3$	0.49	_	269.99	0.91	6.77	47.67	3.77	2.96
Pt/Ni- Al ₂ O ₃	0.47	0.41	295.81	0.95	6.43	51.07	4.86	3.40
Pt/Co- Al ₂ O ₃	0.48	0.43	226.25	0.73	6.44	59.97	5.29	4.77
Pt/Cu- Al ₂ O ₃	0.48	0.44	205.99	0.75	7.25	52.63	3.60	2.86
Al_2O_3	_	_	303.34	1.00	6.62	_	_	_

^a Pt dispersion was determined from CO-pulse chemisorption (the CO/Pt ratio is 1.0); ^b The turnover frequency (TOF) values were calculated via the CO/toluene conversions at 190 °C during the mixture conditions.

3.4. Temperature Programmed Reduction (TPR)

In Figure 3, the H₂-TPR results describe different forms and reduction behaviors of these Pt-based samples. Guo et al. reported that Pd/Al₂O₃ possessed negative peaks that were corresponded to the decomposition of the β -PdH phase, confirmed the existence of metallic Pd nanoparticles [29,30]. In addition, the H₂ desorption peak at higher temperatures indicates that some Pd species are easily reduced at normal temperature. In this work, H₂-TPR results show that one negative peak was observed at about 70–100 °C, and one positive peak was detected at about 450–500 °C for these catalysts. Fu et al. [31] revealed that many Co oxide species loaded onto Pt NPs to form a nanoalloy can be reduced at 100 °C. Regalbuto et al. [32] reported that alloying Pt-M (Co, Ni, Cu) was

enabled to observe hydrogen spillover. Thus, the negative peak could be the characteristic peak of hydrogen desorption due to the effect of metal Pt particles. The positive peak at high temperatures could be attributed to the reduction of lattice oxygen species on the surface of Al_2O_3 . Of course, these positive characteristic peaks at about $450–500\,^{\circ}\mathrm{C}$ can be considered as the reduction peaks of surface lattice oxygen on these catalysts. The above temperature regions of H_2 desorption peak over $Pt-M/Al_2O_3$ catalysts are similar to those of Pd/Al_2O_3 catalysts reported by Guo et al. [30]. Among these catalysts, the negative peak over the $Pt-Co/Al_2O_3$ catalyst slightly shifted to a higher temperature (93 °C), manifesting that the Pt species in $Pt-Co/Al_2O_3$ catalyst could still be easily reduced at lower temperatures. In addition, the addition of transition metal can cause the reduction peak to move slightly, and the intensity of hydrogen consumption at about $450–500\,^{\circ}\mathrm{C}$ on the $Pt-M/Al_2O_3$ catalysts is obviously decreased, which is mainly caused by the electronic interaction between transition metal oxides (MO_x) and Pt nanoparticles.

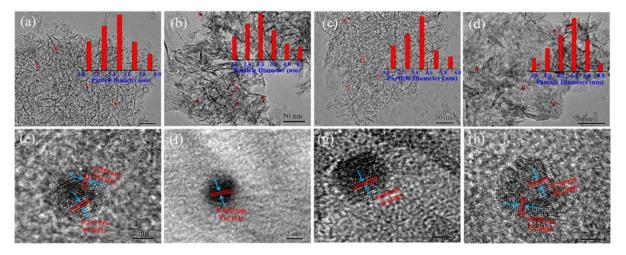


Figure 2. (a) Pt/Al_2O_3 , (b) $Pt-Ni/Al_2O_3$, (c) $Pt-Co/Al_2O_3$, and (d) $Pt-Cu/Al_2O_3$, as well as corresponding to (e-h) high-resolution transmission electron microscopy (HRTEM) images in the (a-d) TEM images, respectively (insets are the histograms to display the size distributions of Pt-based nanoparticles).

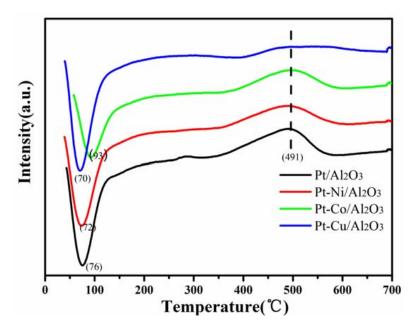


Figure 3. H_2 -TPR profiles of as-synthesized Pt/Al_2O_3 and $Pt-M/Al_2O_3$ samples.

3.5. Surface Element Composition

To further investigate the surface composition of these Pt-based catalysts, X-ray photoelectron spectra (XPS) measurement was tested on the four samples. Figure 4 illustrates Al 2p/Pt 4f and O1s XPS spectra of all the samples. Since the characteristic peaks of Al 2p and Pt 4f were close and overlapped in the range of 73~75 eV, thus the valency of platinum was not determined from Figure 4a. XPS spectra of O 1s were also further analyzed, and three oxygen chemical states were observed on the surface of Pt-based catalysts, as shown in Figure 4b. Wherein, the main peak with an O 1s spectrum appears in the position of binding energy (BE) of around 531.1 eV, which was related to lattice oxygen species (O_{latt}) [33,34]. While the peak at 532.2 eV was considered to be surface absorbed oxygen species (O_{ads}), and the weak peak at 533 eV was ascribed to adsorbed hydroxyl and water molecules (O_{-OH}). Besides, the proportion of three oxygen chemical states over these samples was calculated, the results are shown in Table 2. The oxygen vacancy (O_{ads} + O_{-OH}) ratios were Pt/Al₂O₃ (39.1%), Pt-Ni/Al₂O₃ (40.3%), Pt-Co/Al₂O₃ (42.5%), and Pt-Cu/Al₂O₃ (36.4%), respectively, indicating that Pt-Co/Al₂O₃ can provide the higher content of surface oxygen species. The existence of oxygen vacancies was of great significance to the chemical properties and catalytic activities of nanomaterials.

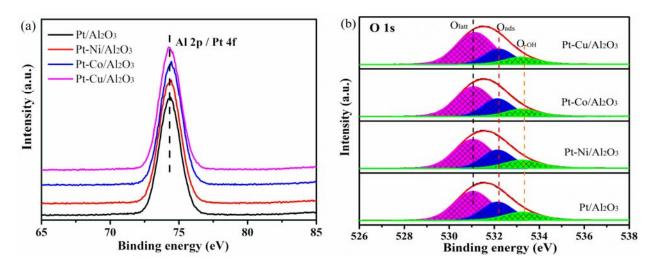


Figure 4. (a) Al 2p/Pt 4f and (b) O1s XPS spectra of these Pt/Al₂O₃ and Pt-M/Al₂O₃ samples.

Table 2. The binding energy and percentage ratio of O 1s XPS results over these Pt-based samples.

Sample	O _{latt} BE (eV)	O _{ads} BE (eV)	O _{-OH} BE (eV)	O _{latt} (%)	O _{ads} (%)	O _{OH} (%)
Pt/Al ₂ O ₃	531.17	532.23	533.41	60.9	23	16.1
$Pt-Ni/Al_2O_3$	531.06	532.24	533.4	59.7	27.0	13.3
Pt-Co/Al ₂ O ₃	531.08	532.13	533.23	57.5	27.3	15.2
Pt-Cu/Al ₂ O ₃	531.13	532.19	533.18	63.6	23.2	13.2

3.6. Oxygen Temperature-Programmed Desorption (O_2 -TPD)

 O_2 -TPD experiments were performed to understand their O_2 desorption behavior, as shown in Figure 5. Three distinct desorption peaks could be seen on four catalysts, corresponding to different desorption oxygen species. The conversion process of oxygen adsorption on a catalyst was followed [35–37]: O_2 (ads) $\rightarrow O_2^-$ (ads) $\rightarrow O^{2-}$ (ads) $\rightarrow O^{2-}$ (ads). Thus, it can be seen that these different states of oxygen on the surface of catalysts. Three distinct peaks were observed at about $170 \sim 210$ °C, $400 \sim 420$ °C, and $500 \sim 550$ °C. A α strong peak in the range of $100 \sim 300$ °C was regarded as the physically surface-adsorbed oxygen species and adsorbed O_2^- species (ads- O_2 and ads- O_2^- , respectively) [36,38,39]. A β peak in between 300 and 450 °C was assigned to surface lattice species (latt- O_2^-),

while the third peak (γ peak in between 450 and 600 °C) belongs to the pyrolysis of lattice oxygen at high temperature [40]. If the catalyst with α peak at a lower temperature level indicated that there could be more likely to produce surface oxygen species, which will provide higher catalytic activity. Generally speaking, a material with abundant reactive oxygen species can perform a redox reaction at lower temperatures, and the high-temperature oxygen fluidity can improve the efficiency of transporting oxygen species. As everyone knows that the oxidation process of VOCs mainly follows a Mars–van Krevelen mechanism and the reaction occurs due to a nucleophilic attack of surface absorbed oxygen species [41,42]. Meanwhile, the higher levels of surface active-oxygen species were conducive to VOCs oxidation [40,43–45]. Abundant surface oxygen vacancies could facilitate the formation of surface adsorbed oxygen species, which was verified by measuring the higher oxygen vacancy molar ratios of catalysts via XPS results in this study. Therefore, the strong desorption peak (α peak) of Pt-Co/Al₂O₃ suggests that more surface adsorption oxygen can be provided by the Pt-Co/Al₂O₃ catalyst, resulting in the catalytic performance of CO/toluene oxidation being improved significantly.

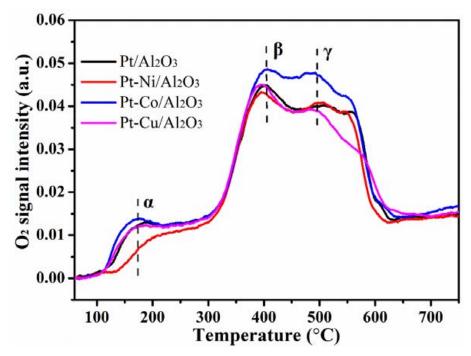


Figure 5. O₂-TPD profiles of these Pt/Al₂O₃ and Pt-M/Al₂O₃ samples.

3.7. Catalytic Activity Measurement

Figure 6 shows the catalytic activities for CO/toluene of Pt-based samples under different reaction conditions as a function of temperature, while the CO/toluene conversion plots were recorded at the heat preservation stage for 1.0 h. CO₂ and H₂O were the main products, while other by-products (below 1.0 ppm) were not detected. The catalytic activities of these samples were compared by using T₁₀, T₅₀, and T₉₉ (the catalytic temperatures of 10%, 50%, and 99% CO/toluene conversion, respectively) as a reference, as described in Table 3. It can be found that all the catalysts have more outstanding catalytic activities than Pt/Al₂O₃ (T₉₉ = 180 °C) for individual CO oxidation in Figure 6a, their T₉₉ values for CO oxidation were achieved at 160 °C with a WHSV of 60,000 mL g⁻¹ h⁻¹. For individual toluene oxidation, Pt-Co/Al₂O₃ catalyst exhibited an optimal catalytic activity among these Pt-based catalysts in Figure 6b, its T₁₀, T₅₀, T₉₉ are 160, 180, and 195 °C, respectively. However, the catalytic performance of bimetallic Pt-Ni/Al₂O₃ and Pt-Cu/Al₂O₃ catalysts for toluene oxidation was reduced, compared with the Pt/Al₂O₃ catalyst. However, when CO and toluene gases simultaneously exist in the reaction gases stream, the catalytic activities for CO and toluene oxidation over all the catalysts were

inhibited due to the competitive adsorption of CO and toluene on the same active sites, as shown in Figure 6c and d. In addition, it can be found that there was an inverse hysteresis in CO or toluene conversion during catalytic oxidation over Pt-Co/Al₂O₃ catalyst in Figure S2, which was due to exothermic combustion. The Pt/Al₂O₃ catalyst exhibited complete oxidation for CO and toluene co-existence at 200 °C. Among bimetallic Pt-M/Al₂O₃ catalysts, Pt-Co/Al₂O₃ catalyst exhibited a more excellent catalytic activity for CO and toluene oxidation in mixture conditions, while Pt-Ni/Al₂O₃ and Pt-Cu/Al₂O₃ catalysts displayed a poorer CO and toluene oxidation activity than the Pt/Al₂O₃ catalyst. The presence of toluene caused an obvious decrease in CO conversion due to competitive adsorption of both CO and toluene on the surface of catalysts. Moreover, Platinum atoms exposed on the surface of catalytic materials were often considered as the active site for controlling the catalytic oxidation of CO/toluene. The TOF values for CO/toluene co-oxidation at 190 °C have also been calculated in Figure 7. With the increased dispersity of Pt in bimetallic catalysts, the Pt-based catalysts would effectively increase the catalytic activity and TOF of each active site. Therefore, the Pt-Co/Al₂O₃ catalyst with the highest dispersity and TOF value exhibited the best catalytic performances for CO/toluene oxidation at a lower temperature.

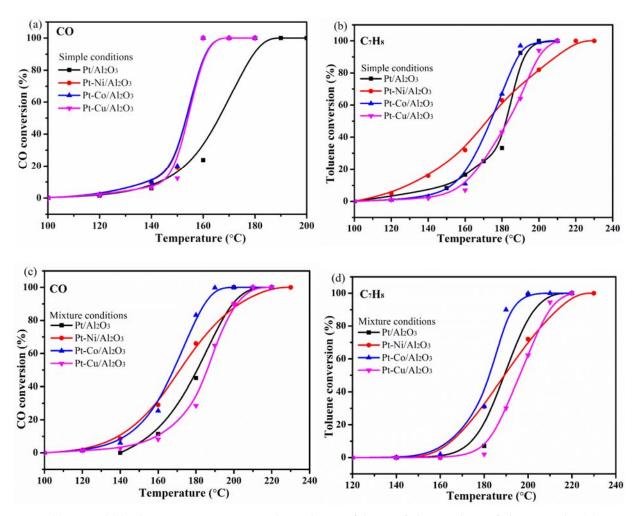


Figure 6. (a) CO and (b) toluene conversions in simple conditions of these Pt/Al_2O_3 and $Pt-M/Al_2O_3$ samples; (c) CO and (d) toluene conversion in mixture conditions of these Pt/Al_2O_3 and $Pt-M/Al_2O_3$ samples. Simple conditions: 1.0 vol.% CO or 1000 ppm toluene balanced with air; Mixture conditions: 1.0 vol.% CO and 1000 ppm toluene balanced with air. All the reactions were kept at WHSV = 60,000 mL g^{-1} h^{-1} .

0 1	Temperature	Simple Conditions			Mixture Conditions		
Sample	(°C)	T ₁₀ /°C	T ₅₀ /°C	T ₉₉ /°C	T ₁₀ /°C	T ₅₀ /°C	T ₉₉ /°C
Pt/Al ₂ O ₃	CO	144	169	180	155	180	200
	Toluene	150	182	200	176	190	200
Pt-Ni/Al ₂ O ₃	CO	140	155	160	139	172	220
	Toluene	130	172	220	166	190	220
Dr. C. / A1. O	CO	140	155	160	142	168	190
Pt-Co/Al ₂ O ₃	Toluene	153	174	195	165	182	200
Pt-Cu/Al ₂ O ₃	CO	143	156	160	160	185	210
	Toluene	158	185	210	182	198	220

Table 3. Catalytic activities of these Pt/Al₂O₃ and Pt-M/Al₂O₃ samples under different conditions.

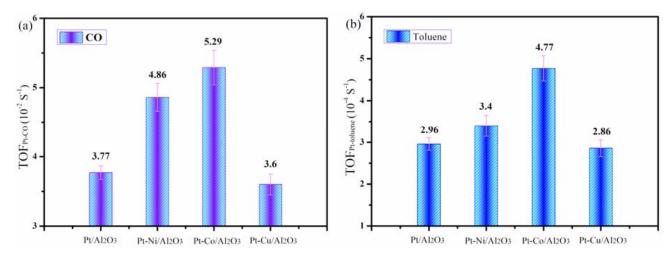


Figure 7. The TOF values for (**a**) CO and (**b**) toluene oxidation over these Pt/Al₂O₃ and Pt-M/Al₂O₃ samples at 190 °C under mixture conditions.

3.8. The Effects of WHSV and Moisture

The effect of WHSV on the catalytic activities of Pt-Co/Al $_2$ O $_3$ catalyst for CO/toluene oxidation was further investigated, as shown in Figure 8. With the increase in WHSV values, the catalytic activities of CO/toluene oxidation decreased. Under the condition of WHSV = 30,000 mL g $^{-1}$ h $^{-1}$, the temperature of complete oxidation for individual CO and toluene oxidation could be obtained at a temperature of 160 and 190 °C, respectively, whereas the T $_{99}$ values for CO and toluene oxidation in mixture conditions were about 170 and 190 °C, respectively. When the WHSV value was further increased to 120,000 mL g $^{-1}$ h $^{-1}$, the Pt-Co/Al $_2$ O $_3$ catalyst can completely degrade the CO and toluene at below 220 °C.

To simulate more realistic conditions, certain moisture was introduced into the simulated off-gas stream, which could obviously affect the catalytic performance of catalyst. The influence of moisture on the catalytic activities of the Pt-Co/Al₂O₃ catalyst for CO/toluene oxidation are showed in Figure 9. Surprisingly, it can be found that H₂O promotes the catalytic activities for CO/toluene oxidation over the Pt-Co/Al₂O₃ catalyst. In addition, the promoting effect of H₂O in individual CO/toluene oxidation is more remarkable than that in CO and toluene co-oxidation. For individual CO/toluene oxidation with moisture, Pt-Co/Al₂O₃ catalyst maintains full CO and toluene conversions at a temperature of 150 °C and 190 °C, respectively. Under the mixture conditions with moisture, the CO and toluene conversions would be mildly facilitated by moisture. Therefore, it can be seen from the experimental data that the Pt-Co/Al₂O₃ catalyst owns an excellent tolerance to H₂O in the oxidation process, and H₂O also have a similar promoting effect on other catalysts [44,46–48].

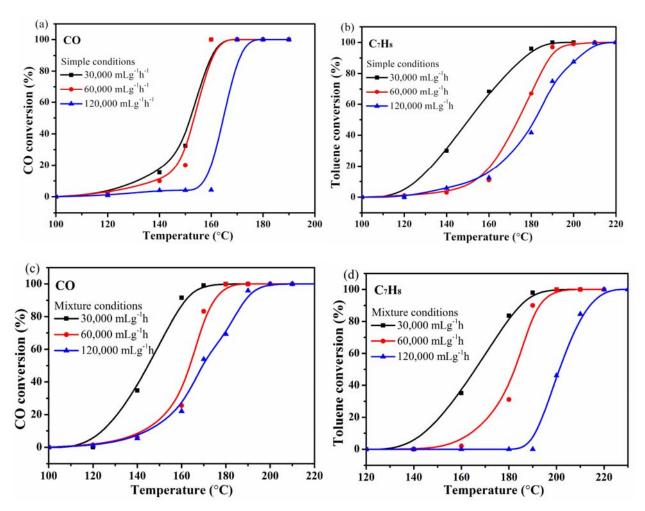


Figure 8. (a) CO and (b) toluene conversions in simple conditions, (c) CO and (d) toluene conversions in mixture conditions over the Pt-Co/Al₂O₃ catalyst under different WHSV.

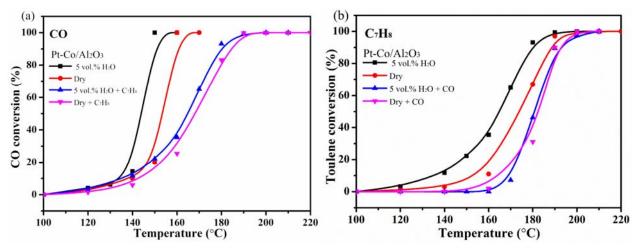


Figure 9. The effect of moisture on the (a) CO and (b) toluene conversions in different conditions over the Pt-Co/Al₂O₃ catalyst with a weight hourly space velocity (WHSV) = $60,000 \text{ mL g}^{-1} \text{ h}^{-1}$.

3.9. Catalytic Stability

Figure S3 shows an on-stream stability experiment for CO/toluene oxidation over the Pt-Co/Al $_2$ O $_3$ catalyst at different conditions under a WHSV of 60,000 mL g $^{-1}$ h $^{-1}$. During the long-term stability test for 48 h, the conversions of CO and toluene over the

Pt-Co/Al $_2$ O $_3$ catalyst under dry conditions at a temperature 200 °C were found to be 100% and 98% in Figure S3a, respectively, which were not significantly decreased. Besides, their CO and toluene conversions with or without H $_2$ O under mixture conditions at a temperature of 180 °C did not fluctuate significantly in Figure S3b. The above results manifest that the Pt-Co/Al $_2$ O $_3$ catalyst exhibits a relatively high catalytic activity for CO/toluene oxidation, good stability as well as high resistance to CO and hydrocarbon inhibition in the simulated exhaust stream, indicating that the Pt-Co/Al $_2$ O $_3$ catalyst can be well applied to CO and toluene co-oxidation.

4. Conclusions

In summary, we have successfully synthesized bimetallic Pt-M (M = Ni, Co, Cu) on alumina substrates via introducing inexpensive metal elements for the catalytic removal of CO and toluene co-existence. It can be found that introducing inexpensive metal elements into Pt/Al₂O₃ catalyst clearly changes the physico-chemical properties, anti-toxic abilities, and catalytic performances for CO and toluene co-oxidation. The catalytic evaluations of CO/toluene oxidation indicate that the Pt-Co/Al₂O₃ catalyst exhibits the best catalytic activity for complete CO and toluene oxidation ($T_{99/CO} = 160$ °C, $T_{99/toluene} = 200$ °C) under individual atmosphere among these Pt-based catalysts. Moreover, the bimetallic Pt- M/Al_2O_3 catalysts display identical catalytic performance ($T_{99/CO} = 160 \,^{\circ}$ C) for individual CO oxidation, which is higher than the Pt/Al₂O₃ catalyst. For CO and toluene cooxidation, the Pt-Co/Al₂O₃ catalyst also had the lowest temperature, and CO and toluene have competitive adsorption at the active sites of catalysts. Importantly, H₂O promotes the catalytic activities for CO/toluene oxidation over the Pt-Co/Al₂O₃ catalyst due to excellent tolerance to H₂O. According to the catalytic and characterization analysis, it can be seen that Pt-Co/Al₂O₃ catalyst with superior activity has the highest turnover frequency (TOF) for CO/toluene conversion and the well dispersity of Pt particles. In addition, the catalytic performance is related to the Pt particle size, metal species, more surface adsorption oxygen, and well redox ability. However, the pathway introducing Ni and Cu elements into Pt/Al₂O₃ to prepare Pt-Ni/Al₂O₃ and Pt-Cu/Al₂O₃ do not achieve the desired goal of increasing catalytic activity for simultaneous CO and toluene oxidation and the synthesis of Pt-based catalysts decorating a low content of Co metal element is a useful method to improve Pt-metal utilization in the CO and toluene oxidation.

Supplementary Materials: The following are available online at https://www.mdpi.com/2227-9 717/9/2/230/s1, Figure S1: XRD patterns of as-synthesized Pt/Al₂O₃ and Pt-M/Al₂O₃ samples, Figure S2: Hysteresis in CO/toluene conversion during catalytic oxidation over Pt-Co/Al₂O₃ catalyst, Figure S3: Long-term stability test for (a) individual CO/toluene oxidation under dry condition and (b) CO/toluene co-oxidation under mixture condition over the Pt-Co/Al₂O₃ catalyst, respectively.

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Conflicts of Interest: The authors declare no conflict of interest.

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Article

High Temperature Adsorption of SO₂ on Mixed Oxides Derived from CaAl Hydrotalcite-Like Compounds

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Abstract: SO_2 which is usually emitted at high temperature is one of the most important air pollutants. It is of great significance to develop high temperature SO_2 adsorbent with high efficiency and low cost. In this work, a series of hydrotalcite-like compound-derived CaAlO and CaXAlO (X = Ce, Co) were prepared by coprecipitation and calcination method, and were employed as adsorbents for SO_2 adsorption at high temperature ($700\,^{\circ}$ C). The structure and surface properties of these adsorbents were characterized by XRD, Brunauer–Emmett–Teller (BET), Derivative thermogravimetric analysis (DTG) and CO_2 -TPD (temperature programmed desorption) measurement. Addition of a minor amount of Ce, Co (5 wt%) could significantly increase the number of weak alkalinity sites. CaO in CaCeAlO showed the best SO_2 adsorption capacity of 1.34 g/g, which is two times higher than that of CaO in CaAlO (0.58 g/g).

Keywords: hydrotalcite-like compounds; SO2; CaAlO; high temperature adsorption

1. Introduction

 SO_2 is regarded as one of the most important air pollutants due to its contribution to acid rain formation and direct threat to public health. Therefore, restricting SO_2 emissions from coal/oil combustion sources is of great importance. In most cases, SO_2 emitted from such sources is accompanied with high temperature, for instance the temperature of SO_2 emitted from power plant does not exceed 200 °C. During the fluid catalytic cracking (FCC) process in the oil refining enterprises, about 5–10% of feed sulfur originated with crude oil is converted to SO_X ($SO_2 \geq 90\%$) and emitted with high temperature (650–700 °C) and high concentration (around 2000 ppmv, in China), which accounts for about 5% or even higher of total SO_2 emission [1]. At present, with the increase in throughput of FCC units and sulfur content in crude oil, the problem of SO_2 pollution is becoming more and more prominent. It is urgent to control SO_2 emitted from such sources characterized with high temperature and high concentration.

Materials such as activated carbons, activated carbon fibers, and fly ash were usually employed in previous studies [2–5]. However, SO_2 storage capacity on these materials is limited and those studies were often carried out at low temperature, and these physical adsorption methods are often inapplicable at high temperature. Thus, it is important to develop efficient and inexpensive adsorbents for high temperature SO_2 adsorption and storage.

Hydrotalcite-like compounds (HTlcs) are known as anionic clay or layered double hydroxides and could be expressed as M_{1-x}^{2+} M_x^{3+} (OH)₂ A_x .nH₂O [6,7], where M^{2+} and M^{3+} represent most divalent and trivalent metal ions, respectively. Owing to the considerable selection of M and A, a wide variety of HTlcs could be synthesized and

used for different application [8]. For SO₂ control at higher temperatures like in the FCC process, MgAlO is widely used with the addition of other elements at laboratory scale [9–13].

In our previous studies, we found that the addition of Ca led to a notable increase in pollutant adsorption capacity [14,15]. Here, based on the fact that CaO is widely used for SO_2 emission control, and that Ca and Mg belong to the same group but the alkalinity of Ca is stronger than that of Mg, it can be concluded that the Ca replacing MgAlO will have excellent SO_2 adsorption performance.

In this article, to test the adsorption capacity of Ca-based mixed metal oxides at high temperature, HTlcs-derived CaAlO was prepared and employed as adsorbent for the SO_2 adsorption experiments at 700 °C. Moreover, high temperature SO_2 adsorption is a chemical adsorption process involving chemical oxidation, so the absorption process could be effectively improved by increasing the amount of reactive oxygen species on the adsorbent surface. Ce and Co are two commonly used transition metal elements in catalytic reactions, which can promote the improvement of oxygen storage capacity of metal oxide materials. Therefore, typical metals like Ce and Co were added to CaAlO to study their effect during the SO_2 adsorption process.

2. Materials and Methods

Materials preparation: CaAl and CaXAl-HTlcs (X = Ce, Co) were synthesized using the coprecipitation method. As for the CaAl-HTlcs, a mixed salt solution containing $Ca(NO_3)_2 \cdot 4H_2O$ (>99%), Al(NO₃)3·9H₂O (>99%), and a solution of NaOH (>96%) and NaNO₃ (>99.8%) were prepared separately with distilled water. After dissolution, the mixed Ca-Al salt solution was added dropwise into the NaOH-NaNO₃ solution under vigorous mechanical stirring with N₂ protection. The precipitate was aged at 80 °C for 24 h, and then the precipitate was thoroughly washed and filtered. The filter cakes of precipitate were dried at 100 °C overnight. The synthesized CaXAl-HTlcs (X = Ce, Co, 5 wt%) were calcined at 800 °C for 4 h to obtain the corresponding HTlcs-derived mixed oxides, which are denoted as CaAlO and CaXAlO (X = Ce, Co). The oxides were then crushed and sized in 20–40 meshes for SO₂ adsorption measurement.

Material characterization: The X-ray diffraction (XRD) patterns of precursors and the derived mixed oxides were recorded on a Rigaku TTR2 powder diffractometer by using Cu K α radiation ($\lambda = 0.154$ nm) with a 20 range of 5–70° at a scanning rate of 4°/min. The tube voltage and current were set at 40 kV and 20 mA, respectively. Thermal decomposition behaviors of as-prepared HTlcs were investigated with Derivative thermogravimetric analysis (DTG) (Seteram, Labsys). In a typical measurement, 20-30 mg of HTlcs sample was heated in a ceramic crucible at a heating rate of 10 °C/min from room temperature to 800 °C, with N₂ purging at a flow rate of 30 mL/min. Textural properties of derived mixed oxides were analyzed by N₂ adsorption/desorption at liquid-nitrogen temperature (77 K) using a gas adsorption analyzer (Quantachrome NOVA-1200). The specific surface area (SSA) was calculated by the Brunauer–Emmett–Teller (BET) equation. The pore volume and pore size distribution were obtained with the Bopp-Jancso-Heinzinger (BJH) method. CO₂-TPD (temperature programmed desorption) was taken by a chemical adsorption instrument (Micromeritics 2720) to characterize the alkalinity adsorption sites of these mixed metal oxides. A total of 50 mg of mixed metal oxide sample was put into a U-type quartz tube, after pretreatment, a stream of 20% CO_2/He (v/v) was introduced for 2 h to reach adsorption saturation, and then the sample was heated at a heating rate of 10 $^{\circ}$ C/min from room temperature to 800 $^{\circ}$ C with He purging at a flow rate of 50 mL/min.

 SO_2 adsorption test: Thermal SO_2 adsorption experiments were carried out in a quartz fixed-bed flow-reactor (i.d. = 6 mm and L = 600 mm) using 0.5 g oxide sorbent (20–40 mesh powder) at atmospheric pressure. The oxide sorbent was pretreated from room temperature to 700 °C with N_2 flowing at 40 mL/min. After stabling for 30 min, N_2 flow was shut off and a stream mixture of SO_2 and air with 0.5% SO_2 at a total flow rate of 50 mL/min was passed through the fixed bed. The sorbent bed was heated by a

tubular furnace, and the temperature was monitored with a thermocouple which was inserted into the bed. The concentration of SO_2 at the outlet was monitored online by an auto-sampling gas chromatograph (GC) which equipped with a Flame photometric detector (FPD), until the concentration reached the origin inlet level of 0.5%. The SO_2 adsorbed on the sample was calculated by the following formula

$$W_{SO_2} = \int_0^t kcidt \tag{1}$$

where ci means the SO_2 concentration at i minutes, and k is the constant, which is calculated by the flow volume, M_{SO_2} , and the mole volume constant.

The saturated adsorption was calculated as

$$W = W_{SO_2}/W_{sorbent} (g/g)$$
 (2)

3. Results and Discussion

Structure of HTlcs and Derived Oxides

Figure 1a shows the X-ray diffraction patterns of CaAl-HTlcs and CaXAl-HTlcs (where X = Ce, Co) which was obtained by drying the filter cake at 100 °C. All the precursors exhibited the typical X-ray diffractogram of hydrotalcite. The peaks at $2\theta = 10^{\circ}$, 21° , 39° corresponding to the (003), (006), and (009) crystal planes indicate the well-formed crystalline layered structure with a rhombohedral symmetry (3R) [16]. The in-plane X-ray diffractions from planes (110) and (113) at 31° and 32° reveal a good dispersion of metal ions in the hydroxide layers [14]. Compared with CaAl-HTlcs, the peaks of CaXAl-HTlcs become stronger, which indicates the better crystallinity. In this study, to avoid the formation of CaCO₃, the metal nitrates were employed instead of the carbonates and the N_2 protection was also introduced during the titration. Therefore, these HTlcs were synthesized successfully and no CaCO₃ (JCPDS 85-1108) were found [17,18].

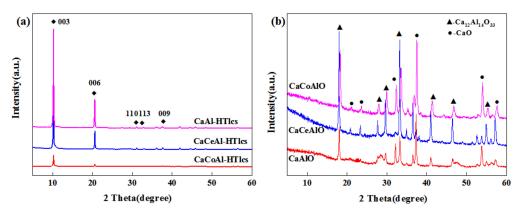


Figure 1. XRD patterns of (a) prepared hydrotalcite-like compounds (HTlcs) and (b) derived metal oxide sorbents.

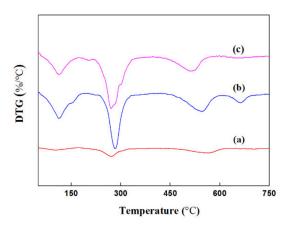
Figure 1b describes the XRD patterns of the obtained mixed metal oxides which were derived from the corresponding HTlcs by the calcination process, which mainly contains dehydration, dehydroxylation, and loss of compensating anions, and leads to acidic or basic mixed oxides. No spinel phase was observed; it can be inferred that during the dehydroxylation and loss of compensating anions processes, Ca could not be melt with Al to form the spinel phase. In fact, CaO (JCPDS 48–1467), marked with \bullet in Figure 1b and Ca₁₂Al₁₄O₃₃ (JCPDS 09-0413), marked with \blacktriangle in Figure 1b were observed in those samples. Here, it can be deduced that Ca₁₂Al₁₄O₃₃ acts a support/binder to disperse the CaO. Among those samples, no obvious peaks single X oxide (where X = Ce, Co) were found, indicating the good dispersion of these metal oxides. The specific surface area, mean pore diameter, and total pore volume were tabulated in Table 1. Obviously, the slight addition of other metals affects the SSA, pore size, and pore volume. Compared with CaAlO, these

parameters values of CaXAlO (X = Ce, Co) samples are lower. Generally, the interparticle pore diameter calculated fell in the range of 15.6–20.2 nm. According to a previous study [19], gas molecule diffusion in such pores could not be the rate-determining step for the gas adsorption.

Table 1. Textual property and SO ₂ adsorption amount of CaO in oxide s
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Sample	SSA(m ² /g)	Pore Size (nm)	Pore Volume (cm ³ /g)	Adsorption Amount (g/g)
CaAlO	30.8	20.2	0.16	0.28
CaCoAlO (Co = 5 wt%)	19.9	15.6	0.08	0.40
CaCeAlO (Ce = 5 wt%)	24.4	19.3	0.12	0.67

In Figure 2, DTG curves present the weight loss rate of these HTlcs during heating in the air. In general, thermo-gravimetric loss during heating involves two or three steps [20]. The first step occurs at 50-200 °C, mainly ascribed to the loss of surfaceadsorbed and interlayer water molecules. The second stage takes place at 200-500 °C, including the dehydroxylation of layer hydroxyl groups and decomposition of interlayer nitrate, causing collapse of the layer structure. In this study, there were three observed peaks of CaAl -HTlcs and CaXAl-HTlcs samples under 600 °C, falling in the range of 50–180 °C, 240–330 °C, and 450–600 °C, respectively. Considering that the loss of OH usually occurred under 200-500 °C and the anion removal temperature of nitrate is higher than 500 °C, it is concluded that the peaks in the range of 50–180 °C, 240–330 °C, and 450–600 °C refer to the loss of H₂O, OH⁻, and NO³⁻, respectively. Compared with CaAlO, the addition of Ce and Co promotes the dehydroxylation temperature (about 5–20 $^{\circ}\mathrm{C}$ higher) and facilitates the decomposition of NO³⁻ (about 10–40 °C lower). It is noted that for the CaCeAlO sample, an obvious peak at 663 °C was observed. We assume that the addition of Ce could remarkably promote the condensation during the transformation from CaAl-HTlc to CaAlO.



 $Figure \ 2. \ \mathsf{DTG} \ \mathsf{profiles} \ \mathsf{of} \ \mathsf{the} \ \mathsf{precursors} \ \mathsf{HTlcs:} \ (a) \ \mathsf{CaAl\text{-}HTlc}, \ (b) \ \mathsf{CaCeAl\text{-}HTlc}, \ \mathsf{and} \ (c) \ \mathsf{CaCoAl\text{-}HTlc}.$

CO2-TPD tests were conducted to characterize the alkalinity of those samples and shown by Figure 3. There were four peaks observed for CaAlO and CaXAlO samples, the first peak represents the weak alkaline sites (<200 °C), the second peak corresponds to the mid-strong alkaline sites (200–400 °C), and the third and the fourth belong to the high temperature peaks, referring to the strong alkaline sites (>400 °C). Compared with CaAlO, the alkalinity of strong alkaline sites of CaCeAlO and CaCoAlO are weaker in that the peak temperature decreased from 628 °C (CaAlO) to 595 °C (CaCeAlO) and 602 °C (CaCoAlO) and the sites numbers characterized by integration area also decrease about 8% and 33% for CaCeAlO and CaCoAlO, respectively. The similar pattern was also observed for the strong alkaline sites in the range of 350–500 °C. As for the weak alkaline sites, the site numbers of CaCeAlO and CaCoAlO were at the same level, about two times those

of CaAlO. The peaks of those weak alkaline sites appeared around $100\,^{\circ}$ C, indicating the adsorption of SO_2 over CaCeAlO and CaCoAlO samples, which would favor further chemical adsorption at high temperature. The adsorption of SO_2 is generally a chemical adsorption process, which includes a series of steps, such as surface diffusion and pore diffusion of SO_2 and chemical reaction occurring on active sites, to form products of sulfate finally [15].

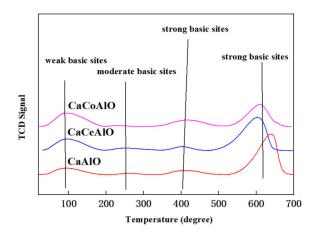


Figure 3. CO₂-TPD profiles of the oxide sorbents.

Figure 4 shows the typical adsorption breakthrough curves of SO_2 over the oxide sorbents. All oxide sorbents seemingly follow a similar sorption patter. As shown in Figure 4, SO_2 adsorption mainly could be divided into three stages. In the initial stage, 5000 ppm SO_2 was completely adsorbed, lasting about 70, 90, and 150 min, for the CaAlO, CaCoAlO and CaCeAlO, respectively. After the initial stage, the SO_2 concentration increases rapidly in the next 60–90 min. Afterward, the increase of SO_2 slows down and finally reaches the initial level of 5000 ppm, indicating that SO_2 is no longer adsorbed on those adsorbents.

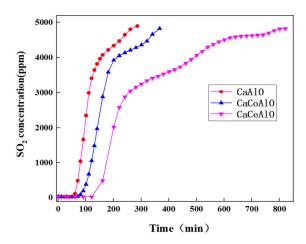


Figure 4. SO₂ adsorption on CaAlO, CaCoAlO and CaCeAlO at 700 °C.

Table 1 lists the SO_2 sorption amounts of all oxides. It is well-known that CaO can quickly capture and strongly hold SO_2 in the calcium sulfate form. It is assumed that the active sites and SO_2 affinity of the oxide sorbent are determinant. In CaAlO and CaXAlO samples, the CaO content was calculated by titration method. Where the mixed samples were resolved by ethylene glycol together with bromocresol green-methyl red mixed indicator solution and determined by HCl titration. The results show that CaO is about 50 wt% of CaAlO and CaXAlO samples. Considering CaO and $Ca_{12}Al_{14}O_{33}$ are formed in

the same process, the dispersion of CaO in CaXAlO might be better that of CaAlO, which could lead to the better contact with SO₂ and result in better adsorption.

Theoretically, 1.14 g SO₂ could be absorbed on 1 g CaO at 100% conversion. In this study, CaO (50 wt%) was mixed with $Ca_{12}Al_{14}O_{33}$ in CaAlO and CaXAlO samples. Therefore, the theoretical maximum SO₂ absorption capacity of CaO will be two times that of these samples. For CaAlO, CaCoAlO, and CaCeAlO samples, the SO₂ absorption capacity is 0.28g/g, 0.40 g/g, and 0.67 g/g, respectively, which correspond to 0.56 g/g, 0.80 g/g, and 1.34 g/g for the adsorption capacity of contained CaO, respectively. It is noted that the SO₂ adsorption in CaCeAlO is higher than the maximum value of 1.14 g/g, suggesting that in the surface of CaCeAlO, one CaO molecule might not absorb only one SO₂ molecule, it might absorb two or even more SO₂ molecules. Addition of a minor amount of Ce, Co (5 wt%) could lead to good dispersion of metal oxide and obviously increase the SO₂ adsorption. In this study, the SO₂ adsorption of CaAlO, CaCoAlO, and CaCeAlO was carried out on fixed-bed flow-reactor, which is closer to the actual situation.

4. Conclusions

CaAl-HTlcs and CaXAlO (X = Ce, Co) were prepared by metal nitrates through coprecipitation method, and the corresponding mixed metal oxide XCaAlO, CaXAlO (X = Ce, Co) were obtained after calcination. The samples were characterized by XRD, BET, DTG, and CO₂-TPD, and the high temperature SO₂ adsorption capacity was measured at 700 °C. The results indicated that Ca was successfully introduced into HTlcs system and CaO was well mixed with Ca₁₂Al₁₄O₃₃ in the CaAlO samples. Introduction of Ce and Co into CaAlO could significantly increase the number of weak alkalinity sites, which have an important effect on the SO₂ adsorption rather than the pore structure parameters. The adsorption of SO₂ by CaCeAlO was 0.67 g/g, and the adsorption of SO₂ by CaO in the CaCeAlO showed a maximum value of 1.34 g/g, suggesting the super adsorption capacity.

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Article

Preparation of K Modified Three-Dimensionally Ordered Macroporous MnCeO_x/Ti_{0.7}Si_{0.3}O₂ Catalysts and Their Catalytic Performance for Soot Combustion

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Abstract: Soot particles in diesel engine exhaust is one of the main reasons for hazy weather and elimination of them is urgent for environmental protection. At present, it is still a challenge to develop new catalysts with high efficiency and low cost. In this paper, a kind of K modified three-dimensionally ordered macroporous (3DOM) MnCeO $_{\rm X}$ /Ti $_{0.7}$ Si $_{0.3}$ O $_{2}$ catalysts are designed and synthesized by a sample method. Due to the macroporous structure and synergistic effect of K, Mn, and Ce, the K $_{\rm n}$ MnCeO $_{\rm x}$ /Ti $_{0.7}$ Si $_{0.3}$ O $_{2}$ (K $_{\rm n}$ MnCeO $_{\rm x}$ /M-TSO) catalysts exhibit good catalytic performance for soot combustion. The catalytic activity of K $_{0.5}$ MnCeO $_{\rm x}$ /M-TSO was the best, and the T $_{10}$, T $_{50}$, and T $_{90}$ are 287, 336, and 367 °C, respectively. After the prepared catalyst was doped with K, the physicochemical properties and catalytic performance changed significantly. In addition, the K $_{0.5}$ MnCeO $_{\rm x}$ /M-TSO catalyst also somewhat exhibits sulfur tolerance owing to it containing Ti. Because of its simple synthesis, high activity, and low cost, the prepared K $_{\rm n}$ MnCeO $_{\rm x}$ /M-TSO catalysts are regarded as a promising candidate for application.

Keywords: 3DOM structure; K_nMnCeO_x/M-TSO; soot combustion; catalysts

1. Introduction

Diesel engines have been widely used in automobile, ship, light truck, heavy machinery, and other fields because of its excellent thermal efficiency and durability [1,2]. However, diesel engines are also considered to be one of the major sources of soot particles emission and a cause of hazy weather [3,4]. With increasing awareness of environmental protection, the standards on exhaust emission of diesel engines have become increasingly stringent. Therefore, it is urgent to eliminate soot particles to meet emission standards. Nowadays, post-treatment technology is considered to be one of the effective ways to eliminate soot particles. However, since the spontaneous combustion temperature of soot particles (550–650 $^{\circ}$ C) is higher than the exhaust temperature of the diesel engine (150–450 $^{\circ}$ C), the development of new catalysts with low cost and excellent catalytic performance is one of the main challenges in the application of post-treatment technology [5,6].

