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# Spectra of Ionized Atoms: From Laboratory to Space

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Edited by  
Joseph Reader

Printed Edition of the Special Issue Published in *Atoms*

# **Spectra of Ionized Atoms: From Laboratory to Space**

Special Issue Editor  
**Joseph Reader**

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Basel, Switzerland

This edition is a reprint of the Special Issue published online in the open access journal *Atoms* (ISSN 2218-2004) from 2016–2017 (available at: [http://www.mdpi.com/journal/atoms/special\\_issues/laboratory\\_space](http://www.mdpi.com/journal/atoms/special_issues/laboratory_space)).

For citation purposes, cite each article independently as indicated on the article page online and as indicated below:

Lastname, F.M.; Lastname, F.M. Article title. <i>Journal Name</i> <b>Year</b> , Article number, page range.
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**First Edition 2018**

**ISBN 978-3-03842-869-5 (Pbk)**

**ISBN 978-3-03842-870-1 (PDF)**

Central portion of the image of the Crab Nebula taken by the Hubble Space Telescope (HST). The Crab Nebula is among the most interesting and well-studied objects in astronomy. The image on the cover was assembled from 24 individual exposures taken with the Wide Field and Planetary Camera 2 (WFPC2). It is the largest image ever taken with WFPC2. WFPC2 was built by the Jet Propulsion Laboratory in Pasadena, California. It was installed on Hubble in 1993 and removed during the servicing mission in 2009. WFPC2 is currently on display at the National Air and Space Museum in Washington, DC.

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## About the Special Issue Editor

**Joseph Reader** is Scientist Emeritus at the National Institute of Standards and Technology (NIST) in Gaithersburg, Maryland, U.S.A. After receiving his Ph.D. from the University of California, Berkeley in 1962 and serving as Postdoctoral Research Associate at the Argonne National Laboratory, in 1963 he joined the staff at NIST. During his years at NIST he has specialized in the observation and interpretation of spectra of highly ionized atoms and the design of optical spectrometers. His measurements of the spectra of neutral and singly ionized platinum have served to calibrate wavelengths of spectra observed with the Hubble Space Telescope. He is a Fellow of the American Physical Society and the Optical Society, and has received the William F. Meggers Award of the Optical Society of America. Before retiring from NIST in 2014, he directed the NIST Atomic Spectroscopy Data Center.



Article

# Spectrum and Energy Levels of Four-Times Ionized Yttrium (Y V)

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Academic Editor: James Babb

Received: 18 November 2016; Accepted: 6 December 2016; Published: 21 December 2016

**Abstract:** The analysis of the spectrum of four-times-ionized yttrium, Y V, was extended to provide a large number of new spectrum lines and energy levels. The new analysis is based on spectrograms made with sliding-spark discharges on 10.7 m normal- and grazing-incidence spectrographs. The measurements cover the region 184–2549 Å. The results revise levels for this spectrum by Zahid-Ali et al. (1975) and by Ateqad et al. (1984). Five hundred and seventy lines were classified as transitions between 23 odd-parity and 90 even-parity levels. The  $4s^2 4p^5$ ,  $4s 4p^6$ ,  $4s^2 4p^4 4d$ ,  $5s$ ,  $5p$ ,  $5d$ ,  $6s$  configurations are now complete. Results for the  $4s^2 4p^4 6d$  and  $7s$  configurations are tentative. Ritz-type wavelengths were determined from the optimized energy levels, with uncertainties as low as  $\pm 0.0004$  Å. The observed configurations were interpreted with Hartree-Fock calculations and least-squares fits of the energy parameters to the observed levels. Oscillator strengths for all classified lines were calculated with the fitted parameters. The results are compared with values for the level energies, percentage compositions, and transition probabilities from recent ab initio theoretical calculations. The ionization energy was revised to  $607,760 \pm 300$  cm<sup>-1</sup> ( $75.353 \pm 0.037$  eV).

**Keywords:** yttrium; ionic spectrum; vacuum ultraviolet; wavelengths; energy levels; transition probabilities; parametric calculations; ionization energy

## 1. Introduction

The four-times ionized yttrium atom, Y V, has a Br-like electronic structure with ground configuration  $4s^2 4p^5$  and excited states  $4s 4p^6$  and  $4s^2 4p^4 nl$ . The spectrum has a somewhat checkered past. It was first analyzed in 1939 by Paul and Rense [1], who, from a set of transitions to the  $4s^2 4p^5$   $^2P$  ground term, determined levels of the  $4s 4p^6$   $^2S_{1/2}$ ,  $4s^2 4p^4 4d$ , and  $4s^2 4p^4 5s$  configurations. Unfortunately, an isoelectronic plot published by Edlén [2] in 1964 showed that the  $4s^2 4p^5$   $^2P_{3/2}$ - $^2P_{1/2}$  interval of Paul and Rense [1] ( $12,068$  cm<sup>-1</sup>) was inconsistent with the known intervals for the rest of the isoelectronic sequence. From his plot, Edlén predicted an interval of  $12,470 \pm 20$  cm<sup>-1</sup>. Since essentially all of their levels were based on transitions to the  $4s^2 4p^5$   $^2P$  term, Edlén concluded that the analysis would have to be completely revised. A start on this revision came in 1970, when Reader and Epstein [3] observed the true  $4s^2 4p^5$   $^2P_{1/2,3/2}$ - $4s 4p^6$   $^2S_{1/2}$  transitions, thus obtaining the position of  $4s 4p^6$   $^2S_{1/2}$  and a revised value for the  $^2P$  term splitting. Their splitting of  $12,459.9 \pm 3.0$  cm<sup>-1</sup> was indeed close to the value predicted by Edlén. In 1972 Reader and Epstein [4] observed further transitions to the  $4s^2 4p^5$   $^2P$  ground term and established nearly all levels of the  $4s^2 4p^4 4d$  and  $5s$  configurations. Only the levels of  $4p^4 4d$  with  $J = 7/2$  and  $9/2$ , which do not combine with  $4p^5$   $^2P_{1/2,3/2}$ , and the  $4p^4 4d$  ( $^3P$ ) $^4D_{1/2}$  level could not be located.

In 1975, Zahid-Ali et al. [5] observed the spectrum at lower wavelengths and reported levels of the  $4s^2 4p^4 5d$ ,  $6s$ ,  $6d$ , and  $7s$  configurations. Since all lines terminated on the  $4s^2 4p^5$   $^2P$  term, again only levels with  $J = 1/2$ ,  $3/2$ , and  $5/2$  could be found. Finally, in 1984 Ateqad and Chaghtai [6] reported



levels of the  $4s^24p^44f$  and  $5p$  configurations. From transitions to these new configurations they were able to report levels of  $4s^24p^44d$  and  $5d$  having  $J = 7/2$  and  $9/2$ .

In the present work we observed the spectrum of Y V in the ultraviolet and determined a new set of energy levels. About half the  $4s^24p^45d$  levels of [5] were found to be spurious. Several of the  $4s^24p^46s$  levels in this paper had incorrect  $J$ -values and in fact belong to  $4s^24p^45d$ . Nearly all of the  $4s^24p^45p$  levels of [6] were spurious, as were all of the reported  $J = 7/2, 9/2$  levels of  $4s^24p^44d$  and  $5d$ .

## 2. Experiment

The observations were the same as used for earlier work in our laboratory on yttrium [4,7,8]. Briefly, the light source was a low-voltage sliding-spark with metallic yttrium electrodes. The source was operated as described by Reader et al. [9]. From 500 to 2549 Å we used the NIST 10.7-m normal-incidence vacuum spectrograph; from 184 to 500 Å we used the NIST 10.7-m grazing-incidence spectrograph. Both instruments had gratings with 1200 lines/mm. The plate factor for the normal-incidence spectrograph was about 0.78 Å/mm. The plate factor for the grazing-incidence spectrograph at 350 Å was 0.25 Å/mm. From 600 to 2549 Å the spectra were calibrated by spectra of Cu II excited in a hollow cathode discharge. Below 600 Å calibration was obtained from lines of Y in various stages of ionization. Shifts between the reference spectra and the yttrium spectra were removed by use of impurity lines of oxygen, nitrogen, carbon, and silicon. Complete references for the calibration spectra are given in Reference [8].

Ionization stages were distinguished by comparing the intensities of the lines at various peak currents in the spark. The spectra of Y V were relatively enhanced at a peak current of about 2000 A.

The wavelengths, intensities, and classifications of the observed lines of Y V are given in Table 1. All wavelengths are in vacuum. The intensities are estimates of photographic plate blackening. The intensities range from 1 to 5,000,000. The system used to obtain this extensive scale of intensities is described in a recent paper on Mo VI [10]. No attempt was made to account for spectrograph or plate emulsion response. The strongest lines in the spectrum appear as a group of  $4p^45p-5d$  transitions around 1350 Å.

The general uncertainty of the wavelengths is  $\pm 0.007$  Å. Hazy lines (h) were given an uncertainty of  $\pm 0.010$  Å; perturbed (p), complex (c), or asymmetric lines (s, l) an uncertainty of  $\pm 0.020$  Å; unresolved (u) or doubly classified (dc) lines an uncertainty of  $\pm 0.030$  Å. All uncertainties are reported at the level of one standard deviation.

**Table 1.** Observed spectral lines of Y V. Wavelengths and wave numbers are in vacuum. Wavelength values in parentheses are Ritz values. General uncertainty of the observed wavelengths is  $\pm 0.007$  Å. Uncertainties for less certain wavelengths are given in Section 2 of the text. |CFI| is the cancellation factor (see text). Unc (Å) is the uncertainty of the Ritz wavelength.

$\lambda_{\text{obs}}$ (Å)	Int <sup>a</sup>	$\sigma_{\text{obs}}$ (cm <sup>-1</sup> )	Even Level <sup>b</sup>	Odd Level <sup>b</sup>	$\lambda_{\text{Ritz}}$ (Å)	Unc (Å)	$g_{\text{U}}/A$ (s <sup>-1</sup> )	$\log(g_{\text{L}}/f)$	CFI
184.144	1	543053	6d83	p5 3	184.1443	0.0049	1.13E+08	-3.25	0.05
187.849	25	532342	7s31	p5 1	187.8490	0.0070	1.99E+09	-1.99	0.69
188.469	3	530591	6d83	p5 1	188.4687	0.0051	3.71E+09	-1.71	0.75
191.571	50	522000	7s25	p5 3	191.5710	0.0070	7.75E+09	-1.38	0.69
193.843	3	515881	6d51	p5 3	193.8426	0.0049	2.45E+08	-2.87	0.40
193.888	3	515762	6d65	p5 3	193.8880	0.0070	2.19E+09	-1.91	0.40
194.165	10	515026	6d73	p5 3	194.1705	0.0061	2.59E+09	-1.84	0.61
194.457	10	514253	6d41	p5 3	194.4567	0.0048	4.97E+09	-1.56	0.54
196.148	30	509819	7s21	p5 3	196.1490	0.0049	4.20E+09	-1.62	0.75
196.206	25	509668	7s33	p5 1	196.2060	0.0070	5.65E+09	-1.49	0.66
196.444	40	509051	7s23	p5 3	196.4440	0.0070	3.06E+09	-1.76	0.75
198.495	3	503791	6d53	p5 3	198.4961	0.0049	1.30E+09	-2.12	0.07
198.640	20	503423	6d51	p5 1	198.6404	0.0051	1.42E+10	-1.08	0.65
198.753	60	503137	6d55	p5 3	198.7530	0.0070	4.59E+09	-1.57	0.50
198.990	3	502538	6d73	p5 1	198.9847	0.0064	9.56E+09	-1.25	0.65
199.285	3	501794	6d41	p5 1	199.2853	0.0051	1.89E+09	-1.96	0.48
199.461	2	501351	6d43	p5 3	199.4610	0.0300	1.47E+09	-2.07	0.26
200.392	80	499022	7s13	p5 3	200.3926	0.0049	1.25E+10	-1.13	0.74
200.694	1	498271	7s15	p5 3	200.6940	0.0300	4.57E+08	-2.57	0.60
201.064	30	497354	7s21	p5 1	201.0631	0.0051	5.12E+09	-1.51	0.57
202.784	30	493136	6d23	p5 3	202.7798	0.0065	1.76E+10	-0.97	0.66
202.792	40	493116	6d25	p5 3	202.7920	0.0200	9.35E+09	-1.25	0.64
203.531	10	491326	6d53	p5 1	203.5300	0.0052	9.88E+09	-1.22	0.53
205.525	1	486559	7s13	p5 1	205.5244	0.0051	9.84E+08	-2.21	0.18
205.731	10	486072	6s31	p5 3	205.7327	0.0004	1.48E+09	-2.03	0.14
208.036	2	480686	6d23	p5 1	208.0362	0.0069	1.25E+09	-2.10	0.08
211.144	20	473610	6s31	p5 1	211.1453	0.0005	3.52E+09	-1.63	0.50
212.318	20	470992	5d85	p5 3	212.3188	0.0004	3.67E+09	-1.61	0.30
217.564	100	459635	6s25	p5 3	217.5632	0.0005	1.36E+10	-1.02	0.55
217.853	80	459025	5d83	p5 1	217.8535	0.0005	1.23E+10	-1.06	0.54
222.825	30	448783	6s21	p5 3	222.8289	0.0005	5.90E+08	-2.36	0.02
223.032	70	448366	5d73	p5 3	223.0363	0.0004	5.03E+09	-1.43	0.23

Table 1. Cont.

$\lambda_{\text{obs}}$ (Å)	Int <sup>a</sup>	$\sigma_{\text{obs}}$ (cm <sup>-1</sup> )	Even Level <sup>b</sup>	Odd Level <sup>b</sup>	$\lambda_{\text{Ritz}}$ (Å)	Unc (Å)	$g_{UL}A$ (s <sup>-1</sup> )	$\log(g_{UL}f)$	CFI
223.561	90	447305	6s33	p5 1	223.5630	0.0005	1.04E+10	-1.11	0.54
223.569	80	447289	5d51	p5 3	223.5749	0.0004	8.34E+09	-1.20	0.19
223.857	200	446714	6s23	p5 3	223.8547	0.0005	2.27E+09	-1.77	0.12
223.857	200	446714	5d75	p5 3	223.8594	0.0004	2.66E+10	-0.70	0.50
224.107	2	446215	6s11	p5 3	224.1101	0.0005	4.26E+06	-4.49	0.00
224.566	100	445303	5d65	p5 3	224.5678	0.0004	8.77E+09	-1.18	0.34
224.726	150	444986	5d63	p5 3	224.7272	0.0004	2.93E+10	-0.65	0.48
225.159	100	444131	5d41	p5 3	225.1599	0.0004	1.22E+10	-1.03	0.27
228.743	200	437172	6s13	p5 3	228.7434	0.0005	2.18E+10	-0.77	0.56
229.191	3	436317	6s21	p5 1	229.1924	0.0006	8.65E+07	-3.17	0.00
229.411	100	435899	5d73	p5 1	229.4118	0.0006	3.44E+10	-0.57	0.47
229.530	20	435673	6s15	p5 3	229.5312	0.0005	1.52E+08	-2.92	0.03
229.845	70	435076	5d53	p5 3	229.8474	0.0005	4.58E+09	-1.44	0.07
229.981	100	434819	5d51	p5 1	229.9816	0.0006	2.83E+10	-0.65	0.49
230.071	150	434648	5d55	p5 3	230.0718	0.0005	4.05E+10	-0.49	0.44
230.277	2	434260	6s23	p5 1	230.2778	0.0006	2.09E+08	-2.78	0.04
231.120	20	432676	5d45	p5 3	231.1214	0.0005	9.45E+08	-2.12	0.27
231.201	50	432524	5d63	p5 1	231.2011	0.0006	7.06E+09	-1.25	0.37
231.659	20	431669	5d41	p5 1	231.6592	0.0006	4.99E+08	-2.40	0.02
231.784	70	431436	5d43	p5 3	231.7843	0.0005	5.06E+09	-1.39	0.27
232.269	20	430535	5d35	p5 3	232.2697	0.0005	1.04E+09	-2.08	0.14
232.370	20	430348	5d33	p5 3	232.3723	0.0005	7.48E+08	-2.22	0.33
232.800	20	429553	5d31	p5 3	232.8009	0.0005	7.21E+08	-2.23	0.15
235.250	200	425080	5d25	p5 3	235.2511	0.0005	3.08E+10	-0.59	0.49
235.386	150	424834	5d23	p5 3	235.3880	0.0005	1.72E+10	-0.84	0.46
235.452	25	424715	6s13	p5 1	235.4543	0.0006	8.34E+08	-2.16	0.07
236.208	70	423356	5d21	p5 3	236.2106	0.0005	3.24E+09	-1.57	0.25
236.623	80	422613	5d53	p5 1	236.6241	0.0006	1.21E+10	-1.00	0.24
238.675	50	418980	5d43	p5 1	238.6775	0.0006	2.96E+09	-1.60	0.10
238.711	10	418917	5d13	p5 3	238.7123	0.0005	7.10E+07	-3.22	0.02
239.298	2	417889	5d33	p5 1	239.3010	0.0006	2.49E+08	-2.67	0.13
239.754	10	417094	5d31	p5 1	239.7555	0.0006	7.80E+08	-2.17	0.10
242.501	60	412369	5d23	p5 1	242.5005	0.0006	2.55E+09	-1.65	0.05
243.375	3	410889	5d21	p5 1	243.3736	0.0006	4.26E+08	-2.42	0.03
245.389	5	407516	5d11	p5 1	245.3885	0.0006	1.81E+08	-2.79	0.04

Table 1. Cont.

$\lambda_{\text{obs}}$ (Å)	Int <sup>a</sup>	H, x A, x	$\sigma_{\text{obs}}$ (cm <sup>-1</sup> )	Even Level <sup>b</sup>	Odd Level <sup>b</sup>	$\lambda_{\text{Ritz}}$ (Å)	Unc (Å)	$g_{UL}A$ (s <sup>-1</sup> )	$\log(g_{UL}f)$	CFI
289.182	90	H, x	345803	5s31	p5 3	289.1826	0.0008	1.16E+09	-1.84	0.03
(299.992)		A, x	333334	5s31	p5 1	299.9920	0.0010	7.43E+09	-1.00	0.28
312.888	50		319603.2	5s33	p5 3	312.8874	0.0008	2.02E+09	-1.53	0.04
313.349	1000		319133.0	5s25	p5 3	313.3494	0.0008	3.24E+10	-0.32	0.42
320.467	500		312044.6	4d83	p5 3	320.4676	0.0009	9.44E+09	-0.84	0.03
321.691	700		310857.3	5s21	p5 3	321.6905	0.0009	1.57E+10	-0.61	0.42
325.580	2000		307144.2	5s33	p5 1	325.5805	0.0011	1.23E+10	-0.71	0.15
326.567	3000		306215.9	5s23	p5 3	326.5675	0.0009	4.03E+10	-0.19	0.83
(328.337)		A, x	304566.1	5s11	p5 3	328.3372	0.0009	1.06E+08	-2.77	0.00
330.398	300		302665.3	4d51	p5 3	330.3989	0.0009	1.06E+10	-0.76	0.05
333.084	10000		300224.6	4d85	p5 3	333.0844	0.0010	7.88E+11	1.12	0.82
333.796	5000		299584.2	4d83	p5 1	333.7963	0.0012	5.17E+11	0.94	0.83
335.125	200		298396.1	5s21	p5 1	335.1232	0.0012	3.32E+10	-0.25	0.68
335.143	800		298380.1	5s13	p5 3	335.1445	0.0010	1.33E+10	-0.65	0.13
336.621	5000		297070.0	4d73	p5 3	336.6197	0.0010	4.71E+11	0.91	0.88
339.023	3000		294965.2	4d41	p5 3	339.0225	0.0010	2.34E+11	0.61	0.71
340.016	1000		294103.8	5s15	p5 3	340.0176	0.0010	7.67E+09	-0.88	0.92
340.419	75		293755.6	5s23	p5 1	340.4194	0.0012	1.61E+09	-1.55	0.11
342.342	50		292105.6	5s11	p5 1	342.3429	0.0012	5.06E+09	-1.05	0.32
344.583	2000		290205.8	4d51	p5 1	344.5848	0.0013	1.97E+11	0.55	0.82
349.648	800		286001.9	4d75	p5 3	349.6483	0.0011	9.34E+08	-1.77	0.00
349.752	300		285916.9	5s13	p5 1	349.7498	0.0013	4.20E+08	-2.11	0.01
351.355	800		284612.4	4d73	p5 1	351.3567	0.0013	3.58E+09	-1.18	0.02
353.976	1500		282505.0	4d41	p5 1	353.9753	0.0013	1.12E+10	-0.68	0.05
355.564	1500		281243.3	4d63	p5 3	355.5625	0.0011	9.16E+09	-0.76	0.09
372.047	4000		268783.2	4d63	p5 1	372.0454	0.0015	1.22E+10	-0.60	0.06
379.963	1000		263183.5	4d65	p5 3	379.9623	0.0013	2.40E+09	-1.29	0.14
397.767	1000		251403.5	4d55	p5 3	397.7663	0.0015	6.86E+08	-1.79	0.01
403.452	1500		247861.0	4d45	p5 3	403.4517	0.0015	2.13E+09	-1.28	0.01
408.806	10		244614.8	4d53	p5 3	408.8086	0.0015	1.31E+08	-2.49	0.00
409.312	1500		244312.4	4d35	p5 3	409.3134	0.0015	1.28E+09	-1.49	0.02
415.027	1500		240948.2	4d43	p5 3	415.0250	0.0016	1.22E+09	-1.50	0.01
418.179	600		239132.0	4d33	p5 3	418.1776	0.0016	1.66E+09	-1.36	0.02
418.591	1800		238896.7	4d31	p5 3	418.5882	0.0017	1.12E+09	-1.53	0.14
419.792	400		238213.2	4d23	p5 3	419.7887	0.0016	3.12E+08	-2.08	0.01
420.737	1500		237678.2	4d25	p5 3	420.7379	0.0017	8.42E+08	-1.65	0.74

Table 1. Cont.

$\lambda_{\text{obs}}$ (Å)	Int <sup>a</sup>	$\sigma_{\text{obs}}$ (cm <sup>-1</sup> )	Even Level <sup>b</sup>	Odd Level <sup>b</sup>	$\lambda_{\text{Ritz}}$ (Å)	Unc (Å)	$g_{\text{U}^A}$ (s <sup>-1</sup> )	$\log(g_{\text{U}^A})$	CFI
427.875	40	233713.1	4d21	p5 3	427.8764	0.0017	1.41E+07	-3.42	0.00
430.753	500	232151.6	4d53	p5 1	430.7502	0.0020	7.11E+07	-2.71	0.00
437.661	500	228487.3	4d43	p5 1	437.6574	0.0021	1.30E+09	-1.43	0.01
441.161	2	226674.6	4d33	p5 1	441.1647	0.0021	1.65E+07	-3.32	0.00
441.622	25	226438.0	4d31	p5 1	441.6217	0.0022	7.60E+07	-2.65	0.01
442.947	300	225760.6	4d23	p5 1	442.9581	0.0022	3.74E+07	-2.96	0.00
451.974	25	221251.7	4d21	p5 1	451.9728	0.0023	9.54E+07	-2.54	0.00
452.911	5	220793.9	4d11	p5 3	452.9095	0.0024	1.26E+07	-3.41	0.00
455.846	35	219372.3	4d13	p5 3	455.8429	0.0020	2.74E+07	-3.07	0.00
(457.838)		218417.9	4d15	p5 3	457.8395	0.0021	4.23E+07	-2.88	0.00
479.994	1	208335.9	4d11	p5 1	479.9972	0.0030	9.83E+06	-3.47	0.00
481.827	20	207543.4	4p61	5p51	481.8281	0.0022	6.46E+08	-1.65	0.21
491.807	5	203331.8	4p61	5p73	491.8074	0.0023	1.69E+08	-2.21	0.21
498.642	90	200544.7	4p61	5p63	498.6395	0.0024	1.15E+09	-1.37	0.26
550.483	1	181658.7	4p61	5p21	550.4803	0.0029	6.84E+07	-2.51	0.10
573.075	2	174497.2	4p61	5p11	573.0754	0.0031	1.02E+08	-2.30	0.16
584.982	50000	170945.4	4p61	p5 3	584.9815	0.0044	1.66E+09	-1.07	0.03
585.101	5	170910.7	4p61	5p13	585.0990	0.0033	1.09E+08	-2.25	0.19
630.973	30000	158485.4	4p61	p5 1	630.9727	0.0056	7.94E+08	-1.33	0.04
690.718	25	144776.9	4d21	5p51	690.7217	0.0018	7.67E+07	-2.26	0.02
693.434	20	144209.8	6s31	5p13	693.4292	0.0028	2.73E+06	-3.71	0.00
702.063	30	142437.4	4d15	5p53	702.0699	0.0026	6.24E+07	-2.34	0.02
706.816	25	141479.5	4d13	5p53	706.8173	0.0023	5.71E+07	-2.37	0.02
709.527	75	140939.0	4d27	5p55	709.5328	0.0024	1.28E+08	-2.02	0.07
709.676	75	140909.4	4d15	5p43	709.6772	0.0026	3.91E+08	-1.53	0.06
711.410	70	140565.9	4d21	5p73	711.4154	0.0019	4.61E+08	-1.45	0.18
713.977	4	140060.5	4d11	5p53	713.9878	0.0040	3.35E+07	-2.59	0.04
714.521	5	139953.9	4d13	5p43	714.5284	0.0023	2.89E+07	-2.66	0.01
715.114	5	139837.8	4d11	5p41	715.1005	0.0040	3.00E+06	-3.64	0.00
717.580	8	139357.3	4d33	5p51	717.5885	0.0016	2.71E+07	-2.68	0.02
721.365	150	138626.1	4d15	5p35	721.3673	0.0027	3.19E+08	-1.60	0.04
722.091	500	138486.7	4d17	5p35	722.0949	0.0034	1.06E+09	-1.08	0.08
726.376	50	137669.7	4d13	5p35	726.3802	0.0024	1.72E+08	-1.87	0.07
731.760	30	136656.8	4d15	5p33	731.7646	0.0028	9.51E+07	-2.12	0.02
732.991	75	136427.3	4d23	5p55	732.9955	0.0021	1.97E+07	-2.80	0.02
734.949	40	136063.9	4d23	5p73	734.9584	0.0021	2.81E+08	-1.65	0.12

Table 1. Cont.

$\lambda_{\text{obs}}$ (Å)	Int <sup>a</sup>	$\sigma_{\text{obs}}$ (cm <sup>-1</sup> )	Even Level <sup>b</sup>	Odd Level <sup>b</sup>	$\lambda_{\text{Ritz}}$ (Å)	Unc (Å)	$g_{U/A}$ (s <sup>-1</sup> )	$\log(g_{U/f})$	CFI
736.921	125	135699.8	4d13	5p33	736.9236	0.0025	3.78E+08	-1.51	0.10
737.953	100	135510.0	4d33	5p55	737.9597	0.0018	3.79E+08	-1.51	0.24
738.669	250	135378.6	4d31	5p73	738.6674	0.0022	8.80E+07	-2.14	0.17
738.669	250	135378.6	4d13	5p31	738.6715	0.0025	6.41E+08	-1.28	0.14
739.566	15	135214.4	4d27	5p27	739.5717	0.0027	2.08E+07	-2.77	0.02
(739.949)		135144.4	4d33	5p73	739.9494	0.0017	7.27E+07	-2.22	0.04
743.145	400	134563.2	4d15	5p23	743.1465	0.0029	8.96E+08	-1.13	0.12
744.719	50	134278.8	4d11	5p33	744.7212	0.0044	1.76E+08	-1.83	0.13
746.501	25	133958.3	4d11	5p31	746.5064	0.0044	9.33E+07	-2.11	0.03
(747.308)		133815.4	4d25	5p63	747.3082	0.0022	3.28E+07	-2.56	0.06
747.983	20	133692.9	4d43	5p55	747.9865	0.0020	5.43E+08	-1.34	0.23
(750.032)		133330.0	4d43	5p73	750.0306	0.0020	6.58E+08	-1.26	0.08
750.571	150	133231.9	4d23	5p63	750.3217	0.0022	6.03E+07	-2.30	0.02
753.083	20	132787.5	4d27	5p45	753.0857	0.0027	1.12E+08	-2.03	0.02
754.179	30	132594.5	4d31	5p63	754.1877	0.0023	1.14E+08	-2.01	0.09
755.513	10	132360.4	4d33	5p63	755.5242	0.0018	4.84E+07	-2.38	0.01
755.822	150	132306.3	4d37	5p55	755.8279	0.0032	6.53E+08	-1.25	0.11
756.525	30	132183.3	4d11	5p23	756.5130	0.0045	4.63E+07	-2.40	0.03
758.670	2000	131809.6	4d11	5p21	758.6650	0.0045	7.25E+08	-1.20	0.17
767.276	800	130331.2	4d35	5p55	767.2829	0.0020	5.58E+08	-1.31	0.28
769.054	600	130029.9	4d53	5p25	769.0631	0.0020	5.91E+08	-1.28	0.23
771.212	1200	129666.0	4d53	5p73	771.2243	0.0019	3.31E+08	-1.53	0.07
778.674	2000	128423.4	4d15	5p17	778.6707	0.0033	7.86E+08	-1.15	0.52
779.517	10000	128284.6	4d17	5p17	779.5184	0.0040	5.04E+09	-0.34	0.68
780.633	5000	128101.2	4d17	5p25	780.6328	0.0039	1.92E+09	-0.76	0.29
785.186	50	127358.4	4d33	5p45	785.1885	0.0020	1.60E+07	-2.83	0.06
785.647	40	127283.6	4d13	5p25	785.6435	0.0028	3.18E+07	-2.53	0.03
786.287	1000	127180.0	4d35	5p63	786.2890	0.0020	5.38E+08	-1.30	0.14
787.875	50	126923.7	4d21	5p41	787.8806	0.0023	1.02E+08	-2.02	0.03
788.155	1200	126878.6	4d53	5p63	788.1586	0.0020	1.08E+09	-1.00	0.15
788.759	3000	126781.4	4d45	5p55	788.7654	0.0023	2.47E+09	-0.64	0.31
791.036	50	126416.5	4d45	5p73	791.0389	0.0022	1.35E+08	-1.90	0.03
793.220	3000	126068.4	4d13	5p11	793.2170	0.0029	1.14E+09	-0.97	0.26
796.085	75	125614.7	4d21	5p43	796.0902	0.0024	2.37E+08	-1.64	0.13

Table 1. Cont.

$\lambda_{\text{obs}}$ (Å)	Int <sup>a</sup>	$\sigma_{\text{obs}}$ (cm <sup>-1</sup> )	Even Level <sup>b</sup>	Odd Level <sup>b</sup>	$\lambda_{\text{Ritz}}$ (Å)	Unc (Å)	$g_{U/A}$ (s <sup>-1</sup> )	$\log(g_{U/A})$	CFI
796.549	150	125541.6	4d43	5p45	796.5496	0.0023	6.33E+08	-1.22	0.34
802.263	4500	124647.4	4d11	5p11	802.2588	0.0051	1.84E+09	-0.75	0.56
802.529	35	124606.1	4d35	5p27	802.5321	0.0023	1.11E+08	-1.97	0.14
805.446	3000	124154.8	4d37	5p45	805.4484	0.0036	1.09E+09	-0.97	0.09
807.914	30000	123775.6	4d15	5p15	807.9081	0.0035	5.66E+09	-0.26	0.66
808.825	50000	123636.1	4d17	5p15	808.8207	0.0043	8.06E+09	-0.10	0.43
810.116	10000	123439.1	4d15	5p13	810.1120	0.0034	3.75E+09	-0.43	0.35
810.775	8000	123338.8	4d27	5p35	810.7736	0.0031	3.34E+09	-0.48	0.20
811.434	1000	123238.6	4d55	5p55	811.4400	0.0027	7.59E+08	-1.12	0.23
811.845	10	123176.2	4d25	5p53	811.8503	0.0026	2.02E+07	-2.70	0.02
813.842	700	122874.0	4d55	5p73	813.8463	0.0026	6.21E+08	-1.21	0.16
814.203	8000	122819.5	4d13	5p15	814.2011	0.0032	1.23E+09	-0.91	0.64
815.407	700	122638.1	4d23	5p53	815.4080	0.0025	1.05E+07	-2.98	0.01
816.442	30000	122482.7	4d13	5p13	816.4396	0.0031	4.07E+09	-0.39	0.65
816.852	50	122421.2	4d23	5p41	816.8597	0.0025	3.10E+07	-2.51	0.01
819.971	500	121955.5	4d31	5p53	819.9759	0.0028	5.13E+08	-1.29	0.18
820.496	15	121877.5	4d53	5p45	820.4957	0.0022	2.46E+07	-2.60	0.03
821.555	450	121720.4	4d33	5p43	821.5560	0.0021	7.68E+08	-1.11	0.22
822.039	450	121648.7	4d25	5p43	822.0399	0.0026	4.72E+08	-1.32	0.26
823.031	900	121502.1	4d33	5p41	823.0296	0.0021	8.60E+08	-1.06	0.38
823.990	450	121360.7	4d21	5p33	823.9898	0.0026	4.57E+08	-1.33	0.34
825.685	1200	121111.6	4d23	5p43	825.6877	0.0026	7.20E+08	-1.14	0.26
826.035	30000	121060.2	4d11	5p13	826.0217	0.0054	1.08E+09	-0.96	0.67
826.035	30000	121060.2	4d45	5p27	826.0640	0.0026	8.57E+08	-1.06	0.45
826.178	90	121039.3	4d21	5p31	826.1758	0.0026	2.36E+08	-1.61	0.18
830.375	10	120427.5	4d31	5p43	830.3718	0.0028	2.04E+07	-2.68	0.01
831.998	50	120192.6	4d33	5p43	831.9922	0.0022	8.61E+08	-1.05	0.19
837.767	1500	119364.9	4d25	5p35	837.7658	0.0028	1.19E+09	-0.90	0.37
838.455	40	119267.0	4d21	5p23	838.4497	0.0026	2.09E+07	-2.65	0.01
841.095	1800	118892.6	4d21	5p21	841.0940	0.0027	1.82E+09	-0.71	0.65
847.209	1600	118034.6	4d47	5p27	847.2103	0.0035	1.54E+09	-0.78	0.69
848.107	90	117909.7	4d33	5p35	848.1050	0.0023	1.95E+08	-1.67	0.11
848.430	10000	117864.8	4d29	5p27	848.4300	0.0072	1.73E+10	0.27	0.74
850.972	100	117512.7	4d55	5p27	850.9677	0.0030	3.09E+08	-1.47	0.51
851.819	30000	117395.8	4d25	5p33	851.8219	0.0028	3.61E+09	-0.41	0.60

Table 1. Cont.

$\lambda_{\text{obs}}$ (Å)	Int <sup>a</sup>	$\sigma_{\text{obs}}$ (cm <sup>-1</sup> )	Even Level <sup>b</sup>	Odd Level <sup>b</sup>	$\lambda_{\text{Ritz}}$ (Å)	Unc (Å)	$g_{\text{U}}A$ (s <sup>-1</sup> )	$\log(g_{\text{U}}I_f)$	CFI
854.303	1000000	117054.5	4d19	5p17	854.3030	0.0072	1.71E+10	0.27	0.79
855.746	30000	116857.1	4d23	5p33	855.7394	0.0028	7.09E+08	-1.11	0.19
856.665	10000	116731.7	5d83	5p31	856.6622	0.0027	2.05E+07	-2.65	0.00
858.081	30000	116539.1	4d35	5p53	858.0633	0.0024	2.03E+09	-0.65	0.25
858.081	30000	116539.1	4d23	5p31	858.0974	0.0028	3.19E+09	-0.46	0.54
859.152	10000	116393.8	4d63	5p83	859.1583	0.0024	5.20E+08	-1.24	0.30
860.292	1800	116239.6	4d53	5p53	860.2902	0.0024	1.00E+09	-0.95	0.28
860.771	75	116174.9	4d31	5p33	860.7718	0.0030	1.43E+08	-1.80	0.16
861.905	2000	116022.1	4d53	5p41	861.9062	0.0024	2.03E+09	-0.65	0.68
862.511	3000	115940.6	4d33	5p33	862.5132	0.0023	8.94E+08	-1.00	0.22
864.926	2000	115616.8	4d33	5p31	864.9086	0.0024	8.39E+07	-2.02	0.02
864.993	5000	115607.9	4d47	5p45	864.9915	0.0035	1.10E+10	0.09	0.66
867.282	10000	115302.8	4d25	5p23	867.2843	0.0029	3.95E+09	-0.35	0.76
868.911	1600	115086.6	4d55	5p45	868.9086	0.0030	8.38E+08	-1.02	0.35
869.451	10000	115015.1	4d35	5p43	869.4541	0.0025	2.86E+09	-0.49	0.33
871.358	25	114763.4	4d23	5p23	871.3457	0.0029	3.53E+07	-2.40	0.01
871.460	2000	114750.0	4d63	5p61	871.4691	0.0030	3.02E+09	-0.46	0.55
871.787	60000	114706.9	4d37	5p35	871.7907	0.0042	8.68E+09	0.00	0.80
872.792	30	114574.8	6s31	5p63	872.7799	0.0044	1.07E+08	-1.91	0.15
874.202	4000	114390.0	4d23	5p21	874.2019	0.0029	8.67E+08	-1.01	0.22
874.741	100	114319.6	6s33	5p11	874.7481	0.0022	1.50E+08	-1.76	0.07
876.241	2000	114123.9	4d43	5p33	876.2416	0.0027	9.74E+08	-0.95	0.25
876.565	2500	114081.7	4d31	5p23	876.5639	0.0031	7.29E+08	-1.08	0.39
878.373	600	113846.9	4d33	5p23	878.3698	0.0024	4.76E+08	-1.26	0.13
878.713	3000	113802.8	4d43	5p31	878.7141	0.0027	1.05E+09	-0.92	0.37
879.466	75	113705.4	4d31	5p21	879.4544	0.0032	1.28E+07	-2.83	0.01
881.272	5000	113472.3	4d33	5p21	881.2723	0.0025	6.82E+08	-1.10	0.20
883.887	5000	113136.6	4d27	5p17	883.8812	0.0039	7.24E+08	-1.07	0.26
885.016	5000	112992.3	4d45	5p53	885.0191	0.0027	1.37E+09	-0.80	0.25
885.312	60000	112954.5	4d27	5p25	885.3143	0.0037	7.71E+09	-0.04	0.80
887.067	75	112731.1	4d35	5p35	887.0659	0.0026	1.23E+08	-1.84	0.05
889.448	60	112429.3	4d53	5p35	889.4461	0.0026	1.14E+08	-1.86	0.08
892.613	8000	112030.6	4d43	5p23	892.6118	0.0028	1.53E+09	-0.74	0.42
895.015	3000	111730.0	4d21	5p11	895.0120	0.0030	1.95E+08	-1.63	0.08
895.609	3000	111655.9	4d43	5p21	895.6094	0.0028	3.68E+08	-1.36	0.08
895.769	8000	111635.9	4d75	5p83	895.7698	0.0029	7.97E+09	-0.02	0.77



Table 1. Cont.

$\lambda_{\text{obs}}$ (Å)	Int <sup>a</sup>	$\sigma_{\text{obs}}$ (cm <sup>-1</sup> )	Even Level <sup>b</sup>	Odd Level <sup>b</sup>	$\lambda_{\text{Ritz}}$ (Å)	Unc (Å)	$g_{U/A}$ (s <sup>-1</sup> )	$\log(g_{U/A})$	CFI
897.155	5000	111463.5	4d45	5p43	897.1419	0.0028	1.10E+09	-0.88	0.13
900.135	8000	111094.4	4d65	5p73	900.1453	0.0022	3.88E+09	-0.33	0.63
902.141	15	H, x	5d83	5p41	902.1284	0.0030	3.83E+07	-2.33	0.01
902.843	4000	110761.2	4d35	5p33	902.8405	0.0027	7.25E+08	-1.05	0.33
905.307	1000	110459.8	4d53	5p33	905.3063	0.0026	4.17E+08	-1.29	0.12
907.946	1000	110138.7	4d53	5p31	907.9457	0.0027	1.65E+08	-1.69	0.10
913.665	8000	109449.3	4d55	5p53	913.6659	0.0033	3.42E+09	-0.36	0.70
915.904	5000	109181.7	4d45	5p35	915.9053	0.0030	6.60E+08	-1.08	0.26
917.601	3000	108979.8	4d25	5p25	917.5967	0.0033	4.78E+08	-1.22	0.51
920.232	3000	108668.2	4d35	5p23	920.2295	0.0027	4.74E+08	-1.22	0.11
921.750	7000	108489.3	4d27	5p15	921.7454	0.0041	1.20E+09	-0.82	0.24
922.118	20000	108446.0	4d57	5p55	922.1279	0.0034	8.24E+09	0.02	0.89
922.118	20000	108446.0	4d23	5p25	922.1442	0.0033	5.10E+06	-3.19	0.02
922.785	700	108367.6	4d53	5p23	922.7913	0.0027	2.08E+08	-1.57	0.06
923.292	3000	108308.1	4d65	5p63	923.2994	0.0023	1.75E+09	-0.65	0.64
924.692	300	108144.1	4d21	5p13	924.6888	0.0033	1.95E+08	-1.59	0.18
925.999	8000	107991.5	4d53	5p21	925.9954	0.0027	7.02E+08	-1.04	0.22
926.587	10000	107922.9	4d55	5p43	926.5919	0.0033	2.82E+09	-0.44	0.59
930.021	25	107524.5	4d33	5p25	930.0148	0.0027	1.44E+08	-1.73	0.16
932.598	3000	107227.3	4d23	5p11	932.5955	0.0033	4.43E+08	-1.24	0.28
932.728	5000	107212.4	4d45	5p33	932.7321	0.0030	1.41E+09	-0.74	0.32
938.575	2000	106544.5	4d31	5p11	938.5756	0.0036	4.74E+08	-1.21	0.75
940.648	1500	106309.7	4d33	5p11	940.6463	0.0028	7.87E+08	-0.98	0.40
941.972	500	106160.3	4d47	5p35	941.9739	0.0042	3.28E+08	-1.36	0.14
946.000	1500	105708.2	4d43	5p25	945.9961	0.0032	1.44E+08	-1.72	0.18
951.300	7000	105119.3	4d45	5p23	946.6212	0.0036	7.32E+07	-2.00	0.09
956.356	15	104563.6	6s25	5p33	951.3034	0.0031	9.14E+08	-0.91	0.19
956.797	75	104515.4	4d25	5p15	956.3568	0.0058	1.12E+09	-0.81	0.78
956.797	75	104515.4	5d75	5p15	956.7919	0.0038	1.26E+08	-1.77	0.11
956.904	75	104503.7	4d37	5p17	956.7967	0.0025	2.17E+07	-2.53	0.00
956.999	5000	104493.3	4d43	5p11	956.8938	0.0052	1.06E+08	-1.83	0.08
958.295	10	104352.0	6s11	5p13	958.2918	0.0032	5.29E+08	-1.14	0.17
958.572	20000	104321.8	4d37	5p25	958.2918	0.0030	3.98E+08	-1.26	0.07
959.888	300	104178.8	4d25	5p13	958.5736	0.0050	2.35E+09	-0.49	0.22
961.737	1500	103978.5	4d23	5p15	959.8846	0.0036	1.51E+08	-1.68	0.12
					961.7373	0.0038	1.31E+08	-1.74	0.23

Table 1. Cont.

$\lambda_{\text{obs}}$ (Å)	Int <sup>a</sup>	$\sigma_{\text{obs}}$ (cm <sup>-1</sup> )	Even Level <sup>b</sup>	Odd Level <sup>b</sup>	$\lambda_{\text{Ritz}}$ (Å)	Unc (Å)	$g_{U/A}$ (s <sup>-1</sup> )	$\log(g_{U/f})$	CFI
964.612	75	103668.6	4d55	5p33	964.6066	0.0036	1.07E+07	-2.82	0.01
964.862	1800	103641.8	4d23	5p13	964.8620	0.0036	1.60E+08	-1.66	0.11
970.302	1000	10360.7	4d33	5p15	970.3014	0.0032	3.12E+08	-1.35	0.22
971.262	8000	102958.8	4d31	5p13	971.2645	0.0039	1.10E+09	-0.81	0.47
973.506	8000	102721.5	4d57	5p27	973.5164	0.0039	2.37E+09	-0.47	0.63
987.710	60	101244.3	4d43	5p15	987.7102	0.0037	3.38E+06	-3.31	0.01
997.069	200	100294.0	4d57	5p45	997.0683	0.0039	1.91E+08	-1.54	0.08
1001.401	8000	99860.1	4d37	5p15	1001.4294	0.0056	2.23E+06	-3.47	0.00
1007.459	8	99259.62	5s13	5p83	1007.4683	0.0024	1.68E+07	-2.59	0.01
1012.182	300	98796.46	4d45	5p25	1012.1782	0.0036	1.13E+08	-1.76	0.05
1013.316	2	98685.90	5d41	5p11	1013.3143	0.0021	8.97E+07	-1.86	0.03
1013.765	2	98642.19	5d65	5p25	1013.7694	0.0023	1.21E+08	-1.73	0.03
1021.642	8000	97881.65	4d35	5p15	1021.6380	0.0037	1.02E+09	-0.80	0.34
1023.866	300	97669.03	4d65	5p53	1023.8658	0.0028	2.65E+08	-1.38	0.25
1024.417	5	97616.50	5s13	5p61	1024.4382	0.0033	1.60E+06	-3.60	0.00
1024.800	2000	97580.02	4d53	5p15	1024.7965	0.0036	2.12E+08	-1.47	0.19
1025.165	8000	97545.27	4d35	5p13	1025.1648	0.0035	4.94E+08	-1.11	0.13
1026.554	20	97413.29	4d85	5p83	1026.5538	0.0025	4.97E+08	-1.10	0.18
1028.336	7000	97244.48	4d63	5p51	1028.3415	0.0028	9.37E+08	-0.83	0.64
1028.336	7000	97244.48	4d53	5p13	1028.3452	0.0034	5.34E+07	-2.07	0.02
1040.119	200	96142.85	4d65	5p43	1040.1257	0.0029	2.31E+08	-1.43	0.21
1043.889	3	95795.63	6s21	5p23	1043.8995	0.0040	2.43E+08	-1.40	0.07
1044.113	500	95775.07	4d47	5p25	1044.1106	0.0051	3.02E+08	-1.31	0.06
1044.349	3	95753.43	5d73	5p21	1044.3602	0.0028	6.83E+07	-1.95	0.01
1049.162	25	95314.17	6s13	5p13	1049.1621	0.0026	7.41E+08	-0.91	0.23
1062.555	500	94112.78	6s23	5p21	1062.5512	0.0035	2.15E+09	-0.44	0.67
1063.881	75	93995.48	4d45	5p13	1063.8787	0.0040	5.32E+07	-2.05	0.02
1065.429	35	93858.91	4d65	5p35	1065.9430	0.0032	8.84E+07	-1.82	0.30
1065.938	200	93814.09	6s15	5p13	1065.9406	0.0028	3.71E+09	-0.20	0.63
1069.777	8000	93477.43	6s15	5p15	1069.7805	0.0032	7.12E+09	0.09	0.77
1072.143	500	93271.14	6s33	5p45	1072.1497	0.0034	5.69E+09	-0.01	0.74
1072.627	90	93229.05	6s11	5p23	1072.6265	0.0037	1.19E+09	-0.69	0.41
(1073.586)		93145.95	6s25	5p45	1073.5858	0.0073	1.50E+09	-0.59	0.95
1074.887	500	93033.04	4d63	5p73	1074.8909	0.0030	5.18E+08	-1.05	0.33
1077.696	3	92790.55	5d55	5p13	1077.7006	0.0022	5.91E+07	-1.99	0.00
1086.914	8	92003.60	5d63	5p23	1086.9113	0.0022	5.29E+08	-1.03	0.13

Table 1. Cont.

$\lambda_{\text{obs}}$ (Å)	Int <sup>a</sup>	$\sigma_{\text{obs}}$ (cm <sup>-1</sup> )	Even Level <sup>b</sup>	Odd Level <sup>b</sup>	$\lambda_{\text{Ritz}}$ (Å)	Unc (Å)	$g_{\text{UL}}A$ (s <sup>-1</sup> )	$\log(g_{\text{UL}}f)$	CFI
(1087.355)		91967.64	6s23	5p31	1087.3552	0.0037	5.74E+07	-1.99	0.03
1088.274	30	91888.62	4d65	5p33	1088.2688	0.0032	8.46E+07	-1.82	0.14
(1090.176)		91728.48	6s13	5p11	1090.1761	0.0028	1.55E+09	-0.56	0.55
1091.166	500	91645.08	6s23	5p33	1091.1651	0.0036	2.58E+09	-0.34	0.52
1093.406	500	91457.34	6s11	5p31	1093.4074	0.0040	2.09E+09	-0.43	0.89
(1097.106)	2	91148.90	5d41	5p23	1097.1087	0.0024	3.23E+08	-1.24	0.31
(1097.260)		91136.19	6s11	5p33	1097.2599	0.0039	8.52E+08	-0.81	0.43
1100.762	500	90846.16	4d57	5p35	1100.7638	0.0048	2.33E+08	-1.37	0.17
1104.810	8000	90513.30	6s13	5p25	1104.8136	0.0029	6.37E+09	0.07	0.83
1105.225	8	90479.31	5d45	5p15	1105.2225	0.0030	5.86E+08	-0.97	0.05
1112.211	5	89911.00	5d63	5p33	1112.2129	0.0024	4.42E+08	-1.09	0.07
1113.632	500	89796.27	4d65	5p23	1113.6345	0.0033	2.86E+08	-1.27	0.26
1115.130	8000	89675.64	6s23	5p35	1115.1319	0.0039	6.41E+09	0.08	0.88
1115.714	35	89628.70	5d53	5p11	1115.7157	0.0021	5.57E+08	-0.98	0.06
1117.949	5000	89449.52	6s21	5p43	1117.9617	0.0046	1.22E+09	-0.64	0.30
1122.891	40	89055.84	5d41	5p33	1122.8930	0.0025	1.48E+09	-0.55	0.67
1123.198	15	89031.50	5d73	5p43	1123.2007	0.0032	3.51E+08	-1.18	0.10
1123.432	5	89012.95	6s15	5p25	1123.4351	0.0031	4.85E+07	-2.04	0.02
1125.741	8000	88830.38	6s15	5p17	1125.7511	0.0037	8.69E+09	0.22	0.93
(1127.686)		88676.22	5d35	5p13	1127.6865	0.0027	5.36E+08	-0.99	0.03
(1128.160)		88640.07	4d75	5p55	1128.1600	0.0041	6.70E+08	-0.89	0.61
1130.833	200	88430.39	6s31	5p83	1130.8356	0.0079	4.02E+09	-0.11	0.98
1131.984	40	88340.47	5d35	5p15	1131.9850	0.0032	2.81E+08	-1.27	0.02
(1133.055)		88257.20	5d65	5p35	1133.0546	0.0030	1.67E+08	-1.50	0.10
1134.495	75	88144.95	6s25	5p63	1134.4903	0.0082	1.51E+09	-0.54	0.38
1136.509	5	87988.74	5d55	5p41	1134.5635	0.0048	2.27E+09	-0.35	0.50
1136.993	20	87951.29	5d51	5p25	1136.5057	0.0024	1.55E+08	-1.52	0.01
1137.123	3	87941.23	5d63	5p43	1136.9939	0.0030	4.84E+08	-1.03	0.13
1137.375	200	87921.75	6s21	5p35	1137.3758	0.0027	6.51E+07	-1.90	0.04
(1142.799)		87504.68	5d73	5p53	1137.3759	0.0048	1.31E+09	-0.60	0.49
1150.971	150	86883.16	5d51	5p33	1142.7989	0.0033	3.50E+08	-1.17	0.17
1157.079	40	86424.52	6d11	5p43	1150.9739	0.0043	1.73E+09	-0.46	0.80
1161.657	20	86083.93	6s23	5p53	1157.0806	0.0032	4.32E+08	-1.06	0.24
1162.889	3	85992.73	5d43	5p41	1161.6681	0.0041	2.25E+08	-1.34	0.17
1163.149	8	85973.51	5d65	5p11	1162.8868	0.0020	2.63E+08	-1.27	0.02
				5p43	1163.1491	0.0030	1.42E+08	-1.54	0.03

Table 1. Cont.

$\lambda_{\text{obs}}$ (Å)	Int <sup>a</sup>	$\sigma_{\text{obs}}$ (cm <sup>-1</sup> )	Even Level <sup>b</sup>	Odd Level <sup>b</sup>	$\lambda_{\text{Ritz}}$ (Å)	Unc (Å)	$g_{U/A}$ (s <sup>-1</sup> )	$\log(g_{U/A})$	CFI
1164.616	200	85865.21	6s23	5p53	1164.6166	0.0042	1.10E+09	-0.65	0.40
1167.437	5	85657.73	5d63	5p43	1167.4378	0.0026	2.34E+08	-1.32	0.04
1168.328	200	85592.40	4d83	5p83	1168.3133	0.0031	2.55E+08	-1.28	0.40
1168.565	4	85575.04	6s11	5p41	1168.5784	0.0045	7.92E+07	-1.79	0.24
1169.735	150	85489.45	4d75	5p63	1169.7331	0.0042	8.55E+07	-1.76	0.05
1169.818	200	85483.38	6s33	5p73	1169.8078	0.0040	2.78E+09	-0.25	0.65
1176.540	300	84994.99	6s25	5p55	1176.5399	0.0089	4.82E+09	0.00	0.81
1177.817	200	84902.83	5d33	5p11	1177.8398	0.0027	4.71E+08	-1.01	0.16
1179.214	8	84802.25	5d41	5p43	1179.2104	0.0028	3.64E+08	-1.12	0.11
1185.554	20	84348.75	5d63	5p41	1185.5535	0.0027	3.41E+08	-1.14	0.13
1187.777	200	84190.89	6s13	5p23	1187.7767	0.0033	1.70E+09	-0.45	0.44
1188.940	5	84108.53	5d31	5p11	1188.9343	0.0027	1.23E+08	-1.59	0.02
1191.195	500	83949.31	4d83	5p61	1191.1959	0.0044	1.20E+09	-0.59	0.61
1191.640	20	83917.96	5d37	5p17	1191.6238	0.0100	1.31E+08	-1.55	0.02
1197.981	300	83473.78	4d65	5p25	1197.9782	0.0039	1.40E+08	-1.52	0.25
1201.630	800	83220.29	5d25	5p13	1201.6217	0.0041	1.28E+09	-0.56	0.12
1209.328	100	82690.55	6s15	5p23	1209.3272	0.0035	2.40E+08	-1.28	0.10
1210.115	500	82636.77	5d23	5p15	1210.1135	0.0033	7.42E+08	-0.79	0.28
1213.322	40	82418.35	6s13	5p31	1213.3120	0.0036	1.98E+08	-1.36	0.19
1218.066	3	82097.36	6s13	5p33	1218.0577	0.0035	5.86E+07	-1.89	0.02
1221.502	150	81866.42	5d73	5p45	1221.4970	0.0039	1.45E+09	-0.49	0.64
1227.090	200	81493.61	5d21	5p13	1227.0824	0.0024	1.32E+09	-0.53	0.24
1230.424	150	81272.80	6s33	5p51	1230.4229	0.0045	1.03E+09	-0.63	0.64
1240.739	3	80597.13	6s15	5p33	1240.7314	0.0037	3.48E+07	-2.10	0.03
1241.643	50	80538.45	5s15	5p55	1241.6320	0.0027	3.43E+07	-2.10	0.01
1242.844	10000	80460.62	4d57	5p25	1242.8343	0.0060	1.83E+08	-1.37	0.12
1246.600	15000	80218.19	5d75	5p45	1246.5996	0.0038	5.57E+09	0.11	0.63
1248.301	75	80108.88	5d57	5p45	1248.2886	0.0022	4.67E+07	-1.96	0.01
1248.301	75	80108.88	5s13	5p51	1248.2891	0.0048	2.70E+07	-2.20	0.01
1250.044	200	79997.18	5d53	5p33	1250.0283	0.0025	8.30E+08	-0.71	0.12
1254.821	100	79692.64	5d45	5p23	1254.8152	0.0032	5.76E+08	-0.87	0.03
1256.150	60	79608.33	4d63	5p53	1256.1462	0.0041	3.84E+07	-2.04	0.27
1256.701	12000	79573.42	5d55	5p33	1256.6933	0.0028	2.23E+09	-0.28	0.20
1259.640	100000	79387.76	5d23	5p11	1259.6400	0.0029	4.28E+09	0.01	0.59
1260.859	12000	79311.01	4d41	5p73	1260.8507	0.0024	2.93E+08	-1.15	0.67
1262.106	15000	79232.65	5d27	5p15	1262.1007	0.0051	1.69E+09	-0.39	0.28

Table 1. Cont.

$\lambda_{\text{obs}}$ (Å)	Int <sup>a</sup>	$\sigma_{\text{obs}}$ (cm <sup>-1</sup> )	Even Level <sup>b</sup>	Odd Level <sup>b</sup>	$\lambda_{\text{Ritz}}$ (Å)	Unc (Å)	$g_{U/A}$ (s <sup>-1</sup> )	$\log(g_{U/A})$	CFI
1265.676	75	79009.16	4d65	5p15	1265.6696	0.0048	1.78E+07	-2.37	0.09
1268.550	300000	78830.16	5d43	5p21	1268.5452	0.0024	5.09E+09	0.09	0.48
1271.817	60	78627.66	6s15	5p35	1271.8124	0.0041	1.91E+08	-1.34	0.06
1273.809	200	78504.71	5s25	5p83	1273.8054	0.0038	2.51E+08	-1.21	0.35
1274.001	10	78492.87	5d63	5p45	1273.9965	0.0034	2.21E+08	-1.27	0.36
(1275.190)		78419.26	5d25	5p25	1275.1895	0.0046	5.59E+09	0.14	0.70
1278.197	5	78235.20	5d25	5p17	1278.1743	0.0053	4.48E+07	-1.96	0.07
1279.227	200	78172.21	5d23	5p25	1279.2227	0.0030	4.74E+08	-0.94	0.25
1280.076	300000	78120.36	5d11	5p13	1280.0759	0.0033	4.17E+09	0.01	0.91
1280.713	50	78081.51	4d63	5p43	1280.7090	0.0043	2.47E+07	-2.22	0.06
1281.503	40	78033.37	5s33	5p83	1281.4978	0.0039	6.24E+07	-1.81	0.29
1283.561	200000	77908.26	5d21	5p11	1283.5609	0.0026	2.83E+09	-0.15	0.88
1284.588	90	77845.97	6s13	5p43	1284.6081	0.0039	1.04E+08	-1.59	0.04
1285.486	400	77791.59	5d75	5p27	1285.4819	0.0045	1.42E+09	-0.46	0.74
1287.278	300000	77683.30	5d57	5p27	1287.2785	0.0055	7.52E+09	0.27	0.77
1288.606	400	77603.24	5d55	5p35	1288.5894	0.0033	8.01E+08	-0.70	0.15
1288.660	700	77599.99	5d45	5p33	1288.6595	0.0034	1.63E+09	-0.39	0.28
1289.155	200000	77570.19	4d73	5p55	1289.1509	0.0028	3.51E+08	-1.06	0.33
1289.429	250000	77553.71	5d35	5p23	1289.4261	0.0034	3.15E+09	-0.11	0.21
1292.599	700	77363.51	5d33	5p23	1292.5942	0.0031	7.63E+08	-0.72	0.17
1295.238	300000	77205.89	4d73	5p73	1295.2349	0.0022	5.46E+08	-0.87	0.23
1297.729	2000000	77057.69	5d13	5p13	1297.7315	0.0030	8.63E+09	0.34	0.88
1299.606	300000	76946.4	5d31	5p21	1299.6041	0.0032	4.84E+09	0.09	0.92
1303.441	300000	76720.00	5d13	5p15	1303.4275	0.0038	3.11E+09	-0.10	0.88
1306.580	25	76535.69	6s13	5p41	1306.5769	0.0040	3.93E+08	-0.99	0.21
1306.759	300000	76525.20	4d41	5p63	1306.7526	0.0026	7.33E+08	-0.73	0.53
(1307.988)		76453.71	5d15	5p13	1307.9875	0.0076	6.73E+09	0.24	0.42
1309.081	10	76389.47	5s33	5p61	1309.0811	0.0055	4.03E+07	-1.98	0.14
1309.538	300000	76362.81	5d43	5p33	1309.5431	0.0024	3.93E+09	0.01	0.58
1309.854	150	76344.39	6s15	5p43	1309.8529	0.0042	5.56E+08	-0.84	0.21
1310.312	15	76317.70	6s13	5p53	1310.3081	0.0041	9.53E+07	-1.61	0.06
1313.774	250	76116.59	5d15	5p15	1313.7740	0.0080	1.12E+10	0.46	0.90
(1314.550)		76071.89	5d17	5p15	1314.5505	0.0055	1.57E+10	0.61	0.64
1315.851	500000	75996.45	4d57	5p15	1315.8442	0.0071	2.90E+07	-2.12	0.06

Table 1. Cont.

$\lambda_{\text{obs}}$ (Å)	Int <sup>a</sup>	$\sigma_{\text{obs}}$ (cm <sup>-1</sup> )	Even Level <sup>b</sup>	Odd Level <sup>b</sup>	$\lambda_{\text{Ritz}}$ (Å)	Unc (Å)	$g_{U/A}$ (s <sup>-1</sup> )	$\log(g_{U/f})$	CFI
1317.557	90	75898.04	5s13	5p73	1317.5505	0.0022	5.68E+06	-2.83	0.00
1317.946	2000000	75875.64	5d47	5p45	1317.9551	0.0055	2.43E+10	0.80	0.96
1318.842	500000	75824.09	4d51	5p51	1318.8428	0.0028	8.90E+08	-0.64	0.67
1320.219	250	75745.01	5d53	5p43	1320.2188	0.0028	6.57E+08	-0.77	0.14
1322.222	500000	75630.26	5d45	5p35	1322.2205	0.0039	3.42E+09	-0.05	0.58
1322.889	3000000	75592.13	5d33	5p31	1322.8927	0.0034	9.64E+09	0.40	0.94
1324.659	500000	75491.13	5d83	5p61	1324.6640	0.0082	1.01E+10	0.42	0.95
1325.186	3000000	75461.11	5d35	5p33	1325.1898	0.0036	8.78E+09	0.36	0.74
1327.651	3000000	75321.00	5d55	5p43	1327.6556	0.0032	9.45E+09	0.40	0.70
1328.540	50	75270.60	5d33	5p33	1328.5363	0.0033	3.35E+08	-1.05	0.08
1335.958	50	74852.65	4d75	5p53	1335.9802	0.0054	2.64E+07	-2.15	0.05
1336.587	40	74817.43	6s15	5p53	1336.5834	0.0044	1.68E+08	-1.35	0.08
1336.645	25	74814.18	5s15	5p27	1336.6350	0.0035	2.00E+07	-2.27	0.00
1336.909	25	74799.41	5d31	5p31	1336.9043	0.0035	1.82E+08	-1.32	0.06
1337.456	2000000	74768.81	5d27	5p25	1337.4604	0.0053	2.23E+10	0.78	0.98
1340.744	500	74585.45	5d27	5p17	1340.7443	0.0060	3.68E+08	-1.00	0.22
1341.665	500000	74534.25	5d11	5p11	1341.6604	0.0036	1.85E+09	-0.30	0.46
1342.673	500	74478.3	5d31	5p33	1342.6683	0.0033	6.55E+08	-0.76	0.40
1343.434	1000000	74436.11	5d53	5p41	1343.4334	0.0030	7.36E+09	0.30	0.80
1343.738	1000000	74419.27	4d73	5p63	1343.7226	0.0024	1.22E+09	-0.49	0.43
1344.216	50	74392.81	5d43	5p35	1344.2154	0.0029	4.96E+08	-0.87	0.21
1347.381	200	74218.06	5d53	5p53	1347.3784	0.0030	8.35E+08	-0.65	0.31
1349.888	500000	74080.22	5d73	5p73	1349.8860	0.0046	5.01E+09	0.13	0.64
1350.389	900000	74052.74	4d85	5p73	1350.3838	0.0025	6.66E+08	-0.73	0.38
1352.760	2	73922.94	5s11	5p51	1352.7493	0.0027	1.50E+07	-2.38	0.11
1354.162	200	73846.41	5d83	5p83	1354.1583	0.0076	1.89E+09	-0.28	0.83
1354.861	500000	73808.31	5d65	5p63	1354.8575	0.0041	7.07E+09	0.29	0.76
1355.128	100000	73793.77	5d55	5p53	1355.1252	0.0034	2.73E+09	-0.12	0.25
1355.245	180000	73787.40	5d29	5p27	1355.2451	0.0081	3.01E+10	0.92	1.00
1356.518	5000000	73718.15	5d37	5p35	1356.5305	0.0127	2.36E+10	0.81	0.99
1359.388	4500000	73562.51	5d19	5p17	1359.3879	0.0084	2.97E+10	0.91	0.99
1360.408	25	73507.36	4d63	5p31	1360.4060	0.0049	1.84E+07	-2.29	0.04
1360.689	500000	73492.18	5d63	5p63	1360.6799	0.0036	5.35E+09	0.17	0.60
1360.689	500000	73492.18	5d35	5p35	1360.7068	0.0041	8.34E+08	-0.64	0.11
1361.069	150000	73471.66	5d13	5p11	1361.0686	0.0033	1.01E+09	-0.55	0.17

Table 1. Cont.

$\lambda_{\text{obs}}$ (Å)	Int <sup>a</sup>	$\sigma_{\text{obs}}$ (cm <sup>-1</sup> )	Even Level <sup>b</sup>	Odd Level <sup>b</sup>	$\lambda_{\text{Ritz}}$ (Å)	Unc (Å)	$g_{\text{UL}}A$ (s <sup>-1</sup> )	$\log(g_{\text{L}}/f)$	CFI
1361.502	300	73448.29	5d47	5p27	1361.4937	0.0063	1.37E+09	-0.42	0.95
1363.284	500000	73352.29	5d85	5p83	1363.2841	0.0090	1.68E+10	0.67	0.98
1367.758	500000	73112.35	5s13	5p63	1367.7557	0.0024	3.08E+08	-1.06	0.09
1369.857	75	73000.32	5d51	5p73	1369.8579	0.0045	1.04E+09	-0.54	0.51
1376.698	100000	72637.57	5d41	5p63	1376.6992	0.0039	2.64E+09	-0.12	0.58
1380.608	500000	72431.86	5d75	5p73	1380.6093	0.0045	6.15E+09	0.25	0.51
1383.652	75	72272.51	5s23	5p51	1383.6407	0.0026	5.21E+07	-1.83	0.06
1383.966	10	72256.11	5d13	5p25	1383.9606	0.0035	3.45E+07	-2.01	0.02
1384.557	8	72225.27	5d23	5p21	1384.5558	0.0035	6.43E+07	-1.73	0.01
1386.785	100	72109.23	5d43	5p43	1386.7829	0.0027	4.73E+08	-0.87	0.07
1387.003	500000	72097.90	5d25	5p23	1387.0083	0.0053	8.83E+09	0.41	0.58
1387.587	100000	72067.55	5d75	5p55	1387.5896	0.0050	3.69E+09	0.03	0.43
1389.683	600000	71958.86	5d57	5p55	1389.6831	0.0062	1.52E+10	0.65	0.97
1391.789	600000	71849.97	5d23	5p23	1391.7813	0.0033	3.99E+09	0.06	0.68
1392.363	600000	71820.35	5d45	5p53	1392.3692	0.0041	1.03E+10	0.48	0.76
1396.402	300	71612.62	4d51	5p73	1396.3986	0.0030	2.01E+08	-1.24	0.33
1396.507	10	71607.23	5d17	5p25	1396.5072	0.0057	1.64E+09	-0.32	0.19
1400.088	500	71424.08	5d17	5p17	1400.0878	0.0064	7.65E+09	0.35	0.99
1403.173	500	71267.05	4d85	5p63	1403.1726	0.0026	1.42E+09	-0.37	0.66
1404.344	400	71207.62	5d35	5p43	1404.3421	0.0041	4.46E+09	0.12	0.60
1408.005	75	71022.48	5d65	5p73	1408.0035	0.0044	3.23E+09	-0.02	0.37
1408.101	60	71017.63	5d33	5p43	1408.1009	0.0037	9.19E+08	-0.56	0.48
1412.421	25	70800.42	5d43	5p41	1412.4202	0.0029	4.78E+07	-1.84	0.01
1414.290	15	70706.86	5d63	5p73	1414.2927	0.0039	4.44E+08	-0.88	0.14
1415.262	800	70658.30	5d65	5p55	1415.2643	0.0049	3.92E+09	0.07	0.38
1416.781	500	70582.54	5d43	5p53	1416.7814	0.0029	1.63E+09	-0.31	0.34
1421.043	400	70370.85	5d21	5p23	1421.0425	0.0030	8.43E+08	-0.60	0.38
1421.641	50	70341.25	5d63	5p55	1421.6187	0.0045	2.32E+09	-0.15	0.75
1422.759	3	70285.97	6s21	5p51	1422.7526	0.0077	4.07E+08	-0.91	0.17
1423.983	5	70225.56	5d31	5p43	1423.9864	0.0038	1.40E+08	-1.37	0.09
1426.967	5	70078.71	5d23	5p31	1426.9714	0.0038	9.71E+07	-1.53	0.04
1428.475	2	70004.73	5d25	5p33	1428.4769	0.0057	2.47E+08	-1.12	0.03
1431.245	600	69869.24	5d75	5p51	1431.2485	0.0053	3.38E+09	0.01	0.72
1431.605	60	69851.67	5d41	5p73	1431.6073	0.0042	8.36E+08	-0.59	0.84

Table 1. Cont.

$\lambda_{\text{obs}}$ (Å)	Int <sup>a</sup>	$\sigma_{\text{obs}}$ (cm <sup>-1</sup> )	Even Level <sup>b</sup>	Odd Level <sup>b</sup>	$\lambda_{\text{Ritz}}$ (Å)	Unc (Å)	$g_{U/A}$ (s <sup>-1</sup> )	$\log(g_{U/A})$	CFI
1433.535	35	69757.63	5d23	5p33	1433.5401	0.0036	5.20E+08	-0.80	0.13
1434.541	3	69708.71	5d33	5p41	1434.5399	0.0039	6.91E+07	-1.67	0.04
1435.114	75	69680.88	5d35	5p53	1435.1135	0.0043	4.03E+08	-0.91	0.09
1439.035	15	69491.01	5d33	5p53	1439.0390	0.0039	9.91E+07	-1.51	0.10
1440.524	60	69419.18	4d73	5p45	1440.5145	0.0030	9.41E+07	-1.54	0.22
1451.028	20	68916.66	5d31	5p41	1451.0311	0.0039	2.33E+08	-1.13	0.10
1453.723	400	68788.90	5d51	5p51	1453.7206	0.0052	2.52E+09	-0.10	0.77
1455.629	15	68698.82	5d31	5p53	1455.6344	0.0040	1.70E+08	-1.27	0.18
1455.759	400	68692.69	4d85	5p27	1455.7530	0.0040	2.37E+08	-1.11	0.70
1457.750	15	68598.87	5d21	5p31	1457.7474	0.0035	1.87E+08	-1.23	0.14
1464.603	8	68277.89	5d21	5p33	1464.6032	0.0032	1.39E+08	-1.35	0.10
1469.257	60	68061.61	5s23	5p73	1469.2521	0.0026	7.48E+07	-1.62	0.05
1476.575	12	67724.29	5d47	5p55	1476.5744	0.0072	2.05E+08	-1.17	0.13
(1478.619)		67630.67	5s21	5p51	1478.6191	0.0031	6.50E+08	-0.67	0.55
1498.117	800	66750.46	5s15	5p53	1498.1125	0.0032	6.00E+08	-0.69	0.19
1503.863	60	66495.42	5d63	5p51	1503.8621	0.0046	6.82E+08	-0.64	0.38
1505.017	1200	66444.43	4d83	5p51	1505.0166	0.0030	1.10E+09	-0.42	0.61
1508.089	150	66309.08	5d13	5p21	1508.0852	0.0041	3.24E+06	-2.96	0.00
1509.064	40	66266.24	4d85	5p45	1509.0561	0.0034	7.31E+07	-1.59	0.21
1522.539	60	65679.76	6s13	5p63	1522.5393	0.0055	3.29E+08	-0.94	0.29
1523.456	12	65640.23	5d41	5p51	1523.4543	0.0050	1.92E+08	-1.17	0.11
(1526.619)		65503.71	5d23	5p43	1526.6194	0.0041	3.63E+08	-0.90	0.07
1531.962	1200	65275.77	5s23	5p63	1531.9592	0.0028	1.08E+09	-0.42	0.66
1533.188	700	65223.57	5s15	5p43	1533.1817	0.0032	2.77E+08	-1.01	0.07
1540.731	3	64904.26	5d11	5p33	1540.7340	0.0046	7.53E+07	-1.57	0.07
1557.043	10	64224.30	5d25	5p53	1557.0348	0.0068	1.45E+08	-1.28	0.02
(1561.446)		64043.37	5d35	5p45	1561.4460	0.0054	1.29E+05	-4.33	0.00
1561.896	12	64024.75	5d21	5p43	1561.8970	0.0037	1.02E+08	-1.43	0.04
1563.049	150	63977.52	5d23	5p53	1563.0522	0.0043	6.08E+08	-0.65	0.15
1566.381	25	63841.43	5d13	5p33	1566.3841	0.0042	1.34E+08	-1.31	0.05
1573.219	800	63563.94	4d73	5p41	1573.2175	0.0032	3.31E+08	-0.92	0.21
1576.805	400	63419.38	5s21	5p73	1576.8043	0.0032	1.47E+08	-1.26	0.66
1583.386	300	63155.79	5d55	5p63	1583.3874	0.0047	6.74E+08	-0.60	0.24
1588.810	400	62940.19	5s15	5p35	1588.8062	0.0040	1.39E+08	-1.28	0.03
1589.983	75	62893.75	6s13	5p73	1589.9818	0.0060	1.46E+07	-2.26	0.02



Table 1. Cont.

$\lambda_{\text{obs}}$ (Å)	Int <sup>a</sup>	$\sigma_{\text{obs}}$ (cm <sup>-1</sup> )	Even Level <sup>b</sup>	Odd Level <sup>b</sup>	$\lambda_{\text{Ritz}}$ (Å)	Unc (Å)	$g_{UL}$ (s <sup>-1</sup> )	$\log(g_{UL}/f)$	CFI
1594.488	3	62716.06	5d21	5p41	1594.4938	0.0039	8.65E+07	-1.48	0.06
1600.054	300	62497.89	5d21	5p53	1600.0540	0.0040	3.85E+08	-0.83	0.23
1600.662	1200	62474.15	5s13	5p53	1600.6584	0.0032	6.22E+08	-0.62	0.20
1606.264	600	62256.27	5s13	5p41	1606.2619	0.0032	2.53E+08	-1.02	0.12
1606.264	600	62256.27	4d73	5p43	1606.2936	0.0032	2.94E+07	-1.95	0.03
1606.856	200	62233.33	4d83	5p73	1606.8596	0.0030	4.72E+07	-1.73	0.04
1609.689	800	62123.80	6s33	5p83	1609.6880	0.0090	2.84E+06	-2.96	0.08
1616.245	30	61871.81	5d13	5p35	1616.2496	0.0049	7.19E+07	-1.55	0.05
1634.471	60	61181.87	5d45	5p63	1634.4717	0.0056	1.16E+08	-1.33	0.12
(1640.133)		60970.52	5s15	5p33	1640.1329	0.0037	2.31E+08	-1.03	0.28
1640.759	600	60947.40	5s13	5p43	1640.7572	0.0032	1.09E+08	-1.36	0.03
1643.670	5	60839.46	4d75	5p17	1643.6701	0.0093	9.07E+06	-2.43	0.13
1644.896	150	60794.12	5d53	5p73	1644.8973	0.0046	3.11E+08	-0.90	0.16
1648.776	20	60651.05	5d11	5p43	1648.7785	0.0053	8.11E+07	-1.48	0.05
1649.261	600	60633.22	5s21	5p63	1649.2544	0.0035	1.87E+08	-1.12	0.63
1649.378	400	60628.92	4d85	5p53	1649.3787	0.0035	1.48E+08	-1.21	0.39
(1656.458)		60369.56	5d55	5p73	1656.4576	0.0051	1.77E+08	-1.15	0.08
1659.064	5	60274.95	5s23	5p45	1659.0513	0.0038	8.14E+06	-2.47	0.01
1663.695	600	60107.17	4d41	5p33	1663.6884	0.0040	9.46E+07	-1.41	0.31
1666.513	50	60005.53	5d55	5p55	1666.5161	0.0059	3.03E+08	-0.90	0.31
1667.463	2	59971.35	4d73	5p35	1667.4554	0.0041	3.71E+07	-1.81	0.10
1668.214	60	59944.35	5d43	5p63	1668.2142	0.0042	2.16E+08	-1.04	0.13
1682.168	8	59447.09	4d83	5p63	1682.1639	0.0033	2.99E+05	-3.90	0.00
1685.140	12	59342.25	5d11	5p41	1685.1448	0.0056	4.37E+07	-1.72	0.05
1691.351	5	59124.33	5d11	5p53	1691.3565	0.0057	4.24E+07	-1.74	0.04
1691.986	500	59102.14	4d85	5p43	1691.9881	0.0036	1.68E+08	-1.13	0.20
1698.233	1500	58884.73	5s33	5p51	1698.2352	0.0042	1.51E+09	-0.19	0.69
1698.443	700	58877.45	5s15	5p23	1698.4365	0.0039	3.19E+08	-0.86	0.19
1704.624	400	58663.96	5s13	5p35	1704.6238	0.0041	1.67E+08	-1.13	0.03
1722.320	20	58061.22	5d13	5p53	1722.3173	0.0052	4.20E+07	-1.73	0.02
1722.320	20	58061.22	5d31	5p63	1722.3446	0.0057	3.80E+07	-1.77	0.08
1724.080	60	58001.95	4d73	5p33	1724.0800	0.0037	4.41E+07	-1.71	0.04
1725.009	400	57970.71	4d51	5p41	1725.0088	0.0044	1.44E+08	-1.21	0.22
1734.923	200	57639.45	4d41	5p21	1734.9226	0.0046	7.25E+07	-1.49	0.29
1759.984	500	56818.70	4d85	5p35	1759.9880	0.0046	1.57E+08	-1.13	0.49
1763.854	3	56694.03	5s13	5p33	1763.8457	0.0037	3.31E+07	-1.81	0.01

Table 1. Cont.

$\lambda_{\text{obs}}$ (Å)	Int <sup>a</sup>	$\sigma_{\text{obs}}$ (cm <sup>-1</sup> )	Even Level <sup>b</sup>	Odd Level <sup>b</sup>	$\lambda_{\text{Ritz}}$ (Å)	Unc (Å)	$g_{U/A}$ (s <sup>-1</sup> )	$\log(g_{U/A})$	CFI
1764.854	25	56661.91	4d51	5p43	1764.8562	0.0046	7.38E+07	-1.47	0.18
1767.320	12	56382.85	5d53	5p51	1767.3212	0.0056	9.91E+07	-1.34	0.05
1773.897	400	56373.06	5s13	5p31	1773.8929	0.0042	1.80E+08	-1.07	0.17
1776.577	600	56288.02	5s11	5p53	1776.5732	0.0042	4.41E+08	-0.68	0.37
1783.481	200	56070.12	5s11	5p41	1783.4786	0.0042	1.54E+08	-1.14	0.50
1788.622	50	55908.96	4d73	5p23	1788.6221	0.0039	2.19E+08	-0.98	0.34
1800.697	35	55534.05	4d73	5p21	1800.6987	0.0043	5.29E+07	-1.60	0.08
1801.507	2000	55509.08	5s25	5p55	1801.5093	0.0054	4.44E+09	0.34	0.76
1813.410	1000	55144.73	5s25	5p73	1813.4129	0.0044	9.62E+08	-0.32	0.81
(1816.934)		55038.23	5s33	5p55	1816.9341	0.0056	1.00E+09	-0.30	0.85
1823.186	200	54849.04	4d85	5p33	1823.1906	0.0042	1.32E+08	-1.18	0.12
1826.103	1800	54761.42	5s11	5p43	1826.1065	0.0043	1.31E+09	-0.18	0.75
1829.037	2000	54673.58	5s33	5p73	1829.0430	0.0045	2.44E+09	0.09	0.64
1830.236	1500	54637.76	5s23	5p53	1830.2378	0.0039	7.41E+08	-0.43	0.35
1831.453	3000	54601.46	5s13	5p23	1831.4579	0.0039	1.94E+09	-0.01	0.57
1836.654	20	54446.84	4d83	5p45	1836.6566	0.0045	1.70E+08	-1.06	0.57
1837.566	300	54419.81	5s23	5p41	1837.5675	0.0039	1.64E+08	-1.09	0.15
1866.128	5	53586.89	5d25	5p63	1866.1431	0.0098	7.76E+07	-1.39	0.05
1874.773	3	53339.79	5d23	5p63	1874.7934	0.0063	6.94E+07	-1.44	0.04
1882.840	250	53111.26	5s23	5p43	1882.8530	0.0040	1.61E+08	-1.07	0.07
1888.675	2	52947.17	5d43	5p51	1888.6765	0.0057	4.22E+07	-1.65	0.04
1895.509	300	52756.28	4d85	5p23	1895.5222	0.0044	7.02E+07	-1.41	0.13
1896.139	30000	52738.75	5s15	5p17	1896.1404	0.0076	6.28E+09	0.53	0.96
1902.748	1	52555.57	5s15	5p25	1902.7475	0.0054	1.79E+07	-2.01	0.01
1909.897	1500	52358.84	5s25	5p63	1909.9026	0.0048	1.24E+09	-0.17	0.42
1919.844	25	52087.57	4d51	5p31	1919.8442	0.0058	9.34E+07	-1.30	0.45
1927.247	1500	51887.49	5s33	5p63	1927.2483	0.0050	8.58E+08	-0.32	0.47
1929.191	1500	51835.20	5s31	5p83	1929.1910	0.0133	2.92E+09	0.21	0.96
1967.435	5000	50827.60	5s23	5p35	1967.4431	0.0053	4.06E+09	0.37	0.96
1979.871	500	50508.34	5s11	5p33	1979.8785	0.0050	5.20E+08	-0.51	0.47
1981.092	20	50477.21	4d41	5p11	1981.0991	0.0060	4.85E+07	-1.55	0.30
1992.386	500	50191.08	5d23	5p55	1992.3903	0.0165	2.37E+06	-2.85	0.01
1992.546	1200	50187.05	5s11	5p31	1992.5463	0.0056	1.11E+09	-0.18	0.86
2008.655	5000	49784.56	5s25	5p27	2008.6537	0.0075	5.31E+09	0.51	0.97
2008.939	1200	49777.52	5s21	5p41	2008.9462	0.0049	9.32E+08	-0.26	0.92
2016.657	4	49587.01	4d73	5p25	2016.6633	0.0056	3.60E+07	-1.67	0.12

Table 1. Cont.

$\lambda_{\text{obs}}$ (Å)	Int <sup>a</sup>	$\sigma_{\text{obs}}$ (cm <sup>-1</sup> )	Even Level <sup>b</sup>	Odd Level <sup>b</sup>	$\lambda_{\text{Ritz}}$ (Å)	Unc (Å)	$g_{\text{UL}}A$ (s <sup>-1</sup> )	$\log(g_{\text{L}}/f)$	CFI
2046.757	1500	48857.78	5s23	5p33	2046.7594	0.0047	1.40E+09	-0.06	0.68
2048.791	8	48809.27	4d83	5p53	2048.8000	0.0048	4.94E+07	-1.50	0.20
2057.983	20	48591.27	4d83	5p41	2057.9892	0.0047	4.55E+07	-1.54	0.11
2060.302	12	48536.57	5s23	5p31	2060.3005	0.0054	5.08E+07	-1.49	0.08
2063.186	1500	48468.73	5s21	5p43	2063.1974	0.0051	1.02E+09	-0.19	0.88
2067.325	20	48371.69	4d73	5p11	2067.3300	0.0057	4.43E+05	-3.56	0.00
2071.281	5000	48279.30	5s13	5p25	2071.2849	0.0057	3.56E+09	0.36	0.96
2079.377	8000	48091.33	5s15	5p15	2079.3838	0.0084	3.53E+09	0.36	0.93
2094.038	4000	47754.63	5s15	5p13	2094.0466	0.0064	1.75E+09	0.06	0.89
2111.562	1200	47358.31	5s25	5p45	2111.5663	0.0065	6.65E+08	-0.35	0.95
2112.086	1	47346.56	5d63	5p83	2112.0917	0.0124	6.57E+07	-1.36	0.22
2114.962	8	47282.17	4d83	5p43	2114.9590	0.0049	2.42E+07	-1.79	0.07
2124.761	3000	47064.12	5s13	5p11	2124.7699	0.0057	1.02E+09	-0.17	0.88
2132.594	20	46891.25	4d41	5p13	2132.5977	0.0071	2.17E+07	-1.83	0.18
2132.785	1200	46887.05	5s23	5p45	2132.7887	0.0068	2.62E+09	0.26	0.77
2138.358	15	46764.85	4d85	5p23	2138.3637	0.0050	4.77E+06	-2.49	0.00
2153.595	1200	46433.99	4d85	5p25	2153.6032	0.0064	1.63E+08	-0.93	0.55
2155.636	2400	46390.02	5s23	5p21	2155.6477	0.0057	9.32E+08	-0.19	0.92
2222.293	1	44998.57	4d83	5p35	2222.2844	0.0066	6.15E+06	-2.33	0.15
2261.667	100	44215.17	5s21	5p33	2261.6611	0.0061	1.91E+07	-1.84	0.06
2278.201	100	43894.28	5s21	5p31	2278.2064	0.0069	1.15E+07	-2.05	0.10
2300.017	3000	43477.94	5s13	5p13	2300.0106	0.0069	3.20E+08	-0.60	0.32
2374.041	400	42122.27	5s21	5p23	2374.0394	0.0066	1.24E+08	-0.98	0.18
2395.369	150	41747.22	5s21	5p21	2395.3622	0.0074	5.30E+07	-1.34	0.18
2401.966	5	41632.56	4d85	5p13	2401.9604	0.0079	1.70E+07	-1.82	0.08
2424.306	5	41248.92	5s33	5p53	2424.2853	0.0077	9.67E+06	-2.07	0.06
2437.169	400	41031.21	5s33	5p41	2437.1620	0.0077	1.06E+08	-1.04	0.43
2442.837	12	40936.01	4d83	5p23	2442.8328	0.0063	1.75E+07	-1.80	0.08
2446.321	300	40877.71	5s11	5p11	2446.3174	0.0081	3.70E+07	-1.48	0.21
2465.420	3	40561.04	4d83	5p21	2465.4152	0.0072	8.56E+06	-2.11	0.03
2472.650	400	40442.44	5s23	5p25	2472.6384	0.0077	6.44E+07	-1.23	0.03
2487.961	400	40193.56	5s25	5p43	2487.9527	0.0077	1.38E+08	-0.89	0.32
2549.253	1	39227.18	5s23	5p11	2549.2424	0.0079	9.27E+06	-2.05	0.02

<sup>a</sup> Symbols; dc, doubly classified; p, perturbed; u, unresolved from close line; s, shaded to shorter wavelength; l, shaded to longer wavelength; x, not included in level optimization; d, double line; c, complex. A, blended or obscured by Y, V1; B, perturbed by O II; C, perturbed by Si IV; D, intensity much higher than expected; E, perturbed by second order line; F, perturbed ghost of Si IV line; G, perturbed by Si IV; H, uncertain stage of ionization; J, perturbed by Y III; K, perturbed by Si II; L, perturbed by C I; M, perturbed by unknown impurity. <sup>b</sup> Level codes are explained in Table 2.

### 3. Spectrum Analysis and Level Values

The analysis was carried out in a manner similar to that used for the recent analysis of Mo V [11]. As described there “Interpretation of the spectrum was guided by calculations of the level structures and transition probabilities with the Hartree-Fock code of Cowan [12]. Further guidance was provided by construction of two-dimensional transition arrays with the computer spreadsheet method described by Reader [13].”

The odd parity energy levels are given in Table 2, the even levels in Table 3. In addition to the usual spectroscopic designations in either LS or  $J_1I$  (pair) coupling, the levels are given shorthand designations that are used in the classification of the spectral lines. The shorthand designations are explained in the footnotes to Tables 2 and 3. As described in [11] “The values of the energy levels were optimized with the computer program ELCALC, an iterative procedure in which the observed wave numbers are weighted according to the inverse square of their uncertainties. The uncertainties of the level values given by this procedure are also listed.” (The program ELCALC was written by L. J. Radziemski of the Research Corporation, Tucson, Arizona 85712. The procedure and definition of level value uncertainties have been described by Radziemski and Kaufman [14].) For the level optimization only the most reliably classified lines were used. That is, lines that were very weak or that appeared with suspiciously high intensities were excluded.

Figure 1 shows a schematic overview of the positions of the  $4s^24p^5$ ,  $4s4p^6$ ,  $4s^24p^44d$ ,  $5s$ ,  $5p$ ,  $5d$ , and  $6s$ , configurations. It also shows the calculated positions of the  $4s^24p^44f$  and  $4s4p^54d$  configurations.

Table 2. Odd parity levels ( $\text{cm}^{-1}$ ) of Y V.

Configuration	Term	$J$	Desig. <sup>a</sup>	Energy	Uncert.	No. Trans.
$4s^24p^5$	$^2P$	3/2	p5 3	0.00	0.86	70
		1/2	p5 1	12460.12	1.05	46
$4s^24p^45p$	$(^3P_2)[1]$	3/2	5p13	341856.85	0.09	26
	$(^3P_2)[2]$	5/2	5p15	342193.59	0.16	23
	$(^3P_2)[1]$	1/2	5p11	345442.71	0.09	24
	$(^3P_2)[3]$	5/2	5p25	346658.00	0.10	26
	$(^3P_2)[3]$	7/2	5p17	346841.13	0.18	13
	$(^3P_1)[0]$	1/2	5p21	352605.14	0.09	20
	$(^3P_2)[2]$	3/2	5p23	352980.10	0.07	31
	$(^3P_0)[1]$	1/2	5p31	354751.98	0.10	21
	$(^3P_1)[2]$	3/2	5p33	355073.09	0.08	41
	$(^3P_1)[2]$	5/2	5p35	357042.76	0.11	29
	$(^3P_0)[1]$	3/2	5p43	359326.26	0.08	40
	$(^3P_1)[1]$	1/2	5p41	360635.14	0.08	25
	$(^3P_1)[1]$	3/2	5p53	360853.08	0.09	39
	$(^1D_2)[3]$	5/2	5p45	366490.78	0.11	22
	$(^1D_2)[3]$	7/2	5p27	368917.16	0.16	14
	$(^1D_2)[1]$	3/2	5p63	371491.26	0.09	30
	$(^1D_2)[2]$	3/2	5p73	374277.21	0.09	31
	$(^1D_2)[2]$	5/2	5p55	374641.58	0.14	23
$(^1D_2)[1]$	1/2	5p51	378488.47	0.11	19	
$(^1S_0)[1]$	1/2	5p61	395993.26	0.30	5	
$(^1S_0)[1]$	3/2	5p83	397637.50	0.22	13	

<sup>a</sup> Designations are given with a short form of the configuration (two places) followed by the ordinal number of the calculated  $J$ -value for the configuration (one place) and the  $J$  value (one place). For example, 5p73 indicates the seventh level with  $J = 3$  for the  $4p^45p$  configuration. p5 3 and p5 1 indicate the  $J = 3/2$  and  $1/2$  levels of the  $4p^5$  configuration, respectively.

Table 3. Even parity energy levels (cm<sup>-1</sup>) of Y V.

Configuration	Term	<i>J</i>	Desig. <sup>a</sup>	Energy	Uncert.	No. Trans.
4s4p <sup>6</sup>	<sup>2</sup> S	1/2	4p61	170945.58	0.95	8
4s <sup>2</sup> 4p <sup>4</sup> 4d	<sup>3</sup> P <sup>4</sup> D	5/2	4d15	218417.13	0.51	9
	<sup>3</sup> P <sup>4</sup> D	7/2	4d17	218556.80	0.64	4
	<sup>3</sup> P <sup>4</sup> D	3/2	4d13	219373.81	0.45	11
	<sup>3</sup> P <sup>4</sup> D	1/2	4d11	220794.66	0.78	10
	<sup>3</sup> P <sup>4</sup> F	9/2	4d19	229786.64	0.98	1
	<sup>3</sup> P <sup>4</sup> F	7/2	4d27	233703.76	0.46	7
	<sup>1</sup> D <sup>2</sup> P	1/2	4d21	233712.36	0.37	12
	<sup>3</sup> P <sup>4</sup> F	5/2	4d25	237677.66	0.37	10
	<sup>3</sup> P <sup>4</sup> F	3/2	4d23	238215.09	0.37	16
	<sup>3</sup> P <sup>4</sup> P	1/2	4d31	238898.28	0.40	11
	<sup>3</sup> P <sup>4</sup> P	3/2	4d33	239132.83	0.30	18
	<sup>1</sup> D <sup>2</sup> D	3/2	4d43	240949.32	0.34	12
	<sup>3</sup> P <sup>2</sup> F	7/2	4d37	242336.33	0.54	6
	<sup>3</sup> P <sup>4</sup> P	5/2	4d35	244311.56	0.32	11
	<sup>1</sup> D <sup>2</sup> P	3/2	4d53	244613.24	0.31	15
	<sup>1</sup> D <sup>2</sup> D	5/2	4d45	247861.17	0.34	11
	<sup>1</sup> D <sup>2</sup> G	7/2	4d47	250882.71	0.46	4
	<sup>1</sup> D <sup>2</sup> G	9/2	4d29	251052.40	0.99	1
	<sup>3</sup> P <sup>2</sup> F	5/2	4d55	251403.88	0.38	9
	<sup>1</sup> D <sup>2</sup> F	5/2	4d65	263184.02	0.26	10
	<sup>1</sup> D <sup>2</sup> F	7/2	4d57	266196.75	0.38	6
	<sup>1</sup> S <sup>2</sup> D	3/2	4d63	281244.51	0.25	9
	<sup>1</sup> S <sup>2</sup> D	5/2	4d75	286001.66	0.29	6
<sup>1</sup> D <sup>2</sup> S	1/2	4d41	294965.68	0.12	8	
<sup>3</sup> P <sup>2</sup> P	3/2	4d73	297071.14	0.10	14	
<sup>3</sup> P <sup>2</sup> D	5/2	4d85	300224.19	0.10	13	
<sup>3</sup> P <sup>2</sup> P	1/2	4d51	302664.42	0.12	7	
<sup>3</sup> P <sup>2</sup> D	3/2	4d83	312044.02	0.08	13	
4s <sup>2</sup> 4p <sup>4</sup> 5s	<sup>3</sup> P <sub>2</sub> [2]	5/2	5s15	294102.42	0.11	12
	<sup>3</sup> P <sub>2</sub> [2]	3/2	5s13	298378.79	0.09	17
	<sup>3</sup> P <sub>0</sub> [0]	1/2	5s11	304564.94	0.10	9
	<sup>3</sup> P <sub>1</sub> [1]	3/2	5s23	306215.37	0.08	16
	<sup>3</sup> P <sub>1</sub> [1]	1/2	5s21	310857.80	0.09	11
	<sup>1</sup> D <sub>2</sub> [2]	5/2	5s25	319132.57	0.10	8
	<sup>1</sup> D <sub>2</sub> [2]	3/2	5s33	319603.81	0.10	11
<sup>1</sup> S <sub>0</sub> [0]	1/2	5s31	345802.30	0.29	3	
4s <sup>2</sup> 4p <sup>4</sup> 5d	<sup>3</sup> P <sub>2</sub> [3]	7/2	5d17	418265.33	0.27	3
	<sup>3</sup> P <sub>2</sub> [2]	5/2	5d15	418310.18	0.44	2
	<sup>3</sup> P <sub>2</sub> [2]	3/2	5d13	418914.39	0.15	9
	<sup>3</sup> P <sub>2</sub> [1]	1/2	5d11	419977.22	0.18	7
	<sup>3</sup> P <sub>2</sub> [4]	9/2	5d19	420403.65	0.42	1
	<sup>3</sup> P <sub>2</sub> [4]	7/2	5d27	421426.57	0.28	3
	<sup>3</sup> P <sub>2</sub> [0]	1/2	5d21	423350.97	0.13	10
	<sup>3</sup> P <sub>2</sub> [1]	3/2	5d23	424830.47	0.16	13
	<sup>3</sup> P <sub>2</sub> [3]	5/2	5d25	425077.72	0.27	8
	<sup>3</sup> P <sub>1</sub> [1]	1/2	5d31	429551.65	0.17	10
	<sup>3</sup> P <sub>0</sub> [2]	3/2	5d33	430343.90	0.17	9
	<sup>3</sup> P <sub>0</sub> [2]	5/2	5d35	430533.98	0.19	9
	<sup>3</sup> P <sub>1</sub> [3]	7/2	5d37	430760.23	0.68	2
	<sup>3</sup> P <sub>1</sub> [1]	3/2	5d43	431435.60	0.12	11
	<sup>3</sup> P <sub>1</sub> [2]	5/2	5d45	432673.11	0.19	7
	<sup>3</sup> P <sub>1</sub> [3]	5/2	5d55	434647.00	0.16	10
	<sup>3</sup> P <sub>1</sub> [2]	3/2	5d53	435071.28	0.14	9
	<sup>1</sup> D <sub>2</sub> [4]	7/2	5d47	442365.90	0.30	3
	<sup>1</sup> D <sub>2</sub> [4]	9/2	5d29	442704.55	0.41	1
	<sup>1</sup> D <sub>2</sub> [0]	1/2	5d41	444128.77	0.18	9
	<sup>1</sup> D <sub>2</sub> [1]	3/2	5d63	444983.93	0.18	13
	<sup>1</sup> D <sub>2</sub> [2]	5/2	5d65	445299.76	0.20	7

Table 3. Cont.

Configuration	Term	<i>J</i>	Desig. <sup>a</sup>	Energy	Uncert.	No. Trans.
	( <sup>1</sup> D <sub>2</sub> )[3]	7/2	5d57	446600.43	0.29	3
	( <sup>1</sup> D <sub>2</sub> )[3]	5/2	5d75	446709.00	0.22	6
	( <sup>1</sup> D <sub>2</sub> )[1]	1/2	5d51	447277.48	0.22	6
	( <sup>1</sup> D <sub>2</sub> )[2]	3/2	5d73	448357.54	0.24	8
	( <sup>1</sup> S <sub>0</sub> )[2]	5/2	5d85	470989.78	0.43	2
	( <sup>1</sup> S <sub>0</sub> )[2]	3/2	5d83	471484.11	0.35	5
4s <sup>2</sup> 4p <sup>4</sup> 6s	( <sup>3</sup> P <sub>2</sub> )[2]	5/2	6s15	435670.71	0.23	10
	( <sup>3</sup> P <sub>2</sub> )[2]	3/2	6s13	437171.00	0.22	13
	( <sup>3</sup> P <sub>0</sub> )[0]	1/2	6s11	446209.20	0.32	7
	( <sup>3</sup> P <sub>1</sub> )[1]	3/2	6s23	446718.25	0.29	8
	( <sup>3</sup> P <sub>1</sub> )[1]	1/2	6s21	448774.76	0.36	7
	( <sup>1</sup> D <sub>2</sub> )[2]	5/2	6s25	459636.57	0.63	5
	( <sup>1</sup> D <sub>2</sub> )[2]	3/2	6s33	459761.34	0.27	6
	( <sup>1</sup> S <sub>0</sub> )[0]	1/2	6s31	486067.68	0.58	5
4s <sup>2</sup> 4p <sup>4</sup> 6d	( <sup>3</sup> P <sub>2</sub> )[3]	5/2	6d25 <sup>c</sup>	493116	49	1
	( <sup>3</sup> P <sub>2</sub> )[1]	3/2	6d23 <sup>b</sup>	493146	16	2
	( <sup>3</sup> P <sub>1</sub> )[1]	3/2	6d43 <sup>c</sup>	501351	75	1
	( <sup>3</sup> P <sub>1</sub> )[3]	5/2	6d55 <sup>c</sup>	503137	18	1
	( <sup>3</sup> P <sub>1</sub> )[2]	3/2	6d53 <sup>b</sup>	503788	12	2
	( <sup>1</sup> D <sub>2</sub> )[0]	1/2	6d41 <sup>b</sup>	514253	13	2
	( <sup>1</sup> D <sub>2</sub> )[2]	3/2	6d73 <sup>b</sup>	515011	16	2
	( <sup>1</sup> D <sub>2</sub> )[2]	5/2	6d65 <sup>c</sup>	515762	19	1
	( <sup>1</sup> D <sub>2</sub> )[1]	1/2	6d51 <sup>b</sup>	515882	13	2
	( <sup>1</sup> S <sub>0</sub> )[2]	3/2	6d83 <sup>b</sup>	543052	14	2
4s <sup>2</sup> 4p <sup>4</sup> 7s	( <sup>3</sup> P <sub>2</sub> )[2]	5/2	7s15 <sup>c</sup>	498271	74	1
	( <sup>3</sup> P <sub>2</sub> )[2]	3/2	7s13 <sup>b</sup>	499020	12	2
	( <sup>3</sup> P <sub>1</sub> )[1]	3/2	7s23 <sup>c</sup>	509051	18	1
	( <sup>3</sup> P <sub>1</sub> )[1]	1/2	7s21 <sup>b</sup>	509817	13	2
	( <sup>1</sup> D <sub>2</sub> )[2]	5/2	7s25 <sup>c</sup>	522000	19	1
	( <sup>1</sup> D <sub>2</sub> )[2]	3/2	7s33 <sup>c</sup>	522129	18	1
	( <sup>1</sup> S <sub>0</sub> )[0]	1/2	7s31 <sup>c</sup>	544803	20	1

<sup>a</sup> Designations are explained in Table 2; 4p61 indicates the *J* = 1/2 level of 4s4p<sup>6</sup>; <sup>b</sup> Tentative designation; not included in LSF; <sup>c</sup> Tentative level with tentative designation; not included in LSF.

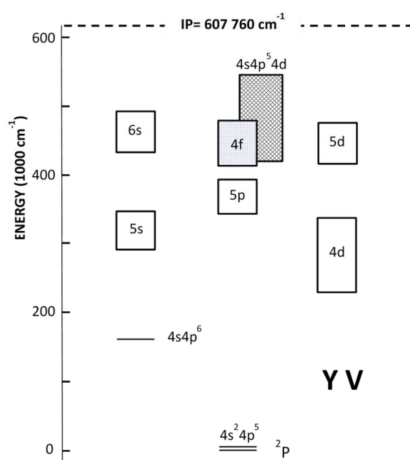


Figure 1. Schematic overview of the observed configurations of Y V. The calculated positions of the 4s<sup>2</sup>4p<sup>4</sup>4f and 4s4p<sup>5</sup>4d configurations are also shown.

### 3.1. $4s^2 4p^4 4d$ Levels

Nearly all levels of this configuration were given in [4]. Remaining as unknown were  $(^3P)^4D_{1/2,7/2}$ ,  $(^3P)^4F_{7/2,9/2}$ ,  $(^3P)^2F_{7/2}$ ,  $(^1D)^2G_{7/2,9/2}$ , and  $(^1D)^2F_{7/2}$ . These levels have now been established based on their transitions to  $4p^4 5p$ . All values for these levels reported in [6] are spurious.

The  $4p^4 4d$   $(^3P)^4F_{9/2}$  (4d19) and  $(^1D)^2G_{9/2}$  (4d29) levels are necessarily based on only a single transition. However, the lines assigned to these transitions are both very strong and place the  $J = 9/2$  levels close to their predicted positions. There is no doubt as to their identifications.

The structure of the  $4p^4 4d$  configuration is shown in Figure 2. This is similar to Figure 1 of [4], except that we show here the observed positions of levels that were previously unknown.

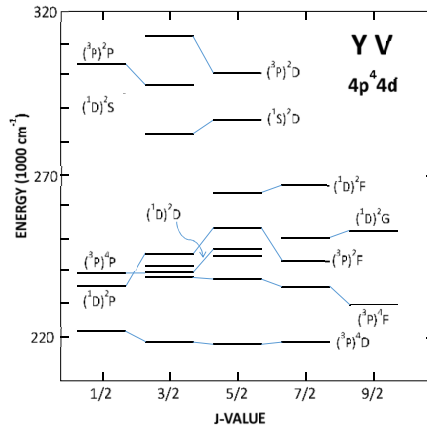


Figure 2. Structure of the  $4s^2 4p^4 4d$  configuration of Y V.

### 3.2. $4s^2 4p^4 5s$ Levels

The levels of the  $4s^2 4p^4 5s$  configuration, which were complete in [4], have improved values as a result of their combinations with  $4p^4 5p$ . In Figure 3 we give the structure of the  $4p^4 5s$  configuration. This is the same as Figure 2 of [4], except that here we designate the levels in  $J_1$ -coupling, rather than  $J_1 j$ -coupling.

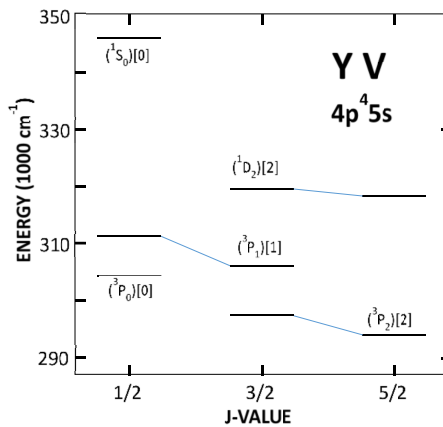


Figure 3. Structure of the  $4s^2 4p^4 5s$  configuration of Y V.

### 3.3. $4s^2 4p^4 5p$ Levels

All levels of this configuration have been located. Of the 21 levels of this configuration given in [6], only three could be confirmed ( $345444$ ,  $360851$ , and  $374278 \text{ cm}^{-1}$ ). The levels at  $342193$  and  $355076 \text{ cm}^{-1}$  were confirmed, but were found to have incorrect  $J$ -values. The structure of the  $4p^4 5p$  levels is shown in Figure 4. The levels are designated in  $J_1 l$ -coupling.

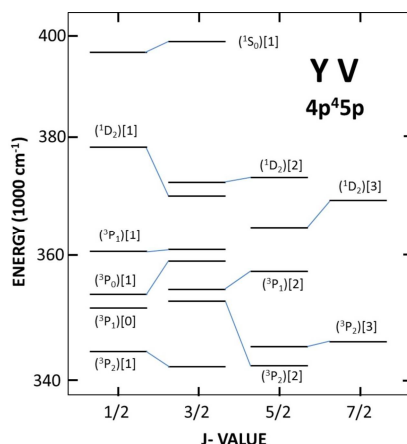


Figure 4. Structure of the  $4s^2 4p^4 5p$  configuration of Y V.

### 3.4. $4s^2 4p^4 5d$ and $4s^2 4p^4 6s$ Levels

The  $4p^4 5d$  and  $6s$  configurations lie very close in energy and are treated together. The levels are shown in Figure 5; they are designated in  $J_1 l$ -coupling. As with  $4p^4 4d$ , the  $J = 9/2$  levels could be established by only a single line. However, there is little doubt as to the identifications. A few of the levels of these configurations given in [5] could be confirmed, although some of the  $J$ -values and configuration assignments had to be revised. All of the  $4p^4 5d$  levels of [6] were found to be spurious.

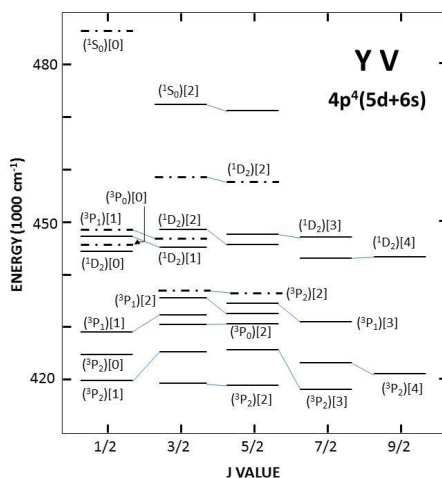


Figure 5. Structures of the  $4s^2 4p^4 5d$  and  $4s^2 4p^4 6s$  configurations of Y V. The  $4s^2 4p^4 6s$  levels are shown as dashed.



### 3.5. $4s^24p^46d$ and $4s^24p^47s$ Levels

Based on our calculations, we were able to assign a number of low wavelength lines with clear Y V character as transitions to the ground term from levels of  $4p^46d$  and  $7s$ . For pairs of lines with wave number differences that closely match the  $4p^5\ ^2P$  interval, the implied levels are relatively certain. However, the designations are considered to be tentative. Where the levels are based on single transitions, the line and level identifications are even less certain. None of these levels were included in the least-squares-fits, described below.

None of the information for the  $4p^5\text{-}4p^46d$ ,  $7s$  transitions and  $4p^46d,7s$  levels of Zahid-Ali et al. [5] could be confirmed.

### 3.6. $4s^24p^44f$ and $4s4p^54d$ Configurations

Extensive efforts to find levels of these configurations were not successful. Levels of  $4p^44f$  were given in [6], but it is almost certain that all of them are spurious.

## 4. Theoretical Interpretation

### 4.1. Odd Parity Configurations

As in [11] “The observed configurations were interpreted theoretically by making least-squares fits of the energy parameters to the observed levels with the Cowan suite of codes, RCN (Hartree-Fock), RCG (energy matrix diagonalization), and RCE (least-squares parameter fitting) [12]. The Hartree-Fock code was run in a relativistic mode (HFR) with a correlation term in the potential. Breit energies were not included. For the initial calculations the HFR values were scaled by factors of 0.85 for the direct electrostatic parameters  $F^k$ , the exchange electrostatic parameters  $G^k$ , and the configuration interaction parameters  $R^k$ .” The odd configurations  $4s^24p^5$ ,  $4s^24p^45p$ ,  $4s^24p^44f$ , and  $4s4p^54d$  were treated as a single group.

The Hartree-Fock and least-squares fitted parameters for the odd configurations are given in Table 4. For these calculations, the  $4p^45p$  exchange electrostatic parameters,  $G^0(4p5p)$  and  $G^2(4p5p)$ , were linked at their HFR ratio. The LSF/HFR ratio of 0.836 is satisfactory. The configuration interaction (CI) parameters for the  $4s^24p^5\text{-}4s^24p^45p$  interaction were held fixed at their scaled HFR values. All other CI parameters and parameters for  $4s^24p^44f$  and  $4s4p^54d$  were fixed at their scaled HFR values. The value of the effective interaction parameter  $\alpha(4p4p)$  for the  $4p^45p$  configuration was fixed at the value observed for the  $4p^4$  core of Y VI [7]. In Table 4, only values for the observed configurations  $4s^24p^5$  and  $4s^24p^45p$  are given.

**Table 4.** Hartree-Fock and least-squares fitted parameters for the odd configurations of Y V. Mean error of fit  $179\text{ cm}^{-1}$ .

Configuration	Parameter	HFR	LSF	Unc.	LSF/HFR
$4s^24p^5$	$E_{av}(4s^24p^5)$	8182	8400	134	
	$\zeta_{4p}$	7941	8369	170	1.054
$4s^24p^45p$	$E_{av}(4s^24p^45p)$	364894	360966	40	0.989
	$F^2(4p4p)$	78434	65400	358	0.834
	$\alpha(4p4p)$		$-56^a$		
	$\zeta_{4p}$	8458	8679	108	1.026
	$\zeta_{5p}$	1688	2016	85	1.194
	$F^2(4p5p)$	22406	20623	364	0.920
	$G^0(4p5p)$	4773	3988 <sup>b</sup>	49	0.836
	$G^2(4p5p)$	6387	5337 <sup>b</sup>	66	0.836
Config. Interaction $4s^24p^5\text{-}4s^24p^45p$	$R^0(4p4p,4p5p)$	2217	1885 <sup>c</sup>		0.850
	$R^2(4p4p,4p5p)$	10661	9062 <sup>c</sup>		0.850

<sup>a</sup> Fixed at value from  $4p^4$  of Y VI [7]; <sup>b</sup> Linked in LSF fit; <sup>c</sup> Fixed at scaled HFR value.

The calculated level values and eigenvector compositions for the odd configurations are given in Table 5. This table gives the percentage compositions for the three leading eigenvector states in LS-coupling and the percentage for the leading eigenvector state in  $J_1I$ -coupling. As can be seen there is not much mixing between the  $4s^24p^5$  and the  $4s^24p^45p$  configurations, and  $4s^24p^45p$  has essentially no mixture of either  $4s^24p^4f$  or  $4s4p^54d$ .

**Table 5.** Calculated energy levels ( $\text{cm}^{-1}$ ) and percentage compositions for the odd levels of Y V.

$J$	Observed	Calculated	O–C	% $J_1I$	Percentage Composition (LS-Coupling)															
3/2	0	0	0	99%	$4p^5$	$(^1S)^2P$														
1/2	12460	12460	0	99%	$4p^5$	$(^1S)^2P$	1%	$4s4p^54d$	$(^1P)^2P$											
3/2	341857	341900	-43	41%	$(^3P_2)[1]$	$(^3P)^4P$	9%	$4p^45p$	$(^3P)^4S$	8%	$4p^45p$	$(^1D)^2P$								
5/2	342194	342140	54	83%	$(^3P_2)[2]$	$(^3P)^4P$	21%	$4p^45p$	$(^3P)^4D$	3%	$4p^45p$	$(^1D)^2D$								
1/2	345443	345735	-292	55%	$(^3P_2)[1]$	$(^3P)^4P$	21%	$4p^45p$	$(^3P)^2P$	17%	$4p^45p$	$(^1D)^2P$								
5/2	346658	346626	32	78%	$(^3P_2)[3]$	$(^3P)^4P$	62%	$4p^45p$	$(^3P)^2D$	16%	$4p^45p$	$(^3P)^4D$	12%	$4p^45p$	$(^3P)^4P$					
7/2	346841	346682	159	92%	$(^3P_2)[3]$	$(^3P)^4D$	92%	$4p^45p$	$(^3P)^4D$	8%	$4p^45p$	$(^1D)^2F$								
1/2	352605	352708	-103	59%	$(^3P_1)[0]$	$(^3P)^4P$	37%	$4p^45p$	$(^3P)^4P$	22%	$4p^45p$	$(^3P)^2P$	17%	$4p^45p$	$(^3P)^4D$					
3/2	352980	352884	96	36%	$(^3P_2)[2]$	$(^3P)^4D$	35%	$4p^45p$	$(^3P)^4D$	24%	$4p^45p$	$(^3P)^2D$	18%	$4p^45p$	$(^3P)^2P$					
1/2	354752	354622	130	62%	$(^3P_1)[1]$	$(^3P)^4D$	70%	$4p^45p$	$(^3P)^4D$	11%	$4p^45p$	$(^3P)^4P$	10%	$4p^45p$	$(^3P)^2S$					
3/2	355073	355061	12	35%	$(^3P_1)[2]$	$(^3P)^4D$	47%	$4p^45p$	$(^3P)^4P$	35%	$4p^45p$	$(^3P)^2P$	9%	$4p^45p$	$(^1D)^2P$					
5/2	357043	356868	175	95%	$(^3P_1)[2]$	$(^3P)^4D$	59%	$4p^45p$	$(^3P)^4D$	27%	$4p^45p$	$(^3P)^2D$	13%	$4p^45p$	$(^3P)^4P$					
3/2	359326	359369	-43	70%	$(^3P_0)[1]$	$(^3P)^4P$	29%	$4p^45p$	$(^3P)^2D$	25%	$4p^45p$	$(^3P)^2P$	15%	$4p^45p$	$(^3P)^4P$					
3/2	360853	360766	87	65%	$(^3P_1)[1]$	$(^3P)^4S$	41%	$4p^45p$	$(^3P)^2D$	5%	$4p^45p$	$(^3P)^4P$								
1/2	360635	361119	-484	61%	$(^3P_1)[1]$	$(^3P)^4S$	14%	$4p^45p$	$(^3P)^2S$	14%	$4p^45p$	$(^3P)^2P$	6%	$4p^45p$	$(^3P)^4D$					
5/2	366491	366367	124	87%	$(^1D_2)[3]$	$(^1D)^2F$	7%	$4p^45p$	$(^3P)^2D$	4%	$4p^45p$	$(^1D)^2D$								
7/2	368917	368795	122	91%	$(^1D_2)[3]$	$(^1D)^2F$	8%	$4p^45p$	$(^3P)^4D$											
3/2	371491	371556	-65	62%	$(^1D_2)[1]$	$(^1D)^2P$	17%	$4p^45p$	$(^1D)^2D$	11%	$4p^45p$	$(^3P)^2P$								
3/2	374277	374172	105	76%	$(^1D_2)[2]$	$(^1D)^2D$	16%	$4p^45p$	$(^3P)^2P$	7%	$4p^45p$	$(^1D)^2P$								
5/2	374642	374641	1	92%	$(^1D_2)[2]$	$(^1D)^2D$	3%	$4p^45p$	$(^1D)^2F$	2%	$4p^45p$	$(^3P)^4P$								
1/2	378488	378486	2	64%	$(^1D_2)[1]$	$(^1D)^2P$	34%	$4p^45p$	$(^3P)^2P$	1%	$4p^45p$	$(^3P)^2S$								
1/2	395993	395986	7	84%	$(^1S_0)[1]$	$(^1S)^2P$	6%	$4p^45p$	$(^3P)^2P$	5%	$4p^45p$	$(^3P)^4D$								
3/2	397637	397712	-75	86%	$(^1S_0)[1]$	$(^1S)^2P$	3%	$4p^45p$	$(^3P)^2D$	3%	$4p^45p$	$(^3P)^4D$								

4.2. Even Parity Configurations

The parameters for the even configurations are given in Table 6. Here, the  $4s4p^6$ ,  $4p^44d$ ,  $5s$ ,  $5d$ ,  $6s$ ,  $6d$ , and  $7s$  configurations were treated as single group. For the initial calculations the HFR values were scaled by factors of 0.85 for the direct electrostatic parameters  $F^k$ , the exchange electrostatic parameters  $G^k$ , and the configuration interaction parameters  $R^k$ . All the parameters that were allowed to vary were well defined in the fit and have reasonable ratios to the HFR values. The exchange parameters  $G^1(4p5d)$  and  $G^3(4p5d)$  were linked at their HFR ratio. The CI parameters for the  $4s4p^6-4s^24p^44d$  and  $4s4p^6-4s^24p^45d$  interactions were also linked at their HFR ratio. The fitted values are reasonable. The other CI parameters and all of the parameters for  $4p^46d$  and  $4p^47s$  were held fixed at their scaled HFR values. As described in [4] the interaction of  $4s4p^6\ ^2S_{1/2}$  with the  $4s^24p^44d\ (^1D)^2S$  level is great, with a mutual repulsion of  $\sim 31,000\ \text{cm}^{-1}$ . On the other hand, interaction between  $4s4p^6$  and  $4s^24p^45d$  is negligible. The value of the effective interaction parameter  $\alpha(4p4p)$  for the  $4p^44d$ ,  $5s$ ,  $5d$ , and  $6s$  configurations was again fixed at the value observed for the  $4p^4$  core of Y VI [7]. The calculated level values and eigenvector compositions for the even levels are given in Table 7. This table gives the percentage compositions for the three leading eigenvector states in LS-coupling and the percentage for the leading eigenvector state in  $J_1I$ -coupling, where appropriate. As can be seen, the purity of the states of the  $4p^44d$  configuration in LS-coupling is low, leading to low leading percentages for many of the levels. Even though the  $4p^45d$  and  $4p^46s$  configurations are practically coincident, there is not much mixing of states.

**Table 6.** Hartree-Fock and least-squares fitted parameters for the even configurations of Y V. Mean error of fit 273 cm<sup>-1</sup>.

Configuration	Parameter	HF	LSF	Unc.	LSF/HFR
4s4p <sup>6</sup>	$E_{av}(4s4p^6)$	215344	203602	511	0.942
4s <sup>2</sup> 4p <sup>4</sup> 4d	$E_{av}(4s^2 4p^4 4d)$	255431	251213	55	0.982
	$F^2(4p4p)$	77057	63230	629	0.821
	$\alpha(4p4p)$		-56 <sup>a</sup>		
	$\zeta_{4p}$	8132	8494	156	1.045
	$\zeta_{4d}$	507	612	73	1.209
	$F^2(4p4d)$	62105	53714	481	0.865
	$G^1(4p4d)$	76519	61136	169	0.799
	$G^3(4p4d)$	47207	39325	921	0.833
4s <sup>2</sup> 4p <sup>4</sup> 5s	$E_{av}(4s^2 4p^4 5s)$	314448	309938	101	0.985
	$F^2(4p4p)$	78065	64882	811	0.831
	$\alpha(4p4p)$		-56 <sup>a</sup>		
	$\zeta_{4p}$	8391	8647	254	1.031
	$G^1(4p5s)$	7780	6747	374	0.867
4s <sup>2</sup> 4p <sup>4</sup> 5d	$E_{av}(4s^2 4p^4 5d)$	438648	434854	54	0.991
	$F^2(4p4p)$	78487	65109	485	0.830
	$\alpha(4p4p)$		-56 <sup>a</sup>		
	$\zeta_{4p}$	8452	8827	119	1.044
	$\zeta_{5d}$	146	214	61	1.463
	$F^2(4p5d)$	16322	13742	557	0.842
	$G^1(4p5d)$	10162	6965 <sup>b</sup>	260	0.685
	$G^3(4p5d)$	7247	4967 <sup>b</sup>	185	0.685
4s <sup>2</sup> 4p <sup>4</sup> 6s	$E_{av}(4s^2 4p^4 6s)$	453803	450227	103	0.991
	$F^2(4p4p)$	78549	64962	784	0.827
	$\alpha(4p4p)$		-56 <sup>a</sup>		
	$\zeta_{4p}$	8477	8833	223	1.042
	$G^1(4p6s)$	2422	2041	372	0.843
Config. Interaction					
4s4p <sup>6</sup> -4s <sup>2</sup> 4p <sup>4</sup> 4d	$R^1(4p4p,4s4d)$	86708	66719 <sup>c</sup>	419	0.769
4s4p <sup>6</sup> -4s <sup>2</sup> 4p <sup>4</sup> 5d	$R^1(4p4p,4s5d)$	30749	23660 <sup>c</sup>	149	0.769
4s4p <sup>6</sup> -4s <sup>2</sup> 4p <sup>4</sup> 5s	$R^1(4p4p,4s5s)$	2884	2452 <sup>d</sup>		0.850
4s4p <sup>6</sup> -4s <sup>2</sup> 4p <sup>4</sup> 6s	$R^1(4p4p,4s6s)$	668	567 <sup>d</sup>		0.850
4s <sup>2</sup> 4p <sup>4</sup> 4d-4s <sup>2</sup> 4p <sup>4</sup> 5s	$R^2(4p4d,4p5s)$	-9422	-8009 <sup>d</sup>		0.850
	$R^1(4p4d,5s4p)$	-1919	-1631 <sup>d</sup>		0.850
4s <sup>2</sup> 4p <sup>4</sup> 4d-4s <sup>2</sup> 4p <sup>4</sup> 6s	$R^2(4p4d,4p6s)$	-5249	-4462 <sup>d</sup>		0.850
	$R^1(4p4d,6s4p)$	-1888	-1605 <sup>d</sup>		0.850

<sup>a</sup> Fixed at value from 4p<sup>4</sup> of Y VI [7]; <sup>b,c</sup> Linked in groups in LSF fit; <sup>d</sup> Fixed at scaled HFR value.

Table 7. Calculated energy levels (cm<sup>-1</sup>) and percentage compositions for the even levels of Y V.

<i>J</i>	Obs.	Calc.	O-C	% <i>J<sub>1</sub>I</i>	Percentage Composition (LS-Coupling)				
1/2	170946	170944	2		( <sup>2</sup> S) <sup>2</sup> S	24%	4p <sup>4</sup> d	( <sup>1</sup> D) <sup>2</sup> S	( <sup>3</sup> P) <sup>2</sup> P
5/2	218417	218286	131	75%	4s4p <sup>6</sup>	3%	4p <sup>4</sup> d	( <sup>3</sup> P) <sup>2</sup> F	4p <sup>4</sup> d
7/2	218557	218521	36	90%	4p <sup>4</sup> d	( <sup>3</sup> P) <sup>2</sup> D	3%	4p <sup>4</sup> d	( <sup>3</sup> P) <sup>2</sup> F
3/2	219374	219237	137	92%	4p <sup>4</sup> d	( <sup>3</sup> P) <sup>2</sup> D	5%	4p <sup>4</sup> d	( <sup>3</sup> P) <sup>2</sup> F
1/2	220795	220814	-19	88%	4p <sup>4</sup> d	( <sup>3</sup> P) <sup>2</sup> D	4%	4p <sup>4</sup> d	( <sup>3</sup> P) <sup>2</sup> P
9/2	229787	229647	140	88%	4p <sup>4</sup> d	( <sup>3</sup> P) <sup>2</sup> D	5%	4p <sup>4</sup> d	( <sup>1</sup> D) <sup>2</sup> P
7/2	233704	233513	191	91%	4p <sup>4</sup> d	( <sup>3</sup> P) <sup>2</sup> F	9%	4p <sup>4</sup> d	( <sup>1</sup> D) <sup>2</sup> G
1/2	233712	234734	-1022	72%	4p <sup>4</sup> d	( <sup>3</sup> P) <sup>2</sup> F	14%	4p <sup>4</sup> d	( <sup>3</sup> P) <sup>2</sup> F
5/2	237678	237425	253	45%	4p <sup>4</sup> d	( <sup>1</sup> D) <sup>2</sup> P	39%	4p <sup>4</sup> d	( <sup>3</sup> P) <sup>2</sup> P
3/2	238215	237945	270	94%	4p <sup>4</sup> d	( <sup>3</sup> P) <sup>2</sup> F	3%	4p <sup>4</sup> d	( <sup>3</sup> P) <sup>2</sup> D
1/2	238898	238811	87	63%	4p <sup>4</sup> d	( <sup>3</sup> P) <sup>2</sup> F	11%	4p <sup>4</sup> d	( <sup>3</sup> P) <sup>2</sup> P
3/2	239133	239284	-151	91%	4p <sup>4</sup> d	( <sup>3</sup> P) <sup>2</sup> P	4%	4p <sup>4</sup> d	( <sup>3</sup> P) <sup>2</sup> P
3/2	240949	240804	145	44%	4p <sup>4</sup> d	( <sup>3</sup> P) <sup>2</sup> P	22%	4p <sup>4</sup> d	( <sup>3</sup> P) <sup>2</sup> F
7/2	242336	242673	-337	38%	4p <sup>4</sup> d	( <sup>1</sup> D) <sup>2</sup> D	24%	4p <sup>4</sup> d	( <sup>3</sup> P) <sup>2</sup> F
5/2	244312	244201	111	48%	4p <sup>4</sup> d	( <sup>3</sup> P) <sup>2</sup> F	20%	4p <sup>4</sup> d	( <sup>3</sup> P) <sup>2</sup> D
3/2	244613	245018	-405	77%	4p <sup>4</sup> d	( <sup>3</sup> P) <sup>2</sup> P	7%	4p <sup>4</sup> d	( <sup>3</sup> P) <sup>2</sup> D
5/2	247861	247600	262	40%	4p <sup>4</sup> d	( <sup>1</sup> D) <sup>2</sup> D	23%	4p <sup>4</sup> d	( <sup>3</sup> P) <sup>2</sup> P
7/2	250883	250572	311	68%	4p <sup>4</sup> d	( <sup>1</sup> D) <sup>2</sup> G	22%	4p <sup>4</sup> d	( <sup>3</sup> P) <sup>2</sup> F
9/2	251052	250641	411	91%	4p <sup>4</sup> d	( <sup>1</sup> D) <sup>2</sup> G	9%	4p <sup>4</sup> d	( <sup>3</sup> P) <sup>2</sup> F
5/2	251404	252009	-605	67%	4p <sup>4</sup> d	( <sup>3</sup> P) <sup>2</sup> F	17%	4p <sup>4</sup> d	( <sup>1</sup> D) <sup>2</sup> D
5/2	263184	263228	-44	80%	4p <sup>4</sup> d	( <sup>1</sup> D) <sup>2</sup> F	11%	4p <sup>4</sup> d	( <sup>3</sup> P) <sup>2</sup> F
7/2	266197	266306	-109	82%	4p <sup>4</sup> d	( <sup>1</sup> D) <sup>2</sup> F	15%	4p <sup>4</sup> d	( <sup>3</sup> P) <sup>2</sup> F
5/2	286002	286024	-22	62%	4p <sup>4</sup> d	( <sup>1</sup> S) <sup>2</sup> D	26%	4p <sup>4</sup> d	( <sup>1</sup> D) <sup>2</sup> D
1/2	294102	294060	42	72%	4p <sup>4</sup> d	( <sup>1</sup> S) <sup>2</sup> D	16%	4p <sup>4</sup> d	( <sup>1</sup> D) <sup>2</sup> D
3/2	281245	281192	53	93%	4p <sup>4</sup> 5s	( <sup>1</sup> P) <sup>2</sup> P	6%	4p <sup>4</sup> 5s	( <sup>1</sup> D) <sup>2</sup> D
5/2	294966	295069	-103	62%	4p <sup>4</sup> d	( <sup>1</sup> D) <sup>2</sup> S	20%	4s4p <sup>6</sup>	( <sup>3</sup> S) <sup>2</sup> S
3/2	297071	296670	401	47%	4p <sup>4</sup> d	( <sup>3</sup> P) <sup>2</sup> P	36%	4p <sup>4</sup> d	( <sup>1</sup> D) <sup>2</sup> D
3/2	298379	298417	-38	47%	4p <sup>4</sup> 5s	( <sup>3</sup> P) <sup>2</sup> P	43%	4p <sup>4</sup> 5s	( <sup>1</sup> D) <sup>2</sup> D
5/2	300224	300747	-523	62%	4p <sup>4</sup> d	( <sup>3</sup> P) <sup>2</sup> D	20%	4p <sup>4</sup> d	( <sup>1</sup> D) <sup>2</sup> D
1/2	302664	301985	679	44%	4p <sup>4</sup> d	( <sup>3</sup> P) <sup>2</sup> P	38%	4p <sup>4</sup> d	( <sup>1</sup> S) <sup>2</sup> D
1/2	304565	304602	-37	90%	4p <sup>4</sup> 5s	( <sup>3</sup> P) <sup>2</sup> P	5%	4p <sup>4</sup> 5s	( <sup>1</sup> S) <sup>2</sup> S
3/2	306215	306149	66	89%	( <sup>3</sup> P) <sup>2</sup> P	( <sup>3</sup> P) <sup>2</sup> P	42%	4p <sup>4</sup> 5s	( <sup>1</sup> D) <sup>2</sup> S
1/2	310858	310839	19	95%	4p <sup>4</sup> 5s	( <sup>3</sup> P) <sup>2</sup> P	4%	4p <sup>4</sup> 5s	( <sup>1</sup> D) <sup>2</sup> D
3/2	312044	312297	-253	54%	4p <sup>4</sup> d	( <sup>3</sup> P) <sup>2</sup> D	20%	4p <sup>4</sup> d	( <sup>1</sup> D) <sup>2</sup> D
5/2	319133	319168	-35	93%	( <sup>1</sup> D) <sup>2</sup> D	( <sup>1</sup> D) <sup>2</sup> D	6%	4p <sup>4</sup> 5s	( <sup>3</sup> P) <sup>2</sup> P
3/2	319604	319699	-95	88%	( <sup>1</sup> D) <sup>2</sup> D	( <sup>1</sup> D) <sup>2</sup> D	10%	4p <sup>4</sup> 5s	( <sup>3</sup> P) <sup>2</sup> P
1/2	345802	345752	50	88%	( <sup>1</sup> S) <sup>2</sup> S	( <sup>1</sup> S) <sup>2</sup> S	6%	4p <sup>4</sup> 5s	( <sup>3</sup> P) <sup>2</sup> P

Table 7. Cont.

<i>J</i>	Obs.	Calc.	O-C	% <i>J<sub>1</sub>I</i>	Percentage Composition (LS-Coupling)							
7/2	418265	418341	-76	91% ( <sup>3</sup> P <sub>2</sub> ) [3]	4p <sup>4</sup> 5d	( <sup>3</sup> P) <sup>4</sup> D	20%	4p <sup>4</sup> 5d	( <sup>3</sup> P) <sup>4</sup> F	5%	4p <sup>4</sup> 5d	(D) <sup>2</sup> F
5/2	418310	418347	-37	57% ( <sup>3</sup> P <sub>2</sub> ) [2]	4p <sup>4</sup> 5d	( <sup>3</sup> P) <sup>4</sup> D	10%	4p <sup>4</sup> 5d	( <sup>3</sup> P) <sup>4</sup> P	10%	4p <sup>4</sup> 5d	( <sup>3</sup> P) <sup>4</sup> F
3/2	418914	418953	-39	60% ( <sup>3</sup> P <sub>2</sub> ) [2]	4p <sup>4</sup> 5d	( <sup>3</sup> P) <sup>4</sup> D	22%	4p <sup>4</sup> 5d	( <sup>3</sup> P) <sup>4</sup> D	5%	4p <sup>4</sup> 5d	(D) <sup>2</sup> D
1/2	419977	420043	-66	78% ( <sup>3</sup> P <sub>2</sub> ) [1]	4p <sup>4</sup> 5d	( <sup>3</sup> P) <sup>4</sup> D	29%	4p <sup>4</sup> 5d	( <sup>3</sup> P) <sup>4</sup> P	15%	4p <sup>4</sup> 5d	( <sup>3</sup> P) <sup>2</sup> P
9/2	420404	420469	-65	91% ( <sup>3</sup> P <sub>2</sub> ) [4]	4p <sup>4</sup> 5d	( <sup>3</sup> P) <sup>4</sup> F	9%	4p <sup>4</sup> 5d	(D) <sup>2</sup> G			
7/2	421427	421205	222	89% ( <sup>3</sup> P <sub>2</sub> ) [4]	4p <sup>4</sup> 5d	( <sup>3</sup> P) <sup>4</sup> F	23%	4p <sup>4</sup> 5d	( <sup>3</sup> P) <sup>4</sup> G	9%	4p <sup>4</sup> 5d	(D) <sup>2</sup> G
1/2	423351	423374	-23	83% ( <sup>3</sup> P <sub>2</sub> ) [0]	4p <sup>4</sup> 5d	( <sup>3</sup> P) <sup>4</sup> P	28%	4p <sup>4</sup> 5d	( <sup>3</sup> P) <sup>2</sup> P	9%	4p <sup>4</sup> 5d	(D) <sup>2</sup> S
3/2	424830	424828	2	64% ( <sup>3</sup> P <sub>2</sub> ) [1]	4p <sup>4</sup> 5d	( <sup>3</sup> P) <sup>4</sup> P	30%	4p <sup>4</sup> 5d	( <sup>3</sup> P) <sup>2</sup> D	13%	4p <sup>4</sup> 5d	( <sup>3</sup> P) <sup>4</sup> D
5/2	425078	425015	63	53% ( <sup>3</sup> P <sub>2</sub> ) [3]	4p <sup>4</sup> 5d	( <sup>3</sup> P) <sup>4</sup> D	27%	4p <sup>4</sup> 5d	( <sup>3</sup> P) <sup>2</sup> F	17%	4p <sup>4</sup> 5d	( <sup>3</sup> P) <sup>4</sup> P
1/2	429552	429752	-200	86% ( <sup>3</sup> P <sub>1</sub> ) [1]	4p <sup>4</sup> 5d	( <sup>3</sup> P) <sup>4</sup> D	34%	4p <sup>4</sup> 5d	( <sup>3</sup> P) <sup>2</sup> P	9%	4p <sup>4</sup> 5d	(D) <sup>2</sup> P
3/2	430344	430325	19	67% ( <sup>3</sup> P <sub>0</sub> ) [2]	4p <sup>4</sup> 5d	( <sup>3</sup> P) <sup>4</sup> F	13%	4p <sup>4</sup> 5d	( <sup>3</sup> P) <sup>4</sup> D	8%	4p <sup>4</sup> 5d	(S) <sup>2</sup> D
5/2	430534	430524	10	51% ( <sup>3</sup> P <sub>0</sub> ) [2]	4p <sup>4</sup> 5d	( <sup>3</sup> P) <sup>4</sup> F	15%	4p <sup>4</sup> 5d	( <sup>3</sup> P) <sup>4</sup> P	14%	4p <sup>4</sup> 5d	( <sup>3</sup> P) <sup>4</sup> D
7/2	430760	430623	137	97% ( <sup>3</sup> P <sub>1</sub> ) [3]	4p <sup>4</sup> 5d	( <sup>3</sup> P) <sup>4</sup> F	24%	4p <sup>4</sup> 5d	( <sup>3</sup> P) <sup>4</sup> D	22%	4p <sup>4</sup> 5d	( <sup>3</sup> P) <sup>4</sup> D
3/2	431436	431423	13	53% ( <sup>3</sup> P <sub>1</sub> ) [1]	4p <sup>4</sup> 5d	( <sup>3</sup> P) <sup>4</sup> P	23%	4p <sup>4</sup> 5d	( <sup>3</sup> P) <sup>4</sup> D	21%	4p <sup>4</sup> 5d	( <sup>3</sup> P) <sup>2</sup> D
5/2	432673	432560	113	97% ( <sup>3</sup> P <sub>1</sub> ) [2]	4p <sup>4</sup> 5d	( <sup>3</sup> P) <sup>4</sup> P	33%	4p <sup>4</sup> 5d	( <sup>3</sup> P) <sup>4</sup> F	11%	4p <sup>4</sup> 5d	( <sup>3</sup> P) <sup>4</sup> F
5/2	434647	434607	40	51% ( <sup>3</sup> P <sub>1</sub> ) [3]	4p <sup>4</sup> 5d	( <sup>3</sup> P) <sup>4</sup> D	34%	4p <sup>4</sup> 5d	( <sup>3</sup> P) <sup>2</sup> F	4%	4p <sup>4</sup> 5d	( <sup>3</sup> P) <sup>4</sup> P
3/2	435071	435299	-228	39% ( <sup>3</sup> P <sub>1</sub> ) [2]	4p <sup>4</sup> 5d	( <sup>3</sup> P) <sup>4</sup> P	19%	4p <sup>4</sup> 5d	( <sup>3</sup> P) <sup>2</sup> D	8%	4p <sup>4</sup> 5d	(D) <sup>2</sup> P
5/2	435671	435664	7	92% ( <sup>3</sup> P <sub>2</sub> ) [2]	4p <sup>4</sup> 6s	( <sup>3</sup> P) <sup>4</sup> P	7%	4p <sup>4</sup> 6s	( <sup>3</sup> P) <sup>4</sup> P	1%	4p <sup>4</sup> 5d	( <sup>3</sup> P) <sup>2</sup> D
3/2	437171	437167	4	89% ( <sup>3</sup> P <sub>2</sub> ) [2]	4p <sup>4</sup> 6s	( <sup>3</sup> P) <sup>4</sup> P	21%	4p <sup>4</sup> 6s	( <sup>3</sup> P) <sup>4</sup> P	8%	4p <sup>4</sup> 6s	(D) <sup>2</sup> D
7/2	442366	442275	91	90% ( <sup>1</sup> D <sub>2</sub> ) [4]	4p <sup>4</sup> 5d	(D) <sup>2</sup> G	7%	4p <sup>4</sup> 5d	( <sup>3</sup> P) <sup>4</sup> F	2%	4p <sup>4</sup> 5d	( <sup>3</sup> P) <sup>4</sup> F
9/2	442705	442669	36	91% ( <sup>1</sup> D <sub>2</sub> ) [4]	4p <sup>4</sup> 5d	(D) <sup>2</sup> G	9%	4p <sup>4</sup> 5d	( <sup>3</sup> P) <sup>4</sup> F	8%	4p <sup>4</sup> 5d	( <sup>3</sup> P) <sup>4</sup> F
1/2	441129	444050	79	79% ( <sup>1</sup> D <sub>2</sub> ) [0]	4p <sup>4</sup> 5d	(D) <sup>2</sup> S	11%	4p <sup>4</sup> 5d	(D) <sup>2</sup> P	8%	4p <sup>4</sup> 5d	( <sup>3</sup> P) <sup>4</sup> P
3/2	444984	444917	67	80% ( <sup>1</sup> D <sub>2</sub> ) [1]	4p <sup>4</sup> 5d	(D) <sup>2</sup> P	6%	4p <sup>4</sup> 5d	( <sup>3</sup> P) <sup>4</sup> P	5%	4p <sup>4</sup> 5d	( <sup>3</sup> P) <sup>4</sup> P
5/2	445300	445422	-122	59% ( <sup>1</sup> D <sub>2</sub> ) [2]	4p <sup>4</sup> 5d	(D) <sup>2</sup> D	36%	4p <sup>4</sup> 5d	(D) <sup>2</sup> F	1%	4p <sup>4</sup> 5d	( <sup>3</sup> P) <sup>4</sup> P
1/2	446210	446244	-34	59% ( <sup>3</sup> P <sub>0</sub> ) [0]	4p <sup>4</sup> 6s	( <sup>3</sup> P) <sup>4</sup> P	7%	4p <sup>4</sup> 6s	(S) <sup>2</sup> S			
7/2	446600	446452	148	93% ( <sup>1</sup> D <sub>2</sub> ) [3]	4p <sup>4</sup> 5d	(D) <sup>2</sup> F	3%	4p <sup>4</sup> 5d	(D) <sup>2</sup> D	2%	4p <sup>4</sup> 5d	( <sup>3</sup> P) <sup>2</sup> F
5/2	446709	446619	90	56% ( <sup>1</sup> D <sub>2</sub> ) [3]	4p <sup>4</sup> 5d	(D) <sup>2</sup> F	32%	4p <sup>4</sup> 5d	(D) <sup>2</sup> D	7%	4p <sup>4</sup> 5d	( <sup>3</sup> P) <sup>2</sup> D
3/2	446718	446692	26	96% ( <sup>3</sup> P <sub>1</sub> ) [1]	4p <sup>4</sup> 6s	( <sup>3</sup> P) <sup>4</sup> P	22%	4p <sup>4</sup> 6s	( <sup>3</sup> P) <sup>2</sup> P	2%	4p <sup>4</sup> 5d	(D) <sup>2</sup> P
1/2	447277	447284	-7	41% ( <sup>1</sup> D <sub>2</sub> ) [1]	4p <sup>4</sup> 5d	(D) <sup>2</sup> P	34%	4p <sup>4</sup> 5d	( <sup>3</sup> P) <sup>2</sup> P	13%	4p <sup>4</sup> 5d	( <sup>3</sup> P) <sup>2</sup> P
3/2	448358	448574	-216	78% ( <sup>1</sup> D <sub>2</sub> ) [2]	4p <sup>4</sup> 5d	(D) <sup>2</sup> D	18%	4p <sup>4</sup> 5d	( <sup>3</sup> P) <sup>2</sup> D	1%	4p <sup>4</sup> 5d	(D) <sup>2</sup> P
1/2	448775	448783	-8	45% ( <sup>3</sup> P <sub>1</sub> ) [1]	4p <sup>4</sup> 6s	( <sup>3</sup> P) <sup>4</sup> P	25%	4p <sup>4</sup> 6s	(D) <sup>2</sup> P	8%	4p <sup>4</sup> 5d	( <sup>3</sup> P) <sup>2</sup> P
5/2	459637	459629	8	92% ( <sup>1</sup> D <sub>2</sub> ) [2]	4p <sup>4</sup> 6s	(D) <sup>2</sup> D	7%	4p <sup>4</sup> 6s	( <sup>3</sup> P) <sup>4</sup> P	1%	4p <sup>4</sup> 6s	( <sup>3</sup> P) <sup>4</sup> P
3/2	459761	459765	-4	91% ( <sup>1</sup> D <sub>2</sub> ) [2]	4p <sup>4</sup> 6s	(D) <sup>2</sup> D	7%	4p <sup>4</sup> 6s	( <sup>3</sup> P) <sup>2</sup> P	3%	4p <sup>4</sup> 5d	( <sup>3</sup> P) <sup>4</sup> P
5/2	470990	471048	-58	88% ( <sup>1</sup> S <sub>0</sub> ) [2]	4p <sup>4</sup> 5d	(S) <sup>2</sup> D	3%	4p <sup>4</sup> 5d	( <sup>3</sup> P) <sup>2</sup> F	4%	4p <sup>4</sup> 5d	( <sup>3</sup> P) <sup>4</sup> D
3/2	471484	471481	3	86% ( <sup>1</sup> S <sub>0</sub> ) [2]	4p <sup>4</sup> 5d	(S) <sup>2</sup> D	5%	4p <sup>4</sup> 5d	( <sup>3</sup> P) <sup>4</sup> F	4%	4p <sup>4</sup> 5d	( <sup>3</sup> P) <sup>4</sup> D
1/2	486068	486067	1	88% ( <sup>1</sup> S <sub>0</sub> ) [0]	4p <sup>4</sup> 6s	(S) <sup>2</sup> S	7%	4p <sup>4</sup> 6s	( <sup>3</sup> P) <sup>4</sup> P	4%	4p <sup>4</sup> 6s	( <sup>3</sup> P) <sup>2</sup> P

### 5. $4s4p^6-4s^24p^45p$ Transitions

Transitions between the  $4s4p^6$  and  $4s^24p^45p$  configurations are normally forbidden as two electron jumps. However, because of configuration interaction between  $4s4p^6$  and  $4s^24p^44d$ , they can in fact take place. We observe six of them in Y V. The wavelengths for these transitions are long relative to the resonance lines and serve to improve the accuracy of the excited levels.

### 6. Ritz Wavelengths

We determined Ritz wavelengths for all of the lines by differencing the energy level values in Tables 2 and 3. The Ritz wavelengths are given in Table 1. The uncertainties of the calculated wavelengths correspond to the square root of the sum of the squares of the uncertainties of the combining levels. The Ritz values have uncertainties that are as low as  $\pm 0.0004 \text{ \AA}$ . Those lines with uncertainties in the Ritz wavelengths of  $\pm 0.0020 \text{ \AA}$  or less should serve well as wavelength standards in the deep VUV.

### 7. Oscillator Strengths

Table 1 lists the transition probabilities  $g_U A$  and  $\log g_L f$  for each observed line as calculated with wavefunctions obtained from the fitted energy parameters. Here,  $f$  is the oscillator strength,  $g_U$  is the statistical weight of the upper level  $2J_U + 1$  and  $g_L$  is the statistical weight of the lower level  $2J_L + 1$ . The  $A$ -values are compared with recently published ab initio values in Section 9 below.

Since there are no experimental values for the transition probabilities of Y V, it is difficult to estimate the uncertainty of the calculated values. One guide is the cancellation factor. This is the ratio of the calculated transition probability to a value calculated with all parts of the wave function taken as positive [12]. Low cancellation factors generally indicate a larger uncertainty in the calculated values. Indeed, many of the values in Table 1 have low cancellation factors. The present calculated transition probabilities can be considered as qualitative estimates of the relative intensities of the lines. Based on general experience, we estimate the uncertainties to be about  $\pm 50\%$ .

### 8. Ionization Energy

An ionization energy of  $605,000 \pm 4000 \text{ cm}^{-1}$  was obtained in [4] by estimating a value for  $n^*(4p^45s)$  of  $2.98 \pm 0.02$ . On the basis of their observed  $4s^24p^4ns$  ( $n = 5-7$ ) and  $nd$  ( $n = 4-6$ ) series, Zahid-Ali, Chaghtai, and Singh [5] revised this downward slightly to  $604,700 \pm 2500 \text{ cm}^{-1}$ . Since many of the levels used in their determination are now known to be spurious, this value must be re-determined.

For our new determination, we use the centers-of-gravity of the  $4p^45s$  and  $4p^46s$  configurations together with an estimated value for the change in effective quantum number  $\Delta n^*(4p^46s-4p^45s) = n^*(4p^46s) - n^*(4p^45s)$ . This allows us to find the limit of the  $4p^4ns$  series, which is the center-of-gravity of the  $4p^4$  configuration of Y VI.

From the observed levels in Table 3, we find the centers-of-gravity of the  $4p^45s$  and  $4p^46s$  configurations as  $309,955.06$  and  $450,284.98 \text{ cm}^{-1}$ , respectively. Our value for  $\Delta n^*(4p^46s-4p^45s)$  is taken from  $\Delta n^*(4p^66s-4p^65s)$  for the one-electron atom Nb V [15],  $1.03577$ . We use Cowan's Hartree-Fock code to estimate the change in going from Nb V to Y V. For Nb V we calculate  $\Delta n^*(4p^66s-4p^65s)$  as  $1.0394$  and for Y V we calculate  $\Delta n^*(4p^46s-4p^45s)$  as  $1.0369$ , a difference of  $0.0025$ . We thus estimate  $\Delta n^*(4p^46s-4p^45s)$  for Y V as  $1.03577 - 0.00251 = 1.0333$ , with an estimated uncertainty of  $\pm 0.0015$ . This produces a limit of  $621,810 \pm 300 \text{ cm}^{-1}$ . The effective quantum numbers for Y V are  $n^*(5s) = 2.966(1)$  and  $n^*(6s) = 3.999(3)$ . Correcting for the energy of the center-of-gravity of  $4p^4$  in Y VI,  $14,051 \text{ cm}^{-1}$  [7], we obtain for the ionization energy of Y V  $607,760 \pm 300 \text{ cm}^{-1}$  ( $75.353 \pm 0.037 \text{ eV}$ ). (Conversion from  $\text{cm}^{-1}$  to eV was done with the factor  $8065.54429(18) \text{ cm}^{-1}/\text{eV}$  [16].)

## 9. Comparison with ab Initio Calculations

Recently, two sets of ab initio calculations for the levels and oscillator strengths of Y V have appeared. Singh et al. [17] used a multiconfiguration Dirac-Fock (MCDF) approach to make calculations for transitions within the  $n = 4$  complex;  $4s^24p^5$ ,  $4s4p^6$ ,  $4s^24p^44d$ . Aggarwal and Keenan [18] used the General-purpose Relativistic Atomic Structure Package (GRASP) for calculations within the same complex of  $n = 4$  configurations. Both calculations are based on new versions of the Grant atomic structure code. Froese Fischer [19] has discussed the accuracy that might be expected from calculations for complex atoms with GRASP, in particular as applied to the Br-like ion  $W^{39+}$ .

Comparisons of our present results with those of the ab initio calculations of [17,18] are given in Tables 8–10. The index numbers for the levels in these tables are those used in [17,18]. The wavelengths for Aggarwal and Keenan [18] in Table 8 are differences of the GRASP3 energies in their Table 3. It should be noted that the level with index 25 in [17] is misprinted  $4s^24p^4(^1D)4d^2P_{3/2}$ ; it should be  $4s^24p^4(^1S)4d^2D_{3/2}$ , as given in [18].

The main difference between the results of [17,18] and our present results is that the energies of the levels designated  $4s^24p^4(^3P)4d^2P_{1/2}$  (index 28) and  $4s^24p^4(^1D)4d^2S_{1/2}$  (index 30) are reversed in order of energy. That is, the level with index 28 corresponds to our level 4d51, and the level with index 30 corresponds to our level 4d41.

That our present order is correct can be seen from the fact that  $(^3P)^2P$  has little interaction with  $4s4p^6^2S$ , and its position is largely fixed by the internal parameters of  $4p^44d$ . If omitted from the LSF calculation, the calculated energy is very close to the observed value. So, there is no doubt about this assignment. This leaves the level at  $294,965 \text{ cm}^{-1}$  as the only possibility for  $(^1D)^2S$ . The position of  $(^1D)^2S$  is harder to pin down, because it is affected not only by the internal parameters of  $4p^44d$ , but also by the amount of its upward displacement due to interaction with  $4s4p^6^2S$ . In our present calculations this uncertainty is removed, because when the level is included in the LSF, the CI parameter  $R^1(4p4p,4s4d)$  takes a fitted value that has a reasonable ratio to HFR. This conclusion is supported by the observed line intensities, which follow the predicted pattern for these two levels. See for example the lines at 339.023, 353.976, 330.398, and  $344.583 \text{ \AA}$  in Table 8. It is clear that in the MCDF calculations the upward displacement of  $4s^24p^4(^1D)4d^2S_{1/2}$  due to interaction with  $4s4p^6^2S_{1/2}$  is a little too large. The LSF/HFR scale factor of 0.769 for this interaction in Table 6 also reflects this circumstance.

In Table 8 we compare the wavelengths and transition probabilities  $A$  ( $\text{s}^{-1}$ ) found from GRASP with our present results. The values of  $A(\text{present})$  in this table are those given in Table 1 divided by the statistical weight of the upper level  $2J_u+1$ . A notable disagreement for the transition probabilities for the  $4s^24p^5^2P_{3/2}-4s^24p^44d(^3P)^4F_{3/2}$  transition (indices 1–12), observed at  $419.792 \text{ \AA}$ . Both Singh et al. [17] and Aggarwal and Keenan [18] find an extremely low transition probability for this transition. However, we obtain a somewhat higher  $A$ -value, and it is indeed observed as a reasonably strong line. This transition is nominally forbidden as an inter-combination line in LS-coupling because of the change of spin. However, although the  $4p^44d$  level ( $238,215 \text{ cm}^{-1}$  observed value) has a leading percentage composition in LS coupling of 63%  $4p^44d(^3P)^4F_{3/2}$ , the full percentage compositions show that it actually has a total doublet character of about 31%. This accounts for our calculated transition probability and observed line strength. Singh et al. [17] report a composition of 88%  $4p^44d(^3P)^4F_{3/2}$  for this level, with no secondary percentage mentioned. Percentage compositions were not reported by Aggarwal and Keenan [18]. The present percentage compositions for Y V are practically the same as were given in [4]. This paper was not cited in either [17] or [18].

Other striking differences can be seen in Table 8. The values found by all three calculations for the  $4s^24p^5^2P_{3/2}-4s^24p^44d(^1S)^4D_{5/2}$  transition (indices 1–26) are extremely discrepant. The value of Aggarwal [18] is a little closer to our present value. The values for the  $4s^24p^5^2P_{1/2}-4s^24p^44d(^3P)^4D_{3/2}$  transition (indices 2–6) also disagree by a large amount. Still, they all predict that this will be a very weak line, and in fact it has not been observed.

**Table 8.** Comparison of wavelengths  $\lambda$  (Å) and transition probabilities  $A$  ( $s^{-1}$ ) for Y V calculated with the MCFD2 method of Singh et al. [17] and the GRASP3 method of Aggarwal and Keenan [18] with present values. Index numbers are those used in [17,18]. Blank spaces indicate that line was not observed. Designations are for the upper levels in the transition.

Lower Level	Upper Level	Desig.	Index	$\lambda$ [17]	$\lambda$ [18]	$\lambda$ (obs)	A [17]	A [18]	A (Pres.)	CF	Int (obs)
$4s^2 4p^5 2P_{3/2}$ (index = 1)	$4s4p^6 2S_{1/2}$	4p61	3	594	555.817	584.982	3.41E+08	6.4885E+08	8.30E+08	0.03	50000
	$4s^2 4p^4 4d(3P)^1 D_{3/2}$	4d15	4	466	447.189	457.838	8.49E+06	1.4695E+07	7.05E+06	0.00	
	$(3P)^1 D_{3/2}$	4d13	6	464	445.053	455.846	5.17E+06	5.7124E+06	6.85E+06	0.00	35
	$(3P)^1 D_{1/2}$	4d11	7	461	442.088	452.911	2.69E+06	1.9727E+06	6.30E+06	0.00	5
	$(1D)^2 P_{1/2}$	4d21	10	427	410.339	451.974	1.10E+07	2.4808E+06	4.77E+07	0.00	25
	$(3P)^1 F_{5/2}$	4d25	11	425	410.674	420.737	9.04E+07	1.3428E+08	1.40E+08	0.74	1500
	$(3P)^1 F_{3/2}$	4d23	12	423	409.298	419.792	2.44E+06	2.4683E+06	7.80E+07	0.01	400
	$(3P)^1 F_{3/2}$	4d33	14	418	403.024	418.179	3.73E+08	4.1741E+08	4.15E+08	0.02	600
	$(1D)^2 D_{3/2}$	4d43	15	414	399.946	415.027	2.77E+08	2.3712E+08	3.05E+08	0.01	1500
	$(3P)^1 F_{5/2}$	4d35	17	410	395.482	409.312	1.10E+08	1.2373E+08	2.13E+08	0.02	1500
	$(1D)^2 F_{3/2}$	4d53	18	408	393.779	408.806	8.38E+07	6.7013E+06	3.28E+07	0.00	10
	$(1D)^2 D_{5/2}$	4d45	19	403	389.248	403.452	3.66E+08	2.4821E+08	3.55E+08	0.01	1500
	$(3P)^1 F_{5/2}$	4d55	22	396	382.946	397.767	1.49E+08	2.2968E+08	1.14E+08	0.01	1000
	$(1S)^2 D_{3/2}$	4d65	23	374	362.156	379.963	2.34E+08	3.3501E+08	4.00E+08	0.14	1000
	$(1S)^2 D_{3/2}$	4d63	25	346	345.203	355.564	1.06E+09	3.1288E+09	2.29E+09	0.09	1500
	$(1S)^1 D_{5/2}$	4d75	26	341	341.242	349.648	5.28E+07	1.4890E+09	1.56E+08	0.00	800
	$(3P)^2 F_{3/2}$	4d73	27	319	324.443	336.621	1.27E+11	1.0669E+11	1.18E+11	0.88	5000
$(3P)^2 P_{1/2}$	4d51	28	315	320.652	330.398	1.07E+11	6.8148E+10	5.30E+09	0.05	300	
$(3P)^2 D_{5/2}$	4d85	29	311	318.592	333.084	1.53E+11	1.2220E+11	1.31E+11	0.82	10000	
$(1D)^2 S_{1/2}$	4d41	30	309	310.266	339.023	3.70E+10	5.8584E+10	1.17E+11	0.71	3000	
$(3P)^2 D_{3/2}$	4d83	31	301	308.303	320.467	6.68E+09	4.2526E+09	2.36E+09	0.03	500	
$4p^5 2P_{1/2}$ (index = 2)	$4s4p^6 2S_{1/2}$	4p61	3	640	595.852	630.973	1.59E+08	3.0194E+08	5.45E+07	0.04	30000
	$4s^2 4p^4 4d(3P)^1 D_{3/2}$	4d13	6	491	470.358	477.944	1.47E+05	7.9784E+04	1.18E+06	0.00	
	$(3P)^1 D_{1/2}$	4d11	7	488	467.049	479.994	3.11E+06	1.7391E+06	4.92E+06	0.00	1
	$(1D)^2 P_{1/2}$	4d21	10	450	431.756	451.974	5.58E+07	2.7075E+07	4.77E+07	0.00	25
	$(3P)^1 F_{3/2}$	4d23	12	446	430.603	442.947	2.89E+07	4.0470E+07	9.35E+06	0.00	300
	$(3P)^1 P_{1/2}$	4d31	13	441	423.647	441.622	1.30E+07	1.1362E+07	3.80E+07	0.01	25
	$(3P)^1 F_{3/2}$	4d33	14	441	423.664	441.161	2.24E+07	2.7072E+06	4.13E+06	0.00	2
	$(1D)^2 D_{3/2}$	4d43	15	436	420.265	437.661	3.20E+08	3.2991E+08	3.25E+08	0.01	500
	$(1D)^2 P_{3/2}$	4d53	18	430	413.461	430.753	2.86E+07	1.7387E+07	1.78E+07	0.00	500
	$(1S)^1 D_{3/2}$	4d63	25	361	360.235	372.047	1.92E+09	5.6428E+08	3.05E+09	0.06	4000
	$(3P)^2 F_{3/2}$	4d73	27	332	337.687	351.355	3.32E+09	2.3159E+09	8.95E+08	0.02	800
	$(3P)^2 P_{1/2}$	4d51	28	328	333.582	344.583	1.03E+11	3.9796E+10	9.85E+10	0.82	2000
	$(1D)^2 S_{1/2}$	4d41	30	321	322.356	353.976	2.85E+10	4.1111E+10	5.60E+09	0.05	1500
	$(3P)^2 D_{3/2}$	4d83	31	312	320.238	333.796	1.46E+11	1.2065E+11	1.29E+11	0.83	5000



Both Singh et al. [17] and Aggarwal and Keenan [18] compare their calculated level values with the observed values given in the NIST Atomic Spectra Database [20]. Since we have made a number of revisions to the  $4p^44d$  levels, a new comparison is called for. This is given in Table 9.

**Table 9.** Comparison of level energies  $E$  ( $\text{cm}^{-1}$ ) for Y V calculated with the MCDF2 method of Singh et al. [17] and the GRASP3 method of Aggarwal and Keenan [18] with present experimental energies. Index numbers are those used in [17,18].

Configuration	Term	Desig.	Index	$J$	$E$ [17]	$E$ [18]	$E$ (Present)
$4s^24p^5$	$^2P$	p5 3	1	3/2	0	0.00	0.00
	$^2P$	p5 1	2	1/2	12147.85	12088.59	12460.12
$4s4p^6$	$^2S$	4p61	3	1/2	168478.74	179915.44	170945.58
$4s^24p^44d$	$(^3P)^4D$	4d15	4	5/2	214469.38	223619.16	218417.13
	$(^3P)^4D$	4d17	5	7/2	214524.25	223608.19	218556.80
	$(^3P)^4D$	4d13	6	3/2	215610.64	224692.39	219373.81
	$(^3P)^4D$	4d11	7	1/2	217092.09	226199.07	220794.66
	$(^3P)^4F$	4d19	8	9/2	227122.02	235877.84	229786.64
	$(^3P)^4F$	4d27	9	7/2	231522.46	240231.10	233703.76
	$(^1D)^2P$	4d21	10	1/2	234342.70	243700.97	233712.36
	$(^3P)^4F$	4d25	11	5/2	235024.04	243502.35	237677.66
	$(^3P)^4F$	4d23	12	3/2	236230.17	244320.98	238215.09
	$(^3P)^4P$	4d31	13	1/2	238754.11	248134.33	238898.28
	$(^3P)^4P$	4d33	14	3/2	239017.48	248124.45	239132.83
	$(^1D)^2D$	4d43	15	3/2	241420.71	250033.87	240949.32
	$(^3P)^2F$	4d37	16	7/2	242276.66	251012.72	242336.33
	$(^3P)^4P$	4d35	17	5/2	244197.05	252856.30	244311.56
	$(^1D)^2P$	4d53	18	3/2	244932.29	253949.27	244613.24
	$(^1D)^2D$	4d45	19	5/2	248290.23	256905.58	247861.17
	$(^1D)^2G$	4d29	20	9/2	251033.65	259335.15	251052.40
	$(^1D)^2G$	4d47	21	7/2	251351.88	259728.01	250882.71
	$(^3P)^2F$	4d55	22	5/2	252383.41	261133.73	251403.88
	$(^1D)^2F$	4d65	23	5/2	267274.68	276123.76	263184.02
	$(^1D)^2F$	4d57	24	7/2	270072.96	278936.31	266196.75
$(^1S)^2D$	4d63	25	3/2	289079.36	289685.02	281244.51	
$(^1S)^2D$	4d75	26	5/2	293095.72	293047.35	286001.66	
$(^3P)^2P$	4d73	27	3/2	313792.06	308220.63	297071.14	
$(^3P)^2P$	4d51	28	1/2	317095.13	311864.99	302664.42	
$(^3P)^2D$	4d85	29	5/2	321122.47	313880.85	300224.19	
$(^1D)^2S$	4d41	30	1/2	323306.23	322304.24	294965.68	
$(^3P)^2D$	4d83	31	3/2	332502.17	324356.31	312044.02	

The percentage compositions for  $4s4p^6$  and  $4s^24p^44d$  obtained in the present work are compared with those obtained in the MCDF calculations of Singh et al. [17] in Table 10. The general agreement is qualitatively reasonable.

**Table 10.** Comparison of the present percentage compositions for the  $4s4p^6$  and  $4s^2 4p^4 4d$  configurations of Y V (in bold type) with those of Singh et al. [17] (in parentheses). Level values are in  $\text{cm}^{-1}$ .

Index	Desig.	J	E (obs) <sup>a</sup>	Percentage Composition	
3	4p61	1/2	170946	75(69)%	$4s^2 S$
4	4d15	5/2	218417	90(92)%	$(^3P)^4D$
5	4d17	7/2	218557	92(94)%	$(^3P)^4D$
6	4d13	3/2	219374	88(91)%	$(^3P)^4D$
7	4d11	1/2	220795	88(91)%	$(^3P)^4D$
8	4d19	9/2	229787	91(93)%	$(^3P)^4F$
9	4d27	7/2	233704	72(81)%	$(^3P)^4F$
10	4d21	1/2	233712	45(45)%	$(^1D)^2P$
11	4d25	5/2	237678	94(94)%	$(^3P)^4F$
12	4d23	3/2	238215	63(88)%	$(^3P)^4F$
13	4d31	1/2	238898	91(92)%	$(^3P)^4P$
14	4d33	3/2	239133	44(56)%	$(^3P)^4P$
15	4d43	3/2	240949	38(40)%	$(^1D)^2D$
16	4d37	7/2	242336	48(57)%	$(^3P)^2F$
17	4d35	5/2	244312	77(89)%	$(^3P)^4P$
18	4d53	3/2	244613	39(24)%	$(^3P)^4P$
19	4d45	5/2	247861	40(42)%	$(^1D)^2D$
20	4d29	9/2	251052	91(93)%	$(^1D)^2G$
21	4d47	7/2	250883	68(73)%	$(^1D)^2G$
22	4d55	5/2	251404	67(65)%	$(^3P)^2F$
23	4d65	5/2	263184	80(83)%	$(^1D)^2F$
24	4d57	7/2	266197	82(83)%	$(^1D)^2F$
25	4d63	3/2	281245	62(67)%	$(^1S)^2D$
26	4d75	5/2	286002	72(74)%	$(^1S)^2D$
27	4d73	3/2	297071	47(51)%	$(^3P)^2P$
28	4d51	1/2	302664	44(38)%	$(^3P)^2P$
29	4d85	5/2	300224	62(65)%	$(^3P)^2D$
30	4d41	1/2	294966	62(53)%	$(^1D)^2S$
31	4d83	3/2	312044	54(60)%	$(^3P)^2D$
				24(30)%	$(^1D)^2S$
				3%	$(^3P)^4F$
				5%	$(^3P)^4F$
				4%	$(^3P)^4D$
				5%	$(^1D)^2P$
				9%	$(^1D)^2G$
				14%	$(^3P)^2G$
				39(40)%	$(^3P)^2P$
				3%	$(^1S)^2D$
				11%	$(^3P)^4D$
				4%	$(^1S)^2D$
				3%	$(^3P)^2P$
				4%	$(^1D)^2P$
				22%	$(^3P)^4F$
				24(25)%	$(^3P)^2D$
				20%	$(^3P)^2F$
				7%	$(^1S)^2D$
				24(33)%	$(^1D)^2P$
				23(25)%	$(^3P)^2D$
				9%	$(^3P)^4F$
				22(19)%	$(^3P)^2F$
				17(16)%	$(^1D)^2D$
				11%	$(^3P)^2F$
				15%	$(^3P)^2F$
				26(26)%	$(^1D)^2D$
				16(16)%	$(^1D)^2D$
				36(41)%	$(^1D)^2P$
				38(37)%	$(^1D)^2P$
				20(21)%	$(^1D)^2D$
				62(65)%	$4s^2 S$
				20(22)%	$4s^2 S$
				20(18)%	$(^1S)^2D$
				12(17)%	$(^3P)^4P$
				8%	$(^1D)^2F$
				10%	$(^1D)^2D$
				7%	$(^1D)^2D$
				1%	$(^1D)^2G$
				4%	$(^1D)^2P$
				4%	$(^3P)^2F$
				7%	$(^1D)^2D$
				10(17)%	$(^1D)^2S$
				14%	$(^1S)^2D$
				8%	$(^1D)^2P$
				13(17)%	$(^1D)^2D$

<sup>a</sup> Present value from Table 3.

**Acknowledgments:** The spectrograms for this analysis were made in collaboration with Romuald Zalubas and Charles Corliss. They were used for our early work on Y VI [7]. I thank Craig Sansonetti and Haris Kunari for their careful reading of the manuscript.

**Conflicts of Interest:** The author declares no conflicts of interest.

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Review

# Spectral Analysis of Moderately Charged Rare-Gas Atoms

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Academic Editor: Joseph Reader

Received: 27 December 2016; Accepted: 21 February 2017; Published: 7 March 2017

**Abstract:** This article presents a review concerning the spectral analysis of several ions of neon, argon, krypton and xenon, with impact on laser studies and astrophysics that were mainly carried out in our collaborative groups between Argentina and Brazil during many years. The spectra were recorded from the vacuum ultraviolet to infrared regions using pulsed discharges. Semi-empirical approaches with relativistic Hartree–Fock and Dirac-Fock calculations were also included in these investigations. The spectral analysis produced new classified lines and energy levels. Lifetimes and oscillator strengths were also calculated.

**Keywords:** atomic spectra; energy levels; relativistic Hartree-Fock calculations

## 1. Introduction

There is great interest in spectroscopy data from rare gases due to applications in collision physics, fusion diagnostics, photo-electron spectroscopy, astrophysics, and to help understanding laser emission mechanisms. Information on wavelengths and intensities of the spectral lines and energy levels of moderately charged rare-gas atoms is important for these studies. Many processes must be considered in few times ionized atoms related with the widths and shapes of the spectral lines due to the presence of electric and magnetic fields. New spectral analysis of the  $p^2$ ,  $p^3$ ,  $p^4$  configurations of moderately ionized noble gases provide us with relevant information to understand the behavior of the atomic parameters in the intermediate type of coupling, when neither a pure electrostatic nor spin-orbit scheme exists.

In plasma physics, the radiative properties of atoms and ions are important for temperature determination and to calculate the concentrations of different plasma components. In the development of future tokamaks, damage by excessive heat load on the plasma-facing components is a major problem. In the ITER (International Thermonuclear Experimental Reactor) Tokamak, injection of krypton has been proposed to produce a peripheral radiating mantle that spreads the heat load, cooling the outermost plasma region and reducing erosion. In the plasma edge and in the divertor region, electron energy ranges from a few to about 100 eV corresponding to Kr I to Kr VIII spectra.

In astrophysics, the spectra of lower stages of ionization are found in space in nebulae, interstellar clouds, chemically peculiar stars, and in the sun. Several atomic parameters, such as energy levels, oscillator strengths, transition probabilities, and radiative lifetimes are important to determine many features of cosmic objects such as element abundance and electronic temperature. Transition probabilities are also needed to calculate the energy transport through the star in model atmospheres.

In this article, a comprehensive review is presented concerning the spectral analysis of several ions of neon, argon, krypton, and xenon, with deep and extended implications for astrophysical and laser studies that were mainly carried out in our collaborative groups between Argentina and Brazil

over many years. Using pulsed discharges, the spectra were recorded from the vacuum ultraviolet (VUV) to infrared regions. Semi-empirical approaches with relativistic Hartree–Fock (HFR) and multi-configurational Dirac-Fock (MCDF) calculations were used in the studies. A great number of new energy levels and classified lines were established, along with lifetimes and weighted oscillator strengths being reported in local and international meetings, distributed through internal reports, and published elsewhere. Regularities and systematic trends from the atomic structure were also used for the interpretation of the spectra.

## 2. Brief History

At the beginning of the 1960s, the activities related with Atomic Spectroscopy carried on by some of the present members of the Centro de Investigaciones Ópticas (CIOp), were centered on the measuring by interferometric methods of secondary standards in the thorium 232 wavelength. These works were done at the Physics Department of the Universidad Nacional de La Plata, under the direction of Athos Giacchetti [1].

From 1964, with the laser already known, research orientation was directed to subjects that can be defined as spectroscopy of the laser. The first works on this new field were made abroad, thanks to fellowships granted to the group members (currently M. Garavaglia, M. Gallardo and C.A. Massone) by the Swedish government. They dealt with noble gases and molecular nitrogen lasers. These works included the spectroscopy study of the emitted radiation, lines assignment, and the analysis of the excitation mechanisms of laser transitions [2–7].

When CIOp was constituted in 1977, investigations of noble gases were centered on studies about the spontaneous and laser spectroscopy of xenon. A pulsed electrical discharge tube was employed in two ways: as generator of stimulated emission in the blue-green and secondly in spontaneous emission developing very rich-in-lines spectra of the first ions of the gas [8,9].

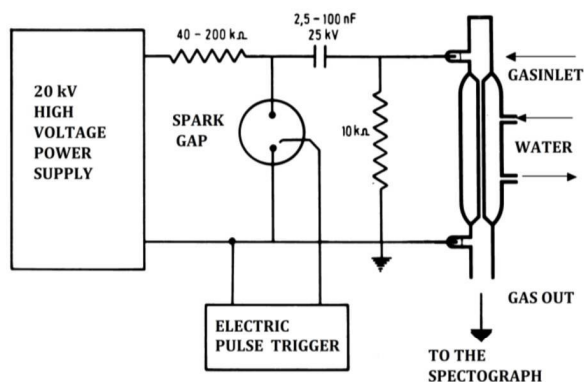
In 1985, A. G. Trigueiros, from Brazil, and J. Reyna Almandos made their postdoctoral studies at the Lund Institute of Technology, Sweden, under the direction of Willy Persson. They were working on the atomic emission spectroscopy of moderately rare gas ions, in particular in obtaining krypton spectra in the VUV region using a  $\theta$ -pinch as a spectral light source. Using these data an extended spectral analysis of the  $4s^2$ ,  $4s4d$ ,  $4p^2$ , and  $4s4p$  configurations in Zn-like six times ionized krypton was completed [10]. The interest in data belonging to this isoelectronic sequence is due to observations of impurity-lines from highly ionized heavy ions with few valence electrons in high temperature plasmas in which such lines have been used for diagnostic purposes. In particular, the resonant transition  $4s^2 1S_0-4s4p^1 P_1$  has been observed for a large range of  $Z$  values in the Zn I isoelectronic sequence.

Since 1986, when A.G.T. returned to the University of Campinas (UNICAMP), Brazil and J.R.A. to CIOp, Argentina, a strong collaboration began on the spectral studies of noble gases that involved both groups. At this point, it is important to mention the support provided to these first activities was given by W. Persson and I. Martinson from the University of Lund, Sweden, which included the donation of one spectrograph for work in the VUV region to the CIOp and two to the UNICAMP. With this equipment, it was possible to extend the spectral range for our studies and new and extended analysis of different ions of Kr, Xe, Ar, and Ne were carried out; some examples of these results were reported in [11–16] (and references therein).

## 3. Experimental Methods

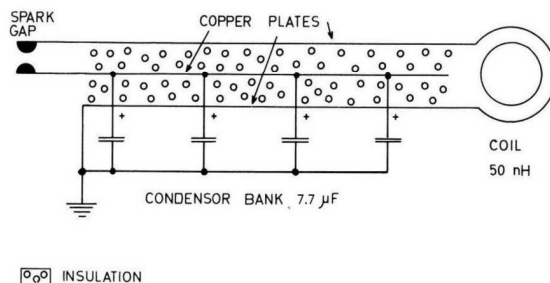
We have used two different light sources in our experiments, a pulsed electrical discharge tube and a  $\theta$ -pinch discharge.

The pulsed discharge tube was built at CIOp [16]. This light source consists of a Pyrex tube 100 cm in length and with an inner diameter 0.5 cm in which the gas excitation is produced by discharging a bank of low-inductance capacitors ranging from 20 to 280 nF, charged with voltages up to 20 kV. The schematic of the electric circuit is shown in Figure 1.



**Figure 1.** Schematic of the electric circuit. Reproduced and modified by permission of IOP Publishing from [16]. (© The Royal Swedish Academy of Sciences. All rights reserved.)

The second experiment was performed using a  $\theta$ -pinch discharge built at the Department of Physics, UNICAMP, where the energy was also fed into the plasma using a capacitor bank of  $7.7 \mu\text{F}$ , charged from a high-voltage power supply. A discharge tube with a length of 100 cm and an outside diameter of 8 cm was used. Figure 2 shows a schematic of the electric circuit and more details of the experiment can be found in Ref. [17].



**Figure 2.** Schematic of the  $\theta$ -pinch electric circuit. Reproduced and modified by permission of IOP Publishing from [18]. (© The Royal Swedish Academy of Sciences. All rights reserved.)

The wavelength range above  $2000 \text{ \AA}$  was observed in La Plata using a diode array detector coupled to the 3.4 m Ebert plane-grating spectrograph with 600 lines/mm and a plate factor of  $5 \text{ \AA/mm}$  in the first diffraction order. Photographic plates were used to record the spectra in the first, second, and third diffraction orders. The spectral lines observed were compared with interferometrically measured  $^{232}\text{Th}$  wavelengths [19] and with known lines of noble gas spectra. The positions of spectral lines were determined by means of a rotating prism photoelectric semiautomatic Grant comparator. For sharp lines, the settings are reproducible to within  $\pm 1 \mu\text{m}$ . A third-order interpolation formula was used to reduce comparator settings to wavelength values. Most of the spectral lines from this region used in the analysis were recorded in the third diffraction order. The accuracy of the thorium standard wavelength values used was on the order of  $0.005 \text{ \AA}$ , and the determination of the overall wavelength values of lines presented in this work was estimated to be correct to  $\pm 0.01 \text{ \AA}$ .

In the wavelength range below  $2100 \text{ \AA}$  light radiation emitted axially was analyzed using a 3 m normal incidence vacuum spectrograph with a concave diffraction grating of  $1200 \text{ lines mm}^{-1}$  and a plate factor in the first order of  $2.77 \text{ \AA mm}^{-1}$ . Kodak SWR and Ilford Q plates were used to record

the spectra. C, N, O, and known lines of noble gas spectra served as internal wavelength standards. The uncertainty of the wavelength below 2100 Å was estimated to be  $\pm 0.02$  Å. By observing the behavior of the spectral line intensity as a function of pressure and discharge voltage, we were able to distinguish the different ionic states of spectra.

Energy level values derived from the observed lines were determined by means of an iterative procedure that takes into account the wave numbers of the lines, weighted by their estimated uncertainties. The uncertainty of the adjusted experimental energy level values was assumed to be lower than  $2 \text{ cm}^{-1}$ .

With the above mentioned experimental devices, it was possible to record the spectra of Ne II-VII, Ar II-VIII, Kr II-VIII, and Xe II-IX in the region between 250 and 7000 Å.

#### 4. Atomic Calculations

Calculation of energy levels and transition probability in different spectral analysis has been carried out using the HFR approach [20]. Weighted oscillator strengths (gf), weighted transition probabilities (gA), and lifetimes were done for the experimentally known dipole transition and levels. Values were determined by using the Hartree-Fock method, including relativistic corrections and core-polarization effects with electrostatic parameters optimized by a least squares procedure in order to obtain energy levels adjusted to the corresponding experimental values in which core polarization refers to the deformation of the internal atomic orbitals due to the orbit of the active electron, which repels the remaining electrons [21]. In our work, we modified the electric dipole matrix elements to take core polarization effects into account. Other extensive calculation and studies on noble gas ions including this effect were also carried out by Biémont and co-workers [22–25]. In this last case, all the radial wave functions were also modified by a model potential, including one- and two-body core-polarization contributions, together with a core-penetration correction. In some of our studies, the fully relativistic MCDF approach was also used, more precisely the general-purpose relativistic atomic structure package (GRASP) [26]. These computations were done with an extended average level (EAL) option.

#### 5. Previous Works and Laser Studies

The spectral analysis of moderately charged rare-gas atoms has been carried out in our groups for many years. Studies on line shifts of Xe II, Xe III, Kr II, and Kr III in high current pinched discharges were also conducted. These shifts were observed when comparing the experimental values obtained through the pulsed discharge tube with those coming from a different kind of discharge [27]. By using a simple collision model, it was possible to show that these shifts may be attributed to the microscopic Stark effect [28,29].

Low-pressure xenon plasma excited by pulsed high-current-high-voltage electrical discharges produces high-gain laser transitions in the near UV and visible. Thus, knowledge of the spectral analysis corresponding to different involved ions, is necessary to understand the population mechanisms responsible for most of the classified laser xenon transitions. Pulsed discharges have been used in La Plata to produce laser action at UV, visible, and infrared (IR) wavelengths corresponding to Xe III, Xe V, Xe VII, Xe VIII [30–33], Xe VI, and Xe IX [16,25]. In these investigations, time-resolved experiments were also done and relativistic Hartree-Fock calculations were also performed to obtain weighted lifetimes and radiative transition rates.

#### 6. Some Recent Results on Xe, Ar and Kr Ions

The spectral analysis of several ions of xenon has a relevant impact on astronomy and laser studies. Various atomic parameters such as energy levels, oscillator strengths, transition probabilities and radiative lifetimes have many important astrophysical applications. Transition probabilities are needed for calculating the energy transport through the star in model atmospheres [34] and for direct analysis of stellar chemical compositions [35]. Xenon is a very rare element in the cosmos, observed in

chemically peculiar stars [36] and in planetary nebulae [37]. Emission lines of Kr III–V, Xe III–V in a sample of planetary nebulae were identified [38] and Kr VI, Kr VII, Xe VI and Xe VII lines were recently observed in the ultraviolet spectrum of the hot DO-type white dwarf RE 0503-289 [39].

### 6.1. Xe V

In a recent spectral analysis of four times ionized xenon, Xe V, 12 new energy levels belonging to the  $5s^2 5p6d$  and  $5s^2 5p7s$  configurations and 81 new classified lines were reported [40]. Using relativistic Hartree–Fock and multi-configurational Dirac–Fock calculations, the lifetimes and weighted oscillator strengths were calculated. Table 1 shows the new energy levels belonging to the configurations  $5s^2 5p6d$  and  $5s^2 5p7s$  and the percentage composition of these levels obtained in the least-squares fit. The calculated radiative lifetimes are also presented. The configurations involved in these transitions were  $5s^2 5p6p$ ,  $5s^2 5p4f$  and  $5s5p^3$ ,  $5s^2 5p5d$ ,  $5s^2 5p6d$ ,  $5s^2 5p6s$ , and  $5s^2 5p7s$  for the even and odd parities. The weighted oscillator strengths for the observed lines were calculated considering fitted values for the energy parameters. The lifetime values calculated with the GRASP program are presented in the Babushkin gauge since this one, in the non-relativistic limits and in many situations, has been found to be the most stable value, in the sense that it converges smoothly as more correlation is included and is less sensitive to the details of the computational method [41].

**Table 1.** Experimental and calculated energy levels established for the  $5s^2 5p6d$  and  $5s^2 5p7s$  configurations of Xe V. Calculated radiative lifetimes are also given. Reproduced with permission from [40]. (© IOP Publishing. All rights reserved.)

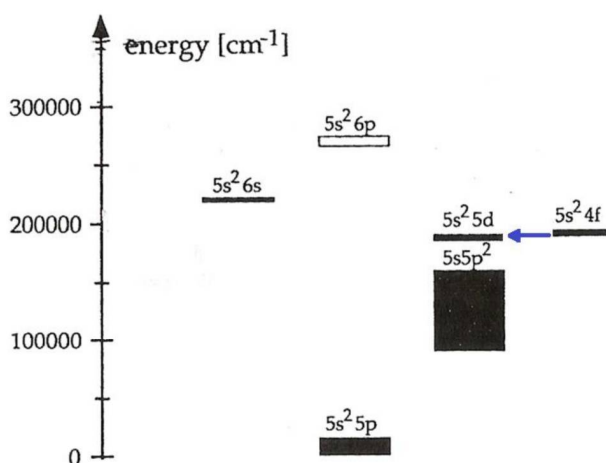
Level	Energy Obs (cm <sup>-1</sup> )	Percentage Composition <sup>a</sup>	Lifetime (ns)		
			HFR	GRASP	
$5s^2 5p6d$	$^3F^{\circ}_2$ 284871 <sup>b</sup>	$72 5s^2 5p6d \ ^3F + 17 5s^2 5p6d \ ^1D$	0.48	0.41	
	$^3D^{\circ}_2$ 287391 (5)	$20 5s^2 5p6d \ ^3P + 20 5s^2 5p6d \ ^3D + 20 5s^2 5p6d \ ^1D$	0.29	0.23	
	$^3F^{\circ}_3$ 287696 (6)	$36 5s^2 5p6d \ ^3F + 17 5s^2 5p6d \ ^3D + 14 5s^2 5p6d \ ^1F$	0.53	0.27	
	$^3D^{\circ}_1$ 288830 (6)	$51 5s^2 5p6d \ ^3D + 16 5s^2 5p6d \ ^1P + 13 5s^2 5p6d \ ^3P$	0.28	0.16	
	$^3F^{\circ}_4$ 298739 (3)	$88 5s^2 5p6d \ ^3F$	0.65	0.55	
	$^1D^{\circ}_2$ 299596 (3)	$46 5s^2 5p6d \ ^1D + 17 5s^2 5p6d \ ^3D + 16 5s^2 5p6d \ ^3F$	0.34	0.21	
	$^3D^{\circ}_3$ 300327 (6)	$54 5s^2 5p6d \ ^3D + 23 5s^2 5p6d \ ^3F$	0.28	0.21	
	$^3P^{\circ}_2$ 301483 (6)	$21 5s^2 5p6d \ ^3P + 25 5s^2 5p6d \ ^3D + 14 5s5p^2 6p \ ^5P$	0.37	0.23	
	$^3P^{\circ}_1$ 301555 (5)	$51 5s^2 5p6d \ ^3P + 20 5s^2 5p6d \ ^3D + 15 5s5p^2 6p \ ^3D$	0.31	0.21	
	$^3P^{\circ}_0$ 301998 (2)	$90 5s^2 5p6d \ ^3P$	0.38	0.25	
	$^1F^{\circ}_3$ 304985 <sup>b</sup>	$68 5s^2 5p6d \ ^1F + 14 5s^2 5p6d \ ^3D$	0.24	0.14	
	$^1P^{\circ}_1$ 306065 (7)	$41 5s^2 5p6d \ ^1P + 19 5s5p^2 6p \ ^5P + 16 5s^2 5p6d \ ^3P$	0.35	0.21	
	$5s^2 5p7s$	$^3P^{\circ}_0$ 297673 <sup>b</sup>	$96 5s^2 5p7s \ ^3P$	0.16	0.19
		$^3P^{\circ}_1$ 298053 (4)	$69 5s^2 5p7s \ ^3P + 28 5s^2 5p7s \ ^1P$	0.15	0.18
$^3P^{\circ}_2$ 312956 (3)		$97 5s^2 5p7s \ ^3P$	0.18	0.23	
$^1P^{\circ}_1$ 313883 (4)		$67 5s^2 5p7s \ ^1P + 27 5s^2 5p7s \ ^3P$	0.14	0.15	

Notes: <sup>a</sup> Percentages below 5% have been omitted. <sup>b</sup> Calculated value. ( ) Number of transitions used for establishing the levels. HFR, relativistic Hartree–Fock calculations. GRASP, general-purpose relativistic atomic structure package.

### 6.2. Xe VI

A new laser line at 33224.0 Å, corresponding to the five-times ionized xenon spectrum and classified as  $5s^2 4f \ ^2F_{7/2} - 5s^2 5d \ ^2D_{5/2}$  was recently observed. Semi-empirical calculations using energy parameters adjusted from least-squares were done and the obtained lifetimes were 10.55 ns and 0.055 ns for the upper and lower levels, respectively. The calculated transition probability value was  $2.4 \times 10^5 \text{ s}^{-1}$ . In Figure 3 the gross structure of the low configurations and the laser transition observed in Xe VI is shown.





**Figure 3.** New  $5s^2 4f^2 F_{7/2} - 5s^2 5d^2 D_{5/2}$  laser line at 33224.0 Å. Reproduced by permission of IOP Publishing from [42]. © The Royal Swedish Academy of Sciences. All rights reserved.)

The first detection of krypton and xenon in a white dwarf [39], encouraged us to extend the spectral analysis of five times ionized xenon, Xe VI. In our work the xenon spectra were recorded in the 400–5700 Å region and 243 lines were observed in the experiments, 146 of which were determined for the first time. 32 new and 33 revised energy levels were reported [43]. The gf, gA and lifetimes were calculated using the HFR approach and HFR plus core polarization (HFR+CP) effects. All Xe VI lines observed in the spectrum of the hot DO-type white dwarf RE 0503-289 by Werner et al. [39] were confirmed. The Xe VI analysis is difficult because of the strong mixing of level composition and the non-smooth behavior of the structure which together result in changes in level positions and composition along the isoelectronic sequence. By using all this research, a new paper on the Xe VI ultraviolet spectrum and the xenon abundance in the hot DO-type white dwarf RE 0503-289 was also reported [44].

### 6.3. Xe VII and Xe VIII

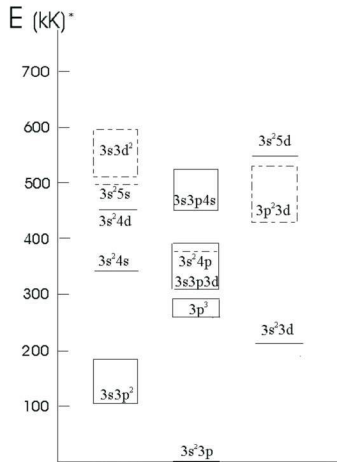
Considering that the red laser line at 6699.40 Å remains unclassified and taking into account the detection of Xe VII in a white dwarf [39], we have decided to make a new spectral analysis of the six- and seven-times ionized xenon spectra. Thus, by using our experimental data covering the wavelength range 430–4640 Å, 40 new transitions of Xe VII and 25 of Xe VIII were classified. We have also revised the values for the previously known energy levels and extended the analysis for Xe VII to 10 new energy levels belonging to  $5s6d$ ,  $5s7s$  and  $5s7p$ ,  $4d^9 5s^2 5p$  even and odd configurations, respectively. Seven new energy levels of the  $4d^9 5s 5d$  core excited configuration of Xe VIII were determined [45]. Relativistic Hartree–Fock and least-squares-fitted parametric calculations were used in the interpretation of the observed spectra.

### 6.4. Ar VI

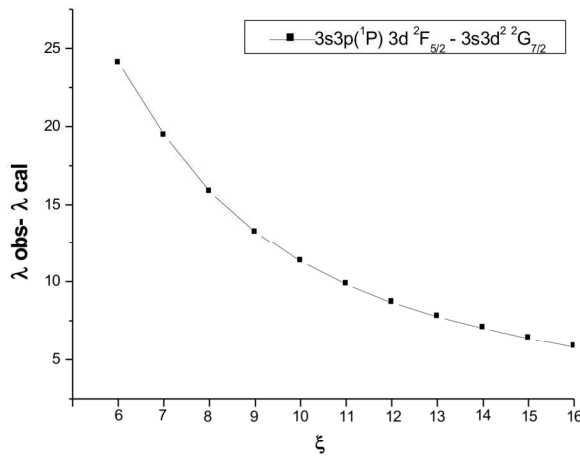
The analysis of the atomic spectra of five times ionized argon (Ar VI), that belongs to the Al I isoelectronic sequence, can be used for studies related with electron-correlation calculations of excited-state structures. As another example of noble gas studies that also have astrophysical interest, an extended analysis of the  $3s^2 4p$ ,  $3s^2 5d$ ,  $3s^2 5s$ ,  $3s 3d^2$ ,  $3s 3p 3d$ ,  $3s 3p 4p$ , and  $3p^2 3d$  configurations in Ar VI, including the determination of new classified lines and energy levels belonging to these configurations, using Al I isoelectronic data and HFR calculations, was completed. Atomic transitions

are expected to be prominent in the absorption spectra of interstellar gas clouds [46], and Ar ions have been identified in the Markarian 3 galaxy [47] Chandra HETGS spectrum. In our analysis 14 new energy levels for the configurations  $3s3p3d$ ,  $3s^24p$ ,  $3s^25s$ ,  $3p^23d$ ,  $3s3d^2$  were established, and two adjusted energy levels for the configuration  $3s^25d$  and 68 new spectral lines were classified [48]. Rydberg series interactions for the  $3s3p3d$  configuration were included as their configuration interaction integrals have shown significant values.

Figure 4 shows the gross structure of the Ar VI configurations and in Figure 5 the behavior of the  $\lambda_{\text{obs}} - \lambda_{\text{cal}}$  versus the net charge for the  $3s3p(^1P)3d\ ^2F_{5/2} - 3s3d^2\ ^2G_{7/2}$  transition in the Al I sequence is shown.



**Figure 4.** Gross structure of the experimental and theoretical (dotted line) Ar VI configurations. ‘kK’ means  $10^3\text{ cm}^{-1}$ . Reproduced by permission of IOP Publishing from [48]. (© The Royal Swedish Academy of Sciences. All rights reserved.)



**Figure 5.**  $\lambda_{\text{obs}} - \lambda_{\text{cal}}$  versus the net charge for the  $3s3p(^1P)3d\ ^2F_{5/2} - 3s3d^2\ ^2G_{7/2}$  transition in the Al I sequence. Reproduced by permission of IOP Publishing from [48]. (© The Royal Swedish Academy of Sciences. All rights reserved.)

6.5. Kr V

Forbidden lines belonging to Kr V transitions were found in many nebulae, such as NGC 2440 [49], IC2501 [49], IC4191 [49], and Hen2-436 [50]. The forbidden Kr V lines have not been directly observed at the laboratory, and their wavelengths are presumed from energy differences between the ground configuration levels. Therefore, a precise determination of such levels is crucial for the establishment of the wavelengths of these lines.

Using experimental data from a 0-pinch and a pulsed discharge, an extended analysis of the Kr V spectrum was conducted. The spectrum was recorded in the 230–4900 Å wavelength range, resulting in 91 new classified lines. We were able to identify 21 new energy levels belonging to the  $4s^2 4p^5 d$ ,  $4s^2 4p^5 s$ ,  $4s^2 4p^6 s$ ,  $4s^2 4p^5 p$ , and  $4s 4p^2 4d$  configurations [51]. Relativistic Hartree–Fock calculations were used to predict energy levels and transitions and, at this stage, it is important to mention the strong interaction that exists between the ground configuration with the  $4p^4$  and the  $4s 4p^2 4d$  configurations in this ion. This behavior was also observed with the  $s^2 p^2$ ,  $p^4$ , and  $sp^2 d$  configurations in the spectral analysis of Xe V and Ar V [31,52].

After this research, a new study on lifetimes and transition probabilities in four times ionized krypton was completed. The gf, gA and lifetimes were calculated for all experimentally known dipole transitions and levels of Kr V. The values were determined by four methods. Three of them were based on the Hartree–Fock method including relativistic corrections (the first including a small set of configurations, the second a large set, and the third including core-polarization effects) with electrostatic parameters optimized by a least-squares procedure, in order to obtain energy levels adjusted to the corresponding experimental values. The fourth method was based on a relativistic multiconfigurational Dirac–Fock approach. The 313 dipole electric lines reported in the 294–3615 Å region, included 47 new classified lines [53]. In this investigation, we have also related the observed line intensity with  $\log_{10}(gA)$  by the statistical correlation coefficient. The analysis was disaggregated by transition arrays between configurations, i.e., between levels with the same set of dominant configurations in their eigenvector composition. Thirteen sets of transitions were identified, and results are shown in Table 2. Comparing the correlation factors, the best results are for HFR large set of configurations, with or without CP, with an average value of 0.40. These calculations display the best values for more than half of the arrays analyzed. The inclusion of CP effects does not cause significant differences in results.

**Table 2.** Statistical correlation between  $\log_{10} gA$  and experimental line intensity. Maximum correlation for each transition array in boldface. Reproduced with permission from [53]. (© IOP Publishing. All rights reserved.)

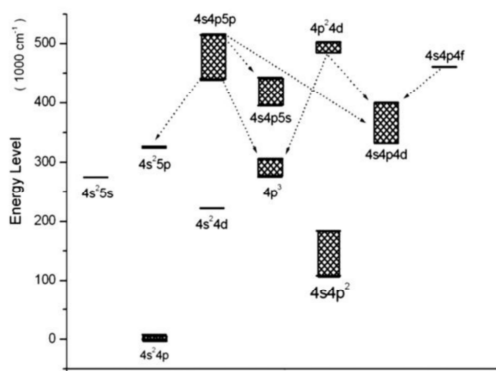
Transitions Arrays	HFR Small Set	HFR Large Set	HFR Large Set + CP	GRASP Babushkin Gauge	Number of Lines	Interval (Å)
$4s^2 4p^2 : 4p^5 s$	0.77	0.77	0.77	0.62	12	404.45–495.72
$4p^5 s : 4p^5 p$	0.59	0.62	0.62	0.52	21	1498.28–3058.63
$4p^4 d : 4p^4$	0.27	0.58	0.58	0.23	6	780.27–3058.63
$4s 4p^3 : 4s 4p^2 4d$	0.19	0.48	0.55	0.03	11	650.27–1131.28
$4s 4p^3 : 4p^4$	0.36	0.45	0.45	0.53	10	526.57–1131.28
$4s^2 4p^2 : 4s 4p^3$	0.35	0.39	0.39	0.35	29	515.35–909.63
$4s 4p^2 4d : 4p^5 d$	0.33	0.33	0.33	−0.55	12	909.63–1735.48
$4s 4p^3 : 4p^5 p$	0.41	0.39	0.39	0.50	39	561.80–1735.48
$4p^4 d : 4p^5 p$	0.44	0.46	0.46	0.31	52	940.55–2426.06
$4p^5 p : 4p^6 s$	0.17	0.21	0.21	0.44	16	1184.84–2426.06
$4p^5 p : 4p^5 d$	0.30	0.27	0.27	0.38	40	1240.02–2069.37
$4p^4 d : 4s 4p^2 4d$	−0.13	0.33	−0.27	0.10	11	1131.57–2442.34
$4s^2 4p^2 : 4p^4 d$	−0.10	−0.09	−0.10	0.15	31	420.67–2442.34
<b>Average</b>	<b>0.30</b>	<b>0.40</b>	<b>0.40</b>	<b>0.28</b>		

Notes: CP, core polarization.

## 6.6. Kr VI

In the first work carried out on this ion the spectrum of five-time ionized krypton was recorded in the 240–2600 Å using both light sources previously described. The study involved the 4s4p4d and the 4s4p5s configurations resulting in 109 new line classifications and 22 new energy levels [54]. This analysis also showed the strong interaction between the 4s4p4d configurations and the other  $n = 4$  complex configurations. Oscillator strengths calculated from fitted values of the energy parameters that give gf values that are in better agreement with line intensity observations, were also reported [55].

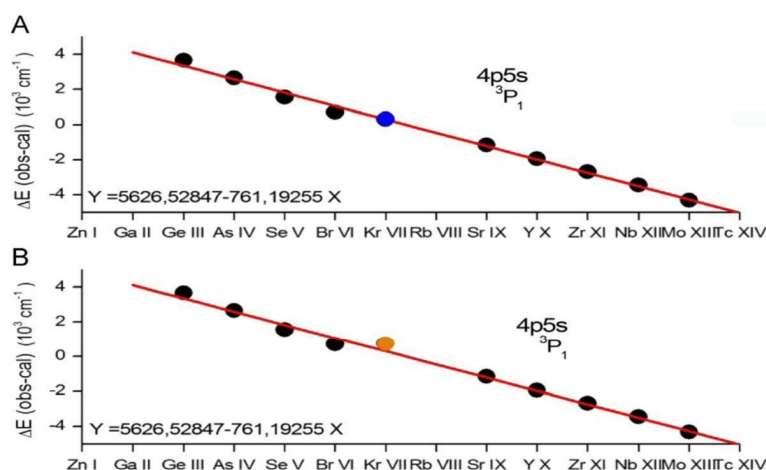
In a recent analysis [56], 61 lines as transitions between levels of configurations  $4p^3$ ,  $4s^25p$ ,  $4s4p4d$ ,  $4s4p5s$ , and  $4s4p5p$  were classified for the first time and all the 18 energy levels belonging to  $4s4p5p$  configuration except one were determined. Eight new energy level values corresponding to configurations  $4s4p4f$  and  $4p^24d$ , supported by 26 new classified lines, were also determined and used in the interpretation of the observed  $4s4p5p$  configuration. In Figure 6, the gross structure of the observed Kr VI configurations is shown. The dashed arrows indicate the  $4s4p5p-4p^3$ ,  $4s4p5p-4s^25p$ ,  $4s4p5p-4s4p4d$ , and  $4s4p5p-4s4p5s$  transitions identified in this work.



**Figure 6.** Gross structure of the observed Kr VI configurations. Reproduced by permission of IOP Publishing from [56]. (© The Royal Swedish Academy of Sciences. All rights reserved.)

## 6.7. Kr VII

Six times ionized krypton belongs to the Zn I isoelectronic sequence and has the ground configuration  $3d^{10}4s^2$ . Due to the considerable interest in the diagnosis of high-temperature laboratory and astrophysical plasmas, the spectra of this sequence has been extensively studied and the first detection of Kr VII in a white dwarf was recently reported [39]. The spectra of the Zn-like Kr ion has been studied by the use of different light sources and by using a  $\theta$ -pinch and a pulsed electrical discharge tube [16] in the region from 300 to 4800 Å. The values for the previously known energy levels were revised and a new extended analysis resulting in 115 new classified lines and 38 new energy levels belonging to  $4s5s$ ,  $4s6s$ ,  $4p4f$ ,  $4s6d$  and  $4p4d$ ,  $4s5p$ ,  $4s4f$ ,  $4p5s$ ,  $4s5f$ ,  $4s6p$ ,  $4s6f$  even and odd configurations were completed [57]. For the prediction of the energy level values we studied the behavior of the difference between the observed and calculated energy values along the isoelectronic sequence. As an example, Figure 7 shows the interpolated value for the  $4p5s\ ^3P_1E_{\text{obs}} - E_{\text{cal}}$  of Kr VII in the Zn-like sequence. The adjusted energy difference value represented in A using our new energy level value in  $587029\text{ cm}^{-1}$  fits better than the value in  $587068\text{ cm}^{-1}$  reported in Ref. [58], as shown in B.



**Figure 7.** Interpolated value for the  $4p5s \ ^3P_1 E_{\text{obs}} - E_{\text{cal}}$  of Kr VII in the Zn-like sequence. Our new adjusted energy difference value represented in (A) fits better than the value reported in Ref. [58]; as shown in (B). Reproduced by permission of IOP Publishing from [57]. (© The Royal Swedish Academy of Sciences. All rights reserved.)

We have recently reported the study of the  $4p^2$ ,  $5p^2$ , and  $5s5f$  excited configurations of the Zn I and Cd I isoelectronic sequences, using relativistic and non-relativistic semi-empirical approaches [59]. The configuration  $5s5f$  was also analyzed taking into account the Landé's interval rule. In this research, different semi-empirical approaches considering the linearity of the Slater integrals for large  $Z$ , the smoothness of the  $sF$  screening parameters, the energy values in terms of  $Z$ , and the differences of the  $E_{\text{obs}} - E_{\text{cal}}$  values were used.  $E_{\text{cal}}$  values means the energies calculated with HFR, and  $E_{\text{obs}}$  are the experimental values.

It is important to mention that most of our results on the studied xenon, krypton, and argon gases were critically compiled and reported by E.B. Saloman [60–62] and an extension and new level optimization of the Ne IV spectrum, that includes our line identification on this gas, was recently made by A. Kramida [63]. Also our previous results a new Kr IV–VII oscillator strengths and an improved spectral analysis of the hot, hydrogen-deficient DO-type white dwarf RE 0503-289, and a new Zr IV–VII, Xe IV-V, and Xe VII oscillator strengths and the Al, Zr, and Xe abundances in the hot white dwarfs G191-B2B and RE 0503-289 were very recently reported [64,65].

## 7. Conclusions

A comprehensive review concerning the spectral analysis of several moderately charged rare-gas atoms carried out by our international collaborative groups was presented. New and earlier analyses for these ions were revised and extended. Semi-empirical approaches with relativistic Hartree–Fock and Dirac-Fock calculations were used in the studies. The spectra were recorded from the VUV to the near-IR regions using two different light sources, a pulsed electrical discharge tube, and a  $\theta$ -pinch discharge.

It is important to point out that both spectral sources, together with the detection and measuring systems previously described, allowed us to generate a large amount of new spectral data with very good accuracy in a wide spectral range. Some experimental data used for the study of moderately charged rare-gas atoms, obtained with other kinds of spectral sources such as beam-foil or collision-based spectroscopy, were improved.

Most of our experimental data were obtained using the pulsed electrical discharge tube source. An important characteristic of this light source is that it generates very rich ion spectra, requiring much less capacity and current in the electric discharge, and producing ion spectra like those generated in the  $\theta$ -pinch.

The pulsed electrical discharge tube also showed that it is a very suitable spectral source for the studies related with the population mechanisms involved in the laser emission of different xenon ions. It is important to continue these works using both time-resolved and frequency spectroscopy under different experimental conditions, together with lifetimes and transition probability calculations for the involved energy levels and lines responsible for the laser emission. Specifically, it is important to extend the theoretical and experimental studies in eight times ionized xenon, where stimulated emission in the VUV was observed on the  $4d^9 5p\ ^1P_1-4d^9\ 5d\ ^1S_0$  transition in the Pd-like Xe ion. It is necessary to analyze how the  $4d^9\ 4f$  configuration affects the plasma dynamics in the Pd-like ions, where the  $4d^9 4f\ ^1P_1-4d^9\ 5d\ ^1S_0$  transition has conditions for laser action in high ions on this sequence. Similar studies on this subject in the Ne-like and Ni-like ions are also important to conduct.

The experimental device that we used to obtain noble gas spectra can also be applied for the study of non noble gases. In fact, the pulsed electrical discharge tube was used in the works on the  $N_2$  laser, showing very high accuracy in the obtained results [3–5]. The  $\theta$ -pinch discharge was also used for oxygen ion studies [66] (and references therein).

Interpreting the atomic observations theoretically and by testing computational predictions by experimental data are interactive processes. In the comparison, the high resolution spectral data show better computational results. This was used in all our works.

Discrepancies between experimental measurements and the theoretical calculations led us to carry out more accurate predictions of the allowed and forbidden transitions. MCDF calculations including more active orbitals enabled dealing with a larger amount of excited configurations. The differences of the gauge values in length and velocity of the E1 oscillator strengths obtained showed the accuracy of our calculations GRASP in the performed studies on Kr V, Xe V, and Xe IX.

In HFR calculations for Kr V, Xe V, Xe VI, and Xe IX, CP effects were included, which, combined with a semi-empirical optimization of radial parameters, minimized the discrepancies between the calculated levels of energy and those experimentally obtained. In this type of calculation, the cancellation factors [20] were also assessed, indicating when the oscillator intensities and transition probabilities were affected by great uncertainty.

The spectral analysis of ionized noble gases related with astrophysics and laser studies will be continued in our future work by using the obtained experimental material, different computational calculations, and semi-empirical approximations.

During all these years of fruitful work, fluid collaborations involved groups working on similar subjects in Argentina (Centro de Investigaciones Opticas, Universidad Nacional del Centro, and Universidad Nacional de Mar del Plata); in Brazil (University of Campinas, Universidad Federal Fluminense, and Universidad Federal de Roraima); in Colombia (Universidad del Atlántico); and in Sweden (University of Lund). These collaborations generated mutual visits performed by scientists and students for courses and/or joint work, the exchange of scientific material, the production of more than a dozen of PhD theses, more than seventy international papers, three book chapters, and various reports to international conferences.

**Acknowledgments:** The careful reading and comments of the manuscript by M. Garavaglia, and Dra. M. Tebaldi are gratefully acknowledged. The Comisión de Investigaciones Científicas de la Provincia de Buenos Aires (CICPBA), Argentina—where J.G. Reyna Almandos and M. Raineri are researchers—is also gratefully acknowledged.

**Author Contributions:** J.R.A. conceived and wrote the paper. M.R. had important participation in the discussions on the final version.

**Conflicts of Interest:** The authors declare no conflict of interest.

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Article

# Resonance Transitions in the Spectra of the $\text{Ag}^{6+}$ – $\text{Ag}^{8+}$ Ions

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Academic Editor: Joseph Reader

Received: 16 January 2017; Accepted: 21 February 2017; Published: 4 March 2017

**Abstract:** The spectrum of silver, excited in a vacuum spark, was recorded in the region 150–350 Å on a 3-m grazing incidence spectrograph. The resonance  $4d^k$ –( $4d^{k-1}5p + 4d^{k-1}4f + 4p^54d^{k+1}$ ) was studied in the  $\text{Ag}^{6+}$ – $\text{Ag}^{8+}$  spectra (Ag VII–Ag IX) with  $k = 5$ – $3$ , respectively. Several hundred lines were identified with the aid of the Cowan code and orthogonal operator technique calculations. The energy levels were found and the transition probabilities were calculated.

**Keywords:** vacuum ultraviolet; ion spectra; wavelengths; energy levels; transition probabilities; parametric calculations

## 1. Introduction

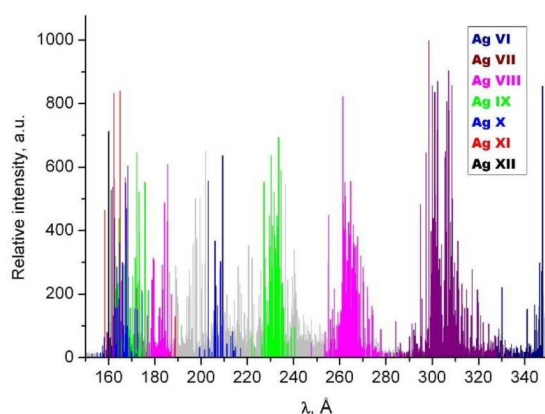
Six- through eight-times ionized silver atoms are the members of the isonuclear sequence of the silver ions with the unfilled  $4d^k$  ( $k = 5$ – $3$ ) ground-state configuration. The spectra of these ions have not been investigated previously. The excitation of the  $4d$  electron leads to the lowest odd configurations  $4d^{k-1}5p$  and  $4d^{k-1}4f$ . The third odd configuration  $4p^54d^{k+1}$  is formed by the excitation of the inner shell  $4p$  electron. The resonance transitions are represented by the transitions from these odd configurations to the ground-state configuration. Out of all resonance transitions only the  $4d^k$ – $4d^{k-1}4p$  ( $k = 9$ – $6$ ) ones were previously studied in the silver spectra of the lower ionization stages: Ag III [1], Ag IV [2], Ag V [3] and Ag VI [4]. On the other hand, all three resonance transition arrays were investigated in rather simple spectra of ions having  $4d$  and  $4d^2$  ground-state configurations: Ag XI [5,6] and Ag X [7]. In this article we report the results of the study of the Ag VII, Ag VIII and Ag IX to fill the gap between the Ag VI and Ag X isonuclear spectra.

This study is part of a project to get atomic data for the ions of lighter than tin chemical elements isoelectronic with Sn IX–Sn XIV which are relevant to a development of bright source for projection lithography at the 135 Å wavelength. The results for the palladium isonuclear spectra were recently published (see [8] and references therein). Such isoelectronic data are necessary for validation of previously reported analyses of the corresponding tin ion spectra [9,10]. Research on these spectra is also of general interest to atomic physics for improving of theoretical methods of calculations of multi-electron heavy atom spectra.

## 2. Experiment

The experimental technique and the theoretical approaches for spectrum calculations were the same as in our previous publications [7,8]. Briefly, the light source was a low-inductance vacuum spark operated with an additional inductance up to 2.5  $\mu\text{H}$ . A 150 or 12  $\mu\text{F}$  capacitor was charged up to 4.5 kV resulting in the spark peak current in a range of  $\sim 10$ – $20$  kA. Ionization stages were distinguished by comparing the intensities of the lines at various peak currents. A 3 m grazing

incidence spectrograph (85° angle of incidence) equipped with a gold coated holographic grating having 3600 lines/mm was used for taking the spectra. A plate factor of the spectrograph in the region 160–350 Å was 0.32–0.46 Å mm<sup>-1</sup> respectively. The spectra were recorded on Kodak SWR photographic plates (Eastman Kodak Company, Rochester, NY, USA) and measured on an EPSON EXPRESSION 10000XL scanner (Seiko Epson Corporation, Suwa, Japan). Wavelengths were calibrated using titanium ion lines [11] as the standards. The titanium spectrum was superimposed on some silver exposures. The measured wavelength uncertainty is estimated as ±0.005 Å for the unperturbed lines of moderate intensity. General view of the silver spectrum in the region 150–350 Å is shown in Figure 1, where the lines identified in this work, previously identified, and remaining unidentified are marked by different colours depending on particular spectrum.



**Figure 1.** Spectrum of silver in the region 150–350 Å excited in a vacuum spark. Lines of different ion spectra are marked by different colours: Ag VI—royal blue, Ag VII—wine, Ag VIII—magenta, Ag IX—green, Ag X—blue, Ag XI—red, Ag XII—black and unidentified lines—gray.

The relative line intensities were obtained as described in our previous article [8] “from the measured optical densities using an approximate photoplate response curve estimated from different experiments. They should be considered mostly as qualitative ones because of some uncertainty of used photoplate response curve and neglect of the wavelength dependence of the spectrograph efficiency and photoplate sensitivity. Also the saturation effects resulting from the photoplate response nonlinearity can significantly influence the intensity ratios of the weak to strong lines.” The intensity  $I = 1000$  was attributed to the strongest line of the  $4d^k-4d^{k-1}5p$  transition array in each ion spectrum.

The program IDEN [12] was used for the spectrum identification. As in [8], ab initio calculations were performed with the use of the Dirac–Fock (DF) code of Parpia et al. [13], or by the Hartree–Fock method with relativistic corrections (HF) with the use of the Cowan code (Cowan programs RCN, RCN2, RCG, and RCE) [14]. Semiempirical correction of ab initio values of Slater parameters was made with the RCE Cowan code or by using a technique of orthogonal operators [15–18].

The energies derived after the identification of spectral lines were optimized using the program LOPT [19].

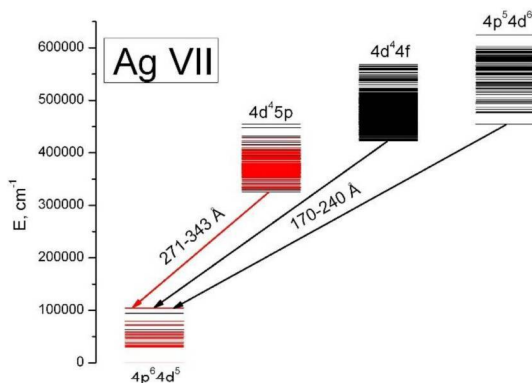
### 3. Results

In the following, the results of the analyses of silver ions in the charge states Ag<sup>6+</sup>, Ag<sup>7+</sup> and Ag<sup>8+</sup> are presented. Line identifications are summarized in Tables A1–A4 (see Appendix A at the end of the document) and energy levels are collected in Tables A5–A11. The data were interpreted using semi-empirical orthogonal parameters and Cowan code calculations resulting in calculated values

for the energy levels, wave-function composition, transition probabilities and energy parameters. The semi-empirical energy parameters and their comparison with the corresponding ab initio values are shown in Tables A12–A14.

### 3.1. Ag VII

A diagram of the low lying configurations of Ag VII with the ground-state configuration  $4d^5$  is shown in Figure 2. As in the case of silver ions in lower stages of ionization (Ag III–Ag VI) we were able to make the analysis of only the  $4d^5$ – $4d^45p$  transition array (Table A1). The lines of these transitions are represented by a compact group in the region 271–343 Å mostly isolated from the other transitions in Ag VII as well as in the neighboring ions (see Figure 1). Three hundred and seventy-eight lines were identified in this transition array, 47 of them were doubly and one trebly identified. Eight lines are probably blended with previously identified Ag VI transitions. Thirty-four levels out of 37 possible  $4d^5$  ones were found (Table A5) and 142 levels of the  $4d^45p$  configurations were located out of 180 possible levels (Table A6). The relative uncertainty of the level energies given by least-squares optimization [19] ranges from 1 to 4  $\text{cm}^{-1}$  for  $4d^5$  levels and from 3 to 8  $\text{cm}^{-1}$  for  $4d^45p$  depending on the number of lines used for the level optimization and on their wavelength uncertainties. Identification was performed with the help of the semi-empirical calculations based on the orthogonal operators. The initial orthogonal energy parameters were extrapolated along the sequence Ag IV–Ag V. Final energy parameters of Ag VII after a fitting of the calculated levels to the found levels are listed in Tables A12 and A13. They are compared with the values from the Parpia et al. code [13]. Only the parameters of the  $4d^5$  and  $4d^45p$  configurations are listed in the tables although the matrixes of the interacting  $4d^5 + 4d^45s + 4d^35s^2$  (even) and  $4d^45p + 4d^35s5p + 4d^25s^25p$  (odd) configurations were used in the fittings. The parameters of the unknown configurations were fixed on extrapolated values; the interaction parameters were fixed on values obtained with scaling by 0.85 of the ab initio integrals.



**Figure 2.** Energy levels of Ag VII. The arrows show electric dipole transitions. The levels found in this work and studied transitions are marked by red color. Black color indicates unknown levels and transitions.

In a treatment of the  $4d^5$  shell (as well as of the other  $4d^k$  shells) by the orthogonal parameter technique O2, O2', Ea' and Eb' are the orthogonal counterparts of the traditional parameters  $F^2(4d,4d)$ ,  $F^4(4d,4d)$ ,  $\alpha$  and  $\beta$ . The one-electron magnetic (spin-orbit) operator  $\zeta(4d)$  and the effective 3-particle electrostatic operators T1 and T2 are the same as in Cowan code and (Ac...A0) are additional 2-body magnetic parameters. The  $4d^45p$  configuration and the other  $4d^{k-1}5p$  configurations contain additional parameters: C1dp–C3pd are the orthogonal counterparts of the Slater exchange integrals

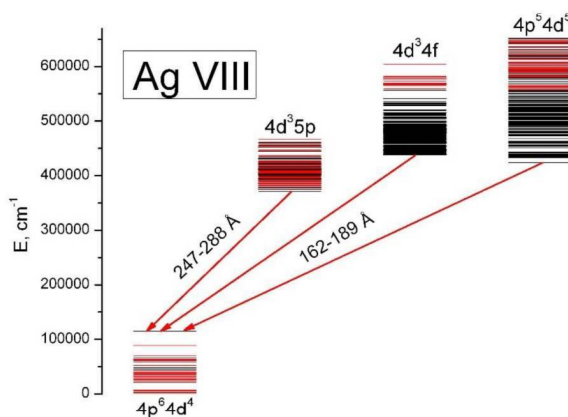
$G^1(4d,5p)-G^3(4d,5p)$ ;  $S1dp$ ,  $S2dp$  are the effective electrostatic 2-body  $dp$ -parameters;  $Sd.Lp \dots SS(dp)20$  are magnetic 2-body  $dp$ -parameters [15], and  $T16$  to  $T35$  are the electrostatic 3-body  $ddp$ -parameters. In case of Ag VII 2-body magnetic parameters were varied at the fitting on one bunch keeping the ratios of the corresponding  $ab$  initio values. Root mean square deviations of the fitting  $\sigma$  were 14 and  $19 \text{ cm}^{-1}$  in even and odd configurations, respectively.

Almost all levels of the  $4d^5$  configuration can be well designated with the leading member of their eigenvector composition. Only  $48,086 \text{ cm}^{-1}$  ( $J = 3/2$ ) and  $47119 \text{ cm}^{-1}$  ( $J = 5/2$ ) were designated with the second term. For  $4d^4 5p$  configuration, in many cases two wave functions have the same first component leading to non-unique labels for the energy levels. Therefore, the level energies are listed in Table A6 along with the level designations to avoid the ambiguities.

According to our predictions the most intense lines of the  $4d^5-(4d^4 4f + 4p^5 4d^6)$  transitions are expected in the 170–240 Å wavelength range. As it is seen in Figure 1 there are many unknown lines in this region but we were not able to make reliable identification of these lines.