At present, owing to three-phase gas(O₂)-solid(soot)-solid(catalyst) reaction for soot combustion, various catalysts were prepared to improve the contact efficiency between soot and catalyst [7,8]. Different morphologies of catalysts with nanotube array, nanobelt, nanofiber, nanowire, disordered macropore, and 3DOM structures are studied to enhance effective contact [9–14]. Among the above morphologies, due to the interconnected macroporous structure with large pore diameter (>50 nm) and low diffusion resistance, the 3DOM catalyst has enough migration space for soot particles in its internal pores, which are expected to show excellent catalytic ability [15–17]. Many previous studies have

shown that the catalytic performance of 3DOM oxide-based catalysts for soot combustion is superior to that of corresponding nanoparticle catalysts due to their structural effects [18–20]. To improve the intrinsic activity, a series of 3DOM oxides-supported Au and Pt catalysts have also been prepared in our research group, and the prepared 3DOM oxides-supported noble metal catalysts exhibit excellent catalytic ability in soot combustion reaction [21–23]. However, it is unsatisfactory that the application of noble metals is restricted by their high cost.

In recent years, considering the economy of catalyst cost, a number of rare earth oxides and transition metals have been studied for soot combustion [20,24–26]. MnO_x-CeO₂ mixed oxides with Mn and Ce synergistic effects have become one of the low cost and high performance catalysts [27–30]. In addition, alkali metals, especially potassium (K), exhibit excellent catalytic ability in soot combustion reaction. However, because of the low melting point of K, K-contained catalysts have weak thermostability in repeated cycles. To improve the stability of K-based catalysts, the incorporation of K into other stable structures is considered to be a promising way to resolve the problem of thermostability, and many kinds of K-doped catalysts have been reported by previous literature [31–33]. However, how to effectively combine the good contact efficiency of 3DOM structure and high catalytic activities of K, Mn, and Ce in one system of catalysts is also a research hotspot in the design and preparation of catalysts [34,35].

In this paper, a series of K-modified 3DOM MnCeO $_{\rm x}/{\rm Ti_{0.7}Si_{0.3}O_2}$ catalysts were synthesized by a simple preparation method. The catalysts have 3DOM structure and three active components of K, Mn, and Ce. The physicochemical properties of the asprepared catalysts were characterized by X-ray diffraction (XRD), scanning electron microscopy (SEM), temperature-programmed reduction with H $_2$ (H $_2$ -TPR), temperature-programmed desorption with O $_2$ (O $_2$ -TPD), temperature-programmed oxidation with NO (NO-TPO), etc. The effect of macropore structure combined with the synergistic effect of K, Mn, and Ce is expected to improve the catalytic ability of the synthesized catalyst in soot combustion reaction.

2. Experimental Section

2.1. Catalysts Preparation

2.1.1. Synthesis of Highly Well-Defined PMMA Microspheres

Monodispersed polymethyl methacrylate (PMMA) microspheres were synthesized by the emulsifier-free emulsion polymerization method with potassium persulfate (KPS) as the initiator and methyl methacrylate (MMA) as the raw material. Ordered macroporous templates were prepared by centrifugal precipitation self-assembly method. The preparation method was reported in our previous work [36].

2.1.2. Synthesis of 3DOM Ti_{0.7}Si_{0.3}O₂

3DOM $Ti_{0.7}Si_{0.3}O_2$ was prepared by the colloidal template method. Tetrabutyl titanate, tetraethyl orthosilicate (TEOS), HCl, H₂O, and ethanol were weighed according to a certain stoichiometric ratio and magnetically stirred for 3 h to obtain a homogeneous and clarified solution. The PMMA crystal template was immersed in the precursor solution for 1 h. After suction filtration and drying, the PMMA colloidal template was removed by calcination with air in a tubular furnace. The heating rate was 1 $^{\circ}$ C/ min, it was calcined at 310 $^{\circ}$ C for 3 h, and then heated to 600 $^{\circ}$ C and subsequently calcined for 4 h.

2.1.3. Synthesis of K Modified 3DOM MnCeO_x/Ti_{0.7}Si_{0.3}O₂

The 3DOM MnCeO $_{\rm x}/{\rm Ti}_{0.7}{\rm Si}_{0.3}{\rm O}_2$ catalysts were synthesized by the incipient wet impregnation method. The raw materials and amount of catalyst preparation are listed in Table 1. Ce(NO $_3$) $_3\cdot6{\rm H}_2{\rm O}$, 50% Mn(NO $_3$) $_2$, and KNO $_3$ solution were dissolved in water, and the total volume was about 2 mL. The impregnated 3DOM Ti $_{0.7}{\rm Si}_{0.3}{\rm O}_2$ was treated by ultrasonic for 15 min and dried at 80 °C for 12 h. The dried solid was calcined at 550 °C

for 4 h to obtain 3DOM $K_nMnCeO_x/Ti_{0.7}Si_{0.3}O_2$. To easily express the prepared catalysts, the 3DOM $Ti_{0.7}Si_{0.3}O_2$ is abbreviated by M-TSO.

Table 1. Expression of catalyst and amount of raw materials.

Catalysts	KNO ₃ /g	Mn(NO ₃) ₂ /g	Ce(NO ₃) ₃ /g	3DOM TiSiO/g	3DOM SiO ₂ /g
MnCeO _x /M-TSO	0	0.823	0.998	0.5	_
$K_{0.1}MnCeO_x/M-TSO$	0.023	0.823	0.998	0.5	_
$K_{0.3}MnCeO_x/M-TSO$	0.070	0.823	0.998	0.5	
$K_{0.5}MnCeO_x/M-TSO$	0.116	0.823	0.998	0.5	
$K_{0.7}MnCeO_x/M-TSO$	0.163	0.823	0.998	0.5	_
$K_{0.9}$ MnCeO _x /M-TSO	0.209	0.823	0.998	0.5	_
$K_1MnCeO_x/M-TSO$	0.232	0.823	0.998	0.5	_
$K_{0.5}MnCeO_x/M-SiO_2$	0.046	0.329	0.399	_	0.2

2.2. Physical and Chemical Characterization

XRD spectrum was obtained using the Rigaku Ultima IV X-ray diffractometer with Cu K α radiation. The scanning range was 10–90° and the scanning speed was 10°/min. The phase identification of the catalyst was performed by comparing with the reference data of ICPDS.

The surface morphology and pore structure of the catalyst were observed by the Hitachi SU8010N scanning electron microscope under 1 V–5 kV accelerating voltage. To improve the quality of SEM photos, the samples were treated by spraying gold.

The specific surface area, pore size, and pore volume of the catalyst were determined by BET technique using the Micromeritics TriStar II: 3020 specific surface analyzer. The samples were analyzed after degassing at 300 °C for 3 h.

 $H_2\text{-}TPR$ measurements were performed by the Micromeritics AutoChem II 2920 Chemical Adsorption Instrument. The sample was first purged with argon at 300 °C for 1 h, and then dropped to room temperature. After switching the gas flow to a hydrogen argon mixture, the instrument rose to 850 °C (heating rate was 10 °C/min) and the thermal conductivity detector (TCD) was used to monitor H_2 consumption signals.

 O_2 -TPD was determined by the TP-5076 adsorption instrument. The 100 mg sample was pretreated in O_2 atmosphere at 300 °C for 1 h, and then dropped to room temperature. The flow rate was switched to He flow (60 mL/min), and the temperature was raised to 900 °C at a heating rate of 10 °C/min. TCD was used to monitor desorption oxygen.

NO-TPO measurements were performed by the NO $_{\rm X}$ Analyzer nCLD 62. After pretreatment of 0.1 g catalyst in argon atmosphere at 200 °C for half an hour, the reaction gas was changed. The total flow rate was 50 mL/min, containing 1000 ppm NO, 10% O $_{\rm 2}$, and the rest was argon. The temperature program was set to rise from 50 °C to 600 °C at a heating rate of 2 °C/min. The instrument can monitor the content of nitrogen oxides in the outlet gas in real time.

2.3. Catalytic Activity Measurements

The catalytic activity of catalysts for soot combustion was evaluated by temperature programmed oxidation (TPO) in a fixed bed tubular quartz reactor (Φ = 8 mm). The model soot was Printx-U particulates (25 nm diameter, purchased from Degussa, Frankfurt, Germany). The elemental composition of Printx-U particles was 94.2% C, 3.1% O, 0.8% H, 0.4% S, 0.2% N, and 4.7% others [37]. Measures of 0.01 g of soot and 0.1 g of catalyst were weighed and mixed uniformly at a mass ratio of 1:10 to simulate loose contact conditions, and then they were loaded into the quartz reactor. The reaction gas (50 mL/min) included 10% O₂, 2000 ppm NO, and the rest was argon. We set the heating program from 100 °C to 650 °C, with a heating rate of 2 °C/min. The main components of the outlet gas were N₂, NO_x, CO₂, and CO. The outlet gas compositions were analyzed by an online gas chromatograph (GC, Agilent 7890B) equipped with a flame ionization detector (FID).

Complete conversion of CO and CO_2 to CH_4 over nickel catalyst was maintained at 380 °C before entering FID. The temperature T_{10} , T_{50} , and T_{90} of 10%, 50%, and 90% conversion of soot particles can be used to evaluate the catalytic activity. The selectivity of CO_2 is another essential standard for evaluating the catalytic combustion of soot. Equation (1) was the calculation method applied.

$$S^{m}{}_{CO_{2}} = \frac{[CO_{2}]_{out}^{max}}{[CO_{2}]_{out}^{max} + [CO]_{out}^{max}} \times 100\%$$
 (1)

 $[CO_2]_{out}^{max}$ and $[CO]_{out}^{max}$ are, respectively, expressed as the concentration of CO_2 and CO in the reaction product when the reaction temperature is the peak temperature, and $S^m_{CO_2}$ is the selectivity of CO_2 when the soot combustion rate is the fastest.

Other reaction conditions remain constant; the sulfur resistance of the catalyst to soot combustion was tested by changing the gas composition of the reaction gas. The total gas flow rate was $50 \, \text{mL/min}$, containing $100 \, \text{ppm}$ or $300 \, \text{ppm}$ SO₂, $10\% \, \text{O}_2$, $2000 \, \text{ppm}$ NO, and the rest was argon.

3. Result and Discussion

3.1. Structural Features of the Synthesized Catalysts

3.1.1. XRD Patterns of the Prepared Catalysts

The XRD patterns of K_nMnCeO_x/M-TSO catalysts with different K doping amounts, M-TSO support, and K_{0.5}MnCeO_x/M-SiO₂ are shown in Figure 1. For M-TSO support, the pattern peak for 2θ of $25.4^{\circ}(101)$ belongs to anatase TiO_2 (marked by " \clubsuit " in Figure 1a; JCPDS Card No. 21-1272) [38–40]. As shown in Figure 1b, MnCeO_x/M-TSO catalyst exhibits four feature peaks, which are located at 2θ of $28.8^{\circ}(111)$, $33.5^{\circ}(200)$, $47.6^{\circ}(220)$, and 56.8°(311) (marked by "\Lambda" in Figure 1b), and these correspond to diffraction peaks of CeO₂. However, the peak of anatase TiO₂ disappeared, which is related to coverage of M-TSO surface by MnCeO_x oxides. It can be seen from Figure 1c-h that the XRD patterns of K_nMnCeO_x/M-TSO catalysts also belonged to the CeO₂ crystal structure when the K was doped into MnCeO_x/M-TSO. However, compared with reported crystal structure of pure CeO₂ (JCPDS Card No. 43-1002), a slight shifting towards a higher diffraction angle of 2θ was observed on K_nMnCeO_x/M -TSO catalysts, in which the 2θ was shifted from 28.5 to 28.8° for the crystal face of (111) [41,42]. In addition, Figure 1c-h also exhibits that no feature peaks of KNO_3 , KO_x , or MnO_x can be observed. The above phenomena indicate that due to the large lattice spacing of CeO₂, K and Mn have been doped into the lattice of CeO₂. It can be seen from Figure 1i that the XRD pattern of the $K_{0.5}MnCeO_x/M-SiO_2$ catalyst also belongs to the CeO_2 crystal structure.

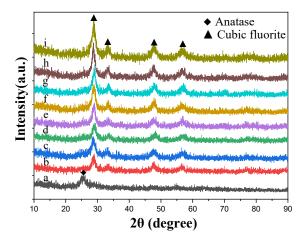


Figure 1. XRD patterns of prepared catalysts (**a**: M-TSO; **b**: MnCeO_x/M-TSO; **c**: $K_{0.1}$ MnCeO_x/M-TSO; **d**: $K_{0.3}$ MnCeO_x/M-TSO; **e**: $K_{0.5}$ MnCeO_x/M-TSO; **f**: $K_{0.7}$ MnCeO_x/M-TSO; **g**: $K_{0.9}$ MnCeO_x/M-TSO; **h**: K_{1} MnCeO_x/M-TSO; **i**: $K_{0.5}$ MnCeO_x/M-SiO₂).

3.1.2. SEM Images of the Catalysts

Figure 2 is the SEM images of prepared catalysts. Figure 2a indicates that macroporous structures can be well observed in the M-TSO support. The diameters of the macropores are about 290–330 nm and the wall thicknesses of macropores are about 30–50 nm. Meanwhile, three small pores with diameter of 80–120 nm, which formed in the contact area of two PMMA spheres, can be also obtained in a macropore, and they are interconnected with other adjacent macropores [43]. When the MnCeO_x and K_nMnCeO_x are loaded on the M-TSO support, the pore structure of MnCeO_x/M-TSO and K_nMnCeO_x/M-TSO are well maintained (Figure 2b–e). The SEM results indicate that the loading processes of MnCeO_x and K_nMnCeO_x do not destroy the pore structure of M-TSO support, and also demonstrate that the 3DOM structure of the M-TSO support is stable and strong. As shown in the SEM image of Figure 2, the prepared catalyst has uniform pore sizes, which are arranged highly periodically and connected through small windows [44]. The ordered pore structures are beneficial to improving catalyst-soot contact efficiency.

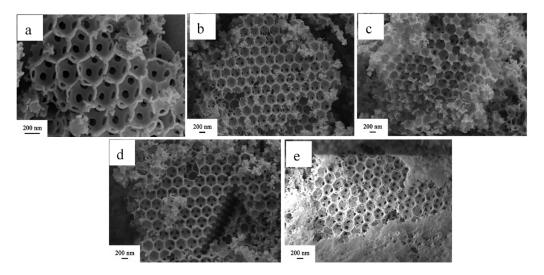
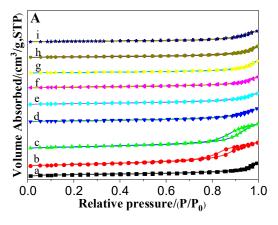


Figure 2. SEM images of the catalysts (**a**: M-TSO; **b**: MnCeO_x/M-TSO; **c**: $K_{0.1}$ MnCeO_x/M-TSO; **d**: $K_{0.5}$ MnCeO_x/M-TSO; **e**: K_{1} MnCeO_x/M-TSO).

3.1.3. N_2 Adsorption–Desorption Isotherms of the Prepared Catalysts

The N₂ adsorption-desorption isotherm and the pore size distribution of the prepared catalyst can be seen in Figure 3. Based on the IUPAC, the prepared catalysts have typical type II adsorption-desorption isotherm [45]. However, the hysteresis loops of prepared catalysts are different with each other when MnCeO_x and K_nMnCeO_x are loaded on the M-TSO support. As shown in Figure 3A(a-c), the M-TSO support exhibits weak intensity of the hysteresis loop, while MnCeO_x/M-TSO and K_{0.1}MnCeO_x/M-TSO catalysts exhibit obvious hysteresis loops at high relative pressure. However, with increasing the doping dosage of K, the hysteresis loops of the K_nMnCeO_x/M-TSO catalysts are changed to indistinct (Figure 3A(d-h)). The pore size distributions in Figure 3B also indicate that MnCeO_x/M-TSO and K_{0.1}MnCeO_x/M-TSO catalysts have obvious mesoporous structures at the range of 2–40 nm, while the other samples do not exhibit mesopores. Textural properties of prepared catalysts are listed in Table 2. Compared with M-TSO support, MnCeO_x/M-TSO and K_{0.1}MnCeO_x/M-TSO catalysts exhibit higher surface area and total pore volume, which are well agreed with the results of N2 adsorption-desorption isotherms and pore size distributions. With the increase of K doping, the surface area decreases, and the value reduces to 30.1 m²/g. The above phenomena are possibly related to the accumulation pores of $MnCeO_x$ and $K_{0.1}MnCeO_x$ active components on the surface of M-TSO, while the morphologies of K_nMnCeO_x may be changed at high doping dosage of K. With the increase of K doping, the total pore volume of K_nMnCeO_x/M-TSO decreased first, and then kept stable, while the pore size decreased first, and then increased. This phenomenon may be related to the deposition of K_nMnCeO_x active components on the surface of M-TSO. When the doping of K is increased, a mass of K or $KMnCeO_x$ species are filled into the surface gaps of M-TSO and reduce the amounts of small pores. Therefore, the pore size increases with the increasing of K doping. Figure 3A(i), Figure 3B(i), and Table 2 show that $K_{0.5}MnCeO_x/M-SiO_2$ also has a lower specific area and a larger pore size than that of $K_{0.5}MnCeO_x/M-TSO$.



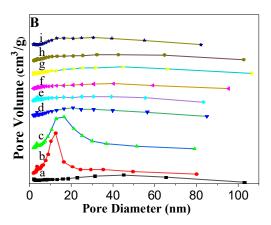


Figure 3. Nitrogen adsorption-desorption isotherms (**A**) and pore size distributions (**B**) of prepared catalysts (**a**: M-TSO; **b**: MnCeO_x/M-TSO; **c**: $K_{0.1}$ MnCeO_x/M-TSO; **d**: $K_{0.3}$ MnCeO_x/M-TSO; **e**: $K_{0.5}$ MnCeO_x/M-TSO; **f**: $K_{0.7}$ MnCeO_x/M-TSO; **g**: $K_{0.9}$ MnCeO_x/M-TSO; **h**: K_{1} MnCeO_x/M-TSO; **i**: $K_{0.5}$ MnCeO_x/M-SiO₂).

Table 2. Textural properties of prepared catalysts.

Catalysts	Surface Area (m²/g)	Total Pore Volume (m²/g) b	Pore Size (nm) ^c
M-TSO	51.3	0.123	9.9
$MnCeO_x/M-TSO$	81.1	0.218	9.4
$K_{0.1}MnCeO_x/M-TSO$	69.7	0.218	11.2
$K_{0.3}$ MnCeO _x /M-TSO	45.0	0.121	10.1
$K_{0.5}MnCeO_x/M-TSO$	44.2	0.105	8.9
$K_{0.7}MnCeO_x/M-TSO$	36.7	0.101	10.5
$K_{0.9}$ MnCeO _x /M-TSO	31.8	0.109	13.8
$K_1MnCeO_x/M-TSO$	30.1	0.101	14.1
$K_{0.5}MnCeO_x/M-SiO_2$	31.2	0.100	13.1

^a Calculated by BET method; ^b Calculated by BJH desorption cumulative volume of pores between 1.7 nm and 300 nm diameter; ^c Calculated by BJH desorption average pore diameter.

3.1.4. H₂-TPR Profiles of the Prepared Catalysts

The inherent redox property of the catalyst is the key to enhance the catalytic activity and deep oxidation of soot. In this work, to clearly investigate the influence of different K doping amounts and different active components, five representative catalysts, i.e., M-TSO, MnCeO_x/M-TSO, K_{0.1}MnCeO_x/M-TSO, K_{0.5}MnCeO_x/M-TSO, and K₁MnCeO_x/M-TSO, were determined by H₂-TPR. Since no obvious reduction peak is observed in Figure 4a at a low temperature (<500 °C), it indicates that the redox ability of M-TSO was very weak. The weak reduction peak observed at 650 °C is related to the reduction reaction of Tiⁿ⁺ in M-TSO [46]. When MnCeO_x and K_nMnCeO_x are loaded on the M-TSO support, the reduction peak positions and types of prepared catalysts have distinct differences with that of M-TSO support. As shown in the Figure 4b–e, the reduction peaks can be divided into four ranges of 178–250 °C, 280–350 °C, 350–450 °C, and >650 °C. Due to the large negative reduction potential, MnO was not reduced to Mn⁰, even above 950 °C. Therefore, MnO was considered to be the final state for the preparation of catalyst reduction [47,48]. According to the reduction process of Mn-based oxides, the first peak at

178–250 °C may be attributed to MnO₂ reduction to Mn₂O₃, the second peak at 280–350 °C could be related to Mn₂O₃ reduction to Mn₃O₄, and the third peak at 350–450 °C could belong to the Mn₃O₄ reduction to MnO [16,49]. The fourth peak at >650 °C is assigned to the reduction of CeO₂ to Ce₂O₃. Compared with MnCeO_x/M-TSO catalyst, the doping of K into MnCeO_x will lead to the lower reduction temperature (Figure 4c). However, with increasing the K doping amounts, the reduction temperature is increased. The H₂-TPR results indicate that the doping of K in MnCeO_x/M-TSO catalyst can modify the reduction properties of K_nMnCeO_x/M-TSO catalysts and is beneficial for regulating catalyst activities.

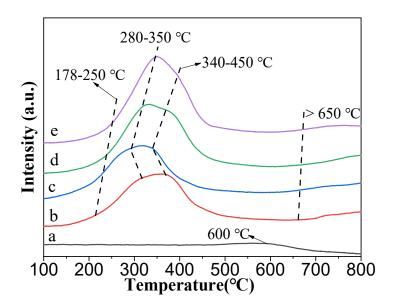


Figure 4. H₂-TPR curves of prepared catalysts (**a**: M-TSO; **b**: MnCeO_x/M-TSO; **c**: $K_{0.1}$ MnCeO_x/M-TSO; **d**: $K_{0.5}$ MnCeO_x/M-TSO; **e**: K_{1} MnCeO_x/M-TSO).

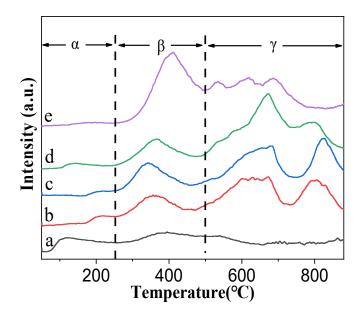
3.1.5. O₂-TPD Results of the Prepared Catalysts

The active oxygen species are essential for improving catalytic activity for deep oxidation of soot combustion. To conformably compare with the H2-TPR results, the same samples as those of H_2 -TPR that were determined were studied by O_2 -TPD, and the results are shown in Figure 5. The oxygen desorption peaks of prepared catalysts can be divided into three peaks, and the temperature regions are located at T \leq 250 °C, 250 °C \leq T \leq 500 °C, and T \geq 500 °C, respectively. However, the M-TSO support exhibits only two obvious oxygen desorption peaks, which are located at 100 and 380 °C. The first oxygen desorption peak (named as α in the Figure 5) at T \leq 250 °C belongs to the surfaceactive oxygen species (O_{surf}) or physically adsorbed oxygen [50]. The second peak, which is located at 250 °C \leq T \leq 500 °C and named as β , can be assigned to chemically adsorbed oxygen on the oxygen vacancies (O_2^-/O^-) [51]. The third peak, named γ , belongs to the desorption of lattice oxygen (O^{2-}) in the MnCeO_x and K_nMnCeO_x [52]. Compared with M-TSO support, it can be discovered that the third peaks are newly appeared. In addition, the shapes of the third peaks are also different with various K doping amounts. The reasons for the above phenomena are possibly related to the interaction of K and $MnCeO_x$.

3.1.6. NO-TPO Results of the Prepared Catalysts

Because of the relationship of "trade off" between soot and NO_x , NO_x is an inevitable gas in the emission of diesel engines [53]. In addition, NO_x , especially NO_2 , is an important factor to improve the catalytic performance. Based on the above reasons, the NO-TPO of the M-TSO support, $MnCeO_x/M$ -TSO, and $K_{0.5}MnCeO_x/M$ -TSO catalysts were studied, and the results of the test are shown in Figure 6. Owing to strong oxidization

ability, soot particles can be directly oxidized by NO2. Therefore, NO2 participates in the reaction and changes the reaction path of soot combustion. The soot combustion reaction will change from gas(O₂)-solid(catalyst)-solid(soot) to gas(O₂)-gas(NO₂)-solid(soot), which is beneficial to enhance the catalytic activity. As shown in the Figure 6A, M-TSO support exhibits low NO₂ concentration at the temperature range of 100–400 °C. When the temperature is higher than 400 °C, there is a little enhancement of NO₂ concentration, and the NO concentration decreases correspondingly. This result indicates that M-TSO support may exhibit low catalytic activity during soot combustion. The low NO₂ concentration also agrees well with the H2-TPR result of M-TSO support. Figure 6B,C exhibit the NO_x, NO, and NO₂ concentration of the MnCeO_x/M-TSO and K_{0.5}MnCeO_x/M-TSO catalyst. Compared with Figure 6A, the NO₂ concentration for the MnCeO_x/M-TSO and K_{0.5}MnCeO_x/M-TSO catalyst has obvious enhancement at the temperatures of 200–500 °C. The generated NO₂ is expected to improve the catalytic activity of the MnCeO_x/M-TSO and K_{0.5}MnCeO_x/M-TSO catalyst for soot combustion. As shown in Figure 6B, the temperature for the most concentration of NO_2 is about 300 °C, while it can be seen from Table 3 that the T₅₀ of K_{0.5}MnCeO_x/M-TSO catalyst for soot combustion is 354 °C. At a high temperature, part of NO₂ has been decomposed and cannot react with soot particles. From Figure 6C, the temperature for the most concentration of NO₂ for the K_{0.5}MnCeO_x/M-TSO catalyst is about 330 °C. This temperature is concordant with the T_{50} of the $K_{0.5}MnCeO_x/M-TSO$ catalyst. Therefore, most of the NO_2 can directly react with soot particles, which is beneficial to improve the catalytic activity.



 $\label{eq:figure 5.0} \textbf{Figure 5.} \ O_2\text{-TPD of prepared catalysts (a: M-TSO; b: MnCeO_x/M-TSO; c: } K_{0.1}\text{MnCeO}_x/\text{M-TSO; d: } K_{0.5}\text{MnCeO}_x/\text{M-TSO; e: } K_1\text{MnCeO}_x/\text{M-TSO).}$

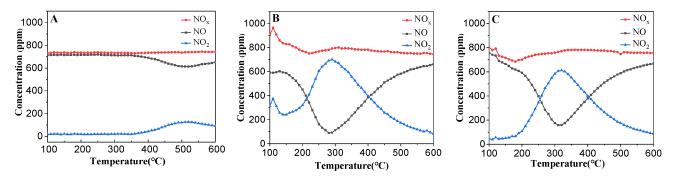


Figure 6. NO_x, NO, and NO₂ concentration over M-TSO support (**A**), MnCeO_x/M-TSO catalyst (**B**), and $K_{0.5}$ MnCeO_x/M-TSO catalyst (**C**).

Table 3. Catalytic performance of prepared catalysts for soot combustion.

Catalysts	T ₁₀ /°C	T ₅₀ /°C	T ₉₀ /°C	Sco ₂ m/%
Soot	457	552	594	41%
M-TSO	376	517	565	50.5%
$MnCeO_x/M-TSO$	284	354	393	99.3%
$K_{0.1}MnCeO_x/M-TSO$	286	346	380	99.4%
$K_{0.3}$ MnCeO _x /M-TSO	285	338	379	98.3%
$K_{0.5}MnCeO_x/M-TSO$	287	336	367	98.9%
$K_{0.7}$ MnCeO _x /M-TSO	293	341	379	97.7%
$K_{0.9}$ MnCeO _x /M-TSO	295	345	379	97.3%
K_1 MnCeO _x /M-TSO	300	349	384	96.7%

3.2. Catalytic Performance in Soot Combustion

3.2.1. Catalytic Activities of the Prepared Catalysts

The catalytic activity of the prepared catalyst in soot combustion was evaluated by TPO test, and to better evaluate the catalytic activity of active components, the combustion performance of soot on M-TSO under the same conditions was compared. As shown in Table 3, the combustion temperatures T_{10} , T_{50} , and T_{90} of pure soot are 457, 552, and 594 °C, respectively. The combustion temperature of soot on M-TSO was slightly lower than that of pure soot. The catalytic activity of M-TSO was very weak, and the T₁₀, T₅₀, and T_{90} were 376, 517, and 565 °C, respectively. However, when MnCeO_x is loaded on the M-TSO support, the catalytic ability of the MnCeO_x/M-TSO catalyst in soot combustion reaction is obviously improved. When the K are doped into the MnCeO_x/M-TSO, the catalytic activities of K_nMnCeO_x/M-TSO catalysts are further improved. With the increase of K doping amounts, the catalytic activity of the catalyst increased continuously until the molar ratio of K to Mn reached 0.5; after that, with the further increase of the K doping amount, the catalytic activity decreased continuously. Among the prepared catalysts, the catalytic activity of the $K_{0.5}MnCeO_x/M$ -TSO catalyst was the best, and the T_{10} , T_{50} , and T_{90} were 287, 336, and 367 °C, respectively. In addition, the CO_2 selectivity of the MnCeO_x/M-TSO and K_nMnCeO_x/M-TSO catalysts are more than 96%, which is much higher than that of the M-TSO support.

3.2.2. Sulfur Resistances of Prepared Catalysts

Due to the methods of the formation of fossil fuels, sulfur compounds are unavoidable in the diesel engine exhausts. Many previous studies have proved that Ti has high sulfur resistance in the catalytic reaction. To demonstrate the sulfur resistance of prepared catalysts, the catalytic performances of the $K_{0.5} Mn CeO_x/M$ -TSO and $K_{0.5} Mn CeO_x/M$ -SiO2 catalysts under 100 ppm SO2 were estimated. It can be seen from Figure 7 that there are significant differences between the two catalysts at T_{10} temperature, which indicates that $K_{0.5} Mn CeO_x/M$ -TSO has somewhat sulfur resistance. However, the temperatures of T_{50} and T_{90} for the tested catalysts are similar. In addition, compared with the results of Table 3 and Figure 7, the catalytic activity of $K_{0.5} Mn CeO_x/M$ -TSO has certainly declined with increasing of SO_2 concentration. The reason for the above phenomena may be related to the sulfuration of $K_{0.5} Mn CeO_x/M$ -TSO catalyst under 300 ppm SO_2 was calcined at $550~^{\circ}C$ for 4 h again to regenerate. After regeneration, the activity test was carried out again under 300 ppm SO_2 . The result indicates that the activity of the regenerated $K_{0.5} Mn CeO_x/M$ -TSO catalyst is also certainly decreased (Figure 7).

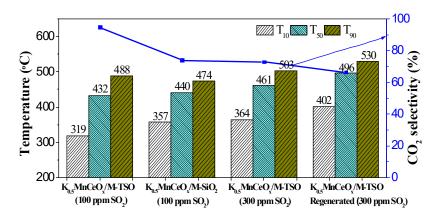


Figure 7. Catalytic performance of catalysts under 100 ppm or 300 ppm SO₂.

4. Conclusions

In summary, a K-modified 3DOM MnCeO $_{\rm x}/{\rm Ti}_{0.7}{\rm Si}_{0.3}{\rm O}_2$ catalyst was prepared by a simple method, in which the catalyst had 3DOM structure and three active components of K, Mn, and Ce. The K $_{\rm n}$ MnCeO $_{\rm x}$ /M-TSO catalysts exhibit excellent catalytic performance for soot combustion because of the macroporous structure and synergistic effect of K, Mn, and Ce. The K $_{0.5}$ MnCeO $_{\rm x}$ /M-TSO catalyst has the best catalytic performance among the prepared catalysts, and the T $_{10}$, T $_{50}$, and T $_{90}$ are 287, 336, and 367 °C, respectively. The characterization results indicate that the physicochemical properties of catalysts are changed when the K is doped into the MnCeO $_{\rm x}$ /M-TSO catalyst, and different doping amounts of K have obvious influence on the catalytic performance. In addition, compared with the K $_{0.5}$ MnCeO $_{\rm x}$ /M-SiO $_{\rm z}$ catalyst, the K $_{0.5}$ MnCeO $_{\rm x}$ /M-TSO catalyst also exhibits somewhat sulfur tolerance owing to it containing Ti. Meantime, the research results show that the prepared K $_{\rm n}$ MnCeO $_{\rm x}$ /M-TSO catalyst has the advantages of simple synthesis method, low cost, and high activity, and this has a certain application prospect.

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Article

Highly Active CuO/KCC-1 Catalysts for Low-Temperature CO Oxidation

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Abstract: Copper catalysts have been extensively studied for CO oxidation at low temperatures. Previous findings on the stability of such catalysts, on the other hand, revealed that they deactivated badly under extreme circumstances. Therefore, in this work, a series of KCC-1-supported copper oxide catalysts were successfully prepared by impregnation method, of which 5% CuO/KCC-1 exhibited the best activity: CO could be completely converted at 120 °C. The 5% CuO/KCC-1 catalyst exhibited better thermal stability, which is mainly attributed to the large specific surface area of KCC-1 that facilitates the high dispersion of CuO species, and because the dendritic layered walls can lengthen the movement distances from particle-to-particle, thus helping to slow down the tendency of active components to sinter. In addition, the 5% CuO/KCC-1 has abundant mesoporous and surface active oxygen species, which are beneficial to the mass transfer and promote the adsorption of CO and the decomposition of Cu⁺-CO species, thus improving the CO oxidation performance of the catalyst.

Keywords: air pollution control; CuO; dendritic mesoporous silica; CO oxidation; sintering resistance

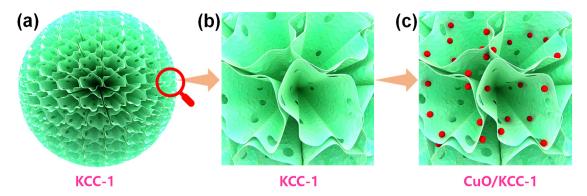
1. Introduction

Colorless, odorless, and tasteless carbon monoxide (CO) is a kind of toxic gas generated by the low combustion efficiency of the fuels from different sources of fuel combustion, such as vehicle exhaust emissions, cement plants, electricity plants, biomass combustion, etc. [1–4]. Catalytic oxidation is considered to be one of the most promising methods for CO elimination, especially at low temperature [5–8]. Recently, the catalytic oxidation of CO has been favored by many researchers due to its wide application in fields, such as indoor air purification, automobile exhaust purification, and providing pure hydrogen to automotive proton exchange membrane fuel cells [3]. Various catalytic systems have been explored as catalysts for the oxidation of CO, including noble metals, transition metals, and rare earth oxides. [9–11]. Noble metal catalysts, such as Au/ZnO [12], Pt/MnO_x [13], and Pd/CeO₂ [14], usually exhibit outstanding low-temperature CO oxidation performance, however, the inherent rarity and high cost restrict their widespread application. Therefore, more attention has been paid to the use of transition metal oxide catalysts, especially copper (Cu)-based catalysts, due to their excellent activity comparable to that of noble metals [15].

However, one of the most fundamental hurdles to overcome in catalytic reactions is sintering, both for precious metals and non-noble metals catalysts [16,17]. In order to retard the sintering of nanoparticles (NPs), some strategies were proposed [18]: (i) steric confinement of NPs by carbon nanotubes or other one-dimensional metal oxides [19,20];

(ii) embedding NPs in a silica matrix or porous shell [21,22]; (iii) restriction of NPs to channels of mesoporous materials, e.g., SBA-15 [23,24], MCM-41 [25]; (iv) stable anchoring of NP to the catalyst surface by a strong metal-support interaction [26,27]. In fact, this sort of confinement can significantly reduce sintering of the active NP's component, resulting in increased catalytic stability. However, traditional confinement strategies, particularly porous or core-shell structures, may hinder the transport of reactants to some extent or sacrifice a fraction of the active sites [28], which is detrimental to the catalytic reaction. Better strategies to stabilize active metal or metal oxide NPs are needed.

In recent years, dendritic mesoporous silica zeolite (such as KCC-1) has been attracting attention as a support with good sintering resistance [29,30]. In particular, Basset and his colleagues synthesized high surface area fibrous mesoporous silica nanospheres with a wide open-mouth spherical morphology [31], consisting of dendritic silica layers presented in three dimensions. The existence of dendritic silica layers with mesoporous channels makes this type of material highly accessible to active sites. In addition, the dendritic layered walls have open-mouth spherical morphology that can lengthen the movement distances from particle-to-particle, thus helping to slow down the tendency of active components to sinter. Peng et al. [18] also found that Ni/KCC-1 catalysts showed satisfying coking and sintering resistance in the dry reforming of a methane reaction due to the special structure of KCC-1. In this work, we used KCC-1 as a support for copper oxide nanoparticles and found that the synthesized catalyst was very effective in CO oxidation due to the mesopore-rich structure with a large specific surface, which facilitates mass transfer and the high dispersion of CuO, as well as the redox performance of the catalyst. Furthermore, the surface spatial confinement effect of KCC-1 support can significantly improve the thermal stability of the catalyst as displayed in Scheme 1.



Scheme 1. Diagram of the surface spatial confinement strategy ((a,b): KCC-1; (c): CuO/KCC-1, red spheres: CuO NPs).

2. Experimental Procedure

2.1. Preparation of Catalysts

All of the reagents were purchased from Sinopharm Chemical Reagent Co., Ltd. (Beijing, China) and utilized without any further purification. KCC−1 support was prepared according to the literature [31]. Typically, 60 mL of cyclohexane (99.5%), 3 mL of n-pentanol (99.5%), and 5.0000 g of tetraethyl orthosilicate (TEOS, 99%, 18.92 mmol) were mixed at room temperature to obtain liquid A; 2.0000 g of cetyltrimethylammonium bromide (CTAB, ≥99%, 5.48 mmol) and 1.2000 g of urea (99%, 19.98 mmol) were dissolved in 60 mL of deionized water to obtain liquid B; liquid B was poured into liquid A slowly and the resulting solution mixed well; then, the mixture was transferred into a stainless steel autoclave, sealed, and maintained at 120 °C for 6 h with constant stirring; after cooled to room temperature, the precipitation was collected by filtering and washing with acetone (99.5%) and ethanol (99.5%); then, the final precipitation was dried at 80 °C overnight and calcined in a muffle furnace at 550 °C for 6 h to remove the template agent (the heating rate was

2 °C min⁻¹); finally, the white powder of mesoporous molecular sieve material KCC-1 was obtained.

CuO/KCC-1 catalysts with different CuO loadings were prepared by an incipient wetness method using the synthesized KCC-1 support. The 0.5000 g of KCC-1 supports were impregnated in a solution containing 10 mL of ethylene glycol (99.5%) and proper amounts of Cu(NO₃)·6H₂O (\geq 99%) Then, the resulting solid–liquid mixture was dried in a vacuum oven at 80 °C until the solvent was completely evaporated; then, the resulting solid was calcined in a tube furnace at 550 °C under N₂ atmosphere for 4 h; finally, the gas was switched to air and maintained at 550 °C for 2 h. The attained catalysts were named as x% CuO/KCC-1–EG, where x% represents the CuO loading in mass fraction. Moreover, the effect of impregnating solution on the catalytic performance was also investigated: we replaced ethylene glycol with deionized water or ethanol, and the other conditions were the same as above; the obtained catalysts were named as x% CuO/KCC-1–H₂O or x% CuO/KCC-1–EtOH, where x% represents the CuO loading in mass fraction.

For comparison, the pristine CuO that without three-dimensional spatial structure was prepared by a homogeneous precipitation method. In a typical process, appropriate amount of $\text{Cu}(\text{NO}_3)_2 \cdot 6\text{H}_2\text{O}$ ($\geq 99\%$) was first dissolved in deionized water (the Cu²+ concentration was 0.1 mol L⁻¹), after 30 min of stirring, ammonia solution (Sinopharm, 25~28 wt.%) was added drop by drop to the above solution until the pH was about 10. The above mixture was stirred at room temperature for 3 h. At last, the precipitation was filtered and washed, dried, and calcined using the same calcination procedures as above.

2.2. Characterization of Catalysts

The detailed characterization of catalysts, including XRD, Nitrogen adsorption–desorption, H₂-TPR, SEM, TEM, and in situ DRIFTS are displayed in the Supplementary Materials.

2.3. Catalytic and Kinetic Tests

The CO catalytic oxidation activity of the prepared samples were measured in a fixed-bed quartz flow reactor with 100 mg of catalyst (60~80 mesh). The feed gases were composed of 1% CO, 21% O_2 , and balanced by high purity N_2 . The total flow rate was $30 \text{ mL} \cdot \text{min}^{-1}$ and the WHSV (weight hourly space velocity) was $18,000 \text{ mL g}_{\text{cat.}}^{-1} \cdot \text{h}^{-1}$. The reactants and products were analyzed on-line on a GC9310 gas chromatograph equipped with a TDX-01 column and a TCD. The conversion of CO (X_{CO}) was calculated using Equation (1)

$$X_{\text{CO}} = \left(1 - \frac{S_{\text{CO-outlet}}}{S_{\text{CO-inlet}}}\right) \times 100\% \tag{1}$$

where $S_{CO-outlet}$ and $S_{CO-inlet}$ are the CO concentrations in the outlet and inlet gas streams, respectively, corresponding to the CO inlet and outlet peak areas, as determined by the gas chromatograph responses using the external standard method. Carbon balance was close to 100%.

We can calculate the normalized reaction rate (r) and apparent activation energy (E_a) of the reaction by performing CO catalytic oxidation reactions at different temperatures to obtain the CO conversion according to Equations (2)–(4) [32]

$$r = \frac{X_{\text{CO}} F_{\text{CO}}}{m_{cat.}} \tag{2}$$

$$r = -\frac{F_{CO}}{m_{cat.}} \times \ln(1 - X_{CO}) \tag{3}$$

$$\ln k = -\frac{E_a}{RT} + \ln A \tag{4}$$

where F_{NO_x} is the gas flow rate (in mol s⁻¹) of CO; $m_{cat.}$ is the mass of the catalyst (in g); A is the pre-exponential factor; T is the reaction temperature (in K); R is the gas constant (in kJ mol⁻¹ K⁻¹). Generally, the reaction orders in the equations were set as first and zero for

CO and O_2 , respectively. The E_a can be calculated from the Arrhenius plots of the reaction rate coefficient.

Differential reaction mode was used to study the reaction kinetics of certain sample catalysts (with CO conversion below 10%). The catalyst was diluted to 200 mg with quartz sand (of the same size) and evaluated under the same conditions as the catalytic test above, with the exception that the gas flow rate was increased to 120 mL min⁻¹, and the absence of mass and heat transfer limitations ensured the reaction was in the kinetic region. Weisz–Prater criteria (C_{WP}) for internal diffusion and Mears' criterion (C_M) for exterior diffusion were used to verify the lack of mass transport resistances according to Equations (5) and (6) [33–36]

$$C_M = \frac{r\rho_b R_p n}{k_c C_{Ab}} < 0.15 \tag{5}$$

$$C_{WP} = \frac{r_{obs}\rho_c R_p^2}{D_{eff}C_{As}} < 1 \tag{6}$$

where r_{obs} is the observed reaction rate (in mol kg_{cat}⁻¹·s⁻¹, $r_{obs} \approx r$); n is the reaction order (the reaction orders in the equations were set as first and zero for CO and O₂, respectively); R_p is the catalyst particle radius $(1.1 \times 10^{-4} \text{ m})$; ρ_c is the solid catalyst density (in kg m⁻³); ρ_b is the bulk density of catalyst bed (in kg m⁻³, $\rho_b \approx \rho_c$); D_{eff} is the effective diffusivity $(8.9 \times 10^{-6} \text{ m}^2 \text{ s}^{-1})$; C_{As} is the gas concentration of CO at the external surface of the catalyst (in mol m⁻³); C_{Ab} is the bulk gas concentration of CO (in mol m⁻³, $C_{Ab} \approx C_{As}$); k_c is the external mass transfer coefficient (0.1 m s^{-1}) .