### 3.2. Ag VIII

The low lying configurations of Ag VIII are shown in Figure 3. The transitions from all low odd configurations decaying to the ground-state  $4d^4$  configuration are identified in this spectrum. The  $4d^4-4d^3 5p$  transitions are overlapped with some unknown lines of moderate intensity. But nevertheless, 118 lines were identified in this transition array (Table A2). Twenty-one lines were doubly and two lines trebly identified. Twenty-nine (out of 34 possible)  $4d^4$  levels were found with the relative uncertainty from 3 to  $7 \text{ cm}^{-1}$  and collected in Table A7. The levels of the  $4d^3 5p$  configurations are contained in Table A8. It was possible to locate 83 out of 110 possible levels of this configuration. Their uncertainties are from 4 to  $14 \text{ cm}^{-1}$ . As in Ag VII the identification of the  $4d^4-4d^3 5p$  transitions was performed with by means of the semi-empirical calculations based on the orthogonal operators.



**Figure 3.** Energy levels of Ag VIII. The arrows show electric dipole transitions studied in this article. The levels found in this work are marked by red color. Black color indicates unknown levels.

The energy parameters obtained in the final fitting are collected in Table A12 for  $4d^4$  and Table A13 for  $4d^3 5p$ . For the meaning of the energy parameters and the procedure of the calculations see Section 3.1. Root mean square deviations of the fitting were 26 and  $47 \text{ cm}^{-1}$  in the  $4d^4$  and  $4d^3 5p$  configurations, respectively. In case of the  $4d^3 5p$  configuration the fitting is affected by the interaction with the levels of the  $4p^5 4d^5$  configuration. The  $4d^3 5p$  levels above  $\sim 424,000 \text{ cm}^{-1}$  overlap with the low lying  $4p^5 4d^5$  levels. Their interaction cannot be taken into account in the orthogonal operator code. The LS-coupling scheme is good approximation for the  $4d^4$  levels. The value of the first component of

the eigenvector composition for all levels is not less than 50%, thus a unique label by the name of the first component can be assigned to all energy levels. To differentiate  $4d^4$  terms with the same LS values (recurring terms) the seniority numbers are used in the orthogonal operator code, whereas the Nielson and Koster sequential indices [20] are employed in the Cowan code [14]. Both labels are retained in Table A7 for the  $4d^4$  levels because the  $4d^4-(4d^35p + 4d^34f + 4p^54d^5)$  transitions were analyzed with the aid of the Cowan code as described below. Contrary to  $4d^4$ , the percentage of the first component of the eigenvector composition is less than 50% for many of the  $4d^35p$  levels. It goes down to 16%. It makes LS-labeling of many levels meaningless in many cases. Therefore, the energy level values are listed in Table A2 along with the LSJ labels for the wavelength identification.

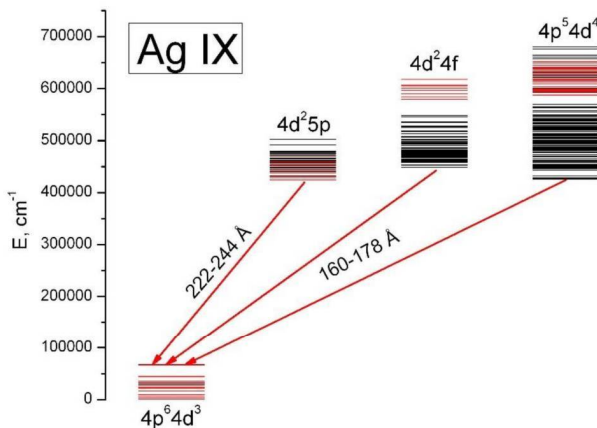
The identification of the  $4d^4-(4d^35p + 4d^34f + 4p^54d^5)$  transitions using the Cowan code resulted in 118 classified lines in the region 162–189 Å (Table A3). Seventeen lines were doubly classified. The wavelengths and intensities of 10 lines are affected by blending with the Ag IX lines. Table A9 contains the  $(4d^34f + 4p^54d^5)$  levels above  $556,000\text{ cm}^{-1}$ . It was possible to find 58 levels of these configurations with the uncertainties from 7 to  $19\text{ cm}^{-1}$ . Cowan's calculations of the odd level system were performed for a matrix of interacting configurations  $4d^35p + 4d^36p + 4d^25s5p + 4d5s^25p + 4d^3(4f-6f) + 4p^54d^5 + 4p^54d^45s$ . Starting energy parameters for the  $4d^35p$ ,  $4d^34f$  and  $4p^54d^5$  configurations in Ag VIII were estimated by extrapolation of the scaling factors (the ratios of the fitted to the corresponding Hartree - Fock energy parameters) from Pd VII [21] and Pd VIII [8]. The ab initio electrostatic parameters in the unknown configurations were multiplied by 0.85 scaling factor. The configuration interaction parameters were scaled by 0.8 and the average energies along with the spin-orbit parameters were fixed at the corresponding HF values. Final energy parameters for the  $4d^35p$ ,  $4d^34f$  and  $4p^54d^5$  configurations obtained in the fitting of the calculated energy levels to the experimental ones using the Cowan code are presented in Table A14. Standard deviation of the fitting  $\sigma$  was  $213\text{ cm}^{-1}$ . It should be noted, that for the  $4d^3$  levels alone, the fitting by the Cowan code results in  $\sigma = 129\text{ cm}^{-1}$  what is 2.7 times larger than at the fitting using the orthogonal parameter code (see Table A13).

All found levels belong to the upper part of configurations ("emissive zone" [22]) from  $557,000$  to  $669,000\text{ cm}^{-1}$ . Only the levels for this energy range are listed in Table A9. According to our calculations full spread of the  $4d^34f + 4p^54d^5$  levels cover the range up to  $424,000\text{ cm}^{-1}$  overlapping with the  $4d^35p$  levels. Because of significant uncertainty in prediction of the low lying  $4d^34f + 4p^54d^5$  levels they are omitted from Table A9.

Examination of Table A9 shows that the percentage contribution of the leading eigenvector component never exceeds 41% and can be as low as 9%. Moreover, the  $4d^34f$  wave function can be found as the leading component only at 13 levels with the largest contribution 31%, second component being mostly  $4p^54d^5$ . Therefore, not only LS-assignment of many levels in Table A3, but also configuration attributions are arbitrary in many cases. Therefore, in Table A9, the upper levels of the transitions are designated by their energies and  $J$  values, whereas for convenience, a configuration name and LS-label are given according to the output files from the Cowan code in spite of possible ambiguity in many cases.

### 3.3. Ag IX

The scheme of the  $4d^3$ ,  $4d^25p$ ,  $4d^24f$  and  $4p^54d^4$  levels for Ag IX is shown in Figure 4. It shows that in comparison with Ag VII and Ag VIII the  $4d^25p$  levels are almost fully imbedded within the widely spread  $4d^24f + 4p^54d^4$  levels. The levels of all odd configurations strongly interact. Their initial prediction in the framework of the Cowan code was performed by cross-extrapolation of the scaling factors and effective parameters from isonuclear Ag VIII (this work) and isoelectronic Pd VIII [8]. The  $4d^3$  energies were calculated in the framework of the orthogonal parameters by extrapolation from Ag VII and Ag VIII (Table A12) and used as an input to Cowan's calculations of the  $4d^3-(4d^25p + 4d^24f + 4p^54d^4)$  transition probabilities. Thus predicted energy levels and transition probabilities were then used for the spectrum analysis by the IDEN code [12].



**Figure 4.** Energy levels of Ag IX. The arrows show electric dipole transitions studied in this article. The levels found in this work are marked by red color. Black color indicates calculated positions of unknown levels.

As a result, 132 lines were identified in the  $4d^3-(4d^2 5p + 4d^2 4f + 4p^5 4d^4)$  transition array (Table A4). Nine lines were doubly classified and one line was trebly classified. The  $4d^3-4d^2 5p$  part of this transition array lying in the 221–244 Å region is overlapped by unidentified lines (see Figure 1) discussed in Section 3.1. Nevertheless, it was possible to select the majority of the Ag IX lines by observation of their intensities with the change of the vacuum spark excitation conditions. The other  $4d^3-(4d^2 4f + 4p^5 4d^4)$  part falls in the middle of the region where the spectrum consists of many overlapping lines in Ag VIII–Ag XII. Therefore 10 lines of Ag IX are found to be blended with Ag VIII and 8 with Ag X. In total, 17 levels of the  $4d^3$  configuration and 78 levels of the  $4d^2 5p + 4d^2 4f + 4p^5 4d^4$  configurations were established and collected in Tables A10 and A11, respectively. The uncertainty of relative positions of the levels after optimization by LOPT [19] ranges from 4 to  $17 \text{ cm}^{-1}$  for the ground-state configuration and from 6 to  $19 \text{ cm}^{-1}$  for the excited configurations.

As was mentioned above the energy levels of the  $4d^3$  configuration were treated by orthogonal operator technique. As in Ag VII and Ag VIII calculated matrix consisted of three interacting configurations:  $4d^3 + 4d^2 5s + 4d 5s^2$  with similar scaling of the energy parameters for unknown configurations. The levels of the  $4d^3$  configuration are presented in Table A10 along with the eigenvector compositions and deviations from the orthogonal parameter calculations. Standard deviation of the fitting was  $27 \text{ cm}^{-1}$ . The resulting energy parameters of this configuration are collected in Table A12 in comparison with those of  $4d^4$  (Ag VIII) and  $4d^5$  (Ag VII). Table A12 shows regular behavior of the parameters and scaling factors along this part of the isonuclear sequence of silver ions. The labeling of the  $4d^3$  energy levels by the first component of their eigenvectors is unambiguous.

Table A11 contains all 306 levels of the  $4d^2 5p + 4d^2 4f + 4p^5 4d^4$  configurations. Because of the numerous blends only 78 levels were found. Similar to Ag VIII, a set of the interacting configurations ( $4d^2 5p + 4d^2 6p + 4d 5s 5p + 5s^2 5p + 4d^2(4f - 6f) + 4p^5 4d^4 + 4p^5 5d^3 5s$ ) with the same treatment of the unknown configurations was used in the Cowan code calculations. The energy parameters for these configurations in Ag IX are listed in Table A14. The standard deviation of the fitting  $\sigma$  was  $327 \text{ cm}^{-1}$ , to be compared with  $\sigma = 213 \text{ cm}^{-1}$  in Ag VIII. It should be noted that in Ag IX more energy parameters than in Ag VIII were fixed on the estimated values for stability of the fitting. Similar considerations are applied to the eigenvector composition of the Ag IX odd levels. There are ambiguities in the LS-labeling and configuration assignment of the levels. Only the level energy and  $J$  value can serve as unique label, what is used in the list of the identified lines in Table A4.

#### 4. Discussion

The spectra reported in this article are relevant to the verification of the identifications of the EUV spectra of Sn ions [9,10] which are used as a “fuel” in the radiation sources for the projection lithography at the 135 Å wavelength. The previous analyses in [9,10] were performed without any isoelectronic or isoionic support. The isoelectronic sequence Rh VIII–Cd XI was recently studied in [7]. It was found by extrapolation to Sn XIII that the identification of this spectrum should be revised. Similar conclusion was made after the identification of the M1 transitions between the levels of ground-state configurations in Sn XIII and other ions with open 4d- shell [23]. More data on the VUV spectra of the neighboring to Sn elements are needed. The analyses of Ag VII, Ag VIII and Ag IX were performed in this work for the first time and all Ag ion spectra with the 4d<sup>k</sup> (k = 1–10) ground-state configuration now became known. After the studies of spectra of the 4d- palladium ions ([8] and references therein) the present work on Ag ion spectra is the next step in the study of the ion spectra isoelectronic with Sn IX–Sn XIII. The work on Cd- and In- ion spectra is in progress at this laboratory.

**Author Contributions:** A.R. recorded the spectra, performed their analyses and wrote the paper; E.K. made spectrum measurements and wrote the paper.

**Conflicts of Interest:** The authors declare no conflict of interest.

#### Appendix A

**Table A1.** Identified lines of the 4d<sup>5</sup>–4d<sup>4</sup>5p transitions in the spectrum of Ag<sup>6+</sup>.

λ (Å) <sup>a</sup>	o-c, (Å) <sup>b</sup>	ν (cm <sup>-1</sup> )	I <sup>c</sup>	gA <sub>ul</sub> (10 <sup>8</sup> s <sup>-1</sup> )	5d <sup>5</sup>		5d <sup>4</sup> 5p	
					Term <sup>e</sup>	E (cm <sup>-1</sup> )	Term <sup>e</sup>	E (cm <sup>-1</sup> )
271.910	0.000	367,768.8	36	31	5 <sup>4</sup> G <sub>11/2</sub>	30,662	(2 <sup>3</sup> F) <sup>4</sup> F <sub>9/2</sub>	398,431
277.706	0.003	360,092.8	11	42	5 <sup>4</sup> G <sub>11/2</sub>	30,662	(4 <sup>1</sup> F) <sup>2</sup> G <sub>9/2</sub>	390,759
277.852	-0.001	359,904.2	19	37	5 <sup>4</sup> G <sub>5/2</sub>	29,390	(2 <sup>3</sup> F) <sup>4</sup> F <sub>3/2</sub>	389,293
277.969	0.003	359,752.2	13	51	5 <sup>4</sup> D <sub>7/2</sub>	36,485	(2 <sup>3</sup> P) <sup>4</sup> D <sub>7/2</sub>	396,241
280.155	-0.002	356,944.6	12	11	5 <sup>4</sup> D <sub>5/2</sub>	39,299	(2 <sup>3</sup> P) <sup>4</sup> D <sub>7/2</sub>	396,241
280.826	0.000	356,092.1	5	48	3 <sup>2</sup> H <sub>9/2</sub>	53,797	(2 <sup>1</sup> G) <sup>2</sup> F <sub>7/2</sub>	409,889
281.791	-0.003	354,872.4	13	47	5 <sup>6</sup> S <sub>5/2</sub>	0	(4 <sup>5</sup> D) <sup>4</sup> D <sub>7/2</sub>	354,869
283.387	0.002	352,874.3	9	44	3 <sup>4</sup> F <sub>3/2</sub>	53,796	(2 <sup>3</sup> F) <sup>4</sup> D <sub>1/2</sub>	406,673
284.236	-0.003	351,820.2	62	518	3 <sup>2</sup> H <sub>11/2</sub>	57,962	(2 <sup>1</sup> G) <sup>2</sup> G <sub>9/2</sub>	409,779
284.511	-0.001	351,479.9	12	93	3 <sup>2</sup> H <sub>11/2</sub>	57,962	(2 <sup>1</sup> G) <sup>2</sup> H <sub>11/2</sub>	409,441
285.168	-0.003	350,670.3	30	276	5 <sup>2</sup> G <sub>9/2</sub>	59,223	(2 <sup>1</sup> G) <sup>2</sup> F <sub>7/2</sub>	409,889
285.727	0.002	349,984.1	6	153	5 <sup>2</sup> F <sub>7/2</sub>	59,792	(2 <sup>1</sup> G) <sup>2</sup> G <sub>9/2</sub>	409,779
285.785	0.004	349,912.9	5	55	3 <sup>4</sup> F <sub>9/2</sub>	49,104	(2 <sup>3</sup> F) <sup>4</sup> G <sub>11/2</sub>	399,022
286.212		349,391.3	32	377	3 <sup>2</sup> G <sub>9/2</sub>	79,131	(2 <sup>1</sup> D) <sup>2</sup> F <sub>7/2</sub>	428,522
286.254	-0.010	349,339.5	30	159	3 <sup>2</sup> H <sub>9/2</sub>	53,797	(2 <sup>3</sup> F) <sup>4</sup> D <sub>7/2</sub>	403,133
286.276	0.011	349,313.3	23	76	3 <sup>4</sup> F <sub>9/2</sub>	49,104	(2 <sup>3</sup> F) <sup>4</sup> F <sub>9/2</sub>	398,431
286.411	-0.002	349,148.6	8	28	3 <sup>4</sup> F <sub>7/2</sub>	48,712	(2 <sup>3</sup> F) <sup>4</sup> G <sub>7/2</sub>	397,858
286.744	0.009	348,743.4	15	132	3 <sup>4</sup> F <sub>9/2</sub>	49,104	(2 <sup>3</sup> F) <sup>4</sup> G <sub>7/2</sub>	397,858
287.950	0.001	347,282.9	15	113	3 <sup>2</sup> F <sub>7/2</sub>	53,353	(4 <sup>1</sup> F) <sup>2</sup> D <sub>5/2</sub>	400,637
288.074	0.003	347,133.0	10	88	3 <sup>4</sup> F <sub>9/2</sub>	49,104	(2 <sup>3</sup> P) <sup>4</sup> D <sub>7/2</sub>	396,241
288.806	0.002	346,253.7	16	36	5 <sup>4</sup> G <sub>9/2</sub>	30,907	(4 <sup>3</sup> D) <sup>4</sup> F <sub>7/2</sub>	377,163
288.970	0.003	346,057.0	12	33	5 <sup>6</sup> S <sub>5/2</sub>	0	(4 <sup>5</sup> D) <sup>4</sup> F <sub>7/2</sub>	346,061
289.226	0.005	345,750.6	16	25	5 <sup>4</sup> G <sub>11/2</sub>	30,662	(4 <sup>1</sup> I) <sup>2</sup> I <sub>13/2</sub>	376,419
289.431	0.001	345,506.0	5	36	5 <sup>4</sup> G <sub>9/2</sub>	30,907	(4 <sup>3</sup> G) <sup>4</sup> G <sub>11/2</sub>	376,414
289.575	0.002	345,334.0	18	95	3 <sup>4</sup> F <sub>7/2</sub>	48,712	(2 <sup>3</sup> F) <sup>4</sup> F <sub>5/2</sub>	394,049
289.665	-0.001	345,225.9	7	28	3 <sup>2</sup> H <sub>9/2</sub>	53,797	(2 <sup>3</sup> F) <sup>4</sup> G <sub>11/2</sub>	399,022
289.944	0.000	344,894.1	18	114	5 <sup>2</sup> G <sub>9/2</sub>	59,223	(2 <sup>3</sup> F) <sup>4</sup> F <sub>7/2</sub>	404,117
290.169	0.006	344,626.6	47	326	3 <sup>2</sup> H <sub>9/2</sub>	53,797	(2 <sup>3</sup> F) <sup>4</sup> F <sub>9/2</sub>	398,431
290.203	-0.003	344,586.3	9	24	3 <sup>4</sup> F <sub>7/2</sub>	48,712	(2 <sup>3</sup> F) <sup>4</sup> G <sub>7/2</sub>	393,295
290.265	-0.006	344,512.5	12	72	3 <sup>2</sup> F <sub>7/2</sub>	53,353	(2 <sup>3</sup> F) <sup>4</sup> G <sub>7/2</sub>	397,858
290.415	0.002	344,335.1	18	53	5 <sup>2</sup> D <sub>3/2</sub>	48,086	(2 <sup>3</sup> P) <sup>4</sup> D <sub>1/2</sub>	392,424
291.263	0.003	343,332.2	52	39	5 <sup>6</sup> S <sub>5/2</sub>	0	(4 <sup>5</sup> D) <sup>4</sup> F <sub>5/2</sub>	343,336



Table A1. Cont.

$\lambda$ (Å) <sup>a</sup>	o-c, (Å) <sup>b</sup>	$\nu$ (cm <sup>-1</sup> )	I <sup>c</sup>	$\frac{gA_r}{(10^8 \text{ s}^{-1})}$	5d <sup>5</sup>		5d <sup>4</sup> 5p	
					Term <sup>e</sup>	E (cm <sup>-1</sup> )	Term <sup>e</sup>	E (cm <sup>-1</sup> )
291.310	0.002	343,277.0	15	113	3 <sup>2</sup> G <sub>7/2</sub>	79,705	(2 <sup>1</sup> D) <sup>2</sup> F <sub>5/2</sub>	422,985
291.817	0.003	342,680.2	14	79	3 <sup>4</sup> F <sub>7/2</sub>	48,712	(2 <sup>3</sup> F) <sup>4</sup> G <sub>5/2</sub>	391,396
291.862	-0.002	342,627.8	19	132	3 <sup>4</sup> F <sub>7/2</sub>	48,712	(2 <sup>3</sup> F) <sup>4</sup> F <sub>7/2</sub>	391,338
291.915	-0.004	342,565.6	32	138	3 <sup>4</sup> F <sub>5/2</sub>	51,049	(4 <sup>1</sup> D) <sup>2</sup> P <sub>3/2</sub>	393,610
292.019	0.001	342,443.3	46	390	3 <sup>2</sup> H <sub>9/2</sub>	53,797	(2 <sup>3</sup> P) <sup>4</sup> D <sub>7/2</sub>	396,241
292.260	0.000	342,160.6	44	235	5 <sup>4</sup> G <sub>11/2</sub>	30,662	(4 <sup>3</sup> G) <sup>4</sup> H <sub>13/2</sub>	372,822
292.700	0.007	341,647.2	53	450	3 <sup>4</sup> F <sub>9/2</sub>	49,104	(4 <sup>1</sup> F) <sup>2</sup> G <sub>9/2</sub>	390,759
292.860	-0.002	341,460.2	37	80	5 <sup>6</sup> S <sub>5/2</sub>	0	(4 <sup>5</sup> D) <sup>6</sup> D <sub>7/2</sub>	341,458
293.002	0.001	341,294.3	17	43	5 <sup>4</sup> G <sub>7/2</sub>	30,378	(4 <sup>3</sup> G) <sup>4</sup> G <sub>7/2</sub>	371,673
293.077	0.000	341,206.8	31	89	5 <sup>2</sup> D <sub>3/2</sub>	48,086	(2 <sup>3</sup> F) <sup>4</sup> F <sub>3/2</sub>	389,293
293.201	-0.002	341,062.7	2	30	3 <sup>2</sup> H <sub>11/2</sub>	57,962	(2 <sup>3</sup> F) <sup>4</sup> G <sub>11/2</sub>	399,022
293.388	0.000	340,845.3	17	225	5 <sup>2</sup> F <sub>7/2</sub>	59,792	(4 <sup>1</sup> F) <sup>2</sup> D <sub>5/2</sub>	400,637
293.457	0.001	340,764.8	8	27	5 <sup>4</sup> G <sub>9/2</sub>	30,907	(4 <sup>3</sup> G) <sup>4</sup> G <sub>7/2</sub>	371,673
293.516	-0.001	340,696.8	32	201	3 <sup>2</sup> F <sub>7/2</sub>	53,353	(2 <sup>3</sup> F) <sup>4</sup> F <sub>5/2</sub>	394,049
293.681	-0.002	340,506.1	33	126	3 <sup>4</sup> F <sub>5/2</sub>	51,049	(2 <sup>3</sup> P) <sup>4</sup> D <sub>3/2</sub>	391,553
293.711	-0.001	340,470.6	14	178	3 <sup>2</sup> H <sub>11/2</sub>	57,962	(2 <sup>3</sup> F) <sup>4</sup> F <sub>9/2</sub>	398,431
293.822	0.004	340,342.2	5	31	3 <sup>4</sup> F <sub>5/2</sub>	51,049	(2 <sup>3</sup> F) <sup>4</sup> G <sub>5/2</sub>	391,396
293.865	-0.003	340,292.7	4	101	3 <sup>4</sup> F <sub>5/2</sub>	51,049	(2 <sup>3</sup> F) <sup>4</sup> F <sub>7/2</sub>	391,338
293.954	-0.001	340,189.4	9	35	5 <sup>4</sup> G <sub>5/2</sub>	29,390	(4 <sup>3</sup> F) <sup>2</sup> F <sub>5/2</sub>	369,578
294.467	-0.002	339,596.6	24	43	5 <sup>4</sup> G <sub>9/2</sub>	30,907	(4 <sup>3</sup> G) <sup>2</sup> H <sub>9/2</sub>	370,501
294.526	-0.001	339,529.1	18	44	5 <sup>2</sup> I <sub>11/2</sub>	44,011	(4 <sup>1</sup> I) <sup>2</sup> H <sub>11/2</sub>	383,539
294.551	-0.001	339,499.6	13	109	3 <sup>2</sup> H <sub>9/2</sub>	53,797	(2 <sup>3</sup> F) <sup>4</sup> G <sub>7/2</sub>	393,295
294.798	-0.006	339,214.9	26	119	5 <sup>2</sup> G <sub>9/2</sub>	59,223	(2 <sup>3</sup> F) <sup>4</sup> F <sub>9/2</sub>	398,431
294.834	-0.002	339,174.3	197	342	5 <sup>6</sup> S <sub>5/2</sub>	0	(4 <sup>5</sup> D) <sup>6</sup> D <sub>5/2</sub>	339,172
294.872	0.003	339,130.2	37	202	3 <sup>2</sup> F <sub>7/2</sub>	53,353	(2 <sup>3</sup> F) <sup>4</sup> G <sub>9/2</sub>	392,486
294.932	-0.002	339,061.6	23	117	3 <sup>4</sup> F <sub>9/2</sub>	49,117	(4 <sup>1</sup> F) <sup>2</sup> G <sub>7/2</sub>	388,163
294.980 <sup>d</sup>	0.004	339,006.0	43	199	3 <sup>4</sup> F <sub>5/2</sub>	51,049	(2 <sup>3</sup> F) <sup>4</sup> F <sub>5/2</sub>	390,060
294.980 <sup>d</sup>	-0.006	339,006.0	43	134	5 <sup>4</sup> G <sub>11/2</sub>	30,662	(4 <sup>1</sup> I) <sup>2</sup> H <sub>11/2</sub>	369,661
295.091	0.002	338,878.2	19	34	5 <sup>4</sup> D <sub>7/2</sub>	36,485	(5 <sup>2</sup> G) <sup>2</sup> G <sub>7/2</sub>	375,365
295.253	-0.003	338,692.6	22	61	3 <sup>2</sup> H <sub>9/2</sub>	53,797	(2 <sup>3</sup> F) <sup>4</sup> G <sub>9/2</sub>	392,486
295.304	0.001	338,633.8	47	203	5 <sup>2</sup> G <sub>9/2</sub>	59,223	(2 <sup>3</sup> F) <sup>4</sup> G <sub>7/2</sub>	397,858
295.304	-0.005	338,633.8	47	159	3 <sup>4</sup> F <sub>3/2</sub>	53,796	(2 <sup>3</sup> P) <sup>4</sup> D <sub>1/2</sub>	392,424
295.537	-0.001	338,367.6	90	657	5 <sup>2</sup> I <sub>11/2</sub>	44,011	(4 <sup>1</sup> I) <sup>2</sup> H <sub>9/2</sub>	382,377
295.648	0.004	338,240.1	12	32	3 <sup>4</sup> F <sub>5/2</sub>	51,049	(2 <sup>3</sup> F) <sup>4</sup> F <sub>3/2</sub>	389,293
295.801	0.001	338,064.9	20	35	5 <sup>2</sup> F <sub>7/2</sub>	59,792	(2 <sup>3</sup> F) <sup>4</sup> G <sub>7/2</sub>	397,858
295.944	0.002	337,901.3	22	85	3 <sup>4</sup> F <sub>7/2</sub>	48,712	(4 <sup>3</sup> F) <sup>2</sup> G <sub>7/2</sub>	386,615
295.980	0.003	337,861.1	10	79	5 <sup>4</sup> D <sub>5/2</sub>	39,299	(4 <sup>3</sup> D) <sup>4</sup> F <sub>7/2</sub>	377,163
296.056	-0.006	337,773.4	22	55	5 <sup>4</sup> G <sub>11/2</sub>	30,662	(4 <sup>3</sup> G) <sup>4</sup> H <sub>9/2</sub>	368,429
296.579	0.005	337,177.8	14	87	5 <sup>4</sup> G <sub>5/2</sub>	29,390	(4 <sup>3</sup> F) <sup>4</sup> F <sub>3/2</sub>	366,573
296.716 <sup>d</sup>	0.004	337,023.2	18	52	5 <sup>4</sup> D <sub>1/2</sub>	38,685	(4 <sup>3</sup> D) <sup>4</sup> D <sub>3/2</sub>	375,706
296.716 <sup>d</sup>	-0.004	337,023.2	18	117	5 <sup>2</sup> G <sub>9/2</sub>	59,223	(2 <sup>3</sup> P) <sup>4</sup> D <sub>7/2</sub>	396,241
296.779	0.003	336,950.9	12	116	3 <sup>2</sup> D <sub>5/2</sub>	72,934	(2 <sup>1</sup> G) <sup>2</sup> F <sub>7/2</sub>	409,889
296.892	-0.001	336,822.6	37	160	5 <sup>4</sup> G <sub>11/2</sub>	30,662	(4 <sup>3</sup> F) <sup>4</sup> G <sub>11/2</sub>	367,483
296.910	0.001	336,802.8	17	103	5 <sup>4</sup> D <sub>1/2</sub>	38,685	(4 <sup>3</sup> D) <sup>4</sup> P <sub>1/2</sub>	375,489
296.944	-0.008	336,763.9	17	103	5 <sup>4</sup> D <sub>3/2</sub>	39,788	(4 <sup>3</sup> D) <sup>4</sup> F <sub>5/2</sub>	376,543
297.106	-0.004	336,580.1	22	55	5 <sup>4</sup> G <sub>9/2</sub>	30,907	(4 <sup>3</sup> F) <sup>4</sup> G <sub>11/2</sub>	367,483
297.124	0.004	336,559.4	22	35	3 <sup>4</sup> P <sub>5/2</sub>	32,005	(4 <sup>3</sup> F) <sup>4</sup> D <sub>3/2</sub>	368,569
297.216	-0.002	336,456.2	29	174	3 <sup>4</sup> P <sub>3/2</sub>	32,994	(4 <sup>3</sup> D) <sup>4</sup> P <sub>3/2</sub>	369,448
297.251	-0.008	336,415.8	12	54	5 <sup>4</sup> D <sub>5/2</sub>	39,299	(4 <sup>3</sup> D) <sup>4</sup> D <sub>3/2</sub>	375,706
297.324		336,333.8	307	565	5 <sup>6</sup> S <sub>5/2</sub>	0	(4 <sup>5</sup> D) <sup>6</sup> P <sub>3/2</sub>	336,333
297.504	-0.004	336,130.1	8	44	5 <sup>4</sup> D <sub>1/2</sub>	38,685	(4 <sup>3</sup> P) <sup>2</sup> P <sub>1/2</sub>	374,810
297.702	-0.007	335,906.6	36	79	5 <sup>4</sup> G <sub>9/2</sub>	30,907	(4 <sup>3</sup> F) <sup>4</sup> F <sub>7/2</sub>	366,806
297.882	-0.002	335,702.9	16	188	5 <sup>4</sup> D <sub>3/2</sub>	39,788	(4 <sup>3</sup> D) <sup>4</sup> P <sub>1/2</sub>	375,489
297.911	-0.002	335,670.5	55	299	3 <sup>4</sup> F <sub>9/2</sub>	49,104	(4 <sup>1</sup> D) <sup>2</sup> F <sub>7/2</sub>	384,772
297.951	-0.003	335,625.9	18	143	5 <sup>2</sup> G <sub>7/2</sub>	55,773	(2 <sup>3</sup> F) <sup>4</sup> G <sub>5/2</sub>	391,396
298.066 <sup>d</sup>	0.001	335,495.9	40	272	3 <sup>4</sup> F <sub>3/2</sub>	53,796	(2 <sup>3</sup> F) <sup>4</sup> F <sub>3/2</sub>	389,293
298.066 <sup>d</sup>	-0.008	335,495.9	41	68	5 <sup>4</sup> G <sub>5/2</sub>	29,390	(4 <sup>3</sup> P) <sup>4</sup> P <sub>5/2</sub>	364,877
298.311	-0.005	335,220.5	52	378	5 <sup>2</sup> I <sub>11/2</sub>	44,011	(4 <sup>3</sup> G) <sup>2</sup> G <sub>9/2</sub>	379,226
298.367	-0.001	335,157.4	35	58	3 <sup>2</sup> D <sub>3/2</sub>	71,517	(2 <sup>3</sup> F) <sup>4</sup> D <sub>1/2</sub>	406,673

Table A1. Cont.

$\lambda$ (Å) <sup>a</sup>	o-c, (Å) <sup>b</sup>	$\nu$ (cm <sup>-1</sup> )	I <sup>c</sup>	$gA_{\nu}$ (10 <sup>8</sup> s <sup>-1</sup> )	5d <sup>5</sup>		5d <sup>4</sup> 5p	
					Term <sup>e</sup>	E (cm <sup>-1</sup> )	Term <sup>e</sup>	E (cm <sup>-1</sup> )
298.564 <sup>d</sup>		334,936.4	660	266	5 <sup>4</sup> D <sub>5/2</sub>	39,299	(4 <sup>3</sup> D) <sup>4</sup> P <sub>3/2</sub>	374,236
298.564 <sup>d</sup>	-0.001	334,936.4	660	239	5 <sup>4</sup> G <sub>9/2</sub>	30,907	(4 <sup>3</sup> F) <sup>2</sup> G <sub>7/2</sub>	365,842
298.591 <sup>d</sup>		334,905.8	1000	1405	5 <sup>6</sup> S <sub>5/2</sub>	0	(4 <sup>5</sup> D) <sup>6</sup> P <sub>7/2</sub>	334,906
298.591 <sup>d</sup>	0.001	334,905.8	1000	621	5 <sup>4</sup> G <sub>11/2</sub>	30,662	(4 <sup>3</sup> F) <sup>4</sup> F <sub>9/2</sub>	365,569
298.651	0.003	334,839.3	23	100	3 <sup>4</sup> P <sub>1/2</sub>	34,605	(4 <sup>3</sup> D) <sup>4</sup> P <sub>3/2</sub>	369,448
299.048	0.002	334,394.9	12	251	3 <sup>4</sup> F <sub>7/2</sub>	48,712	(4 <sup>3</sup> D) <sup>2</sup> F <sub>5/2</sub>	383,109
299.073	-0.011	334,367.0	79	244	5 <sup>4</sup> G <sub>11/2</sub>	30,662	(4 <sup>3</sup> H) <sup>4</sup> H <sub>11/2</sub>	365,017
299.301 <sup>d</sup>	-0.002	334,111.7	82	115	5 <sup>4</sup> G <sub>11/2</sub>	30,662	(4 <sup>3</sup> F) <sup>4</sup> G <sub>9/2</sub>	364,772
299.301 <sup>d</sup>	-0.001	334,111.7	82	221	5 <sup>4</sup> G <sub>9/2</sub>	30,907	(4 <sup>3</sup> H) <sup>4</sup> H <sub>11/2</sub>	365,017
299.346	0.002	334,061.9	26	140	5 <sup>4</sup> G <sub>5/2</sub>	29,390	(4 <sup>3</sup> D) <sup>4</sup> F <sub>3/2</sub>	363,454
299.396	0.002	334,006.1	12	97	3 <sup>4</sup> F <sub>7/2</sub>	48,712	(4 <sup>1</sup> G) <sup>2</sup> G <sub>9/2</sub>	382,720
299.432	-0.002	333,966.1	15	119	3 <sup>4</sup> P <sub>1/2</sub>	34,605	(4 <sup>3</sup> F) <sup>4</sup> D <sub>3/2</sub>	368,569
299.526	0.004	333,861.1	127	498	5 <sup>4</sup> G <sub>9/2</sub>	30,907	(4 <sup>3</sup> F) <sup>4</sup> G <sub>9/2</sub>	364,772
299.719	0.001	333,645.6	63	419	5 <sup>4</sup> G <sub>7/2</sub>	30,378	(4 <sup>3</sup> D) <sup>2</sup> D <sub>5/2</sub>	364,025
299.740	0.001	333,622.6	32	180	3 <sup>4</sup> F <sub>9/2</sub>	49,104	(4 <sup>1</sup> G) <sup>2</sup> G <sub>9/2</sub>	382,728
299.772	-0.002	333,586.8	35	71	5 <sup>4</sup> G <sub>5/2</sub>	29,390	(4 <sup>3</sup> P) <sup>4</sup> D <sub>5/2</sub>	362,975
299.803	0.000	333,551.8	15	72	5 <sup>4</sup> G <sub>5/2</sub>	29,390	(4 <sup>3</sup> G) <sup>4</sup> H <sub>7/2</sub>	362,942
299.941	-0.004	333,399.3	32	185	5 <sup>4</sup> D <sub>7/2</sub>	36,485	(4 <sup>3</sup> P) <sup>4</sup> D <sub>7/2</sub>	369,879
299.954	-0.003	333,384.9	32	46	5 <sup>2</sup> I <sub>11/2</sub>	44,011	(4 <sup>3</sup> F) <sup>2</sup> G <sub>9/2</sub>	377,393
300.006		333,327.1	315	783	5 <sup>6</sup> S <sub>5/2</sub>	0	(4 <sup>5</sup> D) <sup>6</sup> P <sub>5/2</sub>	333,327
300.065 <sup>d</sup>	0.001	333,261.5	41	193	5 <sup>2</sup> G <sub>9/2</sub>	59,223	(2 <sup>3</sup> F) <sup>4</sup> G <sub>9/2</sub>	392,486
300.065 <sup>d</sup>	0.001	333,261.5	41	114	3 <sup>2</sup> F <sub>7/2</sub>	53,353	(4 <sup>1</sup> F) <sup>2</sup> G <sub>7/2</sub>	386,615
300.216	-0.001	333,093.9	36	178	5 <sup>4</sup> D <sub>7/2</sub>	36,485	(4 <sup>3</sup> F) <sup>2</sup> F <sub>5/2</sub>	369,578
300.224	0.000	333,084.2	36	113	3 <sup>4</sup> P <sub>3/2</sub>	32,993	(4 <sup>3</sup> F) <sup>4</sup> F <sub>3/2</sub>	366,077
300.305	-0.003	332,994.5	56	319	5 <sup>4</sup> G <sub>5/2</sub>	29,390	(4 <sup>3</sup> H) <sup>4</sup> G <sub>5/2</sub>	362,381
300.342	-0.001	332,953.5	74	267	5 <sup>4</sup> G <sub>11/2</sub>	30,662	(4 <sup>3</sup> H) <sup>4</sup> I <sub>3/2</sub>	363,614
300.419	0.004	332,868.1	12	66	3 <sup>4</sup> P <sub>5/2</sub>	32,005	(4 <sup>3</sup> P) <sup>4</sup> P <sub>5/2</sub>	364,877
300.473 <sup>d</sup>	0.000	332,808.5	144	274	5 <sup>2</sup> I <sub>3/2</sub>	45,546	(4 <sup>1</sup> I) <sup>2</sup> K <sub>15/2</sub>	378,355
300.473 <sup>d</sup>	-0.010	332,808.5	144	641	3 <sup>2</sup> H <sub>11/2</sub>	57,962	(4 <sup>1</sup> F) <sup>2</sup> G <sub>9/2</sub>	390,759
300.693	-0.001	332,564.7	39	203	5 <sup>4</sup> G <sub>7/2</sub>	30,378	(4 <sup>3</sup> G) <sup>4</sup> H <sub>7/2</sub>	362,942
300.760	-0.007	332,490.7	39	208	5 <sup>4</sup> D <sub>7/2</sub>	36,485	(4 <sup>3</sup> P) <sup>4</sup> D <sub>7/2</sub>	368,968
300.833	-0.006	332,410.2	26	57	5 <sup>2</sup> I <sub>11/2</sub>	44,011	(4 <sup>3</sup> G) <sup>4</sup> G <sub>11/2</sub>	376,414
300.855	0.004	332,385.9	26	96	5 <sup>2</sup> G <sub>7/2</sub>	55,773	(4 <sup>3</sup> F) <sup>2</sup> G <sub>7/2</sub>	388,163
301.047	-0.003	332,174.2	342	1899	5 <sup>2</sup> I <sub>3/2</sub>	45,546	(4 <sup>1</sup> G) <sup>2</sup> H <sub>11/2</sub>	377,717
301.098	-0.003	332,118.1	16	95	5 <sup>2</sup> G <sub>9/2</sub>	59,223	(2 <sup>3</sup> F) <sup>4</sup> F <sub>7/2</sub>	391,338
301.141	-0.001	332,070.5	15	141	5 <sup>4</sup> G <sub>7/2</sub>	30,378	(4 <sup>3</sup> G) <sup>4</sup> F <sub>9/2</sub>	362,447
301.178 <sup>d</sup>	0.006	332,029.0	34	149	5 <sup>4</sup> G <sub>9/2</sub>	30,907	(4 <sup>3</sup> G) <sup>4</sup> H <sub>7/2</sub>	362,942
301.178 <sup>d</sup>	-0.008	332,029.0	34	192	3 <sup>4</sup> P <sub>5/2</sub>	32,005	(4 <sup>3</sup> D) <sup>2</sup> D <sub>5/2</sub>	364,025
301.262	0.007	331,936.7	16	143	5 <sup>4</sup> D <sub>7/2</sub>	36,485	(4 <sup>3</sup> G) <sup>4</sup> H <sub>9/2</sub>	368,429
301.314	-0.006	331,879.4	140	547	5 <sup>4</sup> G <sub>11/2</sub>	30,662	(4 <sup>3</sup> H) <sup>2</sup> I <sub>11/2</sub>	362,535
301.404 <sup>d</sup>	0.002	331,781.0	147	92	5 <sup>4</sup> G <sub>5/2</sub>	29,390	(4 <sup>3</sup> F) <sup>4</sup> G <sub>7/2</sub>	361,173
301.404 <sup>d</sup>	0.004	331,781.0	147	712	5 <sup>4</sup> G <sub>11/2</sub>	30,662	(4 <sup>3</sup> G) <sup>4</sup> F <sub>9/2</sub>	362,447
301.585	0.001	331,581.0	9	152	5 <sup>2</sup> I <sub>11/2</sub>	44,011	(4 <sup>3</sup> D) <sup>4</sup> F <sub>9/2</sub>	375,593
301.618 <sup>d</sup>	0.001	331,545.3	73	415	5 <sup>2</sup> F <sub>7/2</sub>	59,792	(2 <sup>3</sup> F) <sup>4</sup> F <sub>7/2</sub>	391,338
301.618 <sup>d</sup>	-0.008	331,545.3	73	58	5 <sup>2</sup> G <sub>9/2</sub>	59,223	(4 <sup>1</sup> F) <sup>2</sup> G <sub>9/2</sub>	390,759
301.701	-0.004	331,453.7	42	243	3 <sup>4</sup> P <sub>5/2</sub>	32,005	(4 <sup>3</sup> D) <sup>4</sup> F <sub>3/2</sub>	363,454
301.720	0.001	331,433.2	89	388	5 <sup>4</sup> D <sub>7/2</sub>	36,485	(4 <sup>3</sup> D) <sup>4</sup> P <sub>5/2</sub>	367,919
301.866	-0.001	331,272.8	28	65	5 <sup>4</sup> G <sub>7/2</sub>	30,378	(4 <sup>3</sup> H) <sup>4</sup> G <sub>9/2</sub>	361,650
301.920	0.001	331,213.5	60	333	5 <sup>4</sup> G <sub>7/2</sub>	30,378	(4 <sup>3</sup> G) <sup>4</sup> F <sub>7/2</sub>	361,593
301.932		331,200.4	147	211	5 <sup>6</sup> S <sub>5/2</sub>	0	(4 <sup>5</sup> D) <sup>4</sup> P <sub>3/2</sub>	331,200
302.140	-0.005	330,972.2	13	41	5 <sup>2</sup> F <sub>7/2</sub>	59,792	(4 <sup>1</sup> F) <sup>2</sup> G <sub>9/2</sub>	390,759
302.191	0.002	330,916.4	155	680	5 <sup>4</sup> G <sub>7/2</sub>	30,378	(4 <sup>3</sup> F) <sup>4</sup> F <sub>5/2</sub>	361,296
302.226 <sup>d</sup>	-0.009	330,878.0	351	441	5 <sup>2</sup> I <sub>3/2</sub>	45,546	(4 <sup>3</sup> G) <sup>4</sup> G <sub>11/2</sub>	376,414
302.226 <sup>d</sup>	-0.005	330,878.0	351	768	5 <sup>2</sup> I <sub>3/2</sub>	45,546	(4 <sup>1</sup> I) <sup>2</sup> I <sub>13/2</sub>	376,419
302.307 <sup>d</sup>	0.005	330,789.4	146	453	5 <sup>4</sup> G <sub>7/2</sub>	30,378	(4 <sup>3</sup> F) <sup>4</sup> G <sub>7/2</sub>	361,173
302.307 <sup>d</sup>	0.001	330,789.4	146	248	5 <sup>2</sup> D <sub>5/2</sub>	47,119	(4 <sup>1</sup> S) <sup>2</sup> P <sub>3/2</sub>	377,910
302.350 <sup>d</sup>	0.001	330,742.4	565	1173	5 <sup>4</sup> G <sub>9/2</sub>	30,907	(4 <sup>3</sup> H) <sup>4</sup> G <sub>9/2</sub>	361,650
302.350 <sup>d</sup>	0.014	330,742.4	565	619	3 <sup>2</sup> G <sub>9/2</sub>	79,131	(2 <sup>1</sup> G) <sup>2</sup> F <sub>7/2</sub>	409,889
302.401	-0.001	330,687.0	192	881	5 <sup>4</sup> G <sub>9/2</sub>	30,907	(4 <sup>3</sup> G) <sup>4</sup> F <sub>7/2</sub>	361,593

Table A1. Cont.

$\lambda$ (Å) <sup>a</sup>	o-c, (Å) <sup>b</sup>	$\nu$ (cm <sup>-1</sup> )	I <sup>c</sup>	gA <sub>r</sub> (10 <sup>8</sup> s <sup>-1</sup> )	5d <sup>5</sup>		5d <sup>4</sup> 5p	
					Term <sup>e</sup>	E (cm <sup>-1</sup> )	Term <sup>e</sup>	E (cm <sup>-1</sup> )
302.687 <sup>d</sup>	0.002	330,374.0	21	108	3 <sup>4</sup> P <sub>5/2</sub>	32,005	(4 <sup>3</sup> H) <sup>4</sup> G <sub>5/2</sub>	362,381
302.687 <sup>d</sup>	-0.008	330,374.0	21	186	3 <sup>4</sup> F <sub>7/2</sub>	48,712	(4 <sup>1</sup> F) <sup>2</sup> F <sub>5/2</sub>	379,077
302.748 <sup>d</sup>	0.002	330,307.5	57	208	3 <sup>2</sup> G <sub>9/2</sub>	79,131	(2 <sup>1</sup> G) <sup>2</sup> H <sub>11/2</sub>	409,441
302.748 <sup>d</sup>	0.012	330,307.5	57	154	5 <sup>4</sup> D <sub>7/2</sub>	36,485	(4 <sup>3</sup> F) <sup>4</sup> F <sub>7/2</sub>	366,806
302.784 <sup>d</sup>	-0.001	330,268.8	49	87	5 <sup>2</sup> F <sub>7/2</sub>	59,792	(2 <sup>3</sup> F) <sup>4</sup> F <sub>5/2</sub>	390,060
302.784 <sup>d</sup>	-0.003	330,268.8	49	84	5 <sup>4</sup> G <sub>9/2</sub>	30,907	(4 <sup>3</sup> F) <sup>4</sup> G <sub>7/2</sub>	361,173
302.836	-0.004	330,212.1	110	309	5 <sup>4</sup> D <sub>7/2</sub>	36,485	(4 <sup>3</sup> D) <sup>4</sup> D <sub>5/2</sub>	366,693
302.865	0.008	330,180.0	26	413	5 <sup>2</sup> G <sub>7/2</sub>	55,773	(4 <sup>3</sup> D) <sup>2</sup> F <sub>5/2</sub>	385,962
302.936 <sup>d</sup>	0.001	330,103.2	34	150	5 <sup>4</sup> G <sub>7/2</sub>	30,378	(4 <sup>3</sup> F) <sup>4</sup> G <sub>9/2</sub>	360,482
302.936 <sup>d</sup>	0.003	330,103.2	34	225	3 <sup>2</sup> F <sub>5/2</sub>	59,954	(3 <sup>2</sup> F) <sup>4</sup> F <sub>5/2</sub>	390,060
303.045	-0.003	329,983.8	72	299	3 <sup>4</sup> P <sub>3/2</sub>	32,994	(4 <sup>3</sup> P) <sup>4</sup> F <sub>5/2</sub>	362,975
303.063	-0.007	329,964.7	29	442	3 <sup>4</sup> F <sub>9/2</sub>	49,104	(4 <sup>1</sup> G) <sup>2</sup> G <sub>7/2</sub>	379,061
303.133	-0.004	329,888.5	9	47	5 <sup>4</sup> D <sub>1/2</sub>	38,685	(4 <sup>3</sup> F) <sup>4</sup> D <sub>3/2</sub>	368,569
303.191 <sup>d</sup>	-0.001	329,824.7	95	131	5 <sup>2</sup> D <sub>3/2</sub>	48,086	(4 <sup>1</sup> S) <sup>2</sup> F <sub>3/2</sub>	377,910
303.191 <sup>d</sup>	-0.005	329,824.7	95	332	5 <sup>4</sup> G <sub>11/2</sub>	30,662	(4 <sup>3</sup> H) <sup>4</sup> I <sub>11/2</sub>	360,481
303.252	-0.003	329,758.8	20	60	3 <sup>2</sup> F <sub>7/2</sub>	53,353	(4 <sup>3</sup> D) <sup>2</sup> F <sub>5/2</sub>	383,109
303.340	-0.003	329,663.2	11	147	5 <sup>4</sup> D <sub>3/2</sub>	39,788	(4 <sup>3</sup> D) <sup>4</sup> F <sub>3/2</sub>	369,448
303.421	0.000	329,575.0	46	170	5 <sup>4</sup> G <sub>9/2</sub>	30,907	(4 <sup>3</sup> F) <sup>4</sup> G <sub>9/2</sub>	360,482
303.505	-0.002	329,483.4	55	893	3 <sup>2</sup> G <sub>7/2</sub>	79,705	(2 <sup>1</sup> G) <sup>2</sup> F <sub>5/2</sub>	409,186
303.557	-0.003	329,427.2	12	64	5 <sup>2</sup> D <sub>5/2</sub>	47,119	(4 <sup>3</sup> D) <sup>4</sup> F <sub>5/2</sub>	376,543
303.670	0.004	329,304.9	103	391	5 <sup>4</sup> G <sub>7/2</sub>	30,378	(4 <sup>3</sup> G) <sup>4</sup> G <sub>7/2</sub>	359,687
303.791	-0.004	329,173.5	46	331	5 <sup>2</sup> F <sub>5/2</sub>	57,413	(4 <sup>1</sup> S) <sup>2</sup> G <sub>3/2</sub>	386,582
303.852	0.001	329,107.7	69	335	5 <sup>2</sup> I <sub>11/2</sub>	44,011	(4 <sup>3</sup> G) <sup>4</sup> G <sub>9/2</sub>	373,120
303.950 <sup>d</sup>	-0.002	329,001.2	111	371	5 <sup>2</sup> G <sub>7/2</sub>	55,773	(4 <sup>1</sup> D) <sup>2</sup> F <sub>7/2</sub>	384,772
303.950 <sup>d</sup>		329,001.2	111	353	5 <sup>4</sup> G <sub>5/2</sub>	29,390	(4 <sup>3</sup> F) <sup>4</sup> G <sub>5/2</sub>	358,392
304.087	0.002	328,852.8	35	264	5 <sup>2</sup> F <sub>5/2</sub>	57,413	(4 <sup>1</sup> D) <sup>2</sup> D <sub>5/2</sub>	386,268
304.087	-0.004	328,852.8	35	61	3 <sup>4</sup> P <sub>1/2</sub>	34,605	(4 <sup>3</sup> D) <sup>4</sup> F <sub>3/2</sub>	363,454
304.154	-0.001	328,781.1	12	103	5 <sup>4</sup> G <sub>9/2</sub>	30,907	(4 <sup>3</sup> G) <sup>4</sup> G <sub>7/2</sub>	359,687
304.261	0.000	328,665.6	41	348	5 <sup>2</sup> I <sub>11/2</sub>	44,011	(4 <sup>3</sup> H) <sup>2</sup> H <sub>11/2</sub>	372,676
304.302	-0.001	328,621.4	28	210	5 <sup>4</sup> D <sub>5/2</sub>	39,299	(4 <sup>3</sup> D) <sup>4</sup> F <sub>5/2</sub>	367,919
304.338	-0.002	328,582.2	53	421	3 <sup>2</sup> H <sub>9/2</sub>	53,797	(4 <sup>1</sup> I) <sup>2</sup> H <sub>9/2</sub>	382,377
304.515	0.001	328,391.4	17	97	5 <sup>4</sup> D <sub>7/2</sub>	36,485	(4 <sup>3</sup> P) <sup>4</sup> F <sub>5/2</sub>	364,877
304.568		328,334.2	12	215	3 <sup>2</sup> D <sub>3/2</sub>	71,517	(4 <sup>3</sup> F) <sup>2</sup> D <sub>3/2</sub>	399,850
304.608 <sup>d</sup>	-0.004	328,290.9	36	163	5 <sup>4</sup> D <sub>7/2</sub>	36,485	(4 <sup>3</sup> F) <sup>4</sup> G <sub>9/2</sub>	364,772
304.608 <sup>d</sup>	-0.002	328,290.9	36	55	3 <sup>4</sup> F <sub>9/2</sub>	49,104	(4 <sup>3</sup> F) <sup>2</sup> G <sub>9/2</sub>	377,393
304.684	0.000	328,208.5	12	112	3 <sup>2</sup> F <sub>5/2</sub>	59,954	(4 <sup>1</sup> F) <sup>2</sup> G <sub>7/2</sub>	388,163
304.798	0.000	328,086.6	44	281	3 <sup>4</sup> P <sub>5/2</sub>	32,005	(4 <sup>3</sup> P) <sup>4</sup> P <sub>3/2</sub>	360,092
304.831	0.008	328,050.5	8	50	3 <sup>4</sup> F <sub>9/2</sub>	49,104	(4 <sup>3</sup> D) <sup>4</sup> F <sub>7/2</sub>	377,162
305.046 <sup>d</sup>	0.000	327,819.4	18	121	5 <sup>2</sup> D <sub>5/2</sub>	47,119	(4 <sup>3</sup> D) <sup>2</sup> P <sub>3/2</sub>	374,938
305.046 <sup>d</sup>	0.011	327,819.4	18	101	3 <sup>4</sup> F <sub>7/2</sub>	48,712	(4 <sup>3</sup> D) <sup>4</sup> F <sub>5/2</sub>	376,543
305.152	-0.002	327,705.2	91	266	3 <sup>2</sup> D <sub>5/2</sub>	72,934	(4 <sup>1</sup> F) <sup>2</sup> D <sub>5/2</sub>	400,637
305.172	-0.002	327,684.1	91	223	3 <sup>4</sup> P <sub>5/2</sub>	32,005	(4 <sup>3</sup> G) <sup>4</sup> G <sub>7/2</sub>	359,687
305.249	0.001	327,601.6	87	395	5 <sup>4</sup> G <sub>5/2</sub>	29,390	(4 <sup>3</sup> F) <sup>2</sup> D <sub>3/2</sub>	356,993
305.305	-0.003	327,541.3	32	49	3 <sup>2</sup> F <sub>7/2</sub>	53,353	(4 <sup>1</sup> G) <sup>2</sup> F <sub>5/2</sub>	380,891
305.341	0.004	327,503.1	49	406	5 <sup>4</sup> D <sub>5/2</sub>	39,299	(4 <sup>3</sup> F) <sup>4</sup> F <sub>7/2</sub>	366,806
305.441 <sup>t</sup>	-0.003	327,395.2	47	490	5 <sup>2</sup> G <sub>9/2</sub>	59,223	(4 <sup>1</sup> F) <sup>2</sup> G <sub>7/2</sub>	386,615
305.441 <sup>t</sup>	-0.001	327,395.2	47	234	5 <sup>4</sup> D <sub>5/2</sub>	39,299	(4 <sup>3</sup> D) <sup>4</sup> D <sub>5/2</sub>	366,693
305.441 <sup>t</sup>	-0.002	327,395.2	47	108	5 <sup>4</sup> D <sub>1/2</sub>	38,685	(4 <sup>3</sup> F) <sup>4</sup> F <sub>3/2</sub>	366,078
305.469	-0.002	327,365.7	58	111	3 <sup>2</sup> G <sub>9/2</sub>	79,131	(2 <sup>3</sup> F) <sup>2</sup> G <sub>7/2</sub>	406,495
305.524 <sup>d</sup>	0.000	327,306.8	54	145	5 <sup>2</sup> D <sub>5/2</sub>	47,119	(4 <sup>3</sup> G) <sup>4</sup> F <sub>5/2</sub>	374,426
305.524 <sup>d</sup>	0.003	327,306.8	54	154	3 <sup>4</sup> F <sub>9/2</sub>	49,104	(4 <sup>3</sup> G) <sup>4</sup> I <sub>11/2</sub>	376,414
305.554 <sup>d</sup>	0.001	327,274.8	262	868	5 <sup>2</sup> I <sub>13/2</sub>	45,546	(4 <sup>3</sup> G) <sup>4</sup> H <sub>13/2</sub>	372,822
305.554 <sup>d</sup>	-0.001	327,274.8	262	92	5 <sup>4</sup> D <sub>5/2</sub>	39,299	(4 <sup>3</sup> F) <sup>4</sup> F <sub>3/2</sub>	366,573
305.689	0.000	327,129.8	295	1616	5 <sup>2</sup> I <sub>13/2</sub>	45,546	(4 <sup>3</sup> H) <sup>2</sup> H <sub>11/2</sub>	372,676
305.787	0.002	327,025.0	265	1038	5 <sup>4</sup> G <sub>11/2</sub>	30,662	(4 <sup>3</sup> H) <sup>4</sup> G <sub>11/2</sub>	357,689
305.902	0.003	326,901.5	19	143	5 <sup>4</sup> D <sub>3/2</sub>	39,788	(4 <sup>3</sup> D) <sup>4</sup> D <sub>5/2</sub>	366,693
305.961	0.004	326,838.8	107	133	5 <sup>4</sup> G <sub>5/2</sub>	29,390	(4 <sup>3</sup> F) <sup>4</sup> D <sub>5/2</sub>	356,233
306.009 <sup>d</sup>	0.002	326,787.6	173	936	3 <sup>2</sup> G <sub>7/2</sub>	79,705	(2 <sup>3</sup> F) <sup>2</sup> G <sub>7/2</sub>	406,495
306.009 <sup>d</sup>	-0.002	326,787.6	173	266	5 <sup>4</sup> D <sub>3/2</sub>	39,788	(4 <sup>3</sup> F) <sup>4</sup> F <sub>3/2</sub>	366,573

Table A1. Cont.

$\lambda$ (Å) <sup>a</sup>	o-c, (Å) <sup>b</sup>	$\nu$ (cm <sup>-1</sup> )	I <sup>c</sup>	gA <sub>r</sub> (10 <sup>8</sup> s <sup>-1</sup> )	5d <sup>5</sup>		5d <sup>4</sup> 5p	
					Term <sup>e</sup>	E (cm <sup>-1</sup> )	Term <sup>e</sup>	E (cm <sup>-1</sup> )
306.020	0.006	326,775.9	31	397	5 <sup>4</sup> G <sub>9/2</sub>	30,907	(4 <sup>3</sup> H) <sup>4</sup> G <sub>11/2</sub>	357,689
306.072	0.004	326,720.1	21	146	5 <sup>2</sup> D <sub>3/2</sub>	48,086	(4 <sup>3</sup> P) <sup>2</sup> P <sub>1/2</sub>	374,810
306.159	0.000	326,627.8	46	361	3 <sup>2</sup> F <sub>5/2</sub>	59,954	(4 <sup>1</sup> S) <sup>2</sup> P <sub>3/2</sub>	386,582
306.288 <sup>d</sup>	-0.001	326,490.6	372	167	3 <sup>4</sup> F <sub>9/2</sub>	49,104	(4 <sup>3</sup> D) <sup>4</sup> F <sub>9/2</sub>	375,593
306.288 <sup>d</sup>	-0.001	326,490.6	372	1477	5 <sup>2</sup> I <sub>11/2</sub>	44,011	(4 <sup>3</sup> G) <sup>2</sup> H <sub>9/2</sub>	370,501
306.303	0.002	326,474.1	77	436	5 <sup>2</sup> F <sub>7/2</sub>	59,792	(4 <sup>1</sup> D) <sup>2</sup> D <sub>5/2</sub>	386,268
306.425	-0.004	326,344.3	16	55	5 <sup>2</sup> D <sub>3/2</sub>	48,086	(4 <sup>3</sup> G) <sup>4</sup> F <sub>5/2</sub>	374,426
306.479	0.003	326,286.8	12	110	5 <sup>4</sup> D <sub>3/2</sub>	39,788	(4 <sup>3</sup> F) <sup>4</sup> F <sub>3/2</sub>	366,078
306.712	-0.001	326,039.2	12	46	5 <sup>4</sup> G <sub>7/2</sub>	30,378	(4 <sup>3</sup> H) <sup>4</sup> I <sub>9/2</sub>	356,416
306.737	-0.004	326,011.7	23	294	3 <sup>2</sup> F <sub>5/2</sub>	59,954	(4 <sup>3</sup> D) <sup>2</sup> F <sub>5/2</sub>	385,962
306.781	-0.003	325,965.8	62	360	5 <sup>4</sup> D <sub>7/2</sub>	36,485	(4 <sup>3</sup> G) <sup>4</sup> F <sub>9/2</sub>	362,447
306.857	0.002	325,884.4	18	51	5 <sup>4</sup> D <sub>7/2</sub>	36,485	(4 <sup>3</sup> H) <sup>4</sup> G <sub>5/2</sub>	362,381
306.876	0.002	325,864.4	34	417	5 <sup>2</sup> F <sub>5/2</sub>	57,413	(4 <sup>3</sup> D) <sup>2</sup> D <sub>3/2</sub>	383,280
306.981	0.001	325,753.5	133	394	5 <sup>4</sup> G <sub>11/2</sub>	30,662	(4 <sup>3</sup> H) <sup>4</sup> I <sub>9/2</sub>	356,416
307.013	0.004	325,719.5	131	656	3 <sup>2</sup> F <sub>7/2</sub>	53,353	(4 <sup>1</sup> F) <sup>2</sup> F <sub>5/2</sub>	379,077
307.086 <sup>d</sup>	0.008	325,641.9	505	1764	5 <sup>2</sup> I <sub>11/2</sub>	44,011	(4 <sup>1</sup> I) <sup>2</sup> I <sub>11/2</sub>	369,661
307.086 <sup>d</sup>	0.001	325,641.9	505	213	5 <sup>2</sup> I <sub>11/2</sub>	44,011	(4 <sup>1</sup> I) <sup>2</sup> K <sub>13/2</sub>	369,654
307.147 <sup>d</sup>	0.001	325,577.1	393	172	5 <sup>4</sup> D <sub>5/2</sub>	39,299	(4 <sup>3</sup> P) <sup>4</sup> P <sub>5/2</sub>	364,877
307.147 <sup>d</sup>	0.000	325,577.1	393	1711	3 <sup>2</sup> H <sub>11/2</sub>	57,962	(4 <sup>1</sup> I) <sup>2</sup> H <sub>11/2</sub>	383,539
307.178	0.005	325,543.6	100	607	5 <sup>2</sup> G <sub>9/2</sub>	59,223	(4 <sup>1</sup> D) <sup>2</sup> F <sub>7/2</sub>	384,772
307.230	-0.002	325,488.8	31	185	3 <sup>4</sup> P <sub>1/2</sub>	34,605	(4 <sup>3</sup> P) <sup>4</sup> P <sub>3/2</sub>	360,092
307.290	0.003	325,425.5	3	139	3 <sup>2</sup> H <sub>9/2</sub>	53,797	(4 <sup>3</sup> G) <sup>2</sup> G <sub>9/2</sub>	379,226
307.448	0.006	325,257.7	70	609	3 <sup>2</sup> H <sub>9/2</sub>	53,797	(4 <sup>1</sup> G) <sup>2</sup> G <sub>7/2</sub>	379,061
307.579	-0.002	325,120.2	83	598	5 <sup>2</sup> G <sub>7/2</sub>	55,773	(4 <sup>1</sup> G) <sup>2</sup> F <sub>5/2</sub>	380,891
307.608	0.000	325,088.7	14	74	5 <sup>4</sup> D <sub>3/2</sub>	39,788	(4 <sup>3</sup> P) <sup>4</sup> F <sub>5/2</sub>	364,877
307.707	0.001	324,984.9	49	518	3 <sup>2</sup> G <sub>9/2</sub>	79,131	(2 <sup>3</sup> F) <sup>2</sup> F <sub>7/2</sub>	404,117
307.871		324,811.2	111	987	3 <sup>2</sup> G <sub>9/2</sub>	79,131	(2 <sup>3</sup> F) <sup>2</sup> G <sub>9/2</sub>	403,942
307.918 <sup>d</sup>	0.007	324,761.4	147	198	5 <sup>4</sup> D <sub>1/2</sub>	38,685	(4 <sup>3</sup> D) <sup>4</sup> F <sub>3/2</sub>	363,454
307.918 <sup>d</sup>	-0.003	324,761.4	147	786	3 <sup>2</sup> H <sub>11/2</sub>	57,962	(4 <sup>1</sup> G) <sup>2</sup> G <sub>9/2</sub>	382,720
307.981	-0.001	324,695.8	53	394	5 <sup>2</sup> G <sub>7/2</sub>	55,773	(4 <sup>1</sup> F) <sup>2</sup> F <sub>7/2</sub>	380,468
308.024	0.007	324,649.9	11	89	3 <sup>4</sup> F <sub>5/2</sub>	51,049	(4 <sup>3</sup> D) <sup>4</sup> D <sub>3/2</sub>	375,706
308.114	-0.001	324,555.0	16	110	5 <sup>2</sup> D <sub>5/2</sub>	47,119	(4 <sup>3</sup> G) <sup>4</sup> G <sub>7/2</sub>	371,673
308.180	0.002	324,486.0	96	453	3 <sup>4</sup> P <sub>5/2</sub>	32,005	(4 <sup>3</sup> F) <sup>4</sup> D <sub>7/2</sub>	356,493
308.247 <sup>d</sup>	0.003	324,415.1	66	179	5 <sup>2</sup> I <sub>11/2</sub>	44,011	(4 <sup>3</sup> G) <sup>4</sup> H <sub>9/2</sub>	368,429
308.247 <sup>d</sup>	-0.007	324,415.1	66	167	3 <sup>4</sup> F <sub>7/2</sub>	48,712	(4 <sup>3</sup> G) <sup>4</sup> G <sub>9/2</sub>	373,120
308.538 <sup>d</sup>	0.005	324,109.7	515	155	5 <sup>2</sup> I <sub>13/2</sub>	45,546	(4 <sup>1</sup> I) <sup>2</sup> I <sub>11/2</sub>	369,661
308.538 <sup>d</sup>	-0.002	324,109.7	515	1122	5 <sup>2</sup> I <sub>13/2</sub>	45,546	(4 <sup>1</sup> I) <sup>2</sup> K <sub>13/2</sub>	369,654
308.588 <sup>d</sup>		324,056.3	220	408	5 <sup>4</sup> G <sub>11/2</sub>	30,662	(4 <sup>3</sup> H) <sup>4</sup> H <sub>13/2</sub>	354,719
308.588 <sup>d</sup>	0.007	324,056.3	220	196	5 <sup>4</sup> G <sub>5/2</sub>	29,390	(4 <sup>3</sup> G) <sup>4</sup> H <sub>7/2</sub>	353,454
308.640	-0.004	324,001.7	62	284	5 <sup>4</sup> D <sub>7/2</sub>	36,485	(4 <sup>3</sup> F) <sup>4</sup> G <sub>9/2</sub>	360,482
308.685	0.007	323,954.5	16	31	5 <sup>4</sup> G <sub>9/2</sub>	30,907	(4 <sup>3</sup> D) <sup>4</sup> D <sub>7/2</sub>	354,869
308.820	-0.003	323,813.2	58	157	3 <sup>2</sup> F <sub>7/2</sub>	53,353	(4 <sup>3</sup> D) <sup>4</sup> F <sub>7/2</sub>	377,163
308.885	-0.001	323,745.4	59	255	5 <sup>4</sup> G <sub>7/2</sub>	30,378	(4 <sup>3</sup> H) <sup>4</sup> H <sub>9/2</sub>	354,122
308.922	-0.002	323,706.6	20	195	5 <sup>2</sup> G <sub>7/2</sub>	55,773	(4 <sup>3</sup> G) <sup>2</sup> F <sub>5/2</sub>	379,478
309.038	0.011	323,584.5	15	156	3 <sup>2</sup> H <sub>9/2</sub>	53,797	(4 <sup>3</sup> F) <sup>2</sup> G <sub>9/2</sub>	377,393
309.123	0.001	323,496.0	9	163	5 <sup>2</sup> G <sub>9/2</sub>	59,223	(4 <sup>1</sup> G) <sup>2</sup> G <sub>9/2</sub>	382,720
309.159	0.002	323,458.5	78	311	5 <sup>4</sup> G <sub>11/2</sub>	30,662	(4 <sup>3</sup> H) <sup>4</sup> H <sub>9/2</sub>	354,122
309.190	-0.005	323,426.0	12	86	3 <sup>2</sup> G <sub>7/2</sub>	79,705	(2 <sup>3</sup> F) <sup>4</sup> D <sub>7/2</sub>	403,133
309.243 <sup>d</sup>	0.007	323,370.1	45	219	3 <sup>4</sup> F <sub>5/2</sub>	51,049	(4 <sup>3</sup> F) <sup>4</sup> F <sub>5/2</sub>	374,426
309.243 <sup>d</sup>	-0.004	323,370.1	45	165	3 <sup>2</sup> H <sub>9/2</sub>	53,797	(4 <sup>3</sup> D) <sup>4</sup> F <sub>7/2</sub>	377,163
309.286	0.001	323,325.0	13	216	3 <sup>2</sup> F <sub>5/2</sub>	59,954	(4 <sup>3</sup> D) <sup>2</sup> D <sub>3/2</sub>	383,280
309.318	0.002	323,292.4	17	67	5 <sup>4</sup> G <sub>5/2</sub>	29,390	(4 <sup>3</sup> G) <sup>4</sup> G <sub>5/2</sub>	352,685
309.366	-0.002	323,241.3	55	212	3 <sup>4</sup> P <sub>3/2</sub>	32,994	(4 <sup>3</sup> F) <sup>4</sup> D <sub>5/2</sub>	356,233
309.426	0.008	323,178.8	90	168	5 <sup>4</sup> D <sub>3/2</sub>	39,788	(4 <sup>3</sup> P) <sup>4</sup> D <sub>5/2</sub>	362,975
309.450	0.000	323,153.9	90	593	5 <sup>2</sup> G <sub>9/2</sub>	59,223	(4 <sup>1</sup> I) <sup>2</sup> H <sub>9/2</sub>	382,377
309.633	-0.002	322,963.2	107	582	3 <sup>4</sup> F <sub>7/2</sub>	48,712	(4 <sup>3</sup> G) <sup>4</sup> G <sub>7/2</sub>	371,673
309.732	0.004	322,859.6	19	119	3 <sup>4</sup> P <sub>5/2</sub>	32,005	(4 <sup>3</sup> D) <sup>4</sup> D <sub>7/2</sub>	354,869
309.793		322,796.5	32	192	3 <sup>4</sup> P <sub>3/2</sub>	32,994	(4 <sup>3</sup> P) <sup>4</sup> P <sub>1/2</sub>	355,790

Table A1. Cont.

$\lambda$ (Å) <sup>a</sup>	o-c, (Å) <sup>b</sup>	$\nu$ (cm <sup>-1</sup> )	I <sup>c</sup>	gA <sub>ul</sub> (10 <sup>8</sup> s <sup>-1</sup> )	5d <sup>5</sup>		5d <sup>4</sup> 5p	
					Term <sup>e</sup>	E (cm <sup>-1</sup> )	Term <sup>e</sup>	E (cm <sup>-1</sup> )
309.976	0.011	322,605.2	23	148	3 <sup>2</sup> H <sub>9/2</sub>	53,797	(4 <sup>3</sup> G) <sup>4</sup> G <sub>11/2</sub>	376,414
310.029	-0.003	322,550.5	73	151	5 <sup>4</sup> G <sub>9/2</sub>	30,907	(4 <sup>3</sup> G) <sup>4</sup> H <sub>7/2</sub>	353,454
310.140	-0.005	322,434.9	52	310	3 <sup>2</sup> G <sub>9/2</sub>	79,131	(2 <sup>1</sup> G) <sup>2</sup> H <sub>9/2</sub>	401,561
310.211	-0.011	322,360.8	15	111	3 <sup>4</sup> F <sub>7/2</sub>	48,712	(4 <sup>3</sup> H) <sup>2</sup> H <sub>9/2</sub>	371,061
310.259	-0.005	322,311.8	37	90	5 <sup>4</sup> G <sub>7/2</sub>	30,378	(4 <sup>3</sup> G) <sup>4</sup> G <sub>5/2</sub>	352,685
310.340	0.003	322,227.0	48	75	3 <sup>4</sup> P <sub>5/2</sub>	32,005	(4 <sup>5</sup> D) <sup>4</sup> D <sub>5/2</sub>	354,235
310.604	0.004	321,953.2	51	303	3 <sup>4</sup> F <sub>9/2</sub>	49,104	(4 <sup>3</sup> H) <sup>2</sup> H <sub>9/2</sub>	371,061
310.663	-0.003	321,892.2	89	407	3 <sup>4</sup> F <sub>9/2</sub>	49,104	(4 <sup>3</sup> F) <sup>2</sup> F <sub>7/2</sub>	370,993
310.707 <sup>d</sup>	0.002	321,847.2	21	124	5 <sup>2</sup> D <sub>5/2</sub>	47,119	(4 <sup>3</sup> P) <sup>4</sup> D <sub>7/2</sub>	368,968
310.707 <sup>d</sup>	0.009	321,847.2	21	194	3 <sup>2</sup> G <sub>7/2</sub>	79,705	(2 <sup>1</sup> G) <sup>2</sup> H <sub>9/2</sub>	401,561
310.885	0.002	321,662.3	5	165	5 <sup>2</sup> F <sub>5/2</sub>	57,412	(4 <sup>1</sup> F) <sup>2</sup> F <sub>5/2</sub>	379,076
310.923	-0.003	321,622.5	2	86	5 <sup>2</sup> G <sub>7/2</sub>	55,773	(4 <sup>3</sup> F) <sup>2</sup> G <sub>9/2</sub>	377,393
310.985 <sup>d</sup>	0.009	321,559.0	65	194	3 <sup>2</sup> H <sub>9/2</sub>	53,797	(4 <sup>3</sup> G) <sup>2</sup> G <sub>7/2</sub>	375,365
310.985 <sup>d</sup>	-0.001	321,559.0	65	225	5 <sup>2</sup> I <sub>11/2</sub>	44,011	(4 <sup>3</sup> F) <sup>4</sup> F <sub>9/2</sub>	365,569
311.058	0.003	321,483.3	122	687	3 <sup>2</sup> F <sub>7/2</sub>	53,353	(4 <sup>3</sup> H) <sup>4</sup> G <sub>7/2</sub>	374,839
311.121	0.002	321,418.0	17	38	5 <sup>4</sup> G <sub>11/2</sub>	30,662	(4 <sup>3</sup> H) <sup>4</sup> H <sub>11/2</sub>	352,082
311.161	0.007	321,376.6	43	223	3 <sup>4</sup> F <sub>9/2</sub>	49,104	(4 <sup>3</sup> G) <sup>4</sup> H <sub>11/2</sub>	370,488
311.272	0.002	321,262.0	49	513	3 <sup>2</sup> H <sub>11/2</sub>	57,962	(4 <sup>3</sup> G) <sup>2</sup> G <sub>9/2</sub>	379,226
311.355	-0.002	321,177.0	66	185	5 <sup>4</sup> G <sub>9/2</sub>	30,907	(4 <sup>3</sup> H) <sup>4</sup> H <sub>11/2</sub>	352,082
311.414	-0.001	321,115.8	8	169	3 <sup>2</sup> D <sub>5/2</sub>	72,934	(2 <sup>3</sup> F) <sup>4</sup> F <sub>5/2</sub>	394,049
311.453	-0.003	321,076.2	18	81	3 <sup>2</sup> F <sub>7/2</sub>	53,353	(4 <sup>3</sup> G) <sup>4</sup> F <sub>5/2</sub>	374,426
311.518 <sup>d</sup>	-0.006	321,008.4	60	381	3 <sup>4</sup> F <sub>5/2</sub>	51,049	(4 <sup>3</sup> H) <sup>4</sup> G <sub>5/2</sub>	372,051
311.518 <sup>d</sup>	-0.002	321,008.4	60	59	5 <sup>2</sup> I <sub>11/2</sub>	44,011	(4 <sup>3</sup> H) <sup>4</sup> H <sub>11/2</sub>	365,017
311.594 <sup>d</sup>	0.006	320,930.4	36	412	3 <sup>2</sup> F <sub>5/2</sub>	59,954	(4 <sup>1</sup> G) <sup>2</sup> F <sub>5/2</sub>	380,891
311.594 <sup>d</sup>	0.002	320,930.4	36	154	3 <sup>2</sup> G <sub>7/2</sub>	79,705	(4 <sup>1</sup> F) <sup>2</sup> D <sub>5/2</sub>	400,637
311.845	0.003	320,672.7	8	146	3 <sup>2</sup> D <sub>5/2</sub>	72,934	(4 <sup>1</sup> D) <sup>2</sup> P <sub>3/2</sub>	393,610
311.891	0.005	320,624.5	20	135	3 <sup>4</sup> F <sub>3/2</sub>	53,796	(4 <sup>3</sup> G) <sup>4</sup> F <sub>5/2</sub>	374,426
311.963	0.004	320,551.2	24	164	3 <sup>4</sup> P <sub>3/2</sub>	32,994	(4 <sup>5</sup> D) <sup>4</sup> D <sub>3/2</sub>	353,549
312.007	0.001	320,505.8	9	78	5 <sup>2</sup> I <sub>11/2</sub>	44,011	(4 <sup>3</sup> H) <sup>2</sup> I <sub>13/2</sub>	364,518
312.030	0.001	320,481.5	26	118	5 <sup>2</sup> D <sub>3/2</sub>	48,086	(4 <sup>3</sup> F) <sup>4</sup> D <sub>3/2</sub>	368,569
312.465	0.000	320,035.6	29	140	3 <sup>2</sup> D <sub>3/2</sub>	71,517	(2 <sup>3</sup> P) <sup>4</sup> D <sub>3/2</sub>	391,553
312.497	0.000	320,002.7	59	466	5 <sup>2</sup> G <sub>9/2</sub>	59,223	(4 <sup>3</sup> G) <sup>2</sup> G <sub>9/2</sub>	379,226
312.716	0.001	319,779.1	36	152	3 <sup>2</sup> H <sub>9/2</sub>	53,797	(4 <sup>3</sup> F) <sup>4</sup> D <sub>7/2</sub>	373,577
312.742	0.003	319,752.1	36	149	3 <sup>2</sup> H <sub>11/2</sub>	57,962	(4 <sup>1</sup> G) <sup>2</sup> H <sub>11/2</sub>	377,717
312.807	0.000	319,685.6	39	345	5 <sup>2</sup> F <sub>7/2</sub>	59,792	(4 <sup>3</sup> G) <sup>2</sup> F <sub>5/2</sub>	379,478
312.836		319,656.8	99	248	5 <sup>4</sup> G <sub>5/2</sub>	29,390	(4 <sup>3</sup> H) <sup>4</sup> H <sub>7/2</sub>	349,047
312.895	-0.004	319,596.1	46	332	5 <sup>2</sup> G <sub>7/2</sub>	55,773	(4 <sup>3</sup> G) <sup>2</sup> G <sub>7/2</sub>	375,365
312.966	0.000	319,523.7	12	123	3 <sup>2</sup> F <sub>5/2</sub>	59,954	(4 <sup>3</sup> G) <sup>2</sup> F <sub>5/2</sub>	379,478
313.025	0.008	319,463.4	31	228	5 <sup>2</sup> I <sub>13/2</sub>	45,546	(4 <sup>3</sup> H) <sup>4</sup> H <sub>11/2</sub>	365,017
313.058	0.002	319,429.4	59	513	3 <sup>2</sup> H <sub>11/2</sub>	57,962	(4 <sup>3</sup> F) <sup>2</sup> G <sub>9/2</sub>	377,393
313.143	0.000	319,343.1	48	115	5 <sup>4</sup> G <sub>7/2</sub>	30,378	(4 <sup>3</sup> H) <sup>4</sup> I <sub>9/2</sub>	349,721
313.164	0.001	319,321.8	48	199	3 <sup>2</sup> H <sub>9/2</sub>	53,797	(4 <sup>3</sup> G) <sup>4</sup> G <sub>9/2</sub>	373,120
313.208	0.000	319,276.3	23	81	3 <sup>4</sup> P <sub>3/2</sub>	32,994	(4 <sup>5</sup> D) <sup>4</sup> D <sub>1/2</sub>	352,270
313.375	0.000	319,106.8	21	191	3 <sup>2</sup> F <sub>5/2</sub>	59,954	(4 <sup>1</sup> G) <sup>2</sup> G <sub>7/2</sub>	379,061
313.423	0.001	319,057.6	48	155	5 <sup>4</sup> G <sub>11/2</sub>	30,662	(4 <sup>3</sup> H) <sup>4</sup> I <sub>9/2</sub>	349,721
313.522		318,957.4	32	150	3 <sup>2</sup> G <sub>7/2</sub>	79,705	(2 <sup>3</sup> F) <sup>2</sup> F <sub>5/2</sub>	398,662
313.599	0.000	318,879.0	9	82	3 <sup>2</sup> H <sub>9/2</sub>	53,797	(4 <sup>3</sup> H) <sup>2</sup> H <sub>11/2</sub>	372,676
313.641	-0.006	318,835.7	9	72	3 <sup>4</sup> F <sub>5/2</sub>	51,049	(4 <sup>3</sup> P) <sup>4</sup> D <sub>7/2</sub>	369,878
313.957	0.009	318,514.8	17	92	5 <sup>2</sup> I <sub>11/2</sub>	44,011	(4 <sup>3</sup> H) <sup>2</sup> H <sub>11/2</sub>	362,535
313.981 <sup>d</sup>	0.003	318,490.5	17	147	5 <sup>2</sup> G <sub>9/2</sub>	59,223	(4 <sup>1</sup> G) <sup>2</sup> H <sub>11/2</sub>	377,717
313.981 <sup>d</sup>	-0.003	318,490.5	17	165	5 <sup>2</sup> D <sub>3/2</sub>	48,086	(4 <sup>3</sup> F) <sup>4</sup> F <sub>3/2</sub>	366,573
314.013	-0.001	318,458.5	66	339	3 <sup>2</sup> H <sub>11/2</sub>	57,962	(4 <sup>1</sup> I) <sup>2</sup> I <sub>13/2</sub>	376,419
314.152	0.003	318,316.8	7	60	3 <sup>2</sup> F <sub>7/2</sub>	53,353	(4 <sup>3</sup> G) <sup>4</sup> G <sub>7/2</sub>	371,673
314.212	-0.001	318,256.6	22	197	3 <sup>4</sup> F <sub>3/2</sub>	53,796	(4 <sup>3</sup> H) <sup>4</sup> G <sub>5/2</sub>	372,051
314.298 <sup>d</sup>	-0.006	318,169.6	18	206	1 <sup>2</sup> D <sub>3/2</sub>	104,821	(2 <sup>1</sup> D) <sup>2</sup> F <sub>5/2</sub>	422,985
314.298 <sup>d</sup>	0.000	318,169.6	18	220	5 <sup>2</sup> G <sub>9/2</sub>	59,223	(4 <sup>3</sup> F) <sup>2</sup> G <sub>9/2</sub>	377,393
314.370	-0.003	318,096.9	19	75	3 <sup>4</sup> F <sub>7/2</sub>	48,712	(4 <sup>3</sup> F) <sup>4</sup> F <sub>7/2</sub>	366,806
314.400	0.002	318,065.8	8	69	5 <sup>2</sup> I <sub>13/2</sub>	45,546	(4 <sup>3</sup> H) <sup>4</sup> I <sub>13/2</sub>	363,614
314.545	0.000	317,919.3	19	184	3 <sup>4</sup> F <sub>5/2</sub>	51,049	(4 <sup>3</sup> P) <sup>4</sup> D <sub>7/2</sub>	368,968

Table A1. Cont.

$\lambda$ (Å) <sup>a</sup>	o-c, (Å) <sup>b</sup>	$\nu$ (cm <sup>-1</sup> )	I <sup>c</sup>	$gA_r$ (10 <sup>8</sup> s <sup>-1</sup> )	5d <sup>5</sup>		5d <sup>4</sup> 5p	
					Term <sup>e</sup>	E (cm <sup>-1</sup> )	Term <sup>e</sup>	E (cm <sup>-1</sup> )
314.650	-0.010	317,813.5	9	113	5 <sup>2</sup> G <sub>7/2</sub>	55,773	(4 <sup>3</sup> F) <sup>4</sup> D <sub>7/2</sub>	373,577
314.712	-0.001	317,750.9	23	81	5 <sup>4</sup> D <sub>7/2</sub>	36,485	(4 <sup>5</sup> D) <sup>4</sup> D <sub>5/2</sub>	354,235
314.749	0.002	317,713.4	89	236	5 <sup>4</sup> G <sub>11/2</sub>	30,662	(4 <sup>5</sup> D) <sup>6</sup> D <sub>9/2</sub>	348,377
314.797	0.000	317,665.5	23	109	3 <sup>4</sup> P <sub>1/2</sub>	34,605	(4 <sup>3</sup> D) <sup>4</sup> D <sub>1/2</sub>	352,270
314.856	-0.005	317,605.8	22 VI	156	5 <sup>2</sup> F <sub>7/2</sub>	59,792	(4 <sup>2</sup> F) <sup>2</sup> G <sub>9/2</sub>	377,393
315.100	-0.012	317,359.3	14	145	5 <sup>2</sup> G <sub>7/2</sub>	55,773	(4 <sup>3</sup> G) <sup>4</sup> G <sub>9/2</sub>	373,120
315.192	-0.003	317,266.6	11	79	3 <sup>2</sup> H <sub>9/2</sub>	53,797	(4 <sup>3</sup> H) <sup>2</sup> H <sub>9/2</sub>	371,061
315.264 <sup>d</sup>	0.001	317,194.8	83	181	3 <sup>2</sup> H <sub>9/2</sub>	53,797	(4 <sup>3</sup> F) <sup>2</sup> F <sub>7/2</sub>	370,993
315.264 <sup>d</sup>	-0.004	317,194.8	83	310	5 <sup>2</sup> G <sub>9/2</sub>	59,223	(4 <sup>3</sup> G) <sup>4</sup> G <sub>11/2</sub>	376,414
315.327 <sup>d</sup>	-0.001	317,130.8	37	284	3 <sup>4</sup> F <sub>7/2</sub>	48,712	(4 <sup>3</sup> F) <sup>2</sup> G <sub>7/2</sub>	365,842
315.327 <sup>d</sup>	-0.005	317,130.8	37	125	3 <sup>2</sup> D <sub>5/2</sub>	72,934	(2 <sup>3</sup> F) <sup>4</sup> F <sub>5/2</sub>	390,060
315.552	0.001	316,905.2	16	119	5 <sup>2</sup> D <sub>5/2</sub>	47,119	(4 <sup>3</sup> D) <sup>2</sup> D <sub>5/2</sub>	364,025
315.751	-0.002	316,705.6	11	124	3 <sup>2</sup> H <sub>9/2</sub>	53,797	(4 <sup>3</sup> G) <sup>2</sup> H <sub>9/2</sub>	370,501
315.758	-0.007	316,698.2	18	97	3 <sup>2</sup> H <sub>9/2</sub>	53,797	(4 <sup>3</sup> G) <sup>4</sup> H <sub>11/2</sub>	370,488
315.988	0.003	316,467.3	4	41	5 <sup>2</sup> I <sub>11/2</sub>	44,011	(4 <sup>3</sup> H) <sup>4</sup> H <sub>11/2</sub>	360,481
316.291	0.000	316,164.3	18	148	5 <sup>2</sup> F <sub>5/2</sub>	57,413	(4 <sup>3</sup> F) <sup>4</sup> D <sub>7/2</sub>	373,577
316.384	0.010	316,071.5	9	106	3 <sup>2</sup> H <sub>9/2</sub>	53,797	(4 <sup>3</sup> P) <sup>4</sup> D <sub>7/2</sub>	369,878
316.548	0.006	315,907.6	44	248	3 <sup>4</sup> F <sub>9/2</sub>	49,104	(4 <sup>3</sup> H) <sup>4</sup> H <sub>11/2</sub>	365,017
316.588	-0.004	315,867.8	12	103	3 <sup>2</sup> H <sub>9/2</sub>	53,797	(4 <sup>1</sup> I) <sup>2</sup> I <sub>11/2</sub>	369,661
316.780	-0.009	315,676.9	21	149	3 <sup>4</sup> F <sub>9/2</sub>	49,104	(4 <sup>3</sup> F) <sup>4</sup> G <sub>9/2</sub>	364,772
316.804	-0.001	315,652.9	29	26	3 <sup>4</sup> F <sub>3/2</sub>	53,796	(4 <sup>3</sup> D) <sup>4</sup> P <sub>3/2</sub>	369,448
316.843	0.002	315,613.8	83	249	5 <sup>2</sup> G <sub>9/2</sub>	59,223	(4 <sup>3</sup> H) <sup>4</sup> G <sub>7/2</sub>	374,839
317.044	-0.002	315,413.3	8	46	3 <sup>2</sup> F <sub>5/2</sub>	59,954	(4 <sup>3</sup> G) <sup>2</sup> G <sub>7/2</sub>	375,365
317.146	-0.008	315,312.5	4	18	5 <sup>4</sup> G <sub>5/2</sub>	29,389	(4 <sup>3</sup> D) <sup>4</sup> F <sub>5/2</sub>	344,697
317.305	-0.001	315,154.6	126	362	5 <sup>4</sup> G <sub>9/2</sub>	30,907	(4 <sup>3</sup> D) <sup>4</sup> F <sub>7/2</sub>	346,061
317.408	-0.005	315,051.9	14	200	5 <sup>2</sup> F <sub>7/2</sub>	59,792	(4 <sup>3</sup> H) <sup>4</sup> G <sub>7/2</sub>	374,839
317.572	0.000	314,889.0	15	31	5 <sup>2</sup> D <sub>3/2</sub>	48,086	(4 <sup>3</sup> P) <sup>4</sup> D <sub>5/2</sub>	362,975
317.594	-0.003	314,867.0	26	65	5 <sup>4</sup> D <sub>1/2</sub>	38,685	(4 <sup>3</sup> D) <sup>4</sup> D <sub>3/2</sub>	353,549
317.710	-0.001	314,752.3	20	62	3 <sup>2</sup> D <sub>3/2</sub>	71,517	(4 <sup>3</sup> D) <sup>2</sup> D <sub>5/2</sub>	386,268
317.735	0.000	314,728.1	24	91	5 <sup>2</sup> G <sub>7/2</sub>	55,773	(4 <sup>3</sup> G) <sup>2</sup> H <sub>9/2</sub>	370,501
317.823	-0.008	314,640.2	31	135	3 <sup>2</sup> H <sub>9/2</sub>	53,797	(4 <sup>3</sup> G) <sup>4</sup> H <sub>9/2</sub>	368,429
318.013	-0.005	314,452.3	30 VI	156	5 <sup>4</sup> D <sub>3/2</sub>	39,788	(4 <sup>5</sup> D) <sup>4</sup> D <sub>5/2</sub>	354,235
318.174	0.001	314,293.4	30	125	5 <sup>2</sup> D <sub>3/2</sub>	48,086	(4 <sup>3</sup> H) <sup>4</sup> G <sub>5/2</sub>	362,381
318.202	-0.003	314,265.9	19	92	3 <sup>4</sup> F <sub>7/2</sub>	48,712	(4 <sup>3</sup> P) <sup>4</sup> D <sub>5/2</sub>	362,975
318.307	0.001	314,162.5	17	224	3 <sup>2</sup> G <sub>9/2</sub>	79,131	(2 <sup>3</sup> F) <sup>4</sup> G <sub>7/2</sub>	393,295
318.411	-0.004	314,059.9	11	37	3 <sup>4</sup> P <sub>5/2</sub>	32,005	(4 <sup>3</sup> D) <sup>4</sup> F <sub>7/2</sub>	346,061
318.791 <sup>d</sup>	-0.004	313,685.3	9	200	3 <sup>2</sup> D <sub>5/2</sub>	72,934	(4 <sup>1</sup> F) <sup>2</sup> G <sub>7/2</sub>	386,615
318.791 <sup>d</sup>	0.001	313,685.3	9	53	3 <sup>2</sup> H <sub>9/2</sub>	53,797	(4 <sup>3</sup> F) <sup>4</sup> G <sub>11/2</sub>	367,483
318.832	0.003	313,645.3	26	135	3 <sup>2</sup> D <sub>5/2</sub>	72,934	(4 <sup>1</sup> S) <sup>2</sup> P <sub>3/2</sub>	386,582
319.143 <sup>d</sup>	-0.005	313,338.9	14	126	3 <sup>2</sup> D <sub>5/2</sub>	72,934	(4 <sup>1</sup> D) <sup>2</sup> D <sub>5/2</sub>	386,268
319.143 <sup>d</sup>	0.004	313,338.9	14	184	3 <sup>4</sup> F <sub>9/2</sub>	49,104	(4 <sup>3</sup> G) <sup>4</sup> F <sub>9/2</sub>	362,447
319.273	-0.002	313,211.9	14	46	5 <sup>2</sup> D <sub>3/2</sub>	48,086	(4 <sup>3</sup> F) <sup>4</sup> F <sub>5/2</sub>	361,296
319.534	0.002	312,955.9	102	256	5 <sup>4</sup> G <sub>7/2</sub>	30,378	(4 <sup>5</sup> D) <sup>4</sup> F <sub>5/2</sub>	343,336
319.902	-0.003	312,595.6	65	194	5 <sup>4</sup> G <sub>5/2</sub>	29,390	(4 <sup>3</sup> D) <sup>4</sup> F <sub>3/2</sub>	341,983
320.035	-0.001	312,465.5	12	57	5 <sup>2</sup> F <sub>5/2</sub>	57,413	(4 <sup>3</sup> P) <sup>4</sup> D <sub>7/2</sub>	369,878
320.251	0.004	312,255.5	14	30	5 <sup>2</sup> F <sub>7/2</sub>	59,792	(4 <sup>3</sup> H) <sup>4</sup> G <sub>5/2</sub>	372,051
320.366	0.000	312,142.8	18	43	5 <sup>2</sup> I <sub>13/2</sub>	45,546	(4 <sup>3</sup> H) <sup>4</sup> G <sub>11/2</sub>	357,689
320.625	0.001	311,891.2	28	89	5 <sup>4</sup> D <sub>7/2</sub>	36,485	(4 <sup>5</sup> D) <sup>6</sup> D <sub>9/2</sub>	348,377
320.752 <sup>d</sup>	0.003	311,767.4	14	62	5 <sup>2</sup> G <sub>9/2</sub>	59,223	(4 <sup>3</sup> F) <sup>2</sup> F <sub>7/2</sub>	370,993
320.752 <sup>d</sup>	-0.005	311,767.4	9	248	3 <sup>2</sup> D <sub>3/2</sub>	71,517	(4 <sup>3</sup> D) <sup>2</sup> D <sub>3/2</sub>	383,280
320.823 <sup>d</sup>	0.000	311,698.5	25	82	3 <sup>2</sup> H <sub>11/2</sub>	57,962	(4 <sup>1</sup> I) <sup>2</sup> I <sub>11/2</sub>	369,661
320.823 <sup>d</sup>	-0.008	311,698.5	25	216	3 <sup>2</sup> G <sub>7/2</sub>	79,705	(2 <sup>3</sup> S) <sup>2</sup> G <sub>5/2</sub>	391,396
320.900	0.003	311,623.9	60	163	5 <sup>4</sup> G <sub>11/2</sub>	30,662	(4 <sup>5</sup> D) <sup>6</sup> D <sub>9/2</sub>	342,289
321.154	0.001	311,377.5	15 VI	66	3 <sup>4</sup> F <sub>9/2</sub>	49,104	(4 <sup>3</sup> F) <sup>4</sup> G <sub>9/2</sub>	360,482
321.198	-0.003	311,334.3	26	136	3 <sup>4</sup> P <sub>5/2</sub>	32,005	(4 <sup>3</sup> D) <sup>4</sup> F <sub>5/2</sub>	343,336
321.257	0.001	311,277.1	17	19	5 <sup>2</sup> G <sub>9/2</sub>	59,223	(4 <sup>3</sup> G) <sup>2</sup> H <sub>9/2</sub>	370,501
321.312	-0.004	311,224.0	18	42	3 <sup>2</sup> H <sub>9/2</sub>	53,797	(4 <sup>3</sup> H) <sup>4</sup> H <sub>11/2</sub>	365,017

Table A1. Cont.

$\lambda$ (Å) <sup>a</sup>	o-c, (Å) <sup>b</sup>	$\nu$ (cm <sup>-1</sup> )	I <sup>c</sup>	$\frac{gA_r}{(10^8 \text{ s}^{-1})}$	5d <sup>5</sup>		5d <sup>4</sup> 5p	
					Term <sup>e</sup>	E (cm <sup>-1</sup> )	Term <sup>e</sup>	E (cm <sup>-1</sup> )
322.007	-0.001	310,552.4	41	91	5 <sup>4</sup> G <sub>9/2</sub>	30,907	(4 <sup>5</sup> D) <sup>6</sup> D <sub>7/2</sub>	341,458
322.338		310,233.1	29	579	1 <sup>2</sup> D <sub>5/2</sub>	103,996	(2 <sup>3</sup> F) <sup>2</sup> D <sub>5/2</sub>	414,230
322.612	0.002	309,969.4	8	57	3 <sup>4</sup> P <sub>5/2</sub>	32,005	(4 <sup>5</sup> D) <sup>4</sup> F <sub>3/2</sub>	341,976
322.852	0.006	309,739.4	13	74	5 <sup>2</sup> G <sub>9/2</sub>	59,223	(4 <sup>3</sup> P) <sup>4</sup> D <sub>7/2</sub>	368,968
323.598	0.007	309,025.3	12 VI	118	3 <sup>2</sup> G <sub>9/2</sub>	79,131	(4 <sup>1</sup> F) <sup>2</sup> G <sub>7/2</sub>	388,163
323.626	0.000	308,998.8	11	5	5 <sup>2</sup> G <sub>7/2</sub>	55,773	(4 <sup>3</sup> F) <sup>4</sup> G <sub>9/2</sub>	364,772
323.721	-0.001	308,907.5	17	87	5 <sup>2</sup> D <sub>3/2</sub>	48,086	(4 <sup>3</sup> F) <sup>2</sup> D <sub>3/2</sub>	356,993
323.897	-0.002	308,740.0	22	204	3 <sup>2</sup> H <sub>9/2</sub>	53,797	(4 <sup>3</sup> H) <sup>2</sup> I <sub>11/2</sub>	362,535
324.055	-0.005	308,589.8	25	199	3 <sup>4</sup> F <sub>9/2</sub>	49,104	(4 <sup>3</sup> H) <sup>4</sup> G <sub>11/2</sub>	357,689
324.404	0.003	308,257.6	26 VI	79	5 <sup>2</sup> G <sub>9/2</sub>	59,223	(4 <sup>3</sup> F) <sup>4</sup> G <sub>11/2</sub>	367,483
324.427	-0.003	308,235.7	82	59	3 <sup>4</sup> P <sub>3/2</sub>	32,994	(4 <sup>5</sup> D) <sup>6</sup> D <sub>11/2</sub>	341,227
324.458	0.003	308,206.7	38	87	5 <sup>4</sup> D <sub>7/2</sub>	36,485	(4 <sup>5</sup> D) <sup>4</sup> F <sub>5/2</sub>	344,695
324.718	0.002	307,959.3	19	194	3 <sup>2</sup> D <sub>3/2</sub>	71,517	(4 <sup>1</sup> G) <sup>2</sup> F <sub>5/2</sub>	379,478
325.135	-0.005	307,564.4	5	92	3 <sup>2</sup> D <sub>3/2</sub>	71,516	(4 <sup>1</sup> F) <sup>2</sup> F <sub>5/2</sub>	379,077
325.170	0.003	307,531.5	15	74	3 <sup>2</sup> D <sub>5/2</sub>	72,934	(4 <sup>1</sup> F) <sup>2</sup> F <sub>7/2</sub>	380,468
325.319	-0.001	307,390.2	32	161	3 <sup>4</sup> F <sub>9/2</sub>	49,104	(4 <sup>3</sup> F) <sup>4</sup> D <sub>7/2</sub>	356,493
325.829	0.001	306,909.1	5	51	3 <sup>2</sup> G <sub>7/2</sub>	79,705	(4 <sup>1</sup> F) <sup>2</sup> G <sub>7/2</sub>	386,615
325.943	0.008	306,802.0	13	4	3 <sup>2</sup> H <sub>11/2</sub>	57,962	(4 <sup>3</sup> F) <sup>4</sup> G <sub>9/2</sub>	364,772
326.139	0.004	306,618.0	17	19	3 <sup>4</sup> P <sub>1/2</sub>	34,605	(4 <sup>5</sup> D) <sup>6</sup> D <sub>11/2</sub>	341,227
326.204	-0.001	306,556.6	26 VI	122	3 <sup>2</sup> H <sub>11/2</sub>	57,962	(4 <sup>3</sup> H) <sup>2</sup> I <sub>13/2</sub>	364,518
326.519	-0.004	306,260.7	9	129	3 <sup>2</sup> G <sub>7/2</sub>	79,705	(4 <sup>3</sup> D) <sup>2</sup> F <sub>5/2</sub>	385,962
326.609	0.002	306,176.4	13	12	3 <sup>4</sup> P <sub>3/2</sub>	32,994	(4 <sup>5</sup> D) <sup>6</sup> D <sub>5/2</sub>	339,172
326.915 <sup>d</sup>	0.000	305,890.1	24	41	3 <sup>2</sup> H <sub>9/2</sub>	53,797	(4 <sup>3</sup> G) <sup>4</sup> G <sub>7/2</sub>	359,687
326.915 <sup>d</sup>	0.003	305,890.1	24	318	1 <sup>2</sup> D <sub>5/2</sub>	103,996	(2 <sup>1</sup> G) <sup>2</sup> F <sub>7/2</sub>	409,889
327.004	-0.003	305,806.4	11	20	5 <sup>4</sup> D <sub>7/2</sub>	36,485	(4 <sup>3</sup> D) <sup>6</sup> D <sub>9/2</sub>	342,289
327.048	0.000	305,765.2	39	219	3 <sup>4</sup> F <sub>9/2</sub>	49,104	(4 <sup>5</sup> D) <sup>4</sup> D <sub>7/2</sub>	354,869
327.307	-0.001	305,523.8	38 VI	119	3 <sup>4</sup> F <sub>7/2</sub>	48,712	(4 <sup>5</sup> D) <sup>4</sup> D <sub>5/2</sub>	354,235
327.438	-0.002	305,401.0	31	133	5 <sup>4</sup> D <sub>5/2</sub>	39,299	(4 <sup>3</sup> D) <sup>4</sup> F <sub>5/2</sub>	344,697
327.850	0.001	305,017.1	8	20	3 <sup>4</sup> F <sub>9/2</sub>	49,104	(4 <sup>3</sup> H) <sup>4</sup> H <sub>9/2</sub>	354,122
328.555	0.002	304,362.8	31 VI	228	1 <sup>2</sup> D <sub>3/2</sub>	104,821	(2 <sup>1</sup> G) <sup>2</sup> F <sub>5/2</sub>	409,186
329.712	0.003	303,295.2	12	36	5 <sup>4</sup> D <sub>1/2</sub>	38,685	(4 <sup>3</sup> D) <sup>4</sup> F <sub>3/2</sub>	341,983
329.830	0.000	303,186.1	21	94	3 <sup>4</sup> F <sub>5/2</sub>	51,049	(4 <sup>5</sup> D) <sup>4</sup> D <sub>5/2</sub>	354,235
330.391	0.000	302,672.1	16	202	3 <sup>2</sup> G <sub>7/2</sub>	79,705	(4 <sup>1</sup> I) <sup>2</sup> H <sub>9/2</sub>	382,377
330.560	0.004	302,516.8	15	50	3 <sup>2</sup> H <sub>11/2</sub>	57,962	(4 <sup>3</sup> F) <sup>4</sup> G <sub>9/2</sub>	360,482
332.140	-0.006	301,077.9	12	65	3 <sup>2</sup> H <sub>9/2</sub>	53,797	(4 <sup>3</sup> D) <sup>4</sup> D <sub>7/2</sub>	354,869
332.353	-0.003	300,885.1	11	69	3 <sup>2</sup> F <sub>7/2</sub>	53,353	(4 <sup>3</sup> D) <sup>4</sup> D <sub>5/2</sub>	354,235
332.485 <sup>d</sup>	-0.003	300,765.3	12	133	3 <sup>2</sup> G <sub>7/2</sub>	79,705	(4 <sup>1</sup> F) <sup>2</sup> F <sub>7/2</sub>	380,468
332.485 <sup>d</sup>	0.004	300,765.3	12	76	3 <sup>2</sup> F <sub>7/2</sub>	53,353	(4 <sup>3</sup> H) <sup>4</sup> H <sub>9/2</sub>	354,122
333.198	-0.001	300,121.8	4	266	1 <sup>2</sup> D <sub>5/2</sub>	103,996	(2 <sup>3</sup> F) <sup>2</sup> F <sub>7/2</sub>	404,117
334.140	-0.003	299,275.8	12	52	3 <sup>4</sup> F <sub>9/2</sub>	49,104	(4 <sup>5</sup> D) <sup>6</sup> D <sub>9/2</sub>	348,377
334.911	-0.001	298,587.1	1	53	3 <sup>2</sup> G <sub>9/2</sub>	79,131	(4 <sup>4</sup> G) <sup>2</sup> H <sub>11/2</sub>	377,717
338.225	-0.001	295,661.2	15	92	3 <sup>2</sup> G <sub>7/2</sub>	79,705	(4 <sup>3</sup> G) <sup>2</sup> G <sub>7/2</sub>	375,365
341.089	0.008	293,178.3	20	30	3 <sup>4</sup> F <sub>9/2</sub>	49,104	(4 <sup>5</sup> D) <sup>6</sup> D <sub>9/2</sub>	342,289
342.628	0.000	291,861.7	30	9	3 <sup>2</sup> G <sub>9/2</sub>	79,131	(4 <sup>3</sup> F) <sup>2</sup> F <sub>7/2</sub>	370,993

<sup>a</sup> Observed wavelengths, d—doubly identified, t—trebly identified; <sup>b</sup> Difference between the observed wavelength and the wavelength derived from the final level energies (Ritz wavelength). A blank value indicates that the upper level is derived only from that line; <sup>c</sup> Relative intensity; VI—line is also identified as Ag VI; <sup>e</sup> The number preceding the terms is seniority number.

Table A2. Identified lines of the 4d<sup>4</sup>–4d<sup>3</sup>5p transitions in the spectrum of Ag<sup>7+</sup>.

$\lambda$ (Å) <sup>a</sup>	o-c, (Å) <sup>b</sup>	$\nu$ (cm <sup>-1</sup> )	I <sup>c</sup>	$\frac{gA_r}{(10^8 \text{ s}^{-1})}$	5d <sup>4</sup>		5d <sup>3</sup> 5p	
					Term <sup>e</sup>	E (cm <sup>-1</sup> )	Term <sup>f</sup>	E (cm <sup>-1</sup> )
247.539	-0.005	403,976.8	56	150	4 <sup>3</sup> H <sub>6</sub>	28,185	(3 <sup>2</sup> F) <sup>3</sup> G <sub>5</sub>	432,154
253.534	-0.002	394,424.4	54	114	4 <sup>3</sup> H <sub>4</sub>	23,302	(3 <sup>2</sup> H) <sup>3</sup> G <sub>3</sub>	417,724
253.627	0.001	394,279.8	98	383	2 <sup>3</sup> F <sub>4</sub>	60,980	(1 <sup>2</sup> D) <sup>3</sup> F <sub>4</sub>	455,261
253.737	-0.001	394,108.9	60	284	4 <sup>5</sup> D <sub>3</sub>	5292	(3 <sup>4</sup> P) <sup>5</sup> P <sub>3</sub>	399,399

Table A2. Cont.