3. Results and Discussion

3.1. SEM and TEM Results Analysis

To understand the microscopic morphology of the catalysts, the as-prepared KCC-1 support and CuO/KCC-1 series catalysts were characterized by SEM, and the SEM images of the catalysts are shown in Figure 1. We can see that, for the KCC-1 support, the morphology is that of flower-like fibrous microspheres with an average spherical diameter of approximately 500 nm. This structure allows KCC-1 to maintain good thermal stability and an effective surface spatial confinement effect. The morphology did not change significantly when KCC-1 was loaded with a small amount of CuO (as shown in Figure 1b-d), but the morphology of the catalyst was disrupted when the loading of CuO was excessive (as shown in Figure 1e). When the impregnating solution was changed from ethylene glycol to deionized water, the morphology of the catalyst did not change significantly (as shown in Figure 1f).

The micro morphology of CuO/KCC-1 series catalysts and CuO was further studied, and the as-prepared samples were characterized by TEM and EDX-Mapping technologies. As shown in Figure 2a, the TEM image of CuO shows that it is composed of bulk nanoparticles. From Figure 2b–d, we can clearly see the dendritic skeleton structure of KCC-1 spreading from the center to the periphery, which is an important factor for the good stability of the support structure. The interweaving between dendritic fibers forms a pore-rich structure, which is beneficial to the high dispersion of CuO nanoparticles. In addition, it can be seen from the TEM image that after the CuO nanoparticles were confined in KCC-1 support, no large metal particles are seen on the surface of the KCC-1, which indicates that the CuO nanoparticles are highly dispersed on the surface of the KCC-1 supports. As shown in Figure 2e–h, the high-angle annular dark field image and EDX-Mapping images of 5% CuO/KCC-1-EG show that the CuO nanoparticles are uniformly distributed and highly dispersed.

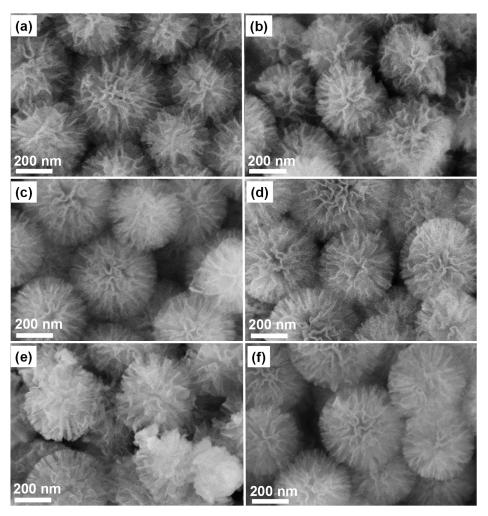


Figure 1. The SEM images of the catalysts ((a) KCC-1; (b) 1% CuO/KCC-1-EG; (c) 3% CuO/KCC-1-EG; (d) 5% CuO/KCC-1-EG; (e) 7% CuO/KCC-1-EG; (f) 5% CuO/KCC-1-H₂O).

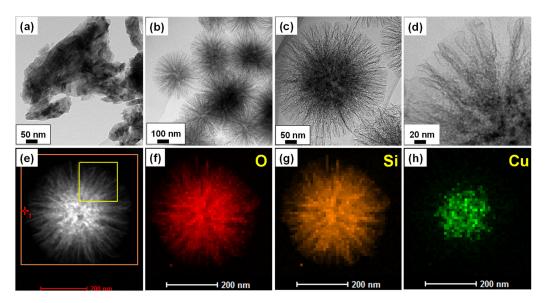


Figure 2. The TEM images of the catalysts ((a) CuO; (b–d) 5% CuO/KCC-1-EG); (e) High-angle annular dark field image of 5% CuO/KCC-1-EG; (f–h) EDX Mappings of 5% CuO/KCC-1-EG).

3.2. CO Oxidation Performance, Kinetic and Thermal Stability

The CO oxidation activity of the CuO/KCC-1 series catalysts were tested, as shown in Figure 3a, from which it can be seen that the dendritic mesoporous molecular sieve KCC-1 composed of SiO_2 showed almost no CO catalytic oxidation activity. When the KCC−1 was loaded with a small amount of CuO, the CO catalytic oxidation activity of the catalyst increased and reached an optimum level when the CuO loading reached 5%, with a complete conversion of CO at 120 °C. The CuO loading should not be too high and the activity of the catalyst decreased when the CuO loading reached 7%, with a complete conversion of CO at 160 °C. Pristine CuO exhibited barely satisfactory CO catalytic oxidation activity, and CO could be completely reacted when the reaction temperature reached 280 °C. By comparing the CuO/KCC-1-EG series catalysts with different CuO contents, it was found that 1% CuO/KCC-1-EG has the lowest catalytic activity, and the CO catalytic oxidation activity of the catalysts was boosted and then decreased with the increasing CuO content. The possible reason for this is that KCC-1, which has a high specific surface area and abundant mesoporous pores, has no catalytic activity, but CuO nanoparticles have a certain CO catalytic oxidation activity. The CuO nanoparticles were highly dispersed on the surface of KCC-1 and in the pore channels, making the catalyst exhibit excellent catalytic performance; as the CuO content increased, the number of active components also increased, thus enhancing the catalytic activity; however, as the CuO content increased further, the CuO nanoparticles covered the surface of the KCC-1, blocking part of the molecular sieve catalyst pore channels, leading to a decrease in the specific surface area and pore volume of the samples, which ultimately led to a decrease in the catalytic oxidation activity of the catalysts. In addition, the influence of the impregnating solution on the catalytic performance of the catalysts was investigated, as presented in Figure 3b, and the resulted showed that the choice of impregnating solution significantly affected the catalytic performance of the catalysts. For 5% CuO/KCC-1-EtOH and 5% CuO/KCC-1-H₂O catalysts, the temperature for complete CO conversion were 220 and 260 °C, respectively. The order of preference is: ethylene glycol > ethanol > deionized water. When ethylene glycol is used as the impregnating solution, it is beneficial to the high dispersion of CuO on the surface of the KCC−1 supports.

In order to test the intrinsic activity of the catalyst and the activation energy of catalytic reaction, high weight hourly space velocity and low conversion (72,000 mL g_{cat.}⁻¹ h⁻¹, CO conversion were less than 10%) and catalysts doped with quartz sand were used to eliminate the effects of mass and heat transfer. The kinetic calculation (Mear and Weisz-Prater's criterion) was used to determine whether the effects of internal and external diffusion were excluded, and the calculation results are displayed in Table 1. The C_M < 0.15 and C_{WP} < 1, therefore, the internal and external diffusion effects and heat transfer effect on the catalysts during the kinetic experiment could be neglected; the activities tested were the intrinsic activity of the catalysts. The Arrhenius curve obtained from the kinetic test of the catalyst is shown in Figure 3c, and the activation energies of the reactions were calculated. The result is $E_a(1\% \text{ CuO/KCC}-1-\text{EG}) \approx E_a(\text{CuO}) > E_a(7\% \text{ CuO/KCC}-1)$ CuO/KCC-1-EG) > $E_a(5\% CuO/KCC-1-EG)$. When 5% CuO/KCC-1-EG was used as the catalyst for the reaction, the catalytic reaction had the lowest activation energy, which was 31 kJ mol^{-1} . The kinetic test results showed that 5% CuO/KCC - 1 - EG could reduce the energy barrier of the catalytic reaction and promoted the catalytic reaction, which was consistent with its optimal CO catalytic oxidation performance. To test the thermal stability of the catalyst, the as-prepared CuO and 5% CuO/KCC-1-EG catalysts were calcined at $700~^{\circ}\text{C}$ for 3 h in air atmosphere, and then their CO catalytic oxidation performances were tested. As shown in Figure 3d, the activity of 5% CuO/KCC-1-EG decreased slightly after high-temperature calcination, the temperature of CO complete conversion increased slightly to 140 °C; although the temperature of CO complete conversion increased slightly to 300 °C over the CuO catalyst, the T₅₀ (the temperature when CO conversion reached 50%) increased obviously from 195 to 240 $^{\circ}$ C. The thermal stability results show that 5%CuO/KCC-1-EG had better thermal stability, which is mainly due to the large specific

surface area of KCC-1 support, which is beneficial to the high dispersion of CuO species. In addition, the dendritic layered walls have open-mouth spherical morphology that can lengthen the movement distances from particle-to-particle, thus helping to slow down the tendency of active components to sinter.

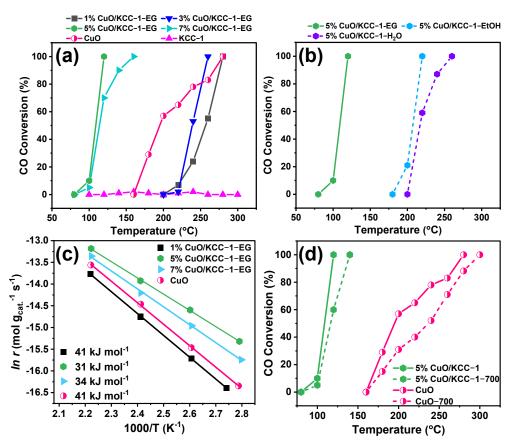


Figure 3. (a) Light-off curves of CO conversion for CO oxidation reaction; (b) Effect of impregnating solution on catalyst performance; (c) Arrhenius curves of CO catalytic oxidation over various catalysts; (d) The thermal stability curves of catalysts.

Table 1. The C_{WP} and C_M over the various catalysts in CO oxidation performance.

Catalysts	$ ho_b$	r	C_{Ab}	T_m a	C_M	C_{WP}
1% CuO/KCC-1	1882	7.6×10^{-5}	0.423	365	3.38×10^{-4}	3.80×10^{-4}
5% CuO/KCC-1	1897	2.2×10^{-4}	0.391	358	1.09×10^{-3}	1.22×10^{-3}
7% CuO/KCC-1	1926	$1.4 imes 10^{-4}$	0.403	358	$6.97 imes 10^{-4}$	$7.84 imes 10^{-4}$
CuO	6114	7.5×10^{-5}	0.412	365	1.12×10^{-3}	1.26×10^{-3}

a: T_m were the maximum temperatures during CO oxidation kinetic measurements (in K).

3.3. XRD Results Analysis

The XRD spectrum of the CuO/KCC-1 series catalysts are shown in Figure 4. It can be seen that a broad diffraction peak appears at a 2θ value at 22.58° , which corresponded to the characteristic diffraction peak of the amorphous SiO₂ of the mesoporous molecular sieve KCC-1 [18]. The pure CuO sample shows a characteristic diffraction peak typical of CuO with a strong peak intensity, indicating a high degree of crystallinity of CuO. For the CuO/KCC-1–EG catalysts impregnated by ethylene glycol, the characteristic diffraction peaks of CuO species were not detected even though the loading of CuO was as high as 7%, indicating that the CuO species were highly dispersed on the surface of KCC-1,

which is consistent with their SEM and TEM results. When the impregnating solution was changed to deionized water, faint characteristic peaks of CuO species could be detected. The above XRD results show that the CuO nanoparticles were highly dispersed on the KCC-1 support and the use of ethylene glycol as the impregnating solution was more favorable to the high dispersion of Cu species on KCC-1 than deionized water.

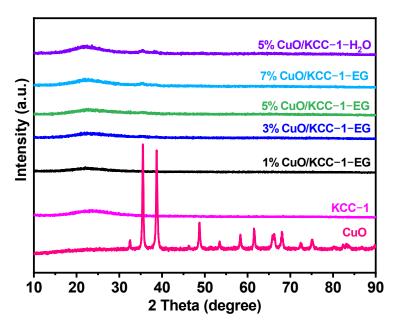


Figure 4. The XRD patterns of the catalysts.

3.4. N₂ Adsorption/Desorption Results Analysis

The N₂ adsorption and desorption isotherms, as well as the pore size distribution curves of CuO/KCC-1 series catalysts, are shown in Figure 5a,b, respectively. Table 2 shows the quantitative data. It can be seen from Figure 5a that the adsorption-desorption isotherms curve of CuO/KCC-1 catalysts showed typical type IV isotherms with a hysteresis loop of type H1 in the p/p_0 between 0.4 and 1.0, which is caused by the capillary condensation phenomenon of the mesoporous structure, indicating that the catalysts have mesoporous structure [18]. As shown in Figure 5b, narrow and strong peaks at 3.5 nm and fluctuations over a range of 10 to 50 nm are observed on the pore size distribution curve of the CuO/KCC-1 catalysts due to the narrow inside channels and broader outside channels. Although the CuO sample also has a pore structure, its pore diameter is basically zero, which shows that its pores are formed by the accumulation of a large number of CuO particles and not its own inherent pore structure, which can also be confirmed by the TEM image of CuO. It can be seen from Table 2 that the specific surface area of pristine CuO is the smallest, only $10 \text{ m}^2 \text{ g}^{-1}$, and the pore volume is only $0.006 \text{ cm}^3 \text{ g}^{-1}$. The KCC-1 support shows high specific surface area (638 m 2 g $^{-1}$) and the largest pore volume (1.68 cm 3 g $^{-1}$). As the loading of CuO increases, the specific surface area and pore volume of the catalyst show a decreasing trend. This is mainly because CuO nanoparticles block part of the pores. Nevertheless, when the ethylene glycol is used as the impregnating solution, the specific surface area of CuO/KCC-1 series samples is still higher than 300 m² g⁻¹, which provides abundant reaction place for the catalytic reaction. When the impregnating solution was changed from ethylene glycol to deionized water, the specific surface area of the catalyst was significantly reduced, which indicated that the type of impregnating liquid would affect the physical structure of the catalyst. Using deionized water as the impregnating liquid is not beneficial to the high dispersion of CuO, which is consistent with the XRD results.

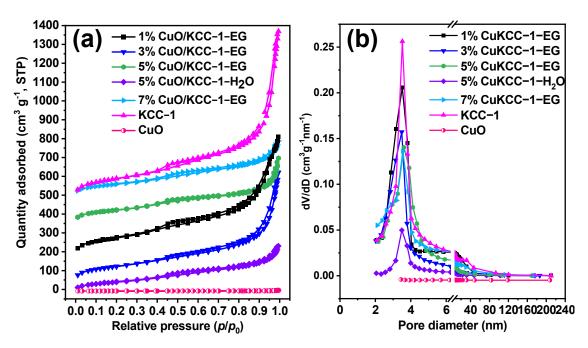


Figure 5. (a) N₂ adsorption—desorption isotherms and (b) pore size distributions of the catalysts.

Table 2. The textual pro	operties of Mn _{0.50} Co	00 49 Vn na 6	and various catalysts.
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Samples	Surface Area $(m^2 g^{-1})$	Pore Volume (cm 3 g $^{-1}$)	Pore Size (nm)
7%Cu/KCC-1-EG	309	0.76	3.5
5%Cu/KCC-1-EG	345	0.95	3.5
5%Cu/KCC-1-H ₂ O	264	0.87	3.4
3%Cu/KCC-1-EG	388	0.97	3.5
1%Cu/KCC-1-EG	457	1.21	3.5
KCC-1	638	1.45	3.5
CuO	10	0.006	7.0

3.5. H₂-TPR Result Analysis

Figure 6 depicts the H₂-TPR curve of the CuO/KCC-1 catalysts. Pure CuO displays a noticeable reduction peak with a peak temperature of 324 °C, which is related to the reduction of CuO to Cu [37]. The 1% CuO/KCC-1-EG has no obvious reduction peak. The reduction peak temperature of 3% CuO/KCC-1-EG is 231 °C, which is not much different from the reduction peak temperature of 5% CuO/KCC-1. When the Cu loading amount reaches 7%, the reduction peak temperature of Cu species shifts to a higher temperature, which is 237 °C. The intertwined abundant pores are beneficial to the transmission and diffusion of substances, and are beneficial to promoting the migration of active oxygen species and, thus, improving the reduction properties of the catalyst. This is the important factor for the improvement of the CO catalytic oxidation performance. In addition, it can be seen that when the impregnating solution was changed from ethylene glycol to deionized water, the reduction peak temperature of the catalyst shifted to the higher temperature, which indicates the decreased reduction property, and that it is consistent with the weaker CO catalytic performance over the 5% CuO/KCC-1-H₂O catalyst.

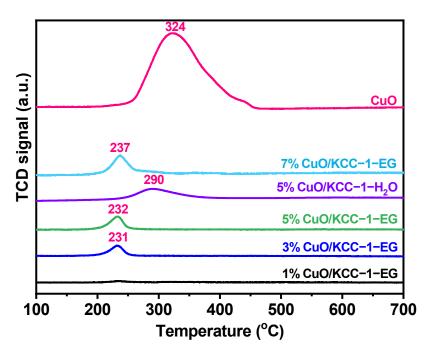


Figure 6. The H₂-TPR curves of the catalysts.

3.6. XPS Result Analysis

Because the catalytic reaction occurs on the catalyst's surface, it is critical to investigate the surface element composition and valence. The XPS spectra of 5% CuO/KCC-1–EG, 5% CuO/KCC-1–H₂O, and CuO catalysts are shown in Figure 7, and the surface atom concentrations' results are shown in Table 3. For the XPS spectrum of O 1s (Figure 7a–c), the peaks located at 530.9 \sim 531.0 eV are ascribed to the surface chemically adsorbed oxygen species; the peaks located at 529.1 \sim 530.3 eV are assigned to the lattice oxygen species [38–41]. It can be seen from the quantitative results in Table 3 that the 5% CuO/KCC-1–EG has the largest surface adsorption oxygen species ratio, followed by the 5% CuO/KCC-1–H₂O, and CuO has the smallest surface adsorption oxygen species ratio. As we all know, the adsorbed oxygen on the surface has stronger mobility than the lattice oxygen and can promote the catalytic oxidation of CO, which is consistent with the H₂-TPR results and catalytic performance. Figure 7d is the spectrum of the Cu 2p orbital of the catalysts. The peak intensity of CuO is significantly higher than that of 5% CuO/KCC-1–EG and 5% CuO/KCC-1–H₂O, which confirms the high dispersion of Cu species on KCC-1 from the side, and this is in accordance with the results of XRD, SEM, and TEM.

3.7. In Situ DRIFTS Results Analysis

In this section, in situ DRIFTS measurements for as-synthesized 5% CuO/KCC-1-EG and CuO were performed at 100 °C to better understand the CO adsorption behavior. As shown in Figure 8a,b, the bands located at 2119~2127 cm $^{-1}$ and 2162~2172 cm $^{-1}$ were observed in both catalysts when exposed in a CO atmosphere, which were attributed to the CO adsorption on Cu $^+$ (Cu $^+$ -CO) species and gaseous CO species [4], respectively. The intensity of the adsorption peak over the 5% CuO/KCC $^-$ 1 $^-$ EG was higher than that of CuO, which indicates that 5% CuO/KCC $^-$ 1 $^-$ EG is more beneficial to the adsorption of CO. The bands located at 2336~2363 were ascribed to gaseous CO $_2$ [4,42], suggesting the incoming CO reduced the surface species of oxides. After being treated with CO for an hour, the catalysts were purged with N $_2$ for 30 min. As presented in Figure 8c,d, the band corresponding to gaseous CO $_2$ disappeared and the band ascribed to Cu $^+$ -CO still existed over the CuO catalyst, the peak intensity decreased with the time of the O $_2$ treatment, but the peak intensity was still high when exposed in an O $_2$ atmosphere for an hour. However, for the 5% CuO/KCC $^-$ 1 $^-$ EG catalyst (Figure 8d), two big bands appeared when the gas was shifted to O $_2$ for only 1 min: gaseous CO $_2$ and Cu $^+$ -CO species emerged

simultaneously, and the intensity declined sharply and almost completely disappeared when treated with O_2 for an hour. The above results indicate that 5% CuO/KCC-1–EG was more beneficial to the adsorption of CO and the decomposition of Cu⁺–CO species: this may be an important reason for its better catalytic activity than that of CuO.

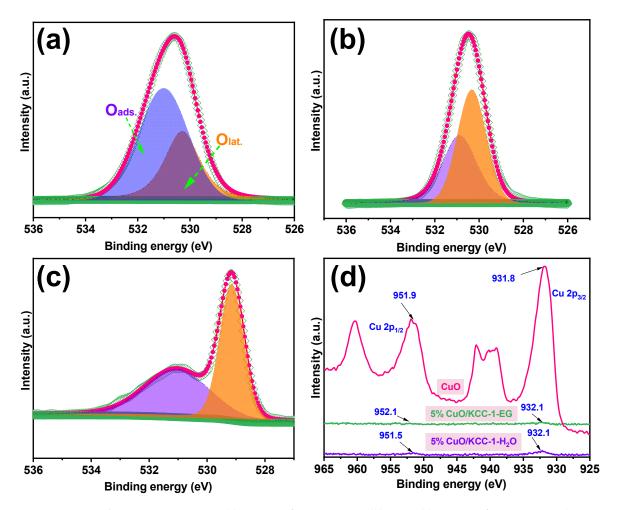


Figure 7. The O 1s XPS patterns (a) 5% CuO/KCC-1-EG; (b) CuO; (c) 5% CuO/KCC $-1-H_2O$); (d) Cu 2p XPS patterns) of the catalysts.

Table 3. Surface atom concentrations of the catalysts.

Samples	Cu 2p Binding Energy (eV)		ΔE (eV)	O 1s Binding Energy (eV)		O _{ads} /O _{lat}
	2p _{1/2}	2p _{3/2}		O _{ads.}	O _{lat.}	
5% Cu/KCC-1-EG	952.1	932.1	20.0	531.0	530.3	1.7
5% Cu/KCC-1-H ₂ O	951.5	932.1	19.4	531.0	529.1	0.9
CuO	951.9	931.8	20.1	530.9	530.3	0.7

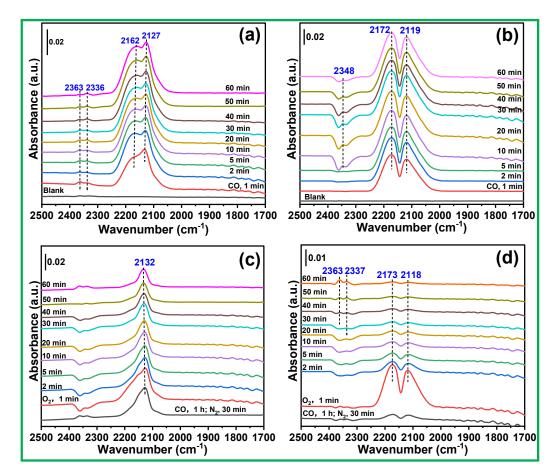


Figure 8. In situ DRIFT spectra of the **(a)** CuO and **(b)** 5% CuO/KCC-1–EG catalysts under an atmosphere of 1000 ppm of CO/N $_2$ (30 mL min $^{-1}$) at 100 °C; in situ DRIFT spectra of the transient reactions at 100 °C between 5% O $_2$ /N $_2$ (30 mL min $^{-1}$) and pre-adsorbed CO/N $_2$ species over the **(c)** CuO and **(d)** 5% CuO/KCC-1–EG catalysts recorded as a function of time.

4. Conclusions

In this work, a series of CuO/KCC-1 catalysts with varying CuO loadings were successfully prepared via the impregnation method and applied to the CO catalytic oxidation reaction. The catalyst showed good catalytic performance, of which 5% CuO/KCC-1–EG exhibited the best activity: CO could be completely converted at 120 °C. Compared with the pristine CuO catalyst, the 5% CuO/KCC-1–EG exhibited better activity and thermal stability, which is mainly attributed to the large specific surface area of KCC-1 that facilitates the high dispersion of CuO species and because the dendritic layered walls can lengthen the movement distances from particle-to-particle, thus helping to slow down the tendency of active components to sinter. In addition, the KCC-1 has abundant mesoporous and surface active oxygen species, which is beneficial to the mass transfer and promotes the adsorption of CO and the decomposition of Cu $^+$ –CO species, thus improving the CO oxidation performance of the catalyst.

Supplementary Materials: The following supporting information can be downloaded at: https://www.mdpi.com/article/10.3390/pr10010145/s1, The he detailed characterization of catalysts, including XRD, Nitrogen adsorption–desorption, H_2 -TPR, SEM, TEM, and in situ DRIFTS are displayed in the Supplementary Materials.

Author Contributions: Conceptualization, H.P. and D.W.; supervision, H.P. and D.W.; writing—original draft, Y.L. (Yiwei Luo), Y.L. (Yonglong Li) and C.W.; writing—review and editing, Y.L. (Yiwei Luo), Y.L. (Yonglong Li) and C.W.; methodology, W.L., J.W., H.P. and D.W. All authors have read and agreed to the published version of the manuscript.

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Conflicts of Interest: The authors declare that they have no known competing financial interest or personal relationships that could have appeared to influence the work reported in this paper.

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Article

Deactivation of Pd/SSZ-13 by Potassium and Water for Passive NO_x Adsorption

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Abstract: The passive NO_x adsorber (PNA) material has been considered an effective candidate for the control of NO_x from diesel exhaust during the engine cold start stage, and Pd/SSZ-13 attracts peoples' attention mainly due to its superior hydrothermal stability and sulfur resistance. However, chemical poisoning tolerance of Pd/SSZ-13 is another key parameter to its practical application and future development. Herein, we prepared potassium-loaded Pd/SSZ-13 and evaluated the influence on NO_x adsorption ability. The characterization results revealed that the loading of potassium could not destruct the structure of SSZ-13 but impaired the BET surface area and pore structure through the sintering of Pd species to PdO. Meanwhile, the grown PdO phase restrained the NO_x adsorption ability and promoted the generation of NO_2 at high temperatures. Moreover, the presence of H_2O could also impair the NO_x adsorption ability due to the competitive adsorption between H_2O and NO_x . This work verifies that the design of Pd/SSZ-13 sample with stable Pd species and excellent hydrophobicity is significant for its further application under harsh conditions.

Keywords: passive NO_x adsorption; Pd/SSZ-13; potassium poisoning; sintering of Pd species; inhibition of water

1. Introduction

The release of nitrogen oxides (NO_x) from mobile sources brings huge damage to both the environment and human health; thus, diesel exhaust purification is a long-term and severe challenge in this field [1–3]. To solve the problem, urea selective catalytic reduction (Urea-SCR/NH₃-SCR) technology has been successfully applied for the control of NO_x release in tail gas commercially. However, unremitting efforts are still being taken to meet the increasingly rigorous requirement for the NO_x emission, especially during the engine cold start period [4–7]. The exhaust temperature is almost below 200 °C during the cold start stage, which is a short time of 1~3 min upon engine starting [6–8]. However, such low temperature could not guarantee the decomposition of urea (>180 °C) and the operation of NH_3 -SCR process (>200 °C). Therefore, a large emission of unpurified NO_x into the atmosphere is inevitable at this stage [9–11]. Particularly, stricter demands for NO_x emission have been raised by Europe, USA and China in recent years [12–14], so it is extremely essential and urgent to reduce the NO_x emitted in the cold start period.

Currently, many efforts have been taken to design passive NO_x adsorber (PNA) materials to reduce the NO_x emission through storing NO_x at low temperatures (<150 °C)

and releasing the adsorbed NO_x at high temperatures (>200 $^{\circ}$ C), which attract significant attention due to the promising application for NO_x control in the cold start period [2,6–9]. Most PNA materials usually use noble metal (e.g., Pd and Pt) as an active adsorption center to improve the NO_x storage efficiency [15-17]. Meanwhile, metal oxides, such as Al₂O₃ and CeO₂, are commonly used as carriers to possess noble metals to prepare PNA materials [6,7,18–20]. However, the existence of sulfur severely weakens the NO_x adsorption ability of these metal oxide-based PNA materials, limiting their application in real exhaust condition [8,21,22]. Based on this, other materials (like zeolites) with high surface area, abundant acid sites, individual skeleton structure and superior resistance to sulfur poisoning attract much attention. Coincidentally, zeolites have been widely used as NH₃-SCR catalysts worldwide, further proving its application potential as the support of applicable PNA material [5–7,23,24]. In 2016, Jonson Matthey first reported that Pdbased zeolites (Pd/CHA, Pd/MFI and Pd/BEA) exhibited high NO_x storage efficiency at $100 \,^{\circ}$ C and with excellent resistance to SO_2 at the same time [8]. Afterwards, various research with respect to the effect of zeolite structure [25], active sites [8,25], Si/Al and Pd/Al ratio [10,11], adsorption chemistry [26] and activation method [9,22] to improve NO_x adsorption ability, has been carried out. Thereinto, the Pd/SSZ-13 zeolite with microporous exhibits huge application potential due to its excellent NO_x storage performance and outstanding hydrothermal stability. Notably, Pd is verified to play a key role in the NO_x adsorption as an active site by Szanyi et al. [15]. During the application of PNA materials for NO_x adsorption, its stability is a predominant parameter for the actual use in automobile industry because of the severe working conditions with various impurities and high working temperature. Specifically, resistance ability to hydrothermal and chemical poisoning, which have been widely discussed in NH3-SCR catalysts, are also typical challenges for PNA materials [27–33]. Aiming at these problems, Kim et al. [22] found optimum hydrothermal aging treatment could enhance the NO_x adsorption activity by redistributing PdO into dispersed Pd²⁺ ions over Pd/SSZ-13. Nevertheless, sintering of PdO may occur predominantly when excessive Pd was loaded. Moreover, Khivantsev et al. [34] analyzed the hydrothermal stability of Pd/BEA zeolites with different crystal sizes and found that the larger crystals were beneficial for the well-dispersion of Pd species, and the improvement of hydrothermal aging resistance was due to the hydrophobicity of zeolite.

Although hydrothermal poisoning of Pd/SSZ-13 has been carefully studied so far, investigation about the chemical poisoning on Pd/SSZ-13 used for NO $_{\rm X}$ adsorption is rarely reported. As is known, additives and impurities, derived from fuel and lubricating oil, may deposit on the catalysts and result in performance degradation due to the pore blocking and loss of active sites [27,28,31,35,36]. Both Beale et al. [35] and Li et al. [36] studied chemical deactivation on Cu/SSZ-13 caused by various impurities; it was found that the zeolite structure as well as catalytic activity were seriously affected because of the redistribution of metal species. Thereinto, K is a common element in the urea solution and biodiesel fuel used in the diesel trucks, and it can be deposited in the downstream catalyst (i.e., DOC, PNA, SCR catalyst) via the engine exhaust. Therefore, it is believed that the study of chemical deactivation of PNA material is also quite essential for the optimization of NO $_{\rm X}$ adsorption ability. However, there are very few studies in the open literature concerning the chemical deactivation of K on Pd/SSZ-13, which is used for passive NO $_{\rm X}$ adsorbers in diesel after-treatment system.

In this work, chemical deactivation of Pd/SSZ-13 was simulated by impregnating potassium with different contents (0.5, 1.0 and 1.5 mmol/ g_{catal}) on the fresh sample. The interaction of the zeolite framework and Pd species were characterized by various kinds of techniques. Meanwhile, the discrepancies of NO_x adsorption performance between fresh and poisoned samples were analyzed. As far as we know, the effect of potassium on Pd/SSZ-13 for NO_x adsorption has rarely been reported. In addition, considering the water exists in the exhaust, the potential effect of water on PNA performance was also evaluated. This work gives us a deep understanding about the degeneration of NO_x adsorption ability

over Pd/SSZ-13 by chemical deactivation and water, which provides valuable information for further design of high efficiency PNA material.

2. Materials and Methods

2.1. Sample Preparation

NH₄/SSZ-13 support with Si/Al ratio of 6 was prepared by a traditional hydrothermal method [37]. Fresh Pd/SSZ-13 with 1 wt.% Pd was synthesized via a "modified ion exchange method" [15] to ensure that the vast majority of Pd species are in the form of Pd²⁺ ions. The potassium poisoned Pd/SSZ-13 was obtained by a traditional wetimpregnated method. In detail, the KNO₃ aqueous solution was used as a potassium source, and the amount of potassium loading was precisely controlled by adjusting the source concentration. Afterwards, the wet sample was dried at room temperature for 3 days and finally calcined at 550 °C for 3 h. The desired potassium content was 0.5, 1.0 and 1.5 mmol/g_{catal}, and the corresponding samples were named as 0.5K-Pd/SSZ-13, 1.0K-Pd/SSZ-13 and 1.5K-Pd/SSZ-13, respectively.

2.2. Sample Characterization

Powder X-ray diffraction (XRD) was performed on a Rigaku SmartLab 9KW X-ray powder diffractometer with a Cu K α radiation. The spectra were obtained between 5 and 40°. BET surface area and pore volume were obtained by N₂ physisorption ASAP 2460. Before the test, the K/Pd-SSZ-13 samples were degassed at 300 °C for 3 h. The chemical state of Pd species was analyzed by Raman spectroscopy (Horiba, Japan). The content of K and Pd was measured by ICP-AES using Thermo Icap 7000. ²⁷Al MAS NMR was conducted on an Agilent 600 MHz solid state NMR spectrometer, and 0.1 M aqueous AlCl₃ solution was used as a reference. The dispersion of Pd species was observed by transmission electron microscopy (STEM, JEOL, JEM 2100F).

2.3. Evaluation of NO_x Adsorption Performance

The NO_x adsorption performance was evaluated in a fixed bed with powder samples (100 mg, 40–60 mesh) loaded in a quartz tube. A three-way value was used to switch the gas between the mixing tank and reactor. Firstly, the sample was treated in $10\% \ O_2/N_2$ (the total flow rate maintains at 200 mL/min) at $500\ ^{\circ}\text{C}$ for 1 h and cooled to 100. Then approximately 220 ppm of NO_x (including NO and inevitable NO_2) and $5\% \ H_2O$ (when used) was added into the mixture gas. Once the mixed gas concentration was stable, NO_x storage was performed for $1200\ ^{\circ}\text{C}$. In the next step, the sample was heated to $500\ ^{\circ}\text{C}$ at a ramping rate of $10\ ^{\circ}\text{C/min}$. The outlet gas was monitored by an online gas analyzer (MKS MultiGas $2030\ FTIR$). The amount of adsorption and desorption NO and NO_2 was calculated by the integral area, and the quantitative value was marked in the figure.

3. Results and Discussion

3.1. XRD and ²⁷Al NMR

To probe the structural changes after K impregnation, XRD patterns of fresh and deactivated samples were conducted. As shown in Figure 1, the fresh Pd/SSZ-13 exhibits typical CHA structure. No distinct Pd species are observed in all samples, probably due to the Pd phases that usually overlap with the CHA characteristic peaks [9,21]. Besides, it is observed that CHA phases of the sample impregnated with K decreased in intensity compared to the fresh sample. However, even after a high K content (1.50 mmol/g_{catal}) is loaded, main CHA features are obviously detected and no amorphous phases are observed, indicating that the zeolite framework is still well maintained. Therefore, it could be implied that a significant disruptive impact on the zeolite framework, such as destruction or collapse, may not take place in K impregnated samples. This observation is quite different from the early report [36].

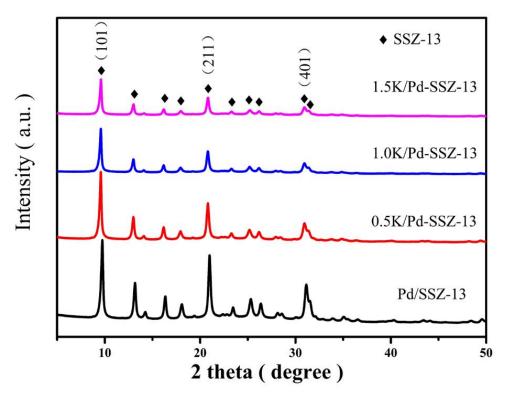


Figure 1. XRD patterns of Pd/SSZ-13 and K-deactivated samples.

As a more sensitive method to examine the dealumination and destruction of zeo-lite, 27 Al NMR analysis is performed to evaluate framework changes in CHA structures of deactivated samples. As exhibited in Figure 2, an intense feature at 58 ppm corresponded to tetrahedral Al (framework Al), a shoulder peak of this feature caused by the distortion of AlO^-_4 tetrahedra, and a broad peak centered at about 0 ppm assigned to octahedral Al (extra-framework Al) were observed [38–40]. After impregnated by K up to 1.50 mmol/ g_{catal} , the intensity of AlO^-_4 tetrahedra obviously increases with increasing the K content, indicating the formation of more AlO^-_4 tetrahedra. It is probably due to that the impregnation of K, which is a cation with large ionic radius, cause the change of T-O-T angle [40]. In addition, the intensity of tetrahedral Al is nearly identical to the fresh counterpart, indicating the addition of K has no significant effect on the Al framework. Such a result explicitly demonstrates that the CHA structures are relatively preserved in deactivated samples.

3.2. N₂ Physisorption and TEM

The N_2 physisorption results of samples are shown in Table 1 and Table S1, and Figure S1 displays the N_2 physisorption isotherms. It can be concluded that all the samples are microporous structure according to the type I isotherm. Based on the surface area and pore volume results, increasing the K content obviously decreases both the surface area and pore volume, especially the $S_{\rm micro}$ and $V_{\rm micro}$, indicating the K loading mainly affects the micropores. This phenomenon is also supported by pore size distributions shown in Figure S2, which is evidenced by the obvious decrease in the number of pores smaller than 2 nm. Combined with the XRD and 27 Al NMR results, it is known that the collapse of zeolite structure is not severe, thus such a decline is mainly due to the blockage of channels and pores in the zeolite framework.

To visualize the K addition on the effect of Pd species, TEM was performed for all samples, and the result is shown in Figure 3. No evident dark contrasts are observed for the Pd/SSZ-13, indicating a well dispersed Pd species in the pure Pd/SSZ-13. After K addition, some dark blocks (circled in yellow) corresponded to large Pd clusters and dark spots (circled in red) assigned to small Pd particles are clearly detected. Additionally,

by increasing the K content, the Pd clusters grow larger and become more evident. The average size of Pd clusters (calculated by the circled Pd species) is 4.9, 6.6 and 28.7 nm for 0.5K-Pd/SSZ-13, 1.0K-Pd/SSZ-13 and 1.5K-Pd/SSZ-13, respectively. It strongly suggests that the K addition promotes the sintering of Pd species. For the 1.5K-Pd/SSZ-13, some large Pd clusters are clearly observed on the crystal surface, indicating an aggregation of Pd species on the surface of zeolite after a large content of K loaded. This observation could be attributed to the fact that some Pd grains migrate and agglomerate to clusters out of the zeolite framework, or the Pd species grow larger in the zeolite pores and eventually break the zeolite structure. As proved above, the zeolite collapse of 1.5K-Pd/SSZ-13 is limited. Therefore, it is reasonable to estimate a facile migration of Pd species with potassium loading.

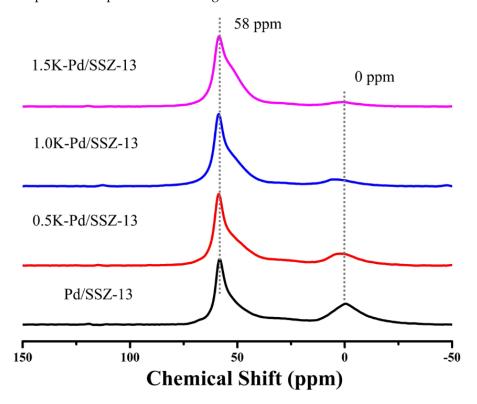


Figure 2. ²⁷ Al NMR patterns of Pd/SSZ-13 and K-deactivated samples.

Table 1. Physicochemical property of Pd/SSZ-13 and K-deactivated samples.

Sample	$S_{BET} m^2/g$	Pore Volume cm ³ /g	Pd Content wt.%	K Content wt.%
Pd/SSZ-13	392	0.23	0.96	-
0.5K-Pd/SSZ-13	348	0.21	0.94	1.81
1.0K-Pd/SSZ-13	318	0.19	0.92	3.52
1.5K-Pd/SSZ-13	262	0.15	0.90	5.41

3.3. Raman

As evidenced by N_2 physisorption and TEM results, the sintering of Pd species is responsible for the blockage of zeolite pores and channels. Raman analysis was performed to confirm the sintering species. As shown in Figure 4, a Raman shift at around 650 cm⁻¹ assigned to bulk PdO is clearly observed for potassium-deactivated samples [41]. The peak intensity becomes even larger with increasing potassium content, which demonstrates that the bulk PdO is the dominant sintering species. With regard to the formation of PdO, it is reasonable to speculate that the addition of K facilitates the Pd²⁺ to migrate out of ion-exchange sites and eventually aggregate to the PdO during the following calcination

process. In this manner, the migration of Pd²⁺ is accelerated and more Pd²⁺ is sintering after excess K loaded and thus clustered PdO is much more observable.

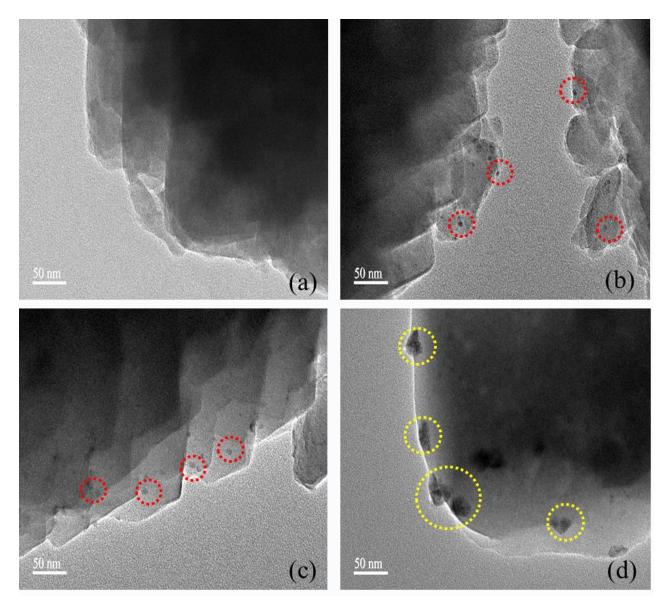


Figure 3. TEM images of the (a) Pd/SSZ-13 and K-deactivated samples (b) 0.5K-Pd/SSZ-13, (c) 1.0K-Pd/SSZ-13 and (d) 1.5K-Pd/SSZ-13. The red and yellow circle represents aggregated Pd clusters.