$\lambda$ (Å) <sup>a</sup>	o-c, (Å) <sup>b</sup>	$\nu$ (cm <sup>-1</sup> )	I <sup>c</sup>	$\frac{gA_{ul}}{(10^8 \text{ s}^{-1})}$	5d <sup>4</sup>		5d <sup>3</sup> 5p	
					Term <sup>e</sup>	E (cm <sup>-1</sup> )	Term <sup>f</sup>	E (cm <sup>-1</sup> )
254.226	-0.003	393,350.8	20	174	4 <sup>1</sup> G <sub>4</sub>	43,104	(3 <sup>2</sup> F) <sup>1</sup> F <sub>3</sub>	436,451
254.451	0.001	393,003.0	23	75	4 <sup>3</sup> H <sub>6</sub>	28,185	(3 <sup>2</sup> H) <sup>1</sup> I <sub>6</sub>	421,189
254.641	0.000	392,709.8	17	41	2 <sup>3</sup> F <sub>3</sub>	62,552	(1 <sup>2</sup> D) <sup>3</sup> F <sub>4</sub>	455,261
255.131	0.000	391,955.5	550	1307	4 <sup>5</sup> D <sub>4</sub>	7443	(3 <sup>4</sup> P) <sup>5</sup> P <sub>3</sub>	399,399
255.214		391,828.0	140	596	2 <sup>3</sup> F <sub>4</sub>	60,980	(1 <sup>2</sup> D) <sup>3</sup> D <sub>3</sub>	452,808
255.570	0.001	391,282.2	28	99	4 <sup>5</sup> D <sub>0</sub>	0	(3 <sup>4</sup> P) <sup>5</sup> P <sub>1</sub>	391,283
255.891	0.000	390,791.4	38	78	2 <sup>3</sup> F <sub>3</sub>	62,552	(1 <sup>2</sup> D) <sup>1</sup> D <sub>2</sub>	453,343
255.891		390,791.4	38	210	4 <sup>3</sup> G <sub>3</sub>	26,967	(3 <sup>2</sup> D) <sup>3</sup> D <sub>2</sub>	417,758
255.919		390,748.6	115	455	4 <sup>5</sup> D <sub>3</sub>	5292	(3 <sup>4</sup> P) <sup>5</sup> P <sub>2</sub>	396,041
256.069		390,519.8	61	435	2 <sup>1</sup> G <sub>4</sub>	69,584	(1 <sup>2</sup> D) <sup>1</sup> F <sub>3</sub>	460,104
256.138		390,414.5	49	231	4 <sup>5</sup> D <sub>2</sub>	3212	(3 <sup>4</sup> P) <sup>5</sup> P <sub>2</sub>	393,630
256.446	-0.002	389,945.7	70	320	4 <sup>5</sup> D <sub>1</sub>	1,340	(3 <sup>4</sup> P) <sup>5</sup> P <sub>1</sub>	391,283
256.757		389,473.3	180	347	4 <sup>3</sup> H <sub>6</sub>	28,185	(3 <sup>2</sup> H) <sup>3</sup> I <sub>7</sub>	417,658
257.391	-0.001	388,514.0	110	354	4 <sup>5</sup> D <sub>4</sub>	7443	(3 <sup>4</sup> F) <sup>5</sup> F <sub>5</sub>	395,955
257.505	-0.003	388,342.0	57	314	4 <sup>5</sup> D <sub>3</sub>	5292	(3 <sup>4</sup> P) <sup>5</sup> P <sub>2</sub>	393,630
257.603	0.003	388,194.3	35	194	4 <sup>3</sup> G <sub>3</sub>	26,967	(3 <sup>4</sup> P) <sup>3</sup> D <sub>3</sub>	415,165
257.627	0.006	388,158.1	160d	114	4 <sup>3</sup> H <sub>4</sub>	23,302	(3 <sup>2</sup> D) <sup>3</sup> D <sub>3</sub>	411,469
257.627	0.007	388,158.1	160d	567	4 <sup>3</sup> F <sub>4</sub>	29,555	(3 <sup>2</sup> H) <sup>3</sup> G <sub>3</sub>	417,724
257.645	-0.004	388,131.0	83	482	4 <sup>3</sup> G <sub>4</sub>	32,698	(3 <sup>2</sup> H) <sup>3</sup> G <sub>4</sub>	420,822
257.685	0.000	388,070.7	260	437	4 <sup>5</sup> D <sub>2</sub>	3212	(3 <sup>4</sup> P) <sup>5</sup> P <sub>1</sub>	391,283
257.740	0.001	387,987.9	33	230	4 <sup>3</sup> P <sub>2</sub>	32,134	(3 <sup>2</sup> F) <sup>3</sup> F <sub>3</sub>	420,123
257.796	-0.002	387,903.6	43	172	4 <sup>5</sup> D <sub>3</sub>	5292	(3 <sup>4</sup> F) <sup>5</sup> F <sub>4</sub>	393,193
257.947	-0.001	387,676.5	68	289	4 <sup>5</sup> D <sub>2</sub>	3212	(3 <sup>4</sup> F) <sup>5</sup> F <sub>3</sub>	390,887
258.332	0.004	387,098.8	26	165	4 <sup>3</sup> F <sub>3</sub>	32926	(3 <sup>2</sup> P) <sup>3</sup> P <sub>2</sub>	420,031
258.347	0.002	387,076.3	29	107	4 <sup>3</sup> H <sub>5</sub>	26,250	(3 <sup>2</sup> G) <sup>1</sup> H <sub>5</sub>	413,329
258.583	0.003	386,723.0	120	492	4 <sup>3</sup> H <sub>5</sub>	26,250	(3 <sup>2</sup> F) <sup>1</sup> G <sub>4</sub>	412,977
258.855		386,316.7	22	82	4 <sup>5</sup> D <sub>0</sub>	0	(3 <sup>4</sup> F) <sup>5</sup> F <sub>1</sub>	386,317
259.104	-0.001	385,945.4	170	944	4 <sup>3</sup> G <sub>5</sub>	35,077	(3 <sup>2</sup> H) <sup>3</sup> G <sub>5</sub>	421,021
259.192	0.000	385,814.4	130	320	4 <sup>3</sup> H <sub>6</sub>	28,185	(3 <sup>2</sup> H) <sup>3</sup> I <sub>6</sub>	413,999
259.239	0.000	385,744.4	60d	412	4 <sup>3</sup> G <sub>5</sub>	35,077	(3 <sup>2</sup> H) <sup>3</sup> G <sub>4</sub>	420,822
259.239	0.004	385,744.4	60d	259	4 <sup>5</sup> D <sub>4</sub>	7443	(3 <sup>4</sup> F) <sup>5</sup> F <sub>4</sub>	393,193
259.283	-0.001	385,679.0	56	106	2 <sup>1</sup> G <sub>4</sub>	69,584	(1 <sup>2</sup> D) <sup>3</sup> F <sub>4</sub>	455,261
259.342	0.001	385,591.2	71d	163	4 <sup>3</sup> P <sub>1</sub>	26,526	(3 <sup>2</sup> D) <sup>3</sup> D <sub>1</sub>	412,118
259.342	0.011	385,591.2	71d	125	4 <sup>3</sup> H <sub>4</sub>	23,302	(3 <sup>2</sup> G) <sup>3</sup> H <sub>5</sub>	408,910
259.432	0.002	385,457.5	39	120	4 <sup>5</sup> D <sub>1</sub>	1340	(3 <sup>4</sup> F) <sup>5</sup> F <sub>2</sub>	386,800
259.643	0.000	385,144.2	120	672	4 <sup>3</sup> H <sub>6</sub>	28,185	(3 <sup>2</sup> G) <sup>1</sup> H <sub>5</sub>	413,329
259.878	-0.001	384,795.9	110d	155	4 <sup>3</sup> G <sub>4</sub>	32,698	(3 <sup>2</sup> D) <sup>3</sup> F <sub>4</sub>	417,492
259.878	0.001	384,795.9	110d	680	4 <sup>3</sup> F <sub>3</sub>	32,926	(3 <sup>2</sup> H) <sup>3</sup> G <sub>3</sub>	417,724
259.978	0.003	384,647.9	130	554	4 <sup>5</sup> D <sub>3</sub>	5292	(3 <sup>4</sup> F) <sup>3</sup> G <sub>3</sub>	389,944
260.115	0.001	384,445.3	37	337	4 <sup>1</sup> F <sub>3</sub>	52,004	(3 <sup>2</sup> F) <sup>1</sup> F <sub>3</sub>	436,451
260.280	0.002	384,201.6	180	746	4 <sup>3</sup> H <sub>4</sub>	23,302	(3 <sup>2</sup> G) <sup>3</sup> F <sub>3</sub>	407,506
260.376	0.005	384,060.0	32	172	4 <sup>3</sup> F <sub>2</sub>	28,051	(3 <sup>2</sup> D) <sup>3</sup> D <sub>1</sub>	412,118
260.443	0.001	383,961.2	81	398	4 <sup>5</sup> D <sub>1</sub>	1340	(3 <sup>4</sup> F) <sup>5</sup> D <sub>2</sub>	385,302
260.575	0.000	383,766.7	41	302	2 <sup>3</sup> F <sub>3</sub>	62,552	(1 <sup>2</sup> D) <sup>3</sup> D <sub>3</sub>	446,318
260.695	-0.001	383,590.0	170	198	4 <sup>5</sup> D <sub>2</sub>	3212	(3 <sup>4</sup> F) <sup>5</sup> F <sub>2</sub>	386,800
260.709	-0.001	383,569.4	130	319	4 <sup>5</sup> D <sub>0</sub>	0	(3 <sup>4</sup> F) <sup>5</sup> D <sub>1</sub>	383,568
260.989	-0.004	383,157.9	59	220	4 <sup>3</sup> D <sub>3</sub>	36,879	(3 <sup>2</sup> P) <sup>3</sup> P <sub>2</sub>	420,031
261.086	0.000	383,015.6	290	561	4 <sup>5</sup> D <sub>4</sub>	7443	(3 <sup>4</sup> F) <sup>5</sup> G <sub>5</sub>	390,458
261.173	0.000	382,888.0	32	207	2 <sup>3</sup> F <sub>2</sub>	61,644	(1 <sup>2</sup> D) <sup>3</sup> D <sub>2</sub>	444,532
261.247	0.002	382,779.5	26	75	4 <sup>3</sup> G <sub>3</sub>	26,967	(3 <sup>2</sup> G) <sup>1</sup> F <sub>3</sub>	409,750
261.323	-0.001	382,668.2	1000	1735	4 <sup>3</sup> H <sub>6</sub>	28,185	(3 <sup>2</sup> G) <sup>3</sup> H <sub>6</sub>	410,851
261.328	0.000	382,660.9	958	1568	4 <sup>3</sup> H <sub>5</sub>	26,250	(3 <sup>2</sup> G) <sup>3</sup> H <sub>5</sub>	408,910
261.400		382,555.5	94	486	4 <sup>3</sup> G <sub>3</sub>	26,967	(3 <sup>2</sup> D) <sup>3</sup> F <sub>2</sub>	409,522
261.458	-0.002	382,470.6	99	547	4 <sup>3</sup> G <sub>4</sub>	32,698	(3 <sup>4</sup> P) <sup>3</sup> D <sub>3</sub>	415,165
261.496	0.000	382,415.0	590	1655	4 <sup>3</sup> G <sub>5</sub>	35,077	(3 <sup>2</sup> D) <sup>3</sup> F <sub>4</sub>	417,492
261.625	0.001	382,226.5	37	267	4 <sup>5</sup> D <sub>1</sub>	1340	(3 <sup>4</sup> F) <sup>5</sup> D <sub>1</sub>	383,568



Table A2. Cont.

$\lambda$ (Å) <sup>a</sup>	o-c, (Å) <sup>b</sup>	$\nu$ (cm <sup>-1</sup> )	I <sup>c</sup>	$\frac{gA_r}{(10^8 \text{ s}^{-1})}$	5d <sup>4</sup>		5d <sup>3</sup> 5p	
					Term <sup>e</sup>	E (cm <sup>-1</sup> )	Term <sup>f</sup>	E (cm <sup>-1</sup> )
261.718	0.000	382,090.7	250	720	4 <sup>5</sup> D <sub>2</sub>	3212	(3 <sup>4</sup> F) <sup>5</sup> D <sub>2</sub>	385,302
261.752	-0.003	382,041.0	490	1121	4 <sup>5</sup> D <sub>3</sub>	5292	(3 <sup>4</sup> F) <sup>5</sup> F <sub>3</sub>	387,329
261.793	0.000	381,981.2	65d	264	2 <sup>3</sup> F <sub>3</sub>	62,552	(1 <sup>2</sup> D) <sup>3</sup> D <sub>2</sub>	444,532
261.793	0.003	381,981.2	65d	399	4 <sup>3</sup> H <sub>5</sub>	26,250	(3 <sup>4</sup> P) <sup>5</sup> D <sub>4</sub>	408,236
261.836	-0.003	381,918.4	160	695	4 <sup>3</sup> F <sub>4</sub>	29,555	(3 <sup>2</sup> D) <sup>3</sup> D <sub>3</sub>	411,469
262.106	-0.003	381,525.0	420	950	4 <sup>5</sup> D <sub>4</sub>	7443	(3 <sup>4</sup> F) <sup>5</sup> F <sub>4</sub>	388,964
262.160	-0.001	381,446.4	670	1886	4 <sup>1</sup> I <sub>6</sub>	39,744	(3 <sup>2</sup> H) <sup>1</sup> I <sub>6</sub>	421,189
262.276	-0.001	381,277.8	620	2055	4 <sup>1</sup> I <sub>6</sub>	39,744	(3 <sup>2</sup> H) <sup>3</sup> G <sub>5</sub>	421,021
262.323	0.000	381,209.4	110	397	4 <sup>3</sup> P <sub>2</sub>	32,134	(3 <sup>2</sup> P) <sup>3</sup> P <sub>1</sub>	413,344
262.340		381,184.7	100	468	4 <sup>5</sup> D <sub>1</sub>	1340	(3 <sup>4</sup> F) <sup>5</sup> D <sub>0</sub>	382,525
262.520	-0.004	380,923.3	280d	359	4 <sup>3</sup> G <sub>5</sub>	35,077	(3 <sup>2</sup> H) <sup>1</sup> H <sub>5</sub>	415,995
262.520		380,923.3	280d	492	4 <sup>3</sup> H <sub>5</sub>	26,250	(3 <sup>4</sup> P) <sup>5</sup> D <sub>4</sub>	407,173
262.535		380,901.6	490	1502	4 <sup>1</sup> G <sub>4</sub>	43,104	(3 <sup>2</sup> P) <sup>3</sup> D <sub>3</sub>	424,006
262.653	-0.004	380,730.5	27	162	4 <sup>3</sup> H <sub>6</sub>	28,185	(3 <sup>2</sup> G) <sup>3</sup> H <sub>5</sub>	408,910
262.787	0.002	380,536.3	51	240	4 <sup>3</sup> G <sub>3</sub>	26,967	(3 <sup>2</sup> G) <sup>3</sup> F <sub>3</sub>	407,506
262.910		380,358.3	250d	553	4 <sup>3</sup> F <sub>2</sub>	28,051	(3 <sup>2</sup> G) <sup>3</sup> F <sub>2</sub>	408,409
262.910	-0.002	380,358.3	250d	688	4 <sup>5</sup> D <sub>2</sub>	3212	(3 <sup>4</sup> F) <sup>5</sup> D <sub>1</sub>	383,568
262.966	0.001	380,277.3	50	392	4 <sup>3</sup> G <sub>4</sub>	32,698	(3 <sup>2</sup> F) <sup>1</sup> G <sub>4</sub>	412,977
263.020	-0.003	380,199.2	87	269	4 <sup>3</sup> F <sub>4</sub>	29,555	(3 <sup>2</sup> G) <sup>1</sup> F <sub>3</sub>	409,750
263.150	-0.001	380,011.4	130	687	4 <sup>5</sup> D <sub>3</sub>	5292	(3 <sup>4</sup> F) <sup>5</sup> D <sub>2</sub>	385,302
263.212	0.003	379,921.9	370	1258	4 <sup>5</sup> D <sub>3</sub>	5292	(3 <sup>4</sup> F) <sup>5</sup> D <sub>4</sub>	385,218
263.240	0.003	379,881.5	73	306	4 <sup>5</sup> D <sub>4</sub>	7443	(3 <sup>4</sup> F) <sup>5</sup> F <sub>3</sub>	387,329
263.303		379,790.6	46	267	4 <sup>1</sup> G <sub>4</sub>	43,104	(3 <sup>2</sup> F) <sup>3</sup> F <sub>3</sub>	422,895
263.336	0.001	379,743.0	35	303	4 <sup>3</sup> P <sub>1</sub>	26,526	(3 <sup>2</sup> D) <sup>3</sup> D <sub>2</sub>	406,270
263.510	-0.004	379,492.3	250	1114	4 <sup>3</sup> F <sub>3</sub>	32,926	(3 <sup>2</sup> P) <sup>3</sup> D <sub>2</sub>	412,412
263.811	0.001	379,059.3	520	1894	4 <sup>3</sup> H <sub>6</sub>	28,185	(3 <sup>2</sup> H) <sup>3</sup> I <sub>5</sub>	407,246
263.914	-0.012	378,911.3	500t	372	4 <sup>3</sup> H <sub>5</sub>	26,250	(3 <sup>2</sup> H) <sup>3</sup> H <sub>5</sub>	405,144
263.914	0.007	378,911.3	500 t	279	4 <sup>3</sup> G <sub>5</sub>	35,077	(3 <sup>2</sup> H) <sup>3</sup> I <sub>6</sub>	413,999
263.914	0.001	378,911.3	500 t	1145	4 <sup>3</sup> H <sub>5</sub>	26,250	(3 <sup>2</sup> G) <sup>3</sup> G <sub>4</sub>	405,162
264.072	-0.003	378,684.6	84	627	4 <sup>3</sup> F <sub>4</sub>	29,555	(3 <sup>4</sup> P) <sup>5</sup> D <sub>4</sub>	408,236
264.159		378,559.9	140	338	4 <sup>3</sup> P <sub>0</sub>	21,309	(3 <sup>2</sup> P) <sup>3</sup> P <sub>1</sub>	399,869
264.293	0.000	378,367.9	470	1252	4 <sup>5</sup> D <sub>2</sub>	3212	(3 <sup>4</sup> F) <sup>5</sup> D <sub>3</sub>	381,580
264.374	0.000	378,252.0	50	384	4 <sup>3</sup> G <sub>5</sub>	35,077	(3 <sup>2</sup> G) <sup>1</sup> H <sub>5</sub>	413,329
264.409	-0.005	378,201.9	33	130	4 <sup>3</sup> G <sub>3</sub>	26,967	(3 <sup>2</sup> G) <sup>3</sup> G <sub>4</sub>	405,162
264.546	-0.001	378,006.1	23	208	4 <sup>3</sup> P <sub>1</sub>	26,526	(3 <sup>2</sup> P) <sup>3</sup> D <sub>1</sub>	404,530
264.581	-0.004	377,956.1	96	406	4 <sup>3</sup> F <sub>4</sub>	29,555	(3 <sup>2</sup> G) <sup>3</sup> F <sub>3</sub>	407,506
264.705	-0.003	377,779.0	680	2033	4 <sup>5</sup> D <sub>4</sub>	7443	(3 <sup>4</sup> F) <sup>5</sup> D <sub>4</sub>	385,218
264.752	0.004	377,712.0	65	753	4 <sup>1</sup> G <sub>4</sub>	43,104	(3 <sup>2</sup> H) <sup>3</sup> G <sub>4</sub>	420,822
264.769	0.002	377,687.7	180	415	4 <sup>3</sup> F <sub>4</sub>	29,555	(3 <sup>2</sup> H) <sup>3</sup> I <sub>5</sub>	407,246
264.802		377,640.7	73	288	2 <sup>1</sup> D <sub>2</sub>	88,586	(1 <sup>2</sup> D) <sup>1</sup> P <sub>1</sub>	466,227
265.169	-0.006	377,118.0	83	467	4 <sup>3</sup> H <sub>5</sub>	26,250	(3 <sup>2</sup> H) <sup>3</sup> H <sub>6</sub>	403,359
265.283	0.002	376,955.9	340	936	4 <sup>3</sup> H <sub>6</sub>	28,185	(3 <sup>2</sup> H) <sup>3</sup> H <sub>5</sub>	405,144
265.439		376,734.4	320d	1405	4 <sup>3</sup> G <sub>4</sub>	32,698	(3 <sup>2</sup> D) <sup>3</sup> F <sub>3</sub>	409,432
265.439	0.000	376,734.4	320d	317	2 <sup>1</sup> G <sub>4</sub>	69,584	(1 <sup>2</sup> D) <sup>3</sup> D <sub>3</sub>	446,318
265.620	0.001	376,477.7	78	366	4 <sup>3</sup> F <sub>2</sub>	28,051	(3 <sup>2</sup> P) <sup>3</sup> D <sub>1</sub>	404,530
265.728	-0.002	376,324.7	390	725	4 <sup>5</sup> D <sub>1</sub>	1340	(3 <sup>4</sup> F) <sup>3</sup> D <sub>2</sub>	377,661
265.782	0.002	376,248.2	500	1790	4 <sup>1</sup> I <sub>6</sub>	39,744	(3 <sup>2</sup> H) <sup>1</sup> H <sub>5</sub>	415,995
265.948	0.001	376,013.3	260	394	4 <sup>3</sup> D <sub>3</sub>	36,879	(3 <sup>2</sup> P) <sup>3</sup> D <sub>2</sub>	412,894
265.977	-0.007	375,972.3	440d	1413	4 <sup>3</sup> H <sub>4</sub>	23,302	(3 <sup>2</sup> G) <sup>1</sup> G <sub>4</sub>	399,265
265.977	0.008	375,972.3	440d	291	4 <sup>5</sup> D <sub>4</sub>	7443	(3 <sup>4</sup> F) <sup>5</sup> G <sub>5</sub>	383,426
266.238	0.002	375,603.8	170	816	4 <sup>3</sup> F <sub>4</sub>	29,555	(3 <sup>2</sup> G) <sup>3</sup> G <sub>4</sub>	405,162
266.285	0.001	375,537.5	140	292	4 <sup>3</sup> G <sub>4</sub>	32,698	(3 <sup>4</sup> P) <sup>5</sup> D <sub>4</sub>	408,236
266.384	0.003	375,397.9	420	1410	4 <sup>3</sup> H <sub>4</sub>	23,302	(3 <sup>2</sup> G) <sup>3</sup> G <sub>3</sub>	398,704
266.545	0.002	375,171.2	320	831	4 <sup>3</sup> H <sub>6</sub>	28,185	(3 <sup>2</sup> H) <sup>3</sup> H <sub>6</sub>	403,359
266.744		374,891.3	77	345	4 <sup>5</sup> D <sub>0</sub>	0	(3 <sup>4</sup> F) <sup>3</sup> D <sub>1</sub>	374,891

Table A2. Cont.

$\lambda$ (Å) <sup>a</sup>	o-c, (Å) <sup>b</sup>	$\nu$ (cm <sup>-1</sup> )	I <sup>c</sup>	$\frac{gA_r}{(10^8 \text{ s}^{-1})}$	5d <sup>4</sup>		5d <sup>3</sup> 5p	
					Term <sup>e</sup>	E (cm <sup>-1</sup> )	Term <sup>f</sup>	E (cm <sup>-1</sup> )
266.964	0.006	374,582.3	430t	921	4 <sup>3</sup> D <sub>3</sub>	36,879	(3 <sup>2</sup> D) <sup>3</sup> D <sub>3</sub>	411,469
266.964		374,582.3	430t	529	4 <sup>3</sup> D <sub>3</sub>	36,879	(3 <sup>4</sup> P) <sup>5</sup> S <sub>2</sub>	411,461
266.964	-0.002	374,582.3	430t	762	4 <sup>3</sup> F <sub>3</sub>	32,926	(3 <sup>2</sup> G) <sup>3</sup> F <sub>3</sub>	407,506
267.197	0.000	374,255.7	120	277	4 <sup>1</sup> I <sub>6</sub>	39,744	(3 <sup>2</sup> H) <sup>3</sup> I <sub>6</sub>	413,999
267.281	-0.001	374,138.1	250d	602	4 <sup>3</sup> P <sub>2</sub>	32,134	(3 <sup>2</sup> D) <sup>3</sup> D <sub>2</sub>	406,270
267.281	-0.001	374,138.1	250d	326	4 <sup>5</sup> D <sub>4</sub>	7443	(3 <sup>4</sup> F) <sup>5</sup> D <sub>3</sub>	381,580
267.426	0.001	373,935.2	130	462	4 <sup>3</sup> G <sub>3</sub>	26,967	(3 <sup>4</sup> P) <sup>5</sup> D <sub>2</sub>	400,904
267.676	-0.001	373,586.0	460d	1579	4 <sup>1</sup> I <sub>6</sub>	39,744	(3 <sup>2</sup> G) <sup>1</sup> H <sub>5</sub>	413,329
267.676	-0.003	373,586.0	460d	310	4 <sup>3</sup> H <sub>5</sub>	26,250	(3 <sup>4</sup> F) <sup>3</sup> G <sub>5</sub>	399,831
267.942	0.004	373,215.1	28	222	4 <sup>3</sup> D <sub>1</sub>	39,191	(3 <sup>2</sup> P) <sup>3</sup> D <sub>2</sub>	412,412
268.145	-0.004	372,932.6	48	324	4 <sup>3</sup> D <sub>1</sub>	39,191	(3 <sup>2</sup> D) <sup>3</sup> D <sub>1</sub>	412,118
268.201	-0.001	372,854.7	81	412	4 <sup>3</sup> F <sub>2</sub>	28,051	(3 <sup>4</sup> P) <sup>5</sup> D <sub>2</sub>	400,904
268.347	0.001	372,651.8	120	332	4 <sup>3</sup> H <sub>4</sub>	23,302	(3 <sup>4</sup> F) <sup>5</sup> F <sub>5</sub>	395,955
268.362		372,631.0	250	1228	4 <sup>1</sup> F <sub>3</sub>	52,004	(3 <sup>2</sup> D) <sup>1</sup> D <sub>2</sub>	424,635
268.487	-0.008	372,457.5	48d	274	4 <sup>3</sup> G <sub>4</sub>	32,698	(3 <sup>2</sup> H) <sup>3</sup> H <sub>5</sub>	405,144
268.487	0.005	372,457.5	48d	205	4 <sup>3</sup> G <sub>4</sub>	32,698	(3 <sup>2</sup> G) <sup>3</sup> G <sub>4</sub>	405,162
268.553	0.002	372,366.0	24	110	4 <sup>5</sup> D <sub>3</sub>	5292	(3 <sup>4</sup> F) <sup>3</sup> D <sub>2</sub>	377,661
268.597	-0.005	372,305.0	28	109	4 <sup>3</sup> G <sub>3</sub>	26,967	(3 <sup>2</sup> G) <sup>1</sup> G <sub>4</sub>	399,265
268.648	0.001	372,234.3	29	308	4 <sup>3</sup> F <sub>3</sub>	32,926	(3 <sup>2</sup> G) <sup>3</sup> G <sub>4</sub>	405,162
268.691	-0.004	372,174.7	31	270	4 <sup>3</sup> G <sub>5</sub>	35,077	(3 <sup>2</sup> H) <sup>3</sup> I <sub>5</sub>	407,246
269.009	0.002	371,734.8	71	618	4 <sup>3</sup> G <sub>3</sub>	26,967	(3 <sup>2</sup> G) <sup>3</sup> G <sub>3</sub>	398,704
269.074	0.001	371,645.0	390	1249	4 <sup>3</sup> H <sub>6</sub>	28,185	(3 <sup>4</sup> F) <sup>3</sup> G <sub>5</sub>	399,831
269.420	0.004	371,167.7	24	201	2 <sup>3</sup> F <sub>4</sub>	60,980	(3 <sup>2</sup> F) <sup>3</sup> G <sub>5</sub>	432,154
269.465	0.001	371,105.7	41	164	4 <sup>1</sup> I <sub>6</sub>	39,744	(3 <sup>2</sup> G) <sup>3</sup> H <sub>6</sub>	410,851
269.790	-0.004	370,658.7	33	364	4 <sup>3</sup> F <sub>2</sub>	28,051	(3 <sup>2</sup> G) <sup>3</sup> G <sub>3</sub>	398,704
270.102	0.001	370,230.5	350d	995	4 <sup>3</sup> H <sub>5</sub>	26,250	(3 <sup>4</sup> F) <sup>3</sup> G <sub>4</sub>	396,481
270.102	-0.004	370,230.5	350d	281	4 <sup>1</sup> G <sub>4</sub>	43,104	(3 <sup>2</sup> G) <sup>1</sup> H <sub>5</sub>	413,329
270.227	0.006	370,059.3	50	255	4 <sup>3</sup> G <sub>5</sub>	35,077	(3 <sup>2</sup> H) <sup>3</sup> H <sub>5</sub>	405,144
270.265		370,007.2	37	356	4 <sup>3</sup> D <sub>2</sub>	38,402	(3 <sup>2</sup> G) <sup>3</sup> F <sub>2</sub>	408,409
270.358		369,879.9	290d	395	2 <sup>3</sup> F <sub>3</sub>	62,552	(3 <sup>2</sup> F) <sup>3</sup> D <sub>2</sub>	432,431
270.358	-0.005	369,879.9	290d	858	4 <sup>1</sup> G <sub>4</sub>	43,104	(3 <sup>2</sup> F) <sup>1</sup> G <sub>4</sub>	412,977
270.518		369,661.2	32	330	2 <sup>3</sup> F <sub>4</sub>	60,980	(3 <sup>2</sup> F) <sup>3</sup> D <sub>3</sub>	430,642
270.958		369,060.9	110	382	2 <sup>3</sup> P <sub>1</sub>	63,371	(3 <sup>2</sup> F) <sup>3</sup> D <sub>2</sub>	432,431
271.536	0.005	368,275.3	37	205	4 <sup>3</sup> G <sub>5</sub>	35,077	(3 <sup>2</sup> H) <sup>3</sup> H <sub>6</sub>	403,359
271.933		367,737.7	270	1089	2 <sup>1</sup> G <sub>4</sub>	69,584	(3 <sup>2</sup> F) <sup>1</sup> G <sub>4</sub>	437,322
272.381	0.000	367,132.8	50	336	4 <sup>3</sup> G <sub>4</sub>	32,698	(3 <sup>4</sup> F) <sup>3</sup> G <sub>5</sub>	399,831
272.579	0.001	366,866.1	150	1131	2 <sup>1</sup> G <sub>4</sub>	69,584	(3 <sup>2</sup> F) <sup>1</sup> F <sub>3</sub>	436,451
272.743	-0.003	366,645.5	99	473	4 <sup>3</sup> H <sub>4</sub>	23,302	(3 <sup>4</sup> F) <sup>3</sup> G <sub>3</sub>	389,944
272.808	0.007	366,558.2	81	500	4 <sup>3</sup> G <sub>4</sub>	32,698	(3 <sup>2</sup> G) <sup>1</sup> G <sub>4</sub>	399,265
273.055	0.000	366,226.6	48	307	4 <sup>3</sup> G <sub>3</sub>	26,967	(3 <sup>4</sup> F) <sup>5</sup> F <sub>4</sub>	393,193
273.866	0.000	365,142.1	200	595	4 <sup>3</sup> G <sub>5</sub>	35,077	(3 <sup>4</sup> F) <sup>3</sup> F <sub>4</sub>	400,219
273.912		365,080.8	43	325	4 <sup>3</sup> G <sub>4</sub>	32,698	(3 <sup>4</sup> F) <sup>3</sup> F <sub>3</sub>	397,779
273.967		365,007.5	15	109	4 <sup>3</sup> P <sub>0</sub>	21,309	(3 <sup>4</sup> F) <sup>5</sup> F <sub>1</sub>	386,317
274.155	-0.002	364,757.2	160 d	415	4 <sup>3</sup> G <sub>5</sub>	35,077	(3 <sup>4</sup> F) <sup>3</sup> G <sub>5</sub>	399,831
274.155	0.000	364,757.2	160 d	663	2 <sup>1</sup> D <sub>2</sub>	88,586	(1 <sup>2</sup> D) <sup>1</sup> D <sub>2</sub>	453,343
274.705	0.000	364,026.9	31	200	4 <sup>3</sup> H <sub>4</sub>	23,302	(3 <sup>4</sup> F) <sup>5</sup> F <sub>3</sub>	387,329
275.061	-0.001	363,555.7	27	292	4 <sup>3</sup> F <sub>3</sub>	32,926	(3 <sup>4</sup> F) <sup>3</sup> G <sub>4</sub>	396,481
275.224	0.000	363,340.4	41	454	4 <sup>3</sup> D <sub>3</sub>	36,879	(3 <sup>4</sup> F) <sup>3</sup> F <sub>4</sub>	400,219
275.408		363,097.7	24	301	2 <sup>3</sup> P <sub>1</sub>	63,371	(3 <sup>4</sup> P) <sup>3</sup> S <sub>1</sub>	426,468
275.702	0.003	362,710.5	35	243	4 <sup>3</sup> H <sub>5</sub>	26,250	(3 <sup>4</sup> F) <sup>5</sup> F <sub>4</sub>	388,964
275.902		362,447.5	22	229	2 <sup>3</sup> F <sub>3</sub>	62,552	(3 <sup>2</sup> F) <sup>3</sup> F <sub>4</sub>	424,999
276.325	0.000	361,892.7	18	175	4 <sup>3</sup> F <sub>2</sub>	28,051	(3 <sup>4</sup> F) <sup>3</sup> G <sub>3</sub>	389,944
276.754	0.000	361,331.7	22	251	4 <sup>3</sup> F <sub>4</sub>	29,555	(3 <sup>4</sup> F) <sup>5</sup> F <sub>3</sub>	390,887
277.091	-0.001	360,892.3	24	140	4 <sup>1</sup> F <sub>3</sub>	52,004	(3 <sup>4</sup> P) <sup>3</sup> D <sub>2</sub>	412,894
277.749	0.003	360,037.3	110 d	376	2 <sup>3</sup> F <sub>4</sub>	60,980	(3 <sup>2</sup> H) <sup>3</sup> G <sub>5</sub>	421,021
277.749		360,037.3	110 d	594	4 <sup>1</sup> F <sub>3</sub>	52,004	(3 <sup>2</sup> H) <sup>1</sup> G <sub>4</sub>	412,041

Table A2. Cont.

$\lambda$ (Å) <sup>a</sup>	o-c, (Å) <sup>b</sup>	$\nu$ (cm <sup>-1</sup> )	I <sup>c</sup>	$gA_r$ (10 <sup>8</sup> s <sup>-1</sup> )	5d <sup>4</sup>		5d <sup>3</sup> 5p	
					Term <sup>e</sup>	E (cm <sup>-1</sup> )	Term <sup>f</sup>	E (cm <sup>-1</sup> )
278.440		359,143.8	24 d	390	2 <sup>1</sup> D <sub>2</sub>	88,586	(1 <sup>2</sup> D) <sup>3</sup> F <sub>2</sub>	447,730
278.440	-0.001	359,143.8	20 d	237	2 <sup>3</sup> F <sub>4</sub>	60,980	(3 <sup>2</sup> F) <sup>3</sup> F <sub>3</sub>	420,123
279.517	0.000	357,760.0	17	34	4 <sup>3</sup> G <sub>4</sub>	32,698	(3 <sup>4</sup> F) <sup>5</sup> G <sub>5</sub>	390,458
280.308	-0.005	356,750.4	22	285	2 <sup>3</sup> F <sub>4</sub>	60,980	(3 <sup>2</sup> H) <sup>3</sup> G <sub>3</sub>	417,724
280.775	0.003	356,157.1	17	188	4 <sup>1</sup> G <sub>4</sub>	43,104	(3 <sup>2</sup> G) <sup>1</sup> G <sub>4</sub>	399,265
281.501	0.002	355,238.5	27	130	4 <sup>3</sup> H <sub>6</sub>	28,185	(3 <sup>4</sup> F) <sup>5</sup> G <sub>5</sub>	383,426
284.333	0.000	351,700.3	12	73	2 <sup>3</sup> F <sub>2</sub>	61,644	(3 <sup>2</sup> P) <sup>3</sup> P <sub>1</sub>	413,344
284.791	0.000	351,134.7	17	147	4 <sup>3</sup> P <sub>1</sub>	26,526	(3 <sup>4</sup> F) <sup>3</sup> D <sub>2</sub>	377,661
287.065	-0.003	348,353.2	18	73	4 <sup>3</sup> G <sub>5</sub>	35,077	(3 <sup>4</sup> F) <sup>5</sup> G <sub>5</sub>	383,426
287.468	0.000	347,864.8	17	227	2 <sup>1</sup> D <sub>2</sub>	88,586	(3 <sup>2</sup> F) <sup>1</sup> F <sub>3</sub>	436,451

<sup>a</sup> Observed wavelengths, d—doubly identified, t—trebly identified; <sup>b</sup> Difference between the observed wavelength and the wavelength derived from the final level energies (Ritz wavelength). A blank value indicates that the upper level is derived only from that line; <sup>c</sup> Relative intensity; <sup>e</sup> The number preceding the terms is seniority number; <sup>f</sup> Term attribution is arbitrary in a few cases (see text) for the level composition, see Table A8. The number preceding the terms of the 5d<sup>3</sup> configuration is seniority number.

Table A3. Identified lines of the 4d<sup>4</sup>-(4d<sup>3</sup>4f + 4p<sup>5</sup>4d<sup>5</sup>) transitions in the spectrum of Ag<sup>7+</sup>.

$\lambda$ , Å <sup>a</sup>	o-c, (Å) <sup>b</sup>	$\nu$ (cm <sup>-1</sup> )	I <sup>c</sup>	$gA_r$ (10 <sup>9</sup> s <sup>-1</sup> )	4d <sup>4</sup>		(4d <sup>3</sup> 4f + 4p <sup>5</sup> 4d <sup>5</sup> )		
					Term <sup>e</sup>	E (cm <sup>-1</sup> )	Config. <sup>f</sup>	Term <sup>f</sup>	E (cm <sup>-1</sup> )
162.528	0.001	615,277	32	394	<sup>3</sup> G <sub>4</sub>	32,698	4p <sup>5</sup> 4d <sup>5</sup>	( <sup>4</sup> F) <sup>3</sup> F <sub>3</sub>	647,982
162.554	-0.001	615,182	26	564	<sup>3</sup> G <sub>5</sub>	35,078	4p <sup>5</sup> 4d <sup>5</sup>	( <sup>4</sup> F) <sup>3</sup> F <sub>4</sub>	650,256
164.321	-0.001	608,564	54	1260	<sup>3</sup> H <sub>5</sub>	26,249	4p <sup>5</sup> 4d <sup>5</sup>	( <sup>4</sup> G) <sup>3</sup> G <sub>4</sub>	634,810
164.542	0.001	607,749	534 IX	4247	<sup>3</sup> H <sub>6</sub>	28,185	4p <sup>5</sup> 4d <sup>5</sup>	( <sup>4</sup> G) <sup>3</sup> G <sub>5</sub>	635,935
165.158	0.004	605,482	122	567	<sup>3</sup> F <sub>4</sub> 2	29,555	4p <sup>5</sup> 4d <sup>5</sup>	( <sup>4</sup> G) <sup>3</sup> G <sub>3</sub>	635,050
165.481		604,300	294	5122	<sup>1</sup> I <sub>6</sub>	39,744	4p <sup>5</sup> 4d <sup>5</sup>	( <sup>2</sup> H) <sup>1</sup> H <sub>5</sub>	644,043
166.744	0.003	599,721	355 IX	2821	<sup>3</sup> G <sub>5</sub>	35,078	4p <sup>5</sup> 4d <sup>5</sup>	( <sup>4</sup> G) <sup>3</sup> G <sub>4</sub>	634,810
166.917	0.006	599,099	72	1966	<sup>1</sup> G <sub>4</sub> 1	69,585	4p <sup>5</sup> 4d <sup>5</sup>	( <sup>2</sup> G) <sup>1</sup> F <sub>3</sub>	668,708
167.156	-0.005	598,244	693	1429	<sup>3</sup> F <sub>4</sub> 2	29,555	4p <sup>5</sup> 4d <sup>5</sup>	( <sup>4</sup> P) <sup>3</sup> D <sub>3</sub>	627,779
167.460		597,158	190 IX	2888	<sup>5</sup> D <sub>4</sub>	7,442	4p <sup>5</sup> 4d <sup>5</sup>	( <sup>6</sup> S) <sup>5</sup> P <sub>3</sub>	604,600
167.731	0.000	596,193	111	275	<sup>1</sup> I <sub>6</sub>	39,744	4p <sup>5</sup> 4d <sup>5</sup>	( <sup>4</sup> G) <sup>3</sup> G <sub>5</sub>	635,935
167.835	-0.003	595,824	83	1261	<sup>3</sup> H <sub>5</sub>	26,249	4p <sup>5</sup> 4d <sup>5</sup>	( <sup>4</sup> D) <sup>3</sup> F <sub>4</sub>	622,060
168.436	0.000	593,698	254 IX	827	<sup>3</sup> G <sub>3</sub>	26,968	4p <sup>5</sup> 4d <sup>5</sup>	( <sup>4</sup> G) <sup>3</sup> F <sub>2</sub>	620,664
168.741	-0.003	592,625	20	509	<sup>3</sup> F <sub>2</sub> 2	28,051	4p <sup>5</sup> 4d <sup>5</sup>	( <sup>4</sup> G) <sup>3</sup> F <sub>2</sub>	620,664
168.932	-0.002	591,953	109 IX	2031	<sup>1</sup> G <sub>4</sub> 2	43,105	4p <sup>5</sup> 4d <sup>5</sup>	( <sup>4</sup> G) <sup>3</sup> G <sub>3</sub>	635,050
169.010	-0.003	591,683	24	591	<sup>5</sup> D <sub>2</sub>	3,212	4p <sup>5</sup> 4d <sup>5</sup>	( <sup>6</sup> S) <sup>5</sup> P <sub>2</sub>	594,881
169.235	0.002	590,894	37	432	<sup>3</sup> D <sub>3</sub>	36,878	4p <sup>5</sup> 4d <sup>5</sup>	( <sup>4</sup> P) <sup>3</sup> D <sub>3</sub>	627,779
169.613	0.003	589,578	72 IX	831	<sup>5</sup> D <sub>3</sub>	5,292	4p <sup>5</sup> 4d <sup>5</sup>	( <sup>6</sup> S) <sup>5</sup> P <sub>2</sub>	594,881
169.676	0.001	589,357	49	597	<sup>3</sup> G <sub>4</sub>	32,698	4p <sup>5</sup> 4d <sup>5</sup>	( <sup>4</sup> D) <sup>3</sup> F <sub>4</sub>	622,060
170.070		587,994	48	1080	<sup>3</sup> F <sub>3</sub> 1	62,552	4p <sup>5</sup> 4d <sup>5</sup>	( <sup>4</sup> F) <sup>3</sup> D <sub>2</sub>	650,545
170.271		587,298	39	513	<sup>1</sup> G <sub>4</sub> 2	43,105	4p <sup>5</sup> 4d <sup>5</sup>	( <sup>2</sup> D) <sup>3</sup> F <sub>3</sub>	630,389
170.359d	0.002	586,994	312 IX	1490	<sup>3</sup> F <sub>4</sub> 1	60,981	4p <sup>5</sup> 4d <sup>5</sup>	( <sup>4</sup> F) <sup>3</sup> F <sub>3</sub>	647,982
170.359d	-0.003	586,994	312 IX	664	<sup>3</sup> G <sub>5</sub>	35,078	4p <sup>5</sup> 4d <sup>5</sup>	( <sup>4</sup> D) <sup>3</sup> F <sub>4</sub>	622,060
170.595	0.002	586,184	57	628	<sup>3</sup> G <sub>5</sub>	35,078	4p <sup>5</sup> 4d <sup>5</sup>	( <sup>2</sup> I) <sup>1</sup> I <sub>6</sub>	621,268
170.812	-0.003	585,439	23	881	<sup>3</sup> F <sub>3</sub> 1	62,552	4p <sup>5</sup> 4d <sup>5</sup>	( <sup>4</sup> F) <sup>3</sup> F <sub>3</sub>	647,982
171.075	0.001	584,539	35	643	<sup>3</sup> F <sub>2</sub> 1	61,645	4p <sup>5</sup> 4d <sup>5</sup>	( <sup>4</sup> D) <sup>3</sup> P <sub>2</sub>	646,185
171.339	-0.001	583,638	46	492	<sup>3</sup> F <sub>3</sub> 1	62,552	4p <sup>5</sup> 4d <sup>5</sup>	( <sup>4</sup> D) <sup>3</sup> P <sub>2</sub>	646,185
171.512	-0.001	583,050	34	337	<sup>1</sup> F <sub>3</sub>	52,004	4p <sup>5</sup> 4d <sup>5</sup>	( <sup>4</sup> G) <sup>3</sup> G <sub>3</sub>	635,050
171.539		582,957	383 IX	2207	<sup>3</sup> F <sub>4</sub> 1	60,981	4p <sup>5</sup> 4d <sup>5</sup>	( <sup>2</sup> H) <sup>1</sup> G <sub>4</sub>	643,939
171.587	0.003	582,795	27	211	<sup>1</sup> F <sub>3</sub>	52,004	4p <sup>5</sup> 4d <sup>5</sup>	( <sup>4</sup> G) <sup>3</sup> G <sub>4</sub>	634,810
171.748	0.004	582,247	20	574	<sup>3</sup> D <sub>2</sub>	38,403	4p <sup>5</sup> 4d <sup>5</sup>	( <sup>4</sup> G) <sup>3</sup> F <sub>2</sub>	620,664
171.960	-0.002	581,530	267	6420	<sup>1</sup> I <sub>6</sub>	39,744	4p <sup>5</sup> 4d <sup>5</sup>	( <sup>2</sup> I) <sup>1</sup> I <sub>6</sub>	621,268
172.171	-0.001	580,818	66	606	<sup>5</sup> D <sub>1</sub>	1,340	4p <sup>5</sup> 4d <sup>5</sup>	( <sup>6</sup> S) <sup>5</sup> P <sub>1</sub>	582,154
172.215	0.000	580,671	787	2558	<sup>1</sup> G <sub>4</sub> 1	69,585	4p <sup>5</sup> 4d <sup>5</sup>	( <sup>4</sup> F) <sup>3</sup> F <sub>4</sub>	650,256
172.372	-0.006	580,140	61	1512	<sup>1</sup> D <sub>2</sub> 1	88,587	4p <sup>5</sup> 4d <sup>5</sup>	( <sup>2</sup> G) <sup>1</sup> F <sub>3</sub>	668,708
172.460		579,846	71	1498	<sup>3</sup> F <sub>2</sub> 1	61,645	4p <sup>5</sup> 4d <sup>5</sup>	( <sup>4</sup> F) <sup>3</sup> F <sub>2</sub>	641,516
172.730	0.001	578,937	92	549	<sup>5</sup> D <sub>2</sub>	3,212	4p <sup>5</sup> 4d <sup>5</sup>	( <sup>6</sup> S) <sup>5</sup> P <sub>1</sub>	582,154
172.968	-0.002	578,143	20	1138	<sup>3</sup> H <sub>5</sub>	26,249	4p <sup>5</sup> 4d <sup>5</sup>	( <sup>2</sup> G) <sup>1</sup> G <sub>4</sub>	604,385
173.327	0.000	576,943	295	5775	<sup>3</sup> H <sub>6</sub>	28,185	4p <sup>5</sup> 4d <sup>5</sup>	( <sup>2</sup> I) <sup>3</sup> H <sub>6</sub>	605,128
173.525	0.000	576,287	28	323	<sup>3</sup> D <sub>3</sub>	36,878	4p <sup>5</sup> 4d <sup>5</sup>	( <sup>4</sup> G) <sup>3</sup> F <sub>4</sub>	613,166
173.682	0.003	575,766	45	1187	<sup>1</sup> F <sub>3</sub>	52,004	4p <sup>5</sup> 4d <sup>5</sup>	( <sup>4</sup> P) <sup>3</sup> D <sub>3</sub>	627,779



Table A3. Cont.

$\lambda, \text{\AA}^a$	o-c, (Å) <sup>b</sup>	$\nu$ (cm <sup>-1</sup> )	I <sup>c</sup>	gA, (10 <sup>9</sup> s <sup>-1</sup> )	4d <sup>4</sup>		(4d <sup>3</sup> 4f + 4p <sup>5</sup> 4d <sup>5</sup> )		
					Term <sup>e</sup>	E (cm <sup>-1</sup> )	Config. <sup>f</sup>	Term <sup>f</sup>	E (cm <sup>-1</sup> )
182.354	-0.001	548,384	65	1175	<sup>3</sup> F <sub>3/2</sub>	32,925	4p <sup>5</sup> 4d <sup>5</sup>	( <sup>2</sup> G <sub>2</sub> ) <sup>3</sup> G <sub>4</sub>	581,306
182.749	-0.003	547,199	145	2520	<sup>3</sup> F <sub>4/2</sub>	29,555	4d <sup>3</sup> 4f	( <sup>4</sup> F) <sup>3</sup> H <sub>5</sub>	576,746
183.131	0.004	546,058	234	3198	<sup>3</sup> G <sub>3</sub>	26,968	4d <sup>3</sup> 4f	( <sup>4</sup> F) <sup>3</sup> H <sub>4</sub>	573,036
183.202	0.000	545,845	355	4991	<sup>3</sup> G <sub>5</sub>	35,078	4d <sup>3</sup> 4f	( <sup>4</sup> F) <sup>3</sup> H <sub>6</sub>	580,923
183.421	0.002	545,194	27	454	<sup>3</sup> D <sub>2</sub>	38,403	4p <sup>5</sup> 4d <sup>5</sup>	( <sup>2</sup> G <sub>1</sub> ) <sup>3</sup> F <sub>3</sub>	583,603
183.482	0.001	545,014	260	2889	<sup>3</sup> H <sub>4</sub>	23,304	4d <sup>3</sup> 4f	( <sup>4</sup> F) <sup>3</sup> I <sub>5</sub>	568,319
183.503	0.000	544,949	62	115	<sup>3</sup> P <sub>2/2</sub>	32,137	4p <sup>5</sup> 4d <sup>5</sup>	( <sup>2</sup> H) <sup>3</sup> G <sub>3</sub>	577,085
183.556	-0.003	544,792	30	721	<sup>1</sup> G <sub>4/1</sub>	69,585	4p <sup>5</sup> 4d <sup>5</sup>	( <sup>2</sup> G <sub>1</sub> ) <sup>1</sup> H <sub>5</sub>	614,370
183.685	0.006	544,411	41	801	<sup>3</sup> D <sub>3</sub>	36,878	4p <sup>5</sup> 4d <sup>5</sup>	( <sup>2</sup> G <sub>2</sub> ) <sup>3</sup> G <sub>4</sub>	581,306
183.808	0.001	544,047	76	1418	<sup>3</sup> G <sub>4</sub>	32,698	4d <sup>3</sup> 4f	( <sup>4</sup> F) <sup>3</sup> H <sub>5</sub>	576,746
184.001	0.002	543,474	24	288	<sup>3</sup> F <sub>4/2</sub>	29,555	4d <sup>3</sup> 4f	( <sup>4</sup> F) <sup>3</sup> H <sub>4</sub>	573,036
184.113	-0.003	543,144	594	6224	<sup>3</sup> H <sub>5</sub>	26,249	4d <sup>3</sup> 4f	( <sup>4</sup> F) <sup>3</sup> I <sub>6</sub>	569,385
184.456	-0.003	542,133	102	2095	<sup>3</sup> H <sub>4</sub>	23,304	4p <sup>5</sup> 4d <sup>5</sup>	( <sup>4</sup> G) <sup>3</sup> F <sub>5</sub>	565,427
184.481	0.003	542,061	29	403	<sup>3</sup> H <sub>5</sub>	26,249	4d <sup>3</sup> 4f	( <sup>4</sup> F) <sup>3</sup> I <sub>5</sub>	568,319
184.560	0.002	541,830	44	1623	<sup>3</sup> F <sub>3/1</sub>	62,552	4p <sup>5</sup> 4d <sup>5</sup>	( <sup>2</sup> G <sub>1</sub> ) <sup>3</sup> G <sub>4</sub>	604,385
184.620	0.005	541,655	32	545	<sup>3</sup> G <sub>5</sub>	35,078	4d <sup>3</sup> 4f	( <sup>4</sup> F)3H <sub>5</sub>	576,746
184.641	0.003	541,592	29	74	<sup>3</sup> H <sub>4</sub>	23,304	4p <sup>5</sup> 4d <sup>5</sup>	( <sup>4</sup> F)5D <sub>4</sub>	564,902
184.780d	0.006	541,184	34	264	<sup>3</sup> H <sub>6</sub>	28,185	4d <sup>3</sup> 4f	( <sup>4</sup> F)3I <sub>6</sub>	569,385
184.780d	-0.002	541,184	34	255	<sup>1</sup> I <sub>6</sub>	39,744	4d <sup>3</sup> 4f	( <sup>4</sup> F)3H <sub>6</sub>	580,923
185.452	-0.001	539,223	520	6429	<sup>1</sup> I <sub>6</sub>	39,744	4d <sup>3</sup> 4f	( <sup>2</sup> H)1K7	578,963
185.553		538,930	741	6779	<sup>3</sup> H <sub>6</sub>	28,185	4d <sup>3</sup> 4f	( <sup>2</sup> H)1K7	567,115
185.607	-0.003	538,773	62	536	<sup>3</sup> F <sub>4/2</sub>	29,555	4d <sup>3</sup> 4f	( <sup>4</sup> F)3I <sub>5</sub>	568,319
185.897	0.001	537,931	31	306	<sup>3</sup> G <sub>3</sub>	26,968	4p <sup>5</sup> 4d <sup>5</sup>	( <sup>4</sup> F)5D <sub>4</sub>	564,902
185.959	0.010	537,753	27	613	<sup>1</sup> F <sub>3</sub>	52,004	4p <sup>5</sup> 4d <sup>5</sup>	( <sup>2</sup> H)3G <sub>4</sub>	589,786
186.615	0.003	535,862	24	121	<sup>3</sup> F <sub>4/2</sub>	29,555	4p <sup>5</sup> 4d <sup>5</sup>	( <sup>4</sup> G)5F <sub>5</sub>	565,427
187.168		534,280	243	2386	<sup>1</sup> G <sub>4/1</sub>	69,585	4d <sup>3</sup> 4f	( <sup>2</sup> D)1H <sub>5</sub>	603,864
188.279	0.004	531,127	68	1100	<sup>3</sup> F <sub>4/1</sub>	60,981	4p <sup>5</sup> 4d <sup>5</sup>	( <sup>2</sup> H)1H <sub>5</sub>	592,118

<sup>a</sup> Observed wavelengths; d—doubly identified, w—wide; <sup>b</sup> Difference between the observed wavelength and the wavelength derived from the final level energies (Ritz wavelength). A blank value indicates that the upper level is derived only from that line; <sup>c</sup> Relative intensity; IX—line is also identified as Ag IX; <sup>e</sup> Numbers following the term values display Nielson and Koster sequential indices [20]; <sup>f</sup> Designation and configuration attribution is arbitrary in a few cases (see text), for the level composition, see Table A9. Numbers following the term values of the 4d<sup>5</sup> configuration display Nielson and Koster sequential indices [20].

Table A4. Identified lines of the 4d<sup>3</sup>–(4d<sup>2</sup>5p + 4d<sup>2</sup>4f + 4p<sup>5</sup>4d<sup>4</sup>) transitions in the spectrum of Ag<sup>8+</sup>.

$\lambda, \text{\AA}^a$	o-c, (Å) <sup>b</sup>	$\nu$ (cm <sup>-1</sup> )	I <sup>c</sup>	gA, (10 <sup>9</sup> s <sup>-1</sup> )	4d <sup>3</sup>		4d <sup>2</sup> 5p + 4d <sup>2</sup> 4f + 4p <sup>5</sup> 4d <sup>4</sup>	
					Term <sup>e</sup>	Config. <sup>f</sup>	Term <sup>f</sup>	E (cm <sup>-1</sup> )
160.837	0.005	621,749	100 X	1092	<sup>4</sup> F <sub>7/2</sub>	4p <sup>5</sup> 4d <sup>4</sup>	( <sup>5</sup> D) <sup>4</sup> D <sub>5/2</sub>	628,302
161.466	-0.005	619,327	50	3141	<sup>4</sup> F <sub>9/2</sub>	4p <sup>5</sup> 4d <sup>4</sup>	( <sup>5</sup> D) <sup>4</sup> D <sub>7/2</sub>	629,173
162.302		616,135	250 X	1091	<sup>2</sup> D <sub>5/2,2</sub>	4p <sup>5</sup> 4d <sup>4</sup>	( <sup>3</sup> P) <sup>1</sup> 2P <sub>3/2</sub>	649,186
162.411	-0.002	615,723	190	1327	<sup>2</sup> F <sub>7/2</sub>	4p <sup>5</sup> 4d <sup>4</sup>	( <sup>1</sup> G) <sup>1</sup> 2F <sub>7/2</sub>	659,798
162.500		615,383	130	645	<sup>4</sup> F <sub>3/2</sub>	4p <sup>5</sup> 4d <sup>4</sup>	( <sup>5</sup> D) <sup>4</sup> D <sub>1/2</sub>	615,385
162.644	0.002	614,839	540	2516	<sup>2</sup> H <sub>9/2</sub>	4p <sup>5</sup> 4d <sup>4</sup>	( <sup>3</sup> H) <sup>2</sup> G <sub>7/2</sub>	647,197
163.010	-0.003	613,458	370	4684	<sup>2</sup> H <sub>11/2</sub>	4p <sup>5</sup> 4d <sup>4</sup>	( <sup>3</sup> H) <sup>2</sup> G <sub>9/2</sub>	644,980
163.132	0.003	613,001	90	1863	<sup>2</sup> F <sub>5/2</sub>	4p <sup>5</sup> 4d <sup>4</sup>	( <sup>3</sup> G) <sup>2</sup> F <sub>5/2</sub>	657,606
163.228	-0.003	612,641	80	464	<sup>2</sup> H <sub>9/2</sub>	4p <sup>5</sup> 4d <sup>4</sup>	( <sup>3</sup> H) <sup>2</sup> G <sub>9/2</sub>	644,980
163.267	0.001	612,494	70	577	<sup>2</sup> G <sub>7/2</sub>	4p <sup>5</sup> 4d <sup>4</sup>	( <sup>3</sup> F) <sup>2</sup> F <sub>7/2</sub>	634,657
163.416	0.003	611,937	180	356	<sup>2</sup> D <sub>5/2,1</sub>	4p <sup>5</sup> 4d <sup>4</sup>	( <sup>3</sup> F) <sup>1</sup> 2D <sub>3/2</sub>	680,196
163.532	-0.004	611,503	220	2272	<sup>2</sup> D <sub>3/2,1</sub>	4p <sup>5</sup> 4d <sup>4</sup>	( <sup>3</sup> F) <sup>1</sup> 2D <sub>3/2</sub>	680,196
163.589	0.004	611,287	110 X	1237	<sup>2</sup> G <sub>9/2</sub>	4p <sup>5</sup> 4d <sup>4</sup>	( <sup>3</sup> F) <sup>2</sup> F <sub>7/2</sub>	634,657
163.839		610,356	140	1254	<sup>2</sup> D <sub>3/2,2</sub>	4p <sup>5</sup> 4d <sup>4</sup>	( <sup>5</sup> D) <sup>4</sup> P <sub>1/2</sub>	637,178
163.949	-0.003	609,947	400	1702	<sup>4</sup> P <sub>5/2</sub>	4p <sup>5</sup> 4d <sup>4</sup>	( <sup>5</sup> D) <sup>4</sup> P <sub>5/2</sub>	632,322
164.099		609,387	110	668	<sup>4</sup> F <sub>5/2</sub>	4p <sup>5</sup> 4d <sup>4</sup>	( <sup>5</sup> D) <sup>4</sup> D <sub>3/2</sub>	612,491
164.397		608,284	310	2866	<sup>2</sup> D <sub>5/2,1</sub>	4p <sup>5</sup> 4d <sup>4</sup>	( <sup>3</sup> F) <sup>1</sup> 2D <sub>5/2</sub>	676,533
164.493		607,930	80	578	<sup>4</sup> P <sub>5/2</sub>	4p <sup>5</sup> 4d <sup>4</sup>	( <sup>5</sup> D) <sup>4</sup> P <sub>3/2</sub>	630,316
164.542d	0.013	607,749	740 VIII	1677	<sup>2</sup> F <sub>7/2</sub>	4p <sup>5</sup> 4d <sup>4</sup>	( <sup>3</sup> P) <sup>2</sup> D <sub>5/2</sub>	651,880
164.542d	-0.005	607,749	740	7777	<sup>2</sup> H <sub>11/2</sub>	4p <sup>5</sup> 4d <sup>4</sup>	( <sup>3</sup> H) <sup>2</sup> H <sub>11/2</sub>	639,262
164.772	0.004	606,900	170	576	<sup>2</sup> H <sub>9/2</sub>	4p <sup>5</sup> 4d <sup>4</sup>	( <sup>3</sup> H) <sup>2</sup> H <sub>11/2</sub>	639,262

Table A4. Cont.

$\lambda, \text{\AA}^a$	o-c, (Å) <sup>b</sup>	$\nu$ (cm <sup>-1</sup> )	I <sup>c</sup>	gA, (10 <sup>9</sup> s <sup>-1</sup> )	4d <sup>3</sup> 4d <sup>2</sup> 5p + 4d <sup>2</sup> 4f + 4p <sup>5</sup> 4d <sup>4</sup>			
					Term <sup>e</sup>	Config. <sup>f</sup>	Term <sup>f</sup>	E (cm <sup>-1</sup> )
164.808	0.005	606,766	370 X	1781	<sup>4</sup> P <sub>5/2</sub>	4p <sup>5</sup> 4d <sup>4</sup>	( <sup>5</sup> D) <sup>4</sup> D <sub>7/2</sub>	629,173
164.952	-0.000	606,239	70	725	<sup>4</sup> F <sub>7/2</sub>	4p <sup>5</sup> 4d <sup>4</sup>	( <sup>5</sup> D) <sup>4</sup> D <sub>5/2</sub>	612,769
165.036	-0.003	605,927	170	831	<sup>4</sup> P <sub>5/2</sub>	4p <sup>5</sup> 4d <sup>4</sup>	( <sup>5</sup> D) <sup>4</sup> D <sub>5/2</sub>	628,302
165.418	0.001	604,531	100	1245	<sup>2</sup> G <sub>7/2</sub>	4p <sup>5</sup> 4d <sup>4</sup>	( <sup>1</sup> D1) <sup>2</sup> F <sub>5/2</sub>	626,693
165.945	-0.002	602,610	90	1679	<sup>2</sup> F <sub>5/2</sub>	4p <sup>5</sup> 4d <sup>4</sup>	( <sup>3</sup> H) <sup>2</sup> G <sub>7/2</sub>	647,197
165.999	0.003	602,412	510 X	1403	<sup>2</sup> P <sub>3/2</sub>	4p <sup>5</sup> 4d <sup>4</sup>	( <sup>3</sup> P2) <sup>2</sup> P <sub>3/2</sub>	638,784
166.023	-0.005	602,325	200	1348	<sup>2</sup> H <sub>9/2</sub>	4p <sup>5</sup> 4d <sup>4</sup>	( <sup>3</sup> F2) <sup>2</sup> F <sub>7/2</sub>	634,657
166.423	0.005	600,880	90	1650	<sup>2</sup> F <sub>7/2</sub>	4p <sup>5</sup> 4d <sup>4</sup>	( <sup>3</sup> H) <sup>2</sup> G <sub>9/2</sub>	644,980
166.518	-0.000	600,537	60	509	<sup>2</sup> H <sub>11/2</sub>	4p <sup>5</sup> 4d <sup>4</sup>	( <sup>3</sup> H) <sup>2</sup> H <sub>9/2</sub>	632,069
166.744	0.000	599,721	490 VIII	5298	<sup>2</sup> H <sub>9/2</sub>	4p <sup>5</sup> 4d <sup>4</sup>	( <sup>3</sup> H) <sup>2</sup> H <sub>9/2</sub>	632,069
166.872	0.002	599,262	50	862	<sup>2</sup> D <sub>5/2,2</sub>	4p <sup>5</sup> 4d <sup>4</sup>	( <sup>5</sup> D) <sup>4</sup> P <sub>5/2</sub>	632,322
167.307		597,704	620	5028	<sup>2</sup> G <sub>9/2</sub>	4p <sup>5</sup> 4d <sup>4</sup>	( <sup>1</sup> G2) <sup>2</sup> G <sub>9/2</sub>	621,061
167.460	-0.002	597,158	270 VIII	2912	<sup>2</sup> F <sub>7/2</sub>	4p <sup>5</sup> 4d <sup>4</sup>	( <sup>1</sup> G2) <sup>2</sup> F <sub>7/2</sub>	641,234
167.492	-0.001	597,042	100	883	<sup>4</sup> F <sub>7/2</sub>	4p <sup>5</sup> 4d <sup>4</sup>	( <sup>5</sup> D) <sup>4</sup> F <sub>9/2</sub>	603,570
167.814		595,896	120	1278	<sup>2</sup> G <sub>7/2</sub>	4p <sup>5</sup> 4d <sup>4</sup>	( <sup>3</sup> D) <sup>2</sup> F <sub>5/2</sub>	618,058
167.898	-0.000	595,601	170 X	1248	<sup>4</sup> P <sub>3/2</sub>	4p <sup>5</sup> 4d <sup>4</sup>	( <sup>5</sup> D) <sup>4</sup> D <sub>5/2</sub>	612,769
168.022	-0.004	595,162	160	1520	<sup>2</sup> D <sub>5/2,1</sub>	4p <sup>5</sup> 4d <sup>4</sup>	( <sup>3</sup> P1) <sup>2</sup> P <sub>3/2</sub>	663,396
168.130		594,778	40	964	<sup>4</sup> P <sub>1/2</sub>	4p <sup>5</sup> 4d <sup>4</sup>	( <sup>5</sup> D) <sup>4</sup> D <sub>3/2</sub>	612,491
168.159	0.004	594,677	30	322	<sup>2</sup> D <sub>3/2,1</sub>	4p <sup>5</sup> 4d <sup>4</sup>	( <sup>3</sup> P1) <sup>2</sup> P <sub>3/2</sub>	663,396
168.294	-0.002	594,197	90	469	<sup>2</sup> F <sub>5/2</sub>	4p <sup>5</sup> 4d <sup>4</sup>	( <sup>3</sup> P2) <sup>2</sup> P <sub>3/2</sub>	638,784
168.414	-0.001	593,775	90	707	<sup>4</sup> F <sub>5/2</sub>	4p <sup>5</sup> 4d <sup>4</sup>	( <sup>5</sup> D) <sup>4</sup> F <sub>7/2</sub>	596,876
168.436d	0.007	593,698	430 VIII	1955	<sup>2</sup> G <sub>7/2</sub>	4p <sup>5</sup> 4d <sup>4</sup>	( <sup>1</sup> G2) <sup>2</sup> G <sub>7/2</sub>	615,884
168.436d	0.001	593,698	430 VIII	3827	<sup>4</sup> F <sub>9/2</sub>	4p <sup>5</sup> 4d <sup>4</sup>	( <sup>5</sup> D) <sup>4</sup> F <sub>9/2</sub>	603,570
168.479	-0.002	593,545	110	909	<sup>2</sup> F <sub>5/2</sub>	4p <sup>5</sup> 4d <sup>4</sup>	( <sup>3</sup> F2) <sup>2</sup> F <sub>5/2</sub>	638,134
168.605	0.005	593,101	50	1153	<sup>2</sup> G <sub>9/2</sub>	4p <sup>5</sup> 4d <sup>4</sup>	( <sup>3</sup> F2) <sup>2</sup> G <sub>9/2</sub>	616,475
168.766	-0.003	592,537	80	1585	<sup>2</sup> G <sub>9/2</sub>	4p <sup>5</sup> 4d <sup>4</sup>	( <sup>1</sup> G2) <sup>2</sup> G <sub>7/2</sub>	615,884
168.808	0.002	592,389	110 X	759	<sup>4</sup> F <sub>7/2</sub>	4p <sup>5</sup> 4d <sup>4</sup>	( <sup>3</sup> F1) <sup>4</sup> D <sub>7/2</sub>	598,929
168.932d	-0.003	591,953	150 VIII	967	<sup>2</sup> P <sub>3/2</sub>	4p <sup>5</sup> 4d <sup>4</sup>	( <sup>5</sup> D) <sup>4</sup> D <sub>5/2</sub>	628,302
168.932d	-0.000	591,953	150 VIII	1267	<sup>2</sup> G <sub>9/2</sub>	4p <sup>5</sup> 4d <sup>4</sup>	( <sup>3</sup> H) <sup>2</sup> H <sub>11/2</sub>	615,308
169.049	0.002	591,543	140	3139	<sup>2</sup> D <sub>5/2,1</sub>	4p <sup>5</sup> 4d <sup>4</sup>	( <sup>1</sup> G1) <sup>2</sup> F <sub>7/2</sub>	659,798
169.392d	-0.004	590,346	270	1157	<sup>2</sup> P <sub>3/2</sub>	4p <sup>5</sup> 4d <sup>4</sup>	( <sup>1</sup> D1) <sup>2</sup> F <sub>5/2</sub>	626,693
169.392d	-0.001	590,346	270	2701	<sup>4</sup> F <sub>7/2</sub>	4p <sup>5</sup> 4d <sup>4</sup>	( <sup>5</sup> D) <sup>4</sup> F <sub>7/2</sub>	596,876
169.475	0.001	590,058	50 X	548	<sup>2</sup> F <sub>5/2</sub>	4p <sup>5</sup> 4d <sup>4</sup>	( <sup>3</sup> F2) <sup>2</sup> F <sub>7/2</sub>	634,657
169.595	0.001	589,642	50	428	<sup>4</sup> F <sub>3/2</sub>	4p <sup>5</sup> 4d <sup>4</sup>	( <sup>5</sup> D) <sup>4</sup> F <sub>5/2</sub>	589,644
169.613	0.000	589,578	100 VIII	765	<sup>4</sup> F <sub>9/2</sub>	4p <sup>5</sup> 4d <sup>4</sup>	( <sup>1</sup> I) <sup>2</sup> H <sub>9/2</sub>	599,446
169.762	0.000	589,062	50	787	<sup>4</sup> F <sub>9/2</sub>	4p <sup>5</sup> 4d <sup>4</sup>	( <sup>3</sup> F1) <sup>4</sup> D <sub>7/2</sub>	598,929
169.806	-0.002	588,907	20	1462	<sup>2</sup> D <sub>3/2,1</sub>	4p <sup>5</sup> 4d <sup>4</sup>	( <sup>3</sup> G) <sup>2</sup> F <sub>5/2</sub>	657,606
170.192	0.002	587,572	30	80	<sup>4</sup> F <sub>7/2</sub>	4p <sup>5</sup> 4d <sup>4</sup>	( <sup>1</sup> D1) <sup>2</sup> F <sub>5/2</sub>	594,111
170.306	-0.001	587,180	60	620	<sup>4</sup> F <sub>5/2</sub>	4d <sup>2</sup> 4f	( <sup>3</sup> P) <sup>4</sup> D <sub>3/2</sub>	590,280
170.359t	0.007	586,994	440 VIII	1882	<sup>4</sup> F <sub>9/2</sub>	4d <sup>2</sup> 4f	( <sup>3</sup> F) <sup>2</sup> I <sub>11/2</sub>	596,885
170.359t	0.004	586,994	440 VIII	769	<sup>4</sup> F <sub>9/2</sub>	4p <sup>5</sup> 4d <sup>4</sup>	( <sup>5</sup> D) <sup>4</sup> F <sub>7/2</sub>	596,876
170.359t	-0.001	586,994	440 VIII	1501	<sup>2</sup> G <sub>7/2</sub>	4p <sup>5</sup> 4d <sup>4</sup>	( <sup>3</sup> G) <sup>2</sup> G <sub>7/2</sub>	609,152
170.490	-0.001	586,545	280	2414	<sup>4</sup> F <sub>5/2</sub>	4p <sup>5</sup> 4d <sup>4</sup>	( <sup>5</sup> D) <sup>4</sup> F <sub>5/2</sub>	589,644
170.933		585,026	120	2598	<sup>2</sup> D <sub>5/2,2</sub>	4d <sup>2</sup> 4f	( <sup>3</sup> P) <sup>2</sup> F <sub>7/2</sub>	618,075
171.286		583,818	260	2018	<sup>4</sup> F <sub>3/2</sub>	4d <sup>2</sup> 4f	( <sup>3</sup> F) <sup>4</sup> F <sub>3/2</sub>	583,819
171.339	-0.002	583,638	60	848	<sup>2</sup> D <sub>5/2,1</sub>	4p <sup>5</sup> 4d <sup>4</sup>	( <sup>3</sup> P2) <sup>2</sup> D <sub>5/2</sub>	651,880
171.493	-0.000	583,114	40	409	<sup>4</sup> F <sub>7/2</sub>	4p <sup>5</sup> 4d <sup>4</sup>	( <sup>5</sup> D) <sup>4</sup> F <sub>5/2</sub>	589,644
171.539	0.001	582,957	530 VIII	5000	<sup>2</sup> H <sub>9/2</sub>	4p <sup>5</sup> 4d <sup>4</sup>	( <sup>3</sup> H) <sup>2</sup> H <sub>11/2</sub>	615,308
171.996	0.001	581,408	40	482	<sup>2</sup> G <sub>7/2</sub>	4p <sup>5</sup> 4d <sup>4</sup>	( <sup>5</sup> D) <sup>4</sup> F <sub>9/2</sub>	603,570
172.215d	-0.001	580,671	1100	4948	<sup>4</sup> F <sub>7/2</sub>	4p <sup>5</sup> 4d <sup>4</sup>	( <sup>3</sup> H) <sup>4</sup> G <sub>9/2,1</sub>	587,200
172.215d	-0.001	580,671	1100	3951	<sup>4</sup> F <sub>5/2</sub>	4d <sup>2</sup> 4f	( <sup>3</sup> F) <sup>4</sup> G <sub>7/2,1</sub>	583,771
172.372		580,140	90	1120	<sup>2</sup> D <sub>3/2,2</sub>	4d <sup>2</sup> 4f	( <sup>1</sup> D) <sup>2</sup> D <sub>3/2</sub>	606,963
172.556	-0.005	579,521	390	3149	<sup>4</sup> F <sub>3/2</sub>	4d <sup>2</sup> 4f	( <sup>3</sup> F) <sup>4</sup> G <sub>5/2</sub>	579,505
173.077	-0.001	577,778	890	5063	<sup>4</sup> F <sub>9/2</sub>	4p <sup>5</sup> 4d <sup>4</sup>	( <sup>3</sup> H) <sup>4</sup> G <sub>11/2</sub>	587,642
173.224d	0.014	577,288	670	765	<sup>4</sup> F <sub>9/2</sub>	4p <sup>5</sup> 4d <sup>4</sup>	( <sup>3</sup> H) <sup>4</sup> G <sub>9/2</sub>	587,200
173.224d	-0.000	577,288	670	4944	<sup>2</sup> G <sub>7/2</sub>	4p <sup>5</sup> 4d <sup>4</sup>	( <sup>1</sup> I) <sup>2</sup> H <sub>9/2</sub>	599,446
173.236	-0.002	577,246	380	932	<sup>4</sup> F <sub>7/2</sub>	4d <sup>2</sup> 4f	( <sup>3</sup> F) <sup>4</sup> G <sub>7/2</sub>	583,771
173.445	-0.003	576,551	150	1869	<sup>4</sup> P <sub>5/2</sub>	4p <sup>5</sup> 4d <sup>4</sup>	( <sup>3</sup> F1) <sup>4</sup> D <sub>7/2</sub>	598,929
173.495	0.005	576,386	60	528	<sup>4</sup> F <sub>5/2</sub>	4d <sup>2</sup> 4f	( <sup>3</sup> F) <sup>4</sup> G <sub>5/2</sub>	579,505
173.578	-0.003	576,110	110	1309	<sup>2</sup> D <sub>5/2,2</sub>	4p <sup>5</sup> 4d <sup>4</sup>	( <sup>3</sup> G) <sup>2</sup> G <sub>7/2</sub>	609,152

Table A4. Cont.

$\lambda, \text{\AA}^a$	o-c, (Å) <sup>b</sup>	$\nu$ (cm <sup>-1</sup> )	I <sup>c</sup>	gA, (10 <sup>9</sup> s <sup>-1</sup> )	4d <sup>3</sup> 4d <sup>2</sup> 5p + 4d <sup>2</sup> 4f + 4p <sup>5</sup> 4d <sup>4</sup>			
					Term <sup>e</sup>	Config. <sup>f</sup>	Term <sup>g</sup>	E (cm <sup>-1</sup> )
174.248	0.003	573,895	30	20	<sup>4</sup> F <sub>9/2</sub>	4d <sup>2</sup> 4f	( <sup>3</sup> F) <sup>4</sup> G <sub>7/2</sub>	583,771
174.357	-0.002	573,535	360 VIII	3568	<sup>2</sup> G <sub>9/2</sub>	4d <sup>2</sup> 4f	( <sup>3</sup> F) <sup>4</sup> I <sub>11/2</sub>	596,885
174.487	0.000	573,110	140	1302	<sup>4</sup> P <sub>3/2</sub>	4d <sup>2</sup> 4f	( <sup>3</sup> P) <sup>4</sup> D <sub>3/2</sub>	590,280
174.526	0.002	572,979	40	690	<sup>2</sup> D <sub>5/2,1</sub>	4p <sup>5</sup> 4d <sup>4</sup>	( <sup>1</sup> G) <sup>2</sup> F <sub>7/2</sub>	641,234
174.618		572,678	100 VIII	1088	<sup>4</sup> P <sub>5/2</sub>	4p <sup>5</sup> 4d <sup>4</sup>	( <sup>3</sup> P) <sup>4</sup> S <sub>3/2</sub>	595,066
174.701	-0.004	572,407	340	2551	<sup>2</sup> F <sub>7/2</sub>	4p <sup>5</sup> 4d <sup>4</sup>	( <sup>3</sup> F) <sup>2</sup> G <sub>9/2</sub>	616,475
174.908	-0.002	571,730	60	94	<sup>4</sup> P <sub>5/2</sub>	4p <sup>5</sup> 4d <sup>4</sup>	( <sup>1</sup> D) <sup>1</sup> F <sub>5/2</sub>	594,111
175.617	0.001	569,422	30	1317	<sup>2</sup> D <sub>3/2,1</sub>	4p <sup>5</sup> 4d <sup>4</sup>	( <sup>3</sup> F) <sup>2</sup> F <sub>5/2</sub>	638,134
175.738		569,029	940	7991	<sup>2</sup> H <sub>11/1</sub>	4d <sup>2</sup> 4f	( <sup>3</sup> F) <sup>2</sup> I <sub>13/2</sub>	600,561
176.977	-0.001	565,044	40	328	<sup>2</sup> G <sub>7/2</sub>	4p <sup>5</sup> 4d <sup>4</sup>	( <sup>3</sup> H) <sup>4</sup> G <sub>9/2</sub>	587,200
177.136d	0.006	564,539	100	1114	<sup>2</sup> F <sub>5/2</sub>	4p <sup>5</sup> 4d <sup>4</sup>	( <sup>3</sup> G) <sup>2</sup> G <sub>7/2</sub>	609,152
177.216d	0.000	564,283	360	2077	<sup>2</sup> G <sub>9/2</sub>	4p <sup>5</sup> 4d <sup>4</sup>	( <sup>3</sup> H) <sup>4</sup> G <sub>11/2</sub>	587,642
221.880	-0.001	450,694	80	22	<sup>4</sup> F <sub>9/2</sub>	4d <sup>2</sup> 5p	( <sup>3</sup> P) <sup>4</sup> D <sub>7/2</sub>	460,559
223.061	0.001	448,307	40	12	<sup>2</sup> G <sub>9/2</sub>	4d <sup>2</sup> 5p	( <sup>1</sup> G) <sup>2</sup> H <sub>11/2</sub>	471,667
226.030	0.003	442,420	120	17	<sup>4</sup> F <sub>9/2</sub>	4d <sup>2</sup> 5p	( <sup>1</sup> G) <sup>2</sup> G <sub>9/2</sub>	452,292
226.226	0.000	442,036	60	15	<sup>2</sup> G <sub>9/2</sub>	4d <sup>2</sup> 5p	( <sup>3</sup> P) <sup>4</sup> D <sub>7/2</sub>	465,394
227.202	-0.001	440,137	700	144	<sup>2</sup> H <sub>11/1,2</sub>	4d <sup>2</sup> 5p	( <sup>1</sup> G) <sup>2</sup> H <sub>11/2</sub>	471,667
227.723	-0.004	439,130	400	81	<sup>4</sup> F <sub>9/2</sub>	4d <sup>2</sup> 5p	( <sup>3</sup> F) <sup>2</sup> F <sub>7/2</sub>	448,989
228.487		437,662	320	67	<sup>4</sup> F <sub>3/2</sub>	4d <sup>2</sup> 5p	( <sup>3</sup> F) <sup>4</sup> D <sub>1/2</sub>	437,662
228.963	0.004	436,751	140	45	<sup>4</sup> P <sub>5/2</sub>	4d <sup>2</sup> 5p	( <sup>3</sup> P) <sup>4</sup> F <sub>3/2</sub>	459,146
229.415		435,891	520	172	<sup>4</sup> F <sub>7/2</sub>	4d <sup>2</sup> 5p	( <sup>3</sup> F) <sup>4</sup> D <sub>5/2</sub>	442,423
229.557		435,621	400	91	<sup>4</sup> F <sub>5/2</sub>	4d <sup>2</sup> 5p	( <sup>3</sup> F) <sup>4</sup> D <sub>3/2</sub>	438,725
229.783	0.001	435,193	340	36	<sup>4</sup> F <sub>5/2</sub>	4d <sup>2</sup> 5p	( <sup>3</sup> F) <sup>4</sup> F <sub>5/2</sub>	438,297
229.820		435,124	200	32	<sup>2</sup> F <sub>5/2</sub>	4d <sup>2</sup> 5p	( <sup>1</sup> G) <sup>2</sup> F <sub>5/2</sub>	479,718
229.877		435,015	100	20	<sup>2</sup> F <sub>5/2</sub>	4d <sup>2</sup> 5p	( <sup>1</sup> G) <sup>2</sup> F <sub>5/2</sub>	479,718
230.176	0.004	434,450	230	61	<sup>2</sup> H <sub>11/1,2</sub>	4d <sup>2</sup> 5p	( <sup>1</sup> G) <sup>2</sup> H <sub>9/2</sub>	465,990
230.241		434,328	630	157	<sup>4</sup> F <sub>9/2</sub>	4d <sup>2</sup> 5p	( <sup>3</sup> F) <sup>4</sup> F <sub>9/2</sub>	444,195
230.601	-0.005	433,650	350	113	<sup>2</sup> H <sub>9/2</sub>	4d <sup>2</sup> 5p	( <sup>1</sup> G) <sup>2</sup> H <sub>9/2</sub>	465,990
230.922	-0.001	433,047	500	89	<sup>2</sup> H <sub>9/2</sub>	4d <sup>2</sup> 5p	( <sup>3</sup> P) <sup>4</sup> D <sub>7/2</sub>	465,394
231.179	0.002	432,565	150	16	<sup>4</sup> F <sub>3/2</sub>	4d <sup>2</sup> 5p	( <sup>3</sup> F) <sup>4</sup> F <sub>5/2</sub>	432,569
231.545		431,882	620	106	<sup>2</sup> H <sub>9/2</sub>	4d <sup>2</sup> 5p	( <sup>1</sup> D) <sup>2</sup> F <sub>7/2</sub>	464,230
231.602d	-0.005	431,774	580	19	<sup>4</sup> F <sub>7/2</sub>	4d <sup>2</sup> 5p	( <sup>3</sup> F) <sup>4</sup> F <sub>5/2</sub>	438,297
231.602d	-0.002	431,774	580	149	<sup>4</sup> F <sub>9/2</sub>	4d <sup>2</sup> 5p	( <sup>3</sup> F) <sup>4</sup> D <sub>7/2</sub>	441,637
231.819		431,370	300	32	<sup>2</sup> F <sub>7/2</sub>	4p <sup>5</sup> 4d <sup>4</sup>	( <sup>3</sup> G) <sup>4</sup> G <sub>7/2</sub>	475,453
231.946	-0.003	431,135	450	154	<sup>4</sup> F <sub>7/2</sub>	4d <sup>2</sup> 5p	( <sup>3</sup> F) <sup>4</sup> F <sub>7/2</sub>	437,662
232.127		430,799	130	13	<sup>2</sup> D <sub>3/2,2</sub>	4d <sup>2</sup> 5p	( <sup>3</sup> P) <sup>4</sup> D <sub>5/2</sub>	457,621
232.259	-0.005	430,554	410	251	<sup>2</sup> G <sub>9/2</sub>	4d <sup>2</sup> 5p	( <sup>1</sup> G) <sup>2</sup> G <sub>7/2</sub>	453,902
232.337		430,410	330	159	<sup>2</sup> G <sub>7/2</sub>	4d <sup>2</sup> 5p	( <sup>1</sup> D) <sup>2</sup> F <sub>5/2</sub>	452,569
232.845	-0.002	429,470	550	102	<sup>4</sup> F <sub>5/2</sub>	4d <sup>2</sup> 5p	( <sup>3</sup> F) <sup>4</sup> F <sub>5/2</sub>	432,569
233.133	-0.003	428,940	450	89	<sup>2</sup> G <sub>9/2</sub>	4d <sup>2</sup> 5p	( <sup>1</sup> G) <sup>2</sup> G <sub>9/2</sub>	452,292
233.206	-0.005	428,806	50	16	<sup>4</sup> P <sub>5/2</sub>	4d <sup>2</sup> 5p	( <sup>3</sup> P) <sup>4</sup> S <sub>3/2</sub>	451,183
233.531	0.000	428,209	750 m	103	<sup>2</sup> H <sub>9/2</sub>	4d <sup>2</sup> 5p	( <sup>3</sup> P) <sup>4</sup> D <sub>7/2</sub>	460,559
233.691		427,915	310	91	<sup>4</sup> F <sub>3/2</sub>	4d <sup>2</sup> 5p	( <sup>3</sup> F) <sup>4</sup> F <sub>3/2</sub>	427,916
233.759	0.003	427,790	300	17	<sup>4</sup> F <sub>9/2</sub>	4d <sup>2</sup> 5p	( <sup>3</sup> F) <sup>4</sup> F <sub>7/2</sub>	437,662
233.877		427,576	170	64	<sup>4</sup> F <sub>9/2</sub>	4d <sup>2</sup> 5p	( <sup>3</sup> F) <sup>4</sup> G <sub>9/2</sub>	437,442
234.539		426,368	1000	424	<sup>2</sup> H <sub>11/1,2</sub>	4d <sup>2</sup> 5p	( <sup>3</sup> F) <sup>2</sup> G <sub>9/2</sub>	457,900
234.686	-0.003	426,101	150	22	<sup>2</sup> D <sub>5/2,2</sub>	4d <sup>2</sup> 5p	( <sup>3</sup> P) <sup>4</sup> F <sub>3/2</sub>	459,146
234.945	0.001	425,631	350	36	<sup>2</sup> G <sub>9/2</sub>	4d <sup>2</sup> 5p	( <sup>3</sup> F) <sup>2</sup> F <sub>7/2</sub>	448,989
235.240	-0.002	425,098	360	88	<sup>2</sup> G <sub>7/2</sub>	4d <sup>2</sup> 5p	( <sup>3</sup> F) <sup>2</sup> G <sub>7/2</sub>	447,255
235.532d		424,570	200	19	<sup>4</sup> F <sub>3/2</sub>	4d <sup>2</sup> 5p	( <sup>3</sup> F) <sup>4</sup> G <sub>5/2</sub>	424,571
235.532d		424,570	200	17	<sup>2</sup> D <sub>5/2,2</sub>	4d <sup>2</sup> 5p	( <sup>3</sup> P) <sup>4</sup> D <sub>5/2</sub>	457,621
235.581		424,482	190	51	<sup>2</sup> G <sub>7/2</sub>	4d <sup>2</sup> 5p	( <sup>3</sup> P) <sup>4</sup> F <sub>5/2</sub>	446,642
235.649		424,360	200	71	<sup>2</sup> D <sub>3/2,2</sub>	4d <sup>2</sup> 5p	( <sup>3</sup> P) <sup>4</sup> S <sub>3/2</sub>	451,183
235.726		424,222	230	101	<sup>2</sup> F <sub>5/2</sub>	4d <sup>2</sup> 5p	( <sup>3</sup> P) <sup>2</sup> D <sub>3/2</sub>	468,817
235.907	0.002	423,895	100	21	<sup>2</sup> G <sub>9/2</sub>	4d <sup>2</sup> 5p	( <sup>3</sup> F) <sup>2</sup> G <sub>7/2</sub>	447,255
236.756		422,376	110	32	<sup>2</sup> F <sub>7/2</sub>	4d <sup>2</sup> 5p	( <sup>1</sup> D) <sup>2</sup> D <sub>5/2</sub>	466,458
237.222	0.004	421,546	70	33	<sup>2</sup> H <sub>9/2</sub>	4d <sup>2</sup> 5p	( <sup>1</sup> G) <sup>2</sup> G <sub>7/2</sub>	453,902

Table A4. Cont.

$\lambda, \text{\AA}^a$	$\text{o-c}, (\text{\AA})^b$	$\nu (\text{cm}^{-1})$	$I^c$	$gA, (10^9 \text{ s}^{-1})$	$4d^3$ $4d^25p + 4d^24f + 4p^54d^4$			
					Term <sup>e</sup>	Config. <sup>f</sup>	Term <sup>f</sup>	E (cm <sup>-1</sup> )
237.458	0.001	421,127	80	15	$4P_{3/2}$	$4d^25p$	$(^3F)^4F_{5/2}$	438,297
239.077	0.003	418,275	160	34	$2G_{9/2}$	$4d^25p$	$(^3F)^4D_{7/2}$	441,637
239.161	0.002	418,129	60	19	$2D_{5/2,2}$	$4d^25p$	$(^3P)^4S_{3/2}$	451,183
240.423	0.002	415,934	160	32	$2D_{5/2,2}$	$4d^25p$	$(^3F)^2F_{7/2}$	448,989
243.734	-0.001	410,284	160	30	$2P_{3/2}$	$4d^25p$	$(^3F)^2F_{5/2}$	446,642

<sup>a</sup> Observed wavelengths; d—doubly identified, t—trebly identified; <sup>b</sup> Difference between the observed wavelength and the wavelength derived from the final level energies (Ritz wavelength). A blank value indicates that the upper level is derived only from that line; <sup>c</sup> Relative intensity: X, VIII—line is also identified as respectively Ag X or Ag VIII; m masked by O IV; <sup>e</sup> Numbers following the term values display Nielson and Koster sequential indices [20]; <sup>f</sup> Designation and configuration attribution is arbitrary in a few cases (see text), for the level composition, see Table A11. Numbers following the term values of the  $4d^4$  configuration display Nielson and Koster sequential indices [20].

Table A5. Energies (in cm<sup>-1</sup>) of the  $4d^5$  configuration of Ag VII.

E <sup>a</sup>	$\text{o-c}^b$	Eigenvector Composition <sup>c</sup>		
$J = 1/2$				
94,730 *		98% $3^2P$	2% $5^2S$	
63,467 *		96% $5^2S$	2% $3^4P$	2% $3^2P$
38,685	6	67% $5^4D$	32% $3^4P$	1% $5^2S$
34,605	-20	66% $3^4P$	33% $5^4D$	1% $5^2S$
$J = 3/2$				
104,821	-27	74% $1^2D$	18% $5^2D$	6% $3^2P$
93,529 *		94% $3^2P$	4% $1^2D$	1% $5^2D$
71,517	-2	97% $3^2D$	2% $1^2D$	1% $5^4D$
53,796	0	55% $3^4F$	37% $5^2D$	6% $1^2D$
48,086	2	42% $5^2D$	43% $3^4F$	13% $1^2D$
39,788	-1	52% $5^4D$	44% $3^4P$	1% $3^4F$
32,994	-4	53% $3^4P$	44% $5^4D$	1% $3^4F$
$J = 5/2$				
103,996	34	80% $1^2D$	19% $5^2D$	1% $3^2D$
72,934	-26	91% $3^2D$	6% $5^2F$	2% $5^4D$
59,954	-5	30% $3^2F$	29% $5^2F$	19% $5^2D$
57,413	2	53% $5^2F$	18% $3^2F$	17% $5^2D$
51,049	11	74% $3^4F$	12% $3^2F$	8% $5^2F$
47,119	2	31% $5^2D$	32% $3^2F$	13% $3^4P$
39,299	10	54% $5^4D$	32% $3^4P$	7% $5^2D$
32,005	-19	44% $3^4P$	35% $5^4D$	13% $5^4G$
29,390	27	79% $5^4G$	8% $3^2F$	4% $3^4P$
0	4	98% $5^6S$	2% $3^4P$	
$J = 7/2$				
79,705	4	96% $3^2G$	2% $5^2F$	1% $5^2G$
59,792	11	75% $5^2F$	15% $3^4F$	6% $3^2F$
55,773	8	74% $5^2G$	17% $3^2F$	8% $5^2F$
53,353	2	47% $3^2F$	34% $3^4F$	8% $5^2G$
48,712	10	45% $3^4F$	26% $3^2F$	15% $5^2G$
36,485	9	92% $5^4D$	4% $3^4F$	3% $5^4G$
30,378	0	93% $5^4G$	3% $3^2F$	2% $3^4F$



Table A5. Cont.

E <sup>a</sup>	o-c <sup>b</sup>	Eigenvector Composition <sup>c</sup>		
<i>J</i> = 9/2				
79,131	−13	99% 3 <sup>2</sup> G	1% 5 <sup>2</sup> G	
59,223	2	47% 5 <sup>2</sup> G	42% 3 <sup>2</sup> H	10% 3 <sup>4</sup> F
53,797	−11	52% 3 <sup>2</sup> H	30% 3 <sup>4</sup> F	18% 5 <sup>2</sup> G
49,104	−11	59% 3 <sup>4</sup> F	34% 5 <sup>2</sup> G	6% 3 <sup>2</sup> H
30,907	−2	97% 5 <sup>4</sup> G	1% 3 <sup>4</sup> F	1% 3 <sup>2</sup> H
<i>J</i> = 11/2				
57,962	2	86% 3 <sup>2</sup> H	11% 5 <sup>2</sup> I	2% 5 <sup>4</sup> G
44,011	1	88% 5 <sup>2</sup> I	10% 3 <sup>2</sup> H	1% 5 <sup>4</sup> G
30,662	−14	96% 5 <sup>4</sup> G	3% 3 <sup>2</sup> H	
<i>J</i> = 13/2				
45,546	3	100% 5 <sup>2</sup> I		

<sup>a</sup> The star \* indicates a calculated value for the level; <sup>b</sup> The difference between the observed and the calculated energies; <sup>c</sup> For the eigenvector composition, up to three components with the largest percentages in the LS-coupling scheme are listed. The number preceding the terms is the seniority number.

Table A6. Energies (in cm<sup>−1</sup>) of the 4d<sup>4</sup>5p configuration of Ag VII.

E <sup>a</sup>	o-c <sup>b</sup>	Eigenvector Composition <sup>c</sup>		
<i>J</i> = 1/2				
448,199 *		68% (0 <sup>1</sup> S) <sup>2</sup> P	15% (1 <sup>1</sup> S) <sup>2</sup> P	14% (2 <sup>1</sup> D) <sup>2</sup> P
419,718 *		64% (2 <sup>1</sup> D) <sup>2</sup> P	12% (0 <sup>1</sup> S) <sup>2</sup> P	11% (1 <sup>1</sup> D) <sup>2</sup> P
409,158 *		47% (3 <sup>1</sup> P) <sup>2</sup> S	27% (3 <sup>1</sup> P) <sup>2</sup> S	12% (2 <sup>3</sup> P) <sup>2</sup> P
406,673	37	39% (2 <sup>3</sup> F) <sup>4</sup> D	20% (3 <sup>1</sup> F) <sup>4</sup> D	13% (2 <sup>3</sup> P) <sup>2</sup> P
405,606 *		28% (2 <sup>3</sup> P) <sup>2</sup> P	13% (2 <sup>3</sup> F) <sup>4</sup> D	10% (3 <sup>1</sup> P) <sup>2</sup> P
394,516 *		41% (2 <sup>3</sup> P) <sup>4</sup> P	11% (3 <sup>1</sup> P) <sup>4</sup> P	9% (2 <sup>3</sup> P) <sup>4</sup> D
392,424	−57	36% (2 <sup>3</sup> P) <sup>4</sup> D	21% (2 <sup>3</sup> P) <sup>4</sup> D	11% (2 <sup>3</sup> P) <sup>4</sup> P
389,336 *		59% (1 <sup>1</sup> D) <sup>2</sup> P	9% (3 <sup>1</sup> P) <sup>4</sup> P	7% (2 <sup>1</sup> D) <sup>2</sup> P
380,449 *		48% (3 <sup>1</sup> D) <sup>2</sup> P	23% (1 <sup>1</sup> S) <sup>2</sup> P	9% (3 <sup>1</sup> D) <sup>4</sup> D
375,489	17	64% (3 <sup>1</sup> D) <sup>4</sup> P	10% (2 <sup>3</sup> P) <sup>4</sup> P	6% (3 <sup>1</sup> D) <sup>4</sup> D
374,810	−24	35% (3 <sup>1</sup> P) <sup>2</sup> P	16% (1 <sup>1</sup> S) <sup>2</sup> P	9% (3 <sup>1</sup> P) <sup>4</sup> P
370,586 *		22% (1 <sup>1</sup> S) <sup>2</sup> P	19% (3 <sup>1</sup> P) <sup>2</sup> S	15% (3 <sup>1</sup> P) <sup>2</sup> S
368,200 *		32% (3 <sup>1</sup> F) <sup>4</sup> D	30% (3 <sup>1</sup> D) <sup>4</sup> D	11% (3 <sup>1</sup> D) <sup>2</sup> P
366,416 *		32% (3 <sup>1</sup> D) <sup>4</sup> D	31% (2 <sup>3</sup> F) <sup>4</sup> D	13% (2 <sup>3</sup> F) <sup>4</sup> D
364,278 *		19% (3 <sup>1</sup> P) <sup>4</sup> P	19% (3 <sup>1</sup> P) <sup>2</sup> P	11% (2 <sup>3</sup> P) <sup>2</sup> S
355,790	−19	32% (3 <sup>1</sup> P) <sup>4</sup> P	16% (3 <sup>1</sup> P) <sup>4</sup> P	13% (2 <sup>3</sup> P) <sup>2</sup> S
352,270	26	77% (3 <sup>1</sup> D) <sup>4</sup> D	9% (3 <sup>1</sup> P) <sup>4</sup> D	4% (3 <sup>1</sup> D) <sup>4</sup> D
347,791 *		32% (3 <sup>1</sup> P) <sup>4</sup> D	23% (2 <sup>3</sup> P) <sup>4</sup> D	10% (3 <sup>1</sup> P) <sup>2</sup> P
341,227	−1	65% (3 <sup>1</sup> D) <sup>6</sup> D	30% (3 <sup>1</sup> D) <sup>4</sup> P	1% (2 <sup>3</sup> P) <sup>2</sup> S
328,555 *		54% (3 <sup>1</sup> D) <sup>4</sup> P	33% (2 <sup>3</sup> D) <sup>6</sup> D	5% (3 <sup>1</sup> P) <sup>4</sup> P
325,860 *		89% (3 <sup>1</sup> D) <sup>6</sup> F	3% (3 <sup>1</sup> P) <sup>4</sup> D	3% (3 <sup>1</sup> D) <sup>4</sup> D
<i>J</i> = 3/2				
455,917 *		74% (0 <sup>1</sup> S) <sup>2</sup> P	16% (1 <sup>1</sup> S) <sup>2</sup> P	7% (2 <sup>1</sup> D) <sup>2</sup> P
429,981 *		65% (2 <sup>1</sup> D) <sup>2</sup> D	24% (1 <sup>1</sup> D) <sup>2</sup> D	6% (2 <sup>1</sup> D) <sup>2</sup> P
416,277 *		29% (2 <sup>3</sup> F) <sup>2</sup> D	18% (3 <sup>1</sup> P) <sup>2</sup> D	14% (3 <sup>1</sup> P) <sup>2</sup> D
415,087 *		56% (2 <sup>1</sup> D) <sup>2</sup> P	6% (3 <sup>1</sup> P) <sup>2</sup> D	6% (1 <sup>1</sup> D) <sup>2</sup> P
406,960 *		38% (2 <sup>3</sup> F) <sup>4</sup> D	17% (2 <sup>3</sup> F) <sup>4</sup> D	11% (2 <sup>3</sup> P) <sup>4</sup> D
404,310 *		23% (2 <sup>3</sup> P) <sup>2</sup> P	14% (2 <sup>3</sup> P) <sup>4</sup> S	13% (2 <sup>3</sup> P) <sup>4</sup> S

Table A6. Cont.

E <sup>a</sup>	o-c <sup>b</sup>	Eigenvector Composition <sup>c</sup>		
403,643 *		31% (2 <sup>3</sup> P) <sup>2</sup> P	22% (3 <sup>3</sup> P) <sup>4</sup> S	19% (3 <sup>3</sup> P) <sup>4</sup> S
399,850	2	41% (1 <sup>1</sup> F) <sup>2</sup> D	13% (3 <sup>3</sup> F) <sup>2</sup> D	8% (2 <sup>3</sup> P) <sup>2</sup> D
395,638 *		39% (1 <sup>1</sup> F) <sup>2</sup> D	18% (2 <sup>3</sup> F) <sup>4</sup> F	12% (2 <sup>3</sup> P) <sup>2</sup> D
393,610	−2	22% (1 <sup>1</sup> D) <sup>2</sup> P	15% (2 <sup>3</sup> P) <sup>4</sup> P	8% (2 <sup>3</sup> F) <sup>4</sup> D
391,553	7	19% (2 <sup>3</sup> P) <sup>4</sup> D	14% (2 <sup>3</sup> P) <sup>4</sup> D	14% (2 <sup>3</sup> F) <sup>2</sup> D
389,293	26	45% (2 <sup>3</sup> F) <sup>4</sup> F	7% (2 <sup>3</sup> P) <sup>4</sup> D	7% (3 <sup>3</sup> D) <sup>2</sup> D
387,806 *		21% (2 <sup>3</sup> P) <sup>4</sup> P	10% (3 <sup>3</sup> P) <sup>4</sup> P	10% (1 <sup>1</sup> D) <sup>2</sup> P
386,582	−38	31% (1 <sup>1</sup> S) <sup>2</sup> P	10% (2 <sup>1</sup> D) <sup>2</sup> D	8% (3 <sup>3</sup> D) <sup>2</sup> P
383,280	4	46% (3 <sup>3</sup> D) <sup>2</sup> D	19% (3 <sup>3</sup> F) <sup>2</sup> D	9% (1 <sup>1</sup> D) <sup>2</sup> D
377,910	34	19% (1 <sup>1</sup> S) <sup>2</sup> P	18% (1 <sup>1</sup> D) <sup>2</sup> D	17% (1 <sup>1</sup> D) <sup>2</sup> P
375,706	21	30% (3 <sup>3</sup> D) <sup>4</sup> D	13% (3 <sup>3</sup> D) <sup>2</sup> P	11% (3 <sup>3</sup> D) <sup>4</sup> F
374,938	0	22% (3 <sup>3</sup> D) <sup>2</sup> P	11% (3 <sup>3</sup> P) <sup>2</sup> P	11% (3 <sup>3</sup> D) <sup>4</sup> F
374,236	31	24% (3 <sup>3</sup> D) <sup>4</sup> P	18% (3 <sup>3</sup> G) <sup>4</sup> F	9% (3 <sup>3</sup> D) <sup>4</sup> F
371,218 *		25% (3 <sup>3</sup> P) <sup>2</sup> D	14% (2 <sup>3</sup> P) <sup>2</sup> P	13% (2 <sup>3</sup> P) <sup>2</sup> D
369,448	−4	27% (3 <sup>3</sup> D) <sup>4</sup> P	18% (3 <sup>3</sup> D) <sup>4</sup> D	15% (3 <sup>3</sup> P) <sup>2</sup> P
368,569	0	22% (3 <sup>3</sup> F) <sup>4</sup> D	10% (3 <sup>3</sup> D) <sup>4</sup> D	8% (3 <sup>3</sup> D) <sup>4</sup> F
366,573	3	25% (3 <sup>3</sup> F) <sup>4</sup> F	14% (3 <sup>3</sup> F) <sup>4</sup> D	9% (3 <sup>3</sup> F) <sup>2</sup> D
366,078	−4	17% (3 <sup>3</sup> F) <sup>4</sup> F	16% (3 <sup>3</sup> P) <sup>4</sup> S	14% (2 <sup>3</sup> P) <sup>4</sup> S
363,454	−23	31% (3 <sup>3</sup> D) <sup>4</sup> F	29% (3 <sup>3</sup> G) <sup>4</sup> F	12% (3 <sup>3</sup> P) <sup>4</sup> P
361,846 *		20% (3 <sup>3</sup> P) <sup>2</sup> P	9% (3 <sup>3</sup> P) <sup>4</sup> S	9% (3 <sup>3</sup> D) <sup>4</sup> D
360,092	−51	34% (3 <sup>3</sup> P) <sup>4</sup> P	14% (3 <sup>3</sup> P) <sup>4</sup> P	11% (3 <sup>3</sup> D) <sup>4</sup> D
356,993	−2	20% (3 <sup>3</sup> F) <sup>2</sup> D	18% (3 <sup>3</sup> F) <sup>4</sup> F	10% (3 <sup>3</sup> P) <sup>4</sup> D
353,549	22	44% (3 <sup>3</sup> D) <sup>4</sup> D	22% (2 <sup>3</sup> P) <sup>4</sup> D	8% (2 <sup>3</sup> P) <sup>4</sup> D
351,904 *		34% (3 <sup>3</sup> D) <sup>4</sup> D	16% (3 <sup>3</sup> P) <sup>4</sup> D	14% (2 <sup>3</sup> P) <sup>4</sup> D
342,965 *		48% (3 <sup>3</sup> D) <sup>4</sup> F	25% (3 <sup>3</sup> D) <sup>6</sup> D	16% (3 <sup>3</sup> D) <sup>4</sup> P
341,983	4	31% (3 <sup>3</sup> D) <sup>4</sup> F	27% (3 <sup>3</sup> D) <sup>4</sup> P	26% (3 <sup>3</sup> D) <sup>6</sup> D
336,333	−24	72% (3 <sup>3</sup> D) <sup>6</sup> P	16% (3 <sup>3</sup> D) <sup>6</sup> D	6% (3 <sup>3</sup> D) <sup>4</sup> P
331,200	−4	41% (3 <sup>3</sup> D) <sup>4</sup> P	31% (3 <sup>3</sup> D) <sup>6</sup> D	22% (3 <sup>3</sup> D) <sup>6</sup> P
327,322 *		91% (3 <sup>3</sup> D) <sup>6</sup> F	3% (3 <sup>3</sup> D) <sup>4</sup> D	2% (2 <sup>3</sup> P) <sup>4</sup> D
<i>J</i> = 5/2				
432,566 *		64% (2 <sup>1</sup> D) <sup>2</sup> D	23% (1 <sup>1</sup> D) <sup>2</sup> D	8% (2 <sup>1</sup> D) <sup>2</sup> F
422,985	−10	43% (2 <sup>1</sup> D) <sup>2</sup> F	17% (1 <sup>1</sup> G) <sup>2</sup> F	13% (1 <sup>1</sup> G) <sup>2</sup> F
414,230	8	46% (2 <sup>3</sup> F) <sup>2</sup> D	17% (3 <sup>3</sup> F) <sup>2</sup> D	14% (2 <sup>3</sup> P) <sup>2</sup> D
409,186	50	51% (2 <sup>1</sup> G) <sup>2</sup> F	21% (2 <sup>1</sup> D) <sup>2</sup> F	8% (2 <sup>3</sup> F) <sup>2</sup> D
405,964 *		45% (2 <sup>3</sup> F) <sup>4</sup> D	16% (3 <sup>3</sup> F) <sup>4</sup> D	12% (2 <sup>3</sup> P) <sup>4</sup> D
400,637	16	28% (1 <sup>1</sup> F) <sup>2</sup> D	10% (2 <sup>3</sup> P) <sup>4</sup> D	10% (2 <sup>3</sup> F) <sup>2</sup> F
398,662	−16	32% (2 <sup>3</sup> F) <sup>2</sup> F	22% (3 <sup>3</sup> F) <sup>4</sup> G	8% (3 <sup>3</sup> F) <sup>4</sup> G
395,990 *		44% (2 <sup>3</sup> P) <sup>4</sup> P	15% (2 <sup>3</sup> P) <sup>4</sup> P	10% (2 <sup>3</sup> P) <sup>2</sup> D
394,049	7	28% (2 <sup>3</sup> F) <sup>4</sup> F	20% (2 <sup>1</sup> F) <sup>2</sup> D	12% (2 <sup>3</sup> P) <sup>4</sup> D
391,396	28	29% (2 <sup>3</sup> F) <sup>4</sup> G	11% (3 <sup>3</sup> F) <sup>2</sup> F	11% (3 <sup>3</sup> F) <sup>4</sup> G
390,060	−66	38% (2 <sup>3</sup> F) <sup>4</sup> F	11% (3 <sup>3</sup> P) <sup>4</sup> D	6% (2 <sup>3</sup> F) <sup>4</sup> D
387,358 *		20% (2 <sup>3</sup> P) <sup>2</sup> D	12% (2 <sup>3</sup> F) <sup>2</sup> D	11% (1 <sup>1</sup> F) <sup>2</sup> D
386,268	−6	25% (1 <sup>1</sup> D) <sup>2</sup> D	17% (2 <sup>1</sup> D) <sup>2</sup> F	9% (2 <sup>3</sup> F) <sup>2</sup> F
385,962	10	21% (3 <sup>3</sup> D) <sup>2</sup> F	13% (2 <sup>3</sup> D) <sup>2</sup> D	12% (1 <sup>1</sup> G) <sup>2</sup> F
383,109	22	25% (3 <sup>3</sup> D) <sup>2</sup> F	8% (1 <sup>1</sup> F) <sup>2</sup> F	7% (3 <sup>3</sup> P) <sup>2</sup> D
380,891	−18	28% (1 <sup>1</sup> G) <sup>2</sup> F	18% (3 <sup>3</sup> D) <sup>2</sup> D	8% (3 <sup>3</sup> F) <sup>2</sup> F
379,478	−25	25% (3 <sup>3</sup> G) <sup>2</sup> F	21% (1 <sup>1</sup> D) <sup>2</sup> F	12% (3 <sup>3</sup> P) <sup>2</sup> D
379,077	−7	29% (1 <sup>1</sup> F) <sup>2</sup> F	13% (3 <sup>3</sup> P) <sup>2</sup> D	12% (2 <sup>3</sup> P) <sup>2</sup> D
376,543	17	23% (3 <sup>3</sup> D) <sup>4</sup> F	17% (3 <sup>3</sup> D) <sup>4</sup> D	9% (3 <sup>3</sup> G) <sup>4</sup> F
374,426	−0	13% (3 <sup>3</sup> G) <sup>4</sup> F	11% (1 <sup>1</sup> G) <sup>2</sup> F	11% (3 <sup>3</sup> P) <sup>2</sup> D
372,051	−6	24% (3 <sup>3</sup> H) <sup>4</sup> G	20% (3 <sup>3</sup> G) <sup>4</sup> G	16% (3 <sup>3</sup> F) <sup>2</sup> F
370,940 *		16% (3 <sup>3</sup> D) <sup>4</sup> D	15% (3 <sup>3</sup> F) <sup>4</sup> D	12% (3 <sup>3</sup> F) <sup>4</sup> F

Table A6. Cont.