3.4. PNA Performance

Compared to the influences of K on Cu/SSZ-13 and Cu-SAPO-34, the deleterious effects on Pd/SSZ-13 are much more significant. For example, after loading 1.0 and 1.5 mmol/g_{catal}, the decrease in S_{BET} and SCR performance of Cu/SSZ-13 was quite small [37], in the contrary, the blockage of channels and pores in Pd/SSZ-13 was much more serious and an obvious deterioration in NO_x adsorption was observed. In addition, the influence of K on the original active metal sites in zeolite is quite different. After introducing K, the aggregation of Cu species in Cu/SSZ-13 was not easily detected. However, large Pd clusters were displayed in all K-deactivated catalysts shown in SEM images. Thus, it is suggested that the substitution of K to Pd in Pd/SSZ-13 is more likely to happen. In order to evaluate the poisoning effect of K on Pd/SSZ-13, the PNA performance of K-deactivated samples was tested. As shown in Figure 5a, the results of NO_x storage at 100 °C followed by a desorption with increasing the temperature at a rate of 10 °C/min to 500°C is depicted, and the profiles of NO and NO₂ are recorded separately to obtain

an unambiguous understanding of respective trapping and desorption behaviors. The NO and NO₂ inlet concentrations are about 210 and 10 ppm, and the inevitably NO₂ in the feed gas probably originates from the oxidation of NO source [34]. The adsorption and desorption content were estimated by the integration of peak area and were marked in the corresponding peak. For the fresh Pd/SSZ-13, it is evident that abundant NO is trapped during the first 1200 s at 100 °C. In contrast, the NO₂ adsorption is few, corresponding to the one-twelfth of NO adsorbing capacity. When increasing the temperature, the trapped NO and NO₂ desorb simultaneously at 200 °C, and the respective desorption amount is 8.9 and 9.2 μmol. It is very impressive for forming quite a large amount of NO₂ since little NO₂ is adsorbed at the trapping step. The desorption of NO₂ is probably due to the decomposition of nitrate species formed by NO. After NO completely desorbs at 280 °C, the NO concentration is below 210 ppm in the temperature range of 280–550 °C, indicating NO is trapped again by Pd/SSZ-13 or consumed in the testing atmosphere. Meanwhile, a second NO₂ shoulder peak centering at 320 °C appears following the initial NO₂ desorption peak, which strongly indicates a new approach or intermediate for NO₂ formation different from the former. In addition, it is noted that the outlet NO and NO2 concentration nearly restores to the initial level at 500 °C eventually. Therefore, it could be mentioned that the oxidation of NO to NO₂ by oxygen at high temperatures is limited for the Pd/SSZ-13 in our study. According to the calculated NO_x concentration shown in Figure 5, it is revealed that although Pd/SSZ-13 adsorbs plenty of NO at 100 °C, the NO_x desorption mainly consists of NO_2 . In order to illustrate the possible pathway for NO_x transformation during the desorption step, oxygen is not purged to the feed gas in the heating-up period to avoid possible oxidation reactions from NO to NO_2 . As shown in Figure S6, the NO_x adsorption ability is almost unchanged, and well-resolved NO and NO₂ desorption peaks are similar to Figure 5a centering at about 200 °C are also observed. Additionally, the estimated desorption amount is close to that calculated in the presence of oxygen. This result clearly reveals that the desorbed NO₂ at low temperatures originates from the decomposition of some chemical intermediates formed in the storage step rather than directly from the oxidation of NO in the desorption process, because oxygen is not essential for the formation of this kind of NO₂. However, for the case heating up in the absence of oxygen, a new broad NO releasing profile rather than an NO storage peak shown in Figure 5a is observed between 250 and 500 °C. Meanwhile, the NO₂ concentration drops to zero. This observation indicates that the second NO₂ formation on Pd/SSZ-13 at high temperatures in the presence of oxygen simply originates from the oxidation of chemisorbed NO in Pd/SSZ-13 rather than the gas phase NO. Besides, based on the fact that two NO desorption peaks are observed in the absence of oxygen, it is reasonable to speculate that there are various adsorption sites for NO on Pd/SSZ-13. To further study the effect of oxygen on NO_x adsorption, the overall test process is conducted without oxygen supplement. As observed in Figure S7, Pd/SSZ-13 mainly adsorbs NO at first 1200 s, while the adsorption ability (9.6 µmol) is much inferior to those performed in the presence of oxygen (19.8 µmol). It indicates that oxygen is beneficial for NO adsorption. A special phenomenon is that a NO₂ formation peak appears at the trapping step. Note that each sample is activated by oxygen before the test, thus it is possible that some NO is oxidized by the adsorbed oxygen to NO₂ in zeolite. When it comes to the desorption stage, two NO desorption peaks are still stable, but the released amount in the low temperature decreases a lot compared with a counterpart in Figure 5a. In addition, no NO₂ formation peak is observed during ramping. According to the above results, it can be concluded that: (1) oxygen enhances the NO storage capacity mainly by reacting with NO on Pd/SSZ-13 to form intermates, which could decompose to NO2 during the heating-up period; (2) The NO desorbed from Pd/SSZ-13 at higher temperature could be easily oxidized by oxygen to form NO₂, which correlates to the NO₂ formation ranging from 280 to 500 °C; (3) The catalytic reaction of NO to NO₂ by oxygen is inconspicuous in our study, which is due to little PdO exists in the as-synthesized Pd/SSZ-13. The K-loaded sample exhibits poor NO storage capacity during the first 1200 s at 100 °C, especially the increased K content

could severely reduce the NO adsorption performance (from $6.6~\mu mol$ of 0.5K-Pd/SSZ-13 to $3.6~\mu mol$ of 1.5K-Pd/SSZ-13). However, the NO₂ adsorption ability was not mainly affected by the addition of K. With increasing the temperature, the trapped NO and NO₂ also desorb simultaneously at about 200 °C, and the respective NO desorption amounts are $2.5\sim1.4~\mu mol$ and NO₂ desorption amounts are $3.6\sim2.4~\mu mol$ for K-Pd/SSZ-13 sample. After NO completely desorbs above 270 °C, a little negative NO peaks below 210 ppm are observed over these K-Pd/SSZ-13 samples along with an increase in NO₂ content, which indicates the NO could be converted to NO₂ over K-Pd/SSZ-13 samples at high temperatures. This is due to the enhanced oxidation of NO to NO₂ by formed PdO.

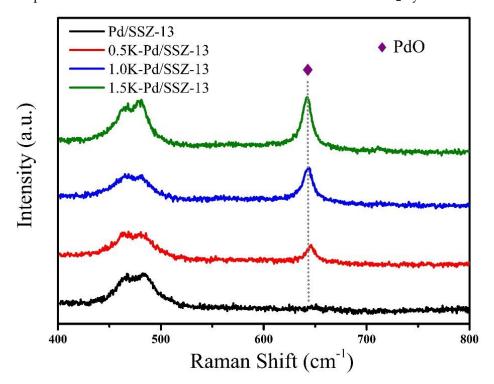
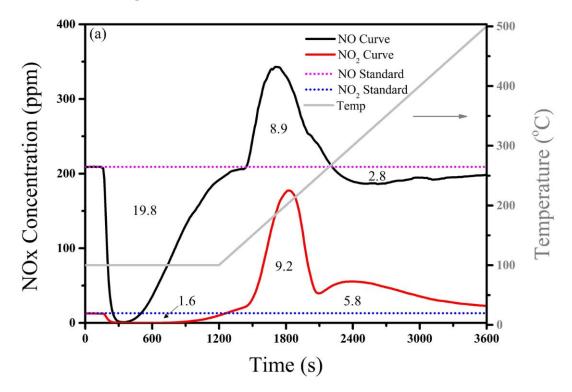
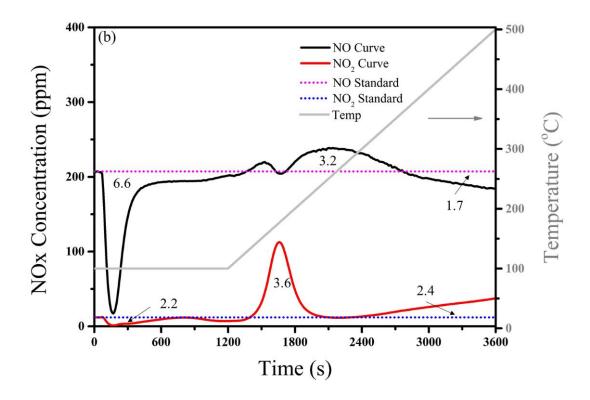


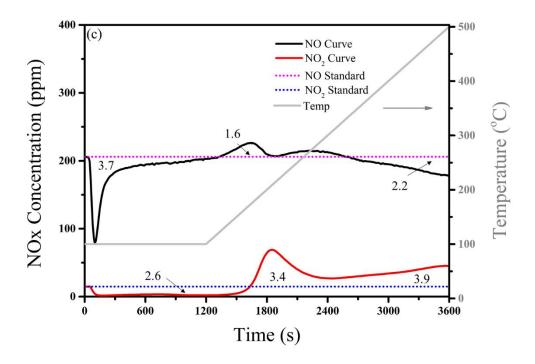
Figure 4. Raman spectra of the Pd/SSZ-13 and K-deactivated samples.

To better simulate the actual after-treatment condition, 5% H₂O was added to the feed gas to evaluate the water tolerance of as-prepared Pd/SSZ-13, and the PNA performance is displayed in Figure 6. Compared to the adsorption ability of fresh Pd/SSZ-13, the addition of H₂O significantly suppresses the NO adsorption on Pd/SSZ-13, as evidenced from the rapid NO saturation adsorption and much smaller total adsorption capacity. In contrast, the NO₂ adsorption is found to be less affected by H₂O. In the ramping process, a second NO adsorption peak centered at 200 °C is clearly displayed. Combined with the fact that H₂O completely desorbs at around 180 °C shown in Figure S8, it is convictive to state that H₂O competes with NO to adsorb on active Pd sites at 100 °C and thus adversely affects the NO storage capacity. Immediately upon the H₂O desorption from adsorption sites that occurs at a higher temperature, the NO could be trapped again. Even though the total NO adsorption amount is still not comparable to those tested in the absence of H2O based on the calculated amount shown in Figure 5a, probably due to the temperature above $180\,^{\circ}\mathrm{C}$ is too high for the full adsorption of NO. With further increasing the temperature to 250 °C, an evident NO release is found, which is quite opposite for the observation in Figure 5a, indicating the oxidation of NO to NO₂ is completely suppressed in the presence of H₂O. When it comes to the NO₂ desorption, only a small peak appears at 190 °C. Considering most Pd active sites are occupied by H_2O during the storage step, it is reasonable to estimate that the desorbed NO₂ mainly comes from physical adsorption sites such as pores and channels or the reaction between NO and the zeolite substrate. As proved by the PNA performance of H-SSZ-13 shown in Figure S9, an evident NO₂ desorption peak centering

at 170 $^{\circ}$ C is depicted and the amount of formed NO₂ (3.4 μ mol) is larger than that of the adsorbed (0.6 μ mol), proving the pure zeolite without Pd addition could still interact with NO and release respectable NO₂.







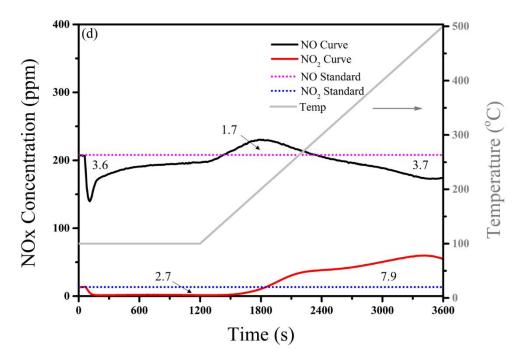


Figure 5. Transient NO_x adsorption at 100 $^{\circ}$ C and temperature programmed desorption of (a) Pd/SSZ-13 and K-deactivated samples (b) 0.5K-Pd/SSZ-13, (c) 1.0K-Pd/SSZ-13 and (d) 1.5K-Pd/SSZ-13.

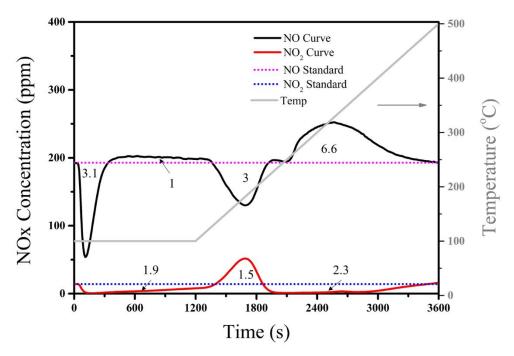


Figure 6. Transient NO_x adsorption at 100 °C and temperature programmed desorption of as-prepared Pd/SSZ-13 when 5% H_2O is added to the flow gas.

4. Conclusions

In this work, the deactivation effect of potassium and water on Pd/SSZ-13 was studied. A series of potassium loaded Pd/SSZ-13 samples were prepared for the NO $_{\rm X}$ adsorption ability. The Raman result demonstrated that the loading of potassium could result in the sintering of Pd species, while the XRD, NMR and BET results indicated the structure of SSZ-13 was stable and the texture parameter of Pd/SSZ-13 sample is reduced after potassium loading. Among the prepared K-Pd/SSZ-13 samples, those with free potassium are the best in NO $_{\rm X}$ storage with poor water tolerance. Overall, the weakened NO $_{\rm X}$ storage performance over K-deactivated Pd/SSZ-13 could be attributed to the transformation of Pd²⁺ to PdO cluster, which was promoted by the increase in potassium content. Besides, the H $_{\rm 2}$ O was also found to have a negative effect on Pd/SSZ-13 due to the competitive adsorption with NO $_{\rm X}$. As a result, the hydrophobicity is significant for the zeolite-based PNA material. The research outcomes give us new insights into the poisoning mechanism of potassium and H $_{\rm 2}$ O for NO $_{\rm X}$ adsorption and could guide the design of efficient PNA materials to control NO $_{\rm X}$ emission during cold start stage.

Supplementary Materials: The following supporting information can be downloaded at: https://www.mdpi.com/article/10.3390/pr10020222/s1, Figure S1: N_2 physisorption isotherms of Pd/SSZ-13 and K deactivated samples; Figure S2: Pore distributions of Pd/SSZ-13 and K deactivated samples; Figure S3: Standard deviation values of 0.5K-Pd/SSZ-13; Figure S4: Standard deviation values of 1.0K-Pd/SSZ-13; Figure S5: Standard deviation values of 1.5K-Pd/SSZ-13; Figure S6: Transient NO_x adsorption at 100 °C and temperature programmed desorption of Pd/SSZ-13 without O_2 in the heating up period; Figure S7: Transient NO_x adsorption at 100 °C and temperature programmed desorption of Pd/SSZ-13 without O_2 in the whole test; Figure S8: Transient O_x adsorption at 100 °C and temperature programmed desorption of the Pd/SSZ-13 catalysts; Figure S9: Transient O_x adsorption at 100 °C and temperature programmed desorption of the H-SSZ-13 catalysts; Table S1: The surface area and pore volume of the samples.

Author Contributions: C.F. and J.M. designed the experiment, characterized samples, and wrote the manuscript. Q.W. helped to synthesize samples and test the PNA performance. J.C. and J.L. offered suggestions and revised the manuscript. All authors have read and agreed to the published version of the manuscript.

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Article

Catalytic Oxidation of NO by Ozone over Mn-Ce/Al₂O₃/TiO₂ Catalyst

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Abstract: In this study, Mn-Ce/Al₂O₃/TiO₂ catalyst prepared by impregnation method was used for synergistic O₃ oxidation NO. The catalyst prepared by impregnating Al₂O₃/TiO₂ at a Mn:Ce molar ratio of 4:1 showed the best catalytic activity. The catalyst performance showed that when the molar ratio of Mn:Ce was 4:1 and the volume ratio of O₃:NO was 1:4, the removal rate of NO could reach 63%, which could increase the removal rate by 40% compared with that of NO oxidized by O₃ alone. BET, XRD, and TEM characterization results showed that when the molar ratio of Mn:Ce was 4:1, the catalyst specific surface area, and pore capacity were the largest. A large amount of MnOx and CeOx were distributed on the catalyst surface. The XPS analysis showed that the oxidation-reduction and oxygen vacancy of Mn (IV)/Mn (III)/Mn (II) and Ce (IV)/Ce (III), had a synergistic effect on the decomposition of O₃ into reactive oxygen species(O*), thus improving the catalytic capacity of Mn-Ce/Al₂O₃/TiO₂ catalyst for O₃. The O₂-TPD analysis showed that the oxygen vacancies and oxygen species in the catalyst could be used as the active point of decomposition of O₃ into O*. The experimental results show that the prepared catalyst can significantly improve the efficiency of ozone oxidation of NO and reduce the amount of ozone. The catalyst can be applied to ozone oxidation denitrification technology.

Keywords: Mn-Ce-based catalyst; catalytic oxidation of NO; process analysis

1. Introduction

With the development of society, the energy demand is increasing. Clean energy, renewable energy, etc., are constantly proposed, and traditional energy sources are mainly non-renewable resources such as coal and oil. Biomass is a new environmentally friendly fuel that is gradually being used. Biomass energy has the advantages of easy storage, stable combustion, and low pollutant emissions compared to traditional energy sources [1,2]. Nowadays, the use of biomass energy is increasing [3–5], such as oil palm, coconut shells, grains, livestock manure, green waste, etc. [6,7]. At present, the main application scenario of biomass in China is mainly boiler combustion, and the mixture of biomass and traditional coal combustion can reduce NO and SO₂ emissions [8,9]. Although the concentration of air pollutants emitted from biomass boilers is lower compared to traditional coal-fired boilers, existing studies show that NOx emissions from biomass boilers are between 200–500 mg/m³, and meeting the emission standards still requires treatment. At present, most biomass boilers in China have not carried out flue gas denitrification. A small number of enterprises use traditional SNCR denitrification technology, but there are a series of problems such as corrosion of the boiler. A small number of enterprises use SCR denitrification technology, but there are problems such as easy clogging and catalyst poisoning [10]. Some enterprises also use ozone (O₃) oxidation denitrification technology, but there are problems such as high O₃ consumption and high operating costs. At present, China lacks economical and efficient treatment technologies for the removal of flue gas nitrogen oxides from biomass boilers.

Given this aforementioned problem, relevant researches have been carried out at home and abroad. One of the directions is to develop suitable catalysts to improve the oxidation performance of O₃ and reduce the usage of O₃. O₃ oxidation for the removal of pollutants generally works in conjunction with associated catalysts to achieve high removal efficiencies. O₃ oxidation efficiency is mainly affected by O₃ concentration and flue gas temperature [11]. For common active components of catalysts, such as Mn-based catalysts, Mn mainly contributes to the decomposition of O₃ into reactive oxygen ions to participate in oxidation [12]. Low oxidation state Mn compounds in Mn/ γ -Al₂O₃ catalyst contribute to the decomposition of O₃ to promote the oxidation of pollutants [13]. Under the co-treatment of NO by TiO₂ catalyst and a high concentration of O₃, the TiO₂ catalyst contributes to the transformation of NO₂ into N₂O₅ [14]. When the volume ratio of O₃:NOx > 1.57, the oxidation rate of NO can reach 95% under the synergistic action of MnOx/Al₂O₃ catalyst and O_3 [15], but too high a concentration of O_3 can produce leaks. V_2O_5 -(NH₄)₂V₆O [16] catalyst was used to synergistically oxidize NO with O₃, when the volume ratio of NO: $O_3 = 2:1$, the oxidation efficiency of NO could be the highest, and the O_3 escape was less than 1 ppm 16. In terms of flue gas treatment, after flue gas was treated by wet flue gas desulfurization (WFGD), Mn-Ce/TiO₂ catalyst was used to oxidize NOx with O₃, and the removal rate of NOx could reach 77.1% [17]. The synergy of O₃ and catalyst has a good effect on the treatment of gas pollutants. In practical application, it is risky to use a high concentration of O₃ in pollutant treatment, and it costs a lot to the economy. Therefore, it is necessary to prepare catalysts that can adapt to lower O₃ concentrations and have higher treatment efficiency.

The purpose of this experiment is to study the effect and process mechanism of catalysts promoting O_3 oxidation of NO. Catalysts with different ratios of active components (Mn:Ce = 1:2, Mn:Ce = 2:1, Mn:Ce = 4:1, Mn:Ce = 5:1) were prepared by impregnation method. The performance of catalysts was investigated by different characterization methods, and the mechanism of catalysts to enhance ozone oxidation of NO was researched. The study can provide theoretical data support for the research on ozone oxidation denitrification technology of biomass boiler flue gas.

2. Materials and Methods

2.1. Preparation of Catalysts

Mn-Ce was selected as the main active component of the catalyst and prepared by the impregnation method. $Mn(NO_3)_2$ and $CeN_3O_9\cdot 6H_2O$ were used as reagents, and nano titanium dioxide and Al_2O_3 were used as carriers. The carrier molar ratio was m (Al_2O_3) :m $(TiO_2) = 1:1$, the mess ratios of m (active component):m (carrier) = 1:1. The active component molar ratios were n (Mn:Ce) = 1:2, n (Mn:Ce) = 2:1, n (Mn:Ce) = 4:1, n (Mn:Ce) = 5:1, and the relevant information of the reagents are shown in Table 1. The weighed $Mn(NO_3)_2$ and $CeN_3O_9\cdot 6H_2O$ were fully mixed in 40 mL deionized water, and then the carrier was added, fully mixed, and stirred for 4 h at 700 RPM. After mixing, the water was filtered and washed alternately with C_2H_6O and deionized water. Then, it was placed in a $100~^{\circ}C$ oven and dried for 2 h, then calcined for 2 h in a muffle oven at $300~^{\circ}C$, cooled, removed, and finally ground and screened. $Mn-Ce/Al_2O_3/TiO_2$ catalysts with different proportions of active components were prepared (Mn:Ce = 1:2, Mn:Ce = 2:1, Mn:Ce = 4:1, Mn:Ce = 5:1 referred to as catalysts).

Table 1. Reagents used in the experiments and purity.

Name of the Reagent	Source of Reagent	Purity
Mn(NO ₃) ₂	Maclean Biochemical Technology Co., Ltd., Shanghai, China	AR
$CeN_3O_9 \cdot 6H_2O$	Aladdin Biochemical Technology Co., Ltd., Shanghai, China	99.95%
Nano titanium dioxide	Hechan Trading Co., Ltd., Guangzhou, China	AR
Al ₂ O ₃ (α -crystalline about 90%, γ -crystalline about 10%)	Damao Chemical Reagent Factory., Tianjing, China	AR
C_2H_6O	Lingfeng Chemical Reagent Co., Ltd., Shanghai, China	AR

2.2. Experimental Setup

The experimental setup consists of O_3 generator and catalytic oxidation adsorption platform, as shown in Figure 1.

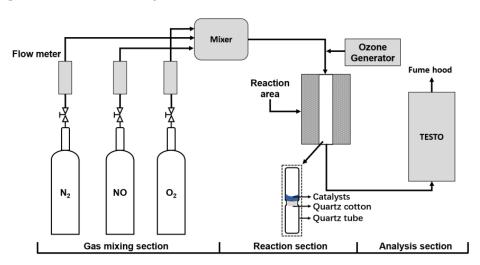


Figure 1. Experimental setup and flow chart.

The O_3 required for the experiment was generated from an ozone generator (Feige Environmental Protection Technology Co., Ltd., Guangzhou, China). After the concentration of O_3 was measured by the ozone analyzer (Zhipu Automation Technology Co., Ltd., Zibo, China), it was passed into the catalytic oxidation adsorption platform. The gas pipeline in the experimental platform was mainly stainless steel, and the gas inflow rate was controlled by a flow meter. N_2 (99.9% N_2 , Yuejia Gas Co., Ltd., Guangzhou, China), NO (4.01% NO + nitrogen balance, Yuejia Gas Co., Ltd., Guangzhou, China), and O_2 (99.9% O_2 , Yuejia Gas Co., Ltd., Guangzhou, China) were mixed in the mixing zone. The mixer can be heated and kept warm as needed. The simulated flue gas was mixed with O_3 before entering the reactor. A quartz tube was placed in the middle of the reactor, and quartz wool was arranged in the middle of the quartz tube as support. The catalyst was evenly placed on the upper part of the quartz wool. During the experiment, the gas passed through the catalyst from top to bottom, and after the gas reacted, the change in the concentration of the exhaust gas was detected by the TESTO 350.

2.3. Catalyst Performance Test

The simulated total flue gas flow rate was 1 L/h, O_2 concentration was 13%, and the volume ratio of O_3 :NO = 1:2, 1:3, 1:4, the O_3 flow rate was 1 L/h, a total of 2 L gas passes through the catalyst, and gas hourly space velocity (GHSV) was 60,000 h⁻¹. The initial

incoming NO concentration was 300 ppm, and the O₃ concentration was 100 ppm. By adjusting different O₃:NO ratios, the main oxidation efficiency was expressed as NO_[removal].

$$NO_{[removal]} = \frac{NO_{[a]} - NO_{[b]}}{NO_{[a]}} \times 100\%,$$
 (1)

where $NO_{[a]}$ was the concentration of NO at the inlet; $NO_{[b]}$ was the concentration at the exit of O_3 (with catalyst).

The main mechanism of the reaction between O₃ and NO was as follows [14]:

$$NO + O_3 \rightarrow NO_2 + O_2, \tag{2}$$

$$NO_2 + O_3 \to NO_3 + O_2,$$
 (3)

$$NO_2 + NO_3 \rightarrow N_2O_5, \tag{4}$$

$$N_2O_5 \to NO_3 + O_2$$
, (5)

$$NO + NO_3 \rightarrow 2NO_2, \tag{6}$$

2.4. Characterization of Catalysts

Specific surface area and pore size were determined by Micromeritics ASAP 2020 Surface Area and Porosity Analyzer. XRD using D8 ADVANCE X-ray diffractometer from Bruker, Germany. TEM was measured using a JEM 2100F instrument with an accelerating voltage of 200 KV and an electron wavelength of 0.0251 Å. XPS was determined using Thermo Scientific Escalab 250Xi. O₂-TPD was determined using MicroActive for AutoChem II 2920 Version 6.01.

3. Results

3.1. Morphology Analysis of Catalysts

Table 2 mainly shows the BET surface area, total pore volume, and average pore size of Mn-Ce/Al₂O₃/TiO₂ catalyst samples with different active component ratios. The specific surface area and pore volume of the catalyst reached the maximum when the molar ratio of Mn:Ce =4:1, but when Mn:Ce =5:1, the specific surface area and pore size of the catalyst began to decrease. The results indicated that when the molar ratio of Mn:Ce =4:1, the carrier has reached the maximum load, and the active component cannot be fully loaded on the carrier when Mn is excessive, and the loading effect is poor. Figure 2a,b shows the N₂ adsorption-desorption isotherms and corresponding pore size distribution curves of Mn-Ce/Al₂O₃/TiO₂. It can be seen from Figure 2a that the N₂ adsorption and desorption isotherms of Mn-Ce/Al₂O₃/TiO₂ with different ratios of active components showed similarly. The first half of the isotherm was similar to the type II isotherm, and the second half was the type IV (a) isotherm, which was the combination of type II and type IV (a), which indicated that there were mesopores (2~50 nm) in the sample. In the relative pressure (P/P_0) range of 0.8~1.0, the shape of the hysteresis loop on the IV (a) isotherm was H3 type. The H3-type hysteresis loop was formed by the stacking of nanoblocks, which indicated the presence of fracture holes, and this analysis was consistent with the results of the TEM (Figure 3). In addition, Mn-Ce/ Al_2O_3 /Ti O_2 has higher adsorption at the relative pressure (P/P_0) of 1, indicated that the sample contains macropores. Figure 2b shows the pore size distribution of the sample. It can be seen from the figure that Mn-Ce/Al₂O₃/TiO₂ has a wide peak range, which was concentrated at 20~50 nm and 60~90 nm, and the results showed that the layered mesoporous/macroporous structure was formed. Table 1 shows the distribution of specific surface area, pore volume, and pore size of the sample. The specific surface area and pore volume increased with the increase of Mn:Ce molar ratios from 1:2 to 4:1. However, the specific surface area and pore volume of Mn-Ce/Al₂O₃/TiO₂ decreased with further increasing of Mn:Ce molar ratios, because the agglomeration of the excess MnOx nanoparticles caused the blockage of some mesopores. It has been generally

acknowledged that the high specific surface areas were beneficial to promote the catalytic performance by offering more active sites.

Table 2. Catalyst pore structure data for different activity group distribution ratios.

Sample	S _{BET} (m ² /g)	V _p (cm ³ /g)	D _p (nm)
Mn:Ce = 1:2	27.564	0.230	43.87
Mn:Ce = 2:1	30.131	0.269	45.25
Mn:Ce = 4:1	52.080	0.346	34.00
Mn:Ce = 5:1	26.134	0.229	41.61

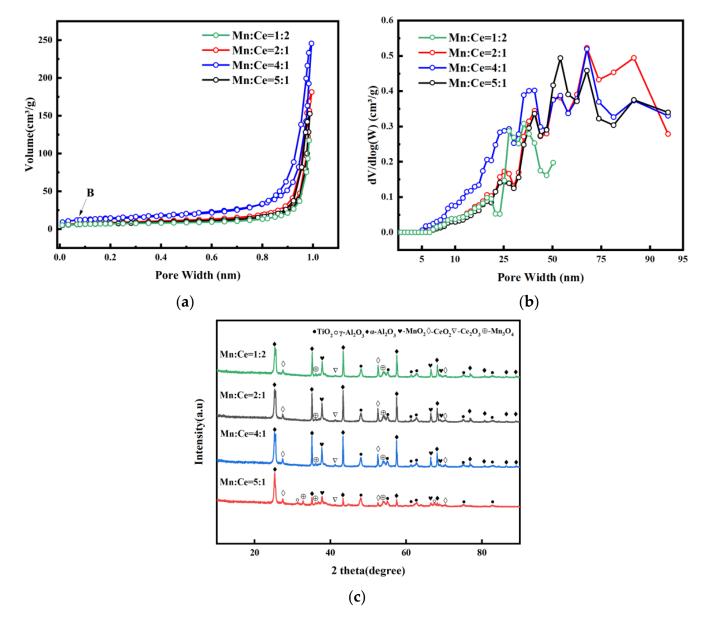


Figure 2. (a) N_2 adsorption and desorption isotherms of Mn-Ce/Al₂O₃/TiO₂ catalyst; (b) Pore size distribution curves of Mn-Ce/Al₂O₃/TiO₂ catalyst; (c) XRD patterns for Mn-Ce/Al₂O₃/TiO₂ catalyst.

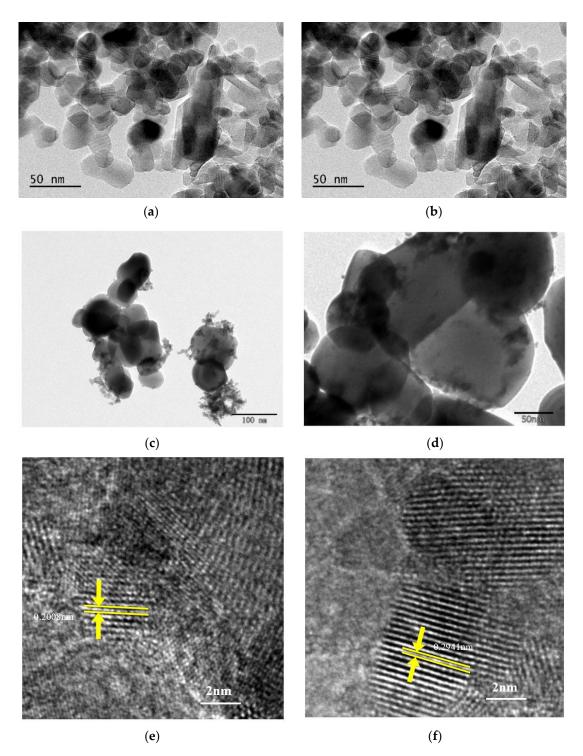


Figure 3. TEM images of Al_2O_3/TiO_2 (**a**,**b**); TEM images of Mn-Ce(4:1)/ Al_2O_3/TiO_2 (**c**,**d**); HRTEM images of Mn-Ce(4:1)/ Al_2O_3/TiO_2 (**e**,**f**).

XRD and TEM were used to analyze the structure of oxide and carrier components in the catalyst. Figure 2c shows the XRD patterns of catalysts prepared under the different molar ratios of Mn:Ce. XRD peaks at $2\theta=25.584$, 37.784, 43.362, 57.581, 70.351, 76.880, 84.375, 86.375, 89.018 are attributed to α -Al₂O₃ (JCPDS 10-0173). XRD peaks at $2\theta=31.988$, 66.761 are attributed to the γ -Al₂O₃ (JCPDFs 29-0063). There is no γ -Al₂O₃ peak in the XRD results of Mn:Ce = 1:2, Mn:Ce = 2:1, Mn:Ce = 4:1, the main reason may be that Mn ions promote the conversion of γ -alumina [18]. However, γ -Al₂O₃ was detected at Mn:Ce = 5:1 and γ -Al₂O₃ appeared at $2\theta=31.988$, 66.761. The possible reason is that the

interaction between Mn-Ce is strengthened [19], and the effect of Mn ions is weakened, so γ -Al₂O₃ was preserved. XRD peaks at 20 = 48.049, 53.890, 62.119, 62.688, 75.029, 82.659, are attributed to the anatase TiO_2 (JCPDS 21-1272). XRD peaks at $2\theta = 31.015$, 36.085, 53.859, corresponding to 200, 211, 312 of Mn₃O₄ (JCPDFs 24-0734). When Mn:Ce = 5:1, the peaks of Mn₃O₄ began to increase (a diffraction peak of Mn₃O₄ appeared at 32.441). With the increase of the amount of Mn ion recombination, the Mn₃O₄ phase increased, mainly due to the coexistence of MnO₂ and Mn₃O₄ phases [20]. XRD peaks at $2\theta = 37.685$, 66.815, 68.594, corresponding to 011, 310, 130 of MnO₂ (JCPDFs 50-0866) [21]. According to the calculation results of the Scherrer equation, it was found that the crystalline size was 17.8 nm at Mn:Ce = 1:2, 15.7 nm at Mn:Ce = 2:1, 16.3 nm at Mn:Ce = 4:1, and 13.8 nm at Mn:Ce = 5:1. It can be seen that in the case of Mn:Ce = 5:1, its crystalline size was the smallest. From the crystallinity and crystalline size of MnO₂, it can be seen that the crystallinity of MnO₂ decreased and the grain size decreased, indicating that the increase of Mn:Ce ratio inhibited the growth of MnO₂ crystalline [22]. At the same time, combined with the removal efficiency of NO under different Mn:Ce, it can be seen that the change of crystallinity of MnO₂ in the catalyst has a certain influence on the catalytic performance of the catalyst. In addition, XRD peaks at $2\theta = 37.868$, corresponding to 332 of Ce₂O₃ (JCPDFs 49-1458). XRD peaks at $2\theta = 27.334$, 52.649, and 70.478, corresponding to 112, 006, and 226 of CeO₂ (JCPDFs 44-1001). With the increase of Mn content, the peak intensity of CeO₂ changed slightly. It is most obvious at 52.649, possibly because the crystallinity of CeO₂ decreased due to the limitation of the crystallite growth of CeO₂ with the increase of the recombination amount of Mn ions [13].

It can be seen from the TEM of Figure 3a,b that the Al₂O₃/TiO₂ was a uniform size nanoblock. The Al₂O₃/TiO₂ nanoblocks ranged from 45–80 nm, and the average nanoblock size was about 60 nm, and it can be clearly seen that there was an obvious heterojunction between Al₂O₃ and TiO₂. It can be seen from Figure 3c,d that the active components of Mn-Ce were uniform nanospheres. The average diameter of the nanospheres was about 2 nm, and the active components of Mn-Ce were evenly distributed on the surface of the Al₂O₃/TiO₂ carrier. The Mn-Ce like particles and Al₂O₃/TiO₂ like blocks were observed, which indicated that the complex contained two morphologies: particle and bulk. Figure 3e,f shows the typical HRTEM image of Mn-Ce(4:1)/Al₂O₃/TiO₂. The observed spacing between the lattice planes of the sample was measured to be 0.2008 nm and 0.2941 nm, matched with (312) crystal plane of Mn₃O₄ and (310) crystal plane of MnO₂, respectively. Therefore, the morphology of Mn-Ce/Al₂O₃/TiO₂ prepared by impregnation method was uniform, the active components were evenly dispersed, and no agglomeration occurred, which indicated that the simple impregnation method can be used to prepare the nano-catalyst with uniform morphology. At the same time, combined with XRD analysis, it can be seen that there was a mutual reaction between the Mn-Ce active component and the carrier Al₂O₃/TiO₂, and there was an interfacial link between the components.

3.2. Catalyst Performance Analysis

Figure 4a shows the efficiency of catalysts with different Mn:Ce molar ratios for the catalytic ozonation of NO when the volume of O_3 :NO = 1:4. As can be seen from Figure 4a, when the volume ratio of O_3 :NO remained unchanged, the temperature had a certain influence on NO removal. With the increase of temperature, NO removal by different ratios of active component catalysts changed greatly. Overall, the Mn-Ce (4:1)/ Al_2O_3 /TiO₂ catalyst was more stable and efficient than other catalysts for NO removal. Different components had a great influence on NO removal, and when the molar ratio of Mn:Ce = 1:4, the catalyst had a good and stable performance [13]. Low-concentration ozone (the volume ratio of O_3 :NO < 2, O_3 concentration < 150 ppm) was mainly used in this experiment. According to the experimental data, the sum of the volume concentrations of NO and NO₂ after the reaction was equivalent to the volume concentration of NO before the reaction. It can be seen that ozone mainly oxidized NO to NO₂, and there were no other types of N-containing oxides. The reaction of ozone oxidation of NO was shown in Equation (2) [11].

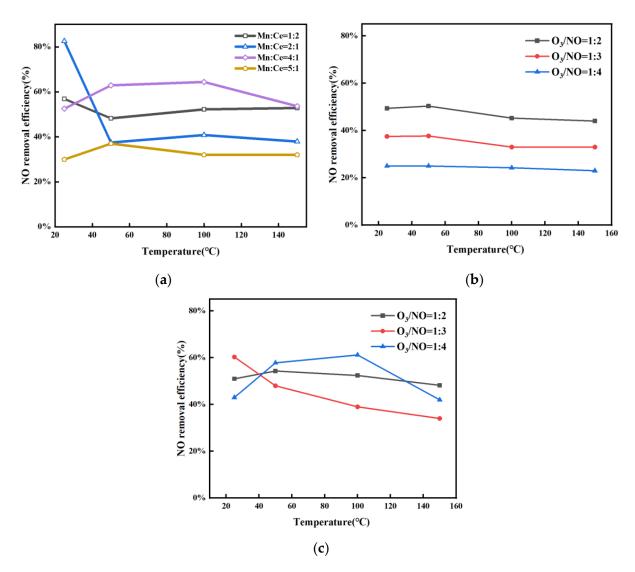


Figure 4. (a) The efficiency of catalysts with different Mn:Ce molar ratios for the catalytic ozonation of NO when the volume of O_3 :NO = 1:4; (b) The effect of increasing the ratio of O_3 on NO removal without catalyst; (c) Under the synergistic catalysis of Mn-Ce (4:1)/Al₂O₃/TiO₂ catalyst, increasing the ratio of O_3 on NO removal Impact.

Figure 4b shows the effect of increasing the ratio of O₃ on NO removal without a catalyst. As can be seen from Figure 4b, when O₃:NO = 1:4, the average NO removal rate was 24%, when $O_3:NO = 1:3$, the average NO removal rate was 35%, and when $O_3:NO = 1:2$, the average removal rate of NO was 47%. With the increased O₃ ratio, the removal rate of NO increased gradually. Figure 4c shows the improvement of NO removal rate of O₃ under the co-catalysis of Mn-Ce $(4:1)/Al_2O_3/TiO_2$ catalyst. It can be found that under the catalysis of Mn-Ce $(4:1)/Al_2O_3/TiO_2$ catalyst, when $O_3:NO = 1:4$, the average NO removal rate was 51%, and when $O_3:NO = 1:3$, the average NO removal rate was 45%. When $O_3:NO = 1:2$, the average NO removal efficiency was 51%. Compared with Figure 4b,c, it can be seen that under the action of the catalyst, with the increase of O₃ concentration, the NO removal rate decreased. This is due to the fact that under the conditions of higher concentration of ozone, the initial NO₂ concentration was relatively high, and then the catalyst is easier to catalyze ozone to promote the conversion of NO₂ to N₂O₅, which reduced the reaction between O₃ and NO, and reduced the removal rate of NO [15]. Therefore, the conversion of NO to NO₂ was more readily promoted at lower ozone concentrations in the presence of catalysts. This study provided an opportunity to improve NO removal using catalyst catalysis at lower ozone concentrations, both to improve ozone utilization and to reduce ozone leakage.

The removal of NOx by ozone oxidation + alkali absorption in the presence of catalyst is shown in Figure 5. When the initial NO concentration was 200 ppm, the volume ratio of O_3 :NO was 1:4, the molar ratio of Mn:Ce was 4:1, the concentration of NaOH was 5 wt%, the NO outlet concentration was 36 ppm, the NO₂ emission concentration was 7 ppm, and the overall NOx emission concentration was 43 ppm, which could meet the relevant flue gas emission requirements. The main reaction equations for NO and NO₂ in NaOH solution are shown in Equations (7) and (8). As time goes on, the removal efficiency of NO₂ gradually decreased, but remained above 85% overall, while the removal efficiency of NO increased gradually with time. Higher concentrations of NO₂ mainly occurs in Equation (8). With the progress of the reaction, the pH of the absorption solution gradually decreased, and Equation (7) gradually became the main reaction. So the removal rate of NO gradually increased and the amount of NO₂ removed decreased [11].

$$NO + NO_2 + 2NaOH \rightarrow 2NaNO_2 + H_2O, \tag{7}$$

$$2NO_2 + 2NaOH \rightarrow NaNO_2 + NaNO_3 + H_2O, \tag{8}$$

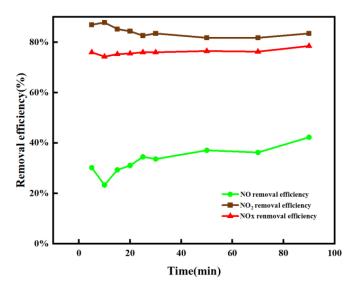


Figure 5. Removal of NOx by NaOH solution (O_3 :NO = 1:4, Mn:Ce = 4:1, 5 wt% NaOH).

The distribution of Mn, Ce, and O elements on the surface of the catalyst was analyzed by XPS. Figure 6a is the XPS spectrum of Mn 2p. The Mn 2p XPS spectra showed two characteristic peaks of Mn 2p1/2 and Mn 2p3/2. The Mn 2p3/2 peak at 640.3 ev, 642.8 ev, 643.4 ev are attributed to Mn^{2+} , Mn^{3+} , and Mn^{4+} species [23]. The Mn 2p1/2 peak at 652.2 ev, 653.1 ev, 653.9 ev are attributed to Mn Mn²⁺, Mn³⁺, and Mn⁴⁺ species [24]. Figure 6a,b showed the XPS spectra of the catalyst (Mn:Ce = 1:2). Mn^{4+} was detected only at 638.3 eV, so the Mn ion content of Mn:Ce = 4:1 catalyst was more, and mainly increased Mn³⁺. Related studies have shown that Mn⁴⁺ can promote the generation of reactive oxygen species (O*) from ozone, and the presence of Mn³⁺ lead to the generation of oxygen vacancies and promoted the generation of O* from ozone, both of which can enhance the performance of NO oxidation by ozone [25]. Therefore, Mn:Ce = 4:1 catalyst is more efficient than Mn:Ce = 1:2 catalyst in promoting ozonation of NO. Table 3 shows the proportion of Mn ions, Ce ions, and O species in the catalyst calculated based on XPS results. According to its distribution, it can be seen that under Mn:Ce = 4:1, the content of Mn²⁺ is the largest. Under ozone conditions, high proportion of Mn²⁺ promoted the conversion to Mn³⁺ and Mn⁴⁺. Figure 6b is the XPS spectrum of Ce 3d showed two characteristic peaks of Ce 3d5/2 and Ce3d3/2. It can be seen that under Mn:Ce = 1:2, the peaks V'' (887.8 ev), U (881.3 ev), V' (903.7 ev), V'' (907.1 ev), V'''' (908.3 ev) are attributed to Ce^{3+} ; the peaks U^0 (882.3 ev), $U'(886.3 \text{ ev}), U'''(888.4 \text{ ev}), U''''(888.6 \text{ ev}), U'V''''(898.3 \text{ ev}), V(900.8 \text{ ev}), V^0(900.9 \text{ ev}),$

 $V^{\prime\prime\prime\prime}$ (907.3 ev), $V^{\prime}V^{\prime\prime\prime\prime\prime}$ (916.7 ev) are attributed to Ce^{4+} . It can be seen that under Mn:Ce = 4:1, the peaks 880.7 ev, 884.0 ev, 885.5 ev, 886.0 ev, 900.7 ev, 903.9 ev, 907.1 ev are attributed to Ce^{3+} ; the peaks 881.1 ev, 900.8 ev, 900.9 ev, 916.0 ev, 916.7 ev are attributed to Ce^{4+} . According to Table 3, when Mn:Ce = 4:1, Ce^{3+} accounted for a large proportion, and a large amount of Ce^{3+} helped to generate O^{2-} , and O^{2-} helped to promote the mutual conversion between Mn ions, which in turn promoted the decomposition of ozone into O^* [26], which indirectly indicated that the Mn:Ce = 4:1 catalyst has higher catalytic activity. In Figure 6c, the XPS patterns of O 1 s showed the presence of two types of surface oxygen in the Mn-Ce/Al₂O₃/TiO₂ catalysts. The fitted peaks could be attributed to lattice oxygen O (lat) (529.5 eV) and chemisorbed oxygen (abs) (532.17 ev, 532.5 ev). It was well recognized that O (abs) species were more active in promoting ozone generation of O* than O (lat) due to their higher mobility [27–29]. Figure 6c and Table 3 show that the surface concentration of O (abs) species over Mn-Ce (4:1)/Al₂O₃/TiO₂ was higher than Mn-Ce (1:2)/Al₂O₃/TiO₂, which was another reason for its higher catalytic activity compared with Mn-Ce (1:2)/Al₂O₃/TiO₂.

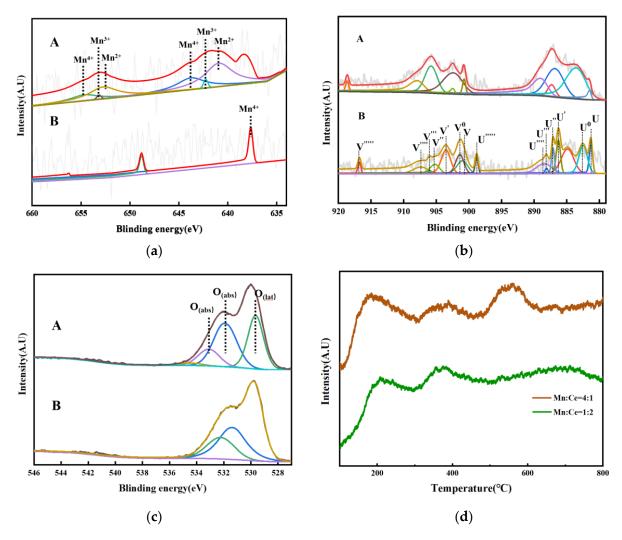


Figure 6. (a) XPS spectra of Mn 2p: A. Mn:Ce = 4:1; B. Mn:Ce = 1:2; (b) XPS spectra of Ce 3d: A. Mn:Ce = 4:1; B. Mn:Ce = 1:2; (c) XPS spectra of O 1 s: A. Mn:Ce = 4:1; B. Mn:Ce = 1:2; (d) O₂-TPD profile of Mn-Ce/Al₂O₃/TiO₂ catalysts (Mn:Ce = 4:1, Mn:Ce = 1:2).

Table 3. Distribution of Mn ions, Ce ions, and O species of synthesis catalysts based on XPS results.

Samples	Mn ²⁺ /(Mn ²⁺ + Mn ³⁺ + Mn ⁴⁺) (%)	Mn ³⁺ /(Mn ²⁺ + Mn ³⁺ + Mn ⁴⁺) (%)	Mn ⁴⁺ /(Mn ²⁺ + Mn ³⁺ + Mn ⁴⁺) (%)	Ce ³⁺ /Ce ⁴⁺	O (lat)	O (lat)/O (abs)
Mn:Ce = $4:1$ Mn:Ce = $1:2$	40.18	26.61 /	33.21	1.29 0.57	38.03 37.65	0.51 0.95

 O_2 -TPD results can be used to represent the type of oxygen species on the catalyst. O (abs) is more easily desorbed than O (lat) and will desorb at lower temperatures. O (abs) generally contains both physically adsorbed oxygen and chemisorbed oxygen, of which physically adsorbed oxygen is usually more easily desorbed than chemisorbed oxygen [30]. As depicted in Figure 6d, two peaks appeared at around 200 °C and 400 °C, which are the characteristic peaks of O (abs); the peak at 600 °C is mainly O (lat). When Mn:Ce = 4:1, more peaks appear when the temperature rises, indicating that there are more oxygen species on the catalyst surface. The desorption capacity of surface oxygen species contributes to improving the oxidation capacity of catalysts.

3.3. Reaction Mechanism

The process mechanism of catalysts promoting O_3 oxidation of NO can be summarized as follows: The catalyst contains large amounts of Mn (II), Mn (III), and Mn (IV). In the ozone atmosphere, Mn (II) and Mn (III) were oxidized and O* was produced at the same time. In combination with Section 3.2, catalyst and ozone have an excellent effect on NO removal, and the effect of O* can be inferred as Equations (9)–(11). NO was combined with O* to form NO \bullet O* in the adsorption state. The adsorbed (NO \bullet O*) will form (NO \bullet O*) $_2$ and react with O_2 in the gas phase to form NO $_2$. The O^{2-} produced by the oxidation reaction between Ce (III) and Ce (IV) in the catalyst contributes to the transformation of Mn (IV) to Mn (II). It can be concluded that the oxidation reaction process of Mn (II) and Mn (III) in the ozone atmosphere is the main reaction promoting the oxidation of NO to NO $_2$. The oxidation-reduction reaction in Ce (III) and Ce (IV) and the oxygen species on the catalyst can promote the oxidation reaction of Mn (II) and Mn (III) in the ozone atmosphere. The reaction pathway is shown in Figure 7. The main reactions here are as follows:

$$NO + O* \rightarrow NO \cdot O*, \tag{9}$$

$$NO \cdot O* + NO \cdot O* \rightarrow (NO \cdot O*)_{2}, \tag{10}$$

$$(NO \cdot O*)_2 + O_2 \rightarrow 2NO_2 + 2O*,$$
 (11)

$$Mn^{3+} + O_3 \rightarrow Mn^{4+} + O_7$$
, (12)

$$Mn^{2+} + O_3 \rightarrow Mn^{3+} + O_7 + O_2$$
, (13)

$$Mn^{2+} + O_3 \rightarrow Mn^{4+} + O^{2-} + O_2,$$
 (14)

$$Mn^{4+} + O^{2-} + O_3 \rightarrow Mn^{2+} + O_2,$$
 (15)

$$Ce^{4+} + Mn^{3+} + O^{2-} \rightarrow Ce^{3+} + Mn^{4+},$$
 (16)

$$Ce^{3+} + O_2 \rightarrow Ce^{4+} + O^{2-},$$
 (17)

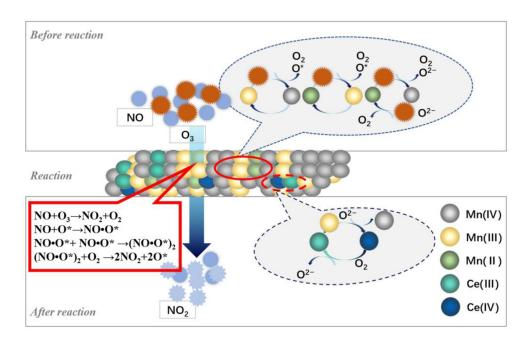


Figure 7. Reaction pathway of Mn-Ce/Al₂O₃/TiO₂ synergistic ozone oxidation of NO.

4. Conclusions

The experimental results show that the catalyst can significantly improve the efficiency of ozone oxidation of NO and reduce the amount of ozone. Based on the experimental results, the main conclusions are as follows:

- 1. The Mn-Ce/Al₂O₃/TiO₂ catalyst was prepared by the impregnation method. The catalysts were characterized by BET, XRD, TEM, XPS, and O₂-TPD. The results show that the catalysts have a large specific surface area (52.080 m²/g) and pore volume (0.346 cm³/g). High-specific surface areas are beneficial to promote the catalytic performance by offering more active sites. The catalyst mainly contains particle and bulk morphology, and the active components (MnOx, CeOx) are uniformly dispersed, and no agglomeration occurs. At the same time, the catalyst contains a large number of CeOx, O (lat), and O (abs) species. The content of MnOx, oxygen species on the surface of the catalyst, is the factor affecting the activity of the catalyst.
- 2. The mechanism study shows that the MnOx content on the catalyst surface is the main factor affecting the catalyst activity. The presence of Mn²⁺ and Mn³⁺ on the surface of the catalyst can promote the decomposition of ozone to produce O*. O²⁻ contributes to the reduction reaction between Mn²⁺ and Mn⁴⁺, and O* and oxygen species on the catalyst surface significantly promote the oxidation of NO to NO₂.
- 3. Under the experimental conditions of flue gas temperature $100-150\,^{\circ}$ C, the molar ratio of Mn:Ce = 4:1, the volume ratio of O₃:NO = 1:4, and the NO removal rate can reach 63%. Compared with the oxidation of NO by ozone alone, the oxidation efficiency of NO can be increased by 40% by adding a catalyst. The experimental results show that the prepared catalyst can significantly improve the efficiency of ozone oxidation of NO and reduce the amount of ozone. After NaOH absorption, the NOx removal efficiency achieves up to 79.6% for the O₃ + Mn-Ce (4:1)/Al₂O₃/TiO₂ method, which can well meet the NOx emission standard in China.

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Review

Application of Stable Isotope Techniques in Tracing the Sources of Atmospheric NO_X and Nitrate

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Abstract: Nitrate is an important component of PM_{2.5}, and its dry deposition and wet deposition can have an impact on ecosystems. Nitrate in the atmosphere is mainly transformed by nitrogen oxides ($NO_X = NO + NO_2$) through a number of photochemical processes. For effective management of the atmosphere's environment, it is crucial to understand the sources of atmospheric NO_X and the processes that produce atmospheric nitrate. The stable isotope method is an effective analytical method for exploring the sources of NO₃⁻ in the atmosphere. This study discusses the range and causes of δ^{15} N data from various sources of NO_X emissions, provides the concepts of stable isotope techniques applied to NO_X traceability, and introduces the use of Bayesian mixture models for the investigation of NO_X sources. The combined application of δ^{15} N and δ^{18} O to determine the pathways of nitrate formation is summarized, and the contribution of $\Delta^{17}O$ to the atmospheric nitrate formation pathway and the progress of combining Δ^{17} O simulations to reveal the atmospheric oxidation characteristics of different regions are discussed, respectively. This paper highlights the application results and development trend of stable isotope techniques in nitrate traceability, discusses the advantages and disadvantages of stable isotope techniques in atmospheric NO_X traceability, and looks forward to its future application in atmospheric nitrate pollution. The research results could provide data support for regional air pollution control measures.

Keywords: nitrogen oxide; nitrogen cycle; atmospheric nitrate; stable isotope

1. Introduction

Human health and daily life have been negatively impacted by $PM_{2.5}$ [1–3]. In view of air pollution, China has taken many measures, and the anthropogenic emission of pollutants has been reduced [4–6]. However, the amount and duration of haze have grown [7]. The composition of atmospheric particulate matter has also changed with the management of the environment. In recent years, the proportion of nitrate in $PM_{2.5}$ has increased significantly, surpassing sulfate and becoming the most abundant component [8]. Winter haze is primarily caused by nitrate, as evidenced by the presence of up to 60% NO_3^- in severe winter haze with $PM_{2.5}$ concentrations above 100 μg m⁻³ [9].

Numerous academic studies have been conducted on NO_X measurement and conversion pathways in order to better understand the issue of NO_X pollution. Nitric acid, a key component of the nitrogen biogeochemical cycle, is formed when atmospheric NO_X ($NO_X = NO + NO_2$) experiences a variety of oxidation reactions and is then deposited to the surface by dry and wet deposition [10]. This process modifies the atmosphere's acid–base balance, favoring the development of acid rain and reducing biodiversity. The nitrates created either adsorb on the alkaline particulate matter to form nitrate or interact with NH_3 in the air to create particulate matter.

1.1. Formation Pathways of Nitrate in Atmospheric Particulate Matter

The gas-phase interaction of NO_2 and OH and the non-homogeneous reaction of N_2O_5 hydrolysis are the two main pathways identified for the formation of nitrate from ambient NO_X , as shown in Figure 1 [11,12].

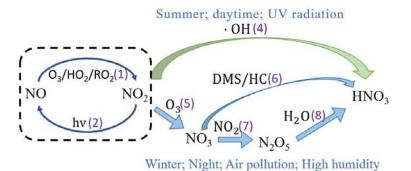


Figure 1. Two reaction pathways for the formation of nitrate from NO_X in the air [10,11]. In this figure, (1) to (6) correspond to the corresponding reactions (1) to (6) below.

The specific reactions are as follows :
$$NO + O_3 \rightarrow NO_2 + O_2$$
 (1)

$$NO_2 + hv \rightarrow NO + O$$
 (2)

$$O + O_2 + M \rightarrow O_3 + M \tag{3}$$

During the day, NO reacts rapidly with O_3 to produce NO_2 , as shown in Reaction (1), NO_2 is photolyzed to produce NO and O atoms as in Reaction (2), and the generated O atoms combine with O_2 to produce ozone. Reaction (3) is the most frequent route for tropospheric O_3 generation.

In Reactions (1)(2), the cyclic reaction between NO and NO₂ reaches a steady state in a short time [13,14], and the concentration of O_3 and the photolysis rate of NO₂ affects the reaction rate in Reaction (1) and (2); the relative concentrations of NO and NO₂ in the atmosphere are affected. NO₂ in the atmosphere also oxidizes to form nitric acid. The formation of nitric acid can be divided into two types: daytime and nighttime. During the day, the reaction in Reaction (4) occurs, and NO₂ is oxidized by OH to form nitric acid:

$$NO_2 + \cdot OH \rightarrow HNO_3$$
 (4)

At night, the concentration of OH is extremely low and NO_2 cannot be oxidized directly to nitric acid. NO_2 is oxidized by ozone to NO_3 (Reaction (5)), which then reacts with dimethyl sulfide (DMS) or hydrocarbons (HC) to produce nitric acid (Reaction (6)), or NO_3 reacts with NO_2 to make N_2O_5 (Reaction (7)), which then hydrolyzes to produce nitric acid (Reaction (8)).

$$NO_2 + O_3 \to NO_3 + O_2$$
 (5)

$$NO_3 + DMS/HC \rightarrow HNO_3$$
 (6)

$$NO_2 + NO_3 \rightarrow N_2O_5 \tag{7}$$

$$N_2O_5 + H_2O \rightarrow 2HNO_3 \tag{8}$$

Particulate nitrate is formed when nitric acid combines with alkaline chemicals in the environment, as shown in Reaction (9).

$$HNO_3 + Alkali \rightarrow NO_3^-$$
 (9)

 O_3 and OH are the major oxidants in the atmosphere, which are closely related to pollutants, such as NO_X , SO_2 , CO, CH_4 , and volatile organic compounds (VOCs), in the atmosphere. Studies have indicated that NO_2 + OH and N_2O_5 + H_2O are the two most important pathways

of tropospheric nitrate generation below 1 km, contributing 41~42% and 28~41% to nitrate generation at the global scale, respectively [15]. As a result of other mechanisms, 6% of nitrate synthesis occurs close to the surface, though they may also take over in some areas [15,16]. In Beijing, the OH route contributed to NO_3 production by about 45.3%, N_2O_5 hydrolysis contributed by about 46.5%, and the NO_3 + HC pathway contributed by about 8.2% [17]. Additionally, in Nanchang, the OH route, N_2O_5 hydrolysis, and NO_3 + HC pathway contributed 37.1%, 33.4%, 60.3%, and 2.6% of the NO_3^- , respectively [18].

1.2. Major Sources of NO_X and Available Analytical Methods

The majority of NO_X 's sources come from anthropogenic and natural sources. Natural sources typically refer to biogenic soil emission, lightning production, and stratospheric transfer. The primary anthropogenic sources include biomass burning, fossil fuel burning, vehicle emissions, and other sources. NO_X emissions in the troposphere have been determined to be mostly caused by human activity, with the burning of fossil fuels responsible for up to 60% of all NO_X emissions globally. Therefore, quantifying the contribution of different emission sources to NO_X emissions is conducive to a better understanding of the atmospheric nitrogen cycle so as to develop effective emission reduction strategies. The reduction of the number of high-polluting sources and the reduction of emissions from low-polluting sources are the two main focuses of the treatment of NO_X sources in the atmosphere. How to determine the source of NO_X in a certain area at a certain time has always been the goal of researchers.

Current work by researchers has focused on four sources of emissions: coal combustion, vehicle emission, biomass burning combustion, and biogenic soil emissions. The main methods for monitoring NO_X in the atmosphere are emission inventory methods, satellite observations, and stable isotope methods. The assessment of emission flux can be achieved with the emission inventory method [19] and the satellite observation method. The emission inventory method has uncertainties in the types of emission sources and emission factors, and even the emission factors of the same emission source under different conditions are quite different [20]. It has been demonstrated that tropospheric NO_X concentrations can be monitored using satellite remote sensing techniques [21]. However, the satellite observation method cannot properly determine the precise sources of NO_X because there are frequently many sources of NO_X emissions in the same area [22]. Both methods can provide a large amount of data and achieve very effective results, but neither method can accurately assess the contributions from different sources.

Stable isotope techniques have the advantages of high measurement accuracy, accurate source resolution, and small measurement error, and their application in various fields has promoted the progress of scientific research. They have steadily developed into a key instrument for researching the source tracing of NO_X emissions in the atmosphere and the mechanism of nitrate creation in the atmosphere, along with the continual advancement of isotope technology, detecting equipment, and analytical methodologies [23–25].

1.3. Analysis of Stable Isotope Techniques and Its NO_X Traceability

The abundance of stable isotopes in a species depends not only on its natural abundance but also on the processes that occurred during the generation of the species. Isotope fractionation is the process whereby an element's isotopes are dispersed among several compounds during a reaction in varying ratios, resulting in slight weight variations amongst the same species. Thus, isotope fractionation can be used to trace information on the origin of species, the processes that produced them, etc. δ is used to indicate isotopic composition values, and the calculation is shown in Equation (10):

$$\delta(\%) = \frac{R_{\text{sample}}}{R_{\text{standard}}} - 1 \tag{10}$$

where R represents the proportion of heavy to light isotopes. The international standard for nitrogen is atmospheric N_2 , and for oxygen is the Vienna Standard Mean Ocean Water (VSMOW).

Different metabolic processes and migratory transformations of atmospheric nitrogen molecules result in nitrogen isotope fractionation, which changes the values of ^{15}N . The value of the δ is positive when the sample is rich in heavy isotopes and negative when the sample is deficient in heavy isotopes.

Combining stable nitrogen isotopes with isotope mixing models has become one of the most reliable tools for quantifying NO_X sources. Since nitrogen isotope fractionation rarely occurs in the process of NO_X conversion to nitrate, $\delta^{15}N$ from different sources is different. According to this concept, we can use $\delta^{15}N$ - NO_3^- to determine the source of nitrate [26,27]. For example, changes in $\delta^{15}N$ - NO_3^- in ice cores by Hastings et al. can clearly indicate a shift in the source of NOx from pre-industrial to modern times. [27]. By measuring $\delta^{15}N$ - NO_3^- and $\Delta^{17}O$ - NO_3^- in shallow ice cores drilled in Antarctica, Cao et al. studied the ability of nitrate isotopes in ice cores to reflect the variation of the ozone column [28]. Zeng et al. determined the proportion of nitrate sources in rainwater in Beijing by studying the δ values of dual isotopes combined with a Bayesian mixing model [29].

Two methods are commonly used to determine the NO_3^- nitrogen to oxygen isotope ratio using the stable isotope method: the bacterial denitrifier method and the chemical reduction method. Both methods measure N_2O gas with less interference, require less sample volume, and allow the simultaneous determination of $\delta^{15}N$ and $\delta^{18}O$.

The bacterial denitrifier method is based on the quantitative production of nitrous oxide gas (N_2O) from nitrate by denitrifying bacteria. The classical denitrification pathway involves the gradual reduction of nitrate (NO_3^-) to nitrite (NO_2^-), nitric oxide (NO_3^-), nitrous oxide (N_2O), and dinitrogen (N_2). In this method, NO_3^- in the sample is converted to nitrous oxide (N_2O) using denitrifying bacteria (Pseudomonas aureofaciens) lacking N_2O reductase activity and then fed into a stable isotope ratio mass spectrometer for analysis [30]. The nitrator method for bacterial denitrification was updated by McIlvin et al. to improve the precision and yield of isotope analysis, and the updated analytical system is shown in Figure 2 and includes a GC-PAL autosampler (CTC Analytics, LEAP Technologies), a custom capture system for the separation and purification of N_2O , and an isotope ratio mass spectrometer (Delta PLUS XP, Finnigan, Germany) [31].

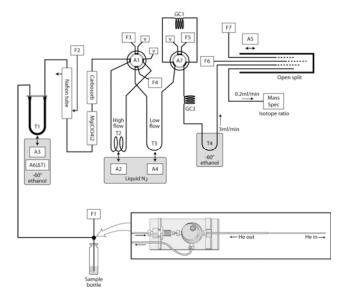


Figure 2. Purge and trap system: T = trap, A = automation controlled by Isodat, F = flow controller, GC = gas chromatogram, V = vent to atmosphere. Inset: custom concentric needle design using the CombiPAL 1 mL syringe holder. Gas flow paths are indicated by arrows. Please refer to text for additional details. Reprinted with permission from Ref. [31]. Copyright 2011 ACS.

The chemical reduction method consists of a two-step reduction for the extracted samples, first to NO_3^- to NO_2^- using Cd and then to NO_2^- to N_2O using an azide-acetate-buffered solution [32,33]. Finally, the reaction is terminated using sodium hydroxide solution (NaOH). With the Precon + Gas Bench II system, the upper layer of N_2O gas in the headspace bottle was blown into MAT253 by an automatic sampler to measure $\delta^{15}N$ and $\delta^{18}O$, and the sample measurement process is shown in Figure 3. Zhao et al. optimized the scheme as follows: NO_3^- is reduced to NO_2^- by HCl-Cd at pH = 8 under the condition of Cl⁻ concentration over 5 M, NO_2^- is reduced to N_2O at pH = 4.5–4.6 in a sodium azide acetate buffer solution, and $\delta^{15}N$ and $\delta^{18}O$ are analyzed by Stable isotope ratio mass spectrometer (MAT253) [34].

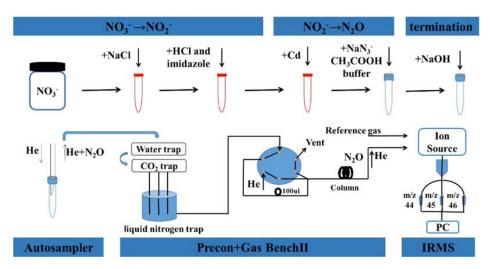


Figure 3. Schematic diagram of nitrate nitrogen and oxygen isotope analysis in atmospheric samples. Reprinted with permission from Ref. [34]. Copyright 2019 Elsevier.

An effective method for examining potential NO_3^- sources in the atmosphere is the stable isotope. Here, we list the $\delta^{15}N$ values for several emission sources and discuss how to locate the source of NO_X emissions using the Bayesian isotope mixing model. The paths of nitrate synthesis were then determined using two techniques that combined $\delta^{15}N$ and $\delta^{18}O$ and $\Delta^{17}O$. Finally, shortcomings of the currently employed techniques are discussed, and recommendations for future isotopic studies of the origins and oxidation processes of atmospheric nitrate are made.

2. Stable Isotope Techniques Determine the $\delta^{15}N$ Values of NO_{χ} in Various Emission Sources

Nitrogen isotopes' accuracy in resolving the source of atmospheric NO_X is dependent on two major aspects. The first relates to the impact of isotope fractionation on the chemical oxidation, transport, and atmospheric N deposition processes, while the second deals with the properties of δ^{15} N-NO_X from various emission sources. δ^{15} N-NO_X is calculated as the following calculation formula in Equation (11), using the calculation of Equation (10):

$$\delta^{15}N - NO_X(\%) = \frac{R_{15}N - NO_X/^{14}N - NO_X}{R_{N_2 - Air}} - 1$$
(11)

Figure 4 summarized the δ^{15} N characteristic values of NO_X emissions from different sources in the available literature, using the δ^{15} N-NO_X values as the X-axis and the different NO_X sources as the Y-axis. The δ^{15} N values for the different emission sources have been summarized in the figure so far, and it can be seen that the δ^{15} N for NO_X emissions from petrol vehicles ranges from -19.4% to 17% and from -23.3% to 8.5% for diesel vehicles. The characteristic δ^{15} N values for the coal combustion process are -5.3% to 25.6%, for natural gas 2.9% to 15.4%, for biomass combustion -11.9% to 5%, and for

the flash process less data is obtained, -0.5% to 1.4%. The data showed that the $\delta^{15}N$ values of NO_X emitted from all sources overlapped with each other in the range, except for the $\delta^{15}N$ values of NO_X emitted from soil, which were in the more negative range. The $\delta^{15}N$ values of NO_X by the same emission source vary considerably due to different N chemical conversion processes. The following section describes the four aspects of vehicle emission, coal and natural gas combustion, biomass burning combustion, and biogenic soil emissions, respectively.

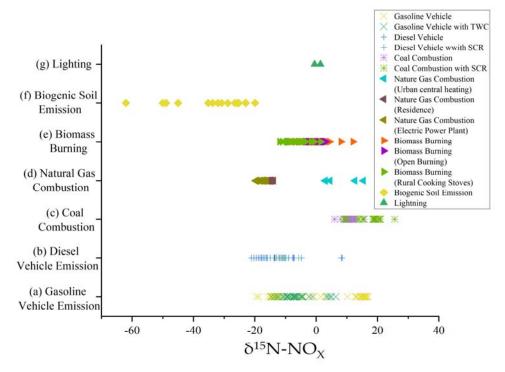


Figure 4. δ^{15} N values for NO_X emissions from different sources. The Y-axis indicates different sources of NO_X emissions and the X-axis indicates the δ^{15} N-NO_X value, with one point representing a measured value; different colors indicate different NO_X generation processes for this source. (a) Walters et al. (2015) [27], Heaton (1990) [35], Moore (1977) [36], Walters et al. (2015) [37], Li et al. (2022) [38]; (b) Chang et al. (2018) [22], Heaton (1990) [35], Walters et al. (2015) [37], Li et al. (2022) [38], Su et al. (2020) [39], Felix et al. (2012) [40], Zong et al. (2020) [41], Widory (2007) [42]; (c) Heaton (1990) [35], Felix et al. (2012) [40], Widory (2007) [42]; (d) Walters et al. (2015) [27], Widory (2007) [42]; (e) Zong et al. (2022) [25], Fibiger (2016) [43], Shi (2021) [44]; (f) Fibiger (2016) [43], Li et al. (2008) [45], Felix et al. (2014) [46], Miller et al. (2018) [47], Su et al. (2020) [48]; (g) Hoering (1957) [49].

2.1. $\delta^{15}N$ of Fossil Fuel Combustion

With a wide range of $\delta^{15}N$ values, fossil fuels, particularly car exhaust and coal combustion exhaust, predominate the NO_X emission inventory. Estimates at the global level show that soils and fossil fuels both contribute about the same amount of NO_X . Additionally, the primary cause of nitrate pollution in cities is NO_X emissions from the combustion of fossil fuels [50]. Different structures of combustion devices will lead to different proportions of NO_X emitted from fossil fuel combustion.

There are two primary sources of NO_X that result from the combustion of fossil fuels: (i) NO_X generated from NO_X inside the fuel (fuel NO_X) and (ii) NO_X generated from atmospheric N_2 oxidation. Different combustion unit configurations can result in different proportions of NO_X sources emitted from fossil fuel combustion (thermal cracking NO_X). For example, NO_X emissions from coal-fired power plants mainly originate from fuel NO_X because their combustion units are at temperatures of $1277{\sim}1402~^{\circ}C$, which are too low to oxidize atmospheric N_2 , while car engines are at temperatures >1727 $^{\circ}C$ and can oxidize atmospheric N_2 , so NO_X emissions from car exhaust are mainly thermal cracking NO_X [35].

Although the mechanism of NO_X generation is similar for different automotive engines, which originate from the conversion of atmospheric N_2 , the $\delta^{15}N$ - NO_X values are also influenced by fuel type, operating conditions, engine type, air-fuel ratio, etc. [51]. In 1977, Moore reported that vehicles equipped with three-way catalytic converters (TWC) emitted NO_X with some $\delta^{15}N$ values of 3.4% to 3.9% [36]. Later, Walters et al. found by comparison that the NO_X concentrations emitted from vehicles equipped with TWC units had a good non-correlation with the $\delta^{15}N$ values because the TWC reacted preferentially with $^{14}NO_X$, giving the remaining emitted NO_X a higher $\delta^{15}N$ value [27].

Heaton reported $\delta^{15}N$ values for the emitted exhaust of cars under load and no load, ranging from -11% to -2% and -13% to -7%, respectively [35]. Walters et al. measured $\delta^{15}N$ -NO $_X$ values for the exhaust of cars as -12.2% to -9.8% for gasoline cars and -23.3% to -2% for diesel cars, respectively [27]. Zong et al. also found the same trend but with different values; they measured the highest $\delta^{15}N$ -NO $_X$ values for LPG vehicles ($-0.1 \pm 1.8\%$), followed by gasoline vehicles ($-7.0 \pm 4.8\%$) and diesel vehicles ($-12.7 \pm 3.4\%$). In addition, they found a significant correlation between $\delta^{15}N$ -NO $_X$ values and NO $_X$ concentrations in vehicle exhausts (p < 0.01). Compared with gasoline engines, the combustion gases of diesel engines mix with air more rapidly, so that only a small fraction of NO $_X$ is decomposed in diesel engines compared with gasoline engines. Additionally, Zong et al. found that the $\delta^{15}N$ values of NO $_X$ emitted from cars in different operating conditions differed, following the trend of warm start ($-5.9 \pm 5.0\%$) > driving ($-7.3 \pm 5.9\%$) > cold start ($-9.2 \pm 2.7\%$) [24]. In summary, the $\delta^{15}N$ characteristic values of NO $_X$ from vehicle exhaust emissions ranged from -23.3% to 17%.

The $\delta^{15}N$ value of NO_X emitted from coal-fired power plants is generally positive because organic nitrogen in coal combustion decomposes into nitrogen-containing reactive substances after combustion to produce NO in the atmosphere, while NO continues to react with nitrogen (NO + N \rightarrow N₂ + O), and in this reaction process, ¹⁴NO is preferentially involved in the reaction, making the remaining NO more enriched ¹⁵N, resulting in a $\delta^{15}N$ value of NO_X emitted from coal-fired power plants positive values [35].

Felix et al. measured NO $_{\rm X}$ emissions from coal-fired power plants installed with SCR installations [40]. The SCR device is a selective catalytic reduction device. Ammonia is injected into the smoke stream, and the gas reacts with NH $_3$ through the catalyst in the presence of oxygen to form N $_2$ and water vapor, which can reduce the emission of nitrogen oxides by 80–90% [52]. NO $_{\rm X}$ emissions from power plants installed with SCR units have higher $\delta^{15}{\rm N}$ values, probably due to the kinetic fractionation that occurs during the selective catalysis process, where the catalytic unit prioritizes $^{14}{\rm NO}_{\rm X}$, enriching $^{15}{\rm NO}_{\rm X}$ resulting in higher $\delta^{15}{\rm N}$ values in the emitted NO $_{\rm X}$ [27,40]. Zong et al. measured the $\delta^{15}{\rm N}$ values of NO $_{\rm X}$ emissions from residential coal combustion in China and found that $\delta^{15}{\rm N}$ -NO $_{\rm X}$ from residential coal combustion was lower than industrial emissions at 17.9 \pm 3.1% [25]. Widory measured a negative $\delta^{15}{\rm N}$ value of -5.3% for NO $_{\rm X}$ emissions from coal combustion for heating purposes in Paris, which is somewhat different from the $\delta^{15}{\rm N}$ value for coal-fired power plants [42]. The distribution of soil NO emissions varies considerably with the region and is dominated by land use type and nitrogen fertilizer use.

Li et al. determined $\delta^{15}N$ values of -48.9% to -19.9% for NO produced by soils under fertilizer application [45]. Later, Felix and Elliott measured values of -30.8% and -26.5% in the same range [46]. Miller et al. found a significant difference in $\delta^{15}N$ -NO $_X$ values between injected ($-32.2 \pm 12.1\%$) and untilled sown manure ($-23.4 \pm 2.1\%$) [47]. Su et al. found that soil in aerobic conditions had $\delta^{15}N$ values in NO emitted under aerobic and anaerobic conditions were different, ranging from -62% to -50% under aerobic conditions, much lower than -45% to -23% under anaerobic conditions, due to the predominance of nitrification and denitrification in soil under aerobic and anaerobic conditions, respectively [48]. The $\delta^{15}N$ values for NO $_X$ emitted from soil sources ranged from -62% to -19.9%, and the low $\delta^{15}N$ values for NO $_X$ emitted from the soil are due to the fact that NO $_X$ emitted from the soil is an intermediate product of microbial nitrification and denitrification reactions, both of which preferentially utilize ^{14}N .

Previous researchers have focused mainly on NO_X emissions from fossil fuel combustion, ignoring the contribution of soil sources to atmospheric NO_X . Subsequent studies will continue to focus on NO_X emissions from soils.

2.2. $\delta^{15}N$ of Other Sources

Ikegami et al. analyzed the composition of aerosol particles in haze weather and found that the haze particles were most likely caused by the growth of particles emitted during biomass combustion through heterogeneous reactions [53]. Furthermore, the analysis of the chemical composition of the particulate matter revealed that the oxidation coefficient of the nitrogen oxide in the atmosphere increased significantly during the combustion phase, which shows that biomass combustion has a significant contribution to NO_X in the atmosphere [54].

Fibiger et al. measured $\delta^{15}N$ values for NO_X emissions from the combustion of forest samples ranging from -7% to 5% [43]. Shi et al. measured $\delta^{15}N$ values for NO_X emissions from biomass combustion in China and compared $\delta^{15}N$ -NO_X from open burning and rural cookstoves with -3.7% to 3.1% and -11.9% to 1.5%, respectively [44]. The measured $\delta^{15}N$ values ranged from 0.1% to 4.1% for nine biomass fuel sources, and this variation was influenced by the biomass fuel source [44]. Zong et al. measured $\delta^{15}N$ -NO_X from biomass combustion ranging from -5.6% to 3.2% (-0.4% $\pm 2.4\%$), which showed a significant linear relationship with $\delta^{15}N$ -biomass [25]. The interval of $\delta^{15}N$ values for NO_X emissions from biomass combustion was -11.9% to 5%.

For lightning sources, it is more difficult to collect actual samples and measure them. $\delta^{15}N$ values of -0.5% to 1.4% for NO_{χ} were collected by Hoering in a laboratory simulation of lightning [49].

In summary, there is a significant overlap in $\delta^{15}N$ values from different sources, and even for the same source, differences in N conversion mechanisms, sampling methods, and regional effects can lead to differences in $\delta^{15}N$ values; e.g., SCR devices during coal combustion, TWC devices during vehicle emissions, etc., can affect the N conversion mechanisms. In addition, inconsistencies in NO_X collection methods in the above literature, such as different collection devices, different absorption solutions, and different collection objects, may lead to some differences in NO_X collection efficiency, which should be avoided in later studies.

3. Bayesian Isotope Mixing Model

3.1. Principle of Bayesian Mixture Model

Mathematical models are frequently used to assess and discuss the origins of NO_X in the collected air particulate matter for the $\delta^{15}N$ data received after sampling and analysis. Phillips et al. created the IsoSoure model in order to assess the contribution of various emission sources using the mass balance concept. The model cannot identify the sources of NO_X because it does not account for the fractionation effect in the NO_X to the nitric acid synthesis process, which limits its applicability to the case when the sources are not more than three [55].

The Bayesian isotope mixing model (SIAR model) was later introduced for the traceability analysis of $\delta^{15}N$ data. As an important branch of stable isotope mass balance models, the Bayesian isotope mixing model can use stable isotope signatures to determine the probability distribution of each source's contribution to the mixture and explicitly account for the uncertainties associated with multiple sources, fractionation, and isotopic signatures, and has been widely used in recent years [56]. The SIAR model sums the total contribution to 100% based on the isotope mass balance law, which can quantitatively resolve the contribution of different sources to the mixture and thus assess the respective contributions of different sources in the mixture, overcoming to some extent the overlap in the $\delta^{15}N$

range of different NO_X sources [57]. The Bayesian isotope mixing model can be expressed as Equations (12) and (13):

$$X_{ij} = \sum_{k=1}^{K} P_k (S_{jk} + C_{jk}) + \varepsilon_{ij}$$
 (12)

$$S_{jk} \sim N(\mu_{jk}, \omega_{jk}^2), C_{jk} \sim N(\lambda_{jk}, \tau_{jk}^2), \epsilon_{jk} \sim N(0, \sigma_j^2)$$
 (13)

Equation (12) is an equation based on the mass balance principle, X_{ij} is the δ value of isotope j in mixture i (I = 1, 2, 3, ..., N; j = 1, 2, 3, ..., J); P_k is the proportion of source k to be calculated, S_{jk} is the δ value of isotope j in source k (k = 1, 2, 3, ..., K); C_{jk} is the fractionation factor (mean λ , standard deviation τ) of isotope j in source k; and ϵ_{ij} is the residual error. Equation (13) indicates that S_{jk} , C_{jk} , and ϵ_{ij} all obey normal distribution.

There are still considerable ambiguities in SİAR models, despite the fact that they can predict emission sources accurately. Based on earlier comments, Fan et al. recommended the following changes to increase the SIAR model's accuracy [16]: In order to reduce uncertainty caused by differing qualities between the input data, the environmental samples used as inputs first need to share the same natural properties. For instance, the sample data need to come from the same season. Second, all sources should be included in the SIAR model; otherwise, the proportions of other sources will be biased. However, developing and employing a conforming local composition of emission sources can also lessen the model's uncertainty.

Additionally, the Bayesian isotope mixing model is being optimized. Zong et al. improved the Bayesian isotope mixing model by introducing isotopic fractionation of the equilibrium/Leighton reaction using the improved model to apportion the annual NO_X sources in North China, and the improved process is shown in Figure 5 [57]. Later, a method was proposed to calculate the isotopic fractionation coefficients by combining oxygen isotopes and the Bayesian isotope mixing model, which can lead to the nitrogen isotopic fractionation coefficients for the conversion of atmospheric $NO_X(g)$ to $HNO_3(g)$, and thus to the resolution of the sources of atmospheric nitrate from different sources [25].

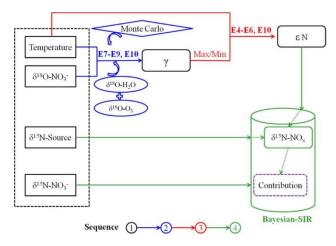


Figure 5. Principle and process of the improved Bayesian model by Zong et al.; the "E" represents equation in the following section, " ε N" refers to N fractionation, and "SIR" is "sampling-importance-resampling". Reprinted with permission from Ref. [57]. Copyright 2017 ACS.

3.2. The Practical Application of Bayesian Mixture Model

The Bayesian isotope mixing model was used to assign sources for several different regions and the results obtained are shown in Table 1.

Table 1. Sources of NO_X in different regions.

Reg	zion	Coal Combustion	Vehicle Emission	Biomass Burning	Biogenic Soil Emission
Beijing	[15,23]	28 ± 12‰ 50‰	29 ± 17‰ 20‰	27 ± 15‰ 26‰	16 ± 7‰ 4‰
Beijing-Tianjin-Shijiazhuang [58]		$17.9 \pm 11.4\%$	$29.4 \pm 19.6\%$	$29.1 \pm 18.9\%$	$23.5 \pm 12.7\%$
Tianjin [59]		14.5‰	47‰ Diesel vehicles 25.6‰ Gasoline vehicles	17.4‰	21.1‰
D. 1 1	1.1 1 [57]	26 52 1 6 66 9	21.4%	27.70 0.000/	12 (0 21(0)
Beihuangchei		$36.53 \pm 6.66\%$	$22.01 \pm 6.92\%$	$27.78 \pm 8.89\%$	$13.68 \pm 3.16\%$
Jiaozuo [38]	Summer Winter	$25\% \pm 9\%$ $31\% \pm 9\%$	$18\% \pm 9\% \\ 18\% \pm 9\%$	$36\% \pm 12\% \ 30\% \pm 12\%$	$22\% \pm 4\% \ 21\% \pm 4\%$
Guangd	ong [39]	$50.1 \pm 13.8\%$	$22.1\pm4.5\%$	$18.4\pm5.1\%$	$9.4\pm4.7\%$
Hangzhou [60]		29.8 ~ 38.4 ‰	33.9 ~ 35.7‰	22.2 ~ 24.7‰	5.3 ~ 11.6‰
Northeast China [61]		34.5‰	19.5‰	34.3‰	11.7‰
Lanzhou [62] (winter-spring periods)		$42.2\pm9.9\%$	$22.2 \pm 12.3\%$	$27.8 \pm 16.2\%$	$7.7 \pm 5.2\%$
Ganzhou [63]	Summer Winter	3.4‰ 4.1‰	59.3‰ 65.1‰	8.7‰ 10.6‰	28.5‰ 20.1‰

The importance of coal combustion sources rises noticeably in the majority of northern Chinese towns during the winter [15,38,61]. This is because coal is frequently used for heating in the winter, and even if denitrification technology is utilized to reduce NO_X emissions during coal combustion, the amount of NO_X in the atmosphere is still increased. Fan et al. showed that the contribution of coal combustion to nitrate aerosols has decreased in recent years, possibly due to the replacement of coal combustion by natural gas as a crop heating fuel [15]. Jiaozuo contributes less to emissions from coal-fired power plants because its industry is less than that of significant cities like Beijing and Tianjin [38]. For Guangdong, there is no need to burn coal for heating, and the significant contribution of coal combustion may be attributed to power plants [39]. The contribution of coal-fired emissions to Ganzhou's energy mix is minimal because clean energy sources like photovoltaic electricity, hydroelectric power, wind power, and biomass power make up a sizeable share of Ganzhou's energy mix [63].

The total number of vehicles in all regions is rapidly increasing due to rapid economic development and rising living standards of the population [58,59], leading to a significant contribution of mobile sources to atmospheric NO_X , especially in Ganzhou [63]. Whereas Tianjin, the largest industrial city in northern China, has more frequent diesel vehicle transport activities, the contribution of diesel vehicle emissions in winter is much lower, probably due to traffic regulation that significantly reduces the number of diesel vehicles during winter days when pollution is more frequent [59]. Additionally, the enhanced contribution of vehicle exhaust to particulate matter NO_3^- under severe pollution in Beijing was discovered by Fan et al. [15]. The contribution of vehicle emissions to NO_X is higher in large cities. Ship emissions are an important source of atmospheric NO_X in coastal areas such as Beihuangcheng Island [57]. In summary, vehicle emissions are relatively more important in urban environments, but coal combustion is more important in non-urban areas for NO_X in $PM_{2.5}$.

The large-scale burning of crop residues occurs in spring and autumn, especially in small cities, generally without the use of pollution control equipment, leading to a sharp increase in NO_X emission values, like in Jiaozuo [38] and northeast China [61]. Agricultural waste, including wood and crop waste, is still utilized for cooking and heating in rural areas of northeast China [61]. In addition, 30% of the power and industrial fuels used in Guangdong come from biomass sources [39]. It is reported that NO_X emissions from biomass burning in China increased more than sixfold from 1990 to 2013 [64].

Soil emissions of NO_X are mainly generated by nitrification and denitrification reactions occurring during the cultivation of crops [46] and are influenced by temperature and humidity [15]. Emissions from soil sources are higher in agricultural land in northeast China [61], as well as in Jiaozhou [38] and Ganzhou [63]. More fertilizer is given to crops during the warm season, which leads to an increased contribution of soil to NO_X [60]. It can be inferred that soil sources are more important for atmospheric NO_X in non-urban areas. Growing urbanization and shrinking agricultural land area in Hangzhou have resulted in a low contribution to atmospheric NO_X from soil sources [60].

At present, our means of combating air pollution is mainly to limit fossil fuel combustion, but it can be seen from Table 1 that non-fossil fuels (biomass burning emissions, biogenic soil emissions) should be equally important for atmospheric NO_X emissions, which is consistent with the study of Song et al. [65].

4. Pathways of Nitrate Production

The oxidation process of NO_X conversion to nitrate is an important reaction mechanism in atmospheric chemistry. Analyzing the formation pathway and relative contribution of nitrate in the atmosphere is of great significance to the study of atmospheric chemistry, such as the assessment of regional air quality and atmospheric oxidation capacity.