E <sup>a</sup>	o-c <sup>b</sup>	Eigenvector Composition <sup>c</sup>			
369,578	12	21% ( <sup>3</sup> F) <sup>2</sup> F	15% ( <sup>3</sup> D) <sup>4</sup> P	11% ( <sup>3</sup> H) <sup>4</sup> G	
367,919	13	24% ( <sup>3</sup> D) <sup>4</sup> P	23% ( <sup>3</sup> P) <sup>4</sup> P	9% ( <sup>3</sup> G) <sup>4</sup> G	
366,693	-15	14% ( <sup>3</sup> D) <sup>4</sup> D	13% ( <sup>3</sup> F) <sup>4</sup> F	13% ( <sup>3</sup> F) <sup>4</sup> D	
364,877	-3	17% ( <sup>3</sup> P) <sup>4</sup> P	13% ( <sup>3</sup> P) <sup>4</sup> P	8% ( <sup>3</sup> P) <sup>2</sup> D	
364,025	-28	15% ( <sup>3</sup> D) <sup>2</sup> D	14% ( <sup>3</sup> D) <sup>4</sup> P	10% ( <sup>3</sup> H) <sup>4</sup> G	
362,975	3	25% ( <sup>3</sup> P) <sup>4</sup> D	17% ( <sup>2</sup> F) <sup>4</sup> F	13% ( <sup>3</sup> G) <sup>4</sup> F	
362,381	56	20% ( <sup>3</sup> H) <sup>4</sup> G	11% ( <sup>3</sup> D) <sup>2</sup> F	10% ( <sup>3</sup> D) <sup>4</sup> F	
361,296	-14	22% ( <sup>3</sup> F) <sup>4</sup> F	13% ( <sup>3</sup> G) <sup>4</sup> F	11% ( <sup>3</sup> F) <sup>2</sup> D	
358,392	29	21% ( <sup>3</sup> F) <sup>4</sup> G	12% ( <sup>3</sup> G) <sup>2</sup> F	8% ( <sup>3</sup> P) <sup>4</sup> D	
356,233	1	14% ( <sup>3</sup> F) <sup>4</sup> D	13% ( <sup>3</sup> F) <sup>4</sup> G	12% ( <sup>3</sup> P) <sup>4</sup> D	
354,235	16	78% ( <sup>5</sup> D) <sup>4</sup> D	4% ( <sup>3</sup> D) <sup>4</sup> D	2% ( <sup>3</sup> F) <sup>4</sup> F	
352,685	45	26% ( <sup>3</sup> G) <sup>4</sup> G	22% ( <sup>3</sup> F) <sup>4</sup> G	14% ( <sup>2</sup> P) <sup>4</sup> G	
344,695	6	32% ( <sup>5</sup> D) <sup>4</sup> F	30% ( <sup>5</sup> D) <sup>4</sup> P	27% ( <sup>5</sup> D) <sup>6</sup> D	
343,336	-17	42% ( <sup>5</sup> D) <sup>4</sup> F	33% ( <sup>5</sup> D) <sup>4</sup> P	5% ( <sup>5</sup> D) <sup>6</sup> P	
339,172	1	50% ( <sup>5</sup> D) <sup>6</sup> D	30% ( <sup>5</sup> D) <sup>6</sup> P	8% ( <sup>5</sup> D) <sup>4</sup> P	
333,327	18	61% ( <sup>5</sup> D) <sup>6</sup> P	18% ( <sup>5</sup> D) <sup>4</sup> P	17% ( <sup>5</sup> D) <sup>6</sup> D	
329,356 *		89% ( <sup>5</sup> D) <sup>6</sup> F	4% ( <sup>5</sup> D) <sup>4</sup> F	2% ( <sup>5</sup> D) <sup>4</sup> D	
<i>J = 7/2</i>					
428,522	-6	70% ( <sup>2</sup> D) <sup>2</sup> F	15% ( <sup>1</sup> D) <sup>2</sup> F	7% ( <sup>1</sup> G) <sup>2</sup> F	
409,889	5	39% ( <sup>2</sup> G) <sup>2</sup> F	14% ( <sup>1</sup> G) <sup>2</sup> G	10% ( <sup>2</sup> F) <sup>2</sup> G	
406,495	-4	46% ( <sup>2</sup> F) <sup>2</sup> G	17% ( <sup>3</sup> F) <sup>2</sup> G	12% ( <sup>2</sup> G) <sup>2</sup> G	
404,117	-8	27% ( <sup>2</sup> F) <sup>2</sup> F	19% ( <sup>2</sup> F) <sup>4</sup> D	9% ( <sup>2</sup> G) <sup>2</sup> G	
403,133	-5	25% ( <sup>2</sup> F) <sup>4</sup> D	17% ( <sup>1</sup> G) <sup>2</sup> G	10% ( <sup>2</sup> F) <sup>4</sup> D	
397,858	12	26% ( <sup>2</sup> F) <sup>4</sup> G	22% ( <sup>2</sup> F) <sup>4</sup> F	9% ( <sup>3</sup> F) <sup>4</sup> G	
396,241	-22	32% ( <sup>2</sup> P) <sup>4</sup> D	21% ( <sup>2</sup> F) <sup>2</sup> F	15% ( <sup>3</sup> P) <sup>4</sup> D	
393,295	-10	20% ( <sup>2</sup> F) <sup>4</sup> G	15% ( <sup>2</sup> F) <sup>4</sup> D	13% ( <sup>2</sup> F) <sup>2</sup> F	
391,338	32	43% ( <sup>2</sup> F) <sup>4</sup> F	12% ( <sup>2</sup> F) <sup>4</sup> G	12% ( <sup>1</sup> D) <sup>2</sup> F	
388,163	-3	23% ( <sup>1</sup> F) <sup>2</sup> G	14% ( <sup>2</sup> D) <sup>2</sup> F	13% ( <sup>1</sup> D) <sup>2</sup> F	
386,615	15	26% ( <sup>1</sup> F) <sup>2</sup> G	21% ( <sup>2</sup> F) <sup>2</sup> F	7% ( <sup>2</sup> F) <sup>4</sup> F	
384,772	25	24% ( <sup>1</sup> D) <sup>2</sup> F	16% ( <sup>1</sup> G) <sup>2</sup> G	11% ( <sup>3</sup> F) <sup>2</sup> F	
380,468	-6	20% ( <sup>1</sup> F) <sup>2</sup> F	19% ( <sup>3</sup> G) <sup>2</sup> G	10% ( <sup>3</sup> D) <sup>2</sup> F	
379,061	-3	21% ( <sup>1</sup> G) <sup>2</sup> G	18% ( <sup>1</sup> F) <sup>2</sup> F	15% ( <sup>3</sup> D) <sup>2</sup> F	
377,163	-3	27% ( <sup>3</sup> D) <sup>4</sup> F	17% ( <sup>3</sup> D) <sup>4</sup> D	17% ( <sup>3</sup> G) <sup>4</sup> F	
375,365	3	37% ( <sup>3</sup> G) <sup>2</sup> G	9% ( <sup>3</sup> D) <sup>2</sup> F	8% ( <sup>3</sup> D) <sup>4</sup> D	
374,839	-5	14% ( <sup>3</sup> H) <sup>4</sup> G	13% ( <sup>1</sup> G) <sup>2</sup> F	11% ( <sup>3</sup> G) <sup>4</sup> F	
373,577	-30	13% ( <sup>3</sup> F) <sup>4</sup> D	10% ( <sup>3</sup> D) <sup>4</sup> D	10% ( <sup>3</sup> G) <sup>2</sup> F	
371,673	0	25% ( <sup>3</sup> G) <sup>4</sup> G	24% ( <sup>1</sup> G) <sup>2</sup> F	7% ( <sup>2</sup> G) <sup>2</sup> F	
370,993	-50	33% ( <sup>3</sup> F) <sup>2</sup> F	25% ( <sup>3</sup> G) <sup>2</sup> F	10% ( <sup>3</sup> D) <sup>4</sup> D	
369,879	-23	28% ( <sup>3</sup> P) <sup>4</sup> D	13% ( <sup>3</sup> D) <sup>4</sup> F	11% ( <sup>2</sup> P) <sup>4</sup> D	
368,968	3	15% ( <sup>3</sup> P) <sup>4</sup> D	10% ( <sup>3</sup> H) <sup>4</sup> G	10% ( <sup>2</sup> P) <sup>4</sup> D	
366,806	21	29% ( <sup>3</sup> F) <sup>4</sup> F	11% ( <sup>3</sup> G) <sup>4</sup> F	8% ( <sup>3</sup> H) <sup>4</sup> G	
365,842	3	16% ( <sup>3</sup> F) <sup>2</sup> G	15% ( <sup>3</sup> F) <sup>4</sup> F	14% ( <sup>3</sup> D) <sup>2</sup> F	
362,942	-4	25% ( <sup>3</sup> G) <sup>4</sup> H	25% ( <sup>3</sup> H) <sup>4</sup> H	10% ( <sup>3</sup> H) <sup>2</sup> G	
361,593	-18	25% ( <sup>3</sup> G) <sup>4</sup> F	18% ( <sup>3</sup> D) <sup>4</sup> F	9% ( <sup>5</sup> D) <sup>4</sup> F	
361,173	-0	39% ( <sup>3</sup> F) <sup>4</sup> G	12% ( <sup>3</sup> H) <sup>4</sup> G	11% ( <sup>3</sup> G) <sup>4</sup> H	
359,687	-10	16% ( <sup>3</sup> G) <sup>4</sup> G	12% ( <sup>3</sup> F) <sup>4</sup> D	12% ( <sup>3</sup> H) <sup>4</sup> G	
356,493	-0	17% ( <sup>3</sup> F) <sup>4</sup> D	11% ( <sup>3</sup> G) <sup>4</sup> G	10% ( <sup>3</sup> H) <sup>4</sup> H	
354,869	-9	68% ( <sup>5</sup> D) <sup>4</sup> D	6% ( <sup>3</sup> D) <sup>4</sup> D	5% ( <sup>3</sup> F) <sup>4</sup> F	
353,454	-22	19% ( <sup>3</sup> G) <sup>4</sup> H	18% ( <sup>3</sup> H) <sup>2</sup> G	9% ( <sup>3</sup> F) <sup>4</sup> G	
349,047	10	47% ( <sup>3</sup> H) <sup>4</sup> H	23% ( <sup>3</sup> G) <sup>4</sup> H	9% ( <sup>3</sup> H) <sup>2</sup> G	
346,061	-1	55% ( <sup>5</sup> D) <sup>4</sup> F	28% ( <sup>5</sup> D) <sup>6</sup> D	3% ( <sup>5</sup> D) <sup>6</sup> F	
341,458	1	59% ( <sup>5</sup> D) <sup>6</sup> D	18% ( <sup>5</sup> D) <sup>4</sup> F	12% ( <sup>5</sup> D) <sup>6</sup> F	
334,906	25	85% ( <sup>5</sup> D) <sup>6</sup> P	6% ( <sup>5</sup> D) <sup>6</sup> D	4% ( <sup>5</sup> D) <sup>4</sup> D	
331,831 *		82% ( <sup>5</sup> D) <sup>6</sup> F	8% ( <sup>5</sup> D) <sup>4</sup> F	4% ( <sup>5</sup> D) <sup>6</sup> D	

Table A6. Cont.

E <sup>a</sup>	o-c <sup>b</sup>	Eigenvector Composition <sup>c</sup>		
<i>J</i> = 9/2				
409,779	3	34% (2 <sup>1</sup> G) <sup>2</sup> G	17% (1 <sup>1</sup> G) <sup>2</sup> G	16% (2 <sup>1</sup> G) <sup>2</sup> H
403,942	−32	49% (2 <sup>3</sup> F) <sup>2</sup> G	12% (3 <sup>3</sup> F) <sup>2</sup> G	11% (2 <sup>3</sup> F) <sup>4</sup> G
401,561	−26	33% (2 <sup>1</sup> G) <sup>2</sup> H	14% (1 <sup>1</sup> G) <sup>2</sup> H	14% (2 <sup>1</sup> G) <sup>2</sup> G
398,431	16	37% (2 <sup>3</sup> F) <sup>4</sup> F	25% (3 <sup>3</sup> F) <sup>4</sup> G	7% (2 <sup>1</sup> G) <sup>2</sup> H
392,486	12	29% (2 <sup>3</sup> F) <sup>4</sup> G	21% (1 <sup>1</sup> F) <sup>2</sup> G	17% (2 <sup>3</sup> F) <sup>4</sup> F
390,759	19	45% (1 <sup>1</sup> F) <sup>2</sup> G	31% (2 <sup>3</sup> F) <sup>4</sup> F	5% (2 <sup>3</sup> F) <sup>2</sup> G
382,720	4	31% (1 <sup>1</sup> G) <sup>2</sup> G	22% (1 <sup>1</sup> G) <sup>2</sup> G	18% (3 <sup>3</sup> G) <sup>2</sup> G
382,377	−27	57% (1 <sup>1</sup> D) <sup>2</sup> H	13% (2 <sup>3</sup> G) <sup>2</sup> H	10% (2 <sup>1</sup> G) <sup>2</sup> H
379,226	12	20% (3 <sup>3</sup> G) <sup>2</sup> G	12% (2 <sup>3</sup> G) <sup>4</sup> F	11% (1 <sup>1</sup> G) <sup>2</sup> H
377,393	24	22% (3 <sup>3</sup> F) <sup>2</sup> G	13% (3 <sup>3</sup> H) <sup>2</sup> G	11% (3 <sup>3</sup> D) <sup>4</sup> F
375,593	8	53% (3 <sup>3</sup> D) <sup>4</sup> F	14% (3 <sup>3</sup> G) <sup>2</sup> G	9% (3 <sup>3</sup> H) <sup>2</sup> G
373,120	4	22% (3 <sup>3</sup> G) <sup>4</sup> G	14% (3 <sup>3</sup> H) <sup>2</sup> H	11% (3 <sup>3</sup> H) <sup>4</sup> G
371,061	−6	22% (3 <sup>3</sup> H) <sup>2</sup> H	21% (3 <sup>3</sup> G) <sup>2</sup> H	13% (3 <sup>3</sup> H) <sup>4</sup> G
370,501	1	13% (3 <sup>3</sup> G) <sup>2</sup> H	11% (3 <sup>3</sup> G) <sup>2</sup> G	10% (3 <sup>3</sup> H) <sup>2</sup> H
368,429	−8	25% (3 <sup>3</sup> G) <sup>4</sup> H	17% (3 <sup>3</sup> F) <sup>4</sup> G	14% (3 <sup>3</sup> F) <sup>4</sup> F
365,569	−33	43% (3 <sup>3</sup> F) <sup>4</sup> F	10% (3 <sup>3</sup> G) <sup>2</sup> H	8% (3 <sup>3</sup> G) <sup>4</sup> H
364,772	−14	17% (3 <sup>3</sup> F) <sup>4</sup> G	17% (3 <sup>3</sup> G) <sup>4</sup> F	13% (3 <sup>3</sup> H) <sup>2</sup> G
362,447	−2	30% (3 <sup>3</sup> G) <sup>4</sup> F	22% (3 <sup>3</sup> H) <sup>4</sup> H	6% (3 <sup>3</sup> G) <sup>4</sup> H
361,650	0	34% (3 <sup>3</sup> H) <sup>4</sup> G	22% (3 <sup>3</sup> G) <sup>4</sup> G	13% (3 <sup>3</sup> F) <sup>2</sup> H
360,482	0	15% (3 <sup>3</sup> F) <sup>4</sup> G	13% (3 <sup>3</sup> G) <sup>4</sup> F	12% (1 <sup>1</sup> G) <sup>2</sup> H
356,416	−9	33% (3 <sup>3</sup> H) <sup>4</sup> I	11% (3 <sup>3</sup> G) <sup>4</sup> H	11% (3 <sup>3</sup> G) <sup>4</sup> G
354,122	−6	29% (3 <sup>3</sup> H) <sup>4</sup> H	14% (3 <sup>3</sup> H) <sup>4</sup> I	13% (3 <sup>3</sup> H) <sup>2</sup> G
349,721	−13	27% (3 <sup>3</sup> H) <sup>4</sup> I	27% (3 <sup>3</sup> H) <sup>4</sup> H	18% (3 <sup>3</sup> G) <sup>4</sup> H
348,377	−14	43% (3 <sup>3</sup> D) <sup>6</sup> D	29% (3 <sup>3</sup> D) <sup>4</sup> F	5% (3 <sup>3</sup> H) <sup>4</sup> I
342,289	−12	41% (3 <sup>3</sup> D) <sup>6</sup> D	27% (3 <sup>3</sup> D) <sup>6</sup> F	24% (3 <sup>3</sup> D) <sup>4</sup> F
334,849 *		69% (3 <sup>3</sup> D) <sup>6</sup> F	15% (3 <sup>3</sup> D) <sup>4</sup> F	9% (3 <sup>3</sup> D) <sup>6</sup> D
<i>J</i> = 11/2				
409,441	8	64% (2 <sup>1</sup> G) <sup>2</sup> H	26% (1 <sup>1</sup> G) <sup>2</sup> H	5% (1 <sup>1</sup> D) <sup>2</sup> H
399,022	−1	78% (2 <sup>3</sup> F) <sup>4</sup> G	14% (3 <sup>3</sup> F) <sup>4</sup> G	4% (2 <sup>1</sup> G) <sup>2</sup> H
383,539	−14	24% (1 <sup>1</sup> D) <sup>2</sup> H	20% (1 <sup>1</sup> G) <sup>2</sup> H	17% (2 <sup>1</sup> G) <sup>2</sup> H
377,717	14	38% (1 <sup>1</sup> G) <sup>2</sup> H	24% (1 <sup>1</sup> D) <sup>2</sup> H	14% (3 <sup>3</sup> G) <sup>2</sup> H
376,414	−1	32% (3 <sup>3</sup> G) <sup>4</sup> G	23% (3 <sup>3</sup> G) <sup>2</sup> H	18% (3 <sup>3</sup> H) <sup>4</sup> G
372,676	6	45% (3 <sup>3</sup> H) <sup>2</sup> H	14% (1 <sup>1</sup> D) <sup>2</sup> H	14% (3 <sup>3</sup> G) <sup>4</sup> G
370,488	−1	20% (3 <sup>3</sup> G) <sup>4</sup> H	18% (3 <sup>3</sup> G) <sup>2</sup> H	15% (3 <sup>3</sup> G) <sup>4</sup> G
369,661	6	33% (1 <sup>1</sup> D) <sup>2</sup> I	21% (3 <sup>3</sup> H) <sup>2</sup> I	15% (3 <sup>3</sup> H) <sup>2</sup> H
367,483	−2	41% (3 <sup>3</sup> F) <sup>4</sup> G	21% (3 <sup>3</sup> H) <sup>2</sup> I	9% (1 <sup>1</sup> D) <sup>2</sup> I
365,017	−2	28% (3 <sup>3</sup> H) <sup>4</sup> H	23% (3 <sup>3</sup> G) <sup>4</sup> H	17% (3 <sup>3</sup> G) <sup>2</sup> H
362,535	−1	35% (3 <sup>3</sup> H) <sup>2</sup> I	14% (3 <sup>3</sup> F) <sup>4</sup> G	13% (3 <sup>3</sup> G) <sup>2</sup> H
360,481	1	52% (3 <sup>3</sup> H) <sup>4</sup> I	14% (3 <sup>3</sup> G) <sup>4</sup> G	14% (3 <sup>3</sup> H) <sup>4</sup> H
357,689	2	45% (3 <sup>3</sup> H) <sup>4</sup> G	12% (3 <sup>3</sup> H) <sup>2</sup> H	12% (3 <sup>3</sup> G) <sup>4</sup> G
352,082	−7	39% (3 <sup>3</sup> H) <sup>4</sup> H	30% (3 <sup>3</sup> H) <sup>4</sup> I	17% (3 <sup>3</sup> G) <sup>4</sup> H
340,947 *		96% (3 <sup>3</sup> D) <sup>6</sup> F	3% (3 <sup>3</sup> F) <sup>4</sup> G	1% (2 <sup>3</sup> F) <sup>4</sup> G
<i>J</i> = 13/2				
376,419	14	55% (1 <sup>1</sup> D) <sup>2</sup> I	38% (1 <sup>1</sup> D) <sup>2</sup> K	4% (3 <sup>3</sup> H) <sup>4</sup> H
372,822	−2	52% (3 <sup>3</sup> G) <sup>4</sup> H	29% (3 <sup>3</sup> H) <sup>2</sup> I	8% (3 <sup>3</sup> H) <sup>4</sup> H
369,654	7	39% (1 <sup>1</sup> D) <sup>2</sup> K	23% (1 <sup>1</sup> D) <sup>2</sup> I	19% (3 <sup>3</sup> H) <sup>2</sup> I
364,518	12	34% (3 <sup>3</sup> H) <sup>2</sup> I	22% (3 <sup>3</sup> G) <sup>4</sup> H	20% (3 <sup>3</sup> H) <sup>4</sup> I
363,614	−26	49% (3 <sup>3</sup> H) <sup>4</sup> I	37% (3 <sup>3</sup> H) <sup>4</sup> H	6% (1 <sup>1</sup> D) <sup>2</sup> K
354,719	3	48% (3 <sup>3</sup> H) <sup>4</sup> H	24% (3 <sup>3</sup> H) <sup>4</sup> I	13% (3 <sup>3</sup> H) <sup>2</sup> I
<i>J</i> = 15/2				
378,355	9	94% (1 <sup>1</sup> D) <sup>2</sup> K	6% (3 <sup>3</sup> H) <sup>4</sup> I	
365,186 *		94% (3 <sup>3</sup> H) <sup>4</sup> I	6% (1 <sup>1</sup> D) <sup>2</sup> K	

<sup>a</sup> The star \* indicates a calculated value for the level; <sup>b</sup> The difference between the observed and the calculated energies; <sup>c</sup> For the eigenvector composition, up to three components with the largest percentages in the LS-coupling scheme are listed. The number preceding the terms is the seniority number.

**Table A7.** Energies (in  $\text{cm}^{-1}$ ) of the  $4d^4$  configuration of Ag VIII.

E <sup>a</sup>	o-c <sup>b</sup>	Eigenvector Composition <sup>c</sup>		
<i>J</i> = 0				
114,851 *		82% 0 <sup>1</sup> S1	17% 4 <sup>1</sup> S2	1% 2 <sup>3</sup> P1
65,762 *		62% 2 <sup>3</sup> P1	35% 4 <sup>3</sup> P2	3% 4 <sup>1</sup> S2
45,338 *		72% 4 <sup>1</sup> S2	16% 0 <sup>1</sup> S1	11% 4 <sup>3</sup> P2
21,309	−37	50% 4 <sup>3</sup> P2	32% 2 <sup>3</sup> P1	8% 4 <sup>5</sup> D
0	−26	92% 4 <sup>5</sup> D	4% 2 <sup>3</sup> P1	4% 4 <sup>3</sup> P2
<i>J</i> = 1				
63,371	−50	63% 2 <sup>3</sup> P1	37% 4 <sup>3</sup> P2	0% 4 <sup>3</sup> D
39,191	−7	95% 4 <sup>3</sup> D	3% 2 <sup>3</sup> P1	1% 4 <sup>3</sup> P2
26,526	19	60% 4 <sup>3</sup> P2	32% 2 <sup>3</sup> P1	4% 4 <sup>3</sup> D
1,340	−10	96% 4 <sup>5</sup> D	2% 2 <sup>3</sup> P1	2% 4 <sup>3</sup> P2
<i>J</i> = 2				
88,586	34	80% 2 <sup>1</sup> D1	19% 4 <sup>1</sup> D2	0% 4 <sup>3</sup> D
61,644	6	68% 2 <sup>3</sup> F1	24% 4 <sup>3</sup> F2	5% 4 <sup>1</sup> D2
58,958 *		64% 2 <sup>3</sup> P1	28% 4 <sup>3</sup> P2	3% 4 <sup>1</sup> D2
48,505 *		61% 4 <sup>1</sup> D2	13% 2 <sup>1</sup> D1	10% 4 <sup>3</sup> D
38,402	17	63% 4 <sup>3</sup> D	12% 2 <sup>3</sup> P1	8% 4 <sup>3</sup> P2
32,134	−19	55% 4 <sup>3</sup> P2	22% 4 <sup>3</sup> D	21% 2 <sup>3</sup> P1
28,051	4	70% 4 <sup>3</sup> F2	21% 2 <sup>3</sup> F1	5% 4 <sup>1</sup> D2
3,212	−7	98% 4 <sup>5</sup> D	1% 2 <sup>3</sup> P1	1% 4 <sup>3</sup> D
<i>J</i> = 3				
62,552	−10	72% 2 <sup>3</sup> F1	17% 4 <sup>3</sup> F2	10% 4 <sup>1</sup> F
52,004	31	85% 4 <sup>1</sup> F	7% 2 <sup>3</sup> F1	5% 4 <sup>3</sup> D
36,879	−39	92% 4 <sup>3</sup> D	3% 4 <sup>1</sup> F	1% 2 <sup>3</sup> F1
32,926	23	50% 4 <sup>3</sup> F2	42% 4 <sup>3</sup> G	7% 2 <sup>3</sup> F1
26,967	11	55% 4 <sup>3</sup> G	31% 4 <sup>3</sup> F2	12% 2 <sup>3</sup> F1
5,292	1	98% 4 <sup>5</sup> D	1% 4 <sup>3</sup> F2	1% 4 <sup>3</sup> D
<i>J</i> = 4				
69,584	−60	66% 2 <sup>1</sup> G1	28% 4 <sup>1</sup> G2	4% 2 <sup>3</sup> F1
60,980	42	83% 2 <sup>3</sup> F1	10% 4 <sup>3</sup> F2	6% 2 <sup>1</sup> G1
43,104	−4	52% 4 <sup>1</sup> G2	18% 2 <sup>1</sup> G1	16% 4 <sup>3</sup> F2
32,698	−11	56% 4 <sup>3</sup> G	20% 4 <sup>3</sup> F2	16% 4 <sup>1</sup> G2
29,555	17	42% 4 <sup>3</sup> F2	25% 4 <sup>3</sup> H	21% 4 <sup>3</sup> G
23,302	−4	68% 4 <sup>3</sup> H	15% 4 <sup>3</sup> G	6% 4 <sup>3</sup> F2
7,443	−5	95% 4 <sup>5</sup> D	3% 4 <sup>3</sup> F2	1% 2 <sup>3</sup> F1
<i>J</i> = 5				
35,077	11	84% 4 <sup>3</sup> G	16% 4 <sup>3</sup> H	
26,250	12	84% 4 <sup>3</sup> H	16% 4 <sup>3</sup> G	
<i>J</i> = 6				
39,744	−4	91% 4 <sup>1</sup> I	9% 4 <sup>3</sup> H	
28,185	−5	91% 4 <sup>3</sup> H	9% 4 <sup>1</sup> I	

<sup>a</sup> The star \* indicates a calculated value for the level; <sup>b</sup> The difference between the observed and the calculated energies; <sup>c</sup> For the eigenvector composition, up to three components with the largest percentages in the LS-coupling scheme are listed. The number preceding the terms is the seniority number. The number following the terms displays Nielson and Koster sequential indices [20].

**Table A8.** Energies (in  $\text{cm}^{-1}$ ) of the  $4d^35p$  configuration of Ag VIII.

$E^a$	$o-c^b$	Eigenvector Composition $c$		
$J = 0$				
460,564 *		72% ( $1^2D$ ) $^3P$	26% ( $3^2D$ ) $^3P$	1% ( $3^2P$ ) $^3P$
422,372 *		44% ( $3^2D$ ) $^3P$	30% ( $3^2P$ ) $^3P$	12% ( $3^2P$ ) $^1S$
410,445 *		48% ( $3^4P$ ) $^3P$	27% ( $3^2P$ ) $^1S$	8% ( $3^2D$ ) $^3P$
400,473 *		53% ( $3^2P$ ) $^3P$	15% ( $3^4P$ ) $^3P$	14% ( $3^2D$ ) $^3P$
398,971 *		39% ( $3^2P$ ) $^1S$	39% ( $3^4P$ ) $^5D$	10% ( $3^4F$ ) $^5D$
391,021 *		34% ( $3^4P$ ) $^5D$	27% ( $3^4P$ ) $^3P$	17% ( $3^2P$ ) $^1S$
382,525	−78	73% ( $3^4F$ ) $^5D$	20% ( $3^4P$ ) $^5D$	2% ( $3^2D$ ) $^3P$
$J = 1$				
466,227	−16	73% ( $1^2D$ ) $^1P$	18% ( $3^2D$ ) $^1P$	4% ( $1^2D$ ) $^3P$
459,403 *		64% ( $1^2D$ ) $^3P$	22% ( $3^2D$ ) $^3P$	6% ( $1^2D$ ) $^5D$
444,840 *		53% ( $1^2D$ ) $^3D$	19% ( $3^2F$ ) $^3D$	15% ( $3^2D$ ) $^3D$
433,769 *		60% ( $3^2F$ ) $^3D$	26% ( $1^2D$ ) $^3D$	8% ( $3^2D$ ) $^1P$
430,256 *		45% ( $3^2P$ ) $^1P$	13% ( $3^4P$ ) $^3S$	10% ( $3^2D$ ) $^1P$
426,468	33	69% ( $3^4P$ ) $^3S$	10% ( $3^2D$ ) $^3P$	5% ( $3^4P$ ) $^3P$
419,422 *		33% ( $3^2D$ ) $^3P$	22% ( $3^2D$ ) $^1P$	11% ( $3^4P$ ) $^3S$
415,902 *		47% ( $3^4P$ ) $^3D$	27% ( $3^2P$ ) $^3S$	9% ( $3^2P$ ) $^3P$
413,344	47	33% ( $3^2P$ ) $^3P$	25% ( $3^4P$ ) $^3D$	22% ( $3^2P$ ) $^3S$
412,118	−9	55% ( $3^2D$ ) $^3D$	11% ( $3^2P$ ) $^3S$	7% ( $1^2D$ ) $^3D$
411,728 *		35% ( $3^2P$ ) $^1P$	13% ( $3^2D$ ) $^1P$	10% ( $3^2P$ ) $^3S$
404,530	9	54% ( $3^2P$ ) $^3D$	13% ( $3^4P$ ) $^3P$	9% ( $3^2P$ ) $^3S$
403,127 *		44% ( $3^4P$ ) $^3P$	30% ( $3^4P$ ) $^5D$	8% ( $3^2P$ ) $^3D$
399,869	32	16% ( $3^2P$ ) $^3P$	15% ( $3^2D$ ) $^3P$	14% ( $3^4P$ ) $^5P$
393,703 *		37% ( $3^4P$ ) $^5D$	23% ( $3^4P$ ) $^3P$	19% ( $3^4F$ ) $^5D$
391,283	81	72% ( $3^4P$ ) $^5P$	7% ( $3^2P$ ) $^3S$	6% ( $3^2P$ ) $^3P$
386,317	−2	53% ( $3^4F$ ) $^5F$	26% ( $3^4F$ ) $^3D$	7% ( $3^4P$ ) $^3D$
383,568	−48	64% ( $3^4F$ ) $^5D$	21% ( $3^4P$ ) $^5D$	6% ( $3^4F$ ) $^5F$
374,891	13	47% ( $3^4F$ ) $^3D$	36% ( $3^4F$ ) $^5F$	7% ( $3^4F$ ) $^3D$
$J = 2$				
457,523 *		59% ( $1^2D$ ) $^3P$	14% ( $3^2D$ ) $^3P$	12% ( $1^2D$ ) $^3D$
453,343	−75	36% ( $1^2D$ ) $^1D$	23% ( $1^2D$ ) $^3F$	12% ( $3^2F$ ) $^1D$
447,730	−20	31% ( $1^2D$ ) $^3F$	21% ( $3^2F$ ) $^1D$	10% ( $3^2D$ ) $^3F$
444,532	−36	44% ( $1^2D$ ) $^3D$	12% ( $1^2D$ ) $^3F$	12% ( $1^2D$ ) $^3P$
432,431	−90	54% ( $3^2F$ ) $^3D$	16% ( $1^2D$ ) $^3D$	11% ( $1^2D$ ) $^1D$
431,074 *		30% ( $1^2D$ ) $^1D$	26% ( $3^2F$ ) $^1D$	12% ( $3^2F$ ) $^3D$
424,635	−19	33% ( $3^2D$ ) $^1D$	26% ( $3^2P$ ) $^1D$	17% ( $3^2F$ ) $^3F$
421,941 *		26% ( $3^2F$ ) $^3F$	22% ( $3^2P$ ) $^1D$	12% ( $3^2P$ ) $^3P$
420,031	58	25% ( $3^2P$ ) $^3P$	22% ( $3^4P$ ) $^3D$	14% ( $3^2D$ ) $^3P$
417,758	31	26% ( $3^2D$ ) $^3D$	16% ( $3^2F$ ) $^3F$	16% ( $3^2P$ ) $^3P$
412,894	30	28% ( $3^4P$ ) $^3D$	21% ( $3^4P$ ) $^5S$	16% ( $3^2D$ ) $^3P$
412,412	−44	50% ( $3^2P$ ) $^3D$	18% ( $3^2G$ ) $^3F$	11% ( $3^2D$ ) $^3F$
411,461	−29	48% ( $3^4P$ ) $^5S$	20% ( $3^4P$ ) $^3P$	11% ( $3^2D$ ) $^3P$
409,522	−14	19% ( $3^2D$ ) $^3F$	15% ( $3^2F$ ) $^1D$	14% ( $3^2D$ ) $^1D$
408,409	−16	52% ( $3^2G$ ) $^3F$	12% ( $3^2P$ ) $^3D$	9% ( $3^2P$ ) $^1D$
406,270	−12	25% ( $3^2D$ ) $^3D$	23% ( $3^2P$ ) $^3P$	22% ( $3^2D$ ) $^3P$
402,086 *		25% ( $3^4P$ ) $^3P$	23% ( $3^4P$ ) $^5D$	16% ( $3^4P$ ) $^5P$
400,904	31	23% ( $3^4P$ ) $^5D$	21% ( $3^4F$ ) $^3F$	16% ( $3^2D$ ) $^3F$
396,041	59	36% ( $3^4P$ ) $^5P$	18% ( $3^4P$ ) $^5D$	15% ( $3^4F$ ) $^5D$
394,552 *		52% ( $3^4F$ ) $^3F$	8% ( $3^2D$ ) $^3F$	7% ( $3^4F$ ) $^5G$
393,630	−4	34% ( $3^4P$ ) $^5P$	27% ( $3^4P$ ) $^3P$	13% ( $3^4F$ ) $^3D$
386,800	−9	55% ( $3^4F$ ) $^5F$	12% ( $3^4P$ ) $^3D$	5% ( $3^4P$ ) $^3D$
385,302	−69	55% ( $3^4F$ ) $^5D$	22% ( $3^4P$ ) $^5D$	5% ( $3^4F$ ) $^5F$
377,661	4	38% ( $3^4F$ ) $^3D$	33% ( $3^4F$ ) $^5F$	17% ( $3^4F$ ) $^5D$
371,899 *		86% ( $3^4F$ ) $^5G$	7% ( $3^4F$ ) $^3F$	3% ( $3^2D$ ) $^3F$

Table A8. Cont.

E <sup>a</sup>	o-c <sup>b</sup>	Eigenvector Composition <sup>c</sup>		
<i>J</i> = 3				
460,104	100	62% (1 <sup>2</sup> D) <sup>1</sup> F	15% (3 <sup>2</sup> D) <sup>1</sup> F	11% (1 <sup>2</sup> D) <sup>3</sup> F
452,808	172	41% (1 <sup>2</sup> D) <sup>3</sup> D	35% (1 <sup>2</sup> D) <sup>3</sup> F	9% (3 <sup>2</sup> D) <sup>3</sup> F
446,318	−13	33% (1 <sup>2</sup> D) <sup>3</sup> D	26% (1 <sup>2</sup> D) <sup>3</sup> F	13% (1 <sup>2</sup> D) <sup>1</sup> F
436,451	−25	74% (3 <sup>2</sup> F) <sup>1</sup> F	11% (3 <sup>2</sup> F) <sup>3</sup> D	5% (3 <sup>2</sup> F) <sup>3</sup> G
430,642	2	26% (3 <sup>2</sup> F) <sup>3</sup> D	19% (3 <sup>2</sup> F) <sup>3</sup> F	19% (3 <sup>2</sup> F) <sup>3</sup> G
427,542 *		21% (3 <sup>2</sup> H) <sup>3</sup> G	19% (3 <sup>2</sup> F) <sup>3</sup> D	18% (3 <sup>2</sup> F) <sup>3</sup> G
424,006	−25	24% (3 <sup>2</sup> P) <sup>3</sup> D	23% (3 <sup>2</sup> D) <sup>1</sup> F	11% (3 <sup>2</sup> G) <sup>1</sup> F
422,895	77	25% (3 <sup>2</sup> F) <sup>3</sup> F	22% (3 <sup>2</sup> D) <sup>3</sup> D	17% (3 <sup>2</sup> H) <sup>3</sup> G
420,123	36	24% (3 <sup>2</sup> F) <sup>3</sup> F	17% (3 <sup>4</sup> P) <sup>3</sup> D	11% (3 <sup>2</sup> P) <sup>3</sup> D
417,724	43	24% (3 <sup>2</sup> H) <sup>3</sup> G	23% (3 <sup>2</sup> F) <sup>3</sup> G	16% (3 <sup>4</sup> P) <sup>3</sup> D
415,165	114	24% (3 <sup>4</sup> P) <sup>3</sup> D	14% (3 <sup>2</sup> G) <sup>1</sup> F	10% (3 <sup>2</sup> H) <sup>3</sup> G
411,469	−67	24% (3 <sup>2</sup> D) <sup>3</sup> D	18% (3 <sup>2</sup> P) <sup>3</sup> D	15% (3 <sup>2</sup> F) <sup>3</sup> D
409,750	−9	25% (3 <sup>2</sup> G) <sup>1</sup> F	13% (3 <sup>2</sup> D) <sup>1</sup> F	11% (3 <sup>2</sup> D) <sup>3</sup> F
409,432	−14	31% (3 <sup>2</sup> D) <sup>3</sup> F	20% (3 <sup>2</sup> G) <sup>3</sup> F	15% (3 <sup>2</sup> D) <sup>3</sup> D
407,506	39	23% (3 <sup>2</sup> G) <sup>3</sup> F	22% (3 <sup>2</sup> G) <sup>3</sup> F	11% (3 <sup>4</sup> F) <sup>3</sup> F
402,520 *		62% (3 <sup>4</sup> P) <sup>5</sup> D	11% (3 <sup>4</sup> F) <sup>3</sup> D	8% (3 <sup>2</sup> P) <sup>3</sup> D
399,399	46	72% (3 <sup>4</sup> P) <sup>5</sup> P	9% (3 <sup>4</sup> F) <sup>3</sup> D	5% (3 <sup>2</sup> P) <sup>3</sup> D
398,704	20	35% (3 <sup>2</sup> G) <sup>3</sup> G	21% (3 <sup>2</sup> G) <sup>1</sup> F	16% (3 <sup>4</sup> F) <sup>3</sup> G
397,779	1	59% (3 <sup>4</sup> F) <sup>3</sup> F	7% (3 <sup>2</sup> D) <sup>3</sup> F	6% (3 <sup>4</sup> P) <sup>5</sup> P
390,887	−10	29% (3 <sup>4</sup> F) <sup>5</sup> F	21% (3 <sup>4</sup> F) <sup>3</sup> D	18% (3 <sup>4</sup> F) <sup>3</sup> G
389,944	−8	31% (3 <sup>4</sup> F) <sup>3</sup> G	15% (3 <sup>4</sup> F) <sup>3</sup> D	14% (3 <sup>4</sup> F) <sup>5</sup> D
387,329	−2	34% (3 <sup>4</sup> F) <sup>5</sup> F	25% (3 <sup>4</sup> F) <sup>5</sup> D	19% (3 <sup>4</sup> F) <sup>3</sup> G
381,580	−5	40% (3 <sup>4</sup> F) <sup>5</sup> D	29% (3 <sup>4</sup> F) <sup>5</sup> F	21% (3 <sup>4</sup> F) <sup>3</sup> D
375,456 *		87% (3 <sup>4</sup> F) <sup>5</sup> G	5% (3 <sup>4</sup> F) <sup>3</sup> F	2% (3 <sup>4</sup> F) <sup>3</sup> G
<i>J</i> = 4				
455,261	29	77% (1 <sup>2</sup> D) <sup>3</sup> F	15% (3 <sup>2</sup> D) <sup>3</sup> F	3% (3 <sup>2</sup> F) <sup>1</sup> G
437,322	112	61% (3 <sup>2</sup> F) <sup>1</sup> G	28% (3 <sup>2</sup> H) <sup>1</sup> G	6% (3 <sup>2</sup> F) <sup>3</sup> G
431,659 *		48% (3 <sup>2</sup> F) <sup>3</sup> G	25% (3 <sup>2</sup> F) <sup>3</sup> F	18% (3 <sup>2</sup> H) <sup>3</sup> G
424,999	1	47% (3 <sup>2</sup> F) <sup>3</sup> F	13% (3 <sup>2</sup> H) <sup>3</sup> G	11% (3 <sup>2</sup> F) <sup>3</sup> G
420,822	37	35% (3 <sup>2</sup> H) <sup>3</sup> G	16% (3 <sup>2</sup> F) <sup>3</sup> G	14% (3 <sup>2</sup> G) <sup>3</sup> F
417,492	−62	67% (3 <sup>2</sup> D) <sup>3</sup> F	10% (1 <sup>2</sup> D) <sup>3</sup> F	7% (3 <sup>4</sup> F) <sup>3</sup> F
412,977	6	22% (3 <sup>2</sup> F) <sup>1</sup> G	17% (3 <sup>2</sup> G) <sup>1</sup> G	13% (3 <sup>2</sup> F) <sup>3</sup> G
412,041	−47	33% (3 <sup>2</sup> H) <sup>1</sup> G	28% (3 <sup>2</sup> G) <sup>1</sup> G	13% (3 <sup>2</sup> H) <sup>3</sup> G
408,236	37	30% (3 <sup>4</sup> P) <sup>5</sup> D	14% (3 <sup>2</sup> H) <sup>3</sup> H	13% (3 <sup>2</sup> G) <sup>3</sup> H
407,173	−50	57% (3 <sup>4</sup> P) <sup>5</sup> D	14% (3 <sup>2</sup> G) <sup>3</sup> F	9% (3 <sup>2</sup> H) <sup>3</sup> H
405,162	−21	52% (3 <sup>2</sup> G) <sup>3</sup> G	16% (3 <sup>2</sup> G) <sup>3</sup> F	13% (3 <sup>2</sup> H) <sup>3</sup> H
400,219	−10	58% (3 <sup>4</sup> F) <sup>3</sup> F	18% (3 <sup>2</sup> G) <sup>3</sup> F	3% (3 <sup>2</sup> H) <sup>3</sup> G
399,265	14	34% (3 <sup>2</sup> G) <sup>1</sup> G	18% (3 <sup>2</sup> G) <sup>3</sup> H	13% (3 <sup>2</sup> H) <sup>3</sup> H
396,481	18	43% (3 <sup>4</sup> F) <sup>3</sup> G	19% (3 <sup>2</sup> H) <sup>3</sup> H	18% (3 <sup>2</sup> G) <sup>3</sup> H
393,193	−2	34% (3 <sup>4</sup> F) <sup>5</sup> F	32% (3 <sup>2</sup> G) <sup>3</sup> H	11% (3 <sup>2</sup> H) <sup>3</sup> H
388,964	4	33% (3 <sup>4</sup> F) <sup>5</sup> F	23% (3 <sup>4</sup> F) <sup>3</sup> G	16% (3 <sup>4</sup> F) <sup>5</sup> G
385,218	−11	67% (3 <sup>4</sup> F) <sup>5</sup> D	15% (3 <sup>4</sup> F) <sup>5</sup> F	6% (3 <sup>4</sup> F) <sup>3</sup> F
379,386 *		80% (3 <sup>4</sup> F) <sup>5</sup> G	7% (3 <sup>4</sup> F) <sup>3</sup> G	6% (3 <sup>4</sup> F) <sup>5</sup> F
<i>J</i> = 5				
432,154	32	85% (3 <sup>2</sup> F) <sup>3</sup> G	13% (3 <sup>2</sup> H) <sup>3</sup> G	1% (3 <sup>2</sup> G) <sup>1</sup> H
421,021	4	45% (3 <sup>2</sup> H) <sup>3</sup> G	16% (3 <sup>2</sup> G) <sup>1</sup> H	13% (3 <sup>2</sup> H) <sup>1</sup> H
415,995	−15	52% (3 <sup>2</sup> H) <sup>1</sup> H	24% (3 <sup>2</sup> G) <sup>3</sup> G	17% (3 <sup>2</sup> H) <sup>3</sup> I
413,329	57	61% (3 <sup>2</sup> G) <sup>1</sup> H	20% (3 <sup>2</sup> H) <sup>3</sup> G	10% (3 <sup>2</sup> H) <sup>3</sup> I
408,910	1	54% (3 <sup>2</sup> G) <sup>3</sup> H	31% (3 <sup>2</sup> H) <sup>3</sup> H	9% (3 <sup>2</sup> G) <sup>3</sup> G
407,246	−19	38% (3 <sup>2</sup> H) <sup>3</sup> I	36% (3 <sup>2</sup> G) <sup>3</sup> G	8% (3 <sup>2</sup> H) <sup>3</sup> G
405,144	26	26% (3 <sup>2</sup> H) <sup>3</sup> H	23% (3 <sup>2</sup> H) <sup>1</sup> H	11% (3 <sup>2</sup> H) <sup>3</sup> I
399,831	−1	47% (3 <sup>4</sup> F) <sup>3</sup> G	23% (3 <sup>4</sup> F) <sup>5</sup> F	16% (3 <sup>2</sup> H) <sup>3</sup> H
395,955	−2	32% (3 <sup>4</sup> F) <sup>5</sup> F	22% (3 <sup>2</sup> G) <sup>3</sup> H	16% (3 <sup>2</sup> H) <sup>3</sup> I
390,458	−6	40% (3 <sup>4</sup> F) <sup>5</sup> G	28% (3 <sup>4</sup> F) <sup>5</sup> F	18% (3 <sup>4</sup> F) <sup>3</sup> G
383,426	−48	58% (3 <sup>4</sup> F) <sup>5</sup> G	15% (3 <sup>4</sup> F) <sup>3</sup> G	13% (3 <sup>4</sup> F) <sup>5</sup> F

Table A8. Cont.

E <sup>a</sup>	o-c <sup>b</sup>	Eigenvector Composition <sup>c</sup>		
<i>J</i> = 6				
421,189	52	67% (3 <sup>2</sup> H) <sup>1</sup> I	19% (3 <sup>2</sup> G) <sup>3</sup> H	7% (3 <sup>2</sup> H) <sup>3</sup> I
413,999	−7	66% (3 <sup>2</sup> H) <sup>3</sup> I	24% (3 <sup>2</sup> H) <sup>3</sup> H	5% (3 <sup>2</sup> H) <sup>1</sup> I
410,851	20	57% (3 <sup>2</sup> G) <sup>3</sup> H	25% (3 <sup>2</sup> H) <sup>1</sup> I	14% (3 <sup>2</sup> H) <sup>3</sup> H
403,359	−13	55% (3 <sup>2</sup> H) <sup>3</sup> H	25% (3 <sup>2</sup> H) <sup>3</sup> I	14% (3 <sup>2</sup> G) <sup>3</sup> H
391,512 *		94% (3 <sup>4</sup> F) <sup>5</sup> G	6% (3 <sup>2</sup> G) <sup>3</sup> H	
<i>J</i> = 7				
417,658	−35	100% (3 <sup>2</sup> H) <sup>3</sup> I		

<sup>a</sup> The star \* indicates a calculated value for the level; <sup>b</sup> The difference between the observed and the calculated energies; <sup>c</sup> For the eigenvector composition, up to three components with the largest percentages in the LS-coupling scheme are listed. The number preceding the terms is the seniority number.

Table A9. Energies (in cm<sup>−1</sup>) of the 4d<sup>3</sup>4f + 4p<sup>5</sup>4d<sup>5</sup> configurations of Ag VIII.

E <sup>a</sup>	o-c <sup>b</sup>	<i>J</i>	Eigenvector Composition <sup>c</sup>		
557,732	258	1	24% 4d <sup>3</sup> 4f (4F) <sup>5</sup> D	20% 4p <sup>5</sup> 4d <sup>5</sup> (4F) <sup>5</sup> D	10% 4p <sup>5</sup> 4d <sup>5</sup> (4D) <sup>5</sup> D
557,962 *		4	40% 4p <sup>5</sup> 4d <sup>5</sup> (2G1) <sup>3</sup> H	10% 4p <sup>5</sup> 4d <sup>5</sup> (2D1) <sup>3</sup> F	6% 4p <sup>5</sup> 4d <sup>5</sup> (2F2) <sup>3</sup> G
558,654	182	1	22% 4p <sup>5</sup> 4d <sup>5</sup> (4G) <sup>5</sup> F	18% 4d <sup>3</sup> 4f (4F) <sup>5</sup> F	17% 4d <sup>3</sup> 4f (4P) <sup>5</sup> F
560,251	257	2	31% 4d <sup>3</sup> 4f (4F) <sup>5</sup> D	27% 4p <sup>5</sup> 4d <sup>5</sup> (4F) <sup>5</sup> D	13% 4p <sup>5</sup> 4d <sup>5</sup> (4D) <sup>5</sup> D
560,857	186	2	27% 4p <sup>5</sup> 4d <sup>5</sup> (4G) <sup>5</sup> F	21% 4d <sup>3</sup> 4f (4F) <sup>5</sup> F	20% 4d <sup>3</sup> 4f (4P) <sup>5</sup> F
560,877 *		4	24% 4p <sup>5</sup> 4d <sup>5</sup> (2D1) <sup>3</sup> F	13% 4p <sup>5</sup> 4d <sup>5</sup> (2D3) <sup>3</sup> F	11% 4p <sup>5</sup> 4d <sup>5</sup> (2G1) <sup>3</sup> F
562,295	122	3	21% 4d <sup>3</sup> 4f (4F) <sup>5</sup> D	21% 4p <sup>5</sup> 4d <sup>5</sup> (4F) <sup>5</sup> D	13% 4p <sup>5</sup> 4d <sup>5</sup> (4G) <sup>5</sup> F
562,825	92	3	14% 4p <sup>5</sup> 4d <sup>5</sup> (4G) <sup>5</sup> F	10% 4d <sup>3</sup> 4f (4F) <sup>5</sup> F	9% 4d <sup>3</sup> 4f (4F) <sup>5</sup> F
564,383	−53	4	20% 4p <sup>5</sup> 4d <sup>5</sup> (4F) <sup>5</sup> D	17% 4d <sup>3</sup> 4f (4F) <sup>5</sup> D	16% 4p <sup>5</sup> 4d <sup>5</sup> (4G) <sup>5</sup> F
565,233 *		3	14% 4p <sup>5</sup> 4d <sup>5</sup> (2D1) <sup>3</sup> F	11% 4p <sup>5</sup> 4d <sup>5</sup> (2D1) <sup>3</sup> F	9% 4d <sup>3</sup> 4f (2D1) <sup>1</sup> F
564,902	−365	4	14% 4p <sup>5</sup> 4d <sup>5</sup> (4G) <sup>5</sup> F	13% 4p <sup>5</sup> 4d <sup>5</sup> (4F) <sup>5</sup> D	10% 4d <sup>3</sup> 4f (4F) <sup>5</sup> F
565,427	−49	5	17% 4p <sup>5</sup> 4d <sup>5</sup> (4G) <sup>5</sup> F	10% 4d <sup>3</sup> 4f (4F) <sup>5</sup> F	9% 4d <sup>3</sup> 4f (4P) <sup>5</sup> F
567,115	119	7	21% 4d <sup>3</sup> 4f (2H) <sup>1</sup> K	18% 4d <sup>3</sup> 4f (4F) <sup>3</sup> I	15% 4d <sup>3</sup> 4f (2H) <sup>3</sup> I
568,319	12	5	15% 4d <sup>3</sup> 4f (4F) <sup>3</sup> I	13% 4p <sup>5</sup> 4d <sup>5</sup> (2I) <sup>3</sup> I	13% 4p <sup>5</sup> 4d <sup>5</sup> (4G) <sup>5</sup> F
568,352 *		2	26% 4p <sup>5</sup> 4d <sup>5</sup> (2P) <sup>3</sup> D	14% 4p <sup>5</sup> 4d <sup>5</sup> (2D1) <sup>3</sup> D	10% 4p <sup>5</sup> 4d <sup>5</sup> (2D1) <sup>3</sup> F
569,385	138	6	22% 4d <sup>3</sup> 4f (4F) <sup>3</sup> I	18% 4p <sup>5</sup> 4d <sup>5</sup> (2I) <sup>3</sup> F	18% 4d <sup>3</sup> 4f (2H) <sup>3</sup> I
571,903 *		1	38% 4p <sup>5</sup> 4d <sup>5</sup> (2P) <sup>3</sup> P	20% 4p <sup>5</sup> 4d <sup>5</sup> (2D1) <sup>3</sup> P	18% 4p <sup>5</sup> 4d <sup>5</sup> (2D3) <sup>3</sup> P
573,036	−36	4	17% 4d <sup>3</sup> 4f (4F) <sup>3</sup> H	11% 4p <sup>5</sup> 4d <sup>5</sup> (2H) <sup>3</sup> H	8% 4d <sup>3</sup> 4f (2G) <sup>3</sup> H
576,375 *		1	20% 4p <sup>5</sup> 4d <sup>5</sup> (2F2) <sup>3</sup> D	10% 4d <sup>3</sup> 4f (2P) <sup>3</sup> D	10% 4d <sup>3</sup> 4f (2D2) <sup>3</sup> D
576,746	−170	5	17% 4d <sup>3</sup> 4f (4F) <sup>3</sup> H	10% 4p <sup>5</sup> 4d <sup>5</sup> (2H) <sup>3</sup> H	8% 4d <sup>3</sup> 4f (2G) <sup>3</sup> H
577,085	−795	3	14% 4p <sup>5</sup> 4d <sup>5</sup> (2H) <sup>3</sup> G	12% 4d <sup>3</sup> 4f (2G) <sup>3</sup> G	11% 4p <sup>5</sup> 4d <sup>5</sup> (2G2) <sup>3</sup> G
578,963	209	7	29% 4d <sup>3</sup> 4f (2H) <sup>1</sup> K	18% 4d <sup>3</sup> 4f (2G) <sup>1</sup> K	14% 4p <sup>5</sup> 4d <sup>5</sup> (2I) <sup>1</sup> K
578,767 *		2	21% 4p <sup>5</sup> 4d <sup>5</sup> (2P) <sup>3</sup> P	15% 4p <sup>5</sup> 4d <sup>5</sup> (2D1) <sup>3</sup> P	12% 4p <sup>5</sup> 4d <sup>5</sup> (2D2) <sup>3</sup> P
579,661 *		1	36% 4p <sup>5</sup> 4d <sup>5</sup> (2P) <sup>3</sup> D	11% 4p <sup>5</sup> 4d <sup>5</sup> (2D1) <sup>3</sup> D	7% 4d <sup>3</sup> 4f (2D1) <sup>3</sup> D
580,373 *		3	15% 4p <sup>5</sup> 4d <sup>5</sup> (2D2) <sup>1</sup> F	15% 4p <sup>5</sup> 4d <sup>5</sup> (2D1) <sup>3</sup> F	8% 4d <sup>3</sup> 4f (2D2) <sup>1</sup> F
580,680 *		2	13% 4p <sup>5</sup> 4d <sup>5</sup> (2F2) <sup>3</sup> D	9% 4d <sup>3</sup> 4f (2P) <sup>3</sup> D	6% 4p <sup>5</sup> 4d <sup>5</sup> (2F1) <sup>3</sup> D
580,568 *		0	39% 4p <sup>5</sup> 4d <sup>5</sup> (2P) <sup>3</sup> P	20% 4p <sup>5</sup> 4d <sup>5</sup> (2D3) <sup>3</sup> P	12% 4p <sup>5</sup> 4d <sup>5</sup> (2P) <sup>1</sup> S
581,094 *		1	32% 4d <sup>3</sup> 4f (2D1) <sup>1</sup> P	19% 4d <sup>3</sup> 4f (2D2) <sup>1</sup> P	12% 4p <sup>5</sup> 4d <sup>5</sup> (2P) <sup>1</sup> P
580,923	−221	6	22% 4d <sup>3</sup> 4f (4F) <sup>3</sup> H	14% 4p <sup>5</sup> 4d <sup>5</sup> (2G) <sup>3</sup> H	14% 4p <sup>5</sup> 4d <sup>5</sup> (2H) <sup>3</sup> H
581,306	22	4	11% 4p <sup>5</sup> 4d <sup>5</sup> (2G2) <sup>3</sup> G	11% 4d <sup>3</sup> 4f (4P) <sup>3</sup> G	7% 4d <sup>3</sup> 4f (2G) <sup>3</sup> G
582,024	−42	5	13% 4d <sup>3</sup> 4f (4P) <sup>3</sup> G	11% 4p <sup>5</sup> 4d <sup>5</sup> (2G2) <sup>3</sup> G	7% 4d <sup>3</sup> 4f (2G) <sup>3</sup> G
582,154	−19	1	30% 4p <sup>5</sup> 4d <sup>5</sup> (6S) <sup>5</sup> P	10% 4d <sup>3</sup> 4f (4F) <sup>5</sup> P	10% 4p <sup>5</sup> 4d <sup>5</sup> (4P) <sup>3</sup> S
583,603	46	3	15% 4p <sup>5</sup> 4d <sup>5</sup> (2G1) <sup>3</sup> F	10% 4d <sup>3</sup> 4f (2D2) <sup>3</sup> F	10% 4p <sup>5</sup> 4d <sup>5</sup> (4F) <sup>3</sup> F
585,291 *		3	10% 4p <sup>5</sup> 4d <sup>5</sup> (2D2) <sup>3</sup> D	9% 4p <sup>5</sup> 4d <sup>5</sup> (2F2) <sup>3</sup> D	6% 4d <sup>3</sup> 4f (2G) <sup>3</sup> D
587,262 *		2	10% 4p <sup>5</sup> 4d <sup>5</sup> (2P) <sup>3</sup> D	9% 4p <sup>5</sup> 4d <sup>5</sup> (2D1) <sup>3</sup> F	7% 4p <sup>5</sup> 4d <sup>5</sup> (2G1) <sup>3</sup> F
589,229	−70	4	12% 4p <sup>5</sup> 4d <sup>5</sup> (2I) <sup>3</sup> H	8% 4d <sup>3</sup> 4f (2H) <sup>3</sup> H	5% 4p <sup>5</sup> 4d <sup>5</sup> (4F) <sup>3</sup> G
589,963	238	2	12% 4p <sup>5</sup> 4d <sup>5</sup> (2D1) <sup>3</sup> F	10% 4p <sup>5</sup> 4d <sup>5</sup> (2D1) <sup>3</sup> P	8% 4p <sup>5</sup> 4d <sup>5</sup> (2D2) <sup>3</sup> D



Table A9. Cont.

E <sup>a</sup>	o-c <sup>b</sup>	J	Eigenvector Composition <sup>c</sup>		
589,786	-107	4	9% 4p <sup>5</sup> 4d <sup>5</sup> (2H) <sup>3</sup> G	4% 4p <sup>5</sup> 4d <sup>5</sup> (2I) <sup>3</sup> H	4% 4d <sup>3</sup> 4f (2D2) <sup>1</sup> G
590,761 *		1	9% 4p <sup>5</sup> 4d <sup>5</sup> (2D2) <sup>3</sup> D	8% 4p <sup>5</sup> 4d <sup>5</sup> (2F1) <sup>3</sup> D	8% 4p <sup>5</sup> 4d <sup>5</sup> (2D2) <sup>1</sup> P
591,056 *		2	13% 4p <sup>5</sup> 4d <sup>5</sup> (2D1) <sup>3</sup> F	11% 4p <sup>5</sup> 4d <sup>5</sup> (2G2) <sup>3</sup> F	8% 4p <sup>5</sup> 4d <sup>5</sup> (2G1) <sup>3</sup> F
591,442	124	3	17% 4p <sup>5</sup> 4d <sup>5</sup> (4F) <sup>3</sup> G	6% 4d <sup>3</sup> 4f (4F) <sup>3</sup> G	6% 4p <sup>5</sup> 4d <sup>5</sup> (4G) <sup>3</sup> G
591,781 *		1	11% 4p <sup>5</sup> 4d <sup>5</sup> (6S) <sup>5</sup> P	11% 4p <sup>5</sup> 4d <sup>5</sup> (2D1) <sup>3</sup> P	7% 4p <sup>5</sup> 4d <sup>5</sup> (4D) <sup>3</sup> P
592,118	-49	5	9% 4p <sup>5</sup> 4d <sup>5</sup> (2H) <sup>1</sup> H	9% 4d <sup>3</sup> 4f (2G) <sup>1</sup> H	8% 4d <sup>3</sup> 4f (2D1) <sup>3</sup> G
593,449 *		2	19% 4p <sup>5</sup> 4d <sup>5</sup> (6S) <sup>5</sup> P	6% 4p <sup>5</sup> 4d <sup>5</sup> (2D2) <sup>3</sup> F	6% 4p <sup>5</sup> 4d <sup>5</sup> (2D1) <sup>3</sup> P
593,578 *		0	17% 4p <sup>5</sup> 4d <sup>5</sup> (4P) <sup>3</sup> P	16% 4p <sup>5</sup> 4d <sup>5</sup> (2D1) <sup>3</sup> P	15% 4p <sup>5</sup> 4d <sup>5</sup> (4D) <sup>3</sup> P
593,064	-698	3	15% 4p <sup>5</sup> 4d <sup>5</sup> (2F1) <sup>3</sup> D	11% 4p <sup>5</sup> 4d <sup>5</sup> (4D) <sup>3</sup> D	11% 4d <sup>3</sup> 4f (2P) <sup>3</sup> D
594,881	-367	2	27% 4p <sup>5</sup> 4d <sup>5</sup> (6S) <sup>5</sup> P	8% 4p <sup>5</sup> 4d <sup>5</sup> (4D) <sup>5</sup> P	8% 4p <sup>5</sup> 4d <sup>5</sup> (4P) <sup>5</sup> P
596,171	-15	4	9% 4p <sup>5</sup> 4d <sup>5</sup> (2I) <sup>3</sup> H	9% 4p <sup>5</sup> 4d <sup>5</sup> (2G2) <sup>1</sup> G	8% 4d <sup>3</sup> 4f (2H) <sup>3</sup> H
598,210	207	4	16% 4p <sup>5</sup> 4d <sup>5</sup> (4F) <sup>3</sup> G	7% 4p <sup>5</sup> 4d <sup>5</sup> (2G2) <sup>3</sup> G	6% 4p <sup>5</sup> 4d <sup>5</sup> (2F1) <sup>1</sup> G
598,784 *		3	17% 4p <sup>5</sup> 4d <sup>5</sup> (2G1) <sup>3</sup> G	15% 4d <sup>3</sup> 4f (2D1) <sup>3</sup> G	5% 4p <sup>5</sup> 4d <sup>5</sup> (2F2) <sup>3</sup> D
599,018	15	1	11% 4p <sup>5</sup> 4d <sup>5</sup> (2P) <sup>3</sup> S	10% 4d <sup>3</sup> 4f (2I) <sup>3</sup> S	9% 4p <sup>5</sup> 4d <sup>5</sup> (2S) <sup>3</sup> P
599,345	109	5	15% 4p <sup>5</sup> 4d <sup>5</sup> (4F) <sup>3</sup> G	10% 4p <sup>5</sup> 4d <sup>5</sup> (2I) <sup>3</sup> H	8% 4p <sup>5</sup> 4d <sup>5</sup> (2G2) <sup>3</sup> G
602,225	723	4	8% 4p <sup>5</sup> 4d <sup>5</sup> (4F) <sup>3</sup> F	7% 4p <sup>5</sup> 4d <sup>5</sup> (2G2) <sup>1</sup> G	7% 4d <sup>3</sup> 4f (2F) <sup>1</sup> G
601,789 *		2	11% 4p <sup>5</sup> 4d <sup>5</sup> (2D3) <sup>3</sup> P	8% 4d <sup>3</sup> 4f (2F) <sup>3</sup> P	7% 4p <sup>5</sup> 4d <sup>5</sup> (4P) <sup>3</sup> P
602,116 *		3	9% 4p <sup>5</sup> 4d <sup>5</sup> (4F) <sup>3</sup> G	8% 4d <sup>3</sup> 4f (2G) <sup>3</sup> F	8% 4p <sup>5</sup> 4d <sup>5</sup> (2G2) <sup>3</sup> F
603,864	132	5	20% 4d <sup>3</sup> 4f (2D1) <sup>1</sup> H	11% 4p <sup>5</sup> 4d <sup>5</sup> (2I) <sup>3</sup> H	9% 4p <sup>5</sup> 4d <sup>5</sup> (2G1) <sup>1</sup> H
604,385	-19	4	24% 4p <sup>5</sup> 4d <sup>5</sup> (2G1) <sup>3</sup> G	13% 4d <sup>3</sup> 4f (2D1) <sup>3</sup> G	7% 4d <sup>3</sup> 4f (2H) <sup>3</sup> G
604,600	3	3	43% 4p <sup>5</sup> 4d <sup>5</sup> (6S) <sup>5</sup> P	12% 4p <sup>5</sup> 4d <sup>5</sup> (4D) <sup>5</sup> P	9% 4p <sup>5</sup> 4d <sup>5</sup> (4P) <sup>5</sup> P
605,132	-102	6	25% 4p <sup>5</sup> 4d <sup>5</sup> (2I) <sup>3</sup> H	14% 4p <sup>5</sup> 4d <sup>5</sup> (2I) <sup>1</sup> I	13% 4p <sup>5</sup> 4d <sup>5</sup> (4G) <sup>3</sup> H
606,529	91	5	17% 4p <sup>5</sup> 4d <sup>5</sup> (4G) <sup>3</sup> G	16% 4p <sup>5</sup> 4d <sup>5</sup> (4F) <sup>3</sup> G	8% 4d <sup>3</sup> 4f (4F) <sup>3</sup> G
607,167 *		1	16% 4p <sup>5</sup> 4d <sup>5</sup> (2P) <sup>3</sup> S	14% 4p <sup>5</sup> 4d <sup>5</sup> (4P) <sup>3</sup> S	6% 4p <sup>5</sup> 4d <sup>5</sup> (2D3) <sup>1</sup> P
607,348 *		2	16% 4p <sup>5</sup> 4d <sup>5</sup> (4D) <sup>3</sup> P	9% 4p <sup>5</sup> 4d <sup>5</sup> (2D1) <sup>3</sup> P	7% 4p <sup>5</sup> 4d <sup>5</sup> (4P) <sup>3</sup> P
607,709 *		0	27% 4p <sup>5</sup> 4d <sup>5</sup> (2P) <sup>3</sup> P	20% 4p <sup>5</sup> 4d <sup>5</sup> (2S) <sup>3</sup> P	19% 4d <sup>3</sup> 4f (2F) <sup>3</sup> P
608,132 *		1	12% 4p <sup>5</sup> 4d <sup>5</sup> (2D2) <sup>1</sup> P	10% 4p <sup>5</sup> 4d <sup>5</sup> (2D2) <sup>3</sup> D	6% 4d <sup>3</sup> 4f (2G) <sup>3</sup> D
607,628	-663	3	10% 4p <sup>5</sup> 4d <sup>5</sup> (2F2) <sup>3</sup> D	10% 4p <sup>5</sup> 4d <sup>5</sup> (2F1) <sup>1</sup> F	8% 4d <sup>3</sup> 4f (2F) <sup>1</sup> F
613,166	-109	4	12% 4p <sup>5</sup> 4d <sup>5</sup> (4G) <sup>3</sup> F	9% 4p <sup>5</sup> 4d <sup>5</sup> (2F2) <sup>1</sup> G	7% 4d <sup>3</sup> 4f (2G) <sup>1</sup> G
614,370	76	5	19% 4p <sup>5</sup> 4d <sup>5</sup> (2G1) <sup>1</sup> H	13% 4p <sup>5</sup> 4d <sup>5</sup> (2G1) <sup>3</sup> G	6% 4p <sup>5</sup> 4d <sup>5</sup> (2I) <sup>1</sup> H
615,653 *		3	11% 4p <sup>5</sup> 4d <sup>5</sup> (2D1) <sup>3</sup> D	8% 4p <sup>5</sup> 4d <sup>5</sup> (4D) <sup>3</sup> D	7% 4p <sup>5</sup> 4d <sup>5</sup> (2F1) <sup>3</sup> D
615,971 *		1	19% 4p <sup>5</sup> 4d <sup>5</sup> (4D) <sup>3</sup> D	16% 4p <sup>5</sup> 4d <sup>5</sup> (2D3) <sup>3</sup> D	11% 4p <sup>5</sup> 4d <sup>5</sup> (4P) <sup>3</sup> D
616,249 *		2	11% 4p <sup>5</sup> 4d <sup>5</sup> (4D) <sup>3</sup> D	11% 4p <sup>5</sup> 4d <sup>5</sup> (2D2) <sup>1</sup> D	11% 4p <sup>5</sup> 4d <sup>5</sup> (2D3) <sup>3</sup> D
617,860 *		1	34% 4p <sup>5</sup> 4d <sup>5</sup> (2D1) <sup>3</sup> D	7% 4d <sup>3</sup> 4f (2D1) <sup>3</sup> D	6% 4d <sup>3</sup> 4f (2D2) <sup>1</sup> P
619,061 *		2	26% 4p <sup>5</sup> 4d <sup>5</sup> (2D1) <sup>3</sup> D	11% 4p <sup>5</sup> 4d <sup>5</sup> (4P) <sup>3</sup> D	9% 4d <sup>3</sup> 4f (2D1) <sup>3</sup> D
620,379 *		3	15% 4p <sup>5</sup> 4d <sup>5</sup> (4G) <sup>3</sup> F	13% 4p <sup>5</sup> 4d <sup>5</sup> (4D) <sup>3</sup> F	5% 4p <sup>5</sup> 4d <sup>5</sup> (4G) <sup>3</sup> G
620,664	128	2	13% 4p <sup>5</sup> 4d <sup>5</sup> (4G) <sup>3</sup> F	10% 4p <sup>5</sup> 4d <sup>5</sup> (2F1) <sup>1</sup> D	9% 4p <sup>5</sup> 4d <sup>5</sup> (2D3) <sup>1</sup> D
621,268	-115	6	41% 4p <sup>5</sup> 4d <sup>5</sup> (2I) <sup>1</sup> I	16% 4p <sup>5</sup> 4d <sup>5</sup> (2I) <sup>3</sup> H	11% 4d <sup>3</sup> 4f (2H) <sup>1</sup> I
622,060	-146	4	20% 4p <sup>5</sup> 4d <sup>5</sup> (4D) <sup>3</sup> F	12% 4p <sup>5</sup> 4d <sup>5</sup> (4G) <sup>3</sup> G	8% 4p <sup>5</sup> 4d <sup>5</sup> (2G1) <sup>3</sup> F
622,489 *		3	15% 4p <sup>5</sup> 4d <sup>5</sup> (4D) <sup>3</sup> D	9% 4p <sup>5</sup> 4d <sup>5</sup> (4P) <sup>3</sup> D	7% 4p <sup>5</sup> 4d <sup>5</sup> (4G) <sup>3</sup> G
624,693 *		2	15% 4p <sup>5</sup> 4d <sup>5</sup> (2D2) <sup>1</sup> D	10% 4p <sup>5</sup> 4d <sup>5</sup> (2P) <sup>1</sup> D	8% 4p <sup>5</sup> 4d <sup>5</sup> (4P) <sup>3</sup> D
627,779	-430	3	12% 4p <sup>5</sup> 4d <sup>5</sup> (4P) <sup>3</sup> D	11% 4p <sup>5</sup> 4d <sup>5</sup> (2G2) <sup>1</sup> F	8% 4p <sup>5</sup> 4d <sup>5</sup> (2F2) <sup>1</sup> F
630,389	405	3	14% 4p <sup>5</sup> 4d <sup>5</sup> (2D3) <sup>1</sup> F	11% 4p <sup>5</sup> 4d <sup>5</sup> (4G) <sup>3</sup> G	11% 4p <sup>5</sup> 4d <sup>5</sup> (2F1) <sup>1</sup> F
630,848 *		2	14% 4p <sup>5</sup> 4d <sup>5</sup> (2P) <sup>1</sup> D	10% 4p <sup>5</sup> 4d <sup>5</sup> (2F2) <sup>1</sup> D	7% 4p <sup>5</sup> 4d <sup>5</sup> (4G) <sup>3</sup> F
634,810	230	4	33% 4p <sup>5</sup> 4d <sup>5</sup> (4G) <sup>3</sup> G	8% 4p <sup>5</sup> 4d <sup>5</sup> (4F) <sup>3</sup> G	8% 4p <sup>5</sup> 4d <sup>5</sup> (4G) <sup>3</sup> F
635,050	-166	3	22% 4p <sup>5</sup> 4d <sup>5</sup> (4G) <sup>3</sup> G	11% 4p <sup>5</sup> 4d <sup>5</sup> (2F2) <sup>1</sup> F	7% 4p <sup>5</sup> 4d <sup>5</sup> (2F1) <sup>1</sup> F
635,935	510	5	41% 4p <sup>5</sup> 4d <sup>5</sup> (4G) <sup>3</sup> G	18% 4p <sup>5</sup> 4d <sup>5</sup> (2H) <sup>3</sup> G	13% 4p <sup>5</sup> 4d <sup>5</sup> (4F) <sup>3</sup> G
635,583 *		1	29% 4p <sup>5</sup> 4d <sup>5</sup> (2D3) <sup>1</sup> P	15% 4p <sup>5</sup> 4d <sup>5</sup> (2I) <sup>1</sup> H	6% 4p <sup>5</sup> 4d <sup>5</sup> (2D3) <sup>3</sup> D
636,245 *		1	39% 4p <sup>5</sup> 4d <sup>5</sup> (4P) <sup>3</sup> S	21% 4p <sup>5</sup> 4d <sup>5</sup> (2P) <sup>3</sup> S	8% 4d <sup>3</sup> 4f (2F) <sup>3</sup> S
641,516	56	2	16% 4p <sup>5</sup> 4d <sup>5</sup> (4F) <sup>3</sup> F	7% 4p <sup>5</sup> 4d <sup>5</sup> (4F) <sup>3</sup> D	5% 4p <sup>5</sup> 4d <sup>5</sup> (4D) <sup>3</sup> P
643,491 *		3	18% 4p <sup>5</sup> 4d <sup>5</sup> (4F) <sup>3</sup> D	11% 4p <sup>5</sup> 4d <sup>5</sup> (2D1) <sup>3</sup> D	9% 4p <sup>5</sup> 4d <sup>5</sup> (2D1) <sup>1</sup> F
644,043	065	5	28% 4p <sup>5</sup> 4d <sup>5</sup> (2H) <sup>1</sup> H	26% 4p <sup>5</sup> 4d <sup>5</sup> (2I) <sup>1</sup> H	21% 4p <sup>5</sup> 4d <sup>5</sup> (2G2) <sup>1</sup> H
643,939	-245	4	18% 4p <sup>5</sup> 4d <sup>5</sup> (2H) <sup>1</sup> G	15% 4p <sup>5</sup> 4d <sup>5</sup> (4F) <sup>3</sup> F	13% 4p <sup>5</sup> 4d <sup>5</sup> (2G1) <sup>1</sup> G
644,760 *		1	25% 4p <sup>5</sup> 4d <sup>5</sup> (4D) <sup>3</sup> P	10% 4p <sup>5</sup> 4d <sup>5</sup> (2D2) <sup>3</sup> P	9% 4p <sup>5</sup> 4d <sup>5</sup> (4F) <sup>3</sup> D

Table A9. Cont.

E <sup>a</sup>	o-c <sup>b</sup>	J	Eigenvector Composition <sup>c</sup>		
645,906	221	2	15% 4p <sup>5</sup> 4d <sup>5</sup> ( <sup>2</sup> D2) <sup>1</sup> D	11% 4p <sup>5</sup> 4d <sup>5</sup> ( <sup>2</sup> D1) <sup>1</sup> D	7% 4d <sup>3</sup> 4f ( <sup>2</sup> D1) <sup>1</sup> D
646,185	348	2	11% 4p <sup>5</sup> 4d <sup>5</sup> ( <sup>4</sup> D) <sup>3</sup> P	9% 4p <sup>5</sup> 4d <sup>5</sup> ( <sup>4</sup> F) <sup>3</sup> F	7% 4p <sup>5</sup> 4d <sup>5</sup> ( <sup>2</sup> D2) <sup>3</sup> P
647,898 *		0	40% 4p <sup>5</sup> 4d <sup>5</sup> ( <sup>4</sup> D) <sup>3</sup> P	14% 4p <sup>5</sup> 4d <sup>5</sup> ( <sup>2</sup> D2) <sup>3</sup> P	10% 4p <sup>5</sup> 4d <sup>5</sup> ( <sup>4</sup> F) <sup>3</sup> P
647,982	30	3	22% 4p <sup>5</sup> 4d <sup>5</sup> ( <sup>4</sup> F) <sup>3</sup> F	12% 4p <sup>5</sup> 4d <sup>5</sup> ( <sup>4</sup> F) <sup>3</sup> D	5% 4p <sup>5</sup> 4d <sup>5</sup> ( <sup>2</sup> G1) <sup>3</sup> F
650,256	171	4	19% 4p <sup>5</sup> 4d <sup>5</sup> ( <sup>4</sup> F) <sup>3</sup> F	13% 4p <sup>5</sup> 4d <sup>5</sup> ( <sup>2</sup> G1) <sup>1</sup> G	11% 4p <sup>5</sup> 4d <sup>5</sup> ( <sup>2</sup> G1) <sup>3</sup> F
650,545	-375	2	23% 4p <sup>5</sup> 4d <sup>5</sup> ( <sup>4</sup> F) <sup>3</sup> D	7% 4p <sup>5</sup> 4d <sup>5</sup> ( <sup>2</sup> P) <sup>3</sup> D	5% 4p <sup>5</sup> 4d <sup>5</sup> ( <sup>4</sup> F) <sup>3</sup> F
651,358 *		3	18% 4p <sup>5</sup> 4d <sup>5</sup> ( <sup>2</sup> F1) <sup>1</sup> F	15% 4p <sup>5</sup> 4d <sup>5</sup> ( <sup>2</sup> G2) <sup>1</sup> F	14% 4p <sup>5</sup> 4d <sup>5</sup> ( <sup>2</sup> D1) <sup>1</sup> F
664,590 *		1	40% 4p <sup>5</sup> 4d <sup>5</sup> ( <sup>2</sup> P) <sup>1</sup> P	15% 4p <sup>5</sup> 4d <sup>5</sup> ( <sup>2</sup> D1) <sup>1</sup> P	9% 4d <sup>3</sup> 4f ( <sup>2</sup> D1) <sup>1</sup> P
668,708	-344	3	32% 4p <sup>5</sup> 4d <sup>5</sup> ( <sup>2</sup> G1) <sup>1</sup> F	15% 4p <sup>5</sup> 4d <sup>5</sup> ( <sup>2</sup> D2) <sup>1</sup> F	13% 4p <sup>5</sup> 4d <sup>5</sup> ( <sup>2</sup> F2) <sup>1</sup> F

<sup>a</sup> The star \* indicates a calculated value for the level; <sup>b</sup> The difference between the observed and the calculated energies; <sup>c</sup> For the eigenvector composition, up to three components with the largest percentages in the LS-coupling scheme are listed. The number following the terms displays Nielson and Koster sequential indices [20].

Table A10. Energies (in cm<sup>-1</sup>) of the 4d<sup>3</sup> configuration of Ag IX.

E <sup>a</sup>	o-c <sup>b</sup>	Eigenvector Composition <sup>c</sup>		
<i>J</i> = 1/2				
28,502 *		87% <sup>2</sup> P	13% <sup>4</sup> P	
17,851 *		87% <sup>4</sup> P	13% <sup>2</sup> P	
<i>J</i> = 3/2				
68,707	48	76% <sup>2</sup> D1	24% <sup>2</sup> D2	
36,360	-6	57% <sup>2</sup> P	27% <sup>2</sup> D2	10% <sup>2</sup> D1
26,823	24	41% <sup>2</sup> D2	25% <sup>4</sup> P	20% <sup>2</sup> P
17,169	56	69% <sup>4</sup> P	23% <sup>2</sup> P	5% <sup>2</sup> D2
0	12	95% <sup>4</sup> F	3% <sup>2</sup> D2	1% <sup>2</sup> D1
<i>J</i> = 5/2				
68,249	-22	83% <sup>2</sup> D1	12% <sup>2</sup> D2	3% <sup>2</sup> F
44,595	-41	96% <sup>2</sup> F	2% <sup>2</sup> D1	2% <sup>2</sup> D2
33,051	10	84% <sup>2</sup> D2	12% <sup>2</sup> D1	2% <sup>4</sup> P
22,387	-10	97% <sup>4</sup> P	2% <sup>2</sup> D1	1% <sup>2</sup> D2
3103	0	98% <sup>4</sup> F	1% <sup>2</sup> D2	0% <sup>2</sup> D1
<i>J</i> = 7/2				
44,082	-3	98% <sup>2</sup> F	1% <sup>2</sup> G	0% <sup>4</sup> F
22,160	-24	96% <sup>2</sup> G	2% <sup>4</sup> F	1% <sup>2</sup> F
6532	4	97% <sup>4</sup> F	2% <sup>2</sup> G	0% <sup>2</sup> F
<i>J</i> = 9/2				
32,349	19	57% <sup>2</sup> H	41% <sup>2</sup> G	2% <sup>4</sup> F
23,357	-22	50% <sup>2</sup> G	43% <sup>2</sup> H	7% <sup>4</sup> F
9867	-13	91% <sup>4</sup> F	8% <sup>2</sup> G	1% <sup>2</sup> H
<i>J</i> = 11/2				
31,532	15	100% <sup>2</sup> H		

<sup>a</sup> The star \* indicates a calculated value for the level; <sup>b</sup> The difference between the observed and the calculated by orthogonal parameter technique energies; <sup>c</sup> For the eigenvector composition, up to three components with the largest percentages in the LS-coupling scheme are listed. The number following the terms displays Nielson and Koster sequential indices [20].

**Table A11.** Energies (in  $\text{cm}^{-1}$ ) of the  $4d^25p + 4d^24f + 4p^54d^4$  configurations of Ag IX.

$E^a$	$o-c^b$	$J$	Config. $c$	Eigenvector Composition $d$		
424,571	90	5/2	$4d^25p$	71% $4d^25p\ (^3F)^4G$	17% $4d^25p\ (^3F)^2F$	7% $4d^25p\ (^1D)^2F$
427,386 *		7/2	$4p^54d^4$	81% $4p^54d^4\ (^3D)^6D$	11% $4p^54d^4\ (^3D)^6F$	6% $4p^54d^4\ (^3D)^6P$
427,916	-112	3/2	$4d^25p$	61% $4d^25p\ (^3F)^4F$	25% $4d^25p\ (^3F)^2D$	7% $4d^25p\ (^3F)^4D$
428,156 *		5/2	$4p^54d^4$	78% $4p^54d^4\ (^3D)^6D$	9% $4p^54d^4\ (^3D)^6P$	8% $4p^54d^4\ (^3D)^6F$
428,306 *		9/2	$4p^54d^4$	85% $4p^54d^4\ (^3D)^6D$	12% $4p^54d^4\ (^3D)^6F$	1% $4p^54d^4\ (^3D)^6P$
430,308 *		3/2	$4p^54d^4$	76% $4p^54d^4\ (^3D)^6D$	9% $4p^54d^4\ (^3D)^6P$	5% $4p^54d^4\ (^3D)^6F$
431,109 *		7/2	$4d^25p$	77% $4d^25p\ (^3F)^4G$	9% $4d^25p\ (^3F)^4F$	9% $4d^25p\ (^3F)^2F$
432,569	157	5/2	$4d^25p$	56% $4d^25p\ (^3F)^4F$	16% $4d^25p\ (^3F)^2D$	16% $4d^25p\ (^3F)^4D$
433,690 *		1/2	$4p^54d^4$	84% $4p^54d^4\ (^3D)^6D$	6% $4p^54d^4\ (^3D)^6P$	4% $4p^54d^4\ (^3D)^6F$
437,442	34	9/2	$4d^25p$	58% $4d^25p\ (^3F)^4G$	25% $4d^25p\ (^3F)^4F$	11% $4d^25p\ (^3F)^2G$
437,662	68	7/2	$4d^25p$	49% $4d^25p\ (^3F)^4D$	35% $4d^25p\ (^3F)^4D$	6% $4d^25p\ (^3F)^2S$
437,662	-478	1/2	$4d^25p$	53% $4d^25p\ (^3F)^4F$	27% $4d^25p\ (^3F)^2D$	10% $4d^25p\ (^3F)^2F$
438,297	-107	5/2	$4d^25p$	29% $4d^25p\ (^3F)^4F$	22% $4d^25p\ (^3F)^4G$	22% $4d^25p\ (^3F)^2F$
438,725	-103	3/2	$4d^25p$	36% $4d^25p\ (^3F)^4D$	28% $4d^25p\ (^3F)^4F$	14% $4d^25p\ (^3F)^2D$
440,957 *		3/2	$4d^25p$	25% $4d^25p\ (^3F)^4D$	25% $4d^25p\ (^3F)^2D$	18% $4d^25p\ (^3F)^2D$
441,473 *		1/2	$4d^25p$	73% $4d^25p\ (^3F)^2S$	15% $4d^25p\ (^3F)^4P$	6% $4d^25p\ (^3F)^4D$
441,637	-122	7/2	$4d^25p$	26% $4d^25p\ (^3F)^4D$	23% $4d^25p\ (^3F)^2F$	20% $4d^25p\ (^3F)^4F$
442,423	120	5/2	$4d^25p$	46% $4d^25p\ (^3F)^4D$	25% $4d^25p\ (^3F)^4D$	13% $4d^25p\ (^1D)^2F$
444,195	220	9/2	$4d^25p$	43% $4d^25p\ (^3F)^4F$	41% $4d^25p\ (^3F)^4G$	10% $4d^25p\ (^3F)^2G$
444,319 *		1/2	$4p^54d^4$	92% $4p^54d^4\ (^3D)^6F$	5% $4p^54d^4\ (^3F)^4G$	1% $4p^54d^4\ (^3F)^4G$
444,355 *		3/2	$4d^25p$	50% $4d^25p\ (^3F)^4S$	15% $4d^25p\ (^1D)^2P$	6% $4d^25p\ (^3F)^4D$
445,529 *		5/2	$4p^54d^4$	41% $4p^54d^4\ (^3H)^4G$	32% $4d^24f\ (^3F)^4G$	10% $4p^54d^4\ (^3G)^4G$
446,642	-4	5/2	$4d^25p$	41% $4d^25p\ (^3F)^2F$	20% $4d^25p\ (^3F)^2D$	18% $4d^25p\ (^3F)^2D$
447,243 *		7/2	$4d^25p$	43% $4d^25p\ (^3F)^2G$	18% $4d^25p\ (^1G)^2G$	10% $4d^25p\ (^3F)^4F$
447,255	-279	7/2	$4p^54d^4$	33% $4p^54d^4\ (^3H)^4G$	30% $4d^24f\ (^3F)^4G$	11% $4p^54d^4\ (^3G)^4G$
447,694 *		11/2	$4d^25p$	97% $4d^25p\ (^3F)^4G$	1% $4d^25p\ (^1G)^2H$	1% $4d^24f\ (^3F)^4G$
448,369 *		7/2	$4d^24f$	32% $4d^24f\ (^3F)^2G$	10% $4p^54d^4\ (^3H)^2G$	8% $4d^25p\ (^3F)^2G$
448,623 *		3/2	$4p^54d^4$	28% $4p^54d^4\ (^3P)^2S$	11% $4d^25p\ (^1D)^2P$	8% $4p^54d^4\ (^3P)^2P$
448,989	232	7/2	$4d^25p$	31% $4d^25p\ (^3F)^2F$	22% $4d^25p\ (^3F)^4D$	12% $4d^25p\ (^3F)^4D$
448,995 *		1/2	$4d^25p$	54% $4d^25p\ (^3F)^4D$	36% $4d^25p\ (^3F)^4D$	3% $4d^25p\ (^3P)^2P$
449,006 *		9/2	$4p^54d^4$	16% $4p^54d^4\ (^3D)^6F$	16% $4d^24f\ (^3F)^4G$	14% $4p^54d^4\ (^3H)^4G$
450,334 *		3/2	$4p^54d^4$	16% $4p^54d^4\ (^3G)^4F$	12% $4d^24f\ (^3F)^4F$	10% $4p^54d^4\ (^3F)^24D$
451,183	-53	3/2	$4d^25p$	31% $4d^25p\ (^3F)^4S$	23% $4d^25p\ (^1D)^2P$	13% $4d^25p\ (^1D)^2D$
451,424 *		9/2	$4p^54d^4$	28% $4p^54d^4\ (^3D)^6F$	14% $4p^54d^4\ (^3H)^4G$	13% $4d^24f\ (^3F)^4G$
451,430 *		5/2	$4p^54d^4$	17% $4p^54d^4\ (^3D)^6F$	16% $4p^54d^4\ (^3F)^24D$	12% $4p^54d^4\ (^3D)^6P$
451,946 *		7/2	$4p^54d^4$	41% $4p^54d^4\ (^3F)^24D$	12% $4p^54d^4\ (^3D)^4D$	12% $4p^54d^4\ (^3D)^4D$
452,041 *		1/2	$4p^54d^4$	28% $4p^54d^4\ (^3D)^6F$	11% $4p^54d^4\ (^3F)^24D$	9% $4p^54d^4\ (^3D)^6P$
452,292	198	9/2	$4d^25p$	22% $4d^25p\ (^1G)^2G$	21% $4d^25p\ (^3F)^4F$	18% $4d^25p\ (^3F)^2G$
452,569	249	5/2	$4d^25p$	59% $4d^25p\ (^1D)^2F$	12% $4d^25p\ (^3F)^2F$	11% $4d^25p\ (^3F)^2D$
452,857 *		3/2	$4d^25p$	28% $4d^25p\ (^3F)^4D$	15% $4d^25p\ (^3F)^4D$	11% $4d^25p\ (^3D)^6P$
452,951 *		9/2	$4p^54d^4$	21% $4p^54d^4\ (^3D)^6F$	20% $4d^24f\ (^3F)^2G$	8% $4p^54d^4\ (^3H)^2G$
453,404 *		3/2	$4d^25p$	24% $4d^25p\ (^3F)^4D$	13% $4p^54d^4\ (^3G)^4F$	11% $4d^25p\ (^3F)^4D$
453,632 *		11/2	$4p^54d^4$	26% $4d^24f\ (^3F)^4G$	22% $4p^54d^4\ (^3H)^4G$	17% $4p^54d^4\ (^3F)^24G$
453,902	-209	7/2	$4d^25p$	52% $4d^25p\ (^1G)^2G$	14% $4d^25p\ (^1D)^2F$	11% $4d^25p\ (^3F)^2G$
454,133 *		5/2	$4p^54d^4$	27% $4p^54d^4\ (^3G)^4F$	12% $4d^24f\ (^3F)^4F$	10% $4p^54d^4\ (^3F)^24D$
455,093 *		7/2	$4p^54d^4$	13% $4p^54d^4\ (^3F)^24D$	13% $4p^54d^4\ (^3D)^6F$	13% $4p^54d^4\ (^3G)^4F$
455,362 *		3/2	$4p^54d^4$	31% $4p^54d^4\ (^3D)^6P$	18% $4p^54d^4\ (^3D)^4P$	15% $4p^54d^4\ (^3F)^24D$
455,506 *		5/2	$4p^54d^4$	20% $4p^54d^4\ (^3P)^4P$	15% $4d^24f\ (^3F)^4P$	10% $4p^54d^4\ (^3P)^24D$
457,009 *		1/2	$4d^25p$	50% $4d^25p\ (^1D)^2P$	39% $4d^25p\ (^3F)^4P$	5% $4d^25p\ (^3F)^4D$
457,621	41	5/2	$4d^25p$	49% $4d^25p\ (^3F)^4D$	19% $4d^25p\ (^3F)^4D$	12% $4d^25p\ (^3F)^2D$
457,734 *		7/2	$4d^24f$	80% $4d^24f\ (^3F)^4H$	3% $4p^54d^4\ (^3G)^4H$	3% $4p^54d^4\ (^3H)^4G$
457,900	111	9/2	$4d^25p$	52% $4d^25p\ (^3F)^2G$	33% $4d^25p\ (^1G)^2G$	10% $4d^25p\ (^1G)^2H$
457,882 *		9/2	$4p^54d^4$	22% $4d^24f\ (^3F)^4H$	9% $4d^24f\ (^3F)^4I$	9% $4p^54d^4\ (^3H)^4H$
458,434 *		1/2	$4d^24f$	26% $4d^24f\ (^3F)^2S$	18% $4p^54d^4\ (^3D)^4P$	16% $4d^24f\ (^3F)^4P$
458,503 *		9/2	$4d^24f$	34% $4d^24f\ (^3F)^4H$	33% $4d^24f\ (^3F)^4I$	7% $4d^24f\ (^1D)^2H$
458,762 *		11/2	$4p^54d^4$	39% $4d^24f\ (^3F)^4H$	23% $4p^54d^4\ (^3H)^4H$	15% $4p^54d^4\ (^3G)^4H$
459,044 *		7/2	$4p^54d^4$	19% $4d^24f\ (^3F)^4F$	16% $4p^54d^4\ (^3D)^6F$	15% $4p^54d^4\ (^3P)^24D$
459,146	-45	3/2	$4d^25p$	59% $4d^25p\ (^3F)^4P$	11% $4d^25p\ (^1D)^2P$	9% $4d^25p\ (^1D)^2D$
460,347 *		13/2	$4p^54d^4$	31% $4d^24f\ (^3F)^4H$	23% $4p^54d^4\ (^3H)^4H$	22% $4p^54d^4\ (^3G)^4H$
460,559	-65	7/2	$4d^25p$	37% $4d^25p\ (^3P)^4D$	15% $4d^25p\ (^3F)^2F$	15% $4d^25p\ (^3F)^4D$
460,753 *		5/2	$4p^54d^4$	11% $4p^54d^4\ (^3F)^24F$	11% $4d^24f\ (^3F)^2F$	11% $4d^24f\ (^3F)^4F$
460,784 *		9/2	$4d^24f$	25% $4p^54d^4\ (^3D)^4F$	20% $4d^24f\ (^3F)^4I$	13% $4d^24f\ (^3F)^4H$
460,974 *		11/2	$4d^24f$	57% $4d^24f\ (^3F)^4I$	13% $4d^24f\ (^3F)^4H$	7% $4p^54d^4\ (^3H)^4I$





**Table A12.** Energy parameters (in  $\text{cm}^{-1}$ ) of the ground configuration in Ag VII, Ag VIII and Ag IX calculated by orthogonal parameter technique in comparison with the Dirac-Fock (DF) parameters.

Name	AgVII ( $4d^5$ )				AgVIII ( $4d^4$ )				AgIX ( $4d^3$ )			
	FIT	Error <sup>a</sup>	DF	FIT/DF	FIT	Error <sup>a</sup>	DF	FIT/DF	FIT	Error <sup>a</sup>	DF	FIT/DF
E <sub>av</sub>	51914	3	60,863	0.853	37,710	6	42,776	0.882	27,795	8	31,440	0.884
O2	8652	2	10,175	0.850	8978	6	10,515	0.854	9295	8	10,834	0.858
O2'	5512	3	6923	0.796	5701	7	7128	0.800	5892	8	7323	0.805
Ea'	213	2			223	3			251	6		
Eb'	38	2			45	6			50	f		
ζ	2493	2	2428	1.027	2655	5	2603	1.020	2830	7	2782	1.017
T1	-4.62	0.08			-4.62	0.19			-4.85	0.36		
T2	0.40	f			0.50	f						
Ac	7.80	1.5	13.21	0.6	7.46	f	12.43	0.6	7.08	f	11.81	0.6
A3	1.93	r	3.27	0.6	1.90	f	3.18	0.6	1.87	f	3.13	0.6
A4	3.28	r	5.56	0.6	3.31	f	5.52	0.6	3.32	f	5.53	0.6
A5	3.16	r	5.36	0.6	3.31	f	5.51	0.6	3.42	f	5.71	0.6
A6	0.96	r	1.63	0.6	0.47	f	0.78	0.6	0.00	f	-0.00	1.0
A1	-0.10	r	-0.16	0.6	-0.05	f	-0.08	0.6	0	f	0	0.6
A2	-0.32	r	-0.55	0.6	-0.43	f	-0.72	0.6	-0.53	f	-0.88	0.6
A0	-0.49	r	0.29	0.6	-0.28	f	-0.46	0.6	-0.25	f	-0.42	0.6
σ	14				26				27			

<sup>a</sup> r—parameters are fixed at DF ratio to Ac, f- fixed parameter.

**Table A13.** Energy parameters (in  $\text{cm}^{-1}$ ) of the  $4d^45p$  configuration in Ag VII and  $4d^35p$  configuration in Ag VIII calculated by orthogonal parameter technique in comparison with the DF parameters.

Name	Ag VII				Ag VIII			
	FIT	Error <sup>a</sup>	DF	FIT/DF	FIT	Error <sup>b</sup>	DF	FIT/DF
E <sub>av</sub>	37,3862	2	384,168	0.973	41,1052	5	417,702	0.984
O2dd	8849	2	10,418	0.849	9147	8	10,738	0.852
O2'dd	5581	4	7070	0.789	5747	12	7265	0.791
Ea'	216	1			221	6		
Eb'	36	3			31	6		
T1	-4.86	0.09			-5.08	0		
T2	0.48	0.09			0.50	f		
ζ(4d)	2631	4	2572	1.023	2809	8	2747	1.022
Ac	8.01	1.8	12.68	0.63	11.76	f	11.76	1.0
A3	1.97	r1	3.12	0.63	3.44	f	3.44	1.0
A4	3.25	r1	5.15	0.63	5.40	f	5.40	1.0
A5	3.46	r1	5.48	0.63	5.68	f	5.68	1.0
A6	0.64	r1	1.02	0.62	0.18	f	0.18	1.0
A1	-0.17	r1	-0.28	0.63	-0.23	f	-0.23	1.0
A2	-0.63	r1	-1.00	0.63	-0.35	f	-0.35	1.0
A0	-0.69	r1	-1.10	0.63	-0.18	f	-0.19	1.0
C1dp	3702	4	4270	0.867	4012	11	4621	0.868
C2dp	2605	3	2998	0.869	2755	10	3176	0.867
C3dp	1258	4	1411	0.891	1321	10	1471	0.898
S1dp	67	3			63	8		
S2dp	-118	3			-129	8		
ζ(5p)	6317	5	5975	1.057	7268	14	6933	1.048
Sd.Lp	-27.49	1.5	-34.81	0.79	-27.2	f	-34.04	0.8
Sp.Ld	-2.77	r2	-3.52	0.79	-2.7	f	-3.46	0.8
Zp2ppa	-19.98	r2	-25.29	0.79	-20.0	f	-25.01	0.8
Zp2dda	13.74	r2	17.42	0.79	13.5	f	16.93	0.8
Zp1ppa	41.56	r2	52.62	0.79	41.2	f	51.56	0.8
Zp1dda	-2.94	r2	-3.71	0.79	-2.3	f	-2.99	0.8
Zp3ppa	10.85	r2	13.74	0.79	11.0	f	13.81	0.8
Zp3dda	-2.22	r2	-2.82	0.79	-2.3	f	-2.95	0.8
SS(dp)02	-1.53	r2	-1.95	0.79	-1.8	f	-2.32	0.8
SS(dp)20	-0.52	r2	-0.66	0.79	-0.3	f	-0.40	0.8

Table A13. Cont.

Name	Ag VII				Ag VIII			
	FIT	Error <sup>a</sup>	DF	FIT/DF	FIT	Error <sup>b</sup>	DF	FIT/DF
t16'	-23.8	2.8			-23.8	f		
t17'	8.0	2.8			8.0	f		
t18'	-10.4	2.9			-10.4	f		
t19'	-8.9	2.1			-8.9	f		
t20'	-42.2	3.6			-42.2	f		
t21'	-3.4	2.3			-3.4	f		
t22'	-14.4	4.6			-14.4	f		
t23'	-4.2	3.9			-4.2	f		
t24'	-7.5	2.9			-7.5	f		
t25'	3.6	2.5			3.6	f		
t26'	-33.5	3.0			-33.5	f		
t27'	18.5	2.4			18.5	f		
t28'	35.6	3.5			35.6	f		
t29'	-12.1	2.5			-12.1	f		
t30'	-45.5	2.7			-45.5	f		
t31'	-4.4	3.0			-4.4	f		
t32'	-0.3	2.2			-0.3	f		
t33'	11.9	2.8			11.9	f		
t34'	-30.2	3.2			-30.2	f		
t35'	-32.3	3.4			-32.3	f		
$\sigma$	19				47			

<sup>a</sup> r1—parameters are fixed at DF ratio to Ac, r1 parameters are fixed at DF ratio to Sd.Lp; <sup>b</sup> f—parameter is fixed on predetermined value.

**Table A14.** Fitted (FIT) with their uncertainties (Unc.) and Hartree - Fock (HF) energy parameters in  $\text{cm}^{-1}$  of the odd  $4d^35p$ ,  $4d^34f$ , and  $4p^54d^4$  configurations in Ag VIII and  $4d^25p$ ,  $4d^24f$  and  $4p^54d^3$  configurations in Ag IX calculated with the Cowan code.

Name <sup>a</sup>	Ag VIII				Ag IX			
	HF	FIT	Unc. <sup>b</sup>	FIT/HF <sup>c</sup>	HF	FIT	Unc. <sup>b</sup>	FIT/HF <sup>c</sup>
$E_{av}(5p)$	417,702	412,728	26	-4974	459,300	455,716	88	-3584
$F^2(4d,4d)$	95,978	80,972	237	0.844	98,603	83,046	1159	0.842
$F^4(4d,4d)$	64,366	56,750	484	0.882	66,314	54,364	3227	0.820
$\alpha$		49	5			71	26	
$\beta$		-627	-99			-600	f	
T1		-4	-1					
$\zeta(4d)$	2702	2812	36	1.041	2870	2919	65	1.017
$\zeta(5p)$	6510	7299	66	1.121	7426	8338	165	1.123
$F^1(4d,5p)$		-2072	-265			-2000	f	
$F^2(4d,5p)$	39,205	32,005	275	0.816	41,777	35,950	898	0.861
$G^1(4d,5p)$	12,359	10,505	137	0.850 <sup>d</sup>	12,926	11,649	342	0.901 <sup>d</sup>
$G^3(4d,5p)$	12,110	10,293	134	0.850 <sup>d</sup>	12,836	11,568	340	0.901 <sup>d</sup>
$E_{av}(4f)$	508,665	496,302	569	-12,363	522,389	507,990	380	-14,399
$F^2(4d,4d)$	95,126	80,381	f	0.845	97,640	80,359	f	0.823
$F^4(4d,4d)$	63,728	55,443	f	0.87	65,594	54,443	f	0.83
$\alpha$		48	f			62	f	
$\beta$		-600	f					
T1		-4	f					
$\zeta(4d)$	2652	2732	f	1.03	2808	2910	f	1.036
$\zeta(4f)$	95	95	f	1.0	124	124	f	1.0

Table A14. Cont.

Name <sup>a</sup>	Ag VIII				Ag IX			
	HF	FIT	Unc. <sup>b</sup>	FIT/HF <sup>c</sup>	HF	FIT	Unc. <sup>b</sup>	FIT/HF <sup>c</sup>
F <sup>2</sup> (4d,4f)	70,569	64,433	1452	0.913 <sup>d</sup>	78,433	71,374	f	0.91
F <sup>4</sup> (4d,4f)	44,636	40,755	919	0.913 <sup>d</sup>	50,344	45,814	f	0.91
G <sup>1</sup> (4d,4f)	83,516	72,648	572	0.87	93,840	85,394	f	0.91
G <sup>3</sup> (4d,4f)	51,477	47,876	377	0.930 <sup>d</sup>	58,481	53,218	f	0.91
G <sup>5</sup> (4d,4f)	36,169	33,640	265	0.930 <sup>d</sup>	41,276	37,562	f	0.91
E <sub>av</sub> (pd)	538,566	526,473	194	−12,093	529,361	52,3487	344	−5874
F <sup>2</sup> (4d,4d)	94,305	79,014	393	0.838	97,018	85,702	496	0.883
F <sup>4</sup> (4d,4d)	63,119	51,318	598	0.813	65,133	50,607	1080	0.777
α		48	f			60	f	
β		−600	f			−600	f	
T1		−4	f			−4	f	
ζ(4p)	29,355	29,355	f	1	30,239	30,576	415	1.011
ζ(4d)	2602	2849	f	1.095	2767	2782	116	1.005
F <sup>2</sup> (4p,4d)	100,314	83,916	1065	0.837	102,723	79,518	973	0.774
G <sup>1</sup> (4p,4d)	127,225	101,162	192	0.795 <sup>d</sup>	130,315	101,056	342	0.775 <sup>d</sup>
G <sup>3</sup> (4p,4d)	79,353	63097	120	0.795 <sup>d</sup>	81,523	63,219	214	0.775 <sup>d</sup>
σ		213				327		

<sup>a</sup> E<sub>av</sub>(5p), E<sub>av</sub>(4f) and E<sub>av</sub>(pd) stand for E<sub>av</sub>(4d<sup>k−1</sup>5p), E<sub>av</sub>(4d<sup>k−1</sup>4f) and E<sub>av</sub>(4p<sup>5</sup>4d<sup>k+1</sup>) for Ag VIII and Ag IX where k = 4 and 3, respectively; <sup>b</sup> f- parameter is fixed on predetermined value; <sup>c</sup> For E<sub>av</sub> the FIT-HF difference is listed; <sup>d</sup> Adjacent pairs of parameters are linked at their HF ratios.

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Article

# The Cu II Spectrum

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Academic Editor: James Babb

Received: 16 December 2016; Accepted: 8 February 2017; Published: 24 February 2017

**Abstract:** New wavelength measurements in the vacuum ultraviolet (VUV), ultraviolet and visible spectral regions have been combined with available literature data to refine and extend the description of the spectrum of singly ionized copper (Cu II). In the VUV region, we measured 401 lines using a concave grating spectrograph and photographic plates. In the UV and visible regions, we measured 276 lines using a Fourier-transform spectrometer. These new measurements were combined with previously unpublished data from the thesis of Ross, with accurate VUV grating measurements of Kaufman and Ward, and with less accurate older measurements of Shenstone to construct a comprehensive list of  $\approx 2440$  observed lines, from which we derived a revised set of 379 optimized energy levels, complemented with 89 additional levels obtained using series formulas. Among the 379 experimental levels, 29 are new. Intensities of all lines observed in different experiments have been reduced to the same uniform scale by using newly calculated transition probabilities ( $A$ -values). We combined our calculations with published measured and calculated  $A$ -values to provide a set of 555 critically evaluated transition probabilities with estimated uncertainties, 162 of which are less than 20%.

**Keywords:** atomic spectra; singly ionized copper; energy levels; wavelengths; Ritz standards; transition probabilities; critical compilation

## 1. Introduction

The spectrum of singly ionized copper, belonging to the Ni isoelectronic sequence, has a long history of research. The most significant contributions to the analysis were made by Shenstone [1] in 1936 and by Ross [2] in 1969. Interest in this spectrum was mainly due to the fact that it has a large number of sharp distinct lines in the vacuum ultraviolet (VUV) region, as well as an equally large number of lines in the ultraviolet (UV), visible, and infrared (IR) regions, from which accurate wavelengths of the VUV lines can be established using the Ritz combination principle, thus providing a large set of lines usable as secondary VUV wavelength standards. This spectrum is also of considerable interest for astrophysics. Lines of Cu II were observed in the spectra of nebulae by Thackeray [3], Aller et al. [4], McKenna et al. [5], and by Wallerstein et al. [6], and also in interstellar H I clouds, as well as in Ap, Be, and Bp stars (Jaschek, and Jaschek [7], Danezis and Theodossiou [8]) and in the Sun (Samain [9]). Cu<sup>+</sup> was successfully used as an active lasing medium in various hollow cathodes. Continuous-wave or pulsed lasing has been reported for 28 lines of Cu II in a wide range from UV to IR (McNeil et al. [10,11], Jain [12], Zinchenko and Ivanov [13]). Since copper is an important impurity in tokamaks, the Cu II spectrum has potential applications in fusion research, where its lines can be used for diagnostic purposes.

For several decades after the original analysis by Shenstone [1] the VUV wavelengths of Cu II calculated from the energy levels (i.e., Ritz wavelengths) were widely used as auxiliary wavelength standards. After the refinements of the measured UV wavelengths by Reader et al. [14] and by Kaufman and Ward [15], and after improved and greatly extended measurements by Ross [2] in the UV and visible ranges, the quality of the VUV Ritz wavelengths of Cu II seemed to be so good that

no further investigations of this spectrum were needed. The only inconvenience stemmed from the fact that Ross's thesis [2] was never published, although a large part of it was released with small modifications as a report of the Los Alamos National Laboratory, see Ross [16]. Energy levels and a few strongest lines from Ross [2] were included in the compilations by Sugar and Musgrove [17] and by Sansonetti and Martin [18], but the bulk of the wavelength and line intensity data remains nearly inaccessible. Thus, the initial goal of the present work was simply to digitize Ross's line lists and include them in the Atomic Spectra Database (ASD; see Kramida et al. [19]) of the National Institute of Standards and Technology (NIST) with consistent energy-level identifications. However, a close examination revealed several problems with Ross's data.