4.1. $\delta^{18}O$ and $\delta^{15}N$ for the Atmospheric Nitrate Pathway

Nitrogen and oxygen isotopic fractionation is assumed to be the same as the temperature and the starting $\delta^{18}O$ and $\delta^{15}N$ of NO_X for the various oxidation pathways. For these pathways, Walters and Michalski calculated relatively different values for $\delta^{18}O\text{-}\delta^{15}N$. For each of the many oxidation processes, HNO3 generally has different $\delta^{18}O$ and $\delta^{15}N$ values. In a hybrid model that may be used to explain the observed $\delta^{18}O$ and $\delta^{15}N$ values in atmospheric NO3, the $\delta^{18}O\text{-}\delta^{15}N$ arrays for various HNO3 production pathways can therefore be specified as isotopic end elements [66]. $\delta^{18}O$ is calculated in Equation (14), using the calculation in Equation (10).

$$\delta^{18}O - NO_3^-(\%) = \frac{R_{18O - NO_3^-/^{16}O - NO_3^-}}{R_{VSMOW}} - 1$$
 (14)

We mentioned earlier in the Introduction section that the main pathways in the conversion of atmospheric NO_X to NO_3^- , after going through the cycle of Reactions (1)–(3), are divided into the gas-phase interaction of NO_2 and OH, the non-homogeneous reaction of N_2O_5 hydrolysis NO_2 (Reaction (4)), and OH and the non-homogeneous reaction of N_2O_5 hydrolysis (Reactions (5), (7), (8)). At the same time, NO_3 also reacts with DMS or HC to form nitric acid (Reaction (6)).

The identification of pollution sources by $\delta^{15} N\text{-NO}_3^-$ alone has some limitations, and the high value of $\delta^{18} O\text{-NO}_3^-$ is usually used to reveal the oxidation pathway of NO_3^- generation from NO_X and to resolve the uncertainty of source analysis using $\delta^{15} N$ alone. Combining $\delta^{15} N$ and $\delta^{18} O$ dual isotopes can further clarify the source, formation, and transport transformation processes of NO_3^- in $PM_{2.5}$ by means of backward trajectories and the Bayesian isotope mixing model [67].

In Guha's study, it was shown that the $\delta^{18}O$ range of O_3 is much higher than that of $\cdot OH$, (90–122%) and (–25–0%), respectively, and that five-sixths of the O atoms in the N_2O_5 pathway come from O_3 , whereas two-thirds of the O atoms in the $\cdot OH$ pathway come from O_3 , leading to a higher expected $\delta^{18}O$ of nitrate formed in the N_2O_5 pathway than in the $\cdot OH$ pathway [68].

Li et al. sampled and analyzed the atmosphere of Jiaozuo, China, and found that $\delta^{18}\text{O-HNO}_3^-$ values for winter samples (82.7% to 103.9%) were close to $\delta^{18}\text{O-HNO}_3^-$ values calculated via the N_2O_5 pathway (103% \pm 0.8%), and values for summer samples (67.8% to 85.7%) were close to $\delta^{18}\text{O-HNO}_3^-$ values calculated by the ·OH oxidation pathway (61% \pm 0.8%), indicating that winter nitrate is mainly produced by the N_2O_5

pathway, while summer samples are mainly from the \cdot OH pathway [38]. Hastings et al. also showed that the \cdot OH pathway dominates in summer, while the N_2O_5 pathway dominates in winter [11].

According to Xiao et al., more than 60% of the nitrate production in Nanchang was caused by the hydrolysis of N_2O_5 . Due to long days and high temperatures, ·OH radical oxidation of NO_X predominated in the summer, whereas N_2O_5 hydrolysis oxidation predominated in the winter due to long nights and low temperatures. While lower ·OH radical concentrations with higher O_3 to ·OH ratios result in higher N_2O_5 hydrolysis contributions and higher NO_3^- concentrations generated in winter, higher ·OH radical concentrations with higher ·OH to O_3 ratios result in lower NO_3^- concentrations. The O_3 to NO_X ratio rises with low ·OH, boosting the NO_3 + HC pathway's contribution [17]. Luo et al. found that $\delta^{18}O$ - NO_3^- values were higher in colder months (63.5–103‰) than in warmer months (50.3–85.4‰), also indicating a shift in the nitrate formation pathway from NO_2 +·OH in the warmer months to the N_2O_5 + H_2O and NO_3 + HC pathways in the colder months [69].

Additionally, N_2O_5 hydrolysis and NO_3 radical reactions with hydrocarbons occur in Nanchang throughout the winter. On average, NO_3 + HCs account for 60‰ of the chemical conversion of NO_X to NO_3^- . With a 33‰ average and a potential of 45‰ on days of exceptionally high nitrate aerosol pollution, NO_3 + HCs channels play a significant role in NO_X oxidation [58]. In Walters' study, it was shown that the daily cycle of the variation of $\delta 18O$ is due to the NO_X photochemical cycle driven by the O_3 pathway, resulting in higher daytime $\delta 18O$ values [70].

Additionally, Luo et al. discovered that $PM_{2.5}$ had an impact on the nitrate generation pathway. When $PM_{2.5}$ climbed from ~25 to >100 $\mu g/m^3$ during the winter months, $\delta^{18}O\text{-}NO_3^-$ levels increased from 65.2–79.9‰ to 80.7–96.2‰, although the change in $\delta^{18}O\text{-}NO_3^-$ was only marginal when $PM_{2.5}$ was over 100 $\mu g/m^3$. It demonstrates that when PM2.5 was below 100 $\mu g/m^3$, the nitrate synthesis route switched from the NO_2 +·OH pathway to the NO_3 + HC and N_2O_5 + H_2O pathways, but when $PM_{2.5}$ was over 100 $\mu g/m^3$, N_2O_5 + H_2O and NO_3 + HC predominated [69]. According to Cheng et al., NO_3 + HC pathway and N_2O_5 + H_2O pathway both contributed more when the concentration of NO_3^- was high, indicating the significance of these two pathways for nitrate production in $PM_{2.5}$, particularly in the winter [63].

Li et al. demonstrate the nonlinear relationships between particle nitrate and the emission controls of nitrogen oxides (NO_X) in the Chinese megalopolises using extensive observations and a regional meteorology chemistry model with optimized mechanisms [71]. They discovered that in the Beijing–Tianjin–Hebei (BTH) and Yangtze River Delta (YRD), decreases in NO_X emissions would result in an approximately linear drop in $PM_{2.5}$ over the summer and fall. Whereas NO_X causes a rather complex response in PM composition in winter, for every 10% reduction in NO_X emissions, nitrate increases by 4.1% in BTH and 5.1% in YTD. It is only at a 30–50% reduction in NO_X emissions that a reduction in ammonia oxides leads to a reduction in nitrates.

In the report of Liu et al., using $\delta^{15}N$ as an indicator, the $\delta^{15}N$ value of NO_3 was $6.9 \pm 4.6\%$ higher than that of NO_2 , indicating that the formation of HNO_3 in the atmosphere is dominated by the hydroxyl radical pathway. The $\delta^{15}N$ value of NO_3^- in the atmospheric particulate matter was $4.9 \pm 4.2\%$ higher than that of HNO_3 , indicating that HNO_3 is the main precursor of particulate matter NO_3^- [72]. Significant isotopic fractionation during oxidation uses significant seasonal variation in nitrate $\delta^{15}N$ concentrations (lower in summer and greater in winter), with seasonal variation in the NO_2 oxidation pathway serving as the primary driver [73].

The proportional contribution of the OH oxidation pathway to nitrate was found to be significantly correlated with latitude (p < 0.01) in Zong et al.'s field measurements of $\delta^{15}\text{N-NO}_3^-$ and $\delta^{18}\text{O-NO}_3^-$ in five Chinese cities, with longer sunlight hours and longer atmospheric action of radicals like OH being more significant for NO_X oxidation at low latitudes than at high latitudes. For the first time, the relationship between the NO_X conversion pathway and $\delta^{18}\text{O}$ and dimensionality was discovered. They also discovered

a substantial correlation between latitude and UV intensity, and they demonstrated and confirmed how UV intensity affects the pathway for NO_X oxidation. [37].

Previous investigations have all shown that heterogeneous hydrolysis of N_2O_5 was the primary source of explosive nitrate accumulation and that photochemistry is typically thought to be secondary in secondary nitrate generation due to lower solar radiation in winter and at night. However, a field study by Zhang et al. in North China highlighted the role of the OH oxidation pathway in the synthesis of nitrate during the winter season, with the daytime OH oxidation pathway playing an equal role to the nocturnal channel (46.4‰ vs. 53.6‰) [74]. In a study, Chen et al. also discovered the significance of the OH channel in Beijing during pollution events, with percentages of 74‰ in urban regions and 76‰ in suburban areas [75]. According to Zhang et al.'s analysis of the atmospheric nitrate in Jinan, the accumulation of nitrate during the summer is sensitive to the formation of HNO₃, and during the night, when heterogeneous nitrogen chemistry is most favorable, the N_2O_5 pathway dominates the oxidation of NO_X due to increased O₃ levels and high aerosol water content during the summer [76]. These results are different from those that had previously been obtained and require more investigation

4.2. Δ^{17} O in the Atmosphere

The wide distribution of $\delta^{15}N$ and $\delta^{18}O$ from different sources and a certain degree of overlap increase the difficulty of the source resolution. Since the reactions leading to ^{17}O value excess occur only in photochemical reactions, they can further quantify the proportional contribution of different oxidation pathways in nitrate formation and become a powerful tool for the in-depth study of atmospheric chemistry, which has been applied to the study of oxidation pathways of nitrate in aerosols [77–79].

In the process of oxygen isotope mass fractionation, a linear relationship is maintained between $\delta^{17}O$ and $\delta^{18}O$: $\delta^{17}O = 0.52 \times \delta^{18}O$. Due to the symmetric structure of O_3 , ^{18}O and ^{17}O are uniformly distributed during the formation of O_3 , independent of their atomic masses, and the above linear relationship does not exist, so this process is called non-mass isotope fractionation (MIF), and the formation of O_3 is the only non-mass isotopic fractionation process that has been discovered so far [80]. In the NO_X photochemical cycle and the HNO_3 production process, the value of $\Delta^{17}O$ is equal to or approximately equal to 0 for all the reactants that provide oxygen atoms for the reaction products (HO_2 , RO_2 , OH, H_2O , etc.), except for O_3 . The degree of non-mass isotopic fractionation is measured by $\Delta^{17}O$ in Equation (15) [81], $\delta^{17}O$ using the calculation of Equation (10):

$$\Delta^{17}O = \delta^{17}O - 0.52 \times \delta^{18}O \tag{15}$$

Abnormal Δ^{17} O values due to MIF is also present in reaction products when non-mass isotope fractionation occurs or during a reaction process in which Δ^{17} O \neq 0 provides oxygen atoms to the reaction products. Therefore, Δ^{17} O can be used to study the pathway of atmospheric nitrate production [82,83].

Changes in external factors such as seasonal variations, human activity effects, geographical variations, different PM_{2.5} concentrations, and relative humidity all have an impact on the value of Δ^{17} O.

The value of $\Delta^{17}O$ can alter due to fluctuations in external factors such as relative humidity, seasonal variations, anthropogenic influences, regional variations, differing PM_{2.5} concentrations, and seasonal changes. Numerous studies have discovered that the seasonal variation of nitrate, which is low in summer and high in winter, is caused by the relatively low nitrate $\Delta^{17}O\text{-NO}_3^-$ formed via the OH pathway in summer and the high nitrate formed via the N₂O₅ and NO₃ pathways in winter, which is related to the seasonal variation characteristics of the concentrations of oxidants O₃ and OH [80,84]. Additionally, there is a distinct diurnal variation in $\Delta^{17}O$, which is associated with the production pathway and is lower during the day and greater at night [82,85].

Human activities also have an influence on $\Delta^{17}O$ values. Wang et al. measured isotopes in PM_{2.5} in Beijing in 2014 and combined them with stable isotope analysis in the R model and found that air pollution (PM_{2.5}, NO₂, and NO₃⁻) reduced the contribution of the OH pathway to nitrate, while atmospheric ozone pollution increased the importance of the OH pathway. They concluded that the influence of $\Delta^{17}O$ values is mainly due to the availability of OH [84]. The study by Li et al. found higher oxygen isotopes at rural sites than at urban sites, suggesting that human activities reduce the contribution of the O₃ pathway to atmospheric nitrate [79].

At the same time, different geographical environments also lead to differences in nitrate formation pathways. Li et al. found in Guiyang, China that the strong ultraviolet radiation in the plateau region may make the OH pathway more important [73]. Zhao et al. sampled and analyzed atmospheric aerosols from different regions in northeast China and found that tropospheric O_3 concentrations in one region were significantly smaller than in other regions, leading to more difficult N_2O_5 production. This may lead to a high contribution of ·OH to the formation of nitrate in this region [86].

In addition, several studies have shown that high $PM_{2.5}$ concentrations and relative humidity during haze are more favorable for nitrate formation via the N_2O_5 non-homogeneous pathway, which may be due to the wetter atmosphere during the haze, which is more favorable for non-homogeneous reactions [86,87]. In the study of Fan et al., the contribution of the N_2O_5 pathway to nitrate during haze was elevated to 64‰, which was significantly higher than during clean atmosphere (39‰) [15].

Because the formation process of atmospheric nitrate is complex and the formation pathways are different under different conditions, it is difficult to analyze the oxidation results only based on the observation results. In addition to simulating $\Delta^{17}O$ in various places to better understand the peculiarities of atmospheric oxidation in various regions and seasons, atmospheric chemistry models are coupled with previous studies to achieve a quantitative analysis of atmospheric nitrate oxidation routes.

Box simulations are simulations of atmospheric photochemical reactions in an enclosed space. All nitrates in the simulation are oxidized by NO_X , which can be used to simulate the $\Delta^{17}O$ of atmospheric nitrates and thus calculate the number of nitrates produced by each reaction pathway in the atmosphere. However, the box simulation does not take into account atmospheric transport, and the calculation results have some bias. In the first simulation of atmospheric nitrate $\Delta^{17}O$ in the contaminated marine boundary layer in California, USA, using the box model, the simulation results can be in good agreement with the test results of the actual samples by Michalski et al. However, the box simulation ignored the regional transport in the atmosphere, resulting in a large difference (0~5%) between the simulated and tested results in spring [85].

Subsequently, Michalski et al. developed an isotope mass balance model ISO-RACM that uses regional atmospheric chemistry mechanisms to predict $\Delta^{17}O$ values of atmospheric nitrate, which can be used to explain $\Delta^{17}O$ in ice cores, aerosols, soils, and precipitation, breaking the limits of the atmospheric medium [88]. Morin et al. further developed a daily integrated isotopic signature model that takes into account the influence of transport processes on the diurnal variation of $\Delta^{17}O$ and helps to quantify the effect of different environments [89]. The application of this model to secondary species with a longer life than one day allows the seasonal variation of $\Delta^{17}O$ to be studied.

In 2009, Alexander et al. presented the first global three-dimensional chemical transport model, GEOS-Chem, incorporating horizontal and vertical transport as well as spatial variation in surface fluxes of some important major pollutants; however, Δ^{17} O values were overestimated for mid- and high-latitudes in winter and underestimated for polar regions in spring and summer [13].

Later, in 2020, Alexander et al. updated the GEOS-Chem global chemical transport model and re-evaluated the model's nitrate formation pathway. The results obtained from the simulations are generally consistent with previous observations, with annual mean $\Delta^{17}{\rm O}$ variability ranging from 7% to 41% and higher $\Delta^{17}{\rm O}$ values in the cold season. It

was also found that $\Delta^{17}\text{O-NO}_3^-$ is lower near the equator and higher in polar regions on a global scale. However, the model underestimates the $\Delta^{17}\text{O}$ in the polar region in spring and summer and in the middle and high dimensional regions to some extent, $0\% \sim 5\%$ and $1\% \sim 7\%$, respectively. The underestimation of $\Delta^{17}\text{O}$ for polar regions is mainly due to the GEOS-Chem model overestimating the contribution of the N_2O_5 hydrolysis pathway by ignoring the importance of the hydrolysis reactions of halogenated elements (XNO₃, X for halogenated elements such as Cl, Br, I) to generate nitrate [15].

In summary, it is concluded that there are differences in the observed values of $\Delta^{17}\text{O-O}_3$ in different regions and differences between observed and simulated values, which may be due to the often large scales of model studies and possible discrepancies with observations in the real atmosphere at local sites. Therefore, observations of $\Delta^{17}\text{O-O}_3$ values on a global scale are important for model validation and for understanding the real atmospheric nitrate formation mechanisms. In future studies, modelling data can be combined with actual observations. The modelling results provide research directions for the actual observations, while the results obtained from the actual observations can provide favorable evidence for the modelling predictions.

5. Conclusions

Nitrate is now a significant component of haze particles as a result of changes in the composition of atmospheric particulate matter during the past several years. One of the hotspots of research in this direction is the process of nitrate synthesis and the origin of its precursor NO_X . In order to analyze NO_X sources in atmospheric particulate matter, stable isotope techniques have made significant strides in recent years.

This paper summarizes the benefits and drawbacks of emission inventories, satellite observations, and stable isotope methods. It also highlights the main developments of stable isotope techniques in the study of NO_X sources and nitrate formation pathways. First, a summary of the stable isotope techniques used for NO_X traceability is presented. The range of $\delta^{15}N$ - NO_X values for various NO_X sources is then noted, while the Bayesian mixture model's calculation approach and its use in the investigation of NO_X sources are discussed. After that, a discussion of how to utilize $\delta^{15}N$ and $\delta^{18}O$ in conjunction to figure out the quantities and paths of nitrate production follows. Finally, the study of routes using $\Delta^{17}O$ is provided in order to learn how different conditions affect the pathways of nitrate generation and to simulate $\Delta^{17}O$ in various places in order to better understand the peculiarities of atmospheric oxidation in various regions and seasons.

The analogous analysis of the literature in this paper presents the continuous progress and application of traceability analysis methods in NO_X in recent decades. The work of current researchers has demonstrated that stable isotope techniques are a useful method for the traceability analysis of NO_X in the atmosphere, and the research findings are helpful for the development of effective emission reduction plans and the implementation of targeted measures, which are crucial for the accurate understanding of atmospheric oxidation activity and atmospheric pollutants.

Although the findings of the current research effort are remarkable, there are still some issues with the stable isotope analysis of NO_X , and we think that the following areas can be further improved.

The lack of source $\delta^{15}N$ data for NO_X tracing using nitrogen isotopes and the large overlap in the data of $\delta^{15}N$ values of NO_X emitted from different sources lead to large uncertainty. More actual measurements of NO_X sources are needed to enrich the $\delta^{15}N$ value data and establish a perfect $\delta^{15}N$ value system to quantify NO_X sources.

The atmospheric NO_X sources and nitrate formation mechanisms in different regions also have great uncertainties. The results of Chen et al. showed that the drivers of nitrate pollution and mitigation strategies for particulate nitrate differed between Beijing and the United States [75]. Therefore, it is necessary to determine a normative way of collecting NO_X to determine precisely the $\delta^{15}N$ values of emission sources in each location and to obtain a more reliable indication of NO_3^- sources. In addition, the contribution of non-

major oxidation pathways for NO_X in specific regions (coastal areas, highland areas, etc.) remains to be evaluated.

For the study of the atmospheric nitrate production pathway, $\Delta^{17}O$ is only related to the nitrate production pathway and should be combined with $\delta^{15}N$, $\delta^{18}O$ isotope analysis to exclude the possible fractionation process during nitrate production to better distinguish and reveal the source and production process of nitrate.

Table 2 summarizes and explains the acronyms used in this paper.

Table 2. List of abbreviations.

Abbreviations	Specific Contents
DMS	Dimethyl sulfide
HC	Hydrocarbons
VOCs	Volatile organic compounds
TWC	Three-way catalytic converter
LPG vehicles	Liquefied petroleum gas vehicles
SCR	Selective catalytic reduction
SIAR model	Bayesian isotope mixing model
VSMOW	the Vienna Standard Mean Ocean Water
MIF	Non-mass isotope fractionation
BTH	Beijing-Tianjin-Hebei
YRD	Yangtze River Delta
	An isotope mass balance model that utilizes the Regional
ISO-RACM	Atmospheric Chemistry Mechanism to predict $\Delta 170$ values in atmospheric nitrate
GEOS-Chem model	A global 3-D model of atmospheric composition

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Article

To Promote the Catalytic Ozonation of Typical VOCs by Modifying NiO with Cetyltrimethylammonium Bromide

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Abstract: A series of mesoporous NiO catalysts with high specific surface area were prepared by a simple hydrothermal method and modified by cetyltrimethylammonium bromide (CTAB) as the crystal structure directing regent. The characterization with SEM, XRD, BET, and H_2 -TPR results demonstrated that the introduction of CTAB effectively improved the dispersion, specific surface area, and pore volume and redox ability of NiO, and thus exposed more active sites. Meanwhile, the NiO catalyst with a CTAB/NiSO₄· $6H_2O$ molar ratio of 2/3 exhibited the better catalytic ozonation performance of toluene, formaldehyde, methanol, and ethyl acetate than NiO. The in-situ DRIFTS elucidated the reaction path of catalytic ozonation of toluene and indicated that the introduction of CTAB facilitated the complete oxidation of by-products into CO₂ and H_2O .

Keywords: catalytic ozonation; typical VOCs; NiO catalyst; CTAB modification

1. Introduction

Volatile organic compounds (VOCs) are a class of organic compounds with boiling points between 50–260 °C at standard atmospheric pressure, and widely originated from fossil fuel combustion, chemical industry, and various waste emissions [1–6]. These VOCs can participate in photochemical reactions, causing environmental problems and serious health problems, and even cancer [7,8]. To control air pollution more effectively, China has issued a series of more stringent environmental policies to reduce VOCs emissions [9]. Consequently, there is an urgent need to develop the technologies that can effectively control VOCs emissions [10,11].

Compared to traditional VOCs control technologies, catalytic ozonation is considered to be one of the most promising technologies for VOCs removal with the decrease in O₃ production cost because of its mild reaction condition [8,10,12]. In addition, it has a wide adaptability to the types and concentrations of VOCs [13]. However, there exist wide differences in the properties and concentrations of VOCs in actual industrial exhaust gases, which is posing a challenge to the applicability and universality of catalytic ozonation catalysts [14,15].

The catalytic ozonation of VOCs over the transition metal oxides, such as Co, Ce, Ni, Cu, Zn, Mg, and Mn, has widely been investigated at low or room temperature [8, 16,17]. The catalytic activity varies greatly for different transition metal oxides. Among them, nickel oxide (NiO_x) is thought to be a valuable catalyst of catalytic ozonation of VOCs because of its valence diversity, controllable crystal morphology, easy formation of oxygen vacancies, and high specific surface area. Additionally, ozone can easily adsorb on the surface of NiO_x and thus generate hydroxyl radicals (OH) and superoxide ions (O₂ $^-$) through radical chains [18]. Moreover, it has been reported that NiO_x with over stoichiometric oxygen can efficiently degrade various compounds [19,20], and exhibit good catalytic activity for many difficult-to-degrade VOCs at low temperature [13,20,21].

On the other hand, suitable surfactants can passivate the nanoparticle surface and reduce the agglomeration, which is helpful to improve the catalytic activity of the catalysts [22]. Cetyltrimethylammonium bromide (CTAB), acting as a capping agent and a structure-directing agent, can effectively promote anisotropic growth of crystals to obtain nanocrystals of different sizes and shapes [23]. Using the CTAB co-precipitation method, Navneet Kaur et al. [23] controlled the specific surface area of NiO nanoparticles, which resulted in significant improvement in their specific surface area and catalytic activity of reactive blue 81 and Coomassie brilliant blue R-250 dyes. In a related study, Tong et al. [24] synthesized LiNi $_{0.8}$ Co $_{0.1}$ Mn $_{0.1}$ O $_{2}$ material with CTAB assistance, which exhibited enhanced crystallinity and cycle stability due to reduced agglomeration.

In this work, a series of mesoporous NiO catalysts were obtained by adding different amounts of CTAB as the directing agent and were used for the catalytic ozonation of VOCs. Various characterizations and performance evaluations suggested that the introduction of CTAB could modify the morphology and particle size of NiO, and thus increase its specific surface area, and enhance catalytic activity. Moreover, we further explored the reaction pathway of the catalytic ozonation of toluene and investigated the catalytic degradation effect of the modified NiO catalysts on other typical VOCs, including formaldehyde (aldehydes), methanol (alcohols), and ethyl acetate (esters).

2. Material and Methods

2.1. Materials

Nickel sulfate hexahydrate, urea, cetyltrimethylammonium bromide (CTAB), toluene, formaldehyde, methanol, and ethyl acetate were purchased from Shanghai Aladdin Biochemical Technology Co., Ltd. (Shanghai, China). Among them, toluene, methanol, formaldehyde, and ethyl acetate were all chromatographically pure.

2.2. Preparation of Catalyst

A series of NiO catalysts were prepared using the hydrothermal method and modified by changing the amount of cetyltrimethylammonium bromide (CTAB) as the crystal structure directing regent. An amount of 13.15 g NiSO₄·6H₂O and 0 g, 6 g, 12 g, and 18 g CTAB (with CTAB/NiSO₄·6H₂O molar ratios of 0, 1/3, 2/3, and 1), respectively, as well as 6.006 g CH₄N₂O, being used to maintain the alkaline condition, were dissolved in 300 mL of deionized water and magnetically stirred at 700 rpm for 30 min until a uniform green solution was obtained. The mixture solution was transferred to a 500 mL polytetrafluoroethylene reactor, sealed, and placed in a vacuum oven for hydrothermal reaction at 180 °C for 12 h. After the reactor was naturally cooled to room temperature, the suspension was filtered using a vacuum pump and washed with deionized water until the filtrate pH was neutral. The obtained solid was then dried at 110 °C overnight and calcined in air at 400 °C for 6 h to obtain CTAB/NiO-Z (Z = 0, 1/3, 2/3, and 1, corresponding to CTAB/NiSO₄·6H₂O molar ratios of 0, 1/3, 2/3, and 1) catalysts, respectively. Finally, the above catalyst powders were pressed into tablets under 20 \pm 5 MPa, then ground, and sieved to obtain 40–60 mesh particles for catalytic performance evaluation.

2.3. Characterization

The morphology of the catalysts was observed utilizing a ZEISS scanning electron microscope (SEM). An X-ray powder diffractometer (XRD, Bruker D8 type, Bruker Corporation, Billerica, MA, USA) was used to analyze the crystal structure of the catalyst in a scanning range of 10° – 90° with a scanning speed of 2° /min and a step size of 0.02° . The obtained catalyst lattice parameters were refined using the Jade-6 software. The specific surface area and pore size distribution of the catalysts were determined at Brunel Emmett Taylor (BET, ASAP2020, Micromeritics Instrument Corp., Norcross, GA, USA) by a gas absorption technique. N_2 adsorption and desorption experiments were carried out at 77 K for specific surface area measurements. In order to remove surface adsorbed impurities, the catalyst underwent a pre-treatment process under vacuum conditions at

 $250\,^{\circ}\mathrm{C}$ for a duration of 3 h. Additionally, pore size distribution and pore volume of the catalyst were calculated by the BJH analysis method. To investigate the reduction performance of the catalyst, H_2 programmed temperature rise reduction (H_2 -TPR) experiments were conducted on an AutoChem 2920 analyzer (Micromeritics Instrument Corporation, USA). The reaction mechanism of catalytic ozonation of toluene was determined by analyzing the oxidation products using an In Situ DRIFTS technique on a Thermo Fisher Scientific (Waltham, MA, USA) Nicolet 6700 FTIR instrument. The scanning range was $400-4000\,\mathrm{cm}^{-1}$ with an instrumental resolution of $4\,\mathrm{cm}^{-1}$.

2.4. Performance Evaluation of Catalytic Ozonation

All catalytic ozonation experiments were performed in a fixed quartz tube reactor with an inner diameter of 5.8 mm at standard atmospheric pressure and 30 °C. The simulated reaction gas is composed of O_3 , VOCs (toluene, formaldehyde, methanol, and ethyl acetate), and water vapor, with compressed air as the balance gas. The total flow rate of the simulated reaction gas was controlled at 1 L/min by the mass flow controller, where O_3 was generated by synthesis gas (5% O_2 /balance gas N_2) through the ozone generator, and the concentration was maintained at 210 ppm. The gaseous VOCs were produced by bubbling N_2 through the liquid VOCs placed in a water bath of 1 \pm 0.2 °C. The target concentration of VOCs is controlled by adjusting the N_2 flow rate, and the concentrations of toluene, formaldehyde, methanol, and ethyl acetate were 30, 100, 100, and 20 ppm, respectively. Similarly, water vapor is obtained by passing N_2 into a bubble column filled with water, and the relative humidity of the reaction gas is stabilized at 50 \pm 5%.

The 0.4 g screened catalyst (40–60 mesh) was first pretreated for 30 min at 150 $^{\circ}$ C in N₂ atmosphere to remove the adsorbed water and the impurities on the surface. Then, the reaction gas was passed over the catalyst (GHSV, about 150,000 h⁻¹, unless specified) to perform the catalytic ozonation of the VOCs.

The concentration of each component in the tail gas was measured at the outlet of the reactor, and the O_3 concentration was determined by an ozone detector (2B Technologies, Boulder, CO, USA). Additionally, VOCs and CO_x were analyzed on-line by a gas chromatograph (GC-2014, Shimadzu, Japan) equipped with a hydrogen flame ionization detector (FID) and a DB-WAX capillary column (30 m \times 320 μ m \times 0.25 μ m). VOCs conversion rate, ozone decomposition rate, CO_x selectivity, and mineralization rate were calculated by Equations (1)–(4), respectively:

$$VOC_{s} conversion (\%) = \frac{VOC_{s(in)} - VOC_{s(out)}}{VOC_{s(in)}} \times 100\%$$
 (1)

$$O_3$$
 decomposition (%) = $\frac{O_{3(in)} - O_{3(out)}}{O_{3(in)}} \times 100\%$ (2)

$$CO_{x} \text{ selectivity } (\%) = \frac{CO_{(out)} + CO_{2(out)}}{(VOC_{s(in)} - VOC_{s(out)}) \times n} \times 100\%$$
 (3)

$$VOC_s$$
 mineralization rate (%) = $\frac{CO_{2(out)}}{VOC_{s(in)} \times n} \times 100\%$ (4)

where $X_{(in)}$ and $X_{(out)}$ are inlet and outlet VOCs, O_3 , CO, or CO_2 concentrations, and n is the number of carbon atoms in VOCs, respectively.

3. Results and Discussion

3.1. Structure and Morphology

The XRD patterns of NiO catalysts before and after CTAB modification were depicted in Figure 1. As shown in Figure 1a, the four NiO catalysts all had the characteristic diffraction peaks of monoclinic nickel oxide (JCPDS 04-007-9781), which are located at 37.3, 43.3, 62.9, 75.4, and 79.4°, corresponding to (110), (200), (111), (021), and (220) crystal

planes. Additionally, there were no diffraction peaks of other crystal phases, indicating that the NiO catalysts before and after modification were all standard monoclinic nickel oxide. In addition, it can be found from the partial expanded figure (Figure 1b) that with the increase in CTAB concentration, the characteristic diffraction peaks of NiO catalyst gradually weaken, broaden, and shift to lower angles. This may be attributed to the impact of CTAB as a surfactant on the crystal growth process of NiO. CTAB with the positive charge can be attracted to the NiO surface with the negative charge to form a bilayer. At the same time, the hydroxyl groups of the CTAB can form hydrogen bonds with the oxygen atoms on the surface of the NiO, further enhancing the binding between them [25]. When the doping concentration of the CTAB gradually increases, the CTAB molecules continuously adsorb on the crystal face of the NiO to form an organic phase, which inhibits the growth of the NiO crystal, and resulted in the decrease of the grain size and crystallinity of the NiO and a slight lattice distortion [26,27].

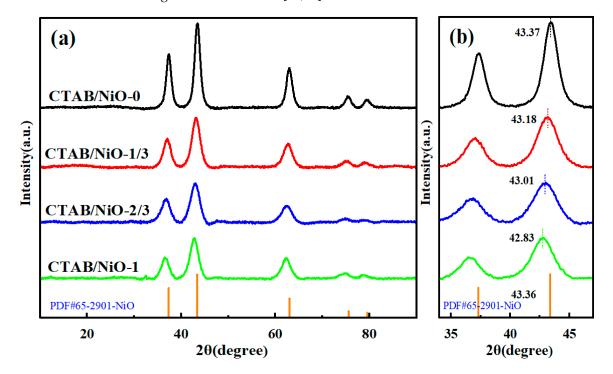


Figure 1. (a) XRD patterns of NiO catalysts modified with different amounts of CTAB, (b) partially expanded XRD patterns.

Figure 2 showed the scanning electron microscopy (SEM) images of the NiO catalysts after and before CTAB modification. As seen from Figure 2a, the NiO before modification displayed regular spheres with diameters of about 3 μ m. The spheres consisted of numerous connected nanorods with a thickness of approximately 10–20 nm and a length of roughly 100–200 nm, and there existed few pores between the nanorods (Figure 2b). In contrast, the CTAB/NiO after CTAB modification exhibited a non-uniform spheroid-like structure being about 1 μ m, with spheres stacking on each other (Figure 2c,e,g). Figure 2d,f,h described that the CTAB/NiO spheres were composed of nanorods with pointed ends, and the thickness of these nanorods was about 5–10 nm and the length was about 50–100 nm. Compared with the unmodified NiO, these nanorods gradually decrease in size, becoming more slender and dispersed as the CTAB doping amount increases. However, when CTAB was doped excessively (Figure 2g,h), the nanorods began to aggregate and the dispersion degree decreased.

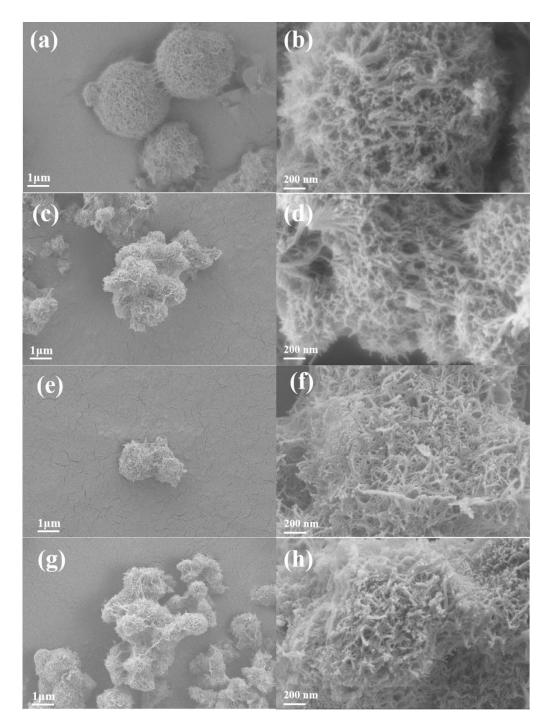


Figure 2. SEM image of NiO catalysts modified with different amounts of CTAB, (**a**,**b**) CTAB/NiO-0, (**c**,**d**) CTAB/NiO-1/3, (**e**,**f**) CTAB/NiO-2/3, and (**g**,**h**) CTAB/NiO-1.

3.2. Surface Area and Pore Structure

The N_2 adsorption isotherm and pore size distribution of the NiO catalyst are shown in Figure 3. It was found that the isotherms of the four catalysts were consistent with the type IV adsorption isotherm of the H_2 hysteresis loop in the IUPAC classification standard, suggesting that the synthesized NiO possessed abundant mesoporous structures. BET surface area and pore parameters calculated by the BJH method were listed in Table 1. The specific surface areas of CTAB/NiO-0, CTAB/NiO-1/3, CTAB/NiO-2/3, and CTAB/NiO-1 are 141.16, 163.18, 202.33, and 172.18 m²/g, respectively. The CTAB modification enhanced the specific surface area and pore volume of the NiO catalysts. It is worth noting that the specific surface area and pore volume of CTAB/NiO-2/3 increased by 43% and 73%,

respectively (Table 1). Clearly, these findings evidenced that the CTAB doping can boost the dispersion and porosity of the CTAB/NiO-0 catalysts, resulting in an increase in their specific surface area and pore volume. It brought in more favorable active sites for the adsorption of VOCs on the catalyst surface and improved their catalytic activity for the catalytic ozonation of VOCs. However, the excessive addition of CTAB may lead to the aggregation of NiO nanorods to form a dense and inefficient structure, which reduced the specific surface area and porosity of the NiO catalyst, thereby inhibiting its catalytic performance. The results are consistent with the SEM.

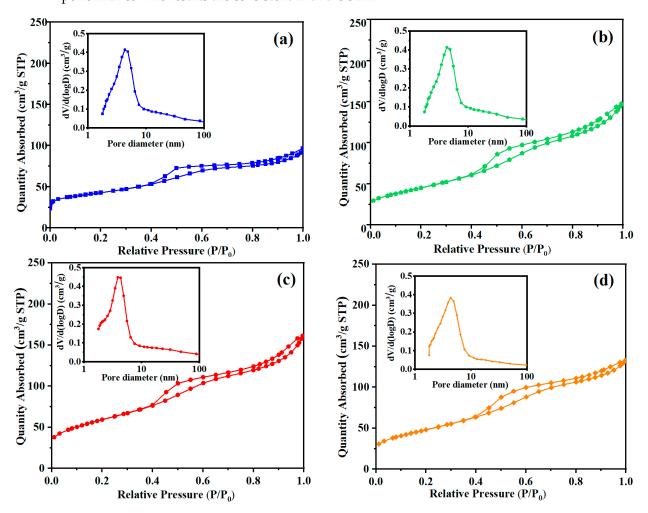


Figure 3. N₂ adsorption/desorption isotherms and pore-size distributions (inset) of (a) CTAB/NiO-0, (b) CTAB/NiO-1/3, (c) CTAB/NiO-2/3, and (d) CTAB/NiO-1.

Table 1. Specific surface area, average pore size, and pore volume of different catalysts.

Catalyst	S_{BET} (m ² /g)	Pore Size (nm)	Pore Volume (cm ³ /g)
CTAB/NiO-0	141.16	5.14	0.1542
CTAB/NiO-1/3	163.18	4.85	0.2317
CTAB/NiO-2/3	202.33	4.22	0.2606
CTAB/NiO-1	172.18	4.21	0.2494

3.3. Redox Properties

 H_2 -TPR can be employed to investigate redox properties of different NiO catalysts. As shown in Figure 4, there was a prominent overlapping peak in the range of 100–400 °C of NiO. According to the main reduction reaction of NiO in the H_2 -TPR process, this overlapping peak can be divided into two reduction peaks, corresponding to the two chemical reactions

of $Ni^{3+} \rightarrow Ni^{2+}$ and $Ni^{2+} \rightarrow Ni$, respectively. Furthermore, it can be clearly seen that the peak temperatures of the two sharp reduction peaks of Ni^{3+} and Ni^{2+} of each NiO were in the descending order of CTAB/NiO-0 > CTAB/NiO-1/3 > CTAB/NiO-1 > CTAB/NiO-2/3. As we all know, the temperature of reduction peaks usually reflects reducibility of catalysts. The reduction temperature of CTAB/NiO-2/3 was the lowest, indicating its outstanding redox ability. H_2 -TPR results demonstrated that CTAB modification did indeed bring about a positive impact on the reduction performance of the NiO catalyst.

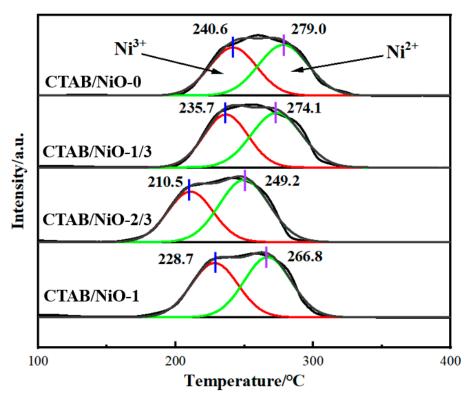


Figure 4. H₂-TPR of different catalysts.

3.4. Catalytic Performance

In this section, the catalytic activity of different concentrations of CTAB-modified NiO catalysts in the catalytic ozonation of toluene was investigated. Before testing the catalytic activity of different catalysts, adsorption experiments were conducted, and the catalyst was saturated with toluene. As shown in Figure 5, the catalytic activity of the unmodified NiO is lower than that of the modified NiO catalysts. As the reaction time increases (4 h), the toluene conversion rate and the ozone decomposition rate drop rapidly from the initial 83% and 100% to 60% and 67%, respectively. The CO_x selectivity and mineralization rate of CTAB/NiO-0 were basically maintained between 50-58% and 35-45%. The activity and stability of the CTAB/NiO-2/3 catalyst were the most excellent, and its initial toluene conversion rate reached 96%. After the reaction for 4 h, the conversion rate dropped by only 14%, while the ozone decomposition rate still remained above 95%. At the same time, during the reaction process, the CO_x selectivity and mineralization rate of CTAB/NiO-2/3 remained in the range of 70–80% and 60–70%, respectively. Compared with CTAB/NiO-0, the toluene conversion rate, ozone decomposition rate, CO_x selectivity, and mineralization rate of CTAB/NiO-2/3 were all increased by more than 20%, while that of CTAB/NiO-1/3 and CTAB/NiO-1 only improved about 10%. Combined with the BET results, it can be deduced that adding an appropriate amount of CTAB can significantly increase the specific surface area and pore volume of NiO, by which the catalytic activity could be promoted.

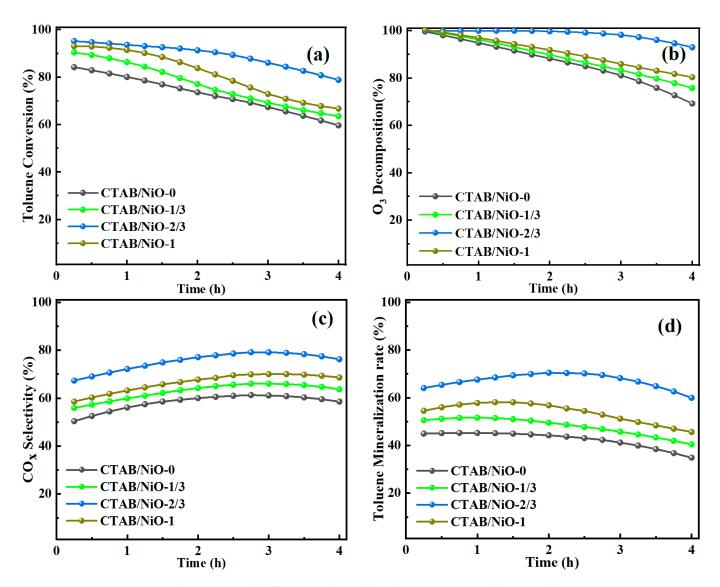


Figure 5. Catalytic activity of different catalysts. (a) Toluene conversion. (b) Ozone decomposition. (c) CO_X selectivity. (d) Toluene mineralization rate $(O_3 = 210 \pm 10 \text{ ppm}, T = 30 \pm 1 \text{ °C}, C_7H_8 = 30 \pm 1 \text{ ppm}, RH = 50 \pm 5\%, GHSV = 150,000 \text{ h}^{-1}).$

3.5. Reaction Path

The reaction intermediate products of NiO catalysts before and after CTAB modification were determined by in situ DRIFTS (Figure 6 and Table 2), and the corresponding reaction path was deduced. The peaks at 819 and 976 cm⁻¹ in the low frequency area of the in-situ DRIFTS spectra correspond to the stretching and torsional vibration peaks of C-H, respectively [28]. The peak observed around 1050 cm⁻¹ was attributed to the C-O stretching vibration peak of alcohols, indicating the formation of benzyl alcohol during the catalytic ozonation of toluene [29]. The signal value of the benzaldehyde species can be observed at 1176 cm⁻¹ [30], together with weak absorption peaks of maleic anhydride (1315 cm⁻¹) [28] and carboxylate (1382 cm⁻¹) [31]. The band detected at 1454 cm⁻¹ is assigned to the -CH=CH- bending vibration of the benzene ring [32,33]. Generally, the bands at around 3400–3800 cm⁻¹ belong to the vibration of Ni-OH and water molecules coordinated to the surface metal cations [32].

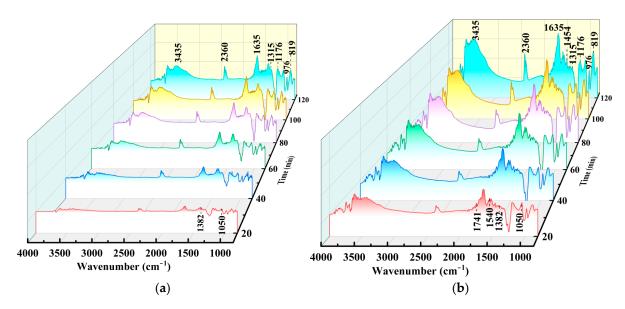


Figure 6. In situ DRIFTS spectra of catalytic ozonation of toluene over (a) CTAB/NiO-0, (b) CTAB/NiO-2/3.