The first problem is with internal consistency of Ross's data. An important aspect of ASD is that it requires the observed wavelengths for an atom to be consistent with the energy levels tabulated for that atom. That is, the wavelengths derived from the energy levels (Ritz wavelengths) must agree with the observed wavelengths to within the stated uncertainties. However, in attempting to incorporate the data of Ross into ASD, we found that for a large number of lines the differences between observed and Ritz wavelengths were much greater than the uncertainties. We decided that, because of the importance of Ritz wavelengths for Cu II, this had to be investigated.

The second problem with Ross's data is the possible presence of systematic shifts in his wavelengths. Nave and Sansonetti [20] showed that Ritz wavelengths below 2400 Å (41667 cm<sup>-1</sup>) derived from Ross's Cu II energy levels are systematically too low, the mean relative deviation being about  $4 \times 10^{-7}$ . This error is significantly greater than the average relative uncertainty of Ritz wavenumbers given by Ross,  $1.2 \times 10^{-7}$ . Near 2000 Å (50000 cm<sup>-1</sup>), it corresponds to an error of 0.02 cm<sup>-1</sup>, compared to the mean stated uncertainty of 0.006 cm<sup>-1</sup>. This puts the usability of Ross's Ritz wavenumbers in the VUV into question.

The third problem is the absence of a consistent description of line intensities throughout the entire range of observed wavelengths. While Ross's own measurements cover the large range above 1980 Å, most of the observed intensities in the VUV region are furnished by old measurements of Shenstone [1], which were made with seven different instruments and with two different light sources. Additional measurements for some selections of strongest lines were made by Reader et al. [14] and by Kaufman and Ward [15], each with their own intensity scale.

Finally, Ross's theoretical interpretation of the energy levels, adopted by Sugar and Musgrove [17] and by Sansonetti and Martin [18], is inadequate. Ross used the *LS* coupling scheme in his analysis, as well as in his final level list. However, the observed fine-structure intervals indicate that the level structure of most configurations is best described by the *J<sub>1</sub>l* (a.k.a. *JK*) coupling scheme, similar to the isoelectronic Ni I spectrum interpreted by Litzén et al. [21].

Another problem that needs to be addressed is the scarcity of available critically evaluated data on radiative transition probabilities (*A*-values). At present, the NIST ASD [19] includes only seven *A*-values of Cu II from the compilation of Wiese and Martin [22]. All of them have large estimated uncertainties ( $\leq 40\%$  for six transitions and  $\leq 50\%$  for one transition).

The main purpose of the present work is to solve the above-mentioned problems and construct a self-consistent set of recommended energy levels and wavelengths of Cu II supplemented with a uniform description of line intensities. Re-interpretation of the energy levels, as well as the search for possible classifications of previously unidentified lines, required new calculations, which necessarily produce radiative transition probabilities (*A*-values). Thus, we also critically evaluate all available data on *A*-values and extend them with our calculated ones found to be of substantially good accuracy.

The usability of the Cu II wavelengths as standards is limited by substantial hyperfine structure (HFS) splitting and presence of two stable isotopes, <sup>63</sup>Cu (69.15%) and <sup>65</sup>Cu (30.85%) in natural copper (Coursey et al. [23]). HFS and isotope shifts (IS) of a few tens of Cu II lines between 2218 Å and 8096 Å were first observed and roughly estimated by Shenstone [1] and then more accurately investigated by Elbel et al. [24,25]. The measured IS was in the range (0.001 to 0.101) cm<sup>-1</sup>. For singly-excited 3d<sup>9</sup>*nl* configurations the IS is smaller than 0.05 cm<sup>-1</sup>, while for the doubly-excited 4d<sup>8</sup>4s<sup>2</sup> configuration

it is about  $0.1 \text{ cm}^{-1}$ . The HFS constants  $A_{\text{hfs}}$  for several  $[3d^9]4s$ ,  $4p$ ,  $4d$ ,  $5s$ ,  $5p$ ,  $5d$ ,  $6s$  and  $[3d^8]4s^2$  and  $4s5p$  levels were found to range from  $0.022 \text{ cm}^{-1}$  to  $0.075 \text{ cm}^{-1}$  except for one level,  $3d^9 4s^3 D_1$ , having a very small  $A_{\text{hfs}} = -0.004 \text{ cm}^{-1}$ . The nuclear spin  $I$  of both  $^{63}\text{Cu}$  and  $^{65}\text{Cu}$  is  $I = 3/2$  [18]. Thus, depending on the total angular momentum  $J$  of the levels, the width of the HFS varies between  $0.016 \text{ cm}^{-1}$  and  $0.5 \text{ cm}^{-1}$ . The ionization energy of  $\text{Cu}^+$  is  $163669.2 \text{ cm}^{-1}$  ( $20.29239 \text{ eV}$ ) (Ross [2]). Thus, excitation of this spectrum requires temperatures in excess of  $6000 \text{ K}$  ( $0.5 \text{ eV}$ ). Such temperatures lead to Doppler broadening  $\Delta\sigma_{\text{Dop}}/\sigma > 4 \times 10^{-6}$ , resulting in line widths  $>0.4 \text{ cm}^{-1}$  at wavelengths near  $1000 \text{ \AA}$ ,  $0.2 \text{ cm}^{-1}$  near  $2000 \text{ \AA}$ , and  $0.1 \text{ cm}^{-1}$  near  $4000 \text{ \AA}$ . As a result, most observed lines possess unresolved or partially resolved HFS and IS. The smallness of HFS and IS explains the scarcity of studies of these effects in  $\text{Cu II}$ . However, these effects should be relatively easy to observe in the infrared region. Such observations would be very valuable.

All wavelength measurements described in the present paper were made with natural copper samples. As we know, there is no such physical entity as an atom of natural copper. Thus, the energy levels and Ritz wavelengths derived from these measurements do not pertain to a real atom, but rather are empirical values that best describe the spectrum as normally observed.

## 2. Wavelength Measurements

The unfortunate consequence of the thorough analysis made by Ross [2,16] is that, in the 46 years after his thesis, there were no studies devoted specifically to  $\text{Cu II}$ . Instead, his  $\text{Cu II}$  Ritz wavelengths were widely used as secondary standards for investigation of other species. In particular, the archive of the NIST Atomic Spectroscopy Group has several tens of photographic plates with VUV spectra obtained with the  $10.7 \text{ m}$  normal incidence vacuum spectrograph with a  $1200 \text{ lines/mm}$  concave grating. These plates were recorded for studies of  $\text{Y}$ ,  $\text{Zr}$ ,  $\text{Ge}$ ,  $\text{La}$ , and other elements. For calibration purposes, separate tracks were exposed on these plates with spectra of copper hollow cathodes. The latter, in addition to copper lines, contain lines of carrier gases (helium, neon, and argon), as well as hydrogen, carbon, oxygen, nitrogen, silicon, and germanium that were present as intrinsic or deliberately introduced impurities. These spectra were obtained in different years from 1969 to 1974. In addition to that, we have several high-resolution spectra recorded with two NIST vacuum Fourier transform spectrometers (FTS) in years 2002 to 2008 using  $\text{Cu/Ge/Pt/Fe/Ne}$  and  $\text{Cu/Re/Ar/He}$  hollow cathodes. The “new” measurements described in the Abstract were all made with these old recordings. However, we carried out new reductions of the wavelengths and re-analyzed the uncertainties, so it is in this sense that the measurements can be considered as new. To obtain a consistent and comprehensive description of the  $\text{Cu II}$  spectrum, we combined these new measurements with the old published data from Shenstone [1], Kaufman and Ward [15], and Ross [2,16], which we re-analyzed to evaluate the wavelength calibration, measurement uncertainties, and observed line intensities. Since this re-analysis depends on our new measurements, we describe them first.

Table 1 lists the exposures used in the present analysis. Since exposures used in grating measurements were taken over a period of several years, several different lamp designs were employed. The design of these lamps was similar to the one described in detail by Reader and Davis [26], except that a special fitting was made to attach them to the NIST vacuum spectrograph. The cathode was solid copper with a cylindrical hole of about  $7 \text{ mm}$  in diameter. Following Kaufman and Ward [15], small pieces of  $\text{Ge}$  and  $\text{Si}$  were placed in the cathode to obtain good reference lines in regions that were not covered well by  $\text{Cu II}$ . The carrier gas was a combination of flowing helium at a pressure of about  $0.5 \text{ kPa}$  ( $4 \text{ Torr}$ ) and neon or argon at about  $70 \text{ Pa}$  ( $0.5 \text{ Torr}$ ). The entrance slit of the spectrometer separated the lamp from the spectrometer chamber, which was maintained at a residual pressure of about  $7 \times 10^{-3} \text{ Pa}$  ( $5 \times 10^{-5} \text{ Torr}$ ). The demountable high-current lamp made at the University of Hannover, used several tens of years later in the FTS measurements, had a similar design described by Danzmann et al. [27]. Ar at a pressure of  $200 \text{ Pa}$  ( $1.5 \text{ Torr}$ ) with an addition of He at  $70 \text{ Pa}$  ( $0.5 \text{ Torr}$ ) was used as a carrier gas in spectrum 14, while Ne at a pressure of  $270 \text{ Pa}$  ( $2 \text{ Torr}$ ) was used in spectra 12 and 13. Pieces of  $\text{Ge}$ ,  $\text{Pt}$ ,  $\text{Fe}$ , or  $\text{Re}$  were placed inside the cathode. The grating spectrograms covered the region ( $636$  to  $2682$ )  $\text{\AA}$ , while the FTS spectrograms covered the region ( $1792$  to  $11733$ )  $\text{\AA}$ .

Table 1. Spectrograms used in the present measurements.

Exposure	Track	Region (Å)	Hollow Cathode Used	Impurities	Equip. <sup>a</sup>	Wavelength Standards <sup>b</sup>	Track Label	Date	Fit Poly <sup>c</sup>	St. Dev. <sup>d</sup>
1	1	636–827	Cu/He/Ar/Ne		NIVS	Ar II (1), Ne I (1), Cu II (TW-1) <sup>e</sup>	418	4/3/1974	2	0.0009
2	2	822–1000	Cu/Ge/Si/He/Ar	H, C, O	NIVS	H I (2), O I (6), O II (1), Ar II (2), Ge II (3)	419_r42	4/4/1974	2	0.0013
3	5	977–1166	Cu/He	H, C, N, O	NIVS	C I (2), C II (1), N I (2), O I (7), Ar I (2), Si II (2), Ge II (3)	419_r42	12/17/1969	2	0.0012
4	7	824–1020	Cu/He	H, O	NIVS	H I (1), O I (5), Cu II (KW66-4, TW-10) <sup>f</sup>	X431_r27	10/24/1974	2	0.0024
5	8	1181–1360	Cu/Ge/Si/He/Ar	H, C, N, O	NIVS, LIF	C I (6), N I (3), Si II (6), Ge II (1), Cu II (KW66-6, TW-1) <sup>g</sup>	X431_r27	10/24/1974	2, 3	0.0021
6	9	1339–1527	Cu/He/Ar	C, N	NIVS, LIF	C I (4), O I (1), Cu II (KW66-8)	X431_r27	12/16/1969	2, 2, 1	0.0010
7	10	1399–1584	Cu/Si/He/Ne	C, N	NIVS	C I (1), Cu II (KW66-2, TW-4) <sup>h</sup>		1/15/1970	2	0.0012
8	11	1920–2106	Cu/Ge/Si/He	C, N	NIVS	C I (1), Cu II (R69-20)		1/15/1970	2	0.0021
9	12	1399–1587	Cu/Ge/Si/He	C, N	NIVS	C I (3), N I (1), Si II (2), Ge II (2), Cu II (KW66-6)	X434_r52	11/11/1974	3	0.0014
10	13	1560–1743	Cu/Ge/Si/He	C, N	NIVS	C I (5), N I (1), Ge II (3), Cu II (KW66-21)	X434_r52	11/11/1974	3	0.0016
11	14	1394–1584	Cu/Ge/Si/He	C, N	NIVS	C I (3), Si II (2), Ge II (3), Cu II (KW66-52)	X434_r27	11/11/1974	2	0.0019
12	13	1559–1743	Cu/Ge/Si/He	C, N	NIVS	C I (7), Si II (1), Cu I (1), Cu II (KW66-14)	X434_r27	11/11/1974	2	0.0019
13	15	1751–1939	Cu/Si/He	C	NIVS	S I (1), Cu I (1), Cu II (KW66-4, R69-1, TW-2) <sup>i</sup>	X434_r27	11/11/1974	4	0.0012
14	16	1790–1980	Cu/Si/He	C	NIVS	C I (1), Cu I (1), Cu II (R69-11)	X433_r27	11/7/1974	2	0.0016
15	18	1977–2162	Cu/Ge/Si/He	H, C, O	NIVS	Si I (2), Ge I (6), Ge II (2), Cu I (1), Cu II (R69-26)	X433_r27	11/7/1974	5	0.0021
16	20	2139–2315	Cu/Ge/Si/He		NIVS	Si I (4), Ge I (1), Cu I (4), Cu II (R69-13)	X433_r27	11/7/1974	3	0.0017
17	21	2336–2517	Cu/Ge/Si/He		NIVS	Si I (3), Cu I (1), Cu II (R69-5)	X433_r27	11/7/1974	2	0.0011
18	22	2490–2682	Cu/Ge/Si/He		NIVS	O I (3), Si I (7), Ge I (3), Ge II (1), Cu I (R69-20)	El6-3	6/3/1969	2	0.0019
19	11	2117–2310	Cu/Ge/Si/He		FIS	Ge II (37)		2002	1	1.7 × 10 <sup>-8</sup>
20	12	1792–3324	Cu/Ge/Pt/Fe/Ne		FIS	Ge II (37)		2002	1	2.0 × 10 <sup>-8</sup>
21	13	1825–3324	Cu/Ge/Pt/Fe/Ne		FIS	Ar II (68)		2009	1	2.0 × 10 <sup>-9</sup>
22	14	2769–11733	Cu/Re/Ar/He		FIS					

<sup>a</sup> Equipment used: NIVS = Normal Incidence Vacuum Spectrograph (NIST, 10.7 m grating, reciprocal linear dispersion 0.78 Å); FTS = Fourier Transform Spectrometer (NIST, FT700 0.2 m vacuum FTS for spectra 12 and 13, and a 2 m vacuum FTS for spectrum 14); LIF = a LIF window was used to remove higher diffraction orders;  
<sup>b</sup> The number of spectral lines of each spectrum used as standards is given in parentheses. Unless otherwise indicated, the standard wavelengths used in grating measurements were the Ritz wavelengths taken from the ASD database [19]. For Cu II lines used as standards, the references are as follows: KW66—Kaufman and Ward [15]; R69—Ross [2]; TW—this work. Standards used in the FTS measurements are described in the text;  
<sup>c</sup> Power of the polynomial used to fit standard lines;  
<sup>d</sup> For grating spectra (exposures 1–11), standard deviation of the measured wavenumbers of the standard lines from the fitted polynomial (Å); For FTS spectra (exposures 12–14), standard deviation of the correction factor from the linear fit (dimensionless);  
<sup>e</sup> Cu II line at 826.9946 Å measured in 1<sup>st</sup> order on track 2 was used as standard on track 1;  
<sup>f</sup> Ten Cu II lines measured in 1<sup>st</sup> order on track 2 were used as standards on track 5;  
<sup>g</sup> Cu II line at 1275.5713 Å measured in 2<sup>nd</sup> order on track 22 was used as standard on track 7;  
<sup>h</sup> Four Cu II lines measured in 1<sup>st</sup> order on tracks 10–12 were used as standards on track 9;  
<sup>i</sup> Cu II lines measured in 1<sup>st</sup> order on tracks 8, 11, and 12 was used as standard on track 10;  
<sup>j</sup> Two Cu II lines measured in 1<sup>st</sup> order on track 15 were used as standards on track 16;  
<sup>k</sup> Long-wavelength end of track 8 was fitted separately with a cubic polynomial;  
<sup>l</sup> Short-wavelength end of track 9 was fitted separately with a 2nd degree polynomial.

The grating spectra were photographed on Kodak SWR plates and measured with a Grant semiautomatic comparator. (Commercial products are identified in this paper for adequate specification of the experimental procedure. This identification does not imply recommendation or endorsement by NIST.) Repeated measurements of the same plates were made, from which the measurement uncertainty of line positions was estimated to be  $1.6 \mu\text{m}$  for isolated well-resolved lines, corresponding to statistical wavelengths uncertainties of  $0.0012 \text{ \AA}$ . Most of the lines were measured on two to six different tracks. Thirty-eight Cu II lines were measured in the second order of diffraction, and one ( $861.9932 \text{ \AA}$ ) in the third order, while the rest of them were measured in the first order. Below  $1980 \text{ \AA}$ , most of the tracks had a sufficient number of impurity lines (H, He, C, N, O, Ne, Si, Ar, Ge), which were used as standards. Cu II lines accurately measured by Kaufman and Ward [15] were also used as standards in the region ( $860$  to  $1663$ )  $\text{ \AA}$ . In the region above  $1980 \text{ \AA}$ , we used Ross's [2] interferometric and grating measurements as standards. Although later we found that Ross's wavelengths are systematically too long (see below), the average error in the wavelengths we used as standards in the grating spectra was only  $(-0.0004 \pm 0.0008) \text{ \AA}$ , well below our total measurement uncertainties. Therefore, we did not remove the systematic errors from Ross's wavelengths used at this stage. The systematic uncertainty of each measured wavelength on our plates was estimated as a combination in quadrature of the standard deviation of the fitted polynomial (given in Table 1) and a mean uncertainty of standard wavelengths in the vicinity of the measured line. These systematic uncertainties were combined in quadrature with the statistical uncertainty ( $0.0012 \text{ \AA}$  for sharp isolated lines and up to  $0.005 \text{ \AA}$  for blended or overexposed lines). Multiple measurements of the same line on different tracks were averaged with weights inversely proportional to squares of total uncertainties. The uncertainty of the mean was calculated as a combination in quadrature of the reduced statistical uncertainty and the straight average systematic uncertainty. In total, we have measured 1217 unique spectral lines in the grating spectra between  $636 \text{ \AA}$  and  $2682 \text{ \AA}$ , of which 938 were either identified as Cu II lines or did not have any identification, and the rest were identified as belonging to impurities noted above. The wavelengths determined in the present work have uncertainties ranging from  $0.0008 \text{ \AA}$  to  $0.010 \text{ \AA}$ . A number of lines reported by Kaufman and Ward [15] were overexposed on our plates, which led to significant systematic shifts in determining their positions. Such overexposed lines were not used in the current wavelength measurements.

Our FTS measurements were calibrated assuming a common calibration factor for all wavenumbers in each spectrogram. The value of the calibration factor was determined as a weighted mean of the ratio  $\sigma/\sigma_{\text{std}}$ , where  $\sigma$  is the measured wavenumber, and  $\sigma_{\text{std}}$  is the tabulated wavenumber of the reference line. For the Ar II and Ge I-II lines used as standards in the FTS spectra, we used the Ritz values from ASD as  $\sigma_{\text{std}}$ . We used reciprocal squared uncertainties of  $\sigma_{\text{std}}$ , combined in quadrature with our measurement uncertainties (see below), as weights in this averaging. Uncertainties of thus obtained calibration factors (given in Table 1) represent the systematic uncertainties in our FTS measurements. Positions of the line centers  $\sigma$ , line widths  $W$ , signal-to-noise ratios  $S/N$ , and total integrated intensities were evaluated using the XGREMLIN code by Nave et al. [28] either automatically, assuming a Lorentzian profile for isolated symmetrical lines, Gaussian profile for nearly symmetrical but visibly perturbed lines, or manually with a Gaussian profile with a line width fixed at a visually estimated value.

For well-resolved symmetrical lines, statistical uncertainties of FTS measurements can be approximated by Equation (1) of Brault [29]:

$$\delta\sigma_{\text{stat}} = \frac{k}{\sqrt{N_w}} \cdot \frac{W}{S/N}, \quad (1)$$

where  $\sigma$  is the wavenumber,  $W$  is the full width at half maximum of the line,  $N_w$  is the number of statistically-independent points in the line width, and  $k$  is a constant depending on the line shape and the algorithm used for fitting the line. For Gaussian profiles,  $k = 0.693$ . For an optimally sampled

spectrum, the interferogram is recorded to a path difference such that  $N_w$  is between 3 and 4 for the majority of the spectral lines. This gives the commonly-used approximation of

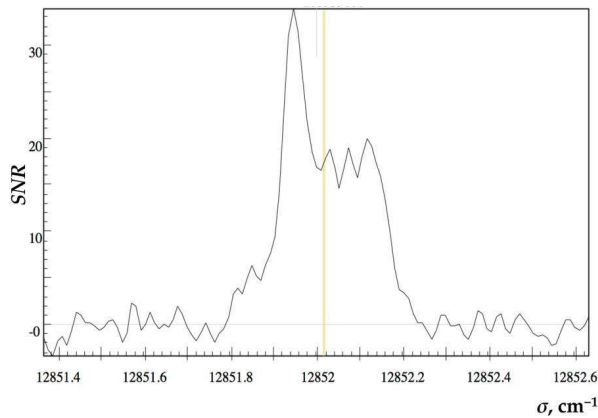
$$\delta\sigma_{\text{stat}} = \frac{W}{2 \cdot S/N} \quad (2)$$

Using  $N_w = W/r$ , where  $r$  is the resolution of the spectrum in  $\text{cm}^{-1}$ , Equation (1) can be re-written as:

$$\delta\sigma_{\text{stat}} = \frac{k}{S/N} \sqrt{rW} \quad (3)$$

Our spectra were taken with  $r = 0.015 \text{ cm}^{-1}$  for the Cu/Re/Ar/He spectrum and  $r = 0.13 \text{ cm}^{-1}$  for the Cu/Ge/Pt/Fe/Ne spectra. Typical line widths of symmetrical lines in our spectra range from  $0.04 \text{ cm}^{-1}$  around  $10000 \text{ cm}^{-1}$  to  $0.25 \text{ cm}^{-1}$  around  $30000 \text{ cm}^{-1}$ , giving values of  $N_w$  between 2.5 and 3. The instrumental line shape of the FTS comes from the finite length of the interferogram and is a sinc function of width  $r$ . When this is convolved with the Gaussian lines in our spectra, the increase in the width is negligible for a line with  $N_w = 3$  and only 0.2% for a line with  $N_w = 2$  and can thus be ignored in the calculation of the statistical uncertainty.

Many of the Cu lines are affected by HFS and cannot be adequately fitted using Gaussian profiles. For example, Figure 1 shows the profile of the Cu II line at  $12852 \text{ cm}^{-1}$ .



**Figure 1.** Profile of the Cu II line at  $12852 \text{ cm}^{-1}$  ( $7778.7 \text{ \AA}$ ) as measured in our Fourier transform spectrometers (FTS) spectrum. This line has a partially resolved hyperfine structure (HFS). The vertical line indicates the center of gravity.

The position of such lines was estimated using the center of gravity. For strong isolated lines ( $S/N > 150$ ), where it is easy to estimate the range for calculation of the center of gravity, Equation (3) can be used to estimate the uncertainty using  $k = 1$  [29]. However, this uncertainty increases for weaker lines where it is not as easy to estimate the range of calculation for the center of gravity. The measurements are further complicated by the asymmetric HFS. Its precise shape and width is not studied so far for the Cu II spectrum. In our high-resolution Cu/Re/Ar/He spectrogram, HFS patterns are partially resolved in 230 out of total 352 Cu II lines. The average width of the HFS of those lines is  $W_{\text{ave}} = 0.14 \text{ cm}^{-1}$ . Since the shapes of the HFS are unknown, an additional uncertainty in the measured centers of gravity arises from the possible omission (or erroneous inclusion) of a weak HFS component at the far wing of the line profile. The possible error caused by this effect of noise is easy to estimate by calculating the shift of the center of gravity of the structure:

$$\delta\sigma_{\text{hfs}} = 0.5W_{\text{hfs}}I_{\text{noise}}/(I_{\text{tot}} + I_{\text{noise}}), \quad (4)$$

where  $I_{\text{tot}}$  is the measured integrated intensity,  $W_{\text{hfs}}$  is the maximum of  $W_{\text{ave}}$  (see above) and the fitted width of the structure, and  $I_{\text{noise}}$  is the estimated possible integrated intensity of a hypothetical missed or erroneously included HFS component, equal to the root of mean square of the noise amplitude in the vicinity of the structure multiplied by the average width of sharp Cu II lines (equal to  $5 \times 10^{-6}$  times wavenumber for this spectrum).

The calibration of exposures 12 and 13, measured with a Cu/Ge/Pt/Ne hollow cathode, was made using 37 Ge I and II lines interferometrically measured by Kaufman and Andrew [30]. The reference wavenumbers from the latter paper have been decreased by 1.4 parts in  $10^8$  to put them on the scale of a recent measurement of  $^{198}\text{Hg}$  by Sansonetti and Veza [31], as described in Nave and Sansonetti [32]. Exposure 14, made with a Cu/Re/Ar/He hollow cathode, was calibrated using 68 Ar II standards from Whaling et al. [33]. Uncertainties of the calibration factors were determined as the sum in quadrature of the statistical uncertainty (coming from the different values of the calibration factor derived from different standard lines) and the mean uncertainty of the standard lines.

The total uncertainty of Cu II measurements was determined as the sum in quadrature of statistical and systematic uncertainties. The former was taken as the sum in quadrature of Equations (3) and (4), and the latter is the uncertainty in the calibration factor (given in Table 1) times the wavenumber. Total uncertainties of our Cu II wavelengths measured by FTS range from 0.000025 Å to 0.023 Å.

Kaufman and Ward [15] photographed the VUV spectrum of a water-cooled hollow cathode discharge containing germanium and silicon in the first, second, and third orders of diffraction of the same 10.7 m Eagle-mounting vacuum grating spectrograph as used in the present work (designated as NIVS in Table 1). They reported 141 measured wavelengths of Cu II in the range (861 to 1663) Å. As wavelength standards, they used lines of Cu II, Ge I, and Si I that were either calculated (Ritz) or interferometrically measured. The reciprocal linear dispersion was 0.78 Å/mm in the first order of diffraction. Many of the reported lines were measured on several (up to 11) spectrograms. We estimated their measurement uncertainties by comparing the measured wavelengths with the Ritz values (using Ross's [2] energy levels) separately for lines measured only in the first order (0.003 Å for a single measurement), measured several times in the 1st order, but only once in the 2nd and/or 3rd order (0.0010 Å), and for lines measured on several spectrograms in several orders of diffraction (varying from 0.0004 Å to 0.0018 Å). These estimates agree well with those given explicitly by Kaufman and Ward for a few lines. Careful work was required to reconstruct the list of observed wavelengths, since some of the values given in Table III of Kaufman and Ward [15] are Ritz wavelengths, but many of them are also given in their Table I including the value of the residual  $\lambda_{\text{Ritz}} - \lambda_{\text{obs}}$ . Since there is no information regarding the wavelength standards actually used in various wavelength regions, all wavelengths reported by Kaufman and Ward [15] were adopted without corrections.

Ross [2,16] investigated the Cu II spectrum photographically from 1979 Å to 11217 Å using plane and concave grating spectrographs and Fabry-Perot interferometers. The light source was a water-cooled hollow cathode discharge with helium or neon as a buffer gas. Ross [2] noted that intensity of most Cu II lines was greatly enhanced when He at a pressure of about 0.9 kPa (7 Torr) was used as the carrier gas, while if Ne is used, only lines below 3000 Å arising from relatively low levels are excited. The standards for the Fabry-Perot interferograms were the lines of  $^{198}\text{Hg}$  emitted by a water-cooled sealed electrodeless-discharge lamp containing argon carrier gas at a pressure of 33 Pa (0.25 Torr), with vacuum wavelengths 5462.27055 Å and 2537.2687 Å referred to Kaufman [34]. For grating measurements, a 9.2 m concave grating spectrograph with Paschen-Runge mounting was used. The grating had 600 lines/mm, was blazed at 10000 Å, and provided a reciprocal dispersion of  $\approx 1.7$  Å/mm. For calibration, interferometrically measured Cu II lines were used as standards.

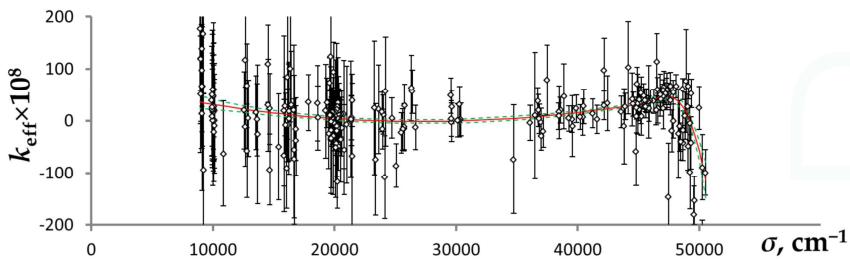
As noted in the Introduction, subsequent studies reported some systematic errors in Ross's short-wavelength measurements. This can be explained by the fact that below 2200 Å, Ross encountered severe technical difficulties in his interferometric measurements, caused by strong absorption in the



crystalline quartz of the plates and windows. He partially solved the problem by removing the windows, which exposed the interferometer to spectroscopically non-standard air and did not permit thorough temperature control. In addition, Kaufman's values for the  $^{198}\text{Hg}$  lines Ross used as standards, 5462.27046 Å and 2537.26877 Å [34], have since been re-evaluated. Their currently recommended vacuum wavelengths are 5462.27062(3) Å and 2537.268755(17) Å [35]. Additional errors could have been due to a possibly imperfect match between filling the interferometer's aperture with light from the hollow cathode and from the mercury lamp. To verify the calibration of Ross's wavelengths, we compared his reported wavelengths with those measured in our FTS spectra. Similar to FTS measurements, interferometric measurements of Ross can be corrected by a multiplicative factor [20]:

$$\sigma_c = (1 + k_{\text{eff}})\sigma_u, \quad (5)$$

where  $\sigma_c$  is the corrected wave number,  $\sigma_u$  is the uncorrected wave number, and the correction factor  $k_{\text{eff}}$  is determined from one or more internal standard lines in the spectrum, in this case from our wavenumbers measured by FTS. Dependence of thus derived  $k_{\text{eff}}$  on wavenumber is plotted in Figure 2.



**Figure 2.** Dependence of calibration factor for interferometric measurements of Ross [2] on wavenumber. The error bars are measurement uncertainties of Ross [2] and our FTS data, combined in quadrature. The solid line is a weighted fit with two cubic polynomials stitched together at about 45,000  $\text{cm}^{-1}$ . The dashed lines are 68% confidence intervals ( $\pm 1$  standard deviation) of the fit.

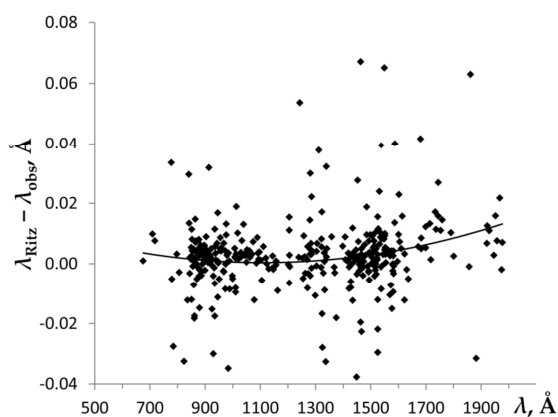
It should be noted that Figure 2 includes all Ross's lines that were also measured in our FTS spectra. Many of those lines were weak in our FTS spectra, resulting in large error bars in Figure 2. However, there was a sufficiently large number of strong lines with small error bars, which explain the very small uncertainties of the fitted curve in Figure 2.

Unlike FTS measurements, where  $k_{\text{eff}}$  is a constant over the entire range of measured lines, the calibration correction of Ross's measurements depends on wavenumber. This dependence is rather weak, and the value of  $k_{\text{eff}}$  is small ( $< 10^{-7}$ ) in the interval (17000 to 38000)  $\text{cm}^{-1}$  (6000 Å to 2700 Å), but  $k_{\text{eff}}$  notably increases (up to  $3.5 \times 10^{-7}$ ) for infrared lines, and varies rapidly for the far-UV lines below 2700 Å. The accuracy of the fitted  $k_{\text{eff}}$  values varies from  $3 \times 10^{-8}$  to  $3.5 \times 10^{-7}$ , depending on the measurement uncertainties in Ross [2] and in our FTS data. It determines the systematic uncertainties in the Ross's wavenumbers as now re-calibrated.

This re-calibration and increased uncertainty associated with it allowed us to explain only a small part of numerous lines strongly deviating from Ritz wavelengths in Ross's list, noted in the Introduction. To explain the remaining problematic lines, additional factors contributing to uncertainties, not accounted for by Ross, must be considered. One such factor can be pressure shifts caused by relatively high pressure of He in his discharge, 0.9 kPa (7 Torr). Such shifts could cause quasi-random deviations of measured wavelengths in both directions from unperturbed values. Another contributing factor could be partially resolved HFS. The Doppler width reported by Ross for the sharp line at 2473 Å (40419  $\text{cm}^{-1}$ ) was about 0.1  $\text{cm}^{-1}$ , which is of the same order of magnitude as most of the known HFS widths. He noted that partially-resolved HFS was indeed a problem in

his wavelength measurements, and that his tabulated results are centers of gravity of observed HFS structures. However, he did not give any details about the method with which these centers of gravity were determined. Such determination depends on the measurement accuracy of the relative intensities of the HFS components, which might have been distorted by non-linearity of response of photographic plates used by Ross. The shift in the measured center-of-gravity wavenumber caused by errors in intensity measurements would be some fraction of the HFS width. We accounted for both types of such possible shifts (caused by pressure and HFS) by adding in quadrature a constant quantity to the wavenumber-measurement uncertainties of Ross [2]. The value of this constant was found empirically to be  $0.007 \text{ cm}^{-1}$ . These increased uncertainties are statistically consistent with residuals  $\sigma_{\text{obs}} - \sigma_{\text{Ritz}}$  of the level-optimization procedure (see Section 3).

Shenstone [1] made the most comprehensive study of the Cu II spectrum prior to Ross [2]. He photographed spectra of a copper hollow cathode (Schuler tube) filled with helium or neon using several spectrographs: 6.4 m and 3 m normal incidence grating spectrographs and two Hilger prism spectrographs for the UV and visible regions, a 2 m normal incidence vacuum grating spectrograph for the VUV region, and another concave grating spectrograph (in NBS) for the infrared region. Since Ross could not observe lines shorter than  $1979 \text{ \AA}$ , Shenstone's line list remained the only source of information about observed Cu II lines and their intensities in the VUV. We have re-measured many of VUV lines listed by Shenstone with much greater accuracy. Most of his lines in the UV, visible, and infrared regions were re-measured by Ross [2]. However, 94 lines from Shenstone [1] ranging from  $836 \text{ \AA}$  to  $6870 \text{ \AA}$  were not observed in our and Ross's spectra. For 15 of them, Shenstone did not give a measured wavelength (apparently, because low resolution did not permit accurate measurement), but gave the observed intensity. Wavelength calibration and uncertainties of Shenstone's measurements were investigated by comparing them with Ritz wavelengths calculated from Ross's [2] energy levels. Because of the relatively low resolution of Shenstone's measurements, the small differences of Ross's Ritz wavelengths from more accurate ones obtained from our final level optimization (see Section 3) did not have any effect on this analysis. Since most of Shenstone's lines used in the final line list were measured with the vacuum grating spectrograph, we compare his measurements made on this instrument with Ritz wavelength in Figure 3.



**Figure 3.** Deviations of vacuum ultraviolet (VUV) wavelengths measured by Shenstone [1] from Ritz values from Ross [2]. The solid line is a 2nd degree polynomial fit.

Although Figure 3 includes all wavelengths reported by Shenstone (excluding a few lines with extremely large deviations), assessment of uncertainties was made separately for “good” wavelengths given with three figures after the decimal point (in  $\text{\AA}$ ) and having no indication of blending or other

perturbations, for wavelengths given with two decimal figures (apparently, deemed less accurate by Shenstone), and for lines indicated as blended or perturbed, or having multiple classifications. The trend indicated in Figure 3 by a solid line was derived from accurately measured lines only. It resulted in a correction to Shenstone's VUV wavelength varying from +0.003 Å for the shortest wavelengths near 700 Å to +0.010 Å near 1980 Å. After this correction, the uncertainty for each category of lines was estimated as a root-mean-square (rms) of the residuals. These uncertainties were found to vary from 0.006 Å for the best measurements to 0.07 Å for the worst. A similar analysis was made separately for each spectrograph used by Shenstone.

For completeness, we included in our line list one line observed by Wagatsuma and Hirokawa [36] at 4485.3 Å, which was not reported by other observers. Since wavelengths reported by Wagatsuma and Hirokawa are the Ritz ones (owing to low precision of their measurements), we also give only the Ritz wavelength for this line.

In all the laboratory studies described above, only electric-dipole allowed (E1) lines could be observed, since densities in the discharge light sources are high enough to collisionally depopulate metastable levels, from which forbidden lines could emerge. However, four forbidden lines of Cu II were observed in other studies. The first observation known to us is that of Thackeray [3] who identified the line of Cu II at 3806.3 Å as the electric-quadrupole (E2)  $3d^{10} 1S_0-3d^9 4s 1D_2$  transition in emission spectra of two nebulae,  $\eta$  Carinae and RR Telescopii. Another E2 transition,  $3d^{10} 1S_0-3d^9 4s 3D_2$  at 4375.8 Å, as well as the hyperfine-induced  $3d^{10} 1S_0-3d^9 4s 3D_3$  transition at 4558.7 Å, were observed but not identified in emission of RR Telescopii by Aller et al. [4]. The above-mentioned E2 transition at 3806.3 Å, as well as the magnetic-dipole (M1)  $3d^{10} 1S_0-3d^9 4s 3D_1$  transition at 4165.7 Å, were observed and identified by McKenna et al. [5] in emission of the same nebula, RR Telescopii. In the laboratory, the two E2 transitions at 3806.3 Å and 4375.8 Å were observed (with an accuracy inferior to astrophysical observations) and their radiative decay rates were measured by Prior [37] in an electrostatic ion trap.

All observed and identified spectral lines of Cu II are collected in Appendix A, Table A1. In addition to observed lines, this table includes several predicted transitions, in particular, six M1 and E2 transitions between the levels of the first excited configuration,  $3d^9 4s$ . This table lists 2557 transitions corresponding to 2494 unique measured spectral lines, 677 of which were measured in this work, and includes 50 additional lines that are either predicted (not observed), observed but not measured, or were masked by stronger neighboring lines in observed spectra. In addition to observed wavelengths, Table A1 gives for each transition the Ritz wavelength with standard uncertainty obtained in the level optimization procedure (see Section 3), energy-level classification, intensity on a unified scale (see Section 5), and a reference to the source of the observed wavelength. For 555 transitions, we also give a critically evaluated transition probability (*A*-value) with its uncertainty estimate and a reference. Lines on which laser action was reported in the literature are marked with "L" in the Notes column.

In Table A1, wavelengths between 2000 Å and 20000 Å are given in standard air; outside of this region, they are in vacuum. Conversion from air to vacuum was made using the five-parameter formula from Peck and Reeder [38]. Ritz wavelengths and their uncertainties were obtained using the LOPT (level optimization) code [39] as described below in Section 3. Transition probabilities are either calculated in the present work or critically compiled from references [40–51] as described in Section 6.

### 3. Energy Levels

The precise positions of energy levels, as well as the Ritz wavelengths and their uncertainties, were derived from the identified lines listed in Table A1 using the least-squares level optimization code LOPT [39]. The resulting energy levels are listed in Table A2.

Of all 2557 transitions in Table A1, 113 were excluded from the level optimization procedure. Among those, there are 61 transitions that were either predicted (e.g., far-IR forbidden transitions), had poorly measured wavelengths (e.g., astrophysically observed forbidden lines), were severely

blended, or were masked by much stronger nearby lines. The remaining 52 lines were excluded because their observed wavelengths deviated too much from the Ritz values. In total, we used 2443 observed transitions in our level-optimization procedure. For comparison, Ross [2,16] used 1691 observed transitions in his level optimization.

If one compares the presently found energy levels with those given by Ross [2,16], the average agreement is good. The mean difference ( $E_{\text{TW}} - E_{\text{Ross}}$ ) is only  $0.007 \text{ cm}^{-1}$  with a standard deviation of  $0.016 \text{ cm}^{-1}$  (the subscript "TW" means "this work"). However, a more detailed comparison shows that, of the 347 levels correctly identified by Ross, 156 deviate from those given in Table A2 by more than two (up to 11) combined uncertainties. Uncertainties of our level values are on average greater than those of Ross by a factor of 1.4, owing to our increased estimate of Ross's wavelength uncertainties. For only 32 levels our uncertainties are smaller than those of Ross (by up to a factor of eight). This improvement is due to our FTS measurements. Similar conclusions can be made for the Ritz wavelengths. Among about 500 Ritz VUV wavelengths listed by Ross, only a few are incorrect because of erroneous identifications described below. If these are excluded, the mean difference ( $\sigma_{\text{TW}} - \sigma_{\text{Ross}}$ ) is  $0.012 \text{ cm}^{-1}$  with a standard deviation of  $0.019 \text{ cm}^{-1}$ . However, for 273 VUV lines (more than half of all given by Ross), Ross's Ritz wavelengths deviate from ours by more than twice the combined uncertainty. Our Table A1 includes 632 Ritz wavelengths for VUV lines below  $2000 \text{ \AA}$ . Most of the new lines were observed and measured in this work.

The analysis that led to Tables A1 and A2 was made in an iterative manner. In the first step, after an initial list of all observed lines was constructed, it contained more than 600 unclassified lines, 143 of which were listed by Ross [2,16], 54 by Shenstone [1], one by Kaufman and Ward [15], and the rest were observed in our VUV grating spectra. Twenty-four of these lines (18 in Ross [2,16] and 6 in Shenstone [1]) were found to be due to previously identified transitions in Cu I. To find possible identifications for the remaining unknown lines and to find proper designations for the energy levels, we made a parametric analysis of the Cu II spectrum using Cowan's suite of atomic codes RCN/RCN2/RCG/RCE [52] (A version of the codes adapted by A. Kramida for Windows-based personal computers is available online: <http://das101.isan.troitsk.ru/COWAN>). In this analysis, we included the following sets of configurations:  $3d^{10}$ ,  $[3d^9](ns, nd)$  ( $n = 4-10$ ),  $ng$  ( $n = 5-10$ ),  $[3d^8](4s^2, 4p^2, 4s4d, 4s5s, 4d^2, 4s5d)$  in the even parity, and  $[3d^9](np, nf)$  ( $n = 4-8$ ),  $nh$  ( $n = 6-8$ ),  $[3d^8](4s4p, 4s4f, 4p4d, 4s5p, 4s5f)$  in the odd parity, 25 configurations in total. All known energy levels from Sugar and Musgrove [17] were included in the least-squares parametric fitting (LSF) with the RCE code. The calculations were made in the relativistic mode (HFR), including Breit corrections and correlation term (explained in the RCN manual). The fitted parameters were substituted as input for the RCG code to obtain a list of predicted lines with calculated  $A$ -values. The calculated  $A$ -values and energy levels, as well as known experimental levels, were used in the input files for the visual line-identification code IDEN1 originally designed by Azarov [53] and later programmed for Windows-based computers by one of the present authors (AK). Using this tool, we identified 117 previously unclassified lines with transitions between known energy levels, revised four levels and found 28 new energy levels. The revised and newly found energy levels explained 79 previously unclassified lines and involved revised classifications of 24 lines previously identified by Ross [2] and Shenstone [1].

At this stage of the analysis, it was also found that two levels listed by Ross [2] and included in the compilation of Sugar and Musgrove [17] had to be rejected. One of them, an undesignated odd-parity level with  $J = 1$  at  $144240.6 \text{ cm}^{-1}$ , was retained by Ross from Shenstone's level list. It was identified by one line measured by Shenstone at  $823.802 \text{ \AA}$ , which we re-measured to be at  $823.8361(18) \text{ \AA}$  and identified with a transition between other previously known levels,  $3d^9 4s^1 D_2 - 3d^9 ({}^2D_{5/2}) 7p^2 [5/2]_2$ . It was also found that there are no possible unknown odd-parity levels with  $J = 1$  sufficiently close to the value given by Ross to explain this level. Another rejected level is also of odd parity, designated by Ross as  $3d^9 6p^3 P^{\circ}_0$  (at  $141154.164 \text{ cm}^{-1}$ ). It was based by Ross on two lines, one observed by Shenstone at  $853.56 \text{ \AA}$  and identified by Ross as a transition from this level to  $3d^9 4s^3 D_1$ , and another observed by Ross at  $3217.641 \text{ \AA}$ , which he interpreted as a transition from this level to  $3d^9 ({}^2D_{3/2}) 5s$

$^2[3/2]_1$  (to be consistent with our tables, we use our new *JK* designations). Both these transitions were predicted to be extremely weak, certainly much weaker than other possible transitions from this level. We re-measured the first line to be at 853.544(2) Å and re-classified both lines as transitions from other levels. In addition, the energy given by Ross deviates too much from that predicted by our parametric fitting.

Two levels listed by Ross as  $3d^9 6p \ ^3F^{\circ}_2$  and  $^3D^{\circ}_1$  at 141244.576  $\text{cm}^{-1}$  and 141734.167  $\text{cm}^{-1}$ , respectively, were each based by Ross on several transitions to lower-lying even levels with  $J = 1$  or 2. Most of the corresponding lines were previously observed and similarly identified by Shenstone. However, we found that observed line intensities agree much better with those predicted if assignments of these two levels are interchanged. Further proof for this revision was provided by our identification of two transitions from the lower of these two levels down to levels with  $J = 3$ . One of the corresponding lines was newly observed in our VUV spectrum, and another one was present among Ross's unclassified lines.

Following Shenstone [1], Ross interpreted the level at 137212.765  $\text{cm}^{-1}$  as  $3d^8 4s 4p \ ^1P^{\circ}_1$ . Sugar and Musgrove [17] gave a more specific designation,  $3d^8(^3P)4s4p(^3P^{\circ}) \ ^1P^{\circ}_1$  based on a parametric calculation made by Roth [54]. We found three transitions connecting this level with even  $J = 3$  levels. Since other combining levels have  $J = 1$  and 2, the only possible  $J$  value for this level is 2. We labeled this strongly mixed level as  $3d^8(^1G)4s4p(^3P^{\circ}) \ ^3F^{\circ}_2$ , although it represents only 36% of the percentage composition; an equal contribution is from  $3d^8(^3F)4s4p(^1P^{\circ}) \ ^3F^{\circ}_2$ , followed by 14% of  $3d^8(^3P)4s4p(^3P^{\circ}) \ ^1D^{\circ}_2$ .

Ross found the level at 147491.888  $\text{cm}^{-1}$ , which he designated as  $3d^9 7p \ ^3F^{\circ}_3$  based on three weak lines at 3360.9941 Å, 9310.353 Å, and 9569.11 Å, identified as transitions from this level down to  $3d^9 4d \ ^3G_3$ ,  $3d^9 5d \ ^3P_2$ , and  $3d^9 5d \ ^3F_4$ . Although these three lines indeed perfectly satisfy the Ritz combination principle, our calculations indicate that their intensities should be negligibly small, while much stronger transitions to other even-parity levels should occur, but were not observed by Ross. The strongest predicted transitions from this level are in the VUV region inaccessible to Ross. We have found three lines in our VUV exposures at 824.663 Å, 1609.342 Å, and 1924.548 Å, which have wavelengths and intensities consistent with this level, placing it at our new revised position, 147525.93  $\text{cm}^{-1}$ . All other odd-parity levels with  $J = 3$  predicted to occur within  $\pm 2000 \text{ cm}^{-1}$  from this energy are experimentally known, which leads us to conclude that the combination of three lines observed by Ross is spurious. We note that the density of observed lines in the UV, visible, and IR regions is sufficiently high to produce several tens of spurious combinations of two, and a few of three lines, which we observed in the combined line list. We could not find alternate identifications for the three lines assigned previously by Ross to this revised level.

Three other levels in Ross's list were found to be questionable, either because they were based on only one or two weak lines, or because the energy strongly disagrees with our parametric calculation. These levels are at 154838.963  $\text{cm}^{-1}$ , 155244.833  $\text{cm}^{-1}$ , and 156958.096  $\text{cm}^{-1}$ , designated by Ross as  $3d^9 8d \ ^3P_1$ ,  $^3P_0$ , and  $^3F_2$ , respectively.

After the new identifications were made, the new experimental energies were incorporated in the LSF procedure, and the questionable levels removed. We also inserted in the LSF several tens of levels belonging to the  $[3d^9]9d$ ,  $10d$ ,  $8g$ ,  $9g$ ,  $10g$ ,  $7f$ ,  $8f$ ,  $6h$ ,  $7h$ , and  $8h$  levels whose positions were accurately extrapolated by Ritz-type quantum defect or polarization formulas (see Section 4). These levels were found to be sufficiently pure, unperturbed by interactions with other configurations, and thus the series formulas provided dependable results.

In this final LSF, 218 known even-parity levels were fitted with 38 free parameters with a standard deviation of 40  $\text{cm}^{-1}$ , and 241 known odd-parity levels were fitted with 35 free parameters with a standard deviation of 72  $\text{cm}^{-1}$ . The fitted (LSF) and ab initio Hartree-Fock (HF) values of parameters are given in Table 3. In both parities, the  $\zeta_{3d}$  parameters of the  $3d^n$  core were linked together in one group for all configurations, so that their LSF/HF ratio was the same for all members of the group, but was allowed to vary in the fitting. Other parameters, similar in different configurations, such as the

effective parameter  $\alpha_{3d}$ , electrostatic parameter  $F^2(3d,3d)$  of the  $3d^8$  core, and configuration-interaction parameters, were also linked in similar groups, which decreased the number of free parameters and made the fitting more stable.

Using the transformation procedures implemented in Cowan's RCE code, eigenvector compositions were calculated in several coupling schemes. Similar to the spectrum of neutral nickel analyzed by Litzén et al. [21], most of the  $3d^9nl$  configurations were found to be best described in the  $J_1l$  (otherwise known as  $JK$  or  $J_cK$ ) coupling scheme, in which the total angular momentum of the core ( $3d^9$  in this case) is combined with the orbital momentum of the valence electron to produce the  $K$  quantum number, which is then combined with the spin of the valence electron to obtain the final total angular momentum  $J$ . In Ni I, Litzén et al. [21] found the lowest  $[3d^9]nl$  configurations,  $4s$ ,  $4p$ , and  $5p$ , to be better described in the  $LS$  coupling scheme, which is also the best for the  $3d^84s^2$  and other  $3d^8nln'l'$  configurations. In Cu II, our findings are similar, except that the  $3d^95p$  configuration is better described by  $J_1l$  coupling. The  $J_1l$  purity of the  $3d^9nl$  configurations increases from 65% for  $3d^96p$  to 100% for  $3d^9ns$ ,  $nh$  ( $n \geq 6$ ), and  $ng$  ( $n \geq 6$ ), and generally increases with increasing  $n$  and  $l$ . This general trend is disrupted in  $3d^96p$ . This configuration strongly interacts with  $3d^84s4p$ , unlike  $3d^95p$ , for which this interaction is somewhat weaker, resulting in the average  $J_1l$  purity of 75%. For the  $3d^84s4p$  configuration, in agreement with the previous analysis by Roth [54], we found that the best description is obtained by first combining the quantum numbers of the  $4s$  and  $4p$  electrons with each other to produce an intermediate  $LSJ$  term ( $^3P^\circ$  or  $^1P^\circ$ ) of the  $4s4p$  valence shell, and then combine it with  $LSJ$  of the  $3d^8$  core. Although the average purity of  $3d^84s4p$  in this coupling scheme is rather high, 73%, many of its levels are strongly mixed with other configurations, rendering assignment of single-configuration labels arbitrary. Several levels attributed to this configuration have a leading percentage of the composition smaller than 30%. In a few cases, such as the levels at  $139331.149 \text{ cm}^{-1}$  ( $J = 3$ ) and  $139710.491 \text{ cm}^{-1}$  ( $J = 2$ ), we assigned labels corresponding to the second leading term in the composition, in order to preserve uniqueness of the labels within the  $J$  manifolds. The labels assigned to the levels do not fully describe their physical nature; percentage compositions given in Table A2 are somewhat better in this regard.

The high  $J_1l$  purity of the  $3d^9ng$  configurations and very small values of parameters describing interactions between  $3d^9$  and  $ng$  shells allows for accurate prediction of the levels that were missing in Ross's levels list. This permitted us to find some of these levels from the lines left unclassified in his analysis.

For each level, Table A2 gives a number of observed lines on which this level is based. Most of the levels are based on more than two observed lines. However, 71 of them are derived from only one or two observed lines. Most of them are firmly identified, because the observed lines are the strongest predicted ones, and the level positions are confirmed by trends along series. Five of such levels are marked as questionable, because the corresponding series are strongly perturbed, or because the observed lines are not the strongest predicted to occur from these levels. The absence of predicted stronger lines could be explained by different registration sensitivity in exposures used in different spectral regions.

We identified the previously missing  $3d^84s^21S_0$  level based on one line observed at  $1807.8535 \text{ \AA}$  in two exposures in our VUV spectra and at  $1807.84 \text{ \AA}$  by Shenstone [1]. We assigned this line to the strongest predicted transition from this level, terminating at  $3d^94p^1P^\circ_1$ . Although this line is observed to be about 20 times stronger than predicted, this was the only unidentified line within the interval of  $\pm 3000 \text{ cm}^{-1}$ , and it places the  $3d^84s^21S_0$  level within  $25 \text{ cm}^{-1}$  of its predicted position. Therefore, we believe that this identification is correct.

Five odd-parity levels are given in Table A2 with revised designations. The level with  $J = 3$  at  $121524.8509 \text{ cm}^{-1}$  was previously labeled by Sugar and Musgrove [17] as  $3d^95p^3D^\circ$  with a 53% contribution of this term in the composition, as given by Roth [54]. Although our calculation yields the same leading term in the composition of this level, the total contribution from the  $3d^84s4p$  configuration is calculated to be greater than from  $3d^95p$ . Therefore, we designated this level by the second largest

component,  $3d^8(^3F)4s4p(^3P^o)^1F^o$ . A marginally larger contribution of the  $3d^95p^3D^o$  term was found in the  $J = 3$  level at  $121079.1501\text{ cm}^{-1}$ , which we attributed to this configuration. The  $J_1l$ -coupling designation gives a better description of this level, the leading term being 54% of  $3d^9(^2D_{5/2})5p^2[5/2]^o$ . In effect, the identifications of these two  $J = 3$  levels at  $121079.1501\text{ cm}^{-1}$  and  $121524.8509\text{ cm}^{-1}$  have been interchanged. This revision is supported by better agreement of observed and calculated line intensities.

The  $J = 4$  level at  $134742.863\text{ cm}^{-1}$  was labeled by Sugar and Musgrove [17] as  $3d^96p^3F^o$ , and its composition was given as 49% of this term and 39% of  $3d^8(^1G)4s4p(^3P^o)^3F^o$ . We found the leading term to be 50% of  $3d^8(^3F)4s4p(^1P^o)^3F^o$ , which we use as a revised label. We note that Sugar and Musgrove gave the same configuration and term label to another  $J = 4$  level at  $139395.786\text{ cm}^{-1}$  with almost the same percentage composition. We found for the latter level 59% contribution from  $3d^96p^3F^o$ , but designated it in  $J_1l$ -coupling as  $3d^9(^2D_{5/2})6p^2[7/2]^o$ .

Another  $J = 4$  level at  $137938.904\text{ cm}^{-1}$  was designated by Sugar and Musgrove [17] as  $3d^8(^3F)4s4p(^1P^o)^3F^o$  with 53% of this term in the composition. We found the leading terms to be 49% of  $3d^8(^1G)4s4p(^3P^o)^3F^o$ , 39% of  $3d^96p^3F^o$ , and only 5% of the term given as label by Sugar and Musgrove. We changed the label to the leading term indicated by our calculation.

The  $J = 3$  level at  $139331.149\text{ cm}^{-1}$  was designated by Sugar and Musgrove [17] as  $3d^96p^3D^o$  with 56% of this term in the composition. In our calculation, the leading  $LS$  term is found to be 46% of  $3d^96p^1F^o$ . However, in  $J_1l$ -coupling adopted for the  $3d^96p$  configuration, the leading term is 32% of  $3d^9(^2D_{5/2})6p^2[7/2]^o$ , which is used to label another level having 62% of this term. Thus, we labeled the level at  $139331.149\text{ cm}^{-1}$  by the second leading  $LS$  term of its composition,  $3d^8(^1G)4s4p(^3P^o)^3F^o$ .

#### 4. Ionization Energy

Ross [2] derived the value for the ionization limit by extrapolation of quantum defects along 12 series of the type  $3d^9nl$  (two  $ns$ , nine  $nd$ , and one  $nf$ , with  $n$  ranging from 4 to 10 for the  $ns\ J = 3$  series, 4 to 9 for the  $ns\ J = 1$  series, and 4 to 8 for the rest). Although Ross used  $LS$  designations for all the levels involved, the series he chose are almost pure in  $J_1l$  coupling, resulting in smooth behavior of quantum defects along the series. Using the RITZPL computer code by Sansonetti [55], we repeated Ross's derivation with our more accurate level values and obtained slightly different values for the series limits. In the derivation of the limit, we added two more 5-member  $3d^9nd$  series, in which we found some new identifications. The weighted average of the limits obtained closely agrees with the average value adopted by Ross. In addition, series limits obtained from six three-member series with an exact fit of the polarization formula (Sansonetti [56]) produced values in close agreement with this average. Thus, we adopted the value for the ionization limit given by Ross [2],  $163669.2(5)\text{ cm}^{-1}$  or  $20.292\ 39(6)\text{ eV}$ , which is now confirmed.

Table A2 includes predicted energies for 89  $[3d^9]nd, nf, ng,$  and  $nh$  levels for which no reliable identification could be found in the observed spectra. These levels are not necessarily those that produce the strongest predicted lines. Rather, they are those that are easier to accurately predict, because the corresponding series have relatively small perturbations. In this derivation, we used predicted positions for centers of gravity of groups of closely located levels along series, using the RITZPL (quantum-defect formula) and POLAR (polarization-formula) extrapolation codes by Sansonetti [55,56], which we combined with fine-structure intervals predicted by the LSF (described in Section 3). Uncertainties assigned to these levels in Table A2 are weighted means of the "observed-calculated" residuals of the LSF, calculated separately for known levels with  $J_1l$  purities of  $\geq 99\%$ , (97 to 98) %, and (92 to 96) %. Some of the remaining unclassified lines observed by Ross [2,16], Shenstone [1], and by us may be due to these levels. However, we could not reliably identify them because of lack of observed Ritz combinations.

## 5. Line Intensities

Procedures used in the present work to adjust observed line intensities to a common scale were described in detail by Kramida [57,58]. In this derivation, line intensities observed in each experiment are roughly modeled as described by Boltzmann level populations with certain effective excitation temperature  $T_{\text{eff}}$ . This temperature is found from a Boltzmann plot built using calculated transition probabilities. The ratios of predicted Boltzmann-population intensities are plotted against wavelengths to derive the response function of the registration equipment, which is then removed from the observed intensities to obtain an improved fit for  $T_{\text{eff}}$  from the Boltzmann plot. For photographic registration, an additional correction of non-linearity of intensity registration with exposure is deduced from a plot of ratios of calculated and observed intensities versus observed intensity. This procedure is repeated iteratively until convergence is achieved. Then it is easy to scale the reduced intensities observed in experiments with different  $T_{\text{eff}}$  and different sensitivity to a common value of  $T_{\text{eff}}$ . In this way, we combined intensities observed in our 22 VUV and 3 FTS spectrograms listed in Table 1 with those reported by Shenstone [1], Kaufman and Ward [15], and Ross [2,16] and reduced them to the scale derived from Ross's observed intensities to produce the average values given in Table A1. This scale corresponds to  $T_{\text{eff}} = 1.5$  eV, which is about average for all experiments included in the analysis. For different experiments, the fitted value of  $T_{\text{eff}}$  varied between 0.6 eV in some of our VUV exposures to 11 eV in observations of Kaufman and Ward [15]. It should be noted that in most experiments analyzed here populations of highly excited levels were enhanced by resonant transfer from excited levels of helium or other rare gases used in the discharges. This population transfer is the mechanism leading to population inversion and producing laser action observed in hollow-cathode discharges. Thus, it should be expected and is indeed observed that level populations deviate from the Boltzmann distribution by a factor of three on average and strongly vary depending on discharge conditions. Line intensities are given in Table A1 in terms of total energy flux under the line contour.

As noted in Section 2, only E1-allowed lines were observed in laboratory discharges. Thus, the intensity scale adopted for E1-forbidden lines is different from the allowed lines. It is based on relative intensities observed in nebulae spectra by Thackeray [3], Aller et al. [4], and McKenna et al. [5], modified in such a way that the relative intensities of lines from a common upper level are consistent for different observations.

## 6. Transition Probabilities

Transition probabilities of Cu II were reported in 42 papers, the full list of which can be found in the NIST Atomic Probability Bibliographic Database (Kramida and Fuhr [59]). In addition, we have calculated them using Cowan's codes [52] using our LSF parameters described in Section 3. To assess the uncertainties of all available data sets, we used evaluation procedures described by Kramida [57].

The initial reference data set was constructed of 41  $A$ -values determined by Ortiz et al. [50] from branching fractions measured using laser-induced breakdown spectroscopy and lifetimes calculated using the Cowan suite of codes [52], modified by inclusion of core-polarization effects. The high accuracy of theoretical lifetimes used in that work was confirmed by excellent agreement with accurate measurements made by Pinnington et al. [51] and Cederquist et al. [43], as well as with other advanced calculations.

This initial selection was expanded by inclusion of theoretical  $A$ -values from Dong and Fritzsche [45] obtained in a large-scale multiconfiguration Dirac-Fock calculation accounting for relaxation effects in the orbitals. Uncertainties of these theoretical data were estimated by comparing the results obtained by those authors in the Babushkin (length) and Coulomb (velocity) gauges. This comparison indicated that the stronger lines with line strength  $S > 10^{-6}$  a.u. were calculated with uncertainties in  $A$ -values of about 12% on average, while for weaker lines the average uncertainty was much larger, 60%. These conclusions are supported by good agreement (less than 10%) of calculated lifetimes with measurements. For 18 transitions the  $A$ -values reported by Dong and



Fritzsche [45] were normalized to lifetimes of the upper levels measured by Pinnington et al. [51] and by Cederquist et al. [43].

For three transitions representing the sole allowed decay channels of their upper levels, the lifetimes measured by Pinnington et al. [51] and by Cederquist et al. [43] were directly converted into  $A$ -values and also added to the reference data set. Further expansion of the reference data set was provided by results of Crespo López-Urrutia et al. [44] obtained by combining their own measurements of emission branching fractions with radiative lifetimes measured in other studies. From this work, the results obtained using the lifetimes reliably measured by Cederquist et al. [43] and by Kono and Hattori [48] were used without adjustments. However, for several transitions we re-normalized their results to lifetimes more accurately measured by Pinnington et al. [51]. Uncertainties of Crespo López-Urrutia et al. [44] were estimated by combining in quadrature systematic contributions from the uncertainties of the lifetimes and statistical uncertainties, which we estimated to vary from less than 5% for the strongest lines to 90% for the weakest lines, which we assumed to have a signal-to-noise ratio about 1.

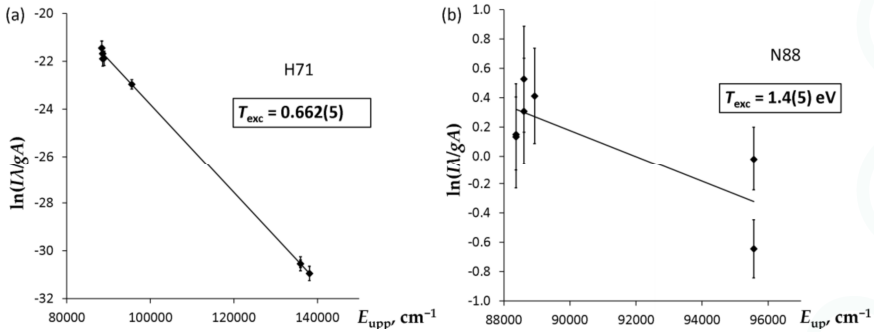
Kono and Hattori [48] measured radiative lifetimes of some of the  $3d^94p$  and  $3d^95s$  levels by a delayed coincidence technique and combined them with branching fractions, some of which were measured in a specially designed discharge tube, and some of which were obtained in a single-configuration LSF-adjusted intermediate-coupling calculation. These authors did not report separately their measured branching fractions, which impedes assessment of their results. Instead, they used all of their data, both experimental and theoretical, together, and adjusted the resulting  $A$ -values to satisfy the  $J$ -file sum rule. We renormalized several of their reported  $A$ -values to radiative lifetimes measured more accurately by Brown et al. [42], Pinnington et al. [51], and Cederquist et al. [43] and estimated the uncertainties by a method similar to the one described above in evaluation of results of Crespo López-Urrutia et al. [44].

Assessment of measurements made by Neger and Jäger [49] and by Hefferlin et al. [47] (hereafter referred to as N88 and H71) presented the greatest difficulties, since they grossly disagree with each other. N88 reported relative transition probabilities ( $A$ -values) of seven Cu II lines measured by using an axial discharge type of an exploding copper wire. The rather vague description of these measurements does not include the temperature value used in the data reduction. However, Neger and Jäger compare their results with those reported by Lux [60], obtained with similar equipment, and note that Lux determined the plasma temperature to be 26500(3500) K (2.3(3) eV) from a Boltzmann plot using several Cu I lines with known transition probabilities. The relative  $A$ -values reported by N88 (using the line at 4555.92 Å as reference) have uncertainties ranging from 18% to 25% and perfectly agree with those of Lux [60]. Thus, we assumed that they used Lux's temperature value in their data reduction and restored the observed line intensities from the reported line ratios and this temperature. Two of the lines reported in N88 are in common with more accurate measurements of Ortiz et al. [50].

Hefferlin et al. [47] (H71) determined relative intensities of 11 Cu II lines from photoelectric radiance measurements on the Burnout V experimental magnetic-confinement fusion reactor at the Oak Ridge National Laboratory. To derive the relative  $\log(gf)$  values from these measurements, they assumed the electron temperature to be 67 eV ( $\pm 50\%$ ). Neger and Jäger [49] blamed this large uncertainty in the temperature value for the discrepancy of the H71 results with theirs. We note that  $\text{Cu}^+$  should be completely ionized at this high temperature. Thus, an obvious path would be to dismiss the results of H71 as erroneous. However, their reported relative  $\log(gf)$  values appear to be internally consistent and agree well with other independent estimates. Thus, we restored the observed line intensities from them, using the 67 eV temperature as reported in H71, and attempted to reconcile the two sets of relative intensities (from H71 and N88) by using the following procedure.

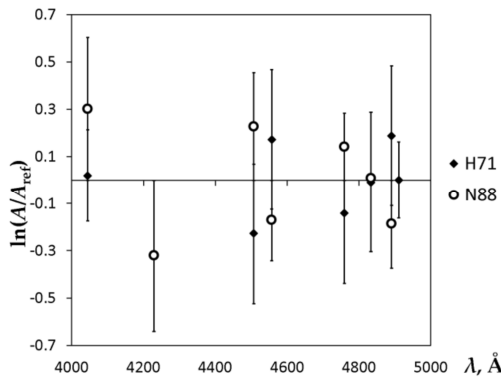
As a first step, to determine initial estimates of the excitation temperatures in H71 and N88, we used Boltzmann plots with reference  $A$ -values for the lines at 4043.48 Å and 4227.94 Å from Ortiz et al. [50], and for the line at 4909.73 Å from Cederquist et al. [43], while for all other lines we used our Cowan-code calculations. As a second step, using the temperatures derived from these

Boltzmann plots, we determined the adjusted  $A$ -values from the H71 and N88 observed line intensities. Then we replaced the Cowan-code  $A$ -values in the reference set with logarithmic means of thus obtained H71 and N88 adjusted  $A$ -values and found adjusted temperature values from the Boltzmann plots. The second step was repeated iteratively until reasonable convergence, i.e., until the change in the temperature values between iterations decreased below 0.001 eV. The final Boltzmann plots for H71 and N88 are shown in Figure 4a,b, respectively.



**Figure 4.** Boltzmann plots for relative intensities of observed lines: (a) Measurements of Hefferlin et al. [47] (H71); (b) Measurements of Neger and Jäger [49] (N88). The  $A$ -values used in these plots are the final adopted values given in Table A1. The error bars are combined uncertainties of  $A$ -values and relative intensities (see text).

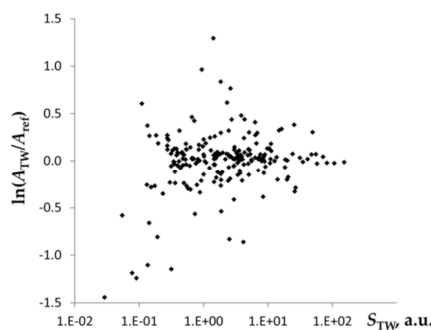
The excitation temperatures determined for the H71 and N88 data sets are 0.662(5) eV and 1.4(5) eV, respectively. The latter is somewhat lower than the Lux [60] value used in N88, 2.3(3) eV. The final adjusted  $A$ -values deduced from the H71 and N88 data are compared with the adopted  $A$ -values in Figure 5. In this plot, the reference  $A$ -values used for the two leftmost lines (4043.48 Å and 4227.94 Å) and for the rightmost line at 4909.73 Å are from Ortiz et al. [50] and Cederquist et al. [43], while the rest of the lines use the mean of H71 and N88. The error bars are combined uncertainties of the measured line ratios and reference  $A$ -values. This plot shows that the adjusted  $A$ -values from H71 and N88 are consistent with each other, as well as with the adopted reference  $A$ -values.



**Figure 5.** Comparison of adjusted  $A$ -values deduced from the line ratios reported by Hefferlin et al. [47] (H71) and by Neger and Jäger [49] (N88). The error bars are combined uncertainties of the measured line ratios and adopted reference  $A$ -values.

With the reference data set constructed from data described above, assessment of uncertainties in the theoretical study by Biémont et al. [41] was relatively easy to do by plotting the ratio of the calculated values to the reference ones against line strength  $S$  and calculating standard deviations for different ranges of  $S$ . This procedure resulted in estimated uncertainties of 9% for  $S \geq 8.5$  atomic units (a.u.), 22% for  $S = (0.2 \text{ to } 8.5)$  a.u., and 120% for  $S < 0.2$  a.u.

Assessment procedures described above resulted in 210 reference  $A$ -values with uncertainties less than 25% covering a wide range of line strengths from 0.06 a.u. to 155 a.u., after which it became possible to evaluate the uncertainties of our LSF calculations. Comparison of our calculated  $A$ -values with the reference ones is illustrated in Figure 6.



**Figure 6.** Comparison of transition probabilities calculated in this work ( $A_{TW}$ ) with reference values ( $A_{ref}$ , see text). Natural logarithm of the ratio  $A_{TW}/A_{ref}$  is plotted against our calculated line strength,  $S_{TW}$  (in atomic units).

This plot displays a typical behavior of theoretical transition probabilities. Namely, the strongest lines exhibit the smallest discrepancies from the reference values, while for weaker lines the magnitude of discrepancies grows. A similar comparison was made between  $A$ -values produced in our two LSFs (the final and preliminary ones, described in Section 3). From these comparisons, we estimated the uncertainties of our  $A$ -values to be  $\leq 10\%$  for  $S > 200$  a.u.,  $\leq 15\%$  for  $S = (50 \text{ to } 200)$  a.u.,  $\leq 30\%$  for  $S = (4.3 \text{ to } 50)$  a.u., and  $\geq 50\%$  for smaller  $S$ . We included 79 of our best calculated  $A$ -values in Table A1.

Studies of E1-forbidden transition probabilities of Cu II are very scarce. Garstang [46] calculated  $A$ -values for several M1 and E2 transitions from the first excited configuration,  $3d^9 4s$ , down to lower-lying levels of the same configuration and to the ground state,  $3d^{10} 1S_0$ . He used the pseudo-relativistic Hartree-Fock method with superposition of configurations and LSF-adjusted Slater parameters, similar to the one implemented in Cowan's codes [52] used in the present work, but limited by inclusion of only three low-lying configurations of even parity. Beck [61] made an ab initio restricted non-relativistic multiconfiguration Hartree-Fock calculation for the  $3d^{10} 1S_0 - 3d^9 4s \ ^1 3D_2$  E2 transition and obtained  $A = 2.33 \text{ s}^{-1}$ , somewhat larger than the sum of Garstang's values for transitions from  $^1 D_2$ ,  $1.7 \text{ s}^{-1}$ , and  $^3 D_2$ ,  $0.12 \text{ s}^{-1}$ . Prior [37] measured the  $A$ -value for the  $3d^{10} 1S_0 - 3d^9 4s \ ^1 D_2$  transition at  $3806.3 \text{ \AA}$  to be  $1.60(24) \text{ s}^{-1}$ , in excellent agreement with Garstang's semiempirical value. The most recent multiconfiguration Dirac-Hartree-Fock calculation of Andersson et al. [40] gave  $A = 1.937 \text{ s}^{-1}$  for this transition. However, their calculated wavelength is  $3724.7 \text{ \AA}$ , significantly shorter than experimental. Adjustment to the experimental wavelength yields  $A_{adj} = 1.74 \text{ s}^{-1}$ , in good agreement with Prior [37] and Garstang [46]. A similar adjustment of the value of Andersson et al. [40] for the  $3d^{10} 1S_0 - 3d^9 4s \ ^3 D_2$  transition at  $4375.8 \text{ \AA}$  (which Andersson et al. [40] calculated to be at  $4275.8 \text{ \AA}$ ) gives  $A_{adj} = 0.093 \text{ s}^{-1}$ , about 30% lower than Garstang's result. For these two E2 transitions, our  $A$ -values calculated with Cowan's codes are too high by a factor of about 1.7. We assume that our  $A$ -value for the predicted  $3d^9 4s \ ^3 D_3 - ^3 D_1$  E2 transition at  $48318 \text{ \AA}$ ,  $9 \times 10^{-8} \text{ s}^{-1}$ , has a similar

low accuracy. The  $3d^{10} 1S_0-3d^9 4s 1D_2$  transition at 3806.3 Å was observed by Thackeray [3] and by McKenna et al. [5] in emission spectra of nebulae.

It should be noted that, in addition to the two E2 transitions mentioned above, Andersson et al. [40] give calculated  $A$ -values for the magnetic-octupole (M3) and hyperfine-induced  $3d^{10} 1S_0-3d^9 4s 3D_3$  transitions at 4559 Å. The latter are different for various HFS components of the two isotopes ( $^{63}\text{Cu}$  and  $^{65}\text{Cu}$ ) and are typically on the order of a few times  $10^{-9} \text{ s}^{-1}$ , three orders of magnitude greater than for the M3 transition. This transition, as well as the  $3d^{10} 1S_0-3d^9 4s 3D_2$  E2 transition at 4375.8 Å, was observed by Aller et al. [4] in the spectrum of the RR Telescopii nebula.

$A$ -values for M1 transitions are relatively easier to calculate than E1 and E2 transitions, since their calculation does not involve radial integrals, but only amplitudes of eigenvector components. We compared our calculated  $A$ -values for M1 transitions with those of Garstang [46] and found that all of them agree to better than 15%. We included in Table A1 our  $A$ -value for the  $3d^{10} 1S_0-3d^9 4s 3D_1$  M1 transition at 4165.7 Å, which was not given by Garstang [46]. It turned out to be extremely small,  $2.1 \times 10^{-12} \text{ s}^{-1}$ . Our calculation indicates that there is no E2 contribution to the total decay rate of the  $3d^9 4s 3D_1$  level. This makes the identification of the line observed at this wavelength by McKenna et al. [5] with this transition questionable. Possible explanations for this observation could be (1) our calculated M1  $A$ -value is greatly underestimated; (2) there is a considerable contribution of E2 transition to this line, which for unknown reason is computed as negligibly small by Cowan's codes; (3) hyperfine-induced transition significantly increases the total radiative rate; (4) the population of the  $3d^9 4s 3D_1$  level in RR Telescopii is many orders of magnitude greater than that of  $3D_2$  and  $1D_2$ ; or (5) the identification is incorrect, and the observed line is possibly due to some other species. As explained above, the first explanation is rather unlikely. To confirm or disprove the second and third explanations, more extensive atomic calculations are needed, while checking the fourth one requires population-kinetics modeling.

## 7. Conclusions

The present work provides a comprehensive list of all observed, classified, and predicted spectral lines of Cu II, which includes 2557 transitions with wavelengths from 675 Å to 10.9 μm. Over 600 of them were measured in this work using grating and Fourier-transform spectrometers. Experimental wavelengths of 2443 transitions were used in a least-squares level optimization procedure to produce optimized values for 379 energy levels, of which 29 are newly identified, and nine are revised. The previous analysis of Ross [2,16] is largely confirmed. However, our extended base for the levels optimization results in more dependable level values and Ritz wavelengths that can be used as secondary standards in the vacuum ultraviolet region. An improved theoretical interpretation of the energy levels was made by a parametric least-squares fitting with Cowan's atomic codes, which included all experimental levels. The fitted Slater parameters were used to calculate radiative transition probabilities for electric-dipole, magnetic-dipole, and electric-quadrupole transitions, which were critically evaluated together with other published data to construct a list of recommended  $A$ -values for 555 transitions.

**Acknowledgments:** This work was partially supported by the National Aeronautics and Space Administration (NASA) under interagency agreement NNH10AN38I.

**Author Contributions:** All authors contributed equally to this work.

**Conflicts of Interest:** The authors declare no conflict of interest.

Appendix A

Table A1. Spectral lines of Cu II.

$\lambda_{\text{obs}}^a$ (Å)	$\sigma_{\text{obs}}^b$ (cm <sup>-1</sup> )	$\lambda_{\text{Ritz}}^c$ (Å)	$\Delta\lambda_{\text{obs-Ritz}}^d$ (Å)	$I_{\text{obs}}^d$ (arb. u.)	Char <sup>e</sup>	Lower Level	Upper Level	A (s <sup>-1</sup> )	Acc <sup>f</sup>	Line Ref. §	TP Ref. §	Notes <sup>h</sup>
675.5994(20)	148016(74)	675.60192(8)	-0.0025	73000		d <sup>10</sup>	<sup>1</sup> S <sub>0</sub>	(3/2) <sup>-1</sup> 3/2 <sup>1</sup> <sub>0</sub>		TW		
677.675(3)	147853(36)	677.67816(8)	-0.003	29000		d <sup>10</sup>	<sup>1</sup> S <sub>0</sub>	(5/2) <sup>-1</sup> 3/2 <sup>1</sup> <sub>0</sub>		TW		7p
685.1377(20)	145956(14)	685.14058(8)	-0.0029	240000		d <sup>10</sup>	<sup>1</sup> S <sub>0</sub>	(5/2) <sup>-1</sup> 3/2 <sup>1</sup> <sub>0</sub>		TW		5f
685.3922(20)	145901(94)	685.39671(8)	-0.0045	45000		d <sup>10</sup>	<sup>1</sup> S <sub>0</sub>	(3/2) <sup>-1</sup> 1/2 <sup>1</sup> <sub>1</sub>		TW		5f
709.3098(20)	140982(14)	709.31287(9)	-0.0031	250000		d <sup>10</sup>	<sup>1</sup> S <sub>0</sub>	(3/2) <sup>-1</sup> 1/2 <sup>1</sup> <sub>1</sub>		TW		5p
718.1766(20)	139241(54)	718.17860(9)	-0.0020	310000		d <sup>10</sup>	<sup>1</sup> S <sub>0</sub>	(5/2) <sup>-1</sup> 3/2 <sup>1</sup> <sub>1</sub>		TW		5p
724.4881(20)	724.48867(9)	724.48867(9)	0.0000	490000		d <sup>10</sup>	<sup>1</sup> S <sub>0</sub>	(3/2) <sup>-1</sup> 3/2 <sup>1</sup> <sub>1</sub>		TW		5p
735.5215(11)	135957.95(20)	735.52023(9)	0.0013	780000		d <sup>10</sup>	<sup>1</sup> S <sub>0</sub>	(5/2) <sup>-1</sup> 3/2 <sup>1</sup> <sub>0</sub>		TW		4f
736.0331(8)	135863.46(16)	736.03185(9)	0.0012	870000		d <sup>10</sup>	<sup>1</sup> S <sub>0</sub>	(3/2) <sup>-1</sup> 1/2 <sup>1</sup> <sub>0</sub>		TW		4f
763.2658(20)	131016(03)	763.2692(3)	-0.0034	140000		4s	<sup>3</sup> D <sub>3</sub>	(3/2) <sup>-1</sup> 3/2 <sup>1</sup> <sub>2</sub>		TWn		3p
768.4821(20)	130126(63)	768.48565(19)	-0.0035	150000		4s	<sup>3</sup> D <sub>3</sub>	(3/2) <sup>-1</sup> 3/2 <sup>1</sup> <sub>2</sub>		TWn		3p
776.484(3)	128785(63)	776.4877(3)	-0.0034	58000		4s	<sup>3</sup> D <sub>1</sub>	(3/2) <sup>-1</sup> 3/2 <sup>1</sup> <sub>0</sub>		TWn		3p
777.579(3)	128577(85)	777.5833(3)	-0.004	56000		4s	<sup>3</sup> D <sub>2</sub>	(3/2) <sup>-1</sup> 3/2 <sup>1</sup> <sub>1</sub>		TW		3p
779.2932(20)	128321.4(3)	779.29473(5)	-0.0015	590000		4s	<sup>3</sup> D <sub>3</sub>	(5/2) <sup>-1</sup> 3/2 <sup>1</sup> <sub>1</sub>		TW		3p
779.328(3)	128315.6(5)	779.33660(4)	-0.008	480000		4s	<sup>3</sup> D <sub>2</sub>	(5/2) <sup>-1</sup> 1/2 <sup>1</sup> <sub>1</sub>		TWn		3p
784.9098(20)	127403.2(3)	784.91229(5)	-0.0025	69000		4s	<sup>3</sup> D <sub>3</sub>	(1D) <sup>-1</sup> 3/2 <sup>1</sup> <sub>1</sub>		TW		3p
786.392(3)	127163.1(5)	786.39222(4)	-0.000	21000	*	4s	<sup>3</sup> D <sub>1</sub>	(5/2) <sup>-1</sup> 1/2 <sup>1</sup> <sub>0</sub>		TWn		6f
786.392(3)	127163.1(5)	786.39795(4)	-0.006	21000	*	4s	<sup>1</sup> D <sub>2</sub>	(3/2) <sup>-1</sup> 3/2 <sup>1</sup> <sub>2</sub>		TW		6f
787.907(3)	126918.5(5)	787.9056(5)	0.001	33000		4s	<sup>3</sup> D <sub>2</sub>	(3/2) <sup>-1</sup> 3/2 <sup>1</sup> <sub>1</sub>		TWn		7p
788.012(3)	126901.6(5)	788.01778(20)	-0.006	45000		4s	<sup>1</sup> D <sub>2</sub>	(1D) <sup>-1</sup> 3/2 <sup>1</sup> <sub>1</sub>		TWn		3p
789.3937(20)	126679.5(3)	789.3933(3)	0.0004	100000	*	4s	<sup>1</sup> D <sub>2</sub>	(3/2) <sup>-1</sup> 3/2 <sup>1</sup> <sub>2</sub>		TWn		3p
789.3937(20)	126679.5(3)	789.3977(3)	-0.0040	100000	*	4s	<sup>3</sup> D <sub>2</sub>	(3/2) <sup>-1</sup> 5/2 <sup>1</sup> <sub>2</sub>		TWn		3p
789.6575(20)	126637.2(3)	789.65867(5)	-0.0011	59000		4s	<sup>3</sup> D <sub>3</sub>	(3/2) <sup>-1</sup> 1/2 <sup>1</sup> <sub>1</sub>		TWn		7p
794.9719(20)	125790.6(3)	794.97430(20)	-0.0024	56000		4s	<sup>1</sup> D <sub>2</sub>	(5/2) <sup>-1</sup> 3/2 <sup>1</sup> <sub>2</sub>		TWn		8p
797.4530(20)	125399.2(3)	797.45498(4)	-0.0020	560000		4s	<sup>3</sup> D <sub>3</sub>	(5/2) <sup>-1</sup> 3/2 <sup>1</sup> <sub>2</sub>		TW		7p
797.6193(20)	125373.1(3)	797.6218(5)	-0.0025	35000		4s	<sup>3</sup> D <sub>1</sub>	(3/2) <sup>-1</sup> 1/2 <sup>1</sup> <sub>0</sub>		TWn		7p
798.977(3)	125160.0(5)	798.97928(3)	-0.002	23000		4s	<sup>1</sup> D <sub>2</sub>	(3/2) <sup>-1</sup> 3/2 <sup>1</sup> <sub>1</sub>		TW		8p
800.6592(20)	124897.1(3)	800.66084(5)	-0.0017	26000		4s	<sup>1</sup> D <sub>2</sub>	(5/2) <sup>-1</sup> 3/2 <sup>1</sup> <sub>1</sub>		TWn		8p
801.8229(20)	124715.8(3)	801.82460(4)	-0.0017	84000		4s	<sup>3</sup> D <sub>2</sub>	(5/2) <sup>-1</sup> 3/2 <sup>1</sup> <sub>1</sub>		TW		7p
803.3370(20)	124480.8(3)	803.33841(4)	-0.0014	77000		4s	<sup>3</sup> D <sub>3</sub>	(5/2) <sup>-1</sup> 3/2 <sup>1</sup> <sub>2</sub>		TW		7p
806.5454(20)	123985.6(3)	806.54699(5)	-0.0016	180000		4s	<sup>1</sup> D <sub>2</sub>	(1D) <sup>-1</sup> 3/2 <sup>1</sup> <sub>2</sub>		TW		8p
809.2942(20)	123564.5(3)	809.29524(4)	-0.0011	17000		4s	<sup>3</sup> D <sub>1</sub>	(5/2) <sup>-1</sup> 3/2 <sup>1</sup> <sub>0</sub>		TW		7p
809.706(3)	123501.6(5)	809.7079(3)	-0.002	12000		4s	<sup>1</sup> D <sub>2</sub>	(3/2) <sup>-1</sup> 3/2 <sup>1</sup> <sub>0</sub>		TWn		7p
809.9630(20)	123462.4(3)	809.9649(3)	-0.0019	45000		4s	<sup>1</sup> D <sub>2</sub>	(3/2) <sup>-1</sup> 3/2 <sup>1</sup> <sub>1</sub>		TWn		7p
810.9987(20)	123304.8(3)	810.99829(11)	0.0004	520000		d <sup>10</sup>	<sup>1</sup> S <sub>0</sub>	(3/2) <sup>-1</sup> 3/2 <sup>1</sup> <sub>1</sub>		TWn		5p
810.6361(3)	123359.8(3)	810.6361(3)	0.0005	86000		4s	<sup>1</sup> D <sub>2</sub>	(3/2) <sup>-1</sup> 3/2 <sup>1</sup> <sub>1</sub>		TWn		7p
811.2843(20)	123261.4(3)	811.2839(4)	0.0004	110000		4s	<sup>1</sup> D <sub>2</sub>	(3/2) <sup>-1</sup> 5/2 <sup>1</sup> <sub>2</sub>		TWn		7p
811.5559(20)	123220.1(3)	811.55946(5)	-0.0036	13000		4s	<sup>1</sup> D <sub>2</sub>	(3/2) <sup>-1</sup> 1/2 <sup>1</sup> <sub>0</sub>		TWn		7p

Table A1. Cont.

$\lambda_{\text{obs}}^a$ (Å)	$\sigma_{\text{obs}}^b$ (cm <sup>-1</sup> )	$\lambda_{\text{Tit}}^c$ (Å)	$\Delta\lambda_{\text{obs-Ritz}}^d$ (Å)	$I_{\text{obs}}^d$ (arb. u.)	Char <sup>e</sup>	Lower Level	Upper Level	A (g <sup>-1</sup> )	Acc <sup>f</sup>	Line Ref. #	TP Ref. #	Notes <sup>h</sup>
813.882(3)	122867(94)	813.88328(11)	-0.001	760000	d <sup>10</sup>	1s <sub>0</sub>	5p	(3/2) <sup>+</sup> 1/2 <sup>1</sup> <sub>1</sub>		TW		
823.059(3)	121497(94)	823.05584(4)	0.004	2000	4s	1D <sub>2</sub>	7p	(5/2) <sup>+</sup> 15/2 <sup>1</sup> <sub>3</sub>		TW		
823.8361(18)	1213831(4)	823.83758(6)	-0.0015	90000	4s	1D <sub>2</sub>	7p	(5/2) <sup>+</sup> 15/2 <sup>1</sup> <sub>2</sub>		TW		
824.4127(20)	121298.5(3)	824.41507(4)	-0.0024	6100	4s	1D <sub>2</sub>	7p	(5/2) <sup>+</sup> 13/2 <sup>1</sup> <sub>1</sub>		TW		
824.6630(19)	121261.7(3)	824.6649(4)	-0.0019	90000	4s	1D <sub>2</sub>	7p	(5/2) <sup>+</sup> 17/2 <sup>1</sup> <sub>3</sub>		TWn		
826.014(3)	121063.3(5)	826.01546(5)	-0.001	4400	4s	1D <sub>2</sub>	7p	(5/2) <sup>+</sup> 13/2 <sup>1</sup> <sub>2</sub>		TW		
826.9946(22)	120919.8(3)	826.99598(12)	-0.0014	1100000	d <sup>10</sup>	1s <sub>0</sub>	5p	(5/2) <sup>+</sup> 13/2 <sup>1</sup> <sub>1</sub>		TW		
829.360(5)	120750(8)	829.35106(14)	0.008	7400	4s	3D <sub>2</sub>	3p	(G) <sup>3</sup> P <sup>3</sup> G <sup>3</sup>		TWn		
836.042(20)	119611(3)	836.02765(3)	0.014	27000	4s	3D <sub>2</sub>	3p	(3/2) <sup>+</sup> 13/2 <sup>1</sup> <sub>2</sub>		S6ec		
841.136(3)	118886.8(4)	841.13445(3)	0.002	30000	4s	3D <sub>2</sub>	3p	(3/2) <sup>+</sup> 13/2 <sup>1</sup> <sub>1</sub>		TW		
842.4973(24)	118694.7(3)	842.49630(3)	0.0010	66000	4s	3D <sub>2</sub>	3p	(3/2) <sup>+</sup> 13/2 <sup>1</sup> <sub>2</sub>		TW		
844.6125(21)	118397.5(3)	844.61287(4)	-0.0003	88000	4s	3D <sub>2</sub>	3p	(3/2) <sup>+</sup> 15/2 <sup>1</sup> <sub>2</sub>		TW		
844.9124(21)	118355.5(3)	844.91208(4)	0.0003	410000	4s	3D <sub>2</sub>	3p	(3/2) <sup>+</sup> 15/2 <sup>1</sup> <sub>3</sub>		TW		
848.8062(20)	117812.5(3)	848.80734(3)	-0.0011	920000	4s	3D <sub>2</sub>	3p	(5/2) <sup>+</sup> 15/2 <sup>1</sup> <sub>3</sub>		TW		
849.3599(19)	117735.7(3)	849.35931(3)	0.0006	240000	4s	3D <sub>1</sub>	3p	(3/2) <sup>+</sup> 13/2 <sup>1</sup> <sub>1</sub>		TW		
850.7481(19)	117543.6(3)	850.74794(3)	0.0001	140000	4s	3D <sub>1</sub>	3p	(3/2) <sup>+</sup> 13/2 <sup>1</sup> <sub>2</sub>		TW		
851.3012(16)	117467.24(23)	851.30253(3)	-0.0013	1100000	4s	3D <sub>2</sub>	3p	(5/2) <sup>+</sup> 17/2 <sup>1</sup> <sub>4</sub>		TW		
851.776(3)	117401.8(4)	851.77122(3)	0.004	21000	4s	3D <sub>3</sub>	3p	(G) <sup>3</sup> P <sup>3</sup> F <sup>3</sup>		TW		
852.9074(21)	117246.0(3)	852.90622(4)	0.0012	370000	4s	3D <sub>1</sub>	3p	(3/2) <sup>+</sup> 15/2 <sup>1</sup> <sub>2</sub>		TW		
853.5444(24)	117158.5(3)	853.54260(15)	0.0018	45000	4s	1D <sub>2</sub>	3p	(G) <sup>3</sup> P <sup>3</sup> G <sup>3</sup>		TWn		
855.4770(19)	116893.9(3)	855.47652(24)	0.0009	270000	4s	3D <sub>2</sub>	3p	(5/2) <sup>+</sup> 15/2 <sup>1</sup> <sub>3</sub>		TW		
855.6994(21)	116863.5(3)	855.70010(3)	-0.0007	720000	4s	3D <sub>2</sub>	3p	(3p) <sup>3</sup> P <sup>3</sup> F <sup>3</sup> <sub>2</sub>		TW		
858.4844(20)	116484.4(3)	858.48671(24)	-0.0024	990000	4s	3D <sub>2</sub>	3p	(G) <sup>3</sup> P <sup>3</sup> F <sup>3</sup> <sub>3</sub>		TW		
858.5639(20)	116473.6(3)	858.566433(20)	-0.0025	890000	4s	3D <sub>2</sub>	3p	(5/2) <sup>+</sup> 17/2 <sup>1</sup> <sub>3</sub>		TW		
859.1522(24)	116393.8(3)	859.15072(3)	0.0014	14000	4s	3D <sub>2</sub>	3p	(5/2) <sup>+</sup> 13/2 <sup>1</sup> <sub>1</sub>		TW		
860.7214(24)	116181.6(3)	860.72158(4)	-0.0001	22000	4s	3D <sub>2</sub>	3p	(5/2) <sup>+</sup> 15/2 <sup>1</sup> <sub>2</sub>		TW		
861.9932(11)	116010.19(14)	861.99338(6)	-0.0002	1900000	4s	3D <sub>3</sub>	3p	(G) <sup>3</sup> P <sup>3</sup> F <sup>3</sup> <sub>4</sub>		TW		
862.8221(20)	115898.7(3)	862.82245(4)	-0.0003	78000	4s	3D <sub>2</sub>	3p	(5/2) <sup>+</sup> 13/2 <sup>1</sup> <sub>2</sub>		TW		
864.163(4)	115718.9(5)	864.15435(3)	0.009	130000	4s	3D <sub>3</sub>	3p	(3p) <sup>3</sup> P <sup>3</sup> D <sup>3</sup> <sub>2</sub>		TW		
864.214(3)	115712.0(4)	864.21371(3)	0.001	670000	4s	3D <sub>1</sub>	3p	(3p) <sup>3</sup> P <sup>3</sup> F <sup>3</sup> <sub>2</sub>		TW		
865.3907(8)	115554.74(11)	865.38986(23)	0.0007	1600000	4s	3D <sub>2</sub>	3p	(5/2) <sup>+</sup> 17/2 <sup>1</sup> <sub>3</sub>		K66		
866.4430(20)	115414.4(3)	866.442524(13)	0.0005	64000	4s	3D <sub>1</sub>	4f	(5/2) <sup>+</sup> 17/2 <sup>1</sup> <sub>3</sub>		TW		
867.7321(21)	115242.9(3)	867.73348(3)	-0.0014	320000	4s	3D <sub>1</sub>	4f	(5/2) <sup>+</sup> 13/2 <sup>1</sup> <sub>1</sub>		TW		
869.0634(18)	115066.40(24)	869.06394(3)	-0.0005	250000	4s	3D <sub>2</sub>	3p	(3F) <sup>3</sup> D <sup>3</sup> <sub>1</sub>		TW		
869.3338(24)	115030.6(3)	869.33592(4)	-0.0021	1200000	4s	3D <sub>1</sub>	3p	(5/2) <sup>+</sup> 15/2 <sup>1</sup> <sub>2</sub>		TW		
870.5390(18)	114871.37(24)	870.538673(24)	0.0003	240000	4s	3D <sub>2</sub>	3p	(3p) <sup>3</sup> D <sup>3</sup> <sub>2</sub>		TW		
871.0674(18)	114801.68(24)	871.06737(3)	0.0000	130000	4s	3D <sub>2</sub>	3p	(3p) <sup>3</sup> P <sup>3</sup> D <sup>3</sup> <sub>2</sub>		TW		
873.2629(21)	114513.0(3)	873.262654(21)	0.0003	310000	4s	3D <sub>3</sub>	3p	(3p) <sup>3</sup> P <sup>3</sup> F <sup>3</sup> <sub>3</sub>		TW		
876.7226(20)	114061.2(3)	876.722456(13)	0.0002	830000	4s	3D <sub>2</sub>	4f	(5/2) <sup>+</sup> 17/2 <sup>1</sup> <sub>3</sub>		TW		

Table A1. Cont.

$\lambda_{\text{obs}}^a$ (Å)	$\epsilon_{\text{obs}}^b$ ( $\text{cm}^{-1}$ )	$\lambda_{\text{lit}}^c$ (Å)	$\Delta\lambda_{\text{obs-lit}}^d$ (Å)	Char <sup>e</sup>	Lower Level	Upper Level	A ( $\text{s}^{-1}$ )	Acc <sup>f</sup>	Line Ref. #	TP Ref. #	Notes <sup>h</sup>
876.973(5)	114028(67)	876.962109(24)	0.011		4s	3D <sub>1</sub>	(3/2) <sup>3</sup> P <sup>o</sup> <sub>2</sub> 1 <sup>o</sup>		TW		
877.0107(24)	114023.7(3)	877.01184(4)	-0.0012		4s	3D <sub>3</sub>	( <sup>3</sup> P) <sup>o</sup> 3S <sub>2</sub>		TW		
877.5531(20)	113953.2(3)	877.554632(23)	-0.0015		4s	3D <sub>2</sub>	( <sup>3</sup> F) <sup>o</sup> 3D <sub>2</sub>		TW		
877.8469(21)	113915.1(3)	877.84692(3)	0.0000		4s	3D <sub>1</sub>	( <sup>3</sup> F) <sup>o</sup> 3D <sub>1</sub>		TW		
878.6984(8)	113804.69(10)	878.69833(3)	0.0001		4s	3D <sub>3</sub>	( <sup>3</sup> F) <sup>o</sup> 3D <sub>3</sub>		K66		
879.8897(24)	113650.6(3)	879.89110(3)	-0.0014		4s	3D <sub>1</sub>	( <sup>3</sup> P) <sup>o</sup> 3D <sub>2</sub>		TW		
880.3225(24)	113594.7(3)	880.322766(20)	-0.0003		4s	3D <sub>2</sub>	( <sup>3</sup> P) <sup>o</sup> 3P <sub>2</sub>		TW		
881.473(5)	113446.4(4)	881.47711(3)	-0.004		4s	3D <sub>3</sub>	( <sup>3</sup> F) <sup>o</sup> 3P <sub>2</sub>		TW		
883.280(20)	113214.4(3)	883.27981(3)	0.0002		4s	3D <sub>1</sub>	( <sup>3</sup> G) <sup>o</sup> 3P <sub>2</sub>		TW,S36r		
883.840(20)	113142.6(3)	883.83830(10)	0.0016		4s	3D <sub>2</sub>	(5/2) <sup>3</sup> F <sup>o</sup> <sub>2</sub> 1 <sup>o</sup> <sub>3</sub>		TW		
884.1340(21)	113105.0(3)	884.13295(4)	0.0011		4s	3D <sub>2</sub>	( <sup>3</sup> P) <sup>o</sup> 3S <sub>2</sub>		TW		
884.4346(18)	113066.58(23)	884.43449(3)	0.0001		4s	3D <sub>3</sub>	( <sup>3</sup> G) <sup>o</sup> 3P <sub>2</sub>		TW		
884.8262(20)	113016.5(3)	884.826019(13)	0.0002		4s	3D <sub>2</sub>	(5/2) <sup>3</sup> F <sup>o</sup> <sub>1</sub> 1 <sup>o</sup> <sub>3</sub>		TW		
885.8463(20)	112886.4(3)	885.846966(24)	-0.0006		4s	3D <sub>2</sub>	( <sup>3</sup> P) <sup>o</sup> 3D <sub>3</sub>		TW		
886.4163(24)	112813.8(3)	886.413782(20)	0.0025		4s	3D <sub>3</sub>	( <sup>3</sup> F) <sup>o</sup> 3P <sub>2</sub>		TW		
886.5113(20)	112801.7(3)	886.510950(24)	0.0004		4s	3D <sub>1</sub>	( <sup>3</sup> P) <sup>o</sup> 3D <sub>2</sub>		TW		
886.9435(8)	112746.75(10)	886.94322(3)	0.0003		4s	3D <sub>3</sub>	( <sup>3</sup> P) <sup>o</sup> 3D <sub>2</sub>		K66		
891.5677(6)	112287.93(8)	891.56671(3)	0.0010		4s	3D <sub>2</sub>	( <sup>3</sup> P) <sup>o</sup> 3P <sub>2</sub>		K66		
891.7636(24)	112137.3(3)	891.76309(3)	0.0005		4s	3D <sub>3</sub>	(5/2) <sup>3</sup> F <sup>o</sup> <sub>2</sub> 1 <sup>o</sup> <sub>3</sub>		TW		
892.4154(6)	112055.44(8)	892.41418(3)	0.0012		4s	3D <sub>3</sub>	( <sup>3</sup> P) <sup>o</sup> 3D <sub>3</sub>		K66		
893.634(5)	111902.7(7)	893.624985(19)	0.0009		4s	3D <sub>1</sub>	(5/2) <sup>3</sup> F <sup>o</sup> <sub>1</sub> 1 <sup>o</sup> <sub>3</sub>		TW		
893.6787(6)	111897.04(8)	893.67746(3)	0.0012		4s	3D <sub>3</sub>	( <sup>3</sup> P) <sup>o</sup> 3P <sub>2</sub>		K66		
894.2260(20)	111828.58(25)	894.227192(24)	-0.0012		4s	3D <sub>2</sub>	( <sup>3</sup> P) <sup>o</sup> 3D <sub>2</sub>		TW		
896.7583(15)	111512.77(19)	896.758608(23)	-0.0003		4s	3D <sub>3</sub>	( <sup>3</sup> P) <sup>o</sup> 3D <sub>1</sub>		TW		
896.9741(20)	111485.94(25)	896.97600(3)	-0.0019		4s	3D <sub>1</sub>	( <sup>3</sup> P) <sup>o</sup> 3P <sub>2</sub>		TW		
897.7927(18)	111384.29(22)	897.79300(3)	-0.0003		4s	1D <sub>2</sub>	( <sup>3</sup> P) <sup>o</sup> 3P <sub>0</sub>		TW		
899.7904(18)	111136.99(22)	899.78867(3)	0.0018	*	4s	3D <sub>2</sub>	( <sup>3</sup> P) <sup>o</sup> 3D <sub>2</sub>		TW		
899.7904(18)	111136.99(22)	899.79200(3)	-0.0016	*	4s	3D <sub>1</sub>	( <sup>3</sup> P) <sup>o</sup> 3P <sub>2</sub>		TW		
901.0757(16)	110978.47(20)	901.07654(7)	-0.0009	*	4s	1D <sub>2</sub>	( <sup>3</sup> P) <sup>o</sup> 3P <sub>1</sub>		TW		
901.0757(16)	110978.47(20)	901.07292(3)	0.0027	*	4s	3D <sub>2</sub>	( <sup>3</sup> P) <sup>o</sup> 3P <sub>2</sub>		TW,S36r		
901.322(3)	110948.2(4)	901.32128(3)	0.000		4s	1D <sub>2</sub>	( <sup>3</sup> P) <sup>o</sup> 3P <sub>2</sub>		TW		
903.522(6)	110678.0(7)	903.52887(3)	-0.007		4s	3D <sub>1</sub>	( <sup>3</sup> G) <sup>o</sup> 3P <sub>2</sub>		TWn		
906.1130(20)	110361.52(24)	906.11330(3)	-0.0003		4s	3D <sub>1</sub>	( <sup>3</sup> P) <sup>o</sup> 3D <sub>2</sub>		S36c		
910.5183(21)	109827.58(25)	910.51831(3)	-0.0000		4s	3D <sub>3</sub>	( <sup>3</sup> P) <sup>o</sup> 3D <sub>1</sub>		TW		
911.630	109693.6	911.629867(16)	0.0000	:	4s	1D <sub>2</sub>	(5/2) <sup>3</sup> F <sup>o</sup> <sub>2</sub> 1 <sup>o</sup> <sub>3</sub>		S36c		
911.679	109687.2	911.67901(4)	15000	:	4s	1D <sub>2</sub>	( <sup>3</sup> P) <sup>o</sup> 3S <sub>2</sub>		S36c		
912.025	109646.2	912.024525(12)	7400	:	4s	1D <sub>2</sub>	(5/2) <sup>3</sup> F <sup>o</sup> <sub>2</sub> 1 <sup>o</sup> <sub>3</sub>		S36c		
912.4142(24)	109599.5(3)	912.415956(16)	-0.0018		4s	1D <sub>2</sub>	(3/2) <sup>3</sup> F <sup>o</sup> <sub>2</sub> 1 <sup>o</sup> <sub>3</sub>		TW		
913.47(4)	109472(5)	913.50160(3)	-0.03		4s	1D <sub>2</sub>	( <sup>3</sup> P) <sup>o</sup> 3D <sub>3</sub>		S36c		
914.2128(6)	109383.72(7)	914.21305(11)	-0.0003		4s	3D <sub>3</sub>	( <sup>3</sup> P) <sup>o</sup> 3D <sub>4</sub>		K66		

Table A1. Cont.