Table 2. The attribution of IR bands in the catalytic ozonation of toluene.

Position (cm ⁻¹)	Assignment	Characteristic of
3600~3000	O-H stretching vibration	metal-OH
1741	C=O symmetrical stretching vibration	quinone
1450~1650	C=C stretching vibrations	aromatic ring
1540	C=O stretching vibrations	benzoate
1382	COO- symmetrical stretching oscillation	carboxylic acid
1315	C-C-C (O) in-plane bending vibration	maleic anhydride
1176	C-O symmetric stretching vibration	benzaldehyde
1050	C-O symmetric stretching vibration	alcohols
976	C-H torsional vibration	olefin
891	C-H stretching vibration	alkyne

In Figure 6a,b, the obvious band at 1635 cm^{-1} is denoted as stretching vibration peaks of the aromatic ring skeleton [28,34]; however, the peak intensity of CTAB/NiO-2/3 was higher than that of NiO, indicating that there were more aromatic compounds generated on the surface of CTAB/NiO-2/3. Interestingly, it can be seen in the spectrum of CTAB/NiO-2/3 that new absorption peaks around 1540 cm⁻¹ and 1741 cm⁻¹ were observed (Figure 6b). The more obvious absorption peak located at 1540 cm⁻¹ is characteristic of the C=O antisymmetric vibration peak in benzoate species [35], which is the key intermediate involved in the oxidation of toluene. Besides, in Figure 6b, the C=O weak stretching vibration peak (1741 cm⁻¹) of quinone appeared; quinone is a kind of higher oxidation product produced by further oxidation of phenol [31,36]. Additionally, the bands at about 2360 cm⁻¹ have been reported to be attributed to the stretching vibrations of C-O bonds from CO₂ [32,37]. It can be clearly seen that the CO₂ signal of CTAB/NiO-2/3 after modification was stronger than that of NiO, explaining that CTAB/NiO-2/3 can oxidize more intermediate by-products to CO₂. In short, according to in-situ DRIFTS spectra, we found that the intermediate products of CTAB/NiO-2/3 were highly oxidized under the same conditions; it is clear that the introduction of CTAB is beneficial to the catalytic oxidation performance of NiO and the deep oxidation of toluene. Therefore, we can preliminarily propose that the oxidation of toluene may follow the path: toluene→benzyl alcohol→benzaldehyde→benzoic acid→benzene→phenol→quinone, followed by ring opening to generate maleic anhydride and other small molecular species, and finally mineralization to CO_2 and H_2O .

3.6. Catalytic Ozonation of Other Typical VOCs

At present, different industrial waste gases discharge various VOCs. Besides monoaromatic hydrocarbons, being the most worrying and most emitted, there are alcohols, aldehydes, and esters, and so on [38]. More importantly, different sorts of VOCs exhibit significant differences in terms of molecular dynamic diameter, hydrophilicity, and molecular polarity, which brings considerable challenges to VOCs removal. In this section, we further investigated the degradation effects of CTAB/NiO catalysts on formaldehyde, methanol, and ethyl acetate, respectively (Figure 7a). Before testing the catalytic activity of different catalysts, the adsorption experiments were conducted, and the catalyst was saturated with VOCs. Figure 7b illustrated that NiO can completely remove ozone under the investigated reaction conditions whether the NiO was modified or not. However, the catalysts exhibited different catalytic activities for the catalytic oxidation of typical VOCs.

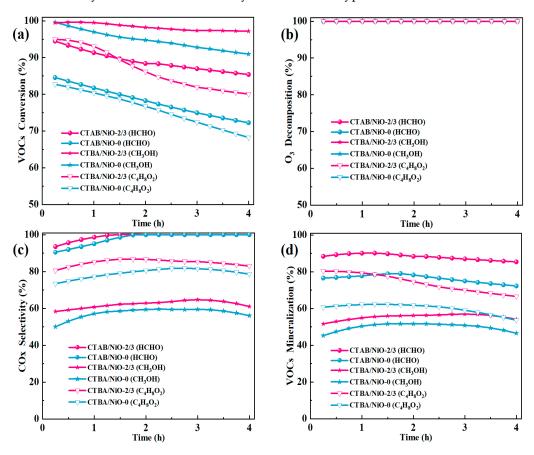


Figure 7. Catalytic activity of typical VOCs of different catalysts. (a) VOCs conversion. (b) Ozone decomposition. (c) CO_X selectivity. (d) VOCs mineralization ($O_3 = 210 \pm 10$ ppm, $T = 30 \pm 1$ °C, HCHO = 100 ± 5 ppm, $CH_3OH = 100 \pm 5$ ppm, $C_4H_8O_2 = 20 \pm 2$ ppm, $C_4H_8O_2 = 20$ ppm, C

HCHO (formaldehyde), the most common aldehyde VOCs, widely exists in industrial production, home decoration, automobile exhaust, etc., causing serious harm to human health and environmental quality. In the catalytic ozonation of HCHO, the initial HCHO conversion rate of CTAB/NiO-2/3 can reach 95%, which is superior to that of CTAB/NiO-0 (86%). After a 4 h reaction, the HCHO conversion rate of CTAB/NiO-2/3 decreased by less than 10% while that of CTAB/NiO-0 decreased by 14%, demonstrating that CTAB modification enhanced the catalytic stability of the catalyst. Figure 7c displayed the effects of the modification on CO_x selectivity and it can be seen that a similar trend of CO_x selectivity change occurs after modification. The HCHO mineralization rate of CTAB/NiO-2/3 was maintained at above 85% during the reaction process (Figure 7d). Catalytic ozonation of formaldehyde involves two reaction steps. First, formaldehyde is oxidized

to formic acid, i.e., HCHO + $O_3 \rightarrow$ HCOOH + O_2 , and then formic acid is oxidized to carbon dioxide and water, i.e., HCOOH + $O_3 \rightarrow$ CO₂ + O₂ + H₂O [39]. Due to the whole reaction having no other by-products, and formic acid can be easily completely oxidized by ozone at room temperature. Therefore, HCHO would be highly selectively oxidized into CO₂ and H₂O, maintaining a high mineralization rate [39]. At the same time, the high mineralization rate also directed that CTAB/NiO-2/3 can make full use of ozone to remove HCHO and avoid secondary pollution to the environment.

 ${\rm CH_3OH}$ (methanol) is widely used in making fragrances, dyes, medicines, antifreeze, and other products. In terms of the catalytic ozonation of ${\rm CH_3OH}$, compared with CTAB/NiO-0, the CTAB/NiO-2/3 still held on a high conversion rate of 97% after 4 h of reaction, demonstrating stronger stability (Figure 7a). However, according to the results in Figure 7c,d, CTAB/NiO-2/3 showed poor ${\rm CO_x}$ selectivity and ${\rm CH_3OH}$ mineralization efficiency, both achieving only 50–60%. During the catalytic ozonation reaction, methanol was first oxidized to formaldehyde, then formaldehyde was oxidized to formic acid, and finally further oxidized to ${\rm CO_2}$ and ${\rm H_2O}$. Based on the results of the previous section (Figure 7), HCHO could not be fully oxidized when the concentration ratio of HCHO/O₃ was about 1:2. Therefore, it can be speculated that in the catalytic ozonation reaction of methanol, the by-products (formaldehyde, formic acid) cannot be timely converted into ${\rm CO_2}$ and ${\rm H_2O}$, and may accumulate on the surface of the catalyst [40]. Which may account for the low ${\rm CO_x}$ selectivity and methanol conversion of CTAB/NiO-0 and CTAB/NiO-2/3.

 $C_4H_8O_2$ (ethyl acetate) is a versatile fine chemical product and industrial solvent, mainly used in the manufacture of paint, artificial leather, plastic products, etc. [41,42]. As shown in Figure 7a, the initial $C_4H_8O_2$ conversion rate of CTAB/NiO-2/3 can reach 95%, which exceeded that of CTAB/NiO-0 (82%), and after a 4 h reaction, the conversion rate of CTAB/NiO-2/3 decreased to about 80%, while that of CTAB/NiO-0 decreased to 68%. Moreover, both CTAB/NiO-0 and CTAB/NiO-2/3 exhibited high CO_x selectivity over $C_4H_8O_2$ during the reaction, reaching about 75% and 80%, respectively (Figure 7c). What is more, CTAB/NiO-2/3 possessed better $C_4H_8O_2$ mineralization efficiency. Therefore, compared with CTAB/NiO-0, the modified CTAB/NiO-2/3 displayed a significant improvement in catalytic performance for typical VOCs in terms of the conversion rate, CO_x selectivity, and mineralization rate.

The oxygen-containing functionalities were also reported to enhance electron donor-accept interaction and electrostatic interaction between adsorbents and polar molecules [43]. Therefore, OVOCs (aldehydes, alcohols, and esters, etc.) tended to interact more with H_2O , which reduced the adsorption capacity of OVOCs and H_2O on the catalyst surface, and also weakened the competitive adsorption of O_3 and O_3 and O_4 and O_4 alcohols, and esters was superior to that in the catalytic ozonation of toluene.

4. Conclusions

In our work, a series of CTAB-modified NiO catalysts were prepared using a thermal solvent method and modified with CTAB as a crystal structure-directing agent. The effect of CTAB on the catalytic ozonation performance of the NiO catalysts was investigated. XRD analysis revealed that both pristine and CTAB-modified NiO have a monoclinic structure. BET and H_2 -TPR results showed that the introduction of CTAB was beneficial to the enhancement of surface area and redox properties. CTAB/NiO-2/3 exhibited the best catalytic activity in catalytic ozonation of toluene at room temperature (30 °C), which was superior to unmodified NiO. What is more, according to in situ DRIFTS, it is clear that the by-products on the CTAB/NiO-2/3 surface were oxidized to a higher degree, which contributed to the oxidation of toluene to CO_2 and H_2O . Additionally, CTAB modification could significantly enhance the catalytic ozonation performance for formaldehyde, methanol, and ethyl acetate.

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Writing—original draft, C.A.; Writing—review & editing, T.Z. All authors have read and agreed to the published version of the manuscript.

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Conflicts of Interest: The authors declare no conflict of interest.

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Article

The Promoting Effect of Metal Vacancy on CoAl Hydrotalcite-Derived Oxides for the Catalytic Oxidation of Formaldehyde

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Abstract: Formaldehyde (HCHO) is a major harmful volatile organic compound (VOC) that is particularly detrimental to human health indoors. Therefore, effectively eliminating formaldehyde is of paramount importance to ensure indoor air quality. In this study, CoAl hydrotalcite (LDH) was prepared using the co-precipitation method and transformed into composite metal oxides (LDO) through calcination. Additionally, a metal Al vacancy was constructed on the surface of the composite metal oxides (E_X -LDO and E_X -LDO/NF) using an alkaline etching technique. SEM demonstrated the successful loading of CoAl-LDO onto nickel foam surfaces (LDO/NF), and an extended etching time resulted in a greater number of porous structures in the samples. XRD confirmed the successful synthesis of the precursor materials, CoAl hydrotalcite (CoAl-LDH) and CoAl layered double oxides (CoAl-LDO). EDS analysis confirmed a reduction in aluminum content after alkaline etching. XPS analysis verified the presence of abundant Co²⁺ and surface oxygen as crucial factors contributing to the catalyst's excellent catalytic activity. The experimental results indicated that catalysts containing metal cation vacancies exhibited superior catalytic performance in formaldehyde oxidation compared to conventional hydrotalcite-derived composite oxides. H_2 -TPR confirmed a significant enhancement in the participation of lattice oxygen in the catalytic oxidation reaction; it was found that the proportion of surface lattice oxygen consumption by the E5-LDO catalyst (30.2%) is higher than that of the LDO catalyst (23.4%), and the proportion of surface lattice oxygen consumption by the E₁-LDO/NF catalyst (27.5%) is higher than that of the LDO/NF catalyst (14.6%), suggesting that cation vacancies can activate the surface lattice oxygen of the material, thereby facilitating improved catalytic activity. This study not only reveals the critical role of surface lattice oxygen in catalytic oxidation activity, but also aids in the further development of novel catalysts for efficient room-temperature oxidation of HCHO. Moreover, it provides possibilities for developing high-performance catalysts through surface modification.

Keywords: formaldehyde (HCHO); layered double oxides (LDOs); metal vacancy; alkaline etching

1. Introduction

Formaldehyde (HCHO) is a commonly found volatile organic compound (VOC) and a highly detrimental indoor air pollutant, primarily originating from wooden furniture and building materials. Moreover, the time spent indoors by individuals has increased (80–90%), especially after the outbreak of the coronavirus disease (COVID-19) [1]. Prolonged exposure to even low concentrations (ppm) of HCHO may lead to various health issues, such as inflammation of the eyes and throat, chronic respiratory diseases, neurological disorders, and even cancer [2–4]. To meet the requirements of increasingly stringent environmental regulations, the development of effective techniques for removing indoor formaldehyde

is particularly important and urgent. Various strategies have been developed to reduce indoor HCHO levels. While traditional physical adsorption and ventilation are known for their removal efficiency of HCHO, unfortunately, adsorbents are limited in their removal capacity and can only be effective for a short period, while ventilation methods have low efficiency in removing indoor HCHO. In contrast, catalytic oxidation is considered the most effective method, as it can continuously and completely oxidize HCHO to water and carbon dioxide at room temperature [5–9].

Layered double hydroxides (LDHs) are a type of layered bimetallic hydroxide that possess characteristics such as interlayer ion exchange and alkalinity. Hydrotalcite, a representative LDH, is composed of layers and interlayer organic/inorganic anions. The divalent metal cations (Mg²⁺, Fe²⁺, Cu²⁺, Ni²⁺, etc.) are coordinated with hydroxyl groups to form octahedra, constituting the layers. The structure consists of positively charged host layers of metal hydroxides and interlayer regions with compensating anions and solvent molecules [10,11]. The general formula of LDH is $[M_{1-x}^{2+}M_x^{3+}(OH)_2]^{x+} \bullet A_{x/n}^{n-} \bullet mH_2O$, where M^{2+} and M^{3+} represent the divalent and trivalent metal cations; A^{n-} is the interlayer anion, X denotes the proportion of trivalent metal cations (usually 0.2 < X < 0.33), and m represents the number of solvent molecules (typically water) [10–15]. LDHs have received significant attention due to their high stability and structural diversity [12–15]. Li et al. [15] prepared Au-decorated cobalt (Co)-doped Mg/Al layered double hydroxide catalysts by depositing uniformly distributed Au nanoparticles onto preformed Co-LDH nanosheets using in situ deposition. The loading amount of Au was 2 wt% (2%Au/Co-LDH). The 2% Au/Co-LDH catalyst demonstrated higher activity for the complete oxidation of indoor formaldehyde (HCHO) to CO₂ compared to the undoped 2% Au/LDH binary sample and other control samples. The mixed oxides obtained by calcining LDHs are referred to as layered double oxides (LDOs). Compared to the pristine LDHs, LDOs exhibit unique structures characterized by high surface area, abundant active sites, and stable dispersed metals. These features make LDOs highly attractive as adsorbents, catalysts, or catalyst precursors. Particularly, in recent years, transition metal-containing LDOs have been widely employed as highly active catalysts for the degradation of air pollution [16-19]. Xie et al. [18] synthesized Co₂Ca₁Al₁-LDO as a type of layered double oxide (LDO) material. For the first time, Co₂Ca₁Al₁-LDO was employed for the activation of peracetic acid (PAA). The Co₂Ca₁Al₁-LDO/PAA system exhibited removal rates ranging from 90.4% to 100% for various micro-pollutants. Additionally, the catalyst demonstrated excellent reusability and stability. Chen et al. [19] incorporated Co into Mn₁Fe_{0.25}Al_{0.75}O_x-LDO and found that the N₂ selectivity for NH₃-SCR significantly improved within the low temperature range of 150-250 °C when the Co/Mn molar ratio was 0.5. Zeng et al. [17] prepared NiMnAl-LDO catalysts with different treatment times using a solution plasma-assisted method for CO₂ methanation reaction. The results demonstrated an enhancement in the low-temperature activity of the catalysts. Among them, the highly dispersed NiMnAl-LDO-P (20) catalyst exhibited the highest catalytic activity for CO₂ methanation (at 200 °C, CO₂ conversion rate of 81.3% and CH₄ selectivity of 96.7%); even after 70 h of operation, the catalyst maintained a high level of stability.

As a typical transition metal oxide, cobalt oxide (Co_3O_4) exhibits significant performance in the catalytic oxidation of formaldehyde due to its good low-temperature reducibility, high oxygen migration rate, and generation of reactive oxygen species (ROS). Co^{3+} and oxygen vacancies are the active sites for formaldehyde chemical adsorption and O_2 activation, respectively. As a representative non-layered material, $2D Co_3O_4$ nanosheets exhibit the characteristics of both the bulk and 2D structure. Ultra-thin $2D Co_3O_4$ nanosheets have been employed for catalytic oxidation of gaseous pollutants [7,20,21]. However, considering that most reported Co_3O_4 -based catalysts completely degrade HCHO at temperatures above room temperature, achieving effective catalytic oxidation of HCHO on Co_3O_4 remains challenging [6,22].

Nickel foam (NF) possesses a unique porous structure that is suitable for loading other metal oxides or active functional groups, making it widely studied in the fields of electrocatalysis, photocatalysis, and more [23]. Additionally, NF exhibits excellent thermal shock resistance, ensuring sufficient stability as a catalyst support. Moreover, the good thermal conductivity of NF is advantageous for many thermos-catalytic reaction processes. Therefore, using NF as a carrier for photo-thermal catalysis is highly suitable [9,24].

In this study, LDO catalysts were successfully prepared on nickel foam via a welldesigned hydrothermal method and alkaline etching. The influence of etching time on the catalytic oxidation of formaldehyde (HCHO) and the degradation efficiency was investigated. The crystal structure and morphology of LDO were characterized using X-ray diffraction (XRD), scanning electron microscopy (SEM), energy-dispersive X-ray spectroscopy (EDS), Brunauer-Emmett-Teller (BET) analysis, hydrogen temperature-programmed reduction (H₂-TPR), and X-ray photoelectron spectroscopy (XPS). The samples exhibited a unique two-dimensional nanoarray structure and abundant large-scale porous morphology. The experimental results indicated that catalysts containing metal cation vacancies exhibited superior catalytic performance in formaldehyde oxidation compared to conventional hydrotalcite-derived composite oxides. H₂-TPR confirmed a significant enhancement in the participation of lattice oxygen in the catalytic oxidation reaction; it was found that the proportion of surface lattice oxygen consumption by the E_5 -LDO catalyst (30.2%) is higher than that of the LDO catalyst (23.4%), and the proportion of surface lattice oxygen consumption by the E_1 -LDO/NF catalyst (27.5%) is higher than that of the LDO/NF catalyst (14.6%), suggesting that cation vacancies can activate the surface lattice oxygen of the material, thereby facilitating improved catalytic activity. The excellent HCHO purification performance of the prepared material demonstrated that the rational selection of the preparation process and alkali etching modification to create oxygen vacancies are effective strategies for enhancing the material's HCHO purification capability. The experimental results indicated that catalysts containing metal cation vacancies exhibited superior catalytic performance in formaldehyde oxidation compared to conventional hydrotalcite-derived composite oxides.

2. Experimental Section

2.1. Materials

All of the reagents employed in this study were of analytical reagent grade and without purification. Cobaltous nitrate hexahydrate [Co(NO₃)₂·6H₂O], aluminum nitrate nonahydrate [Al(NO₃)₃·9H₂O], urea [CO(NH₂)₂], sodium NaOH, C₃H₆O, NaOH, HCl, and C₂H₅OH were commercially available from China National Pharmaceutical Reagent Co., Ltd. Foam nickel (purity: 99.9%, thickness: 1.5 mm, porosity: 97 \pm 2%) was purchased from Taiyuan Lizhiyuan Technology Co., Ltd. (Shanxi, China).

2.2. Catalyst Preparation

2.2.1. Pretreatment of Nickel Foam

First, foam nickel was cut into rectangular blocks measuring $2.5~\rm cm \times 6~\rm cm$. Subsequently, the cut foam nickel blocks were placed in separate beakers and immersed in acetone solution for $10~\rm min$ under ultrasonic treatment to remove surface-adsorbed organic compounds and impurities. After ultrasonic treatment, the foam nickel was rinsed with distilled water for $5~\rm min$ to remove residual acetone. Then, the foam nickel blocks were soaked in $2~\rm mol/L$ HCl for $10~\rm min$ to remove the surface oxide layer. Finally, the pre-treated foam nickel was washed three times with deionized water and dried in a vacuum drying oven at $80~\rm ^{\circ}C$ to obtain the prepared foam nickel.

2.2.2. Synthesis of LDO and LDO on Ni Foam

Briefly, 9 mmol of cobalt nitrate and 3 mmol of aluminum nitrate were separately weighed into a beaker and dissolved in an appropriate amount of deionized water, resulting in solution A. Then, 40 mmol of urea was weighed and dissolved in an appropriate amount of deionized water, resulting in solution B. Solution A and solution B were mixed together, and 2 mL of ethylene glycol solution was added to prepare a 70 mL mixed solution. The

mixed solution was subjected to ultrasonic treatment for 30 min and then transferred to a reaction vessel. The pre-treated foam nickel was placed into the solution, and the reaction was conducted at 100 °C for 9 h. After the 9 h reaction at 100 °C, the foam nickel samples were washed three times with deionized water and anhydrous ethanol, respectively. Meanwhile, the residual solution in the reaction vessel was left undisturbed for 1 h, and the supernatant was removed. The obtained precipitate was filtered using a suction filtration apparatus until neutral, resulting in the CoAl-LDH sample. The obtained foam nickel and CoAl-LDH were dried in an air drying oven at 60 °C for 6 h and then calcined in a muffle furnace at 350 °C for 3 h to obtain CoAl-LDO supported on foam nickel (CoAl-LDO/NF) and powdered CoAl-LDO.

2.2.3. Synthesis of Etched LDO and LDO on Ni Foam

Alkaline etching of prepared CoAl-LDO/NF and CoAl-LDO: The prepared CoAl-LDO/NF and CoAl-LDO samples were individually subjected to reaction in a 6 mol/L NaOH solution in a reaction vessel for 1 h and 5 h, respectively. After removing the samples from the solution, they were washed repeatedly with deionized water and ethanol, followed by drying at 60 °C for 8 h. The obtained samples were labeled as LDO/NF, E_1 -LDO/NF, E_5 -LDO/NF and LDO, E_1 -LDO, E_5 -LDO.

2.3. Catalyst Characterization

The powder X-ray diffraction (XRD) measurements were carried out on a desktop X-ray diffractometer (Bruker D8 Advance, German) in reflection mode with Cu K α radiation (λ = 1.54060 Å). Diffraction patterns were recorded within the 2 θ range of 10–80 $^{\circ}$ with a scanning rate of 2 $^{\circ}$ min⁻¹.

The morphology and microstructure of the samples were tested using a scanning electron microscope (SEM, ZEISS Gemini 300) and elemental mapping was performed by EDX spectroscopy using an OXFORD XPLORE30 detector.

The Brunauer-Emmett-Teller (BET) surface area and pore size distributions of catalysts were measured by N_2 adsorption and desorption isotherms at 77.35 K using an Autosorb iQ Station 2.

The redox capability of the catalyst was analyzed using H_2 temperature-programmed reduction (H_2 -TPR). The H_2 -TPR experiment was conducted on a chemisorption instrument equipped with a thermal conductivity detector (TCD). Firstly, 20 mg of the catalyst (in the case of bulk catalyst, it was cut into small pieces) was weighed and placed into a quartz reactor. Then, the catalyst was pretreated under N_2 atmosphere at 100 °C for 1 h. After the catalyst reached room temperature, the reduction experiment was carried out under a 5% H_2/N_2 atmosphere, and the temperature was increased from room temperature to 800 °C at a heating rate of 10 °C/min.

X-ray photoelectron spectroscopy (XPS) is a method used to measure the energy distribution of emitted photoelectrons and Auger electrons from the surface of a sample when irradiated with X-ray photons, using an electron spectrometer. XPS is employed for qualitative and quantitative analysis of the elemental composition and chemical states of the surface species based on their unique binding energies. XPS measurements were performed on a Thermo ESCALAB 250Xi electron spectrometer.

2.4. Catalytic Activity Tests

Catalyst performance evaluation was carried out in a micro-fixed-bed reactor, with 50 mg of catalyst loaded into a reaction tube with an inner diameter of 6 mm. A diffusion bottle containing 150 g of paraformaldehyde was heated using a water bath, causing the decomposition of paraformaldehyde and generating a gas stream containing formaldehyde. The inlet gas composition was 100 mL/min of 21% O_2/N_2 , and nitrogen (N_2) as carrier gas was introduced through the paraformaldehyde solid powder immersed in the water bath to generate formaldehyde gas, with a concentration of 22 ppm and a water bath temperature of 40 °C. The reaction temperature ranged from 50 to 200 °C, and the temperature ramp

was controlled by a temperature controller with a heating rate of 5 $^{\circ}$ C/min. Prior to heating, the catalyst was purged with a flow of gas containing formaldehyde (100 ppm) at 30 $^{\circ}$ C for 3 h to test the formaldehyde adsorption performance of the catalyst and eliminate the interference of adsorption on subsequent reaction evaluations. The reaction gas flow passed through the catalyst in the quartz reaction tube, where formaldehyde was oxidized to carbon dioxide (CO₂) and H₂O. The gas flow rate was controlled using a mass flow controller, and the temperature of the catalyst bed was maintained. The reaction product, CO₂, was detected and analyzed using a gas chromatograph equipped with a carbon dioxide detector. Before recording data, the corresponding temperature was maintained for 40 min to obtain stable values. The concentration of CO₂ was recorded every 11 min during the test. Three samples were taken at each temperature point, and then the temperature was increased for data collection at the next temperature point. No other carbon-containing compounds were detected in the reaction products besides CO₂. Therefore, the concentration of CO₂ reflects the activity of the catalyst, i.e., the conversion rate of formaldehyde. The formula is as follows:

$$HCHO\ conversion\ \% = \frac{[\Delta C\ O_2]}{[HCHO]_{in}} \times 100\%$$

Here, $[HCHO]_{in}$ represents the concentration of formaldehyde (ppm) in the gas stream before the reaction, and $[\Delta CO_2]$ represents the difference in CO_2 concentration (ppm) in the gas stream before and after the reaction.

3. Results and Discussion

3.1. Morphology and Structure

In this study, the microstructure of synthesized material samples was characterized using scanning electron microscopy (SEM) and energy-dispersive spectroscopy (EDS) (Figure 1). Nickel foam (Figure 1g) exhibited an interconnected framework structure with large voids, making it an ideal template for the growth of other active materials and providing a higher specific surface area for anchoring CoAl-LDH. After loading with LDO, the originally smooth surface of the nickel foam was covered with a uniform layer of E₁-LDO (Figure 1a,c,e), which showed a cross-linked structure, significantly enhancing the adhesion of the active metal. Meanwhile, the thickness of the active substance loaded on the surfaces of E₁-LDO/NF and E₅-LDO/NF was thinner than that of LDO/NF, which may be attributed to the etching of Al3+. Figure 1a,b displayed the growth of LDO on nickel foam, showing a uniform layered structure that was consistent with the morphology reported in the literature [16]. Figure 1c,d were SEM images of E₁-LDO/NF thin films on nickel foam, which exhibited a thinner and well-separated structure compared to LDO/NF, featuring a unique porous morphology and higher specific surface area. Figure 1e,f were SEM images of E₅-LDO/NF thin films on nickel foam, and the sample etched for 5 h exhibited more porous structures than the one etched for 1 h, maximizing the contact efficiency between gas molecules and active sites. The SEM image of LDO (Figure 2b) revealed that the original regular hexagonal flakes were disrupted and became disordered, increasing the specific surface area of LDO, which indicated a higher exposure of active sites compared to LDH for subsequent experiments [25]. However, it can be observed that the regular hexagonal flakes on the surface of E_5 -LDO/NF remained intact, possibly due to insufficient calcination. The structure of the E5-LDO/NF sample and E5-LDO were analyzed via energy-dispersive spectroscopy (EDS) (Figure 1i,j), and it was observed that Co and Al elements were uniformly distributed on the surface of the nickel foam, indicating the successful preparation of LDO material on the nickel foam. Furthermore, with an increase in etching time, the ratio of Co to Al gradually increased (Table 1). However, the presence of residual Al indicated that Ex-LDO/NF was only partially etched by NaOH, and not completely etched.

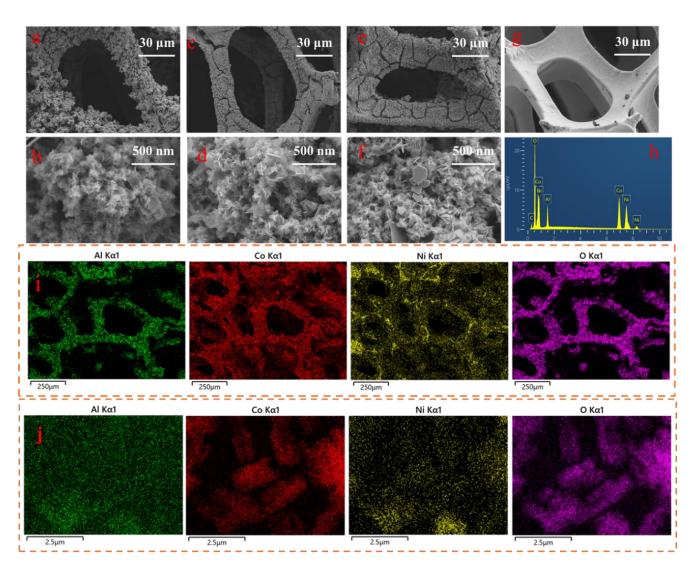


Figure 1. SEM images of (a,b) LDO/NF, (c,d) E_1 -LDO/NF, (e,f) E_5 -LDO/NF, (g) Ni foam, (h) EDX pattern of E_5 -LDO/NF, (i) EDS mapping of the E_5 -LDO/NF, and (j) EDS mapping of the E_5 -LDO.

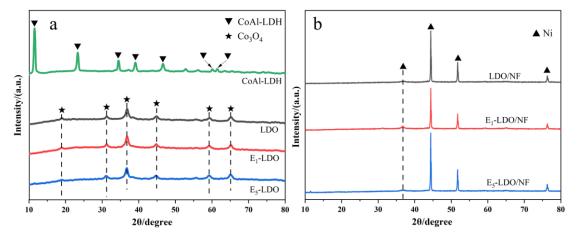


Figure 2. XRD patterns of (a) CoAl-LDH, LDO and E_X -LDO (X = 1, 5) and (b) LDO/NF and E_X -LDO/NF (X = 1, 5).

Table 1. Distribution of element content on catalyst surface, obtained via EDS surface scanning.

wt%	LDO/NF	E ₁ -LDO/NF	E ₅ -LDO/NF
Со	19	17	18
Al	6.	4	4
С	17	19	19
O	43	44	43
Ni	15	16	16

In this work, X-ray diffraction (XRD) patterns were used to investigate the composition and structural characteristics of the materials. Figure 2 shows the XRD spectra of CoAl-LDH, LDO and E_X -LDO (X = 1, 5). Figure 2a presents a comparison of XRD patterns between CoAl-LDH and LDO prepared under different etching times. It can be observed that the diffraction peaks of CoAl-LDH at 11.5° , 23.5° , 34.8° , 39.4° , 46.6° , 56.2° , and 61.5° correspond to the (003), (006), (009), (015), (018), (110), and (113) planes, respectively [26–28]. These peaks indicate the typical layered double hydroxide (LDH) structure of the sample (JCPDS 51-0045). The XRD diffraction peaks of the precursor material, CoAl-LDH are consistent with the literature, confirming the successful synthesis of the precursor and the target product. The sharpness of the (003) and (006) diffraction peaks suggests the high crystallinity of the prepared CoAl-LDH [29,30]. By comparing the XRD patterns of the precursor CoAl-LDH and LDO and E_X -LDO (X = 1, 5), significant changes in the crystal plane characteristics of CoAl-LDH can be observed. After calcination at 350 °C and etching treatment with NaOH solution, the XRD characteristic peaks of CoAl-LDH disappear, and the characteristic peaks of LDO are observed at 19.2°, 31.2°, 36.6°, 44.8°, 59.4°, and 65.1°, corresponding to the (011), (220), (311), (400), (511), and (440) planes of CoAl₂O₄ (JCPDS no. 38e0814), respectively. This indicates a significant phase transformation of CoAl-LDH during high-temperature treatment. The layered structure of CoAl-LDH is destroyed after calcination, resulting in a highly dispersed mixture of metal oxide. Figure 2b shows the XRD spectra of LDO/NF and E_X -LDO/NF (X = 1, 5). For the bulk catalyst LDO/NF, the characteristic peak at 36.7° (311) can be attributed to NiO (JCPDS card No. 47-1049), while the peaks at 44.45° (111), 51.8° (200), and 76.3° (220) correspond to Ni [23,31]. No peaks from other phases were detected in both modes, indicating that the loaded LDO structure is not prominent. Additionally, in the XRD spectrum of E5-LDO/NF, the Ni characteristic peaks are stronger and have larger integrated areas compared to E₅-LDO, indicating that extending the etching time exposes more active sites and can improve the crystallinity of other metal oxides on nickel foam.

The N₂ adsorption-desorption isotherms and pore size distributions of LDO and E_1 -LDO are shown in Figure 3, according to the standard of scientific papers. The isotherms are consistent with type IV isotherms and exhibit an H_3 hysteresis loop (P/P₀ > 0.4), indicating the formation of mesopores with a three-dimensional interconnected porous structure, which is beneficial for rapid mass transfer [28,32,33]. The specific surface areas of both catalysts can be calculated from the N₂ desorption isotherms using the BET method. The specific surface area of E_1 -LDO (136 m² g⁻¹) is significantly larger than that of LDO (69 m² g⁻¹). E₁-LDO possesses more active sites than LDO, suggesting that the etching effect of NaOH results in a higher specific surface area for E₁-LDO. The pore size distribution reveals that E₁-LDO with a diameter of 3–7 nm has a narrower pore size distribution compared to LDO with a diameter of 3-10 nm. The larger specific surface area and uniform porous structure provide more active sites and facilitate the adsorption of reactants, which is advantageous for excellent catalytic performance. However, the specific surface area of E_5 -LDO (71 m² g⁻¹) is not significantly different from that of LDO (69 m² g⁻¹). However, the catalytic activity of E₅-LDO is much higher than that of LDO, indicating that the specific surface area is not the primary factor affecting the catalytic performance of the catalyst for formaldehyde oxidation.

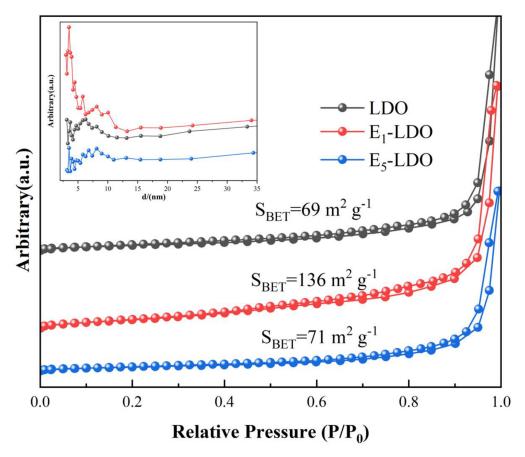


Figure 3. N₂ adsorption and desorption isotherms and pore size distribution (inset) of LDO and E_X -LDO (X = 1, 5) catalysts prepared by calcination at 500 °C.

3.2. Activation Performance of Prepared Material

The variation in formaldehyde conversion rates with temperature (50–175 °C) for the LDO, E_X -LDO (X = 1, 5) and LDO/NF, E_X -LDO/NF (X = 1, 5) catalysts with different etching times are shown in Figure 4. It can be observed that etching has a significant effect on the catalytic activity of both catalysts towards formaldehyde, and the etching time greatly influences the catalytic performance of the catalysts. It can be observed that at the highest temperature of 175 °C, the HCHO conversion rate of LDO catalyst is less than 50%, indicating low catalytic activity. Compared to LDO, the etched catalysts E₁-LDO and E₅-LDO exhibit improved catalytic activity over the entire temperature range. E₁-LDO achieves a 50% HCHO conversion rate at 81 °C, while E₅-LDO reaches a 90% HCHO conversion rate at 110 °C. E₅-LDO shows higher HCHO conversion rates than E₁-LDO across the entire temperature range, which may be attributed to the longer etching time, resulting in a higher concentration of active oxygen species in E_5 -LDO, thereby promoting the activity towards HCHO. Comparing the powder-type CoAl-LDO_X catalysts to the supported catalysts, the former exhibit higher HCHO conversion rates, which could be attributed to the lower loading of active components on the surface of LDO/NF and E_X -LDO/NF (X = 1, 5).

3.3. Surface Chemistry

The surface elemental composition and oxidation states of surface materials were investigated using X-ray photoelectron spectroscopy (XPS). All binding energies were calibrated using the C1s peak at 284.6 eV. The Co 2p and O 1s XPS spectra of the catalyst are shown in Figure 5, and the quantitative analysis of the different oxidation states of Co and O is presented in Table 2, based on the XPS spectra. As shown in Figure 5a, the Co 2p peak exhibits spin–orbit splitting into doublets. The spin–orbit peaks can be fitted with

two pairs of peaks. One pair of peaks located at 780.6 and 796.2 eV is assigned to Co 2p3/2, while the other pair at 779.4 and 794.7 eV is assigned to Co 2p1/2. The peaks at 790.1 and 805.2 eV are attributed to satellite peaks. These values are in good agreement with the reference data for Co₃O₄ [34,35]. Furthermore, the coexistence and transformation of Co²⁺ and Co³⁺ in the Co-Al system provide possible catalytic mechanisms [36,37]. The ratio of surface Co²⁺/Co³⁺ in the catalyst was calculated based on the peak areas in the XPS spectra, as shown in Table 2. The results indicate that the Co²⁺ content on the catalyst surface is higher after etching compared to before, and the Co²⁺ content increases with longer etching time. Generally, a higher surface Co²⁺ content indicates a higher concentration of surface oxygen vacancies, which is considered a prerequisite for achieving high catalytic activity [38,39]. In Figure 5c,d, it can be seen that the O1s spectrum is deconvoluted into three characteristic peaks with binding energies of 532.47~533.2, 531.3~531.4, and $529.5 \sim 529.8$ eV. The black peaks ($529.5 \sim 529.8$ eV) are attributed to lattice oxygen (O_{latt} : O^{2-}) in a coordinated saturated environment. The red peaks (531.3~531.4 eV) are associated with surface-adsorbed oxygen (O_{ads}: O₂²⁻, O₂⁻ or O⁻) and oxygen defects in an unsaturated coordination mode. The blue peaks (532.47~533.2 eV) are related to the OH groups of water molecules adsorbed on the sample surface. A higher density of surface oxygen vacancies (O_V) is generally associated with the easier activation of gaseous oxygen to form electrophilic O_{ads} species, which plays a crucial role in the deep oxidation of VOCs [40]. According to Table 2, the O_{ads}/O_{latt} ratio of the catalyst increases after etching compared to before, indicating a higher amount of surface adsorbed oxygen. Therefore, enhanced surface oxygen properties can promote the oxidation of formaldehyde. Consistent with the results of the activity experiments, it can be concluded that the abundance of Co²⁺ and surface oxygen is an important factor contributing to the excellent catalytic activity of the catalyst.

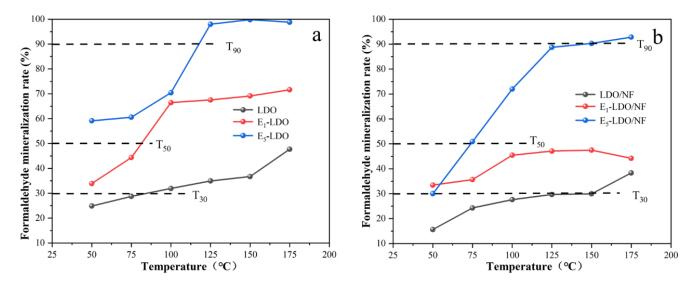


Figure 4. HCHO conversion of (a) CoAl-LDO_X and (b) E_X -LDO/NF catalysts (X = 1, 5). Reaction conditions: [HCHO] = 20 ppm, $[O_2]$ = 21 vol%, GHSV = 30,000 h⁻¹ and N_2 as balance gas.

Table 2. The surface compositions of the different samples.

	LDO	E ₁ -LDO	E ₅ -LDO	LDO/NF	E ₁ -DO/NF	E ₅ -LDO/NF
Co ²⁺ /Co ³⁺	97.0394	105.9704	122.922	100.0167	110.9602	120.4848
O _{ads} /O _{latt}	90.33875	93.54537	104.5528	45.57956	125.4108	127.7475

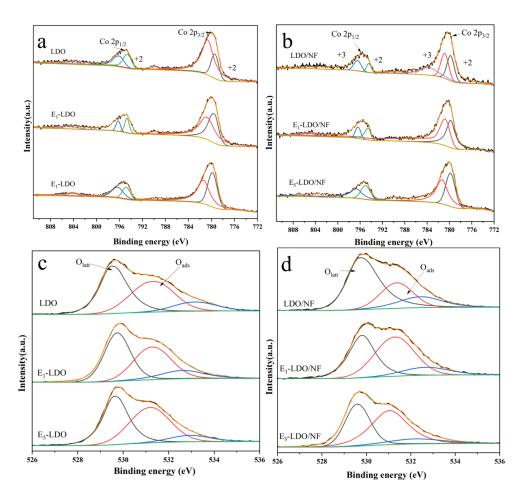


Figure 5. XPS spectra of the (a) Co 2p core level of LDO and E_X -LDO (X = 1, 5); (b) Co 2p core level of LDO/NF and E_X -LDO/NF (X = 1, 5); (c) O1s core level of LDO and E_X -LDO (X = 1, 5); and (d) O1s core level of LDO/NF and E_X -LDO/NF (X = 1, 5).

The oxidation of formaldehyde is closely related to the redox performance of the catalysts, wherein the reduction temperature and hydrogen consumption collectively reflect the catalyst's reduction ability. H₂-TPR (temperature-programmed reduction) was conducted, as shown in Figure 6, to determine the reduction behavior of Co and Al species. Previous studies suggest that the reduction of Co₃O₄ typically proceeds in the sequence of $Co^{3+} \rightarrow Co^{2+} \rightarrow Co^{0}$, with T_{max} at 300 °C and 400 °C [41,42]. The catalyst exhibits reduction in three major temperature ranges: the low-temperature reduction (200-300 °C) represents the transition from Co³⁺ to Co²⁺, the mid-temperature peak (300–500 °C) corresponds to the reduction of Co²⁺ to Co⁰, and the high-temperature peak (500–900 °C) can be attributed to the reduction of CoAl₂O₄ [41–43]. E₁-LDO and E₅-LDO show more pronounced reducible peaks compared to LDO, indicating the presence of more active oxygen in E₁-LDO and E₅-LDO. In the CoAl₂O₄ compound, the polarization of Co-O bonds by Al³⁺ ions leads to an increase in the reduction temperature of Co²⁺, providing a plausible explanation for the presence of the third TPR peak [44] in the Figure 6a. For LDO, E₁-LDO, and E₅-LDO, the reduction of Co³⁺ to metallic Co⁰ gives rise to three peaks in the temperature range, which are associated with oxygen adsorbed on surface vacancies, surface lattice oxygen, and bulk lattice oxygen, respectively. Compared to LDO/NF, the low-temperature peak of E₁-LDO/NF and E₅-LDO/NF is enhanced, and the peaks of the catalyst shift towards the lower temperature region after etching. A larger H₂ consumption area indicates that alkaline etching significantly promotes the activation of surface lattice oxygen, suggesting the stronger redox capability of the latter. The etched catalyst facilitates the completion of redox cycles. By calculating the ratio of the amount of hydrogen consumed by the surface lattice oxygen of the catalyst to the total amount of hydrogen consumed, it is

found that the proportion of surface lattice oxygen consumption by the E_5 -LDO catalyst (30.2%) is higher than that of the LDO catalyst (23.4%), and the proportion of surface lattice oxygen consumption by the E_1 -LDO/NF catalyst (27.5%) is higher than that of the LDO/NF catalyst (14.6%). These results show that cationic vacancy is formed on the surface of the material by alkali etching, which can activate the lattice oxygen of the oxide surface, and promote the catalytic oxidation of cobalt aluminum composite metal oxides to formaldehyde (Figure 7).

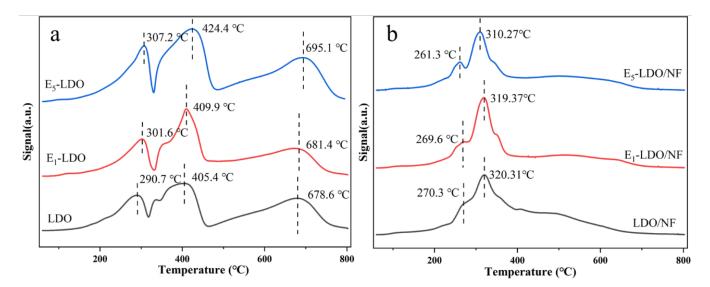


Figure 6. H₂-TPR patterns of (a) LDO and E_X -LDO (X = 1, 5) and (b) LDO/NF and E_X -LDO/NF (X = 1, 5).

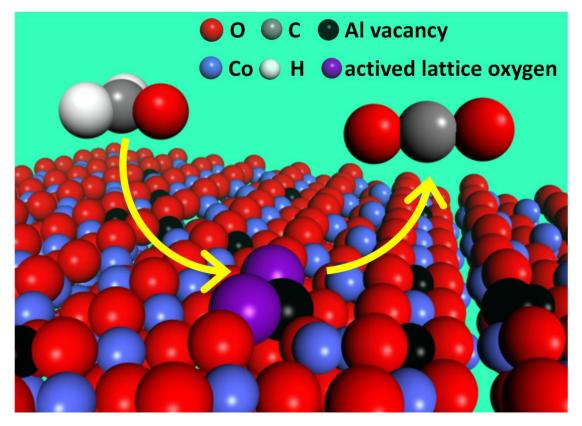


Figure 7. The cation vacancy activated the surface lattice oxygen and promoted the oxidation of formaldehyde.

4. Conclusions

In this study, $CoAl-LDO_X/NF$ catalysts were successfully prepared on nickel foam via a well-designed hydrothermal method and alkaline etching. The influence of etching time on the catalytic oxidation of formaldehyde (HCHO) and the degradation efficiency was investigated. XRD confirmed the successful synthesis of the precursor CoAl-LDH and CoAl-LDO. SEM demonstrated that CoAl-LDO was successfully loaded onto the surface of nickel foam, and increasing the etching time resulted in more porous structures in the samples. EDS analysis indicated a decrease in the aluminum content after alkaline etching. XPS revealed that the presence of abundant Co^{2+} and surface oxygen is an important factor contributing to the catalyst's excellent catalytic activity. The experimental results showed that catalysts containing metal cation vacancies exhibited superior catalytic performance in formaldehyde oxidation compared to conventional hydrotalcite-derived composite oxides. H₂-TPR confirmed a significant enhancement in the involvement of lattice oxygen in the catalytic oxidation reaction, indicating that cation vacancies can activate the lattice oxygen on the material's surface, thereby promoting improved catalytic activity, By calculating the ratio of the amount of hydrogen consumed by the surface lattice oxygen of the catalyst to the total amount of hydrogen consumed, it is found that the proportion of surface lattice oxygen consumption by the E5-LDO catalyst (30.2%) is higher than that of the LDO catalyst (23.4%), and the proportion of surface lattice oxygen consumption by the E₁-LDO/NF catalyst (27.5%) is higher than that of the LDO/NF catalyst (14.6%). This study not only elucidates the crucial role of surface lattice oxygen in catalytic oxidation activity, but also contributes to the development of novel catalysts for the efficient catalytic oxidation of formaldehyde at room temperature. Furthermore, it demonstrates the possibility of developing high-performance catalysts through surface modification.

Author Contributions: All authors contributed to the study conception and design. Y.C. and S.Z. put forward the review ideas and organized the first draft. H.Y., X.T. and S.Z. refined and finally approved the whole content. The Sections of Results and Discussion were arranged by F.G., Q.Y. and Y.Z. All authors commented on previous versions of the manuscript. All authors have read and agreed to the published version of the manuscript.

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Article

Collaborative Effect of In-Plasma Catalysis with Sequential Na₂SO₃ Wet Scrubbing on Co-Elimination of NOx and VOCs from Simulated Sinter Flue Gas

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Abstract: Sinter flue gas produced by the iron-ore sinter process in steel plants is characterized by a large gas volume and complex components. Among the major air pollutants, preliminary emissions of volatile organic compounds (VOCs) and nitrogen oxides (NOx) exhibit an inevitable contribution to secondary aerosol and ozone formation. Herein, oxidation–absorption collaborative technology for in-plasma catalysis with sequential Na₂SO₃ wet scrubbing, aiming at co-elimination of NOx and VOCs from sinter flue gas, is proposed. Experimental parameters, including plasma discharge status, NO initial concentration, gas feed flux, Na₂SO₃ concentration, pH value, and absorption ions, were systematically investigated. The VOC and NOx removal performance of the integrated system was further investigated by taking simulated sinter flue gas as model pollutants. The results showed that the collaborative system has satisfactory performance for TVOC and NO removal rates for the effective oxidation of in-plasma catalysis and Na₂SO₃ absorption. The integration of plasma catalysis with Na₂SO₃ scrubbing could be an alternative technology for the co-elimination of sinter flue gas multi-compounds.

Keywords: sinter flue gas; volatile organic compounds; in-plasma catalytic; nitrogen oxides; Na₂SO₃; integration

1. Introduction

Air-pollutant emissions from anthropogenic sources have contributed to severe hazards for atmospheric pollution and human health on a global scale and especially in China in recent decades [1–3]. Despite the positive collaborative governance effort towards haze pollution reduction [4,5], China still faces the co-existing threats of $PM_{2.5}$ and O_3 pollution during the current 14th five-year plan period. Among the main anthropogenic sources, the iron and steel industry is a major primary atmospheric pollutant emission source, owing to its intensive energy and material consumption. As well as being the largest global iron and steel producer, China's annual crude steel production reached 1.03 billion tons in 2022 and has accounted for more than 50% of the global total output for decades. The current air-pollutant emission amount from the iron and steel industry have exceeded that of thermal power plants [6]. It has also been identified that haze outbreaks and air-quality improvement concurrently occur with steel-making activities [7–9].

The iron-ore sinter process, with high dependence on fossil fuel, negative suction combustion, and massive air consumption, accounts for the largest proportion of steel-making emissions [10–12]. The components of sinter flue gas are also complicated, including particulate matter (PM) [13,14], SO₂ [15,16], NOx [17], VOCs [18], heavy metals [19], dioxins [20], and trace elements [21]. The ultra-low emission policy of the Ministry of Ecology and Environment of China regulates sinter flue gas PM, SO₂, and NOx emissions as having to be less than 10, 35, and 50 mg·m⁻³. Our previous study

revealed and investigated the simultaneous emissions of VOCs and NO during the sintering process [22]. Moreover, NOx can contribute to photochemical smog and O₃ formation when co-existing with VOCs under sunlight irradiation via a series of free-radical reactions [23,24]. The massive primary emissions of NOx and VOCs from sinter flue gas on secondary aerosol formation are much less studied, and their total impact may be underestimated. Therefore, NOx and VOCs exhibit huge deduction potential among the major air pollutants of sinter flue gas. It is urgently necessary to develop advanced elimination techniques aiming at the simultaneous abatement of NOx and VOCs from sinter flue gas emissions before the primary emission from sinter exhausts and to develop multipollutant control technology.

Various measures have been widely applied to decrease sinter flue gas primary emissions, such as desulfurization, denitrification facilities, and electrostatic precipitators. However, whether the VOC emissions can be jointly controlled by the measures taken to control PM, SO₂, and NOx emissions in sinter flue gas is not understood. Currently, primary flue gas denitrification (deNOx) technology includes selective catalytic reduction (SCR) [25], wet and dry scrubbing [26], adsorption [27], and biological treatments [28]. As for VOC removal methods, adsorption [29], biotechnology [30], catalytic oxidation (combustion) [31,32], and non-thermal plasma [33] have been developed. Both SCR and catalytic oxidation technologies play essential roles in flue gas deNOx and VOC elimination for high efficiency and fewer secondary byproducts. However, for coal-fired flue gas VOC components, the conventional pollutant control process (SCR and WFGD) has only a limited effect on VOC reduction [34]. Moreover, research concerning the co-elimination of VOCs and NOx from sinter flue gas is scarce. The modified V_2O_5 -WO₃/TiO₂ (VWT) SCR catalyst is feasible for the simultaneous removal of NO and VOCs within the reaction range of 260–420 °C [35]. Xiao et al. constructed a Cu-VWT bifunctional catalyst for deep oxidation of VOCs and the simultaneous removal of NOx under complex coal-fired flue gas conditions [36]. The removal efficiency of toluene, propylene, dichloromethane, and naphthalene exceeded 99% under 350 °C. Chen et al. developed Ce [37], Ce/Mo [35], and Cu, Fe, and Co [38] modified VWT catalysts that exhibited the collaborative removal of NO and VOCs (benzene and toluene) with different calcination temperatures and transition metal loadings. However, the desirable NOx and VOC removal performance required a specific temperature range (usually >300 °C) that was much higher than the temperature of typical sinter flue gas. Therefore, the sinter flue gas exhaust temperature could not meet the requirements of the SCR and the catalytic combustion temperature, and additional heating energy consumption was needed, which increased initial investment and operating-energy consumption. There is an urgent need to develop deNOx and VOC elimination technology suitable for low-temperature sinter flue gas.

Wet NOx removal technology has a low operating temperature and can simultaneously remove soluble volatile compounds and SO₂. More than 90% of the sinter flue gas NOx emissions are NO with poor solubility. Therefore, efficient NOx removal requires the efficient oxidation of NO to NO₂, capable of absorption by alkaline and reductive absorption. Non-thermal plasma (NTP) is an advanced oxidation method that can effectively oxidize NO and VOCs at mild operating temperatures and has the advantages of easy start-up and non-selectivity [39]. The combination of NTP and heterogeneous catalysis (the plasma-driven catalysis reaction) can improve catalytic oxidation efficiency. Different catalysts were investigated to enhance VOC removal efficiency and to inhibit byproducts [40–43]. Some other integration techniques have also been investigated for different industrial applications. Zhang et al. [44] developed an integrated system of a spray tower and photocatalysis and applied it to purify the waste gas emitted from a printed circuit board (PCB) manufacturing facility. The integrated technique achieved an average removal efficiency (RE) of 72.39% of 66 VOCs during the nine-month continuous treatment.

As discussed above, to tackle VOC and NOx emissions in the sintering process, it is necessary to design a new strategy to accomplish the simultaneous abatement of VOCs and NOx [45]. In this study, we develop an integration system of in-plasma catalysis (IPC) with sequential Na₂SO₃ wet scrubbing for the co-elimination of NOx and VOCs from sinter flue gas. NO can be fast and effectively oxidized to NO₂ in the IPC region and further absorbed by Na₂SO₃ wet scrubbing. Experimental parameters, including plasma discharge status, NO initial concentration, gas feed flux, Na₂SO₃ concentration, pH value, and absorption ions, were systematically investigated. The VOC and NO removal performance of the integrated system was further investigated by taking simulated sinter flue gas as model pollutants.

2. Materials and Methods

2.1. Chemicals and Reagents

The reagents used in the experiments are all of analytical grade without further purification. In short, sodium sulfite (Na₂SO₃) and ascorbic acid (C₆H₈O₆) were bought from Shanghai Macklin Biochemical Co., Ltd. (Shanghai, China). Gas feed, including nitrogen monoxide, nitrogen dioxide, and sulfur dioxide with purity \geq 99.999%, was bought from Shanghai Weichuang Co., Ltd. (Shanghai, China). Copper foam with purity \geq 99.8% was bought from Kunshan Jiayisheng Electronics Co., Ltd. (Kunshan, China). Iron-ore sinter raw material, composed of iron-bearing materials, fluxes, and solid fuel, was provided by Taiyuan Iron & Steel Co., Ltd. (TISCO, Taiyuan, China) to generate simulated sinter flue gas.

2.2. Experimental Setup and Analytical Method

The experiment setup (Figure 1) was divided into three units with different functions. Specifically, gas feed, controlled via a mass flow meter (pure air containing VOCs, NOx, and SO₂) after mixing in Chamber 1, was purged into a plasma catalytic reactor, followed by sequential Na₂SO₃ scrubbing. Another gas feed was provided by the air pushing the sinter raw mix into the center of a tubular furnace under different sinter temperatures to generate simulated sinter flue gas containing VOCs, NO, and SO₂ components under practical sinter conditions. After thorough mixing in Chamber 2, the simulating flue gas was purged into the IPC unit and tail Na₂SO₃ scrubbing unit.

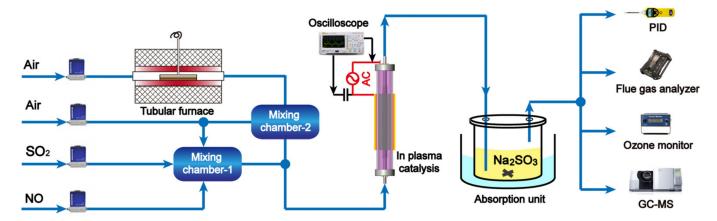


Figure 1. Experimental setups for co-elimination of VOCs and NOx from sinter flue gas.

The in-plasma catalytic unit was constructed by a typical coaxial dielectric barrier discharge (DBD) reactor, which consisted of a quartz tube and CuO foam catalyst (Figure S1 in the Supplementary Materials). Specifically, a tubular quartz tube (>99.9% SiO₂, dielectric constant: 3.75) with a length of 300 mm, inner diameter of 20 mm, and wall thickness of 2.5 mm was the discharge barrier. A wedged stainless-steel rod with a diameter of 14 mm was end-fixed along the axis of the cylinder and acted as a high-voltage electrode. A stainless-steel mesh with a length of 15 cm wrapped outside the quartz tube acted as

a ground electrode to achieve a discharge volume of 24.0 cm³. The in-plasma discharge gap was filled with monolithic CuO foam (length = 15 mm, thickness = 3 mm), which was fabricated by the calcination of copper foam before being manually rolled into a hollow cylindrical shape, as reported in our previous work [46].

The plasma-generating power supply (AC in Figure 1) was further illustrated in Figure S2 in the Supplementary Materials. Using a high-voltage alternating current (AC) power supply (CTP-2000K, Nanjing Suman Electronics Corp., Nanjing, China) equipped with an amplifier, the employed peak voltage of gas discharge can be adjusted. The maximum voltage of the power supply was 30 kV, and the frequency can vary between 1 kHz to 100 kHz. A high-voltage probe (Tektronix 6015A, 1000:1, Shanghai, China) and a voltage probe (PVP2150, RIGOL, Beijing, China) were used to record the applied high-voltage and voltage across the external capacitor, respectively. Both voltage signals were monitored using an oscilloscope (DS5062MA, RIGOL, Beijing, China). A capacitor (1 μ F) was connected between the DBD reactor and the ground to measure the amount of transferred charge. The discharge power was controlled by varying the applied voltage across the plasma reactor, which was calculated using the standard Q-U Lissajous method (detailed information was provided in Text S3 and Figure S3 in the Supplementary Materials).

As for the gas analytical unit, NOx concentration was detected by a flue gas analyzer (Testo 340, Black Forest, Germany), with a resolution of 0.1 ppm and measurement accuracy of ±5%. Both inlet and outlet VOC concentrations were recorded online using a photo ion detector (PID, RAE 3000, Honeywell, Morris Plains, NJ, USA), with a resolution of 0.1 ppm and accuracy of $\pm 3\%$ in the TVOC value from 10 to 2000 ppm. VOC components analysis was performed by thermal desorption using a sorbent tube. Specifically, a commercial stainless-steel sorbent tube (TD100xr, Markes International, Bridgend, UK) packed with a carbon molecular sieve was used for the in situ collection of sinter flue gas VOCs. The gas was collected under a consistent flow rate of 50 mL/min for 30 min and then analyzed with a GC-MS system (7890B-5977B, Agilent, Santa Clara, CA, USA). Before each use, the sorbent tube was conditioned by 300 °C thermal cleaning with N_2 (purity \geq 99.999%). In addition, a blank tube was analyzed before running the sample tubes. The absorption liquid anion (SO_4^{2-} , SO_3^{2-} , NO_3^{-} , NO_2^{-} , and Cl^{-}) was characterized using ion chromatography (IC 883, Metrohm, Herisau, Switzerland). The tail gas ozone concentration was monitored by an ozone monitor (Model 106, 2B, CO, USA) with detection accuracy of 1%.

2.3. Plasma Status Determination and Calculation

The discharge power employed for VOC and NO conversion was valued by applied peak voltage and specific input energy (SIE, J/L). The discharge power can be controlled by adjusting the applied voltage through the amplifier, with the input discharge power varying from 4.3 to 27 W, corresponding to SIE varying from 31.6 to 633.2 J/L (shown in Table S1 in the Supplementary Materials).

The efficiencies of the NO removal rate (η_{NO}), NOx removal (η_{Nox}), and TVOC removal efficiency (η_{TVOC}) were calculated using the following Equations (1) to (3):

$$\eta_{NO} = \left(\frac{[NO]_{in} - [NO]_{out}}{[NO]_{in}}\right) \times 100\%$$
(1)

$$\eta_{\text{NOx}} = \left(\frac{[\text{NOx}]_{\text{in}} - [\text{NOx}]_{\text{out}}}{[\text{NOx}]_{\text{in}}}\right) \times 100\%$$
 (2)

$$\eta_{\text{TVOC}} = \left(\frac{[\text{TVOC}]_{\text{in}} - [\text{TVOC}]_{\text{out}}}{[\text{TVOC}]_{\text{in}}}\right) \times 100\%$$
(3)

3. Results and Discussion

3.1. In-Plasma Catalytic Oxidation of Nitric Oxide

NO is the major NOx component in sinter flue gas, which accounts for over 95% depending on the sinter raw mix and sinter bed permeability [47]. In addition, desirable NOx removal requires high NO-to-NO $_2$ conversion and effective sequential NO $_2$ absorption efficiency. After NO is quickly oxidized by oxidants produced from the plasma catalytic oxidation process, NO $_2$ exists as the main component of NOx. Therefore, NO oxidation efficiency plays a leading role in NO remediation owing to the desirable Na $_2$ SO $_3$ scrubbing of NO $_2$.

NO conversion, NO₂ generation, and electron temperature under in-plasma catalysis were investigated. Pure N_2 and O_2 gas streams were well premixed with a volume ratio of 80:20 in a mixing chamber prior to the plasma catalytic region, giving a fixed inlet NO concentration of 200 ppm and flux of 400 mL/min without specific illustration. The electron temperature was monitored by an infrared thermometer (UT300S, Uni-Trend Technology CO., Ltd., Dongguan, China) by measuring infrared energy radiated from the high-voltage or discharge barrier surface. Under ideal discharge conditions, it was expected that NO would exhibit a higher conversion rate and result in relatively low NO₂ production. As shown in Figure 2, the NO conversion rate significantly improved to 92% when discharge power was above 6.75 W, and the concentration of NO₂ and electron temperature also increased, indicating the generation of energetic electrons by the electric field injection. When the discharge power was less than 10 W, the plasma discharge was not complete. After that, NO conversion was lower than 30%, and NO₂ generation reached about 120 ppm. After discharge power increased to 10 W, more active oxygen species were generated, thus leading to the NO removal efficiency increase by 93.3% and the corresponding NO₂ concentration of 125.3 ppm. When discharge power increased to 15 W, maximum NO conversion was 97.1%, and NO₂ concentration was 169.5 ppm. The electron temperature also increased to 50.4 °C. When discharge power increased to above 17 W, NO₂ generation and electron temperature increased obviously, and the NO conversion sharply decreased. Under complete discharge conditions, NO can be effectively oxidized to NO₂ by plasma-induced oxidants via a series of reactions [48,49]. The increasing amount of NO₂ was attributed to the plasma discharge of N₂ oxidation under an air atmosphere.

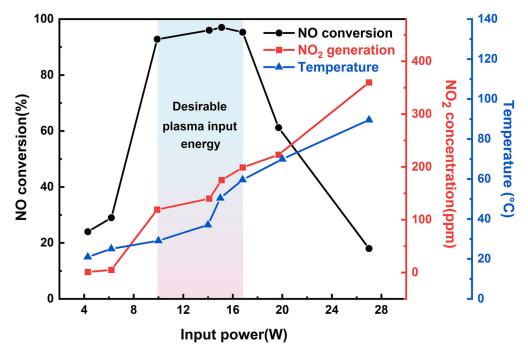


Figure 2. NO conversion (black), NO₂ generation (red), and electron temperature (blue) during a plasma catalytic oxidation reaction.

To sum up, depending on the NO conversion to NO_2 under different plasma power, the desirable discharge power range was between 10 to 17 W, the NO conversion rate reached 95.7 \pm 1.47%, and the corresponding NO_2 concentration reached 157.3 \pm 27.4 ppm.

3.2. NOx Removal by IPC Coupling with Na₂SO₃ Scrubbing

3.2.1. Investigation on Na₂SO₃ Initial Concentration

The effective reaction of SO_3^{2-} with NO_2 mainly depends on the Na_2SO_3 concentration in wet scrubbing reaction. A total of 0.5% of ascorbic acid was initially added to Na_2SO_3 absorption liquid to enhance the reducibility of the scrubbing process for each test. By fixed discharge power of 15 W, the NO conversion rate and corresponding NO_2 generation under different Na_2SO_3 concentration absorption were investigated. As shown in Figure 3a, the NO conversion rate remained at more than 95% after 120 min, when Na_2SO_3 concentration varied from 0.5% (wt.) to 5%. In addition, the increasing concentration of Na_2SO_3 exhibited a slight improvement in NO conversion. However, Na_2SO_3 concentration had a significant influence on NO_2 generation (Figure 3b). When the Na_2SO_3 concentration was 0.5%, after 45 min, the Na_2SO_3 scrubbing reaction was invalid. The increase in Na_2SO_3 concentration from 1% to 5% led to a longer capable absorption of NO_2 after 120 min. Increasing SO_3^{2-} concentration exhibited a promotion effect on NO_2 absorption efficiency due to the reaction of SO_3^{2-} and HSO_3^{-} with NO_2 molecules [50].

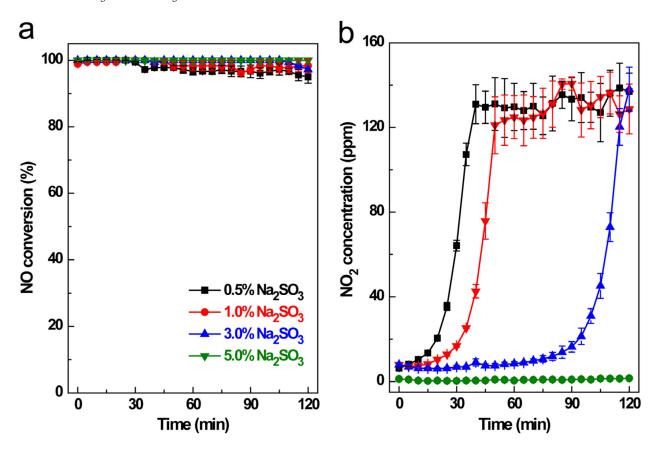


Figure 3. Effects of Na_2SO_3 initial concentration on NO conversion (**a**) and NO_2 generation (**b**) (input plasma power = 15 W, NO inlet concentration = 200 ppm, gas velocity = 500 mL/min, pH = 10).

To further confirm the Na₂SO₃ scrubbing mechanism, the absorption liquid was analyzed using ion chromatography, and the results are shown in Figure 4. It was obvious that SO_4^{2-} , NO_3^- , and NO_2^- were major anions in the absorption liquid. However, the characteristic peak of SO_3^{2-} does not appear in ion chromatography due to the ion chromatographic column (IonPac, AS22) not being able to separate SO_3^{2-} and SO_4^{2-} . With the Na₂SO₃ initial concentration increasing from 0.5% to 5%, the SO_4^{2-} concentration in the absorption liquid

dramatically increased. It can be observed in Figure 3 that SO_3^{2-} was completely consumed by the reaction with NO_2 and O_3 when the Na_2SO_3 initial concentration was less than 3%. When 5% of Na_2SO_3 was introduced, none of the NO_2 concentration was detected in the gas effluent, indicating that the excess of SO_3^{2-} remained in the scrubbing solution. With the increasing Na_2SO_3 concentration, NO_2^- concentration increased. According to Equation (4), the enhancement of SO_3^{2-} in the absorption liquid was favorable for NO_2 conversion to NO_3^- and NO_2^- due to the improving alkalinity and reducibility. However, NO_3^- concentration was relatively constant after different Na_2SO_3 absorption. A total of 1% of Na_2SO_3 was chosen for the following experiment.

$$2NO_2 + H_2O + 2SO_3^{2-} \rightarrow NO_2^{-} + NO_3^{-} + 2HSO_3^{-}$$
(4)

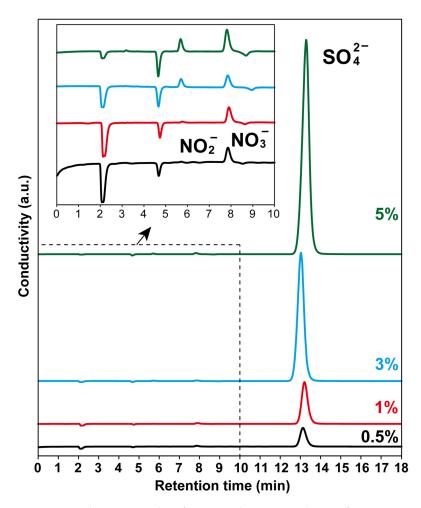


Figure 4. Ion chromatography of Na₂SO₃ absorption solution after 120 min reaction under different Na₂SO₃ concentrations.

3.2.2. Investigation of pH Value

The influence of Na_2SO_3 solution pH value on both NO conversion and NO_2 generation is shown in Figure 5a. Compared to the effects of Na_2SO_3 concentration, pH value had a slight influence on NO conversion but exhibited different affection on NO_2 generation. The enhancing acidity of the Na_2SO_3 solution inhibited NO conversion to some extent. Specifically, NO conversion decreased to 91.3% after 40 min absorption under a pH value of 5. For a pH value of 7, the NO conversion was 100% when absorption started and decreased to 91.5% after 30 min. When the pH value increased to 10 and 12, NO conversion was 100% at 35 min after the reaction and remained at 94.3% and 97.5% after 120 min, respectively.

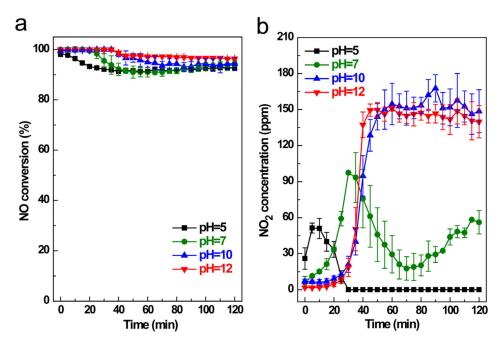


Figure 5. Effects of Na_2SO_3 solution pH value on NO conversion (**a**) and NO_2 generation (**b**). (Input plasma power = 15 W, NO inlet concentration = 200 ppm, gas velocity = 500 mL/min, Na_2SO_3 concentration: 1% wt.).

The influence of Na_2SO_3 solution pH value on NO conversion can be further analyzed by outlet NO_2 concentration. Figure 5b shows that outlet NO_2 concentration fluctuated obviously under different pH values. When the pH value was 5, NO_2 increased to 51.4 ppm and decreased from 10 min. No NO_2 was detected after 35 min of reaction. When the pH value was 7, NO_2 generation increased to 100 ppm after 30 min and then decreased from 30 min to 70 min. In the acid Na_2SO_3 solution, the weak reducibility resulted in a fast SO_3^{2-} consumption by NO_2 . After that, the outlet NO_2 concentration in the first 30 min increased under pH = 5 and pH = 7. In addition, SO_2 was generated after 30 min of reaction, suggesting that by promoting the acidity of Na_2SO_3 absorption, the existing abundant H^+ reacted with SO_3^{2-} facilitated the reaction of $SO_2+NO_2 \rightarrow SO_3+NO$, thus leading to a decrease in NO_2 concentration and NO conversion. When the pH value increased to 10 and 12, obvious NO_2 emission was observed after 30 min absorption, suggesting SO_3^{2-} had been completely consumed, and the outlet NO_2 concentration remained at $140\sim150$ ppm throughout 120 min of reaction.

The absorption liquid under different pH values was also investigated by ion chromatography, as shown in Figure 6. By fixing Na₂SO₃ concentration of 1%, it was apparent that SO_4^{2-} peak intensity was approximate under different pH values. The obvious difference was NO_3^{-} and NO_2^{-} , where the pH value increased from 5 to 12. When the pH value was less than 7, only NO_3^{-} and SO_4^{2-} existed in the scrubbing solution, which indicated the invalidity of SO_3^{2-} after 120 min reaction. With the pH value increased to 10 and 12, obvious NO_2^{-} was detected, indicating that the reducibility of the scrubbing solution can promote the reaction of SO_3^{2-} with NO_2 . The following experiment fixed the Na_2SO_3 solution pH value of 10.

3.2.3. Investigation of NO Velocity

Depending on different sinter conditions, the NO velocity in sinter flue gas may fluctuate due to the gas permeability by air suction in the sinter bed [47]. The influence of gas velocity was also an important parameter that influenced removal efficiency. As shown in Figure 7a, IPC coupling with Na_2SO_3 scrubbing exhibited desirable NOx removal under different NO velocities. When NO velocity increased from 400 mL/min to 1500 mL/min, the NO_2 concentration after IPC coupling Na_2SO_3 scrubbing showed a slight increase

(Figure 7b), and the NOx removal rate showed a declining trend. The NOx removal rate was more than 70% under a velocity of 1500 mL/min, and the corresponding NO_2 concentration was less than 15 ppm. The thorough treatment efficiency of NO under different velocities can be attributed to the effective oxidation capacity of the in-plasma catalytic oxidation of NO molecules.

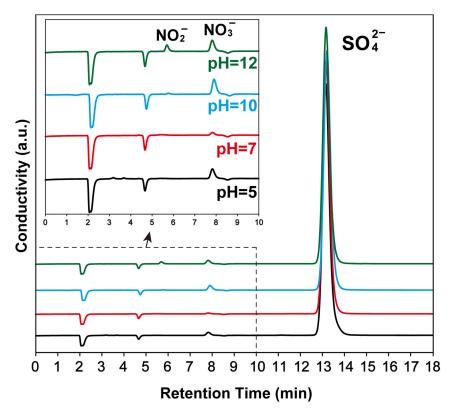


Figure 6. Ion chromatography (IC) of Na_2SO_3 absorption solution after 120 min reaction under different pH values.

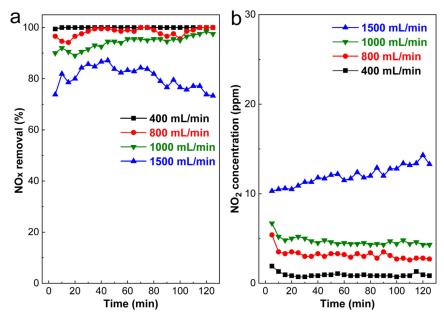


Figure 7. Effects of NO velocity on NOx removal (a) and outlet NO_2 concentration (b) (NO initial concentration = 200 ppm, discharge power = 15 W, $Na_2SO_3 = 1\%$, pH value = 10).

3.2.4. Investigation of NO Initial Concentration

The NO concentration in industrial sinter flue gas is often variable due to the uneven distribution of fossil-fuel nitrogen and incomplete combustion [51]. The different sinter raw mix and ratio also affect NO emission [52]. Herein, the influence of NO initial concentration on NOx removal was investigated, and the results are shown in Figure 8. The outlet NO_2 concentration after IPC coupled Na_2SO_3 absorption kept less than 35 ppm when NO initial concentration was 100 to 600 ppm. The inlet NO concentration had an obvious influence on NOx removal efficiency. NOx removal decreased with the increase in NO inlet concentration. When NO inlet concentration was 100 ppm, 300 ppm, 450 ppm, and 600 ppm, the corresponding NOx removal efficiencies after 120 min reaction were 100%, 44.5%, 23%, and 4%, respectively. The inlet NO concentration determined the NO molecules amount throughout the plasma region per unit of time. Under the same discharge power, the reactive oxygen species $(O_3, \cdot OH, \cdot O, \text{ etc.})$ were consistent. After that, more NO molecules may not be effectively oxidized to NO_2 with the increase in NO concentration, which resulted in an obvious decrease in NOx removal efficiency.

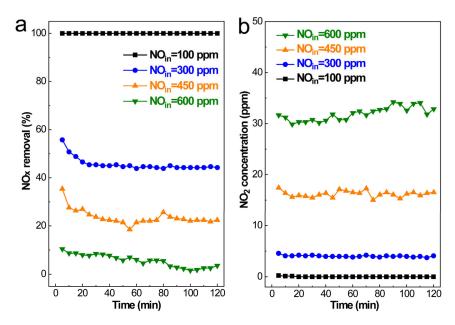


Figure 8. Influence of NO initial concentration on NOx removal (a) and outlet NO₂ concentration (b) (NO velocity = 200 mL/min, discharge power = 15 W, Na₂SO₃ = 1%, pH value = 10).

It can be observed from Figure 8b that the outlet NO_2 concentration after treatment of IPC coupling with Na_2SO_3 absorption can be effectively reduced, which is less than 35 ppm when inlet NO concentration varies from 100 to 600 ppm. In conclusion, NO concentration showed a greater influence than that of NO velocity.

3.3. Co-Elimination of NO and VOCs after IPC Combined with Na₂SO₃ Wet Scrubbing 3.3.1. Removal of NO

First, the sinter raw mix was heated to 400, 450, and 500 $^{\circ}$ C in the tubular furnace using air as a carrier gas, thus providing simulated sinter flue gas with different NO inlet concentrations. It should be noted that under fixed calcination temperature, the simulating sinter flue gas NO concentration was not stable due to fuel-N combustion. As shown in Figure 9a, under calcination temperatures of 400, 450, and 500 $^{\circ}$ C, the corresponding maximum NO concentrations were 120 ppm, 304 ppm, and 450 ppm. When the sinter temperature was 400 $^{\circ}$ C, the NO produced by the sinter raw mix followed an increasing trend for 20 min and then kept steady until 120 min. Meanwhile, no NO was observed in the outlet after IPC and Na₂SO₃ scrubbing, indicating that NO inlet within 120 ppm can be effectively eliminated. When the sintering temperature increased to 450 and 500 $^{\circ}$ C, the NO

concentration generated by fuel-N combustion fluctuated, showing an increasing trend, followed by a decrease after 30 min. We further calculated the NO removal efficiency corresponding to NO inlet concentration varying from 100 ppm to 450 ppm (Figure 9b). When the NO inlet concentration was less than 200 ppm, the NO removal rate was more than 80%. In addition, the NO removal rate decreased to 60% when the NO inlet concentration was 450 ppm. The above results indicated that high NO concentration has a suppressive influence on the NO removal rate, while IPC coupled with Na₂SO₃ scrubbing for practical NO treatment showed a wide application range of different NO concentrations.

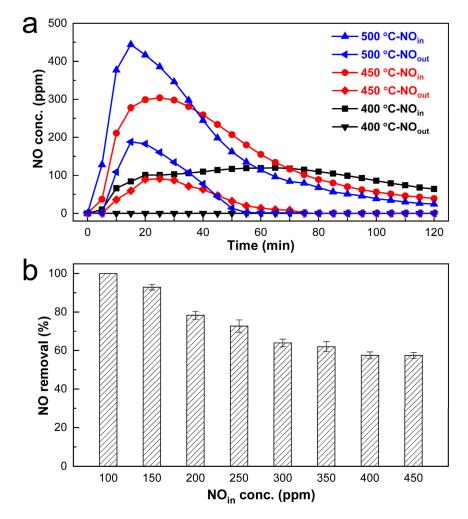


Figure 9. NO removal by IPC coupled Na₂SO₃ absorption (under different sinter time and sinter temperature (a); under different NO inlet concentrations (b)).

3.3.2. Removal of VOCs

VOCs can be produced simultaneously by the heating of sinter raw mix in a fixed airflow. TVOC emission showed a similar trend, with NO concentration under different sinter temperatures, as shown in Figure 10a. With the increasing sinter temperature, the TVOC emission showed an obvious enhancement from 400 °C to 450 °C. The maximum TVOC was 14.9 ppm, 58.6 ppm, and 82.2 ppm, corresponding to sinter temperatures of 400, 450, and 500 °C. The TVOC removal efficiency was calculated by TVOC $_{\rm in}$ and TVOC $_{\rm out}$ using a PID detector. IPC coupling with Na $_2$ SO $_3$ wet scrubbing showed remarkable performance for sinter flue gas VOC elimination under different sinter temperatures (Figure S4 in the Supplementary Materials). The TVOC removal efficiency appeared to have a slight descending trend when TVOC initial concentration varied from 20 to 80 ppm (Figure 10b), with 99% at 20 ppm and 85.7% at 80 ppm. Na $_2$ SO $_3$ wet scrubbing can effectively absorb the excess O $_3$ and dissolved organic molecules produced by the plasma catalytic reaction.

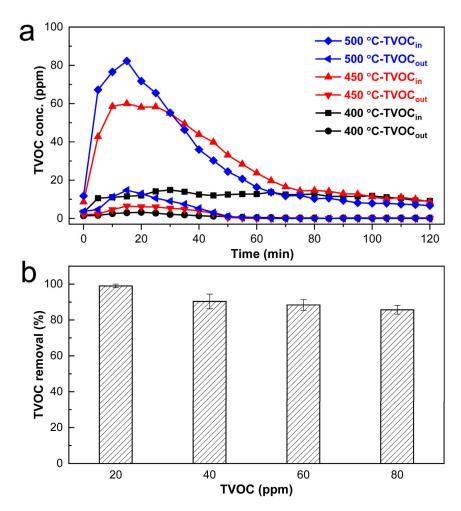


Figure 10. TVOC removal by IPC coupling with Na₂SO₃ scrubbing: under different sinter times and sinter temperatures (**a**); under different VOCs inlet concentration (**b**).

To investigate the VOC removal efficiency by the coupling system, we further conducted TG-GC-MS analysis. The simulated sinter flue gas VOC components were collected and concentrated using a TD100xr sorbent tube under 450 °C and a flow rate of 50 mL/min for 30 min and then analyzed by TG-GC-MS analysis. As shown in Figure 11, the detected VOC components before treatment comprised more than 50 species, of which BTEX was the dominant component. The results were in accordance with our previous research [22]. Distinctive VOC reduction was observed after the IPC with $\rm Na_2SO_3$ scrubbing treatment, suggesting the satisfactory removal efficiency of VOCs, which can also be proved by Figure 10b with TVOC removal > 88% under 450 °C. The detected VOCs were only methylcyclohexane, toluene, p-Xylene, propylbenzene, 1,4-dichloro-benzene, and benzaldehyde, with an obvious decreasing chromatographic peak intensity, respectively. However, the increasing peak intensity of benzene indicated that benzene was the major degradation byproduct. The VOC removal results indicated that IPC with $\rm Na_2SO_3$ scrubbing removes the features of flue gas with NO and VOC components and large gas flux.

3.4. Role of Na₂SO₃ Scrubbing

To investigate the NOx conversion route and elimination mechanism via IPC combined with the sequential Na_2SO_3 scrubbing treatment, we analyzed different absorption solutions after 30 min of IPC reaction using ion chromatography (IC-883, Metrohm). Before analysis, simulated sinter flue gas was obtained by mixing 300 ppm SO_2 with sinter flue gas produced by 450 °C heating of sinter raw mix in a tubular furnace. As shown in Figure 12, the major anions by pure water absorption for IPC pre-oxidation of simulating sinter flue

gas were SO_3^{2-} , SO_4^{2-} , and F^{-1} . They can be attributed to SO_2 and fluoride dissolution and further oxidation by reactive oxidation species generated by plasma catalysis. The NO_3^- peak after water absorption can be clearly observed when the simulated sinter flue gas was treated via an in-plasma catalytic region, indicating the efficient oxidation of NO to NO_2 . When using 1% Na_2SO_3 as a scrubber, only SO_3^{2-} and SO_4^{2-} were observed in the absorption liquid. In addition, the peak intensity of SO_4^{2-} was obviously higher than that of SO_3^{2-} due to the excess ozone oxidation, which was generated by plasma. It should be noted that the absorption liquid of 1% Na_2SO_3 was diluted 100-fold compared to that of water as a scrubber.

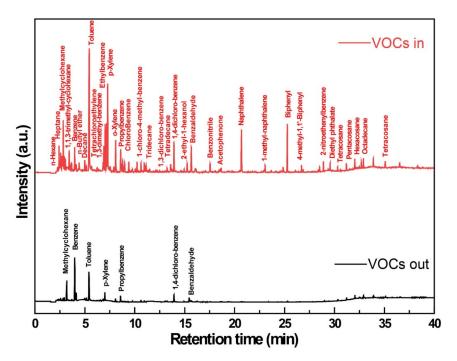


Figure 11. TG-GC-MS characterization of sinter flue gas VOC components before and after IPC coupled Na₂SO₃ scrubbing.

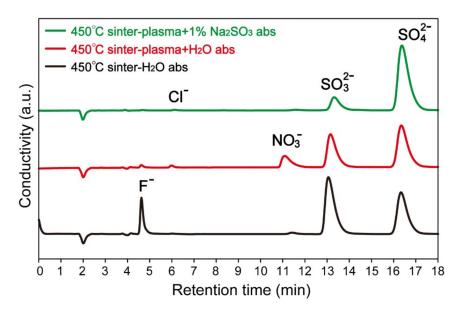


Figure 12. Ion chromatography of sinter flue gas different absorption solutions before and after IPC treatment.

4. Conclusions

The enormous and complex air-pollutant emissions from the iron and steel industry place a huge burden on China's regional atmospheric environment. The integration of in-plasma catalysis with sequential Na₂SO₃ treatment can be effective for the co-elimination of sinter flue gas multi-components. The plasma discharge status was optimized by investigating NO conversion. The VOC and NO removal performance of the integrated system was further investigated by taking simulated sinter flue gas as model pollutants. NO removal rate was more than 80% when the initial concentration was less than 200 ppm. In addition, 88% of the TVOC removal rate can be realized when the TVOC concentration is no more than 80 ppm. The findings indicate that plasma catalysis integrates with Na₂SO₃ scrubbing for a collaborative effect in the co-elimination of sinter flue gas multi-compound emissions. The future investigation of the proposed technology should consider the nitrogen compound balance and the evaluation of practical sinter flue gas. The development of a plasma catalyst and the optimization of DBD reactor geometry can also promote the application of the combining system.

Supplementary Materials: The following supporting information can be downloaded at https: //www.mdpi.com/article/10.3390/pr11102916/s1, Figure S1: DBD reactor with wedged high-voltage electrode: figure illustration (a) and photograph (b); Figure S2: Schematic diagram of experimental setup for plasma status detection; Figure S3: Output voltage signals of plasma discharge (a) and Lissajous figure (b) at 15 kV, 7.5 kHz; Figure S4: Comparison of different treatment processes on sinter flue gas TVOC removal; Table S1: Specific input energy (SIE) with different input power and peak voltage. Text S1: Description of DBD reactor; Text S2: Detailed plasma status detection; Text S3: Discharge power calculation. Text S4: Investigation on different treatment process on sinter flue gas TVOC removal.

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