$\lambda_{\text{obs}}^a$ (Å)	$\sigma_{\text{obs}}^b$ (cm <sup>-1</sup> )	$\lambda_{\text{lit}}^c$ (Å)	$\Delta\lambda_{\text{obs-lit}}^d$ (Å)	$I_{\text{obs}}^d$ (arb. u.)	Char <sup>e</sup>	Lower Level	Upper Level	A (s <sup>-1</sup> )	Acc <sup>f</sup>	Line Ref. #	TP Ref. #	Notes <sup>h</sup>
917.3051(20)	10901.498(23)	917.30556(8)	-0.0004	380000		4s	3D <sub>3</sub>	(p) <sup>3</sup> p <sup>2</sup> 3D <sub>2</sub>		TW		
922.0188(8)	108457.66(9)	922.01869(14)	0.0001	520000		4s	3D <sub>2</sub>	(D) <sup>3</sup> p <sup>2</sup> 3P <sub>2</sub>		K66		
922.4141(16)	108411.18(19)	922.41586(3)	-0.0018	350000		4s	1D <sub>2</sub>	(p) <sup>3</sup> p <sup>2</sup> 3P <sub>2</sub>		TW		
924.2381(8)	108197.23(9)	924.23840(7)	-0.0003	550000		4s	3D <sub>2</sub>	(p) <sup>3</sup> p <sup>2</sup> 3D <sub>2</sub>		K66		
925.1191(10)	108094.20(12)	925.09896(8)	0.020	510000	*	4s	3D <sub>2</sub>	(p) <sup>3</sup> p <sup>2</sup> 3D <sub>2</sub>		TW		
925.1191(10)	108094.20(12)	925.10963(3)	0.009	510000	*	4s	1D <sub>2</sub>	(p) <sup>3</sup> p <sup>2</sup> 3D <sub>2</sub>		TW		
925.1191(10)	108094.20(12)	925.13612(7)	-0.007	510000	*	4s	3D <sub>2</sub>	(p) <sup>3</sup> p <sup>2</sup> 3D <sub>2</sub>		TW		
929.702(5)	107361.4(3)	929.70175(3)	0.000	18000		4s	1D <sub>2</sub>	(p) <sup>3</sup> p <sup>2</sup> 3P <sub>2</sub>		TW		
929.8940(20)	107539.14(23)	929.89272(14)	0.0013	18000		4s	3D <sub>2</sub>	(D) <sup>3</sup> p <sup>2</sup> 3P <sub>2</sub>		TW		
932.9398(6)	107188.05(9)	932.93989(10)	-0.0001	590000		4s	3D <sub>3</sub>	(D) <sup>3</sup> p <sup>2</sup> 3D <sub>3</sub>	1.7e+08	C	B00	
934.9761(18)	106954.61(18)	934.97102(14)	0.0050	280000	?	4s	3D <sub>1</sub>	(p) <sup>3</sup> p <sup>2</sup> 3D <sub>2</sub>		TWn		
935.0564(14)	106945.42(17)	935.05755(8)	-0.0012	380000		4s	3D <sub>1</sub>	(p) <sup>3</sup> p <sup>2</sup> 3D <sub>2</sub>		TW		
		935.08529(7)			m	4s	3D <sub>1</sub>	(p) <sup>3</sup> p <sup>2</sup> 3D <sub>2</sub>		S36c		
935.2307(22)	106925.48(25)	935.23232(7)	-0.0016	450000		4s	3D <sub>2</sub>	(D) <sup>3</sup> p <sup>2</sup> 3D <sub>2</sub>		TW		
935.3408(18)	106912.90(20)	935.34317(5)	-0.0023	360000		4s	3D <sub>2</sub>	(D) <sup>3</sup> p <sup>2</sup> 3P <sub>2</sub>		TW		
935.892(3)	106849.9(3)	935.89753(15)	-0.0026	620000		4s	3D <sub>3</sub>	(D) <sup>3</sup> p <sup>2</sup> 3P <sub>2</sub>	1.12e+08	C	B00	
937.815(6)	106630.8(7)	937.81726(7)	-0.002	48000		4s	3D <sub>3</sub>	(D) <sup>3</sup> p <sup>2</sup> 3P <sub>2</sub>		S36c		
939.5218(15)	106437.12(16)	939.52288(6)	-0.0010	190000		4s	3D <sub>3</sub>	(D) <sup>3</sup> p <sup>2</sup> 3P <sub>2</sub>		TW		
943.3333(18)	106007.07(20)	943.33466(7)	-0.0014	580000		4s	3D <sub>2</sub>	(D) <sup>3</sup> p <sup>2</sup> 3D <sub>2</sub>	1.4e+08	C	B00	
945.5223(17)	105761.65(19)	945.52474(6)	-0.0025	510000		4s	3D <sub>1</sub>	(D) <sup>3</sup> p <sup>2</sup> 3P <sub>2</sub>		TW		
945.8771(21)	105721.98(24)	945.87663(7)	0.0005	400000		4s	3D <sub>2</sub>	(D) <sup>3</sup> p <sup>2</sup> 3D <sub>2</sub>		TW		
945.9614(21)	105712.56(24)	945.96464(7)	-0.0033	460000		4s	3D <sub>2</sub>	(D) <sup>3</sup> p <sup>2</sup> 3P <sub>2</sub>	1.1e+08	C	B00	
947.6989(17)	105518.74(19)	947.70005(6)	-0.0011	14000		4s	3D <sub>2</sub>	(D) <sup>3</sup> p <sup>2</sup> 3P <sub>2</sub>		TW		
951.4068(15)	105107.51(16)	951.40774(8)	-0.0010	24000		4s	3D <sub>1</sub>	(D) <sup>3</sup> p <sup>2</sup> 3P <sub>2</sub>		TW		
954.3815(15)	104779.91(16)	954.38279(7)	-0.0013	270000		4s	1D <sub>2</sub>	(p) <sup>3</sup> p <sup>2</sup> 3D <sub>3</sub>		TW		
955.306(5)	104678.5(6)	955.30043(8)	0.005	9900		4s	1D <sub>2</sub>	(p) <sup>3</sup> p <sup>2</sup> 3D <sub>2</sub>		TW		
955.320(5)	104677.0(6)	955.32939(7)	-0.009	9900		4s	1D <sub>2</sub>	(p) <sup>3</sup> p <sup>2</sup> 3D <sub>2</sub>		TW		
956.287(17)	104571.11(19)	956.29010(7)	-0.0030	300000		4s	3D <sub>1</sub>	(p) <sup>3</sup> p <sup>2</sup> 3D <sub>1</sub>	1.8e+08	C	B00	
958.1503(17)	104367.76(19)	958.15393(6)	-0.0037	380000		4s	3D <sub>1</sub>	(D) <sup>3</sup> p <sup>2</sup> 3P <sub>2</sub>	1.6e+08	C	B00	
960.4115(17)	104112.04(19)	960.41317(15)	-0.0017	270000		4s	1D <sub>2</sub>	(D) <sup>3</sup> p <sup>2</sup> 3P <sub>2</sub>		TW		
966.2283(21)	103995.21(23)	966.22839(6)	-0.0001	11000		4s	1D <sub>2</sub>	(D) <sup>3</sup> p <sup>2</sup> 3P <sub>2</sub>		TW		
967.8711(21)	103319.54(23)	967.87255(7)	-0.0015	4800		4s	3D <sub>3</sub>	(p) <sup>3</sup> p <sup>2</sup> 3P <sub>2</sub>		TW		
968.0392(17)	103301.60(18)	968.04176(16)	-0.0025	250000		4s	3D <sub>3</sub>	(p) <sup>3</sup> p <sup>2</sup> 3P <sub>2</sub>		TW		
972.2703(19)	102852.06(20)	972.26872(10)	0.0016	24000		4s	1D <sub>2</sub>	(D) <sup>3</sup> p <sup>2</sup> 3D <sub>3</sub>		TW		
973.5091(10)	102721.2(11)	973.49928(20)	0.010	18000		4s	3D <sub>2</sub>	(p) <sup>3</sup> p <sup>2</sup> 3P <sub>1</sub>		S36c		
974.7581(15)	102589.56(15)	974.75876(8)	-0.0007	200000		4s	1D <sub>2</sub>	(D) <sup>3</sup> p <sup>2</sup> 3D <sub>2</sub>		TW		
976.5524(15)	102401.06(15)	976.55293(7)	-0.0005	110000		4s	3D <sub>2</sub>	(p) <sup>3</sup> p <sup>2</sup> 3P <sub>2</sub>		TW		
976.7238(17)	102383.09(18)	976.72519(17)	-0.0014	35000		4s	3D <sub>2</sub>	(p) <sup>3</sup> p <sup>2</sup> 3P <sub>2</sub>		TW		
977.5662(13)	102294.86(14)	977.56714(7)	-0.0009	190000		4s	1D <sub>2</sub>	(D) <sup>3</sup> p <sup>2</sup> 3P <sub>2</sub>		TW		
979.4200(15)	102101.25(16)	979.42055(6)	-0.0006	12000		4s	1D <sub>2</sub>	(D) <sup>3</sup> p <sup>2</sup> 3P <sub>2</sub>		TW		
984.02(4)	101624(4)	983.979887(19)	0.04	9100		4s	3D <sub>3</sub>	(s/2) <sup>3</sup> p <sup>2</sup> 3P <sub>2</sub>		S36c		
984.5331(15)	101570.98(15)	984.53339(21)	-0.0003	88000		4s	3D <sub>1</sub>	(p) <sup>3</sup> p <sup>2</sup> 3P <sub>1</sub>		TW		



Table A1. Cont.

$\lambda_{obs}^a$ (Å)	$\epsilon_{obs}^b$ (cm <sup>-1</sup> )	$\lambda_{lit}^c$ (Å)	$\Delta\lambda_{obs-lit}^d$ (Å)	Char <sup>e</sup>	Lower Level	Upper Level	A (s <sup>-1</sup> )	Acc <sup>f</sup>	Line Ref. #	TP Ref. #	Notes <sup>h</sup>
987.6568(12)	101249.75(12)	987.6567(8)	-0.0000	4s	3D <sub>1</sub>	3P <sup>o</sup> 3s <sup>o</sup> 3p <sup>o</sup> <sub>2</sub>			TW		
988.2364(12)	101088.07(12)	989.236270(17)	0.0002	4s	3D <sub>2</sub>	(3/2) <sup>o</sup> 15/21 <sup>o</sup> <sub>3</sub>			TW		
992.9530(13)	100709.70(13)	992.952929(16)	0.0001	4s	3D <sub>2</sub>	(3/2) <sup>o</sup> 15/21 <sup>o</sup> <sub>3</sub>			TW		
998.3067(14)	100169.62(14)	998.305876(14)	0.0008	4s	3D <sub>2</sub>	(3/2) <sup>o</sup> 15/21 <sup>o</sup> <sub>3</sub>			TW		
999.797(3)	100020.3(3)	999.793812(15)	0.003	4s	3D <sub>2</sub>	(3/2) <sup>o</sup> 11/21 <sup>o</sup> <sub>3</sub>			TW		
1001.0129(19)	99898.81(19)	1001.012710(14)	0.0002	4s	3D <sub>2</sub>	(3/2) <sup>o</sup> 15/21 <sup>o</sup> <sub>2</sub>			TW		
1004.0540(17)	99596.24(17)	1004.055195(18)	-0.0012	4s	3D <sub>3</sub>	(3P <sup>o</sup> 3p <sup>o</sup> 1F <sup>o</sup> ) <sub>3</sub>			TW		
1006.980(6)	99306.8(6)	1006.983925(18)	-0.004	4s	3D <sub>1</sub>	(3/2) <sup>o</sup> 13/21 <sup>o</sup> <sub>1</sub>			S3ec		
1008.5674(17)	99130.51(16)	1008.568623(17)	-0.0012	4s	3D <sub>2</sub>	(3/2) <sup>o</sup> 15/21 <sup>o</sup> <sub>3</sub>			TW		
1008.7274(17)	99134.81(16)	1008.728151(15)	-0.0008	4s	3D <sub>2</sub>	(3P <sup>o</sup> ) <sup>o</sup> 1D <sup>o</sup> <sub>2</sub>			TW		
1010.2680(17)	98983.64(16)	1010.26867(8)	-0.0007	4s	1D <sub>2</sub>	(3P <sup>o</sup> ) <sup>o</sup> 3p <sup>o</sup> <sub>2</sub>			TW		
1010.4520(18)	98965.61(18)	1010.45303(18)	-0.0011	4s	1D <sub>2</sub>	(3P <sup>o</sup> ) <sup>o</sup> 3p <sup>o</sup> <sub>3</sub>			TW		
1010.640(3)	98947.2(3)	1010.639186(19)	0.001	4s	3D <sub>3</sub>	(3/2) <sup>o</sup> 15/21 <sup>o</sup> <sub>2</sub>			TW		
1011.436	98869.4	1011.435606(17)	29000	4s	3D <sub>1</sub>	(3/2) <sup>o</sup> 11/21 <sup>o</sup> <sub>2</sub>			S3ec		
1012.5956(18)	98756.11(18)	1012.59696(18)	-0.0013	4s	3D <sub>1</sub>	(3/2) <sup>o</sup> 17/21 <sup>o</sup> <sub>3</sub>			TW		
1012.6813(18)	98747.75(18)	1012.683073(16)	-0.0017	4s	3D <sub>1</sub>	(3/2) <sup>o</sup> 15/21 <sup>o</sup> <sub>2</sub>			TW		
1013.382(20)	98679.5(19)	1013.398849(15)	-0.018	4s	3D <sub>2</sub>	(3P <sup>o</sup> ) <sup>o</sup> 1F <sup>o</sup> <sub>3</sub>			S3ec		
1017.9976(18)	98232.06(18)	1017.997872(13)	-0.0002	4s	3D <sub>2</sub>	(3/2) <sup>o</sup> 15/21 <sup>o</sup> <sub>3</sub>			TW		
1018.0628(19)	98225.77(18)	1018.064039(22)	-0.0013	4s	3D <sub>1</sub>	(3/2) <sup>o</sup> 11/21 <sup>o</sup> <sub>0</sub>			TW		
1018.7031(24)	98164.03(23)	1018.707024(17)	-0.0039	4s	3D <sub>3</sub>	(5/2) <sup>o</sup> 13/21 <sup>o</sup> <sub>2</sub>			TW		
1019.6525(18)	98072.62(17)	1019.654307(13)	-0.0018	4s	3D <sub>2</sub>	(5/2) <sup>o</sup> 13/21 <sup>o</sup> <sub>2</sub>			TW		
1020.1070(18)	98028.93(18)	1020.107372(16)	-0.0004	4s	3D <sub>2</sub>	(5/2) <sup>o</sup> 15/21 <sup>o</sup> <sub>1</sub>			TW		
1022.102	97837.6	1022.101982(15)	91000	4s	3D <sub>2</sub>	(3/2) <sup>o</sup> 17/21 <sup>o</sup> <sub>3</sub>			S3ec		
1027.825(3)	97292.8(3)	1027.830823(19)	-0.006	4s	1D <sub>2</sub>	(3/2) <sup>o</sup> 13/21 <sup>o</sup> <sub>2</sub>	1.7e+08	C	TW	B00	
1028.3251(18)	97245.51(17)	1028.327701(13)	-0.0026	4s	3D <sub>2</sub>	(5/2) <sup>o</sup> 13/21 <sup>o</sup> <sub>2</sub>			TW		
1029.7493(18)	97111.01(17)	1029.750492(24)	-0.0012	4s	3D <sub>3</sub>	(3P <sup>o</sup> ) <sup>o</sup> 3p <sup>o</sup> <sub>2</sub>			TW		
1030.2612(18)	97062.76(17)	1030.26297(7)	-0.0017	4s	3D <sub>3</sub>	(3P <sup>o</sup> ) <sup>o</sup> 3p <sup>o</sup> <sub>3</sub>			TW		
1031.7650(18)	96921.30(17)	1031.766015(15)	-0.0010	4s	3D <sub>1</sub>	(5/2) <sup>o</sup> 13/21 <sup>o</sup> <sub>1</sub>			TW		
1033.5668(18)	96752.33(17)	1033.567510(18)	-0.0007	4s	1D <sub>2</sub>	(3/2) <sup>o</sup> 15/21 <sup>o</sup> <sub>3</sub>			TW		
1035.161(3)	96603.3(3)	1035.162498(19)	-0.001	4s	1D <sub>2</sub>	(3/2) <sup>o</sup> 11/21 <sup>o</sup> <sub>3</sub>			TW		
1036.465(3)	96481.8(3)	1036.469217(18)	-0.004	4s	1D <sub>2</sub>	(3/2) <sup>o</sup> 15/21 <sup>o</sup> <sub>2</sub>	1.01e+08	C	TW	B00	
1039.341(3)	96214.8(3)	1039.34743(3)	-0.006	4s	3D <sub>2</sub>	(3P <sup>o</sup> ) <sup>o</sup> 3p <sup>o</sup> <sub>3</sub>	2.0e+08	C	TW	B00	
1039.579(3)	96192.8(3)	1039.581895(21)	-0.003	4s	3D <sub>2</sub>	(3P <sup>o</sup> ) <sup>o</sup> 3p <sup>o</sup> <sub>2</sub>	2.0e+08	C	TW	B00	
1044.5185(18)	95737.89(7)	1044.51849(6)	0.0000	4s	1D <sub>2</sub>	(3P <sup>o</sup> ) <sup>o</sup> 3p <sup>o</sup> <sub>2</sub>	2.3e+08	C	K66	B00	
1044.7437(18)	95717.26(7)	1044.743170(19)	0.0005	4s	3D <sub>2</sub>	(3P <sup>o</sup> ) <sup>o</sup> 1D <sup>o</sup> <sub>2</sub>	4.8e+08	C	K66	B00	
1049.3642(18)	95295.80(17)	1049.363833(22)	0.0004	4s	3D <sub>2</sub>	(3P <sup>o</sup> ) <sup>o</sup> 3p <sup>o</sup> <sub>3</sub>	1.11e+08	C	TW	B00	
1049.7551(6)	95260.31(5)	1049.755242(19)	-0.0001	4s	1D <sub>2</sub>	(3P <sup>o</sup> ) <sup>o</sup> 3p <sup>o</sup> <sub>3</sub>	1.04e+08	C	K66	B00	
1050.1523(18)	95224.28(17)	1050.15339(3)	-0.0010	4s	3D <sub>2</sub>	(3P <sup>o</sup> ) <sup>o</sup> 3p <sup>o</sup> <sub>1</sub>	1.4e+08	C	TW	B00	
1050.4013(18)	95201.71(17)	1050.402433(3)	-0.0012	4s	3D <sub>1</sub>	(3P <sup>o</sup> ) <sup>o</sup> 3p <sup>o</sup> <sub>2</sub>	8.2e+07	C	TW	B00	
1052.1742(18)	95041.30(16)	1052.174562(23)	-0.0004	4s	3D <sub>1</sub>	(3P <sup>o</sup> ) <sup>o</sup> 3p <sup>o</sup> <sub>2</sub>	7.3e+07	C	TW	B00	
1054.6907(6)	94814.53(5)	1054.689891(17)	0.0008	4s	1D <sub>2</sub>	(5/2) <sup>o</sup> 15/21 <sup>o</sup> <sub>3</sub>	2.1e+08	C	K66	B00	
1055.792(3)	94715.6(3)	1055.79644(4)	-0.005	4s	3D <sub>3</sub>	(3P <sup>o</sup> ) <sup>o</sup> 3p <sup>o</sup> <sub>3</sub>	2.1e+08	C	TW	B00	

Table A1. Cont.

$\lambda_{\text{obs}}^a$ (Å)	$\epsilon_{\text{obs}}^b$ (cm <sup>-1</sup> )	$\lambda_{\text{lit.}}^c$ (Å)	$\Delta\lambda_{\text{obs-lit.}}^d$ (Å)	$I_{\text{obs}}^d$ (arb. u.)	Char <sup>e</sup>	Lower Level	Upper Level	A (g <sup>-1</sup> )	Acc <sup>f</sup>	Line Ref. #	TP Ref. #	Notes <sup>h</sup>
1056.9549(6)	94611.42(5)	1056.954568(20)	0.0005	2300000		4s	1D <sub>2</sub>	(5/2) <sup>+</sup> [5/2] <sub>2</sub>	4.0e+08	K66	B00	
1058.798(3)	94446.7(3)	1058.79854(4)	-0.000	1800000		4s	3D <sub>3</sub>	(F) <sup>+</sup> P <sup>-</sup> 3D <sub>3</sub>	1.9e+08	TW	B00	
1059.0963(8)	94420.12(7)	1059.095825(18)	0.0005	1400000		4s	1D <sub>2</sub>	(5/2) <sup>+</sup> [7/2] <sub>3</sub>		K66		
1060.631(3)	94283.5(3)	1060.634409(3)	-0.003	1700000		4s	3D <sub>1</sub>	(F) <sup>+</sup> P <sup>-</sup> 3D <sub>2</sub>	3.0e+08	TW	B00	
1063.0027(18)	94073.14(16)	1063.00505(3)	-0.0024	1400000		4s	3D <sub>1</sub>	(F) <sup>+</sup> P <sup>-</sup> 3D <sub>1</sub>	4.2e+08	TW	B00	
1065.7837(18)	93827.67(16)	1065.781839(17)	0.0019	560000		4s	1D <sub>2</sub>	(5/2) <sup>+</sup> [3/2] <sub>2</sub>		TW		
1066.1356(18)	93796.70(16)	1066.13397(4)	0.0017	590000		4s	3D <sub>2</sub>	(F) <sup>+</sup> P <sup>-</sup> 3D <sub>3</sub>		TW		
1069.1944(18)	93528.36(16)	1069.19523(4)	-0.0008	1000000		4s	3D <sub>2</sub>	(F) <sup>+</sup> P <sup>-</sup> 3D <sub>3</sub>	1.03e+08	TW	B00	
1070.3134(18)	93430.58(16)	1070.31087(6)	0.0025	380000		4s	3D <sub>3</sub>	(F) <sup>+</sup> P <sup>-</sup> 3G <sup>-</sup> 4		TW		
1073.7444(18)	93132.04(16)	1073.74516(3)	-0.0008	720000		4s	3D <sub>1</sub>	(F) <sup>+</sup> P <sup>-</sup> 3D <sub>2</sub>	1.5e+08	TW	B00	
1077.889(20)	92773.9(17)	1077.87559(3)	0.013	20000		4s	1D <sub>2</sub>	(F) <sup>+</sup> P <sup>-</sup> 3F <sub>2</sub>		S36c		
1086.1134(18)	92071.42(15)	1086.10984(8)	0.0036	72000		4s	3D <sub>3</sub>	(F) <sup>+</sup> P <sup>-</sup> 3F <sub>3</sub>		TW		
1088.405(5)	91877.6(4)	1088.39510(3)	0.010	27000		4s	1D <sub>2</sub>	(F) <sup>+</sup> P <sup>-</sup> 3F <sub>3</sub>		TW		
1089.237(6)	91807.4(5)	1089.24451(3)	-0.007	39000		4s	1D <sub>2</sub>	(F) <sup>+</sup> P <sup>-</sup> 3D <sub>2</sub>		S36c		
1091.293(5)	91634.43(24)	1091.29136(8)	0.001	40000		4s	3D <sub>2</sub>	(F) <sup>+</sup> P <sup>-</sup> 3F <sub>2</sub>		TW		
1094.399(3)	91374.35(24)	1094.40214(8)	-0.003	440000		4s	3D <sub>3</sub>	(F) <sup>+</sup> P <sup>-</sup> 3F <sub>4</sub>		TW		
1097.0512(18)	91153.45(15)	1097.05257(8)	-0.0014	320000		4s	3D <sub>2</sub>	(F) <sup>+</sup> P <sup>-</sup> 3F <sub>3</sub>		TW		
1100.523(3)	90865.86(24)	1100.52419(3)	-0.001	25000		4s	1D <sub>2</sub>	(F) <sup>+</sup> P <sup>-</sup> 3D <sub>2</sub>		TW		
1101.836(6)	90757.6(5)	1101.83633(13)	-0.000	8200		4s	3D <sub>1</sub>	(F) <sup>+</sup> P <sup>-</sup> 3F <sub>1</sub>		S36c		
1105.1751(18)	90483.40(15)	1105.17629(8)	-0.0012	60000		4s	3D <sub>1</sub>	(F) <sup>+</sup> P <sup>-</sup> 3F <sub>2</sub>		TW		
1106.447	90379.4	1106.44670(4)		23000	:	4s	1D <sub>2</sub>	(F) <sup>+</sup> P <sup>-</sup> 3G <sup>-</sup> 3		S36c		
1109.744	90110.9	1109.7420(4)		7200	:	4s	1D <sub>2</sub>	(F) <sup>+</sup> P <sup>-</sup> 3D <sub>3</sub>		S36c		
1111.753(6)	89948.0(5)	1111.75742(11)	-0.004	3000		4s	3D <sub>3</sub>	(F) <sup>+</sup> P <sup>-</sup> 3G <sup>-</sup> 4		S36c		
1119.9480(18)	89289.86(15)	1119.94659(11)	0.0014	98000		4s	3D <sub>3</sub>	(F) <sup>+</sup> P <sup>-</sup> 3G <sup>-</sup> 3		TW		
1123.2265(18)	89029.24(14)	1123.22580(11)	0.0007	21000		4s	3D <sub>2</sub>	(F) <sup>+</sup> P <sup>-</sup> 3G <sup>-</sup> 3		TW		
1127.2516(18)	88711.34(14)			1800		4p	3F <sub>2</sub>	(3/2) <sup>+</sup> [5/2] <sub>1</sub>		TWn		
1130.888(12)	88426.1(9)			4500	*	4p	3D <sub>1</sub>	(F) <sup>+</sup> P <sup>-</sup> 3G <sup>-</sup> 2		S36c		
1130.888(12)	88426.1(9)	1130.8852(3)	0.003	4500	*	4p	3D <sub>1</sub>	(3/2) <sup>+</sup> [3/2] <sub>1</sub>		S36c		
		1130.96216(16)	-0.010	4500		4p	3F <sub>2</sub>	(5/2) <sup>+</sup> [5/2] <sub>1</sub>		S36c		
1135.3657(18)	88077.35(14)	1135.34826(20)	0.0174	8200	m	4p	3F <sub>3</sub>	(5/2) <sup>+</sup> [5/2] <sub>2</sub>		S36cm		X
1142.6593(18)	87516.68(14)	1142.64027(10)	-0.0009	73000	?	4p	3D <sub>2</sub>	(F) <sup>+</sup> P <sup>-</sup> 3D <sub>2</sub>		TW		
1144.853(3)	87347.48(22)	1144.85531(8)	-0.003	120000		4s	3D <sub>3</sub>	(F) <sup>+</sup> P <sup>-</sup> 3D <sub>3</sub>		TW		
1147.7628(18)	87176.02(14)			25000		4s	3D <sub>1</sub>	(F) <sup>+</sup> P <sup>-</sup> 3D <sub>1</sub>		TW		
1157.0194(18)	86428.97(14)	1157.02043(8)	-0.0010	15000		4s	3D <sub>2</sub>	(F) <sup>+</sup> P <sup>-</sup> 3D <sub>3</sub>		TW		
1157.8714(18)	86365.38(14)	1157.87172(10)	-0.0004	19000		4s	3D <sub>1</sub>	(F) <sup>+</sup> P <sup>-</sup> 3D <sub>2</sub>		TW		
		1157.88056(11)		19000	m	4p	3F <sub>1</sub>	(5/2) <sup>+</sup> [5/2] <sub>1</sub>		TW		
1162.5991(18)	86014.17(13)	1162.60059(14)	-0.0015	6300		4s	3D <sub>3</sub>	(F) <sup>+</sup> P <sup>-</sup> 3D <sub>4</sub>		TW		
1185.899	84324.2	1185.89903(5)		19000	:	4p	3F <sub>2</sub>	(5/2) <sup>+</sup> [5/2] <sub>3</sub>		S36c		
1201.627(6)	83220.5(4)	1201.62566(8)	0.001	1800		4p	3F <sub>3</sub>	(5/2) <sup>+</sup> [9/2] <sub>4</sub>		S36c		
1204.643(20)	83012.1(14)	1204.61568(7)	0.027	9100	*	4p	3F <sub>4</sub>	(5/2) <sup>+</sup> [7/2] <sub>4</sub>		S36c		
1204.643(20)	83012.1(14)	1204.63538(5)	0.008	9100	*	4p	3F <sub>4</sub>	(5/2) <sup>+</sup> [7/2] <sub>3</sub>		S36c		
1204.643(20)	83012.1(14)	1204.65288(9)	-0.010	9100	*	4p	1D <sub>2</sub>	(F) <sup>+</sup> P <sup>-</sup> 3D <sub>3</sub>		S36c		
1205.180(12)	82975.2(8)	1205.14656(6)	0.034	4800	*	4p	3F <sub>4</sub>	(5/2) <sup>+</sup> [5/2] <sub>3</sub>		S36c		

Table A1. Cont.

$\lambda_{\text{obs}}^a$ (Å)	$\epsilon_{\text{obs}}^b$ ( $\text{cm}^{-1}$ )	$\lambda_{\text{NIST}}^c$ (Å)	$\Delta\lambda_{\text{obs-NIST}}^d$ (Å)	$I_{\text{obs}}^e$ (arb. u.)	Char <sup>e</sup>	Lower Level	Upper Level	A ( $\text{e}^{-1}$ )	Ace <sup>f</sup>	Line Ref. #	TP Ref. #	Notes <sup>h</sup>
1205.180(12)	82975.2(8)	1205.19424(8)	-0.014	4800	*	4p	1F <sub>3</sub>	(3/2) <sup>+</sup> [5/2] <sub>1</sub>		S36c		
1205.180(12)	82975.2(8)	1205.2024(3)	-0.022	4800	*	4p	3D <sub>2</sub>	(3/2) <sup>+</sup> [5/2] <sub>1</sub>		S36c		
1205.180(12)	82975.2(8)	1205.21874(7)	-0.039	4800	*	4p	3F <sub>2</sub>	(3/2) <sup>+</sup> [5/2] <sub>1</sub>		S36cn		
1205.971(6)	82925.5(4)	1206.90271(8)	-0.002	4400		4p	3F <sub>4</sub>	(5/2) <sup>+</sup> [9/2] <sub>1</sub>		S36c		
1206.771(6)	82865.8(4)	1206.76901(6)	0.002	4400		4p	3P <sub>1</sub>	(5/2) <sup>+</sup> [5/2] <sub>1</sub>		S36c		
1214.540	82335.7	1214.53971(8)		9600	:	4p	3D <sub>3</sub>	(5/2) <sup>+</sup> [5/2] <sub>1</sub>		S36c		
1214.554	82334.7	1214.55446(5)		8600	:	4p	3F <sub>3</sub>	(5/2) <sup>+</sup> [5/2] <sub>1</sub>		S36c		
1219.334	82012.0	1219.3363(5)		8500	:	4p	3F <sub>4</sub>	(5/2) <sup>+</sup> [5/2] <sub>1</sub>		S36c		
1235.935(5)	80911(3)	1235.87291(5)	0.06	4000		4p	3F <sub>2</sub>	(5/2) <sup>+</sup> [5/2] <sub>1</sub>		S36c		
1240.026(6)	80643.5(4)	1240.02707(5)	-0.001	7400		4p	3P <sub>1</sub>	(5/2) <sup>+</sup> [5/2] <sub>1</sub>		S36c		
1241.964	80517.6	1241.96398(3)		14000	:	4p	3P <sub>2</sub>	(5/2) <sup>+</sup> [5/2] <sub>1</sub>		S36c		
1243.03(5)	80448(3)	1243.08537(6)	-0.05	7300		4p	3P <sub>1</sub>	(3/2) <sup>+</sup> [1/2] <sub>1</sub>		S36c		
1248.796(3)	80077.12(17)	1248.79156(5)	0.005	26000		4p	3P <sub>2</sub>	(5/2) <sup>+</sup> [5/2] <sub>1</sub>		TW		
1250.058(4)	79996.30(22)	1250.04822(6)	0.010	69000		4p	3P <sub>2</sub>	(5/2) <sup>+</sup> [5/2] <sub>1</sub>		TW		
1253.185(5)	79796.67(17)	1253.18074(7)	0.004	25000		4p	3P <sub>2</sub>	(5/2) <sup>+</sup> [1/2] <sub>1</sub>		TW		
1255.163(6)	79670.9(4)	1255.15693(6)	0.006	6800		4p	3P <sub>0</sub>	(3/2) <sup>+</sup> [5/2] <sub>1</sub>		S36c		
1257.675(6)	79511.8(4)	1257.68320(7)	-0.008	6700		4p	3P <sub>0</sub>	(3/2) <sup>+</sup> [1/2] <sub>1</sub>		S36c		
1261.214(6)	79288.7(4)	1261.21537(5)	-0.001	3500		4p	1D <sub>2</sub>	(5/2) <sup>+</sup> [5/2] <sub>1</sub>		S36c		
1262.929(6)	79181.0(4)	1262.92481(9)	0.004	19000		4p	3P <sub>1</sub>	(5/2) <sup>+</sup> [1/2] <sub>1</sub>		S36c		
1265.510(3)	79019.53(17)	1265.50624(3)	0.004	27000		4p	3P <sub>1</sub>	(3/2) <sup>+</sup> [3/2] <sub>1</sub>		TW		
1266.313(3)	78969.42(17)	1266.3092(4)	0.003	27000		4p	3P <sub>1</sub>	(3/2) <sup>+</sup> [3/2] <sub>1</sub>		TW		
1268.71(5)	78820(3)	1268.66846(5)	0.04	3300		4p	3D <sub>3</sub>	(5/2) <sup>+</sup> [5/2] <sub>1</sub>		S36c		
1269.446(6)	78774.5(4)	1269.44626(6)	0.000	6200		4p	3F <sub>2</sub>	(5/2) <sup>+</sup> [5/2] <sub>1</sub>		S36c		
1271.327(6)	78638.0(4)	1271.31771(4)	0.010	12000		4p	3P <sub>1</sub>	(5/2) <sup>+</sup> [5/2] <sub>1</sub>		S36c		
1272.043(3)	78613.69(17)	1272.04165(6)	0.001	31000		4p	3F <sub>2</sub>	(3/2) <sup>+</sup> [7/2] <sub>1</sub>		TW		
1273.705(6)	78511.1(4)	1273.70053(5)	0.005	11000		4p	3P <sub>1</sub>	(5/2) <sup>+</sup> [5/2] <sub>1</sub>		S36c		
1274.071	78488.6	1274.07065(3)		17000	:	4p	3P <sub>3</sub>	(5/2) <sup>+</sup> [5/2] <sub>1</sub>		S36c		
1274.465	78464.3	1274.46493(3)		16000	:	4p	3P <sub>3</sub>	(5/2) <sup>+</sup> [5/2] <sub>1</sub>		S36c		
1275.5713(15)	78396.24(9)	1275.57159(3)	-0.0003	75000		4p	3F <sub>3</sub>	(5/2) <sup>+</sup> [5/2] <sub>1</sub>		TW		
1279.948(20)	78128.1(12)	1279.96123(5)	-0.013	2700		4p	3F <sub>3</sub>	(5/2) <sup>+</sup> [7/2] <sub>1</sub>		S36c		
1280.277(3)	78108.48(17)	1280.26800(4)	0.003	30000		4p	3F <sub>3</sub>	(5/2) <sup>+</sup> [7/2] <sub>1</sub>		TW,S36r		
1281.094(3)	78058.29(17)	1281.09394(9)	-0.000	10000		s <sub>1</sub> <sup>2</sup>	3F <sub>4</sub>	(5/2) <sup>+</sup> [5/2] <sub>1</sub> <sup>3</sup>		TW		
1281.228(20)	78050.1(12)	1281.25682(6)	-0.029	16000		4p	3F <sub>3</sub>	(5/2) <sup>+</sup> [5/2] <sub>1</sub>		S36c		
1281.462(3)	78035.88(17)	1281.46142(4)	0.000	44000		4p	3P <sub>0</sub>	(3/2) <sup>+</sup> [5/2] <sub>1</sub>		TW		
1282.455(3)	77975.44(17)	1282.45466(5)	0.000	72000		4p	3P <sub>0</sub>	(5/2) <sup>+</sup> [9/2] <sub>1</sub>		TW		
1283.824(6)	77892.5(4)	1283.82966(10)	-0.005	5300		s <sub>2</sub> <sup>2</sup>	3F <sub>4</sub>	(5/2) <sup>+</sup> [7/2] <sub>1</sub> <sup>4</sup>		S36c		
1284.872(3)	77828.74(16)	1284.87116(5)	0.001	36000		4p	3F <sub>4</sub>	(5/2) <sup>+</sup> [7/2] <sub>1</sub>		TW		
1285.521(6)	77789.5(4)	1285.51841(5)	0.003	5400		4p	1F <sub>3</sub>	(5/2) <sup>+</sup> [5/2] <sub>1</sub>		S36c		
1285.901(20)	77766.5(12)	1285.92203(6)	-0.021	5100		4p	1F <sub>3</sub>	(5/2) <sup>+</sup> [5/2] <sub>1</sub>		S36c		
1287.469(8)	77671.77(5)	1287.43101(6)	0.0009	53000	m	4p	3F <sub>4</sub>	(5/2) <sup>+</sup> [7/2] <sub>1</sub>		S36c		
1287.550(4)	77668.31(21)	1287.46810(6)	0.000	4900		4p	3F <sub>4</sub>	(5/2) <sup>+</sup> [9/2] <sub>1</sub>		K66		
1297.979(20)	77042.8(12)	1297.9922(9)	-0.013	4900		s <sub>2</sub> <sup>2</sup>	3F <sub>2</sub>	(3/2) <sup>+</sup> [5/2] <sub>1</sub>		S36cn		
1298.3952(8)	77018.15(5)	1298.39471(4)	0.0005	60000		4p	3F <sub>2</sub>	(3/2) <sup>+</sup> [3/2] <sub>1</sub>		K66		

Table A1. Cont.

$\lambda_{\text{obs}}^a$ (Å)	$\epsilon_{\text{obs}}^b$ (cm <sup>-1</sup> )	$\lambda_{\text{lit.}}^c$ (Å)	$\Delta\lambda_{\text{obs-Ritz}}^d$ (Å)	Char <sup>e</sup>	Lower Level	Upper Level	A (s <sup>-1</sup> )	Acc <sup>f</sup>	Line Ref. #	TP Ref. #	Notes <sup>h</sup>
1298.917(12)	76987.2(7)	1298.90527(6)	0.012	4p	1D <sup>2</sup> <sub>2</sub>	6d	(3/2) <sup>+</sup> [7/2] <sub>3</sub>		S36c		
1299.2684(8)	76966.39(5)	1299.26777(3)	0.0006	4p	3P <sup>1</sup> <sub>1</sub>	7s	(5/2) <sup>+</sup> [5/2] <sub>2</sub>		K66		
1303.661(4)	76707.04(21)	1303.66001(5)	0.001	4p	3F <sup>2</sup> <sub>2</sub>	6d	(5/2) <sup>+</sup> [5/2] <sub>2</sub>		TW		
1303.978(3)	76688.38(16)	1303.97824(4)	0.000	4p	3F <sup>2</sup> <sub>3</sub>	6d	(5/2) <sup>+</sup> [7/2] <sub>3</sub>		TW		
1305.562(3)	76595.40(16)	1305.56082(6)	0.001	4p	3D <sup>2</sup> <sub>3</sub>	6d	(3/2) <sup>+</sup> [7/2] <sub>3</sub>		TW		
1308.2982(6)	76435.17(4)	1308.29687(3)	0.0013	4p	3F <sup>3</sup> <sub>3</sub>	7s	(5/2) <sup>+</sup> [5/2] <sub>2</sub>		K66		
1309.464(3)	76367.12(16)	1309.46310(3)	0.001	4p	3F <sup>3</sup> <sub>2</sub>	7s	(5/2) <sup>+</sup> [5/2] <sub>2</sub>		TW		
1311.76(4)	76233.5(23)	1311.79458(10)	-0.04	s <sup>2</sup>	3F <sup>3</sup> <sub>3</sub>	7p	(5/2) <sup>+</sup> [5/2] <sub>3</sub>		S36c		
1314.1498(8)	76094.83(5)	1314.14956(4)	0.0004	4p	1F <sup>3</sup> <sub>3</sub>	7s	(3/2) <sup>+</sup> [5/2] <sub>2</sub>		K66		
1314.3371(6)	76083.98(3)	1314.33637(3)	0.0007	4p	3F <sup>3</sup> <sub>4</sub>	7s	(5/2) <sup>+</sup> [5/2] <sub>3</sub>		K66		
1320.687(3)	75718.15(16)	1320.68581(5)	0.002	4p	1F <sup>3</sup> <sub>3</sub>	6d	(5/2) <sup>+</sup> [7/2] <sub>4</sub>		TW		
1321.798(3)	75654.53(16)	1321.79611(6)	0.002	4p	1F <sup>3</sup> <sub>3</sub>	6d	(5/2) <sup>+</sup> [5/2] <sub>2</sub>		TW		
1322.628(6)	75607.0(3)	1322.63248(13)	-0.004	4p	1P <sup>1</sup> <sub>1</sub>	6d	(3/2) <sup>+</sup> [1/2] <sub>0</sub>		S36c		
1323.188(20)	75575.0(11)	1323.20408(6)	-0.016	4p	1F <sup>3</sup> <sub>3</sub>	6d	(5/2) <sup>+</sup> [3/2] <sub>2</sub>		S36c		
1323.812(20)	75559.4(11)	1323.79410(6)	0.018	4p	3D <sup>1</sup> <sub>1</sub>	6d	(3/2) <sup>+</sup> [5/2] <sub>2</sub>		S36c		
1325.272(20)	75486.2(11)	1325.24199(5)	0.030	4p	3D <sup>1</sup> <sub>1</sub>	6d	(3/2) <sup>+</sup> [5/2] <sub>2</sub>		S36c		
1325.515(3)	75442.39(15)	1325.51345(3)	0.001	4p	1D <sup>2</sup> <sub>2</sub>	7s	(3/2) <sup>+</sup> [5/2] <sub>2</sub>		TW		
1326.396(3)	75392.26(15)	1326.39519(4)	0.001	4p	1D <sup>2</sup> <sub>2</sub>	7s	(3/2) <sup>+</sup> [5/2] <sub>2</sub>		TW		
1328.415(3)	75277.66(15)	1328.41289(5)	0.002	4p	3D <sup>2</sup> <sub>2</sub>	6d	(3/2) <sup>+</sup> [5/2] <sub>2</sub>		TW		
1329.656(20)	75207.4(11)	1329.66943(6)	-0.014	4p	1D <sup>2</sup> <sub>2</sub>	6d	(3/2) <sup>+</sup> [3/2] <sub>2</sub>		S36c		
1331.892(3)	75081.17(15)	1331.89052(5)	0.001	4p	1D <sup>2</sup> <sub>2</sub>	6d	(5/2) <sup>+</sup> [5/2] <sub>2</sub>		TW		
1332.224(3)	75062.46(15)	1332.22268(4)	0.001	4p	1D <sup>2</sup> <sub>2</sub>	6d	(5/2) <sup>+</sup> [7/2] <sub>3</sub>		TW		
1333.0457(8)	75016.18(5)	1333.04501(3)	0.0007	4p	3D <sup>3</sup> <sub>3</sub>	7s	(3/2) <sup>+</sup> [5/2] <sub>2</sub>		K66		
		1333.0670(3)		m	3F <sup>2</sup> <sub>2</sub>	7s	(5/2) <sup>+</sup> [5/2] <sub>2</sub>		TW		
		1334.50604(5)	0.05	p	1D <sup>2</sup> <sub>2</sub>	6d	(5/2) <sup>+</sup> [5/2] <sub>2</sub>		S36c		X
1334.56(4)	74931.2(22)	1334.65445(7)	-0.005	4p	1P <sup>1</sup> <sub>1</sub>	6d	(3/2) <sup>+</sup> [5/2] <sub>2</sub>		TW		
1334.650(4)	74926.02(20)	1334.65792(17)	-0.002	s <sup>2</sup>	3F <sup>2</sup> <sub>2</sub>	7p	(5/2) <sup>+</sup> [5/2] <sub>3</sub>		TW		
1334.686(6)	74924.0(3)	1337.51122(8)	0.03	4p	1P <sup>1</sup> <sub>1</sub>	6d	(3/2) <sup>+</sup> [1/2] <sub>0</sub>		S36c		
1337.55(4)	74763.8(22)	1339.49492(5)	-0.03	4p	3D <sup>3</sup> <sub>3</sub>	6d	(5/2) <sup>+</sup> [5/2] <sub>2</sub>		S36c		
1339.46(4)	74656.7(22)	1339.77126(5)	0.0022	4p	3D <sup>3</sup> <sub>3</sub>	6d	(5/2) <sup>+</sup> [7/2] <sub>4</sub>		S36c		
1339.7734(23)	74639.49(13)	1340.91390(6)	0.0022	4p	3D <sup>3</sup> <sub>3</sub>	6d	(5/2) <sup>+</sup> [5/2] <sub>2</sub>		TW		
1340.9161(23)	74575.88(13)	1350.59358(4)	0.0027	4p	1F <sup>3</sup> <sub>3</sub>	7s	(5/2) <sup>+</sup> [5/2] <sub>2</sub>		TW		
1350.5963(20)	74041.37(11)	1351.83646(3)	0.0019	4p	1F <sup>3</sup> <sub>3</sub>	7s	(5/2) <sup>+</sup> [5/2] <sub>2</sub>		K66		
1351.8384(8)	73973.34(4)	1355.30507(4)	0.0015	4p	3D <sup>1</sup> <sub>1</sub>	7s	(3/2) <sup>+</sup> [5/2] <sub>2</sub>		K66		
1355.3066(8)	73784.04(4)	1358.7729(3)	0.0007	d <sup>10</sup>	1S <sub>0</sub>	4p	3.3e+08	C+	B09		
1358.7736(6)	73595.78(3)	1359.00914(3)	0.0016	4p	3D <sup>2</sup> <sub>2</sub>	7s	(3/2) <sup>+</sup> [3/2] <sub>2</sub>		K66		
1359.0107(8)	73582.94(4)	1359.93602(4)	0.0034	4p	3D <sup>2</sup> <sub>2</sub>	7s	(3/2) <sup>+</sup> [3/2] <sub>2</sub>		K66		
1359.9394(20)	73532.60(11)	1362.59959(3)	0.0008	4p	1D <sup>2</sup> <sub>2</sub>	7s	(3/2) <sup>+</sup> [5/2] <sub>2</sub>		TW		
1362.6004(6)	73389.09(3)	1367.50304(4)	0.003	4p	1P <sup>1</sup> <sub>1</sub>	7s	(3/2) <sup>+</sup> [5/2] <sub>2</sub>		K66		
1363.506(2)	73340.36(13)	1367.9509(3)	-0.0001	d <sup>10</sup>	1S <sub>0</sub>	4p	8.3e+07	C+	D05		
1367.9508(6)	73102.04(3)	1370.25181(6)	0.005	4p	1P <sup>1</sup> <sub>1</sub>	6d	(5/2) <sup>+</sup> [5/2] <sub>2</sub>		S36c		
1370.257(6)	72979.0(3)										

Table A1. Cont.

$\lambda_{\text{obs}}^a$ (Å)	$\epsilon_{\text{obs}}^b$ ( $\text{cm}^{-1}$ )	$\lambda_{\text{ritz}}^c$ (Å)	$\Delta\lambda_{\text{obs-ritz}}^d$ (Å)	$I_{\text{obs}}^d$ (arb. u.)	Char <sup>e</sup>	Lower Level	Upper Level	A ( $\text{g}^{-1}$ )	Acc <sup>f</sup>	Line Ref. #	TP Ref. #	Notes <sup>h</sup>
1370.561(3)	72962.83(18)	1370.55975(3)	0.001	1800	4p	3D <sup>3</sup> <sub>3</sub>	(5/2) <sup>+</sup> [5/2] <sub>2</sub>					TW
1371.8400(6)	72894.80(3)	1371.83967(3)	0.0003	4300	4p	3D <sup>3</sup> <sub>3</sub> 7s	(5/2) <sup>+</sup> [5/2] <sub>3</sub>					K66
1375.522(20)	72699.7(11)	1375.52173(4)	0.020	6900	4p	3P <sup>2</sup> <sub>2</sub> 5d	(3/2) <sup>+</sup> [5/2] <sub>3</sub>					S36c
1393.129(2)	71780.88(13)	1393.12738(3)	0.0001	1800	4p	3D <sup>1</sup> <sub>1</sub> 7s	(5/2) <sup>+</sup> [5/2] <sub>2</sub>					TW
1398.6428(16)	71497.88(18)	1398.64196(11)	0.0009	4000	s <sup>2</sup>	3F <sub>4</sub> 6p	(3/2) <sup>+</sup> [5/2] <sub>3</sub>					TW
1399.3532(17)	71461.59(9)	1399.35262(3)	0.0005	15000	4p	3D <sup>2</sup> <sub>2</sub> 7s	(5/2) <sup>+</sup> [5/2] <sub>2</sub>					TW
1402.7785(8)	71287.09(4)	1402.77693(4)	0.0016	98000	4p	1P <sup>1</sup> <sub>1</sub> 7s	(5/2) <sup>+</sup> [5/2] <sub>2</sub>					K66
1403.985(3)	71225.85(16)	1403.99171(5)	-0.007	4900	4p	3P <sup>1</sup> <sub>1</sub> 5d	(3/2) <sup>+</sup> [5/2] <sub>2</sub>					TW
1407.1688(16)	71064.68(8)	1407.16862(5)	0.0001	6000	4p	3P <sup>1</sup> <sub>1</sub> 5d	(3/2) <sup>+</sup> [5/2] <sub>2</sub>					TW
1408.8131(23)	70981.74(12)	1408.81230(5)	0.0008	4900	4p	3P <sup>1</sup> <sub>1</sub> 5d	(3/2) <sup>+</sup> [5/2] <sub>2</sub>					TW
1414.4390(19)	70699.41(10)	1414.4371(4)	0.0019	26000	s <sup>2</sup>	3F <sub>2</sub> 5p	(3/2) <sup>+</sup> [5/2] <sub>1</sub>					TWn
1414.8980(15)	70676.47(8)	1414.89768(6)	0.0003	49000	4p	3P <sup>1</sup> <sub>1</sub> 5d	(3/2) <sup>+</sup> [1/2] <sub>1</sub>					TW
1418.4250(14)	70500.73(7)	1418.42631(3)	-0.0014	140000	4p	3P <sup>2</sup> <sub>2</sub> 5d	(5/2) <sup>+</sup> [5/2] <sub>2</sub>					TW
1419.7465(20)	70435.11(10)	1419.74554(4)	0.0010	7500	4p	3F <sup>3</sup> <sub>3</sub> 5d	(3/2) <sup>+</sup> [7/2] <sub>4</sub>					TW
1421.3746(13)	70354.43(7)	1421.37346(5)	0.0011	35000	4p	3P <sup>2</sup> <sub>2</sub> 5d	(5/2) <sup>+</sup> [5/2] <sub>1</sub>					TW
1421.7587(6)	70335.42(3)	1421.75866(4)	0.0000	200000	4p	3P <sup>2</sup> <sub>2</sub> 5d	(5/2) <sup>+</sup> [5/2] <sub>2</sub>					K66
1427.5920(12)	70048.03(6)	1427.59106(6)	0.0009	58000	4p	3P <sup>2</sup> <sub>0</sub> 5d	(3/2) <sup>+</sup> [5/2] <sub>1</sub>					TW
1427.8283(8)	70036.43(4)	1427.82905(7)	-0.0007	180000	s <sup>2</sup>	3F <sub>4</sub> 6p	(5/2) <sup>+</sup> [5/2] <sub>3</sub>					K66
1428.3572(8)	70010.50(4)	1428.35801(11)	-0.0008	190000	s <sup>2</sup>	3F <sub>3</sub> 6p	(3/2) <sup>+</sup> [3/2] <sub>3</sub>					K66
1430.2425(8)	69918.21(4)	1430.24252(5)	-0.0000	240000	4p	3P <sup>2</sup> <sub>2</sub> 5d	(5/2) <sup>+</sup> [1/2] <sub>1</sub>					K66
1433.8415(12)	69742.72(6)	1433.84011(7)	0.0014	53000	4p	3P <sup>2</sup> <sub>2</sub> 5d	(3/2) <sup>+</sup> [1/2] <sub>1</sub>					TW
1434.452(3)	69713.01(13)	1434.45240(14)	-0.000	3600	s <sup>2</sup>	3F <sub>3</sub> 6p	(3/2) <sup>+</sup> [5/2] <sub>2</sub>					TWn
1434.7712(12)	69697.52(6)	1434.76999(6)	0.0013	76000	4p	3P <sup>1</sup> <sub>1</sub> 5d	(5/2) <sup>+</sup> [1/2] <sub>1</sub>					TW
1434.9035(6)	69691.10(3)	1434.90377(9)	-0.0003	270000	s <sup>2</sup>	3F <sub>1</sub> 6p	(5/2) <sup>+</sup> [7/2] <sub>4</sub>					K66
1435.3153(13)	69671.10(6)	1435.31565(13)	-0.0004	110000	s <sup>2</sup>	3F <sub>3</sub> 6p	(3/2) <sup>+</sup> [5/2] <sub>3</sub>					TW
1436.2352(12)	69626.48(6)	1436.23585(7)	-0.0007	130000	s <sup>2</sup>	3F <sub>4</sub> 6p	( <sup>1</sup> G) <sup>+</sup> 3F <sup>3</sup> <sub>3</sub>					TW
1442.1398(12)	69341.40(6)	1442.13845(4)	0.0014	66000	4p	3P <sup>2</sup> <sub>2</sub> 6s	(3/2) <sup>+</sup> [5/2] <sub>2</sub>					TW
1443.5423(12)	69274.04(6)	1443.54170(6)	0.0006	73000	4p	3P <sup>2</sup> <sub>2</sub> 5d	(3/2) <sup>+</sup> [5/2] <sub>2</sub>					TW
1444.1295(22)	69245.87(10)	1444.13017(4)	-0.0007	7700	4p	3P <sup>2</sup> <sub>2</sub> 6s	(3/2) <sup>+</sup> [3/2] <sub>1</sub>					TW
1445.9841(12)	69157.05(6)	1445.98335(4)	0.0007	97000	4p	3P <sup>1</sup> <sub>1</sub> 5d	(5/2) <sup>+</sup> [5/2] <sub>2</sub>					TW
1446.9088(22)	69113.24(10)	1446.90033(6)	0.0005	4600	4p	3P <sup>2</sup> <sub>2</sub> 5d	(3/2) <sup>+</sup> [5/2] <sub>2</sub>					TW
1448.6390(19)	69030.31(9)	1448.63819(6)	0.0008	6100	4p	3P <sup>2</sup> <sub>2</sub> 5d	(3/2) <sup>+</sup> [5/2] <sub>2</sub>					TW
1449.0578(8)	69010.36(4)	1449.05784(12)	-0.0000	180000	s <sup>2</sup>	3F <sub>2</sub> 6p	(3/2) <sup>+</sup> [3/2] <sub>1</sub>					K66
1450.3032(12)	68951.10(6)	1450.30363(4)	-0.0004	170000	4p	3P <sup>1</sup> <sub>1</sub> 5d	(3/2) <sup>+</sup> [5/2] <sub>1</sub>					TW
1452.2950(12)	68856.53(6)	1452.29331(5)	0.0017	97000	4p	3P <sup>1</sup> <sub>1</sub> 5d	(5/2) <sup>+</sup> [5/2] <sub>2</sub>					TW
1452.670(20)	68838.7(9)	1452.66954(5)	-0.025	3600	4p	3P <sup>1</sup> <sub>1</sub> 5d	(5/2) <sup>+</sup> [3/2] <sub>2</sub>					S36c
1455.6643(13)	68697.16(6)	1455.66225(7)	0.0021	22000	s <sup>2</sup>	3F <sub>4</sub> 6p	(5/2) <sup>+</sup> [7/2] <sub>3</sub>					TW
1457.1778(12)	68625.81(6)	1457.17584(5)	0.0023	55000	4p	3F <sup>3</sup> <sub>3</sub> 5d	(3/2) <sup>+</sup> [5/2] <sub>2</sub>					TW
1458.0022(6)	68587.00(3)	1458.00133(5)	0.0009	150000	4p	3F <sup>3</sup> <sub>3</sub> 5d	(5/2) <sup>+</sup> [7/2] <sub>3</sub>					K66
1459.4131(6)	68520.70(3)	1459.41216(15)	0.0009	220000	s <sup>2</sup>	3F <sub>2</sub> 6p	(3/2) <sup>+</sup> [5/2] <sub>2</sub>					K66
1460.3076(13)	68478.72(6)	1460.30573(14)	0.0018	14000	s <sup>2</sup>	3F <sub>2</sub> 6p	(3/2) <sup>+</sup> [5/2] <sub>3</sub>					TW
1460.4620(13)	68471.48(6)	1460.45917(4)	0.0028	17000	4p	3F <sup>3</sup> <sub>3</sub> 5d	(5/2) <sup>+</sup> [5/2] <sub>3</sub>					TW

Table A1. Cont.

$\lambda_{\text{obs}}^a$ (Å)	$\epsilon_{\text{obs}}^b$ (cm <sup>-1</sup> )	$\lambda_{\text{lit}}^c$ (Å)	$\Delta\lambda_{\text{obs-Ritz}}^d$ (Å)	$I_{\text{obs}}^d$ (arb. u.)	Char <sup>e</sup>	Lower Level	Upper Level	A (s <sup>-1</sup> )	Acc <sup>f</sup>	Line Ref. #	TP Ref. #	Notes <sup>h</sup>
1461.5557(11)	68420.25(5)	1461.55369(5)	0.0020	60000	4p	3p <sup>2</sup>	(5/2) <sup>2</sup> [1/2] <sub>1</sub>			TW		
1462.8534(18)	68359.35(9)	1462.85242(6)	0.0010	5100	s <sup>2</sup>	3F <sub>4</sub>	(3/2) <sup>2</sup> [9/2] <sub>1</sub> <sup>5</sup>			TW		
1463.7512(16)	68317.62(3)	1463.75130(4)	-0.0001	350000	4p	3F <sub>3</sub>	(5/2) <sup>2</sup> [9/2] <sub>1</sub> <sup>5</sup>			K66		
1463.8367(6)	68313.63(3)	1463.83785(5)	-0.0012	20000	4p	3F <sub>4</sub>	(5/2) <sup>2</sup> [7/2] <sub>1</sub>			K66		
1463.9947(12)	68306.26(6)	1463.99219(5)	0.0025	20000	4p	3F <sub>3</sub>	(5/2) <sup>2</sup> [3/2] <sub>1</sub>			TW		
1464.1173(22)	68300.54(10)	1464.11637(6)	0.0009	4600	4p	1F <sub>3</sub>	(3/2) <sup>2</sup> [5/2] <sub>1</sub>			TW		
1464.6035(11)	68277.86(5)	1464.60141(5)	0.0021	69000	4p	1F <sub>3</sub>	(3/2) <sup>2</sup> [5/2] <sub>1</sub>			TW		
1465.0339(18)	68257.81(9)	1465.03633(14)	-0.0024	4300	s <sup>2</sup>	3F <sub>2</sub>	(3/2) <sup>2</sup> [1/2] <sub>1</sub>			TW		
1465.5404(6)	68234.22(3)	1465.54069(16)	-0.0003	170000	s <sup>2</sup>	3F <sub>4</sub>	(G) <sup>3</sup> P <sup>o</sup> -3F <sup>o</sup> <sub>4</sub>			K66		
1466.0705(6)	68209.54(3)	1466.07026(9)	0.0002	280000	s <sup>2</sup>	3F <sub>3</sub>	(5/2) <sup>2</sup> [5/2] <sub>1</sub> <sup>3</sup>			K66		
1466.5247(10)	68188.42(5)	1466.52373(4)	0.0010	79000	4p	3F <sub>4</sub>	(5/2) <sup>2</sup> [5/2] <sub>1</sub>			K66		
1466.7305(12)	68178.85(6)	1466.72839(10)	0.0022	42000	s <sup>2</sup>	3F <sub>3</sub>	(F) <sup>3</sup> P <sup>o</sup> -3F <sup>o</sup> <sub>2</sub>			TW		
1467.574(5)	68139.68(24)	1467.57153(6)	0.002	1400	4p	1F <sub>3</sub>	(3/2) <sup>2</sup> [3/2] <sub>1</sub>			TW		
1469.6935(6)	68041.40(3)	1469.69291(5)	0.0006	150000	4p	1F <sub>3</sub>	(3/2) <sup>2</sup> [3/2] <sub>1</sub>			K66		
1469.8457(12)	68034.35(5)	1469.84329(5)	0.0024	49000	4p	3F <sub>4</sub>	(5/2) <sup>2</sup> [9/2] <sub>1</sub>			TW		
1470.6970(6)	67994.97(3)	1470.69711(4)	-0.0001	500000	4p	3F <sub>4</sub>	(5/2) <sup>2</sup> [9/2] <sub>1</sub>			K66		
1471.072(5)	67977.65(24)	1471.07289(5)	-0.001	2700	4p	1F <sub>3</sub>	(3/2) <sup>2</sup> [7/2] <sub>1</sub>	8.e+06	E	TW		
1472.3946(6)	67916.58(3)	1472.3953(4)	-0.0004	6800000	d <sup>10</sup>	1S <sub>0</sub>	(5/2) <sup>2</sup> [7/2] <sub>1</sub> <sup>4</sup>			K66		D05sec
1473.5295(8)	67864.27(4)	1473.53001(10)	-0.0005	100000	s <sup>2</sup>	3F <sub>3</sub>	(3/2) <sup>2</sup> [3/2] <sub>1</sub>			K66		
1473.9786(6)	67843.59(3)	1473.97844(4)	0.0002	190000	4p	3P <sup>o</sup> <sub>1</sub>	(G) <sup>3</sup> P <sup>o</sup> -3F <sup>o</sup> <sub>3</sub>			K66		
1474.9348(6)	67799.61(3)	1474.93480(9)	-0.0000	230000	s <sup>2</sup>	3F <sub>3</sub>	(D) <sup>3</sup> P <sup>o</sup> -1P <sup>o</sup> <sub>3</sub>			TWn		
1475.4361(22)	67776.57(10)	1475.4383(9)	-0.0023	23000	s <sup>2</sup>	1D <sub>2</sub>	(3/2) <sup>2</sup> [5/2] <sub>1</sub>			K66		
1476.0596(6)	67747.94(3)	1476.05914(4)	0.0005	130000	4p	3P <sup>o</sup> <sub>1</sub>	(3/2) <sup>2</sup> [5/2] <sub>1</sub>			K66		
1478.2385(13)	67648.08(6)	1478.23606(6)	0.0024	23000	4p	1D <sub>2</sub>	(3/2) <sup>2</sup> [5/2] <sub>1</sub>			TW		
1481.5438(6)	67497.16(3)	1481.54375(12)	0.0000	130000	s <sup>2</sup>	3F <sub>3</sub>	(5/2) <sup>2</sup> [5/2] <sub>1</sub> <sup>2</sup>			K66		
1484.178(5)	67377.37(24)	1484.17557(13)	0.002	1200	s <sup>2</sup>	3F <sub>4</sub>	(G) <sup>3</sup> P <sup>o</sup> -3H <sup>o</sup> <sub>5</sub>			TW		
1485.3282(8)	67325.19(4)	1485.32773(4)	0.0005	110000	4p	1D <sub>2</sub>	(3/2) <sup>2</sup> [7/2] <sub>1</sub>			K66		
1485.6143(13)	67312.22(6)	1485.60994(4)	0.0043	53000	4p	3F <sub>3</sub>	(3/2) <sup>2</sup> [3/2] <sub>1</sub>			TW		
1485.6788(8)	67309.30(4)	1485.67761(4)	0.0012	110000	4p	3P <sup>o</sup> <sub>2</sub>	(5/2) <sup>2</sup> [5/2] <sub>1</sub>			K66		
1487.612(5)	67221.81(24)	1487.60927(6)	0.003	1400	4p	3D <sub>3</sub>	(3/2) <sup>2</sup> [5/2] <sub>1</sub>			TW		
1487.8005(12)	67214.22(5)	1487.79200(12)	0.0013	68000	s <sup>2</sup>	3F <sub>3</sub>	(5/2) <sup>2</sup> [5/2] <sub>1</sub> <sup>2</sup>			TW		
1487.9719(12)	67205.57(5)	1487.96988(5)	0.0020	70000	4p	3F <sub>2</sub>	(5/2) <sup>2</sup> [5/2] <sub>1</sub>			TW		
1488.1123(12)	67199.23(5)	1488.11000(4)	0.0023	53000	4p	3D <sub>3</sub>	(3/2) <sup>2</sup> [5/2] <sub>1</sub>			TW		
1488.2853(13)	67191.42(6)	1488.2853(12)	-0.0000	34000	s <sup>2</sup>	1D <sub>2</sub>	(5/2) <sup>2</sup> [5/2] <sub>1</sub> <sup>2</sup>			TWn		
1488.6366(6)	67175.56(3)	1488.63692(4)	-0.0003	1100000	4p	3P <sup>o</sup> <sub>2</sub>	(5/2) <sup>2</sup> [5/2] <sub>1</sub>			K66		
1488.8319(12)	67166.75(6)	1488.83094(5)	0.0009	120000	4p	3F <sub>2</sub>	(3/2) <sup>2</sup> [7/2] <sub>1</sub>			TW		
1491.178(5)	67061.07(24)	1491.17634(6)	0.002	1400	4p	3D <sub>3</sub>	(5/2) <sup>2</sup> [7/2] <sub>1</sub>			TW		
1491.384(6)	67051.8(3)	1491.39392(4)	-0.010	1200	4p	3P <sup>o</sup> <sub>2</sub>	(3/2) <sup>2</sup> [5/2] <sub>1</sub>			TW		
1492.1535(10)	67017.23(4)	1492.15247(11)	0.0010	95000	s <sup>2</sup>	3F <sub>2</sub>	(5/2) <sup>2</sup> [5/2] <sub>1</sub> <sup>3</sup>			TW		
1492.6819(10)	66993.51(4)	1492.68146(13)	0.0004	100000	4p	1P <sup>o</sup> <sub>1</sub>	(3/2) <sup>2</sup> [1/2] <sub>0</sub>			K66		

Table A1. Cont.

$\lambda_{\text{obs}}^a$ (Å)	$\sigma_{\text{obs}}^b$ (cm <sup>-1</sup> )	$\lambda_{\text{lit}}^c$ (Å)	$\Delta\lambda_{\text{obs-lit}}^d$ (Å)	Char <sup>e</sup>	Lower Level	Upper Level	A (s <sup>-1</sup> )	Acc <sup>f</sup>	Line Ref. #	TP Ref. #	Notes <sup>h</sup>
1492.83423(11)	66986.66(3)	1492.83423(11)	0.0004	s <sup>2</sup>	3F <sub>2</sub>	( <sup>3</sup> P) <sup>o</sup> 3P <sup>o</sup> 3P <sup>o</sup>	5.5e+08	D+	K66		TW
1493.3675(6)	66962.75(3)	1493.3656(4)	0.0009	4p	3D <sub>3</sub> 5d	(3/2) <sup>o</sup> [7/2] <sub>4</sub>			K66		
1494.661(6)	66904.8(3)	1494.65244(5)	0.008	4p	3F <sub>2</sub> 5d	(3/2) <sup>o</sup> [5/2] <sub>1</sub>			S36c		
1494.7930(19)	66898.89(8)	1494.79138(4)	0.0016	4p	3D <sub>3</sub> 5d	(3/2) <sup>o</sup> [7/2] <sub>3</sub>			TW		
1495.4296(6)	66870.42(3)	1495.42965(9)	-0.0001	20000	3	(5/2) <sup>o</sup> [7/2] <sub>3</sub>			K66		
1496.6862(6)	66814.27(3)	1496.68654(4)	-0.0003	4p	3P <sup>o</sup> 6s	(3/2) <sup>o</sup> [3/2] <sub>1</sub>			K66		
1498.5779(14)	66729.93(6)	1498.57545(7)	0.0024	18000	3F <sub>3</sub> 4f	(3/2) <sup>o</sup> [7/2] <sub>3</sub>			TW		
1499.5135(10)	66688.30(4)	1499.51299(7)	0.0005	79000	3F <sub>3</sub> 4f	(3/2) <sup>o</sup> [7/2] <sub>4</sub>			K66		
1500.016(3)	66665.97(13)	1500.0148(7)	0.001	14000	1D <sub>2</sub> 8p	(3/2) <sup>o</sup> [3/2] <sub>2</sub>			TWn		
1501.3359(12)	66607.35(5)	1501.33622(11)	-0.0003	110000	3F <sub>2</sub> sp	( <sup>3</sup> G) <sup>o</sup> 3P <sup>o</sup> 3P <sup>o</sup>			TW		
1502.811(3)	66541.96(13)	1502.80934(8)	0.002	2600	3F <sub>3</sub> 4f	(3/2) <sup>o</sup> [9/2] <sub>4</sub>			TW		
1503.3675(6)	66517.34(3)	1503.36800(13)	-0.0005	150000	3F <sub>2</sub> 6p	(5/2) <sup>o</sup> [3/2] <sub>1</sub>			K66		
1504.7561(6)	66455.95(3)	1504.75691(4)	-0.0008	22000	3F <sub>4</sub> 4f	(5/2) <sup>o</sup> [9/2] <sub>3</sub>			K66		
1505.3866(6)	66428.12(3)	1505.38756(4)	-0.0010	16000	3F <sub>4</sub> 4f	(5/2) <sup>o</sup> [7/2] <sub>3</sub>			K66		
1505.8576(12)	66407.34(5)	1505.85714(18)	0.0005	6000	3F <sub>3</sub> 4f	( <sup>3</sup> G) <sup>o</sup> 3P <sup>o</sup> 3P <sup>o</sup>			TW		
1507.4705(22)	66336.29(10)	1507.4706(5)	-0.0000	9700	3F <sub>2</sub> 7f	(3/2) <sup>o</sup> [5/2] <sub>2</sub>			TWn		
1507.6008(22)	66330.56(10)	1507.59910(4)	0.0017	3200	3F <sub>4</sub> 4f	(3/2) <sup>o</sup> [5/2] <sub>3</sub>			TW		
1508.1835(6)	66304.93(3)	1508.18443(13)	-0.0009	170000	3F <sub>2</sub> 6p	(3/2) <sup>o</sup> [5/2] <sub>2</sub>			K66		
1508.4845(22)	66291.70(10)	1508.4829(15)	0.0016	6400	3F <sub>2</sub> 7f	(5/2) <sup>o</sup> [3/2] <sub>1</sub>			TWn		
1508.6313(6)	66285.25(3)	1508.63203(5)	-0.0007	150000	3F <sub>4</sub> 4f	(5/2) <sup>o</sup> [7/2] <sub>3</sub>			K66		
1510.5051(6)	66203.02(3)	1510.50562(5)	-0.0005	210000	1F <sup>o</sup> 5d	(5/2) <sup>o</sup> [7/2] <sub>4</sub>			K66		
1510.724(3)	66193.41(13)	1510.72666(5)	-0.002	8900	1F <sup>o</sup> 5d	(5/2) <sup>o</sup> [7/2] <sub>3</sub>			TW		
1512.1738(12)	66129.96(5)	1512.17367(6)	0.0002	98000	3F <sub>4</sub> sp	( <sup>3</sup> P) <sup>o</sup> 3P <sup>o</sup> 3P <sup>o</sup>			TW		
1512.4640(8)	66117.28(3)	1512.46442(11)	-0.0004	97000	3F <sub>3</sub> sp	( <sup>3</sup> P) <sup>o</sup> 3P <sup>o</sup> 3P <sup>o</sup>			K66		
1512.5393(19)	66113.98(8)	1512.5391(6)	0.0003	18000	3F <sub>1</sub> 8p	(3/2) <sup>o</sup> [1/2] <sub>1</sub>			TWn		
1513.0157(22)	66093.17(9)	1513.0151(5)	0.0005	9800	3F <sub>1</sub> 7f	(5/2) <sup>o</sup> [5/2] <sub>2</sub>			TWn		
1513.3651(6)	66077.91(3)	1513.36565(4)	-0.0005	140000	1F <sup>o</sup> 5d	(5/2) <sup>o</sup> [5/2] <sub>3</sub>			K66		
1513.9340(13)	66053.08(6)	1513.93287(14)	0.0011	46000	1D <sub>2</sub> 6f	(5/2) <sup>o</sup> [7/2] <sub>3</sub>			TW		
1514.2339(8)	66040.00(3)	1514.23361(6)	0.0003	80000	3D <sup>o</sup> 5d	(3/2) <sup>o</sup> [5/2] <sub>2</sub>			K66		
1514.3380(12)	66035.46(5)	1514.33770(11)	0.0003	110000	1D <sub>2</sub> 8p	(3/2) <sup>o</sup> [5/2] <sub>1</sub>			TW		
1514.4921(6)	66028.74(3)	1514.49222(8)	-0.0001	700000	3F <sub>4</sub> sp	( <sup>3</sup> P) <sup>o</sup> 3P <sup>o</sup> 3P <sup>o</sup>	4.8e+08	D+	K66		TW
1514.6461(13)	66022.02(6)	1514.64663(14)	-0.0005	48000	3F <sub>2</sub> 6p	(3/2) <sup>o</sup> [3/2] <sub>2</sub>			TW		
1514.805(5)	66015.12(23)	1514.80334(10)	0.001	13000	1D <sub>2</sub> 6f	(5/2) <sup>o</sup> [5/2] <sub>2</sub>			TW		
1515.456(3)	65986.75(12)	1515.46044(10)	-0.005	8600	1D <sub>2</sub> 6f	(5/2) <sup>o</sup> [3/2] <sub>2</sub>			TW		
1515.491(5)	65985.22(23)	1515.49438(15)	-0.004	4300	1D <sub>2</sub> 6f	(5/2) <sup>o</sup> [3/2] <sub>1</sub>			TW		
1516.9018(13)	65923.84(6)	1516.90090(5)	0.0009	43000	1F <sup>o</sup> 5d	(5/2) <sup>o</sup> [9/2] <sub>4</sub>			TW		
1517.1600(12)	65892.63(5)	1517.15960(5)	0.0004	81000	1F <sup>o</sup> 5d	(5/2) <sup>o</sup> [5/2] <sub>2</sub>			TW		
1517.6309(8)	65892.17(3)	1517.63100(4)	-0.0001	130000	3F <sup>o</sup> 2	(3/2) <sup>o</sup> [5/2] <sub>2</sub>			K66		
1517.9297(8)	65879.20(3)	1517.92987(6)	0.0000	87000	3D <sup>o</sup> 1	(3/2) <sup>o</sup> [5/2] <sub>2</sub>			K66		
1519.4914(6)	65871.49(3)	1519.49170(4)	-0.0003	410000	3F <sup>o</sup> 1	(5/2) <sup>o</sup> [5/2] <sub>2</sub>			K66		
1519.8366(6)	65796.55(3)	1519.83686(4)	-0.0003	540000	3F <sup>o</sup> 2	(3/2) <sup>o</sup> [5/2] <sub>1</sub>			K66		

Table A1. Cont.

$\lambda_{\text{obs}}^a$ (Å)	$\epsilon_{\text{obs}}^b$ ( $\text{cm}^{-1}$ )	$\lambda_{\text{lit}}^c$ (Å)	$\Delta\lambda_{\text{obs-Ritz}}^d$ (Å)	$I_{\text{obs}}^d$ (arb. u.)	Char <sup>e</sup>	Lower Level	Upper Level	A ( $\text{e}^{-1}$ )	Acc <sup>f</sup>	Line Ref. #	TP Ref. #	Notes <sup>h</sup>
1519.923(3)	65792.81(13)	1519.9246(6)	0.007	11000	m	4p	3D <sup>2</sup> <sub>1</sub> 5d	(3/2) <sup>+</sup> [5/2] <sub>1</sub>		K66		
1519.923(3)	65792.81(13)	1519.9165(7)	0.007	11000	+	s <sup>2</sup>	3F <sup>2</sup> <sub>2</sub> 8p	(3/2) <sup>+</sup> [1/2] <sub>1</sub>		TWn		
1519.923(3)	65792.81(13)	1519.9261(7)	-0.003	11000	+	s <sup>2</sup>	3F <sup>2</sup> <sub>2</sub> 8p	(3P) <sup>+</sup> P <sup>+</sup> -3S <sup>+</sup> <sub>1</sub>		TWn		
1520.0166(12)	65788.75(5)	1520.01664(7)	-0.0000	53000	4p	4p	3D <sup>2</sup> <sub>2</sub> 5d	(3/2) <sup>+</sup> [5/2] <sub>2</sub>		TW		
1520.3899(12)	63772.60(5)	1520.38979(17)	0.0001	150000	4p	4p	1D <sup>2</sup> <sub>2</sub> 6f	(5/2) <sup>+</sup> [1/2] <sub>1</sub>		TWn		
1520.5397(6)	65766.12(3)	1520.53944(5)	0.0003	150000	4p	4p	3D <sup>2</sup> <sub>2</sub> 5d	(3/2) <sup>+</sup> [5/2] <sub>2</sub>		K66		
1521.4252(22)	63727.84(9)	1521.4270(16)	-0.0018	8000	4p	4p	3F <sup>2</sup> <sub>0</sub> 7f	(5/2) <sup>+</sup> [3/2] <sub>1</sub>		TWn		
1522.5070(19)	65681.14(8)	1522.50482(12)	0.0022	8900	s <sup>2</sup>	s <sup>2</sup>	(G) <sup>+</sup> P <sup>+</sup> -3P <sup>+</sup> <sub>2</sub>	(3/2) <sup>+</sup> [3/2] <sub>1</sub>		TWn		
1522.5767(6)	65678.14(3)	1522.57664(11)	0.0001	97000	s <sup>2</sup>	s <sup>2</sup>	3F <sup>2</sup> <sub>2</sub> 6p	(3/2) <sup>+</sup> [7/2] <sub>3</sub>		K66		
1523.7415(8)	65277.93(3)	1523.74102(6)	0.0005	76000	4p	4p	3D <sup>2</sup> <sub>2</sub> 5d	(3/2) <sup>+</sup> [5/2] <sub>2</sub>		K66		
1523.9231(15)	65230.93(11)	1523.92300(10)	0.0001	31000	s <sup>2</sup>	s <sup>2</sup>	3F <sup>2</sup> <sub>1</sub> 8p	(3/2) <sup>+</sup> [3/2] <sub>1</sub>		TWn		
1524.8604(8)	65279.77(3)	1524.85998(5)	0.0004	130000	4p	4p	1D <sup>2</sup> <sub>2</sub> 5d	(5/2) <sup>+</sup> [5/2] <sub>2</sub>		K66		
1525.656(20)	65545.6(9)	1525.63103(13)	0.025	92000	s <sup>2</sup>	s <sup>2</sup>	3F <sup>2</sup> <sub>2</sub> 5p	(3P) <sup>+</sup> P <sup>+</sup> -3G <sup>+</sup> <sub>3</sub>		S36c		
1525.6433(13)	65546.12(5)	1525.64085(7)	0.0026	73000	4p	4p	1P <sup>+</sup> <sub>1</sub> 5d	(3/2) <sup>+</sup> [5/2] <sub>2</sub>		TW		
1525.656(20)	65545.6(9)	1525.66850(6)	-0.013	97000	4p	4p	3D <sup>2</sup> <sub>2</sub> 5d	(3/2) <sup>+</sup> [5/2] <sub>2</sub>		S36c		
1525.7649(6)	65540.90(3)	1525.76429(5)	0.0006	130000	4p	4p	1D <sup>2</sup> <sub>2</sub> 5d	(5/2) <sup>+</sup> [7/2] <sub>3</sub>		K66		
1525.8388(8)	6537.72(3)	1525.83781(9)	0.0010	92000	s <sup>2</sup>	s <sup>2</sup>	3F <sup>2</sup> <sub>2</sub> 4f	(3/2) <sup>+</sup> [7/2] <sub>3</sub>		K66		
1526.932(5)	65490.79(21)	1526.92724(7)	0.005	32000	4p	4p	3D <sup>2</sup> <sub>1</sub> 5d	(3/2) <sup>+</sup> [1/2] <sub>1</sub>		TW		
1526.9944(7)	65488.12(3)	1526.9931(5)	0.0013	130000	s <sup>2</sup>	s <sup>2</sup>	3F <sup>2</sup> <sub>2</sub> 5p	3D <sup>2</sup> <sub>3</sub>		K66n		
1527.8127(13)	65453.05(6)	1527.81239(9)	0.0003	42000	s <sup>2</sup>	s <sup>2</sup>	1D <sup>2</sup> <sub>2</sub> 5d	(3/2) <sup>+</sup> [5/2] <sub>2</sub>		TW		
1528.4583(22)	65425.40(9)	1528.45612(3)	0.0022	4700	4p	4p	3F <sup>2</sup> <sub>2</sub> 4f	(5/2) <sup>+</sup> [5/2] <sub>2</sub>		TW		X
1528.785(20)	65411.4(9)	1528.89495(9)	-0.110	19000	s <sup>2</sup>	s <sup>2</sup>	3F <sup>2</sup> <sub>2</sub> 4f	(3/2) <sup>+</sup> [5/2] <sub>2</sub>		S36c		
1529.3927(22)	65385.43(9)	1529.39267(7)	0.0000	4900	4p	4p	1P <sup>+</sup> <sub>1</sub> 5d	(3/2) <sup>+</sup> [5/2] <sub>2</sub>		TW		
1531.2874(14)	65304.53(6)	1531.28647(11)	0.0010	70000	s <sup>2</sup>	s <sup>2</sup>	3F <sup>2</sup> <sub>2</sub> 4f	(3/2) <sup>+</sup> [3/2] <sub>1</sub>		TW		
1531.3338(14)	65302.55(6)	1531.33448(7)	-0.0007	41000	4p	4p	1P <sup>+</sup> <sub>1</sub> 5d	(3/2) <sup>+</sup> [5/2] <sub>2</sub>		TW		
1531.4120(14)	65299.21(6)	1531.4121(10)	-0.0002	60000	s <sup>2</sup>	s <sup>2</sup>	3F <sup>2</sup> <sub>0</sub> 8p	(3/2) <sup>+</sup> [3/2] <sub>1</sub>		TWn		
1531.8555(6)	65280.31(3)	1531.85562(4)	-0.0001	700000	4p	4p	3F <sup>2</sup> <sub>3</sub> 6s	(5/2) <sup>+</sup> [5/2] <sub>2</sub>		K66		
1532.128(3)	65268.70(13)	1532.13042(10)	-0.003	390000	s <sup>2</sup>	s <sup>2</sup>	1D <sup>2</sup> <sub>2</sub> 5d	(5/2) <sup>+</sup> [3/2] <sub>1</sub>		TW		
1532.8083(15)	65239.73(6)	1532.80783(7)	0.0004	17000	4p	4p	3F <sup>2</sup> <sub>2</sub> 5p	(3P) <sup>+</sup> P <sup>+</sup> -3D <sup>+</sup> <sub>2</sub>	1.0e+09	D+		TW
1533.9867(6)	65189.61(3)	1533.98624(12)	0.0005	170000	s <sup>2</sup>	s <sup>2</sup>	3F <sup>2</sup> <sub>2</sub> 5d	(3/2) <sup>+</sup> [1/2] <sub>1</sub>		TW		
1534.6282(13)	65162.37(6)	1534.62719(10)	0.0010	43000	s <sup>2</sup>	s <sup>2</sup>	3F <sup>2</sup> <sub>3</sub> 6s	(G) <sup>+</sup> P <sup>+</sup> -3H <sup>+</sup> <sub>4</sub>		K66		
1535.0023(6)	65124.34(3)	1535.00194(4)	0.0004	350000	4p	4p	3F <sup>2</sup> <sub>3</sub> 6s	(5/2) <sup>+</sup> [5/2] <sub>3</sub>		K66		
1535.5242(6)	65124.34(3)	1535.52352(4)	0.0007	130000	4p	4p	3D <sup>2</sup> <sub>3</sub> 5d	(5/2) <sup>+</sup> [7/2] <sub>4</sub>		K66		
1536.193(5)	65096.00(21)	1536.19869(21)	-0.006	8200	s <sup>2</sup>	s <sup>2</sup>	3F <sup>2</sup> <sub>2</sub> 6f	(3/2) <sup>+</sup> [3/2] <sub>1</sub>		TW		
1536.9317(16)	65064.70(7)	1536.93333(14)	-0.0016	24000	s <sup>2</sup>	s <sup>2</sup>	3F <sup>2</sup> <sub>2</sub> 6f	(3/2) <sup>+</sup> [3/2] <sub>1</sub>		TW		
1537.3218(12)	65048.19(5)	1537.32130(14)	0.0005	120000	s <sup>2</sup>	s <sup>2</sup>	3F <sup>2</sup> <sub>2</sub> 6f	(3/2) <sup>+</sup> [5/2] <sub>2</sub>		TW		
1537.5581(6)	65038.19(3)	1537.55884(8)	-0.0007	860000	s <sup>2</sup>	s <sup>2</sup>	3F <sup>2</sup> <sub>4</sub> 9p	(3P) <sup>+</sup> P <sup>+</sup> -3P <sup>+</sup> <sub>4</sub>	1.4e+09	D+		TW
1538.4795(6)	64999.24(3)	1538.47917(3)	0.0003	96000	4p	4p	3D <sup>2</sup> <sub>3</sub> 5d	(5/2) <sup>+</sup> [5/2] <sub>3</sub>		K66		
1538.522(5)	64997.45(21)	1538.52706(8)	-0.005	40000	4p	4p	1P <sup>+</sup> <sub>1</sub> 5d	(3/2) <sup>+</sup> [1/2] <sub>1</sub>		TW		
1540.2392(6)	64924.98(3)	1540.23914(12)	0.0001	120000	s <sup>2</sup>	s <sup>2</sup>	3F <sup>2</sup> <sub>2</sub> 5p	(3P) <sup>+</sup> P <sup>+</sup> -1D <sup>+</sup> <sub>2</sub>		K66		
1540.3886(6)	64918.68(3)	1540.38850(4)	0.0001	290000	4p	4p	1F <sup>+</sup> <sub>3</sub> 6s	(3/2) <sup>+</sup> [3/2] <sub>2</sub>		K66		



Table A1. Cont.

$\lambda_{\text{obs}}^a$ (Å)	$\epsilon_{\text{obs}}^b$ (cm <sup>-1</sup> )	$\lambda_{\text{lit}}^c$ (Å)	$\Delta\lambda_{\text{obs-Ritz}}^d$ (Å)	$I_{\text{obs}}^d$ (arb. u.)	Char <sup>e</sup>	Lower Level	Upper Level	A (s <sup>-1</sup> )	Acc <sup>f</sup>	Line Ref. #	TP Ref. #	Notes <sup>h</sup>
1540.5879(6)	64910.29(3)	1540.58814(9)	-0.0002	600000	s <sup>2</sup>	3F <sub>3</sub> sp	( <sup>3</sup> P) <sup>1</sup> P <sup>3</sup> P <sub>3</sub> <sup>2</sup>	9.e+08	D+	K66	TW	
1541.246(5)	64882.59(22)	1541.24593(13)	-0.000	5200	s <sup>2</sup>	3F <sub>1</sub> 6s	(3/2) <sup>1</sup> [5/2] <sub>1</sub> <sup>2</sup>			TW		
1541.7007(22)	64863.43(9)	1541.70280(5)	-0.0021	860000	4p	3F <sub>4</sub> 6s	(5/2) <sup>1</sup> [5/2] <sub>3</sub>			K66		
1541.7542(18)	64861.18(8)	1541.75580(18)	-0.0016	260000	s <sup>2</sup>	1D <sub>2</sub> sp	(D) <sup>1</sup> P <sup>3</sup> D <sub>2</sub>	1.4e+09	D+	K66	TW	
1541.9565(22)	64852.67(9)	1541.95701(21)	-0.0005	11000	s <sup>2</sup>	3F <sub>1</sub> 6f	(3/2) <sup>1</sup> [3/2] <sub>1</sub> <sup>2</sup>			TW		
1542.4007(13)	64834.00(6)	1542.40025(4)	0.0004	55000	4p	3D <sub>3</sub> 5d	(5/2) <sup>1</sup> [3/2] <sub>2</sub>			TW		
1542.6989(22)	64821.46(9)	1542.69717(14)	0.0017	10000	3f	3F <sub>1</sub> 6f	(3/2) <sup>1</sup> [3/2] <sub>2</sub>			TW		
1543.1328(13)	64803.24(5)	1543.1327(9)	0.0001	64000	s <sup>2</sup>	3F <sub>2</sub> sp	(D) <sup>1</sup> P <sup>3</sup> P <sub>1</sub>			TWn		
1544.6764(6)	64738.48(3)	1544.67690(8)	-0.0005	430000	s <sup>2</sup>	3F <sub>3</sub> 4f	(5/2) <sup>1</sup> [9/2] <sub>1</sub> <sup>4</sup>			K66		
1547.9581(8)	64601.23(3)	1547.95800(7)	0.0001	59000	s <sup>2</sup>	3F <sub>5</sub> 4f	(5/2) <sup>1</sup> [7/2] <sub>1</sub> <sup>4</sup>			K66		
1548.4169(12)	64582.09(5)	1548.4165(12)	0.0004	200000	s <sup>2</sup>	3F <sub>2</sub> sp	( <sup>3</sup> P) <sup>1</sup> P <sup>3</sup> P <sub>2</sub>	1.0e+09	D+	TWn	TW	
1548.942(3)	64560.22(12)	1548.9433(10)	-0.002	15000	s <sup>2</sup>	3F <sub>1</sub> sp	(D) <sup>1</sup> P <sup>3</sup> P <sub>1</sub>			TWn		
1549.56(7)	64534(3)	1549.62492(22)	-0.06	24000	s <sup>2</sup>	3F <sub>0</sub> 6f	(3/2) <sup>1</sup> [3/2] <sub>1</sub>			Stanc		
1550.0971(17)	64512.09(7)	1550.09682(9)	0.0003	20000	4p	3D <sub>1</sub> 5d	(5/2) <sup>1</sup> [1/2] <sub>0</sub>			TW		
1550.2978(13)	64503.73(5)	1550.29648(7)	0.0014	29000	3f	3F <sub>3</sub> 4f	(5/2) <sup>1</sup> [5/2] <sub>3</sub>			TW		
1550.6528(6)	64488.969(25)	1550.65296(13)	-0.0002	180000	s <sup>2</sup>	3F <sub>2</sub> sp	(G) <sup>3</sup> P <sup>3</sup> P <sub>2</sub>	7.3e+08	D+	K66n	TW	
1551.3886(6)	64458.383(25)	1551.38877(7)	-0.0002	250000	s <sup>2</sup>	3F <sub>3</sub> 4f	(5/2) <sup>1</sup> [7/2] <sub>3</sub>			K66		
1552.297(5)	64420.66(22)	1552.29519(14)	0.002	1100	s <sup>2</sup>	3F <sub>3</sub> 4f	( <sup>3</sup> P) <sup>1</sup> P <sup>3</sup> S <sub>2</sub>			TW		
1552.6450(6)	64406.223(25)	1552.64631(10)	-0.0013	720000	s <sup>2</sup>	3F <sub>4</sub> sp	( <sup>3</sup> P) <sup>1</sup> P <sup>3</sup> S <sub>2</sub>	1.9e+09	D+	K66	TW	
1553.3473(13)	64377.11(5)	1553.3472(13)	0.0001	96000	s <sup>2</sup>	1D <sub>2</sub> 7p	(3/2) <sup>1</sup> [3/2] <sub>1</sub>			TWn		
1553.8961(6)	64354.367(25)	1553.89596(14)	0.0001	210000	s <sup>2</sup>	1D <sub>2</sub> sp	( <sup>3</sup> P) <sup>1</sup> P <sup>3</sup> C <sub>3</sub>	1.4e+09	D+	K66	TW	
1554.2933(12)	64337.92(5)	1554.2934(11)	-0.0001	120000	s <sup>2</sup>	3F <sub>2</sub> sp	(3/2) <sup>1</sup> [3/2] <sub>2</sub>			TWn		
1555.1336(6)	64303.157(25)	1555.13425(6)	-0.0007	810000	s <sup>2</sup>	3F <sub>3</sub> sp	( <sup>3</sup> P) <sup>1</sup> P <sup>3</sup> G <sub>4</sub>	1.3e+09	D+	K66	TW	
1555.7018(6)	64279.67(25)	1555.70295(9)	-0.0012	880000	s <sup>2</sup>	3F <sub>4</sub> sp	( <sup>3</sup> P) <sup>1</sup> P <sup>3</sup> D <sub>3</sub>	6.8e+08	D+	K66	TW	
1556.0269(8)	64259.68(21)	1556.02548(4)	0.0014	40000	4p	1D <sub>2</sub> 6s	(3/2) <sup>1</sup> [5/2] <sub>2</sub>			K66		
1556.6836(12)	64239.13(9)	1556.6810(10)	0.0027	19000	s <sup>2</sup>	3F <sub>0</sub> sp	(D) <sup>1</sup> P <sup>3</sup> P <sub>1</sub>			TWn		
1556.7668(12)	64235.70(5)	1556.7668(12)	0.0001	180000	s <sup>2</sup>	1D <sub>2</sub> 7p	(3/2) <sup>1</sup> [5/2] <sub>3</sub>			TWn		
1557.884(25)	64201.884(25)	1557.88652(10)	0.0002	110000	s <sup>2</sup>	3F <sub>2</sub> sp	( <sup>3</sup> P) <sup>1</sup> P <sup>3</sup> D <sub>3</sub>			TWn		
1558.1590(13)	64178.30(6)	1558.1587(13)	0.0003	62000	s <sup>2</sup>	3F <sub>1</sub> sp	( <sup>3</sup> P) <sup>1</sup> P <sup>3</sup> P <sub>0</sub>			TWn		
1558.3446(6)	64170.659(25)	1558.34444(4)	0.0002	180000	4p	1D <sub>2</sub> 6s	(3/2) <sup>1</sup> [3/2] <sub>1</sub>			K66		
1559.1587(14)	64157.15(6)	1559.1576(13)	0.0011	210000	s <sup>2</sup>	1D <sub>2</sub> 7p	(3/2) <sup>1</sup> [5/2] <sub>1</sub> <sup>2</sup>			TWn		
1563.108(3)	63975.10(12)	1563.1083(13)	-0.000	9400	s <sup>2</sup>	3F <sub>1</sub> 8p	(5/2) <sup>1</sup> [5/2] <sub>1</sub> <sup>2</sup>			TWn		
1563.1959(13)	63971.51(5)	1563.1933(5)	0.0024	22000	4p	3D <sub>1</sub> 5d	(5/2) <sup>1</sup> [5/2] <sub>2</sub>			TW		
1565.9244(6)	63860.043(24)	1565.92444(4)	0.0003	190000	4p	3F <sub>2</sub> 6s	(5/2) <sup>1</sup> [5/2] <sub>2</sub>			K66		
1566.4148(4)	63840.051(16)	1566.41460(4)	0.0002	220000	4p	3D <sub>3</sub> 6s	(3/2) <sup>1</sup> [3/2] <sub>2</sub>			K66		
1569.2124(8)	63726.24(3)	1569.21212(4)	0.0003	40000	4p	3F <sub>2</sub> 6s	(3/2) <sup>1</sup> [5/2] <sub>1</sub>			K66		
1569.4154(11)	63717.99(4)	1569.41524(11)	0.0001	42000	3f	3F <sub>2</sub> sp	( <sup>3</sup> P) <sup>1</sup> P <sup>3</sup> P <sub>3</sub>			TW		
1570.0365(11)	63692.79(4)	1570.0367(6)	-0.0002	94000	s <sup>2</sup>	3F <sub>2</sub> 8p	(3/2) <sup>1</sup> [3/2] <sub>1</sub> <sup>2</sup>			TW,S36r		
1570.5722(12)	63671.06(5)	1570.57051(5)	0.0017	17000	4p	3D <sub>1</sub> 5d	(5/2) <sup>1</sup> [5/2] <sub>1</sub>			TW		
1573.1666(22)	63566.06(9)	1573.16667(4)	-0.0001	4000	4p	3D <sub>2</sub> 5d	(5/2) <sup>1</sup> [5/2] <sub>3</sub>			TW		
1575.3547(12)	63477.77(5)	1575.35310(6)	0.0016	34000	4p	1F <sub>1</sub> 5d	(5/2) <sup>1</sup> [5/2] <sub>2</sub>			TW		
1576.0523(12)	63449.67(5)	1576.0520(6)	0.0003	47000	s <sup>2</sup>	3F <sub>1</sub> 8p	(5/2) <sup>1</sup> [3/2] <sub>1</sub> <sup>2</sup>			TWn		
1577.2693(22)	63400.71(9)	1577.26680(5)	0.0025	4500	4p	3D <sub>2</sub> 5d	(5/2) <sup>1</sup> [3/2] <sub>2</sub>			TW		

Table A1. Cont.

$\lambda_{\text{obs}}^a$ (Å)	$\epsilon_{\text{obs}}^b$ (cm <sup>-1</sup> )	$\lambda_{\text{lit}}^c$ (Å)	$\Delta\lambda_{\text{obs-lit}}^d$ (Å)	Char <sup>e</sup>	Lower Level	Upper Level	A (g <sup>-1</sup> )	Acc <sup>f</sup>	Line Ref. #	TP Ref. #	Notes <sup>h</sup>
1579.4926(8)	63311.47(3)	1579.49148(9)	0.0011	64000	s <sup>2</sup>	3F <sub>2</sub> <sup>4</sup>	(5/2) <sup>+</sup> [5/2] <sup>+</sup> <sub>3</sub>	K66			
1580.0260(11)	63290.10(4)	1580.02469(9)	0.0013	43000	s <sup>2</sup>	3F <sub>2</sub> <sup>4</sup>	(5/2) <sup>+</sup> [5/2] <sup>+</sup> <sub>2</sub>	TW			
1580.6238(6)	63266.081(24)	1580.62531(9)	0.0005	71000	s <sup>2</sup>	3F <sub>2</sub> <sup>4</sup>	(5/2) <sup>+</sup> [7/2] <sup>+</sup> <sub>3</sub>	K66			
1581.4029(14)	63234.99(6)	1581.40630(5)	-0.0034	4p	4p	3D <sup>1</sup> <sub>1</sub> 5d	(5/2) <sup>+</sup> [1/2] <sup>+</sup> <sub>1</sub>	TW			
1581.4200(12)	63234.3(5)	1581.41834(10)	0.001	2300	s <sup>2</sup>	3F <sub>2</sub> <sup>4</sup>	(5/2) <sup>+</sup> [3/2] <sup>+</sup> <sub>1</sub>	S36c			
1581.9962(6)	63211.277(24)	1581.99510(10)	0.0011	82000	s <sup>2</sup>	3F <sub>2</sub> <sup>4</sup>	(5/2) <sup>+</sup> [3/2] <sup>+</sup> <sub>2</sub>	K66			
1582.6074(20)	63186.36(8)	1582.60633(9)	0.0011	6600	s <sup>2</sup>	3F <sub>2</sub> <sup>4</sup>	(5/2) <sup>+</sup> [3/2] <sup>+</sup> <sub>2</sub>	TW			
1582.8471(11)	63177.80(4)	1582.84538(6)	0.0015	33000	4p	1p <sup>1</sup> <sub>1</sub> 5d	(5/2) <sup>+</sup> [3/2] <sup>+</sup> <sub>1</sub>	TW			
1583.6831(4)	63143.946(16)	1583.68224(10)	0.0009	160000	3F <sub>3</sub> <sup>5</sup>	3F <sub>3</sub> <sup>5</sup>	(5/2) <sup>+</sup> [3/2] <sup>+</sup> <sub>1</sub>	K66			
1586.276(5)	63040.74(21)	1586.27882(10)	-0.003	4100	s <sup>2</sup>	3F <sub>2</sub> <sup>4</sup>	(5/2) <sup>+</sup> [5/2] <sup>+</sup> <sub>3</sub>	TW			
1587.0607(22)	63009.56(9)	1587.05935(12)	0.0014	6100	s <sup>2</sup>	3F <sub>2</sub> <sup>4</sup>	(5/2) <sup>+</sup> [5/2] <sup>+</sup> <sub>3</sub>	TW			
1587.716(3)	62983.56(11)	1587.71486(5)	0.001	2600	4p	3D <sup>1</sup> <sub>2</sub> 5d	(5/2) <sup>+</sup> [1/2] <sup>+</sup> <sub>1</sub>	TW			
1590.1649(4)	62886.560(16)	1590.16460(4)	0.0003	110000	4p	1F <sub>3</sub> <sup>6</sup>	(5/2) <sup>+</sup> [5/2] <sup>+</sup> <sub>2</sub>	K66			
1593.5559(4)	62752.741(16)	1593.55527(4)	0.0006	190000	4p	1F <sub>3</sub> <sup>6</sup>	(5/2) <sup>+</sup> [5/2] <sup>+</sup> <sub>2</sub>	K66			
1596.749(6)	62627.26(24)	1596.74558(10)	0.003	5100	s <sup>2</sup>	1D <sub>2</sub> 5f	(3/2) <sup>+</sup> [3/2] <sup>+</sup> <sub>1</sub>	S36c			
1598.4025(4)	62562.465(16)	1598.40212(4)	0.0004	140000	4p	3D <sup>1</sup> <sub>1</sub> 6s	(3/2) <sup>+</sup> [3/2] <sup>+</sup> <sub>1</sub>	K66			
1601.211(3)	62452.75(12)	1601.20967(12)	0.001	2800	s <sup>2</sup>	3F <sub>3</sub> <sup>5</sup>	(3/2) <sup>+</sup> [3/2] <sup>+</sup> <sub>1</sub>	TW			
1602.2739(8)	62411.30(3)	1602.27264(12)	0.0013	28000	s <sup>2</sup>	3F <sub>2</sub> <sup>4</sup>	(3/2) <sup>+</sup> [3/2] <sup>+</sup> <sub>1</sub>	K66			
1602.3887(4)	62406.831(16)	1602.38797(4)	0.0007	130000	4p	3D <sup>1</sup> <sub>2</sub> 6s	(3/2) <sup>+</sup> [3/2] <sup>+</sup> <sub>2</sub>	K66			
1603.2280(23)	62374.16(9)	1603.22651(14)	0.0014	13000	s <sup>2</sup>	1D <sub>2</sub> 7p	(5/2) <sup>+</sup> [5/2] <sup>+</sup> <sub>3</sub>	TW			
1604.8475(4)	62311.216(16)	1604.84729(4)	0.0002	56000	4p	3D <sup>1</sup> <sub>2</sub> 6s	(3/2) <sup>+</sup> [3/2] <sup>+</sup> <sub>1</sub>	K66			
1605.2810(4)	62294.390(16)	1605.28112(12)	-0.0001	150000	s <sup>2</sup>	3F <sub>3</sub> <sup>5</sup>	(3/2) <sup>+</sup> [3/2] <sup>+</sup> <sub>1</sub>	K66			
1606.1963(17)	62238.89(6)	1606.19537(24)	0.0009	76000	s <sup>2</sup>	1D <sub>2</sub> 7p	(3/2) <sup>+</sup> [5/2] <sup>+</sup> <sub>2</sub>	TW			
1606.8338(4)	62234.190(15)	1606.83396(4)	-0.0002	170000	4p	1D <sup>2</sup> <sub>2</sub> 6s	(5/2) <sup>+</sup> [5/2] <sup>+</sup> <sub>2</sub>	K66			
1608.3931(17)	62173.85(6)	1608.39195(15)	0.0012	87000	s <sup>2</sup>	1D <sub>2</sub> 7p	(5/2) <sup>+</sup> [3/2] <sup>+</sup> <sub>1</sub>	TW			
1608.6395(4)	62164.332(15)	1608.63928(6)	0.0002	72000	4p	1p <sup>1</sup> <sub>1</sub> 6s	(3/2) <sup>+</sup> [3/2] <sup>+</sup> <sub>2</sub>	K66			
1609.3421(23)	62137.19(9)	1609.3430(15)	-0.0009	10000	s <sup>2</sup>	1D <sub>2</sub> 7p	(5/2) <sup>+</sup> [7/2] <sup>+</sup> <sub>3</sub>	TWn			
1610.2967(8)	62100.36(3)	1610.29617(4)	0.0005	21000	4p	1D <sup>2</sup> <sub>2</sub> 6s	(5/2) <sup>+</sup> [5/2] <sup>+</sup> <sub>2</sub>	K66			
1611.1185(20)	62068.68(8)	1611.11784(6)	0.0006	12000	4p	3F <sub>2</sub> <sup>4</sup>	(3/2) <sup>+</sup> [3/2] <sup>+</sup> <sub>1</sub>	TW			
1614.159(5)	61951.76(21)	1614.16058(12)	-0.001	2100	s <sup>2</sup>	3F <sub>2</sub> <sup>4</sup>	(3/2) <sup>+</sup> [3/2] <sup>+</sup> <sub>1</sub>	TW			
1614.4945(18)	61938.89(7)	1614.49462(18)	-0.0002	73000	s <sup>2</sup>	1D <sub>2</sub> 7p	(5/2) <sup>+</sup> [3/2] <sup>+</sup> <sub>2</sub>	TW			
1617.9152(8)	61870.94(3)	1617.91504(4)	0.0002	24000	4p	3D <sup>1</sup> <sub>3</sub> 6s	(5/2) <sup>+</sup> [5/2] <sup>+</sup> <sub>2</sub>	K66			
1621.4262(4)	61674.099(15)	1621.42522(4)	0.0010	84000	4p	3D <sup>1</sup> <sub>3</sub> 6s	(5/2) <sup>+</sup> [5/2] <sup>+</sup> <sub>2</sub>	K66			
1622.4281(4)	61636.013(15)	1622.42766(12)	0.0004	80000	s <sup>2</sup>	3F <sub>2</sub> <sup>4</sup>	(3/2) <sup>+</sup> [5/2] <sup>+</sup> <sub>3</sub>	K66			
1623.1726(6)	61607.743(23)	1623.1731(3)	-0.0005	36000	s <sup>2</sup>	3F <sub>4</sub> <sup>4</sup>	(3/2) <sup>+</sup> [5/2] <sup>+</sup> <sub>3</sub>	K66			
1629.603(3)	61364.65(12)	1629.6017(12)	0.001	9500	s <sup>2</sup>	3F <sub>2</sub> <sup>4</sup>	(3/2) <sup>+</sup> [3/2] <sup>+</sup> <sub>2</sub>	TWn			
1630.269(18)	61339.65(7)	1630.26799(21)	-0.0011	32000	s <sup>2</sup>	3F <sub>2</sub> <sup>4</sup>	(3/2) <sup>+</sup> [3/2] <sup>+</sup> <sub>2</sub>	TW			
1636.0706(23)	61122.0(6)	1636.06917(21)	0.0014	19000	s <sup>2</sup>	3F <sub>2</sub> <sup>4</sup>	(3/2) <sup>+</sup> [1/2] <sup>+</sup> <sub>1</sub>	TWn			
1636.6049(20)	61102.10(7)	1636.60469(14)	0.0002	11000	s <sup>2</sup>	3F <sub>2</sub> <sup>4</sup>	(3/2) <sup>+</sup> [3/2] <sup>+</sup> <sub>2</sub>	TW			
1645.6583(23)	60765.95(8)	1645.6575(22)	0.0008	12000	s <sup>2</sup>	3F <sub>1</sub> <sup>4</sup>	(5/2) <sup>+</sup> [1/2] <sup>+</sup> <sub>0</sub>	TWn			

Table A1. Cont.

$\lambda_{\text{obs}}^a$ (Å)	$\epsilon_{\text{obs}}^b$ (cm <sup>-1</sup> )	$\lambda_{\text{lit}}^c$ (Å)	$\Delta\lambda_{\text{obs-Ritz}}^d$ (Å)	$I_{\text{obs}}^d$ (arb. u.)	Char <sup>e</sup>	Lower Level	Upper Level	A (s <sup>-1</sup> )	Ace <sup>f</sup>	Line Ref. #	TP Ref. #	Notes <sup>h</sup>
1649.4570(14)	60626.01(5)	1649.45739(4)	-0.0004	26000	:	4p	3D <sup>1</sup> <sub>1</sub> 6s	(5/2) <sup>+</sup> [5/2] <sub>2</sub>		K66		
1656.322	60574.74	1656.32175(4)		27000		4p	3D <sup>2</sup> <sub>2</sub> 6s	(5/2) <sup>+</sup> [5/2] <sub>2</sub>		S36c		
1660.0022(14)	60240.88(5)	1660.00075(4)	0.0014	18000		4p	3D <sup>2</sup> <sub>1</sub> 6s	(5/2) <sup>+</sup> [5/2] <sub>3</sub>		K66		
1663.0029(14)	60132.19(5)	1663.00184(5)	0.0011	31000		4p	1P <sup>1</sup> <sub>1</sub> 6s	(5/2) <sup>+</sup> [5/2] <sub>3</sub>		K66		
1672.7773(23)	59780.82(8)	1672.7755(4)	0.0018	8600		s <sup>2</sup>	3F <sub>3</sub> sp	(3p) <sup>3</sup> p <sup>2</sup> 5D <sup>1</sup> <sub>4</sub>		TW		
1680.27(4)	59514.1(14)	1680.31169(23)	-0.04	980		s <sup>2</sup>	3F <sub>2</sub> sp	(3p) <sup>3</sup> p <sup>2</sup> 5D <sup>1</sup> <sub>3</sub>		S36c		
1683.152(5)	59412.32(18)	1683.1596(3)	-0.007	34000	*	s <sup>2</sup>	3F <sub>4</sub> sp	(1D) <sup>3</sup> p <sup>2</sup> 3D <sup>1</sup> <sub>3</sub>	1.1e+08	TW	B00	
1683.152(5)	59412.32(18)	1683.1583(3)	-0.006	34000	*	s <sup>2</sup>	3F <sub>3</sub> sp	(3p) <sup>3</sup> p <sup>2</sup> 3D <sup>2</sup> <sub>3</sub>		TW		
1695.9031(23)	58965.63(8)	1695.90238(20)	0.0007	12000		s <sup>2</sup>	3F <sub>2</sub> 7p	(5/2) <sup>+</sup> [3/2] <sub>2</sub>		TW		
1699.0958(20)	58854.83(7)	1699.0950(5)	0.0008	22000	*	s <sup>2</sup>	3F <sub>3</sub> sp	(1D) <sup>3</sup> p <sup>2</sup> 3P <sup>2</sup> <sub>2</sub>		TW		
1699.0958(20)	58854.83(7)	1699.10217(23)	-0.0064	22000	*	s <sup>2</sup>	3F <sub>4</sub> sp	(1D) <sup>3</sup> p <sup>2</sup> 3P <sup>2</sup> <sub>3</sub>		TW		
1702.9236(23)	58722.54(8)	1702.92295(21)	0.0006	8600		s <sup>2</sup>	3P <sub>1</sub> 7p	(5/2) <sup>+</sup> [3/2] <sub>2</sub>		TW		
1714.655(20)	58370.8(7)	1714.6631(3)	-0.008	460		s <sup>2</sup>	3F <sub>2</sub> sp	(3p) <sup>3</sup> p <sup>2</sup> 5D <sup>1</sup> <sub>2</sub>		S36c		
1717.7188(22)	58216.75(7)	1717.7210(3)	-0.0023	11000		s <sup>2</sup>	3F <sub>2</sub> sp	(3p) <sup>3</sup> p <sup>2</sup> 5D <sup>1</sup> <sub>3</sub>		TW		
1734.2254(23)	57662.63(8)	1734.2267(5)	-0.0013	4200		s <sup>2</sup>	3F <sub>2</sub> sp	(1D) <sup>3</sup> p <sup>2</sup> 3P <sup>2</sup> <sub>1</sub>		TW		
1736.5531(22)	57585.34(7)	1736.5563(3)	-0.0032	8900		s <sup>2</sup>	3F <sub>3</sub> sp	(1D) <sup>3</sup> p <sup>2</sup> 3D <sup>1</sup> <sub>3</sub>		TW		
1744.506(20)	57322.8(7)	1744.5159(3)	-0.010	22000		s <sup>2</sup>	3F <sub>3</sub> sp	(1D) <sup>3</sup> p <sup>2</sup> 3P <sup>2</sup> <sub>1</sub>	5.9e+07	S36c	B00	
1753.2791(21)	57035.99(7)	1753.28069(22)	-0.0016	21000		s <sup>2</sup>	3F <sub>2</sub> sp	(1D) <sup>3</sup> p <sup>2</sup> 3P <sup>2</sup> <sub>2</sub>		TW		
1759.5030(21)	56834.23(7)	1759.50415(22)	-0.0012	3400		s <sup>2</sup>	3F <sub>3</sub> sp	(1D) <sup>3</sup> p <sup>2</sup> 3P <sup>2</sup> <sub>2</sub>		TW		
1781.573(3)	56130.16(10)	1781.5715(3)	0.002	4400		s <sup>2</sup>	3F <sub>2</sub> sp	(1D) <sup>3</sup> p <sup>2</sup> 3D <sup>1</sup> <sub>2</sub>		TW		
1790.606(21)	55845.31(7)	1790.6599(3)	0.0007	33000		s <sup>2</sup>	3F <sub>2</sub> sp	(1D) <sup>3</sup> p <sup>2</sup> 3D <sup>1</sup> <sub>3</sub>	4.5e+07	TW	B00	
1800.9806(24)	55525.31(7)	1800.9789(6)	0.0018	11000		s <sup>2</sup>	3F <sub>4</sub> sp	(3p) <sup>3</sup> p <sup>2</sup> 3P <sup>2</sup> <sub>3</sub>		TW		
1807.8535(21)	55314.22(7)			160000		4p	1P <sup>1</sup> <sub>1</sub> s <sup>2</sup>	1S <sub>0</sub>		TW,S36r		
1856.957(20)	53852.1(6)	1856.92890(17)	0.009	14000		s <sup>2</sup>	1D <sub>2</sub> 6p	(5/2) <sup>+</sup> [3/2] <sub>1</sub>		S36c		
1861.57(4)	53718.2(12)	1861.6226(3)	-0.06	10000		s <sup>2</sup>	3F <sub>3</sub> sp	(3p) <sup>3</sup> p <sup>2</sup> 3P <sup>2</sup> <sub>2</sub>		S36c		
1874.166(5)	53357.06(14)	1874.16676(18)	-0.001	14000		s <sup>2</sup>	1D <sub>2</sub> 6p	(5/2) <sup>+</sup> [3/2] <sub>2</sub>		TW		
1875.74638(18)	53312.112(5)	1875.74622(7)	0.00016	20000		s <sup>2</sup>	3F <sub>4</sub> 5p	(3/2) <sup>+</sup> [5/2] <sub>3</sub>		F		
1882.253(3)	53127.82(8)	1882.2566(10)	-0.003	17000		s <sup>2</sup>	1D <sub>2</sub> sp	(3p) <sup>3</sup> p <sup>2</sup> 3S <sup>1</sup> <sub>1</sub>		TWn		
1903.858(5)	52524.93(15)	1903.86698(15)	-0.009	410		s <sup>2</sup>	1D <sub>2</sub> sp	(3p) <sup>3</sup> p <sup>2</sup> 3D <sup>1</sup> <sub>1</sub>		TW		
1920.6709(8)	52065.141(22)	1920.67133(7)	-0.0004	43000		4p	3P <sup>2</sup> <sub>2</sub> 4d	(3/2) <sup>+</sup> [5/2] <sub>3</sub>	1.5e+07	F	B00	
1922.14229(17)	52025.285(5)	1922.14231(11)	-0.00003	94000		s <sup>2</sup>	3F <sub>3</sub> 5p	(5/2) <sup>+</sup> [3/2] <sub>2</sub>		F		
1924.548(3)	51960.26(9)	1924.5458(22)	0.002	5200		s <sup>2</sup>	1G <sub>4</sub> 7p	(5/2) <sup>+</sup> [7/2] <sub>3</sub>		F		
1928.46(4)	51854.9(11)	1928.4863(3)	-0.03	46000		s <sup>2</sup>	1D <sub>2</sub> sp	(3p) <sup>3</sup> p <sup>2</sup> 1P <sup>1</sup> <sub>1</sub>		TWn		
1929.75131(6)	51820.488(16)	1929.60764(17)	0.00002	34000	m	s <sup>2</sup>	3F <sub>4</sub> sp	(G) <sup>3</sup> p <sup>3</sup> 1P <sup>1</sup> <sub>1</sub>		S36cn		
1942.3030(7)	51485.272(19)	1942.3050(12)	0.0001	31000		s <sup>2</sup>	3F <sub>2</sub> 5p	(3p) <sup>3</sup> p <sup>2</sup> 1F <sup>1</sup> <sub>3</sub>	2.1e+07	F	B00	
1944.59596(14)	51424.564(4)	1944.59601(6)	-0.00005	600000		4s	3P <sub>1</sub> 4p	(3/2) <sup>+</sup> [5/2] <sub>3</sub>		F		D05se
1946.4928(3)	51374.451(7)	1946.49291(7)	-0.0001	13000		s <sup>2</sup>	3F <sub>3</sub> 4p	(3/2) <sup>+</sup> [5/2] <sub>3</sub>	1.99e+07	F		
1952.5792(18)	51214.31(5)	1952.57557(12)	0.0037	97000		s <sup>2</sup>	3F <sub>4</sub> 5p	(5/2) <sup>+</sup> [5/2] <sub>3</sub>		F		
1957.5176(3)	51085.108(8)	1957.51767(7)	-0.0000	190000		s <sup>2</sup>	3F <sub>4</sub> 5p	(5/2) <sup>+</sup> [7/2] <sub>4</sub>		F		
1968.008(3)	50812.79(8)	1968.01129(8)	-0.003	9700		4p	3P <sup>2</sup> <sub>2</sub> 4d	(3/2) <sup>+</sup> [1/2] <sub>1</sub>	1.8e+07	TW	O07	

Table A1. Cont.

$\lambda_{\text{obs}}^a$ (Å)	$\epsilon_{\text{obs}}^b$ (cm <sup>-1</sup> )	$\lambda_{\text{lit.}}^c$ (Å)	$\Delta\lambda_{\text{obs-lit.}}^d$ (Å)	$I_{\text{obs}}^d$ (arb. u.)	Char <sup>e</sup>	Lower Level	Upper Level	A (s <sup>-1</sup> )	Acc <sup>f</sup>	Line Ref. #	TP Ref. #	Notes <sup>h</sup>
1970.4935(6)	50748.707(15)	1970.4935(7)	-0.0004	760000	4s	3D <sub>2</sub>	4p	1P <sup>o</sup> <sub>1</sub>	C+	F	K82cor	
1974.467(3)	50646.507(8)	1974.4673(8)	-0.000	2800	s <sup>2</sup>	1D <sub>2</sub>	5f	(5/2) <sup>o</sup> [5/2] <sub>1</sub> <sup>3</sup>		TW		
1977.0266(3)	50581.009(6)	1977.02671(15)	-0.0001	8000	s <sup>2</sup>	3F <sub>2</sub>	4p	(3/2) <sup>o</sup> [3/2] <sub>1</sub>		F	D05se	
1979.95578(4)	50506.1785(10)	1979.95579(3)	-0.00002	18000000	4s	3D <sub>2</sub>	5p	3D <sup>o</sup> <sub>2</sub>	C+	F		
1982.15103(20)	50450.26(5)	1982.14827(12)	0.0021	16000	s <sup>2</sup>	3F <sub>3</sub>	4p	( <sup>o</sup> P) <sup>3</sup> P <sup>o</sup> - <sup>o</sup> D <sup>o</sup> <sub>2</sub>		TW		
1984.763(3)	50383.85(8)	1984.76431(19)	-0.001	14000	s <sup>2</sup>	1D <sub>2</sub>	6p	(5/2) <sup>o</sup> [3/2] <sub>1</sub> <sup>2</sup>		TW		
1986.307(3)	50344.68(8)	1986.30794(14)	-0.001	8100	s <sup>2</sup>	1D <sub>2</sub>	4p	( <sup>o</sup> P) <sup>3</sup> P <sup>o</sup> - <sup>o</sup> D <sup>o</sup> <sub>3</sub>		TW		
1989.85478(6)	50294.9238(9)	1989.85480(3)	-0.00001	7400000	4s	3D <sub>2</sub>	4p	3D <sup>o</sup> <sub>1</sub>	C+	F	D05	
1990.18000(19)	50246.711(5)	1990.18009(7)	-0.00009	670000	4p	3P <sup>o</sup> <sub>1</sub>	4d	(3/2) <sup>o</sup> [3/2] <sub>2</sub>	C	F	B00	
1993.8395(21)	50154.49(5)	1993.8395(12)	-0.0000	34000	s <sup>2</sup>	3F <sub>2</sub>	5p	( <sup>o</sup> P) <sup>3</sup> P <sup>o</sup> - <sup>o</sup> S <sup>o</sup> <sub>1</sub>		TWh		
1994.257(3)	50143.98(8)	1994.25958(15)	-0.0002	17000	s <sup>2</sup>	3F <sub>2</sub>	5p	(3/2) <sup>o</sup> [1/2] <sub>1</sub> <sup>o</sup>		TW		
1998.55751(16)	50036.09(4)	1998.55790(7)	-0.0004	34000	4p	3F <sub>3</sub>	4d	(3/2) <sup>o</sup> [5/2] <sub>1</sub>	F	F		
1999.5327(18)	50011.69(5)	1999.53361(8)	-0.0009	140000	4p	3P <sup>o</sup> <sub>1</sub>	4d	(3/2) <sup>o</sup> [3/2] <sub>1</sub>	C	TW	B00	
1999.69752(6)	49991.3640(16)	1999.69754(5)	-0.00002	20000000	4s	3D <sub>3</sub>	4p	3D <sup>o</sup> <sub>3</sub>	B	F	C94c	
2002.9033(20)	49911.36(5)	2002.9020(12)	0.0013	73000	s <sup>2</sup>	3F <sub>1</sub>	4p	( <sup>o</sup> P) <sup>3</sup> P <sup>o</sup> - <sup>o</sup> S <sup>o</sup> <sub>1</sub>		TWh		
2009.32(15)	49752(4)	2009.28239(8)	0.04	6800	4p	3F <sup>o</sup> <sub>4</sub>	4d	(3/2) <sup>o</sup> [5/2] <sub>1</sub>		S36c		
2012.98037(14)	49661.540(4)	2012.98041(6)	-0.00004	1800000	4p	3P <sup>o</sup> <sub>2</sub>	4d	(3/2) <sup>o</sup> [5/2] <sub>2</sub>	C	F	B00	
2015.5822(4)	49597.442(10)	2015.58222(8)	0.0000	1400000	4s	3D <sub>1</sub>	4p	1P <sup>o</sup> <sub>1</sub>	C+	F	K82cor	
2015.8660(24)	49590.46(6)	2015.8649(12)	0.0011	39000	s <sup>2</sup>	3F <sub>0</sub>	4p	( <sup>o</sup> P) <sup>3</sup> P <sup>o</sup> - <sup>o</sup> S <sup>o</sup> <sub>1</sub>		TWh		
2016.8964(6)	49565.129(14)	2016.89673(6)	-0.0003	1700000	4s	3D <sub>3</sub>	4p	1D <sup>o</sup> <sub>2</sub>	C+	F	D05se	
2017.6096(16)	49547.61(4)	2017.60977(12)	-0.0002	160000	s <sup>2</sup>	3F <sub>3</sub>	5p	(5/2) <sup>o</sup> [5/2] <sub>1</sub> <sup>3</sup>		F		
2022.1913(16)	49435.37(4)	2022.19147(7)	-0.0002	170000	4p	3F <sup>o</sup> <sub>3</sub>	4d	(3/2) <sup>o</sup> [7/2] <sub>4</sub>	C+	F	O07	
2025.46773(12)	49354.924(9)	2025.46775(5)	-0.00001	8100000	4s	3D <sub>1</sub>	4p	3D <sup>o</sup> <sub>2</sub>	C+	F	D05se	
2025.919(3)	49344.43(8)	2025.91683(13)	0.002	25000	s <sup>2</sup>	3F <sub>3</sub>	5p	(5/2) <sup>o</sup> [5/2] <sub>1</sub> <sup>2</sup>		TW		
2027.1336(6)	49314.858(15)	2027.13416(9)	-0.0005	610000	4p	3P <sup>o</sup> <sub>1</sub>	4d	(3/2) <sup>o</sup> [1/2] <sub>1</sub>	C	F	O07se	
2029.471(3)	49258.06(8)	2029.47227(16)	-0.001	37000	s <sup>2</sup>	3F <sub>2</sub>	4d	( <sup>o</sup> P) <sup>3</sup> P <sup>o</sup> - <sup>o</sup> D <sup>o</sup> <sub>2</sub>		TW		
2029.9491(7)	49246.469(17)	2029.94908(6)	0.0000	560000	4p	3P <sup>o</sup> <sub>2</sub>	4d	(5/2) <sup>o</sup> [3/2] <sub>1</sub>	B	F	O07	
2031.03579(16)	49220.123(4)	2031.03598(6)	-0.00020	2700000	4p	3P <sup>o</sup> <sub>2</sub>	4d	(5/2) <sup>o</sup> [3/2] <sub>2</sub>	B	F	O07	
2033.844(3)	49152.18(8)	2033.84242(8)	0.001	62000	4p	3F <sup>o</sup> <sub>4</sub>	4d	(3/2) <sup>o</sup> [7/2] <sub>1</sub>	C+	TW	D05	
2035.8532(6)	49103.6704(15)	2035.85327(4)	-0.00006	19000000	4s	3D <sub>1</sub>	4d	3D <sup>o</sup> <sub>1</sub>	C+	F	D05	
2036.9201(3)	49077.954(8)	2036.92001(9)	0.00001	730000	4p	3P <sup>o</sup> <sub>0</sub>	4d	(3/2) <sup>o</sup> [3/2] <sub>1</sub>	C	F	B00	
2037.12672(4)	49072.9776(9)	2037.12668(3)	0.00004	13000000	4s	3D <sub>2</sub>	4p	3D <sup>o</sup> <sub>3</sub>	C	F	C94c	
2043.8019(5)	48912.725(11)	2043.80148(7)	0.0004	21000000	4s	3D <sub>3</sub>	4p	1F <sup>o</sup> <sub>3</sub>	C+	R1c	D05se	
2047.67825(16)	48820.143(4)	2047.67825(11)	-0.00000	1300000	4p	3P <sup>o</sup> <sub>1</sub>	4d	(3/2) <sup>o</sup> [1/2] <sub>2</sub>	B+	F	B09	
2054.25259(21)	48663.922(5)	2054.25263(8)	-0.00003	810000	4p	3F <sup>o</sup> <sub>2</sub>	4d	(3/2) <sup>o</sup> [5/2] <sub>2</sub>	C	F	B00	
2054.4171(3)	48640.025(7)	2054.41739(8)	-0.0003	960000	4p	3P <sup>o</sup> <sub>2</sub>	4d	(5/2) <sup>o</sup> [1/2] <sub>1</sub>	C	F	R00	
2054.97836(4)	48566.7370(10)	2054.97836(3)	0.00001	18000000	4s	3D <sub>2</sub>	4p	1D <sup>o</sup> <sub>2</sub>	C+	F	D05se	
2058.611(3)	48560.91(8)	2058.61377(13)	-0.003	49000	s <sup>2</sup>	3F <sub>3</sub>	5p	(5/2) <sup>o</sup> [3/2] <sub>1</sub> <sup>2</sup>		TW		
2062.4201(4)	48471.230(8)	2062.42011(6)	-0.0000	1300000	4p	3P <sup>o</sup> <sub>1</sub>	4d	(5/2) <sup>o</sup> [5/2] <sub>2</sub>	C	F	B00	

Table A1. Cont.

$\lambda_{\text{obs}}^a$ (Å)	$\sigma_{\text{obs}}^b$ (cm <sup>-1</sup> )	$\lambda_{\text{lit}}^c$ (Å)	$\Delta\lambda_{\text{obs-lit}}^d$ (Å)	Char <sup>e</sup>	Lower Level	Upper Level	A (s <sup>-1</sup> )	Acc <sup>f</sup>	Line Ref. #	TP Ref. #	Notes <sup>h</sup>
2066.2609(5)	48381.143(12)	2066.26109(10)	-0.0002		4p	3p <sup>o</sup> 4d	2.00e+08	B+	F	O07	
2067.368(3)	48355.23(7)	2067.36392(16)	0.004		s <sup>2</sup>	3f <sub>2</sub> 5p			TW	B00	
2069.9336(13)	48295.27(3)	2069.93487(7)	0.0007		4p	3f <sub>2</sub> 4d	3.7e+07	C	F	B00	
2074.213(3)	48195.68(8)	2074.20995(16)	0.003		s <sup>2</sup>	3f <sub>2</sub> 5p			TW	O07	
		2074.24066(15)		m	s <sup>2</sup>	(3p) <sup>3</sup> P <sup>o</sup> 3D <sup>o</sup> <sub>2</sub>			TW	O07	
2078.66147(9)	48092.5549(21)	2078.66153(6)	-0.00005		4p	3p <sub>2</sub> 4d	6.3e+08	B+	F	O07	
2080.0593(13)	48060.24(3)	2080.05953(9)	-0.0002		4p	3p <sub>2</sub> 4d	4.9e+07	C	R1c	B00	
2082.920(20)	47994.2(3)	2082.91335(6)	0.005		4s	3p <sub>2</sub> 4d	1.0e+06	E	S3ec	D05se	
2084.32929(20)	47961.94(5)	2084.32369(22)	-0.0008		s <sup>2</sup>	(3p) <sup>3</sup> P <sup>o</sup> 3P <sup>o</sup> <sub>4</sub>			TW	B00	
2085.27359(4)	47940.081(21)	2085.27476(6)	-0.0012		4p	3p <sub>2</sub> 4d	6.7e+07	C	R1c	B00	
2085.297(4)	47939.55(9)	2085.30956(7)	-0.013		4s	3p <sub>2</sub> 4d	4.1e+06	C+	TW	D05kor	
2087.91812(11)	47879.3666(25)	2087.91817(7)	-0.00005		4p	3p <sub>2</sub> 4d	4.2e+08	B	F	B00	
2087.96979(24)	47878.182(5)	2087.96987(6)	-0.00008		4p	3p <sub>2</sub> 4d	2.6e+08	C	F	B00	
2083.63866(5)	47748.606(11)	2083.63705(6)	-0.0004		4p	3p <sub>2</sub> 4d	2.0e+08	B	R1c	O07	
2094.7925(9)	47722.26(21)	2094.79321(6)	-0.0007		4p	3p <sub>1</sub> 4d	2.21e+07	C+	R1c	O07	
2096.1891(14)	47690.47(3)	2096.19052(9)	-0.0014		4p	1F <sub>3</sub> 4d	1.6e+07	C	R1c	B00	
2098.3067(3)	47642.348(7)	2098.30677(8)	-0.0001		4p	1F <sub>3</sub> 4d	1.01e+08	C	F	B00	
2098.3971(2)	47640.295(6)	2098.39724(8)	-0.0001		4p	3F <sub>4</sub> 4d	2.09e+08	B	R1c	O07	
2098.7405(9)	47632.502(21)	2098.74108(6)	-0.0006		4p	3F <sub>4</sub> 4d	2.0e+07	C	R1c	B00	
2100.397(3)	47594.94(7)	2100.39318(8)	0.004		4p	3F <sub>4</sub> 4d			TW	O07	
2104.79587(5)	47495.4827(11)	2104.79586(4)	0.00002		4s	3D <sub>1</sub>	7.7e+07	C+	F	D05se	
2106.3816(11)	47459.73(6)	2106.3791(3)	0.025		s <sup>2</sup>	3F <sub>5</sub> 3p			F		
2110.308(6)	47371.45(7)	2110.30833(15)	-0.001		s <sup>2</sup>	3F <sub>2</sub> 3p			TW	B00	
2111.2934(4)	47349.333(10)	2111.29323(8)	0.0001		4p	3F <sub>4</sub> 4d			R1c	B00	
2112.09930(19)	47331.268(4)	2112.09946(9)	-0.00016		4s	1D <sub>2</sub> 4p	6.6e+07	C	F	D05se	
2112.52451(14)	47321.74(3)	2112.52195(8)	0.0026		4p	1F <sub>3</sub> 4d	3.5e+08	C+	R1c	B00	
2117.30881(9)	47214.8259(20)	2117.30874(7)	0.00006		4p	3F <sub>3</sub> 4d	1.2e+07	C	F	B00	
2118.3748(20)	47191.07(5)	2118.37484(7)	-0.0001		4p	3F <sub>3</sub> 4d	7.2e+08	B	F	O07	
2122.97861(13)	47088.745(3)	2122.97858(6)	0.00003		4s	1D <sub>2</sub> 4p	2.7e+07	B	TW	O07	
2125.10512(12)	47041.631(3)	2125.10507(7)	0.00004		4p	1F <sub>3</sub> 4d	2.2e+08	C+	F	D05se	
2125.2670(5)	47038.048(12)	2125.26686(8)	0.0001		4p	1D <sub>2</sub> 4d	2.28e+08	B+	F	O07	
2126.04361(6)	47020.8676(14)	2126.04362(5)	-0.00001		4p	3D <sub>2</sub> 4d	6.6e+07	C	F	B00	
2130.0848(5)	46931.669(10)	2130.08459(9)	0.0002		4p	3F <sub>4</sub> 4d	1.41e+08	B	R1c	C94c	
2131.2548(6)	46905.908(13)	2131.25395(8)	-0.0011		4p	1F <sub>3</sub> 4d	4.4e+07	B+	R1c	O07	
2134.3400(4)	46838.113(9)	2134.34030(8)	-0.0003		4p	3F <sub>4</sub> 4d	1.3e+07	C	R1c	B00	
2135.399	46814.89	2135.9887(8)		:	4p	3P <sup>o</sup> 4d	7.7e+08	B	R1c	B00	
2135.9808(7)	46802.1511(16)	2135.98004(6)	0.00004		4s	3P <sup>o</sup> <sub>2</sub>	4.e+07	E	F	O07se	
2144.7061(10)	46611.76(22)	2144.70358(6)	0.002	*	4p	3D <sup>o</sup> <sub>3</sub>	4.59e+08	A+	R1c	P97	
							1.3e+07	C	R1c	B00	

Table A1. Cont.

$\lambda_{\text{obs}}^a$ (Å)	$\sigma_{\text{obs}}^b$ (cm <sup>-1</sup> )	$\lambda_{\text{NIST}}^c$ (Å)	$\Delta\lambda_{\text{obs-NIST}}^d$ (Å)	Char <sup>e</sup>	Lower Level	Upper Level	A (s <sup>-1</sup> )	Acc <sup>f</sup>	Line Ref. #	TP Ref. #	Notes <sup>h</sup>
2144.706(10)	46611.76(22)	2144.72206(16)	-0.016	s <sup>2</sup>	3F <sub>3</sub>	( <sup>3</sup> P) <sup>3</sup> P <sup>3</sup> F <sub>3</sub>			R1c		
2145.4920(4)	46594.68(9)	2145.49206(7)	-0.0001	4p	3P <sup>1</sup> <sub>1</sub>	(5/2) <sup>2</sup> [1/2] <sub>1</sub>	1.14e+08	B	R1c	O07	
2146.9187(4)	46563.722(8)	2146.91894(7)	-0.0002	4p	3D <sup>3</sup> <sub>3</sub>	(3/2) <sup>2</sup> [5/2] <sub>3</sub>	1.04e+08	C	F		
		2148.94587(6)		4s	3F <sub>2</sub>	(5/2) <sup>2</sup> [5/2] <sub>2</sub>	1.12e+08	C	S36c	B00	
2148.9830(6)	46518.99(13)	2148.98283(8)	0.0002	4s	3D <sup>3</sup> <sub>2</sub>	3F <sub>3</sub>	8.8e+07	B	R1c	C94c	
2151.8083(4)	46457.927(9)	2151.80815(7)	0.0001	4p	3F <sub>2</sub>	(5/2) <sup>2</sup> [7/2] <sub>1</sub>	2.59e+08	B	R1c	B00	
2152.9102(0)	46434.2(4)	2152.90029(9)	0.010	4p	1D <sup>2</sup> <sub>2</sub>	(3/2) <sup>2</sup> [3/2] <sub>1</sub>			S36c		
2158.4108(10)	46315.829(21)	2158.41130(19)	-0.0005	s <sup>2</sup>	3F <sub>2</sub>	( <sup>3</sup> F) <sup>3</sup> P <sup>3</sup> F <sub>2</sub>			R1c		
2161.31978(23)	46253.498(5)	2161.31990(7)	-0.00012	4p	3D <sup>3</sup> <sub>2</sub>	(3/2) <sup>2</sup> [7/2] <sub>3</sub>	3.1e+08	B	F	B00	
2161.7998(10)	46243.228(21)	2161.80255(7)	-0.00027	4p	3D <sup>3</sup> <sub>3</sub>	(3/2) <sup>2</sup> [5/2] <sub>2</sub>			R1c		
2166.850(20)	46135.5(4)	2166.8678(3)	-0.018	s <sup>2</sup>	3F <sub>3</sub>	( <sup>3</sup> F) <sup>3</sup> P <sup>3</sup> F <sub>3</sub>	4.9e+08	B	S36c	O07	
2174.98119(9)	45963.0038(18)	2174.98126(6)	-0.00007	4p	3D <sup>3</sup> <sub>3</sub>	(3/2) <sup>2</sup> [7/2] <sub>4</sub>	2.15e+08	B	F	C94c	
2179.41026(22)	45869.606(5)	2179.40994(6)	0.00033	4s	3D <sup>1</sup> <sub>1</sub>	( <sup>3</sup> F) <sup>3</sup> P <sup>3</sup> C <sup>3</sup> C <sup>3</sup> <sub>5</sub>			R1c		
2180.7598(5)	45841.413(11)			s <sup>2</sup>	3F <sub>4</sub>				R1c		
2181.4243(4)	45827.26(9)	2181.42461(7)	-0.0003	4p	3D <sup>3</sup> <sub>3</sub>	(3/2) <sup>2</sup> [7/2] <sub>3</sub>	2.4e+07	C	R1c	B00	
2182.8585(5)	45797.154(11)	2182.85780(7)	0.0007	4p	3F <sub>2</sub>	(5/2) <sup>2</sup> [3/2] <sub>1</sub>	8.0e+07	C+	R1c	O07	
2189.3693(10)	45660.976(21)	2189.36930(8)	0.0000	4p	3P <sup>0</sup> <sub>0</sub>	(5/2) <sup>2</sup> [1/2] <sub>1</sub>	1.3e+07	C	R1c	O07se	
2189.62967(9)	45635.5468(18)	2189.62971(6)	-0.00004	4s	1D <sup>2</sup> <sub>2</sub>	(3/2) <sup>2</sup> [1/2] <sub>1</sub>	1.04e+08	B	FR1c	C94c	
2190.500(20)	45637.4(4)	2190.5192(3)	-0.019	s <sup>2</sup>	1G <sub>4</sub>	3D <sup>3</sup> <sub>3</sub>			S36c		
2192.26759(8)	45600.6159(16)	2192.26753(6)	0.00007	4s	3D <sup>3</sup> <sub>2</sub>	(3/2) <sup>2</sup> [5/2] <sub>3</sub>	2.8e+08	B	F	C94c	
2195.68180(17)	45529.716(4)	2195.68192(7)	-0.00012	4p	1F <sup>3</sup> <sub>3</sub>	(5/2) <sup>2</sup> [7/2] <sub>4</sub>	4.2e+08	B	F	O07	
2197.8688(15)	45484.42(3)	2197.86726(7)	0.0016	4p	1F <sup>3</sup> <sub>3</sub>	(5/2) <sup>2</sup> [7/2] <sub>3</sub>			R1c		
2200.300(20)	45434.2(4)	2200.31543(20)	-0.015	s <sup>2</sup>	3F <sub>0</sub>	( <sup>3</sup> P) <sup>3</sup> P <sup>3</sup> D <sup>3</sup> <sub>1</sub>			S36c		
2200.5078(3)	45429.874(6)	2200.50822(8)	-0.0004	4p	3D <sup>1</sup> <sub>1</sub>	(3/2) <sup>2</sup> [5/2] <sub>2</sub>	2.1e+08	C	F	B00	
2201.000(20)	45419.7(4)	2201.02822(20)	-0.028	s <sup>2</sup>	3F <sub>2</sub>	( <sup>3</sup> F) <sup>3</sup> P <sup>3</sup> F <sub>3</sub>			S36c		
2209.8049(4)	45238.760(8)	2209.80507(7)	-0.0002	4p	1F <sup>3</sup> <sub>3</sub>	(5/2) <sup>2</sup> [5/2] <sub>3</sub>	2.1e+08	C	R1c	B00	
2210.26692(11)	45229.3048(22)	2210.26693(6)	-0.00001	4s	1D <sup>2</sup> <sub>2</sub>	1D <sup>2</sup> <sub>2</sub>	1.53e+08	C+	F	D05se	
2212.7470(6)	45178.67(12)	2212.74730(8)	-0.0003	4p	3D <sup>3</sup> <sub>2</sub>	(3/2) <sup>2</sup> [5/2] <sub>2</sub>	1.4e+08	C	F	B00	
2215.1054(3)	45130.521(5)	2215.10550(8)	-0.0001	4p	3D <sup>3</sup> <sub>2</sub>	(3/2) <sup>2</sup> [5/2] <sub>3</sub>	4.9e+08	B	F	B00	
2218.10770(6)	45069.4401(12)	2218.10772(5)	-0.00002	4s	3D <sup>2</sup> <sub>2</sub>	3P <sup>1</sup> <sub>1</sub>	3.5e+08	C+	F	D05se	
2218.5123(4)	45061.222(4)	2218.51209(8)	0.0002	4p	3D <sup>1</sup> <sub>1</sub>	(3/2) <sup>2</sup> [3/2] <sub>2</sub>	2.6e+08	C	R1c	B00	
2221.649(3)	44997.60(6)	2221.6477(8)	0.001	s <sup>2</sup>	1D <sup>2</sup> <sub>2</sub>	( <sup>1</sup> D) <sup>3</sup> P <sup>3</sup> P <sup>3</sup> <sub>2</sub>			R1c		
2224.690(5)	44936.092(10)	2224.69062(11)	-0.0000	4p	1P <sup>1</sup> <sub>1</sub>	(3/2) <sup>2</sup> [5/2] <sub>2</sub>	1.3e+08	C	R1c	B00	
2226.7798(4)	44893.936(8)	2226.77999(6)	-0.0002	4s	3D <sup>1</sup> <sub>1</sub>	(5/2) <sup>2</sup> [5/2] <sub>2</sub>	2.9e+08	C	R1c	B00	
2228.86748(6)	44851.8904(11)	2228.86745(6)	0.00003	4s	3D <sup>1</sup> <sub>1</sub>	3P <sup>0</sup> <sub>0</sub>	3.88e+08	B+	F	P97	
2229.8529(4)	44832.072(8)	2229.85346(6)	-0.0006	4p	1D <sup>2</sup> <sub>2</sub>	(5/2) <sup>2</sup> [7/2] <sub>1</sub>	2.1e+08	C	R1c	B00	
2230.1439(7)	44826.221(15)	2230.14604(9)	-0.0022	4p	3D <sup>1</sup> <sub>1</sub>	(3/2) <sup>2</sup> [3/2] <sub>1</sub>	1.9e+08	C	R1c	B00	
2230.3979(7)	44821.118(13)	2230.39901(9)	-0.0011	4p	1F <sup>3</sup> <sub>3</sub>	(5/2) <sup>2</sup> [9/2] <sub>4</sub>	2.0e+07	C	R1c	O07se	

Table A1. Cont.

$\lambda_{\text{obs}}^a$ (Å)	$\sigma_{\text{obs}}^b$ (cm <sup>-1</sup> )	$\lambda_{\text{NIST}}^c$ (Å)	$\Delta\lambda_{\text{obs-NIST}}^d$ (Å)	Char <sup>e</sup>	Lower Level	Upper Level	A (s <sup>-1</sup> )	Ace <sup>f</sup>	Line Ref. #	TP Ref. #	Notes <sup>h</sup>
2230.9512(6)	44810.0031(12)	2230.95279(8)	-0.0016	4p	3D <sup>2</sup>	4d	(3/2) <sup>2</sup> [5/2] <sub>2</sub>	C	R1c	B00	
2231.5817(4)	44797.343(8)	2231.58204(7)	-0.0003	4p	1F <sup>3</sup>	4d	(5/2) <sup>2</sup> [5/2] <sub>2</sub>	B	R1c	O07	
2242.1424(11)	44586.363(21)	2242.14217(6)	0.0003	4p	1D <sup>2</sup>	4d	(5/2) <sup>2</sup> [5/2] <sub>3</sub>	C	R1c	B00	
2242.61775(10)	44576.9146(20)	2242.61764(7)	0.00011	4s	1D <sup>2</sup>	4d	1F <sup>3</sup>	C+	F	D05se	
2242.718(3)	44574.93(5)	2242.71791(9)	-0.000	4p	3D <sup>2</sup>	4d	(3/2) <sup>2</sup> [3/2] <sub>1</sub>	C	TW	B00	
2243.0938(7)	44567.454(14)	2243.09395(10)	-0.0001	4p	1P <sup>1</sup>	4d	(3/2) <sup>2</sup> [3/2] <sub>2</sub>	C	R1c	B00	
2247.0017(5)	44489.953(11)	2247.00170(9)	-0.0000	4s	3P <sup>3</sup>	4d	1S <sup>0</sup>	B	R1c	O94c	
2248.9666(4)	44451.086(8)	2248.96667(6)	-0.0001	4p	3D <sup>3</sup>	4d	(5/2) <sup>2</sup> [7/2] <sub>1</sub>	C	R1c	O07	
2251.8564(5)	44394.049(9)	2251.85601(8)	0.0004	4p	1D <sup>2</sup>	4d	(3/2) <sup>2</sup> [7/2] <sub>3</sub>	C	R1c	B00	
2253.0326(16)	44370.87(3)	2253.0273(3)	0.0053	s <sup>2</sup>	1D <sup>2</sup>	4d	(1D) <sup>1</sup> P <sup>3</sup> -3P <sup>1</sup>	C	R1c	B00	
2254.9880(4)	44332.402(8)	2254.98778(11)	0.0002	4p	1P <sup>1</sup>	4d	(3/2) <sup>2</sup> [5/2] <sub>1</sub>	B+	R1c	B00	
2263.2130(4)	44171.302(8)	2263.21318(6)	-0.0002	4p	1D <sup>2</sup>	4d	(5/2) <sup>2</sup> [5/2] <sub>1</sub>	C	R1c	O07	
2263.7857(4)	44160.128(8)	2263.78578(6)	-0.0000	4p	1D <sup>3</sup>	4d	(5/2) <sup>2</sup> [5/2] <sub>2</sub>	E	R1c	O07se	
2264.5671(16)	44144.89(3)	2264.56423(6)	0.0029	4p	1D <sup>2</sup>	4d	(3/2) <sup>2</sup> [1/2] <sub>1</sub>	B	R1c	O07	
2265.3643(4)	44129.358(8)	2265.36424(10)	0.0001	4p	3D <sup>1</sup>	4d	(3/2) <sup>2</sup> [5/2] <sub>2</sub>	E	R1c	O94	
2274.7407(6)	43947.476(11)	2274.74107(8)	-0.0004	4s	3P <sup>2</sup>	5s	(3/2) <sup>2</sup> F <sup>3</sup> -2D <sup>3</sup>	C+	R1c	D05se	
2276.2577(4)	43918.191(8)	2276.25797(7)	-0.0003	4s	3D <sup>1</sup>	4p	3P <sup>1</sup>	C+	R1c	D05se	
2278.3378(5)	43878.098(10)	2278.33737(10)	0.0004	4p	3D <sup>2</sup>	4d	(3/2) <sup>2</sup> [1/2] <sub>1</sub>	B+	R1c	O07	
2280.9423(4)	43827.999(8)	2280.9428(3)	-0.0005	s <sup>2</sup>	3F <sup>3</sup>	4d	(1F) <sup>3</sup> P <sup>3</sup> -3G <sup>4</sup>		R1c		
2284.202(4)	43765.46(7)	2284.19835(22)	0.004	s <sup>2</sup>	1G <sub>4</sub>	sp	(1G) <sup>3</sup> P <sup>3</sup> -3F <sup>3</sup>		R1c		
2286.6447(4)	43718.713(8)	2286.64494(6)	-0.0002	4p	3D <sup>3</sup>	4d	(5/2) <sup>2</sup> [3/2] <sub>2</sub>	B+	R1c	O07	
2289.4160(4)	43665.797(8)	2289.41619(8)	-0.0002	4p	3P <sup>2</sup>	5s	(3/2) <sup>2</sup> [3/2] <sub>1</sub>	D	R1c	O94	
2290.1666(7)	43631.600(14)	2290.16119(23)	-0.006	s <sup>2</sup>	3F <sup>2</sup>	sp	(1P) <sup>3</sup> P <sup>3</sup> -2D <sup>3</sup>		R1c		
2291.0018(4)	43635.575(8)	2291.00110(12)	0.0007	5s	1P <sup>1</sup>	4d	(3/2) <sup>2</sup> [1/2] <sub>1</sub>	B+	R1c	O07	
2292.6896(6)	43603.454(11)	2292.69060(8)	-0.0010	4s	1D <sup>2</sup>	4p	(1P) <sup>3</sup> P <sup>3</sup> -3F <sup>4</sup>	E	R1c	D05cor	
2292.9699(6)	43598.124(11)	2292.9700(3)	-0.0002	s <sup>2</sup>	3F <sub>4</sub>	sp	3P <sup>2</sup>		R1c		
2294.3674(4)	43571.571(8)	2294.36738(7)	-0.0002	4s	3D <sup>2</sup>	4p	(5/2) <sup>2</sup> [1/2] <sub>0</sub>	C+	R1c	O94c	
2299.4885(5)	43474.547(9)	2299.48891(10)	-0.0004	4p	3D <sup>1</sup>	4d	(5/2) <sup>2</sup> [5/2] <sub>2</sub>	C	R1c	B00	
2309.5189(4)	43285.747(8)	2309.51890(6)	-0.0000	4p	3D <sup>1</sup>	4d	(1D) <sup>3</sup> P <sup>3</sup> -3F <sup>3</sup>		R1c	B00	
2315.681(5)	43170.571(10)	2315.6826(4)	-0.002	s <sup>2</sup>	1D <sup>2</sup>	sp	(5/2) <sup>2</sup> [7/2] <sub>3</sub>	C	R1c	B00	
2323.009(5)	43034.495(9)	2323.00409(6)	-0.0002	4p	3D <sup>2</sup>	4d	(5/2) <sup>2</sup> [5/2] <sub>2</sub>		R1c		
2323.9280(6)	43017.383(11)	2323.92802(7)	0.0000	4p	1D <sup>2</sup>	4d	(5/2) <sup>2</sup> [1/2] <sub>1</sub>		R1c		
2325.9100(17)	42980.73(3)	2325.90832(12)	0.0017	4p	1P <sup>1</sup>	4d	(5/2) <sup>2</sup> [1/2] <sub>0</sub>		R1c		
2327.5669(6)	42950.137(11)	2327.5672(4)	-0.0003	s <sup>2</sup>	3F <sub>3</sub>	sp	(1P) <sup>3</sup> P <sup>3</sup> -3F <sup>2</sup>		R1c		
2333.743(3)	42836.49(6)	2333.75088(22)	-0.008	s <sup>2</sup>	1G <sub>4</sub>	6p	(5/2) <sup>2</sup> [7/2] <sub>3</sub>		R1c		
2336.1707(4)	42791.971(8)	2336.17057(10)	0.0001	1P <sup>1</sup>	1D <sup>1</sup>	4d	(5/2) <sup>2</sup> [5/2] <sub>2</sub>		R1c	B00	
2339.7275(5)	42726.924(10)	2339.72732(6)	0.0002	4p	3D <sup>2</sup>	4d	(5/2) <sup>2</sup> [5/2] <sub>1</sub>		R1c		
2341.3713(12)	42696.930(21)	2341.3713(12)	-0.0011	s <sup>2</sup>	3F <sub>4</sub>	sp	(1P) <sup>3</sup> P <sup>3</sup> -3P <sup>5</sup>		R1c		
2342.1723(17)	42682.33(3)	2342.1723(17)	-0.0000	s <sup>2</sup>	3P <sup>2</sup>	sp	(1P) <sup>3</sup> P <sup>3</sup> -3D <sup>3</sup>		R1c		
2347.890(20)	42578.4(4)	2347.8850(4)	0.005	s <sup>2</sup>	3P <sup>2</sup>	sp	(1P) <sup>3</sup> P <sup>3</sup> -3D <sup>1</sup>		S36c		

Table A1. Cont.

$\lambda_{\text{obs}}^a$ (Å)	$\sigma_{\text{obs}}^b$ (cm <sup>-1</sup> )	$\lambda_{\text{lit}}^c$ (Å)	$\Delta\lambda_{\text{obs-lit}}^d$ (Å)	Char <sup>e</sup>	Lower Level	Upper Level	A (s <sup>-1</sup> )	Acc <sup>f</sup>	Line Ref. #	TP Ref. #	Notes <sup>h</sup>
2347.890(20)	42578.4(4)	2347.914(3)	-0.024	5s	(3/2) <sup>3</sup> [2] <sub>2</sub>	sp			S6cen		
2348.7330(4)	42563.115(8)	2348.73311(7)	-0.0001	4p	3D <sup>1</sup> <sub>1</sub>	4d	2.8e+07	B		O07	
2350.1902(8)	42536.727(15)	2350.18820(6)	0.0020	4p	3D <sup>1</sup> <sub>1</sub>	4d			R1c		
2352.2911(12)	42498.740(21)	2352.29447(19)	-0.0034	s <sup>2</sup>	1G <sub>4</sub>	4f			R1c		
2353.9437(5)	42468.905(9)	2353.9434(4)	0.0003	s <sup>2</sup>	3F <sub>3</sub>	3F <sub>3</sub>			R1c		
2355.0143(6)	42449.600(11)	2355.01447(8)	-0.0001	4p	3P <sup>1</sup> <sub>1</sub>	5s	2.5e+07	C+	R1c	K82	
2356.6402(5)	42420.316(9)	2356.64033(9)	-0.0001	4p	3P <sup>1</sup> <sub>1</sub>	5s	3.0e+06	C+	R1c	C94c	
2360.6389(9)	42348.465(16)	2360.6391(9)	-0.0002	s <sup>2</sup>	3P <sup>1</sup> <sub>1</sub>	sp			R2hc		
2361.1901(12)	42338.579(21)	2361.1910(5)	-0.0008	s <sup>2</sup>	3P <sup>1</sup> <sub>1</sub>	sp			R1c		
2362.6809(9)	42311.867(16)	2362.68143(7)	-0.0005	4p	3D <sup>2</sup> <sub>2</sub>	4d	6.3e+06	C+	R1c	O07	
2364.1538(6)	42285.508(10)	2364.15386(7)	-0.0000	4p	3D <sup>2</sup> <sub>2</sub>	4d	3.4e+06	B	R1c	O07	
2366.980(3)	42235.03(5)	2366.9785(4)	0.001	5s	(5/2) <sup>3</sup> [5/2] <sub>1</sub>	5s			R1c		
2369.8893(5)	42183.179(9)	2369.88902(9)	0.0003	4s	1D <sup>2</sup> <sub>2</sub>	4p	5.3e+07	B	R1c	C94c	
2370.7464(5)	42167.930(8)	2370.74698(8)	-0.0006	4p	1P <sup>1</sup> <sub>1</sub>	5s	2.4e+07	C+	R1c	K82	
2376.3030(4)	42069.335(8)	2376.30277(10)	0.0003	4p	1P <sup>1</sup> <sub>1</sub>	4d	1.61e+08	C+	R1c	O07se	
2377.7920(6)	42042.994(10)	2377.79223(10)	-0.0003	4p	1P <sup>1</sup> <sub>1</sub>	4d	3.3e+06	D+	R1c	O07	
2378.4047(7)	42032.163(13)	2378.4063(6)	-0.0015	s <sup>2</sup>	3F <sub>2</sub>	sp			R1c		
2378.8442(12)	42024.399(21)	2378.8439(9)	0.0002	s <sup>2</sup>	3F <sub>2</sub>	sp			R1c		
2379.4048(12)	42014.499(21)	2379.4055(5)	-0.0007	s <sup>2</sup>	3F <sub>0</sub>	sp			R1c		
2384.80(6)	41919.5(11)	2384.85893(9)	-0.06	4p	3P <sup>2</sup> <sub>2</sub>	5s			R1c		
2384.9439(4)	41916.926(8)	2384.94408(9)	-0.0002	4p	3P <sup>2</sup> <sub>2</sub>	5s	6e+05	E	S36c	K82cal	
2385.0951(18)	41914.27(3)	2385.0945(4)	0.0006	s <sup>2</sup>	(5/2) <sup>3</sup> [5/2] <sub>1</sub>	sp	7e+06	E	R1c	K82cal	
2392.6632(18)	41781.32(3)	2392.6638(9)	-0.0006	s <sup>2</sup>	3P <sup>1</sup> <sub>1</sub>	sp			R1c		
2393.2599(5)	41771.287(9)	2393.2602(4)	-0.0003	s <sup>2</sup>	3F <sub>3</sub>	sp			R1c		
2394.0296(5)	41757.858(9)	2394.0296(4)	-0.0000	s <sup>2</sup>	3F <sub>2</sub>	sp			R1c		
2400.1140(7)	41652.008(12)	2400.11404(9)	-0.0001	4s	1D <sup>2</sup> <sub>2</sub>	4p	6.9e+06	C+	R1c	D05se	
2403.3373(5)	41596.149(8)	2403.33713(9)	0.0002	4p	3P <sup>2</sup> <sub>2</sub>	5s	1.06e+08	C+	R1c	C94	
2414.1881(5)	41409.205(9)	2414.18856(8)	-0.0004	4p	3D <sup>1</sup> <sub>1</sub>	4d	2e+06	E	R1c	O07cal	
2414.8568(5)	41397.740(9)	2414.8563(4)	0.0005	s <sup>2</sup>	3D <sup>2</sup> <sub>2</sub>	sp			R1c		
2421.9424(6)	41276.637(11)	2421.9425(4)	-0.0001	4p	3F <sub>2</sub>	sp			R1c		
2424.4338(3)	41254.223(5)	2424.43430(9)	-0.0005	4p	3P <sup>0</sup> <sub>0</sub>	5s	5.0e+07	C+	R1c	C94	
2426.558(5)	41190.13(8)	2426.5614(9)	-0.003	4d	(5/2) <sup>3</sup> [11/2] <sub>1</sub> <sup>6</sup>	8f			R1c		
2426.996(9)	41190.69(15)	2427.016(3)	-0.019	5s	(5/2) <sup>3</sup> [5/2] <sub>1</sub> <sup>2</sup>	7p			R2hc		
2428.9274(5)	41157.944(8)	2428.92746(8)	-0.0000	4p	1G <sub>4</sub>	4d	1.93e+07	C+	R1c	O07	
2430.6721(13)	41128.318(21)	2430.67651(24)	0.0007	s <sup>2</sup>	3D <sup>2</sup> <sub>2</sub>	sp			R1c		
2432.420(3)	41098.86(5)	2432.4183(5)	0.001	4d	(5/2) <sup>3</sup> [9/2] <sub>1</sub> <sup>8</sup>	8f			R1c		
2442.6646(5)	40926.494(9)			s <sup>2</sup>	3F <sub>4</sub>	sp			R1c		
2443.3256(5)	40915.423(8)	2443.32555(11)	0.0001	4p	1P <sup>1</sup> <sub>1</sub>	4d	2.00e+07	B	R1c	O07	
2448.2143(13)	40833.727(21)	2448.2131(4)	0.0012	s <sup>2</sup>	3P <sup>2</sup> <sub>2</sub>	sp			R1c		
2452.951(6)	40754.88(10)	2452.9576(7)	-0.006	s <sup>2</sup>	(D) <sup>3</sup> P <sup>2</sup> -3D <sup>3</sup> <sub>3</sub>	sp			R1c		



Table A1. Cont.

$\lambda_{\text{obs}}^a$ (Å)	$\sigma_{\text{obs}}^b$ (cm <sup>-1</sup> )	$\lambda_{\text{lit}}^c$ (Å)	$\Delta\lambda_{\text{obs-lit}}^d$ (Å)	Char <sup>e</sup>	Lower Level	Upper Level	A (s <sup>-1</sup> )	Acc <sup>f</sup>	Line Ref. #	TP Ref. #	Notes <sup>h</sup>
2456.008(4)	40704.16(7)	2455.99461(18)	0.013	s <sup>2</sup>	1G <sub>4</sub>	4f	(5/2) <sup>3</sup> F <sub>7/2</sub> <sup>o</sup>		R1c		
2462.6140(19)	40594.98(3)	2462.61266(17)	0.0014	s <sup>2</sup>	1G <sub>4</sub>	4f	(5/2) <sup>3</sup> F <sub>9/2</sub> <sup>o</sup>		R1c		
2464.307(5)	40567.10(8)	2464.30282(17)	0.004	s <sup>2</sup>	1G <sub>4</sub>	4f	(5/2) <sup>3</sup> F <sub>7/2</sub> <sup>o</sup>		R1c		
2468.3475(8)	40500.69(13)	2468.3480(6)	-0.0005	s <sup>2</sup>	3F <sub>1</sub>	5p	(1D) <sup>3</sup> P <sup>o</sup> -3P <sup>o</sup>		R1c		
2468.5000(5)	40498.187(8)	2468.5011(9)	-0.0011	4p	3F <sub>2</sub> <sup>o</sup>	5s	(3/2) <sup>3</sup> F <sub>2</sub> <sup>o</sup>	1.30e+07	C+	K82	
2473.3333(4)	40419.053(7)	2473.33345(9)	-0.0002	4p	3P <sub>2</sub> <sup>o</sup>	5s	(5/2) <sup>3</sup> F <sub>2</sub> <sup>o</sup>	5.9e+07	C+	C94	
2476.4439(7)	40368.287(11)	2476.44459(19)	-0.0007	s <sup>2</sup>	1G <sub>4</sub>	4f	(5/2) <sup>3</sup> F <sub>7/2</sub> <sup>o</sup>		R1c		
2483.784(5)	40249.00(8)	2483.7876(5)	-0.003	s <sup>2</sup>	3P <sub>1</sub>	5p	(1D) <sup>3</sup> P <sup>o</sup> -3D <sup>o</sup>		R1c		
2485.7919(5)	40216.489(8)	2485.79176(9)	0.0002	1000000	3F <sub>2</sub> <sup>o</sup>	5s	(3/2) <sup>3</sup> F <sub>2</sub> <sup>o</sup>	1.42e+08	C+	C94	L
2489.6523(6)	40154.136(10)	2489.65226(11)	-0.0001	4p	1D <sub>2</sub>	4s	(3/2) <sup>3</sup> F <sub>2</sub> <sup>o</sup>	1.0e+06	D+	C94c	
2499.0011(8)	40003.94(12)	2499.0132(4)	-0.013	s <sup>2</sup>	3F <sub>2</sub> <sup>o</sup>	5p	(1D) <sup>3</sup> P <sup>o</sup> -3P <sup>o</sup>		R1c		
2501.4933(13)	39964.07(21)	2501.4947(5)	-0.0014	4800	3F <sub>1</sub>	5p	(1D) <sup>3</sup> P <sup>o</sup> -3D <sup>o</sup>		R1c		
2506.2727(3)	39887.871(5)	2506.27258(10)	0.0001	1000000	3F <sub>3</sub> <sup>o</sup>	5s	(5/2) <sup>3</sup> F <sub>2</sub> <sup>o</sup>	2.0e+08	C+	C94	L
2514.2919(10)	39760.659(16)	2514.2931(4)	-0.0012	4200	3P <sub>1</sub>	5p	(1D) <sup>3</sup> P <sup>o</sup> -3P <sup>o</sup>		R1c		
2515.0822(7)	39748.166(11)	2515.0831(5)	-0.0008	8400	(5/2) <sup>3</sup> F <sub>2</sub> <sup>o</sup>	7p	(5/2) <sup>3</sup> F <sub>2</sub> <sup>o</sup>		R1c		
2518.9484(5)	39687.164(8)	2518.9484(5)	-0.0001	34000	3F <sub>3</sub> <sup>o</sup>	5p	(1D) <sup>3</sup> P <sup>o</sup> -3G <sup>o</sup>		R1c		
2526.3277(14)	39571.246(21)	2526.3234(4)	0.0043	1900	3F <sub>4</sub> <sup>o</sup>	5p	(1D) <sup>3</sup> P <sup>o</sup> -3D <sup>o</sup>		R1c		
2526.5923(5)	39567.103(7)	2526.59232(10)	-0.0000	500000	3F <sub>3</sub> <sup>o</sup>	5s	(5/2) <sup>3</sup> F <sub>2</sub> <sup>o</sup>	2.7e+07	C+	K82	
2529.30395(21)	39524.686(3)	2529.30385(10)	0.00010	940000	1F <sub>3</sub> <sup>o</sup>	5s	(3/2) <sup>3</sup> F <sub>2</sub> <sup>o</sup>	1.06e+08	C+	C94	
2542.9345(8)	39312.840(12)	2542.9357(4)	-0.0012	3200	(5/2) <sup>3</sup> F <sub>2</sub> <sup>o</sup>	7p	(5/2) <sup>3</sup> F <sub>2</sub> <sup>o</sup>		R1c		
2544.8050(20)	39283.945(3)	2544.80482(11)	0.00027	1200000	3F <sub>4</sub> <sup>o</sup>	5s	(5/2) <sup>3</sup> F <sub>2</sub> <sup>o</sup>	1.94e+08	B	B00	
2553.3430(5)	39152.595(8)	2553.3430(5)	-0.0000	14000	3F <sub>2</sub> <sup>o</sup>	5p	(1D) <sup>3</sup> P <sup>o</sup> -3G <sup>o</sup>		R1c		
2556.3698(9)	39106.241(13)	2556.3691(3)	0.0007	2800	(5/2) <sup>3</sup> F <sub>2</sub> <sup>o</sup>	7f	(5/2) <sup>3</sup> F <sub>2</sub> <sup>o</sup>		R1c		
2558.2130(5)	39078.067(8)	2558.2134(4)	-0.0004	5400	(5/2) <sup>3</sup> F <sub>2</sub> <sup>o</sup>	7f	(5/2) <sup>3</sup> F <sub>2</sub> <sup>o</sup>		R1c		
2559.4301(14)	39059.485(21)	2559.4301(13)	-0.0000	2700	(5/2) <sup>3</sup> F <sub>2</sub> <sup>o</sup>	7f	(5/2) <sup>3</sup> F <sub>2</sub> <sup>o</sup>		R1c		
2559.7925(20)	39053.96(3)	2559.7938(18)	-0.0012	4400	(5/2) <sup>3</sup> F <sub>2</sub> <sup>o</sup>	7f	(5/2) <sup>3</sup> F <sub>2</sub> <sup>o</sup>		R2hc		
2564.7257(6)	38978.841(9)	2564.7264(4)	-0.0007	5100	(5/2) <sup>3</sup> F <sub>2</sub> <sup>o</sup>	8p	(5/2) <sup>3</sup> F <sub>2</sub> <sup>o</sup>		R2hc		
2565.0459(7)	38973.975(10)	2565.0471(5)	-0.0011	2500	(3/2) <sup>3</sup> F <sub>2</sub> <sup>o</sup>	7f	(3/2) <sup>3</sup> F <sub>2</sub> <sup>o</sup>		R1c		
2568.9061(20)	38915.41(3)	2568.9075(4)	-0.0014	2400	(5/2) <sup>3</sup> F <sub>2</sub> <sup>o</sup>	6f	(5/2) <sup>3</sup> F <sub>2</sub> <sup>o</sup>		R1c		
2571.7551(6)	38872.306(9)	2571.7556(8)	-0.0004	22000	1D <sub>2</sub> <sup>o</sup>	5s	(3/2) <sup>3</sup> F <sub>2</sub> <sup>o</sup>	1.10e+07	C+	K82	
2574.4124(7)	38822.188(11)	2574.4125(5)	-0.0001	2100	3F <sub>3</sub> <sup>o</sup>	5p	(1D) <sup>3</sup> P <sup>o</sup> -3D <sup>o</sup>		R1c		
2574.6371(7)	38828.796(11)	2574.6371(5)	-0.0000	4600	(3/2) <sup>3</sup> F <sub>2</sub> <sup>o</sup>	7f	(3/2) <sup>3</sup> F <sub>2</sub> <sup>o</sup>		R1c		
2590.4012(9)	38592.515(14)	2590.3994(4)	0.0019	990	(5/2) <sup>3</sup> F <sub>2</sub> <sup>o</sup>	7f	(5/2) <sup>3</sup> F <sub>2</sub> <sup>o</sup>		R1c		
2590.52825(17)	38590.6236(25)	2590.52826(8)	-0.00001	440000	1D <sub>2</sub> <sup>o</sup>	5s	(3/2) <sup>3</sup> F <sub>2</sub> <sup>o</sup>	6.0e+07	C+	C94	L
2598.8126(6)	38467.613(9)	2598.81194(10)	0.0006	400000	3F <sub>2</sub> <sup>o</sup>	5s	(5/2) <sup>3</sup> F <sub>2</sub> <sup>o</sup>	4.2e+07	C+	K82	L
2600.26992(14)	38446.0554(20)	2600.26973(8)	0.00018	500000	3D <sub>5</sub> <sup>o</sup>	10s	(3/2) <sup>3</sup> F <sub>2</sub> <sup>o</sup>	1.01e+08	C+	C94	X
2604.523(21)	38383.24(3)	2604.5089(11)	0.0164	870	(1D) <sup>3</sup> P <sup>o</sup> -3F <sub>3</sub> <sup>o</sup>	10s	(5/2) <sup>3</sup> F <sub>2</sub> <sup>o</sup>		R1c		
2606.5804(14)	38352.984(21)	2606.5819(5)	-0.0015	1700	(5/2) <sup>3</sup> F <sub>2</sub> <sup>o</sup>	7f	(5/2) <sup>3</sup> F <sub>2</sub> <sup>o</sup>		R1c		
2606.8761(8)	38348.634(12)	2606.8759(4)	0.0001	3400	(5/2) <sup>3</sup> F <sub>2</sub> <sup>o</sup>	7f	(5/2) <sup>3</sup> F <sub>2</sub> <sup>o</sup>		R1c		
2606.9973(10)	38346.850(15)	2606.9973(4)	0.0001	2500	(5/2) <sup>3</sup> F <sub>2</sub> <sup>o</sup>	7f	(5/2) <sup>3</sup> F <sub>2</sub> <sup>o</sup>		R1c		
2607.041	38346.21	2607.0410(4)	0.0000	4400	(5/2) <sup>3</sup> F <sub>2</sub> <sup>o</sup>	7f	(5/2) <sup>3</sup> F <sub>2</sub> <sup>o</sup>		R1c		
2609.9088(6)	38304.075(9)	2609.9094(3)	-0.0006	8400	(5/2) <sup>3</sup> F <sub>2</sub> <sup>o</sup>	7f	(5/2) <sup>3</sup> F <sub>2</sub> <sup>o</sup>		R1c		
2610.7937(14)	38291.094(21)	2610.7940(5)	-0.0003	1600	(5/2) <sup>3</sup> F <sub>2</sub> <sup>o</sup>	7f	(5/2) <sup>3</sup> F <sub>2</sub> <sup>o</sup>		R1c		

Table A1. Cont.

$\lambda_{\text{obs}}^a$ (Å)	$\epsilon_{\text{obs}}^b$ (cm <sup>-1</sup> )	$\lambda_{\text{titz}}^c$ (Å)	$\Delta\lambda_{\text{obs-titz}}^d$ (Å)	$I_{\text{obs}}^d$ (arb. u.)	Char <sup>e</sup>	Lower Level	Upper Level	A (s <sup>-1</sup> )	Ace <sup>f</sup>	Line Ref. #	TP Ref. #	Notes <sup>h</sup>
2611.2544(8)	38284.338(11)	2611.2546(4)	-0.0002	810	4d	(5/2) <sup>+</sup> [5/2] <sub>2</sub>	7f	(5/2) <sup>+</sup> [5/2] <sub>3</sub>		R1c		
2614.4127(7)	38238.052(11)	2614.4126(7)	0.0001	15000	s <sup>2</sup>	3F <sub>4</sub>	5p	(3P) <sup>+</sup> 3D <sub>4</sub>		R1c		
2619.2104(5)	38168.094(8)	2619.21044(15)	-0.0000	8000	1D <sub>2</sub>	1D <sub>2</sub>	3p	(3/2) <sup>+</sup> [3/2] <sub>2</sub>		R1c	K82cal	
2620.6656(5)	38146.862(7)	2620.66627(10)	-0.0007	56000	4p	3F <sub>2</sub> 5s	5p	(5/2) <sup>+</sup> [5/2] <sub>2</sub>	E	R1c		
2636.6187(6)	37916.065(8)	2636.61965(16)	-0.0010	2200	s <sup>2</sup>	1D <sub>2</sub> 5p	5p	(3/2) <sup>+</sup> [3/2] <sub>1</sub>		R1c		
2648.6056(7)	37744.477(9)	2648.6059(4)	-0.0003	3000	s <sup>2</sup>	3F <sub>2</sub> 3p	3F <sub>2</sub>	(3P) <sup>+</sup> 3D <sub>3</sub>		R1c		
2655.9644(7)	37639.406(9)	2655.9642(5)	0.0002	840	s <sup>2</sup>	3F <sub>2</sub>	3p	(3P) <sup>+</sup> 3D <sub>3</sub>		R1c		
2666.2906(5)	37494.194(8)	2666.29047(11)	0.0001	230000	4p	1F <sub>2</sub> 5s	5p	(5/2) <sup>+</sup> [5/2] <sub>2</sub>	C+	R1c	K82	
2667.4229(13)	37478.224(21)	2667.4230(4)	-0.0021	990	5s	(3/2) <sup>+</sup> [3/2] <sub>1</sub> 7p	5p	(5/2) <sup>+</sup> [5/2] <sub>1</sub>		R1c		
2676.0606(6)	37357.184(8)	2676.06654(15)	-0.0005	3100	s <sup>2</sup>	1D <sub>2</sub> 5p	5p	(3/2) <sup>+</sup> [5/2] <sub>2</sub>		R1c		
2681.4966(13)	37281.533(21)	2681.4957(7)	0.0008	2100	5s	(3/2) <sup>+</sup> [3/2] <sub>2</sub> 7p	5p	(5/2) <sup>+</sup> [5/2] <sub>2</sub>		R1c		
2682.7484(8)	37264.137(11)	2682.75015(9)	-0.0017	440	4p	3D <sub>1</sub> 5s	5s	(3/2) <sup>+</sup> [5/2] <sub>2</sub>	E	R1c	K82cal	
2689.2934(5)	37173.370(7)	2689.29332(11)	0.0000	410000	4p	1F <sub>2</sub> 5s	5s	(5/2) <sup>+</sup> [5/2] <sub>2</sub>	C+	R1c	C94	
2692.4978(15)	37129.213(21)	2692.4942(4)	0.0036	3200	4d	3D <sub>2</sub> 5s	6f	(3/2) <sup>+</sup> [9/2] <sub>4</sub>		R1c		
2700.96242(17)	37012.8599(24)	2700.96252(9)	-0.0011	520000	4p	3D <sub>2</sub> 5s	6f	(3/2) <sup>+</sup> [5/2] <sub>2</sub>	C+	F	C94	
2703.18424(13)	36982.4398(18)	2703.18448(8)	-0.00024	540000	4p	3D <sub>1</sub> 5s	5p	(3/2) <sup>+</sup> [3/2] <sub>1</sub>	C+	F	C94	
2704.5194(23)	36964.18(3)	2704.5157(16)	0.0037	11000	s <sup>2</sup>	3F <sub>1</sub>	3p	(3P) <sup>+</sup> 3P <sub>1</sub>		R1c		
2708.2695(8)	36913.003(11)	2708.2695(3)	-0.0000	7200	4d	(5/2) <sup>+</sup> [1/2] <sub>1</sub> 8p	6f	(5/2) <sup>+</sup> [3/2] <sub>1</sub>		R1c		
2709.7592(6)	36892.711(8)	2709.7597(3)	-0.0006	1600	4d	(5/2) <sup>+</sup> [1/2] <sub>1</sub> 6f	6f	(5/2) <sup>+</sup> [5/2] <sub>2</sub>		R1c		
2710.2454(16)	36886.093(21)	2710.2434(6)	0.0020	2700	s <sup>2</sup>	3F <sub>2</sub>	3p	(3P) <sup>+</sup> 3P <sub>2</sub>		R1c		
2710.6069(16)	36881.173(21)	2710.6071(7)	-0.0001	700	4d	(5/2) <sup>+</sup> [1/2] <sub>2</sub> 6f	6f	(3/2) <sup>+</sup> [3/2] <sub>1</sub>		R1c		
2711.5767(23)	36867.98(3)	2711.5711(13)	0.0057	350	s <sup>2</sup>	3F <sub>2</sub>	3p	(3P) <sup>+</sup> 3P <sub>3</sub>		R2mc		
2711.8649(6)	36864.066(6)	2711.8639(3)	0.0010	18000	4d	(5/2) <sup>+</sup> [1/2] <sub>1</sub> 6f	6f	(5/2) <sup>+</sup> [3/2] <sub>2</sub>		R1c		
2713.5078(5)	36841.748(7)	2713.50740(10)	0.0004	400000	4p	1D <sub>2</sub> 5s	5p	(5/2) <sup>+</sup> [5/2] <sub>2</sub>	C+	R1c	C94	
2715.4038(6)	36816.024(8)	2715.4039(6)	-0.0000	10000	4d	(5/2) <sup>+</sup> [1/2] <sub>1</sub> 6f	6f	(5/2) <sup>+</sup> [1/2] <sub>1</sub>		R1c		
2718.770(3)	36770.349(4)	2718.7770(14)	-0.0007	440000	4p	1P <sub>1</sub> 5s	5s	(3/2) <sup>+</sup> [3/2] <sub>2</sub>	C+	F	C94	
2721.674(2)	36731.179(3)	2721.67628(9)	0.0002	300000	4p	3D <sub>2</sub> 5s	5p	(3/2) <sup>+</sup> [3/2] <sub>1</sub>	C+	F	K82	
2727.6947(6)	36650.142(8)	2727.6948(5)	-0.0001	620	4d	(5/2) <sup>+</sup> [1/2] <sub>1</sub> 6f	6f	(5/2) <sup>+</sup> [1/2] <sub>1</sub>		R2mc		L
2728.204(7)	36643.30(10)	2728.2019(16)	0.002	310	s <sup>2</sup>	3F <sub>0</sub>	3p	(3P) <sup>+</sup> 3P <sub>1</sub>		R1c		
2731.9477(6)	36593.089(7)	2731.94820(16)	-0.0005	6300	s <sup>2</sup>	1D <sub>2</sub> 5p	5p	(3P) <sup>+</sup> 3D <sub>2</sub>		R1c		
2737.3415(6)	36520.989(7)	2737.34194(10)	-0.0005	48000	4p	1D <sub>2</sub> 5s	5p	(5/2) <sup>+</sup> [5/2] <sub>2</sub>		R1c		
2739.7662(6)	36488.669(8)	2739.76664(14)	-0.0004	86000	4p	1P <sub>1</sub> 5s	5s	(3/2) <sup>+</sup> [3/2] <sub>1</sub>	D	R1c	C94	
2745.2710(6)	36415.506(7)	2745.27056(10)	0.0005	140000	4p	3D <sub>3</sub> 5s	5p	(5/2) <sup>+</sup> [5/2] <sub>2</sub>	D	R1c	C94	
2757.3283(7)	36256.276(9)	2757.3290(4)	-0.0007	770	4d	2F <sub>5</sub> 3D <sub>0</sub> (4)	4d	(3/2) <sup>+</sup> [5/2] <sub>2</sub>	C+	R1c		
2759.6070(8)	36226.340(11)	2759.6065(7)	0.0005	760	4d	(3/2) <sup>+</sup> [1/2] <sub>1</sub> 6f	6f	(3/2) <sup>+</sup> [3/2] <sub>1</sub>		R1c		
2762.481(20)	36188.6(3)	2762.4581(4)	0.023	1000	4d	(3/2) <sup>+</sup> [5/2] <sub>2</sub> 7f	7f	(3/2) <sup>+</sup> [7/2] <sub>4</sub>		R1c		
2762.481(20)	36188.6(3)	2762.4072(5)	-0.026	1000	4d	(3/2) <sup>+</sup> [5/2] <sub>2</sub> 7f	7f	(5/2) <sup>+</sup> [5/2] <sub>3</sub>		R1c		
2769.6690(6)	36094.738(7)	2769.66832(9)	0.0002	310000	4p	3D <sub>3</sub> 5s	5s	(5/2) <sup>+</sup> [5/2] <sub>2</sub>	C+	R1c	C94	
2788.2614(47)	35854.067(9)	2788.2619(3)	-0.0005	5700	4d	(5/2) <sup>+</sup> [9/2] <sub>5</sub> 6f	6f	(5/2) <sup>+</sup> [9/2] <sub>5</sub>		R1c		
2789.2226(17)	35841.712(21)	2789.2218(12)	0.0009	210	5p	(5/2) <sup>+</sup> [7/2] <sub>3</sub> 10s	10s	(5/2) <sup>+</sup> [5/2] <sub>2</sub>		R1c		
2791.7945(6)	35808.695(8)	2791.7947(4)	-0.0002	54000	4d	(5/2) <sup>+</sup> [9/2] <sub>5</sub> 6f	6f	(5/2) <sup>+</sup> [11/2] <sub>6</sub>		R1c		
2792.224(11)	35803.19(14)	2792.2125(3)	0.012	420	4d	(5/2) <sup>+</sup> [9/2] <sub>5</sub> 6f	6f	(5/2) <sup>+</sup> [11/2] <sub>6</sub>		R1c		
2792.224(11)	35803.19(14)	2792.22312(4)	-0.007	420	4d	(5/2) <sup>+</sup> [7/2] <sub>3</sub> 6f	6f	(5/2) <sup>+</sup> [7/2] <sub>3</sub>		R1c		

Table A1. Cont.

$\lambda_{\text{obs}}^a$ (Å)	$\epsilon_{\text{obs}}^b$ (cm <sup>-1</sup> )	$\lambda_{\text{lit}}^c$ (Å)	$\Delta\lambda_{\text{obs-Ritz}}^d$ (Å)	$I_{\text{obs}}^e$ (arb. u.)	Char <sup>e</sup>	Lower Level	Upper Level	A (s <sup>-1</sup> )	Acc <sup>f</sup>	Line Ref. #	TP Ref. #	Notes <sup>h</sup>
2793.6079(7)	35785.452(9)	2793.691(3)	-0.0012	620	4d	(5/2) <sup>3</sup> [3/2] <sub>2</sub>	8p	(5/2) <sup>3</sup> [3/2] <sub>1</sub>		Rlc		
2795.2979(6)	35763.818(8)	2795.2980(3)	-0.0001	8000	4d	(5/2) <sup>3</sup> [3/2] <sub>2</sub>	6f	(5/2) <sup>3</sup> [5/2] <sub>3</sub>		Rlc		
2795.6571(7)	35759.223(9)	2795.6567(3)	0.0004	4600	4d	(5/2) <sup>3</sup> [9/2] <sub>4</sub>	6f	(5/2) <sup>3</sup> [9/2] <sub>4</sub>		Rlc		
2795.8729(11)	35756.463(14)	2795.8732(3)	-0.0003	610	4d	(5/2) <sup>3</sup> [9/2] <sub>4</sub>	6f	(3/2) <sup>3</sup> [7/2] <sub>1</sub>		Rlc		
2796.2625(7)	35751.482(9)	2796.2624(5)	0.0001	820	4d	(3/2) <sup>3</sup> [9/2] <sub>4</sub>	6f	(3/2) <sup>3</sup> [7/2] <sub>1</sub>		Rlc		
2797.2549(6)	35738.798(8)	2797.2557(3)	-0.0008	7500	4d	(5/2) <sup>3</sup> [3/2] <sub>1</sub>	6f	(5/2) <sup>3</sup> [5/2] <sub>2</sub>		Rlc		
2797.4336(6)	35736.516(8)	2797.4337(3)	-0.0001	8300	4d	(5/2) <sup>3</sup> [3/2] <sub>1</sub>	6f	(5/2) <sup>3</sup> [3/2] <sub>1</sub>		Rlc		
2797.5493(12)	35735.038(16)	2797.5494(5)	-0.0001	410	4d	(5/2) <sup>3</sup> [3/2] <sub>2</sub>	6f	(5/2) <sup>3</sup> [3/2] <sub>1</sub>		Rlc		
2798.8296(17)	35718.692(21)			200	5p	(5/2) <sup>3</sup> [7/2] <sub>4</sub>	10s	(5/2) <sup>3</sup> [5/2] <sub>3</sub>		Rlc		
2799.5280(6)	35709.781(8)	2799.5291(3)	-0.0010	35000	4d	(5/2) <sup>3</sup> [9/2] <sub>4</sub>	6f	(5/2) <sup>3</sup> [11/2] <sub>5</sub>		Rlc		
2799.6805(6)	35707.837(8)	2799.6812(4)	-0.0007	10000	4d	(3/2) <sup>3</sup> [7/2] <sub>1</sub>	6f	(3/2) <sup>3</sup> [9/2] <sub>4</sub>		Rlc		
2801.0500(6)	35690.379(8)	2801.05008(16)	-0.0001	1000	s <sup>2</sup>	<sup>1</sup> D <sub>2</sub>	5p	(5/2) <sup>3</sup> [5/2] <sub>3</sub>		Rlc		
2801.3182(24)	35686.96(3)	2801.3220(17)	-0.0038	400	4d	(3/2) <sup>3</sup> [3/2] <sub>1</sub>	sp	<sup>3</sup> D <sub>3</sub>		R2mc		
2803.2711(17)	35662.102(21)	2803.2706(6)	0.0005	390	4d	(5/2) <sup>3</sup> [3/2] <sub>1</sub>	6f	(5/2) <sup>3</sup> [11/2] <sub>5</sub>		Rlc		
2804.1888(17)	35650.432(21)	2804.1896(12)	-0.0008	200	5p	(5/2) <sup>3</sup> [5/2] <sub>2</sub>	10s	(5/2) <sup>3</sup> [5/2] <sub>2</sub>		Rlc		
2807.1550(8)	35612.763(10)	2807.1556(5)	-0.0006	770	4d	(3/2) <sup>3</sup> [7/2] <sub>1</sub>	6f	(3/2) <sup>3</sup> [7/2] <sub>1</sub>		Rlc		
2810.3655(17)	35572.082(21)	2810.3657(4)	-0.0002	190	4d	(3/2) <sup>3</sup> [7/2] <sub>1</sub>	6f	(3/2) <sup>3</sup> [9/2] <sub>4</sub>		Rlc		
2810.8038(6)	35566.536(7)	2810.8039(4)	-0.0001	14000	4d	(3/2) <sup>3</sup> [7/2] <sub>1</sub>	6f	(3/2) <sup>3</sup> [9/2] <sub>4</sub>		Rlc		
2813.6315(7)	35530.793(9)	2813.63100(16)	0.0005	2900	s <sup>2</sup>	<sup>1</sup> D <sub>2</sub>	5p	(5/2) <sup>3</sup> [3/2] <sub>1</sub>		Rlc		
2816.1978(9)	35498.417(11)	2816.1982(5)	-0.0004	3700	4d	(3/2) <sup>3</sup> [3/2] <sub>1</sub>	6f	(3/2) <sup>3</sup> [3/2] <sub>1</sub>		Rlc		
2817.0843(7)	35487.247(9)	2817.08465(18)	-0.0004	370	s <sup>2</sup>	<sup>1</sup> D <sub>2</sub>	5p	(5/2) <sup>3</sup> [5/2] <sub>2</sub>		Rlc		
2828.6968(7)	35341.570(9)	2828.6970(5)	-0.0002	3500	4d	(5/2) <sup>3</sup> [5/2] <sub>3</sub>	6f	(5/2) <sup>3</sup> [9/2] <sub>4</sub>		Rlc		
2828.9184(12)	35338.802(15)	2828.9187(3)	-0.0003	3500	4d	(5/2) <sup>3</sup> [5/2] <sub>3</sub>	6f	(5/2) <sup>3</sup> [9/2] <sub>4</sub>		Rlc		
2830.2314(8)	35322.408(10)	2830.2323(3)	-0.0008	6100	4d	(5/2) <sup>3</sup> [5/2] <sub>3</sub>	6f	(5/2) <sup>3</sup> [15/2] <sub>3</sub>		Rlc		
2832.4214(7)	35295.099(9)	2832.4217(3)	-0.0004	3400	4d	(5/2) <sup>3</sup> [5/2] <sub>3</sub>	6f	(5/2) <sup>3</sup> [15/2] <sub>3</sub>		Rlc		
2833.053(2)	35287.23(3)	2833.0250(5)	0.028	170	sp	( <sup>3</sup> F) <sup>3</sup> - <sup>3</sup> D <sub>3</sub>	7d	(5/2) <sup>3</sup> [5/2] <sub>2</sub>		Rlc		X
2836.9699(17)	35263.372(21)	2834.9704(5)	-0.0005	510	4d	(3/2) <sup>3</sup> [3/2] <sub>1</sub>	6f	(3/2) <sup>3</sup> [3/2] <sub>1</sub>		Rlc		
2836.2898(8)	35246.962(10)	2836.2911(5)	-0.0013	4600	4d	(3/2) <sup>3</sup> [3/2] <sub>1</sub>	6f	(3/2) <sup>3</sup> [5/2] <sub>2</sub>		Rlc		
2836.6971(17)	35241.902(21)	2836.7011(6)	-0.0230	840	sp	( <sup>3</sup> F) <sup>3</sup> sp <sup>2</sup>	9s	(5/2) <sup>3</sup> [5/2] <sub>2</sub>		Rlc		X
2837.3682(6)	35233.566(7)	2837.36814(10)	0.0001	150000	4p	<sup>3</sup> D <sub>1</sub>	5s	(5/2) <sup>3</sup> [5/2] <sub>2</sub>		Rlc		C94
2840.4918(16)	35194.823(8)	2840.49162(17)	0.0002	5800	s <sup>2</sup>	<sup>3</sup> D <sub>1</sub>	5s	(5/2) <sup>3</sup> [5/2] <sub>2</sub>	2.3e+07	C+		
2846.8683(7)	35115.996(8)	2846.8693(5)	-0.0009	4300	4d	(5/2) <sup>3</sup> [7/2] <sub>1</sub>	6f	(5/2) <sup>3</sup> [3/2] <sub>1</sub>		Rlc		
2848.4999(6)	35095.883(8)	2848.5005(3)	-0.0005	11000	4d	(5/2) <sup>3</sup> [7/2] <sub>1</sub>	6f	(5/2) <sup>3</sup> [9/2] <sub>4</sub>		Rlc		
2848.7252(6)	35093.108(8)	2848.7252(3)	-0.0000	9100	4d	(5/2) <sup>3</sup> [7/2] <sub>1</sub>	6f	(5/2) <sup>3</sup> [9/2] <sub>4</sub>		Rlc		
2849.9526(10)	35077.995(12)	2849.9500(3)	0.0026	160	4d	(5/2) <sup>3</sup> [7/2] <sub>1</sub>	6f	(5/2) <sup>3</sup> [5/2] <sub>2</sub>		Rlc		
2851.8949(8)	35054.106(10)	2851.8944(5)	0.0005	4700	4d	(5/2) <sup>3</sup> [5/2] <sub>2</sub>	6f	(5/2) <sup>3</sup> [7/2] <sub>1</sub>		Rlc		
2852.0764(7)	35051.875(8)	2852.0764(3)	0.0001	12000	4d	(5/2) <sup>3</sup> [7/2] <sub>1</sub>	6f	(5/2) <sup>3</sup> [9/2] <sub>4</sub>		Rlc		
2852.1785(11)	35050.621(13)	2852.1793(3)	-0.0008	6300	4d	(5/2) <sup>3</sup> [7/2] <sub>1</sub>	6f	(5/2) <sup>3</sup> [9/2] <sub>4</sub>		Rlc		
2852.4042(6)	35047.847(8)	2852.4046(3)	-0.0004	3900	4d	(5/2) <sup>3</sup> [7/2] <sub>1</sub>	6f	(5/2) <sup>3</sup> [7/2] <sub>1</sub>		Rlc		
2853.7401(7)	35031.439(8)	2853.7401(3)	0.0002	630	4d	(5/2) <sup>3</sup> [7/2] <sub>1</sub>	6f	(5/2) <sup>3</sup> [5/2] <sub>2</sub>		Rlc		
2854.9858(7)	35016.157(9)	2854.9860(3)	-0.0002	2100	4d	(5/2) <sup>3</sup> [5/2] <sub>2</sub>	6f	(5/2) <sup>3</sup> [5/2] <sub>2</sub>		Rlc		

Table A1. Cont.

$\lambda_{\text{obs}}^a$ (Å)	$\epsilon_{\text{obs}}^b$ (cm <sup>-1</sup> )	$\lambda_{\text{rtz}}^c$ (Å)	$\Delta\lambda_{\text{obs-rtz}}^d$ (Å)	$I_{\text{obs}}^d$ (arb. u.)	Char <sup>e</sup>	Lower Level	Upper Level	A (s <sup>-1</sup> )	Ace <sup>f</sup>	Line Ref. #	TP Ref. #	Notes <sup>h</sup>
2855.0930(17)	35014.842(21)	2855.0785(5)	-0.0007	310	m	4d	(3/2) <sup>3</sup> [7/2] <sub>3</sub>	6f		Rtc		
2855.3206(7)	33012.052(8)	2855.0937(3)	-0.0009	4700		4d	(5/2) <sup>3</sup> [5/2] <sub>3</sub>	6f		Rtc		
2855.3206(7)	33012.052(8)	2855.3215(5)	0.0010	310		4d	(3/2) <sup>3</sup> [7/2] <sub>4</sub>	6f		Rtc		
2857.4418(17)	33011.138(8)	2856.2100(4)	-0.0007	310		4d	(5/2) <sup>3</sup> [7/2] <sub>1,5</sub>	6f		Rtc		
2857.4484(6)	34986.062(21)	2857.4425(5)	-0.0003	19000		4p	(5/2) <sup>3</sup> [3/2] <sub>1</sub>	5s	E	K82cal		
2859.0051(7)	34966.932(8)	2857.7480(8)	-0.0003	5300		4d	(3/2) <sup>3</sup> [5/2] <sub>2</sub>	6f		Rtc		
2859.9192(7)	34959.192(7)	2859.9187(4)	0.0005	2300		4d	(3/2) <sup>3</sup> [5/2] <sub>1,2</sub>	6f		Rtc		
2860.2493(9)	34951.723(11)	2860.2486(19)	-0.0006	1100		s <sup>2</sup>	(3/2) <sup>3</sup> [3/2] <sub>2</sub>	5p		Rtc		
2862.3233(7)	34826.399(8)	2862.3233(5)	-0.0000	3000		4d	(3/2) <sup>3</sup> [5/2] <sub>1,3</sub>	6f		Rtc		
2866.7012(5)	34878.302(21)	2866.2702(5)	0.0004	740		4d	(3/2) <sup>3</sup> [5/2] <sub>1,3</sub>	6f		Rtc		
2868.7914(8)	34847.656(9)	2868.7906(4)	0.0008	440		4d	(5/2) <sup>3</sup> [3/2] <sub>1,5</sub>	8p		Rtc		
2872.9461(7)	34797.263(8)	2872.9460(5)	0.0001	570		4d	(5/2) <sup>3</sup> [1/2] <sub>0</sub>	6f		Rtc		
2875.3341(7)	34768.345(9)	2875.3346(5)	-0.0005	580		5p	(5/2) <sup>3</sup> [3/2] <sub>2</sub>	8d		Rtc		
2877.6996(6)	34739.786(7)	2877.6989(16)	0.0007	170000		4p	(3/2) <sup>3</sup> [3/2] <sub>2</sub>	8d	C+	C94		
2880.7003(7)	34703.600(9)	2880.6994(17)	-0.0009	2000		s <sup>2</sup>	(5/2) <sup>3</sup> [3/2] <sub>2</sub>	1D <sub>2</sub> 5p		Rtc		
2881.0216(8)	34699.730(9)	2881.0219(20)	-0.0003	1000		s <sup>2</sup>	(3/2) <sup>3</sup> [3/2] <sub>1</sub>	5p		Rtc		
2883.1886(18)	34673.651(21)	2883.1886(18)	0.0000	2800		5p	(5/2) <sup>3</sup> [1/2] <sub>1</sub>	8d		Rtc		
2884.1954(6)	34661.548(8)	2884.1959(8)	-0.0006	41000		4p	(3/2) <sup>3</sup> [5/2] <sub>1,3</sub>	5s	C+	C94		
2884.7560(7)	34654.812(9)	2884.7557(16)	0.0003	280	s <sup>2</sup> 3p	s <sup>2</sup>	(3/2) <sup>3</sup> [5/2] <sub>1,3</sub>	5p		Rtc		
2897.2206(7)	34505.726(8)	2897.21944(17)	0.0011	1200		s <sup>2</sup>	(3/2) <sup>3</sup> [1/2] <sub>0</sub>	5p		Rtc		
2907.9162(8)	34378.816(10)	2907.9158(5)	0.0004	1300		s <sup>2</sup>	(3/2) <sup>3</sup> [3/2] <sub>1,1</sub>	5p		Rtc		
2908.863(3)	34367.65(3)	2908.8746(4)	-0.012	130		sp	(3/2) <sup>3</sup> [3/2] <sub>1,1</sub>	5p		Rtc		
2912.4526(18)	34325.271(21)	2912.4526(18)	0.0000	250		5p	(3/2) <sup>3</sup> [3/2] <sub>1,1</sub>	8d		Rtc		
2917.7762(9)	34262.646(11)	2917.77629(20)	-0.0001	620		s <sup>2</sup>	(5/2) <sup>3</sup> [3/2] <sub>1,1</sub>	8d		Rtc		
2923.2569(18)	34198.411(21)	2923.2586(8)	-0.0017	240		5p	(3/2) <sup>3</sup> [1/2] <sub>1</sub>	8d		Rtc		
2926.2499(7)	34163.434(8)	2926.2501(4)	-0.0002	240		5p	(5/2) <sup>3</sup> [7/2] <sub>3</sub>	8d		Rtc		
2927.2539(7)	34151.717(9)	2927.2535(5)	0.0003	2900		5p	(5/2) <sup>3</sup> [2/2] <sub>2</sub>	9s		Rtc		
2928.1916(18)	34140.781(21)	2928.18542(19)	0.0062	240		s <sup>2</sup>	(5/2) <sup>3</sup> [7/2] <sub>3</sub>	8d		Rtc		
2931.789(3)	34098.89(4)	2931.7851(4)	0.004	230		sp	(3/2) <sup>3</sup> [1/2] <sub>0</sub>	5p		Rtc		
2932.2253(7)	34093.818(9)	2932.2254(6)	-0.0002	1200		5p	(3/2) <sup>3</sup> [3/2] <sub>1,1</sub>	8s		Rtc		
2933.565(6)	34078.25(7)	2933.5614(6)	0.003	230		sp	(3/2) <sup>3</sup> [7/2] <sub>4</sub>	8d		Rtc		
2936.9533(7)	34038.912(8)	2936.9555(7)	-0.0002	2900		5p	(3/2) <sup>3</sup> [7/2] <sub>4</sub>	8d		Rtc		
2939.7041(9)	34007.084(10)	2939.7036(8)	0.0005	1100		5p	(5/2) <sup>3</sup> [5/2] <sub>1,2</sub>	8d		Rtc		
2941.2137(18)	33989.631(21)	2941.2085(6)	0.0052	1100		sp	(3/2) <sup>3</sup> [3/2] <sub>1,1</sub>	7d		Rtc		
2942.623(5)	33973.35(6)	2942.6237(18)	-0.001	230		5p	(5/2) <sup>3</sup> [3/2] <sub>1,1</sub>	8d		Rtc		
2945.370(8)	33941.66(9)	2945.3640(3)	0.007	6100		s <sup>2</sup>	(3/2) <sup>3</sup> [1/2] <sub>1</sub>	5p		S86c		
2947.3037(11)	33919.401(12)	2947.3037(11)	0.0000	670		5p	(5/2) <sup>3</sup> [3/2] <sub>1,1</sub>	8d		Rtc		
2949.3463(18)	33895.911(21)	2949.3453(10)	0.0010	550		5p	(3/2) <sup>3</sup> [5/2] <sub>1,3</sub>	9d		Rtc		
2957.3211(19)	33804.511(21)	2957.3242(6)	-0.0032	1100		5p	(5/2) <sup>3</sup> [5/2] <sub>1,3</sub>	8d		Rtc		
2959.3285(19)	33781.581(21)	2959.3276(5)	0.0009	740		5p	(5/2) <sup>3</sup> [5/2] <sub>1,3</sub>	8d		Rtc		X

Table A1. Cont.

$\lambda_{\text{obs}}^a$ (Å)	$\sigma_{\text{obs}}^b$ (cm <sup>-1</sup> )	$\lambda_{\text{Ritz}}^c$ (Å)	$\Delta\lambda_{\text{obs-Ritz}}^d$ (Å)	$I_{\text{obs}}^d$ (arb. u.)	Char <sup>e</sup>	Lower Level	Upper Level	A (s <sup>-1</sup> )	Acc <sup>f</sup>	Line Ref. <sup>g</sup>	TP Ref. <sup>h</sup>	Notes <sup>b</sup>
2968.744(3)	33674.44(3)	2968.7445(4)	-0.000	200	4d	(3/2) <sup>+</sup> 7/2 <sub>1/2</sub>	6f	(5/2) <sup>+</sup> 9/2 <sub>1/2</sub>	Ric			
2973.6495(7)	33618.897(8)	2973.64712(23)	0.0024	1300	s <sup>2</sup>	3P <sub>1</sub>	5p	(3/2) <sup>+</sup> 11/2 <sub>1/2</sub>	Ric			
2975.271(5)	33600.57(6)	2975.2681(3)	0.003	300	sp	( <sup>3</sup> F) <sup>+</sup> 3F <sup>+</sup> <sub>3</sub>	7d	(5/2) <sup>+</sup> 7/2 <sub>1/2</sub>	Ric			
2975.6294(8)	33596.629(9)	2975.6286(7)	0.0008	1200	5p	(5/2) <sup>+</sup> 7/2 <sub>1/2</sub>	9s	(5/2) <sup>+</sup> 5/2 <sub>1/2</sub>	Ric			
2977.0081(19)	33580.971(21)	2977.0087(16)	-0.0006	1100	5p	(3/2) <sup>+</sup> 5/2 <sub>1/2</sub>	9s	(3/2) <sup>+</sup> 3/2 <sub>1/2</sub>	Ric			
2981.7867(12)	33527.156(14)	2981.7860(4)	0.0007	1000	5s	(5/2) <sup>+</sup> 15/2 <sub>1/2</sub>	6p	(3/2) <sup>+</sup> 13/2 <sub>1/2</sub>	Ric			
2981.945(3)	33525.38(3)	2981.9449(5)	-0.000	1400	sp	( <sup>3</sup> F) <sup>+</sup> 3F <sup>+</sup> <sub>3</sub>	7d	(5/2) <sup>+</sup> 9/2 <sub>1/2</sub>	Ric			
2983.7677(10)	33504.898(11)	2983.7658(3)	0.0018	1100	4d	(5/2) <sup>+</sup> 11/2 <sub>1/2</sub>	5f	(3/2) <sup>+</sup> 9/2 <sub>1/2</sub>	Ric			
2986.3345(8)	33476.101(9)	2986.3327(3)	0.0017	5700	4d	(5/2) <sup>+</sup> 11/2 <sub>1/2</sub>	5f	(3/2) <sup>+</sup> 9/2 <sub>1/2</sub>	Ric			
2987.2351(7)	33466.009(8)	2987.2353(5)	-0.0002	1400	5p	(5/2) <sup>+</sup> 7/2 <sub>1/2</sub>	4	(5/2) <sup>+</sup> 5/2 <sub>1/2</sub>	Ric			
2992.6695(19)	33405.241(21)	2992.6698(7)	-0.0003	460	5p	(5/2) <sup>+</sup> 5/2 <sub>1/2</sub>	8d	(5/2) <sup>+</sup> 5/2 <sub>1/2</sub>	Ric			
2993.024(5)	33401.28(5)	2993.024(5)	-0.0008	920	5s	(5/2) <sup>+</sup> 15/2 <sub>1/2</sub>	6p	(3/2) <sup>+</sup> 13/2 <sub>1/2</sub>	Ric			
2993.2667(8)	33398.576(9)	2993.2675(4)	-0.0008	920	5s	(5/2) <sup>+</sup> 15/2 <sub>1/2</sub>	6p	(3/2) <sup>+</sup> 13/2 <sub>1/2</sub>	Ric			
2996.8412(19)	33358.741(21)	2996.8382(6)	0.0030	720	sp	( <sup>3</sup> F) <sup>+</sup> 3F <sup>+</sup> <sub>3</sub>	8d	(5/2) <sup>+</sup> 7/2 <sub>1/2</sub>	Ric			
2998.893(5)	33335.92(6)	2998.8956(6)	-0.003	180	sp	( <sup>3</sup> F) <sup>+</sup> 3F <sup>+</sup> <sub>3</sub>	8d	(5/2) <sup>+</sup> 7/2 <sub>1/2</sub>	Ric			
2999.8710(19)	33325.051(21)	2999.8701(8)	0.0009	530	5p	(3/2) <sup>+</sup> 5/2 <sub>1/2</sub>	9s	(3/2) <sup>+</sup> 3/2 <sub>1/2</sub>	Ric			
3004.058(5)	33278.60(6)	3004.0535(5)	0.003	260	4d	(3/2) <sup>+</sup> 13/2 <sub>1/2</sub>	6f	(5/2) <sup>+</sup> 7/2 <sub>1/2</sub>	Ric			
3010.5921(19)	33206.381(21)	3010.5910(4)	0.0011	1700	5s	(5/2) <sup>+</sup> 15/2 <sub>1/2</sub>	6p	(3/2) <sup>+</sup> 13/2 <sub>1/2</sub>	Ric			
3012.2768(19)	33187.811(21)	3012.2786(5)	-0.0018	170	5s	(5/2) <sup>+</sup> 15/2 <sub>1/2</sub>	6p	(3/2) <sup>+</sup> 13/2 <sub>1/2</sub>	Ric			
3013.2896(11)	33176.656(12)	3013.2888(5)	0.0008	170	5p	(5/2) <sup>+</sup> 5/2 <sub>1/2</sub>	9s	(5/2) <sup>+</sup> 5/2 <sub>1/2</sub>	Ric			
3014.5445(8)	33162.846(9)	3014.54413(18)	0.0004	6200	s <sup>2</sup>	3P <sub>2</sub>	sp	( <sup>3</sup> F) <sup>+</sup> 3F <sup>+</sup> <sub>3</sub>	Ric			
3024.1816(19)	33057.171(21)	3024.1822(19)	-0.0005	230	5s	(3/2) <sup>+</sup> 13/2 <sub>1/2</sub>	sp	( <sup>3</sup> G) <sup>+</sup> 3G <sup>+</sup> <sub>3</sub>	R2nc			
3027.388(6)	33022.16(6)	3027.39453(17)	-0.006	76	sp	(3/2) <sup>+</sup> 13/2 <sub>1/2</sub>	sp	( <sup>3</sup> G) <sup>+</sup> 3G <sup>+</sup> <sub>3</sub>	Ric			
3037.6082(20)	32911.061(21)	3037.6081(19)	0.0001	140	sp	( <sup>3</sup> F) <sup>+</sup> 3F <sup>+</sup> <sub>3</sub>	8d	(5/2) <sup>+</sup> 7/2 <sub>1/2</sub>	Ric			
3037.801(3)	32908.97(3)	3037.8031(6)	-0.002	710	5s	(5/2) <sup>+</sup> 15/2 <sub>1/2</sub>	6p	(3/2) <sup>+</sup> 13/2 <sub>1/2</sub>	Ric			
3041.678(8)	32867.019(9)	3041.6786(5)	0.0002	4500	5s	(5/2) <sup>+</sup> 15/2 <sub>1/2</sub>	6p	(3/2) <sup>+</sup> 13/2 <sub>1/2</sub>	Ric			
3042.8556(8)	32854.308(9)	3042.8551(5)	0.0005	340	5p	(5/2) <sup>+</sup> 5/2 <sub>1/2</sub>	7d	(3/2) <sup>+</sup> 3/2 <sub>1/2</sub>	Ric			
3049.2831(10)	32785.058(11)	3049.2836(8)	-0.0005	130	5p	(3/2) <sup>+</sup> 5/2 <sub>1/2</sub>	9s	(3/2) <sup>+</sup> 3/2 <sub>1/2</sub>	Ric			
3051.9472(20)	32756.441(21)	3051.9539(7)	-0.0038	130	sp	( <sup>3</sup> F) <sup>+</sup> 3F <sup>+</sup> <sub>3</sub>	sp	( <sup>3</sup> F) <sup>+</sup> 3F <sup>+</sup> <sub>3</sub>	Ric			
3052.1596(20)	32754.161(21)	3052.15798(24)	0.0016	130	s <sup>2</sup>	1D <sub>2</sub>	sp	( <sup>3</sup> F) <sup>+</sup> 3F <sup>+</sup> <sub>3</sub>	Ric			
3053.5737(15)	32738.993(16)	3053.5735(6)	0.0003	190	5p	(5/2) <sup>+</sup> 5/2 <sub>1/2</sub>	7d	(3/2) <sup>+</sup> 3/2 <sub>1/2</sub>	Ric			
3055.6134(8)	32717.140(9)	3055.61251(18)	0.0009	500	5p	3P <sub>2</sub>	5p	(5/2) <sup>+</sup> 5/2 <sub>1/2</sub>	Ric			
3056.8491(9)	32703.914(9)	3056.8484(3)	0.0007	310	sp	( <sup>3</sup> F) <sup>+</sup> 3F <sup>+</sup> <sub>3</sub>	7d	(5/2) <sup>+</sup> 7/2 <sub>1/2</sub>	Ric			
3059.8637(9)	32671.695(10)	3059.8632(5)	0.0005	420	5s	(5/2) <sup>+</sup> 15/2 <sub>1/2</sub>	7d	(3/2) <sup>+</sup> 11/2 <sub>1/2</sub>	Ric			
3062.2814(8)	32645.902(8)	3062.2814(5)	-0.0000	590	5s	(5/2) <sup>+</sup> 15/2 <sub>1/2</sub>	7d	(3/2) <sup>+</sup> 11/2 <sub>1/2</sub>	Ric			
3066.6018(12)	32599.9100(13)	3066.5985(3)	0.0033	400	sp	( <sup>3</sup> F) <sup>+</sup> 3F <sup>+</sup> <sub>3</sub>	8s	(5/2) <sup>+</sup> 5/2 <sub>1/2</sub>	Ric			
3080.3202(20)	32454.730(21)	3080.3284(6)	-0.0082	400	sp	( <sup>3</sup> F) <sup>+</sup> 3F <sup>+</sup> <sub>3</sub>	7s	(3/2) <sup>+</sup> 3/2 <sub>1/2</sub>	Ric			
3081.4480(14)	32442.832(15)	3081.4527(3)	-0.0046	150	4d	(5/2) <sup>+</sup> 9/2 <sub>1/2</sub>	5f	(3/2) <sup>+</sup> 7/2 <sub>1/2</sub>	Ric			
3082.935(3)	32427.21(3)	3082.9398(3)	0.0000	97	4d	(5/2) <sup>+</sup> 13/2 <sub>1/2</sub>	5f	(3/2) <sup>+</sup> 13/2 <sub>1/2</sub>	Ric			
3083.3677(8)	32422.654(8)	3083.3669(3)	0.0009	970	4d	(5/2) <sup>+</sup> 13/2 <sub>1/2</sub>	5f	(3/2) <sup>+</sup> 13/2 <sub>1/2</sub>	Ric			
3085.4342(20)	32400.940(21)	3085.4421(3)	-0.0079	95	4d	(5/2) <sup>+</sup> 13/2 <sub>1/2</sub>	5f	(3/2) <sup>+</sup> 13/2 <sub>1/2</sub>	Ric			
3085.5818(20)	32399.390(21)	3085.6280(3)	-0.0462	94	4d	(5/2) <sup>+</sup> 9/2 <sub>1/2</sub>	5f	(3/2) <sup>+</sup> 9/2 <sub>1/2</sub>	Ric			X

Table A1. Cont.

$\lambda_{\text{obs}}^a$ (Å)	$\sigma_{\text{obs}}^b$ (cm <sup>-1</sup> )	$\lambda_{\text{Ritz}}^c$ (Å)	$\Delta\lambda_{\text{obs-Ritz}}^d$ (Å)	$I_{\text{obs}}^d$ (arb. u.)	Char <sup>e</sup>	Lower Level	Upper Level	A (s <sup>-1</sup> )	Acc <sup>f</sup>	Line Ref. <sup>g</sup>	TP Ref. <sup>h</sup>	Notes <sup>b</sup>
3088.7489(7)	32366.170(8)	3088.74858(24)	0.0003	550		4d	(5/2) <sup>3</sup> P <sup>o</sup> 2/1 <sub>1</sub>	5f		Ric		
3097.8651(13)	32270.9291(3)	3097.86615(23)	-0.0011	410	s <sup>2</sup>	sp	(3P) <sup>3</sup> P <sup>o</sup> 3D <sup>o</sup> 3	6d		Ric		
3110.4745(10)	32140.1121(0)	3110.4732(4)	0.0013	70	sp	4d	(5/2) <sup>3</sup> P <sup>o</sup> 2/1 <sub>1</sub>	5f		Ric		
3121.3959(8)	32027.662(8)	3121.3961(5)	-0.0002	150	4d	4d	(5/2) <sup>3</sup> P <sup>o</sup> 2/1 <sub>1</sub>	7p		Ric		
3121.6428(7)	32025.129(7)	3121.6415(3)	0.0013	240	4d	4d	(5/2) <sup>3</sup> P <sup>o</sup> 2/1 <sub>1</sub>	5f		Ric		
3121.8708(21)	32022.790(21)	3121.8736(3)	-0.0027	90	4d	4d	(5/2) <sup>3</sup> P <sup>o</sup> 2/1 <sub>1</sub>	5f		Ric		
3124.7229(8)	31993.563(8)	3124.7222(3)	0.0006	440	s <sup>2</sup>	sp	(3P) <sup>3</sup> P <sup>o</sup> 1D <sup>o</sup> 2	5p		Ric		
3139.7885(9)	31840.054(9)	3139.7857(6)	0.0028	610	bl	sp	(3P) <sup>3</sup> P <sup>o</sup> 1D <sup>o</sup> 2	7d		Ric		
3140.4073(9)	31833.781(9)	3140.4064(6)	0.0008	280	sp	4d	(3P) <sup>3</sup> P <sup>o</sup> 1D <sup>o</sup> 2	7d		Ric		
3146.0122(8)	31777.068(8)	3146.0119(3)	0.0003	430	4d	4d	(3P) <sup>3</sup> P <sup>o</sup> 1D <sup>o</sup> 2	5f		Ric		
3148.7869(8)	31749.067(8)	3148.7856(5)	0.0013	170	sp	4d	(3P) <sup>3</sup> P <sup>o</sup> 1D <sup>o</sup> 2	7d		Ric		
3149.6815(21)	31740.650(21)	3149.6769(3)	0.0046	260	bl	4d	(5/2) <sup>3</sup> P <sup>o</sup> 2/1 <sub>1</sub>	5f		Ric		
3150.2634(9)	31734.187(9)	3150.2636(3)	-0.0002	88	4d	4d	(5/2) <sup>3</sup> P <sup>o</sup> 2/1 <sub>1</sub>	5f		Ric		
3150.540(8)	31731.40(8)	3150.4999(3)	0.040	4600	?	4d	(5/2) <sup>3</sup> P <sup>o</sup> 2/1 <sub>1</sub>	5f		S86c		X
3150.642(9)	31730.372(9)	3150.64124(19)	0.0010	3000	s <sup>2</sup>	sp	(3P) <sup>3</sup> P <sup>o</sup> 2/1 <sub>1</sub>	5f		Ric		
3151.0505(7)	31726.261(7)	3151.0506(3)	-0.0001	10000	5s	4d	(5/2) <sup>3</sup> P <sup>o</sup> 2/1 <sub>1</sub>	6p		Ric		
3152.9000(7)	31707.651(7)	3152.8992(3)	0.0008	3500	4d	4d	(5/2) <sup>3</sup> P <sup>o</sup> 2/1 <sub>1</sub>	5f		Ric		
3154.0935(8)	31695.653(8)	3154.0934(4)	0.0001	550	5s	4d	(5/2) <sup>3</sup> P <sup>o</sup> 2/1 <sub>1</sub>	5f		Ric		
3155.3760(9)	31682.771(9)	3155.3765(5)	-0.0005	380	4d	4d	(5/2) <sup>3</sup> P <sup>o</sup> 2/1 <sub>1</sub>	sp		Ric		
3155.8323(21)	31678.190(21)	3155.8290(3)	0.0033	190	4d	4d	(5/2) <sup>3</sup> P <sup>o</sup> 2/1 <sub>1</sub>	7p		Ric		
3156.2820(7)	31673.677(7)	3156.2817(3)	0.0003	1900	4d	4d	(5/2) <sup>3</sup> P <sup>o</sup> 2/1 <sub>1</sub>	5f		Ric		
3157.8901(8)	31657.548(8)	3157.88927(23)	0.0007	1900	4d	4d	(5/2) <sup>3</sup> P <sup>o</sup> 2/1 <sub>1</sub>	5f		Ric		
3158.6729(8)	31649.703(8)	3158.6734(5)	-0.0005	3700	5s	4d	(5/2) <sup>3</sup> P <sup>o</sup> 2/1 <sub>1</sub>	6p		Ric		
3162.0434(7)	31615.968(7)	3162.0438(4)	-0.0004	2300	5p	4d	(5/2) <sup>3</sup> P <sup>o</sup> 2/1 <sub>1</sub>	7d		Ric		
3163.6838(11)	31599.575(11)	3163.6842(4)	-0.0003	610	4d	4d	(5/2) <sup>3</sup> P <sup>o</sup> 2/1 <sub>1</sub>	5f		Ric		
3166.5879(7)	31570.596(7)	3166.5873(5)	0.0006	3500	5p	4d	(5/2) <sup>3</sup> P <sup>o</sup> 2/1 <sub>1</sub>	7d		Ric		
3170.6936(8)	31529.717(8)	3170.6935(5)	0.0001	540	5p	4d	(3/2) <sup>3</sup> P <sup>o</sup> 1/2 <sup>o</sup>	5f		Ric		
3173.6092(9)	31500.732(9)	3173.6088(3)	0.0004	330	sp	4d	(3P) <sup>3</sup> P <sup>o</sup> 3D <sup>o</sup> 2	6d		Ric		
3174.9680(12)	31482.271(11)	3174.96642(22)	0.0016	840	s <sup>2</sup>	4d	(3P) <sup>3</sup> P <sup>o</sup> 3D <sup>o</sup> 2	6d		Ric		
3176.3094(16)	31473.974(16)	3176.3108(3)	-0.0014	230	4d	4d	(5/2) <sup>3</sup> P <sup>o</sup> 2/1 <sub>1</sub>	5f		Ric		
3177.7392(8)	31459.813(8)	3177.7397(7)	-0.0005	1700	5p	4d	(5/2) <sup>3</sup> P <sup>o</sup> 2/1 <sub>1</sub>	7d		Ric		
3177.9692(8)	31457.536(8)	3177.9705(5)	-0.0012	2300	5s	4d	(5/2) <sup>3</sup> P <sup>o</sup> 2/1 <sub>1</sub>	7d		Ric		
3179.3173(17)	31444.198(17)	3179.3163(4)	0.0010	2700	5p	4d	(5/2) <sup>3</sup> P <sup>o</sup> 2/1 <sub>1</sub>	6p		Ric		
3179.7846(8)	31439.577(8)	3179.7842(4)	0.0004	6400	4d	4d	(5/2) <sup>3</sup> P <sup>o</sup> 2/1 <sub>1</sub>	5f		Ric		
3180.2932(9)	31434.550(9)	3180.2935(6)	-0.0003	4700	5p	4d	(3/2) <sup>3</sup> P <sup>o</sup> 1/2 <sup>o</sup>	5f		Ric		
3180.7930(21)	31429.610(21)	3180.7922(4)	0.0008	230	sp	4d	(3P) <sup>3</sup> P <sup>o</sup> 3D <sup>o</sup> 2	6d		Ric		
3182.171(7)	31415.994(7)	3182.1718(3)	-0.0002	11000	4d	4d	(5/2) <sup>3</sup> P <sup>o</sup> 2/1 <sub>1</sub>	5f		Ric		
3184.6224(12)	31391.819(12)	3184.6233(5)	-0.0010	480	4d	4d	(5/2) <sup>3</sup> P <sup>o</sup> 2/1 <sub>1</sub>	7p		Ric		
3184.8404(8)	31389.670(8)	3184.8409(3)	-0.0005	15000	4d	4d	(5/2) <sup>3</sup> P <sup>o</sup> 2/1 <sub>1</sub>	5f		Ric		
3185.7249(7)	31380.955(7)	3185.7256(4)	-0.0006	4000	5s	4d	(5/2) <sup>3</sup> P <sup>o</sup> 2/1 <sub>1</sub>	6p		Ric		
3186.0148(7)	31378.100(7)	3186.0153(4)	-0.0005	6400	4d	4d	(5/2) <sup>3</sup> P <sup>o</sup> 2/1 <sub>1</sub>	5f		Ric		

Table A1. Cont.

$\lambda_{\text{obs}}^a$ (Å)	$\sigma_{\text{obs}}^b$ (cm <sup>-1</sup> )	$\lambda_{\text{Ritz}}^c$ (Å)	$\Delta\lambda_{\text{obs-Ritz}}^d$ (Å)	$I_{\text{obs}}^d$ (arb. u.)	Char <sup>e</sup>	Lower Level	Upper Level	A (s <sup>-1</sup> )	Acc <sup>f</sup>	Line Ref. <sup>g</sup>	TP Ref. <sup>h</sup>	Notes <sup>b</sup>
3186.341(8)	31374.887(8)	3186.3415(4)	-0.0004	3000	5s	(5/2) <sup>-1</sup> 5/2 <sub>2</sub>	sp	( <sup>3</sup> F) <sup>o</sup> 3 <sup>-2</sup>		Ric		
3187.0427(13)	31367.980(13)	3187.0386(5)	0.0041	1200	5s	(3/2) <sup>-1</sup> 3/2 <sub>2</sub>	6p	(3/2) <sup>-1</sup> 3/2 <sub>1</sub>		Ric		
3188.723(22)	31351.450(21)	3188.7259(4)	-0.0028	490	sp	( <sup>3</sup> F) <sup>o</sup> 3 <sup>-2</sup> D <sup>o</sup>	6d	(3/2) <sup>-1</sup> 7/2 <sub>2</sub>		Ric		
3192.3023(22)	31316.301(21)	3192.3011(3)	0.0012	250	5p	(5/2) <sup>-1</sup> 5/2 <sub>2</sub>	7d	( <sup>1</sup> G) <sup>o</sup> 3 <sup>-2</sup> F <sup>o</sup> <sub>3</sub>		Ric		
3198.1052(10)	31259.480(9)	3198.1052(8)	-0.0001	1000	5p	(5/2) <sup>-1</sup> 3/2 <sub>1</sub>	7d	(5/2) <sup>-1</sup> 11/2 <sub>2</sub>		Ric		
3204.5231(16)	31196.877(16)	3204.5259(6)	-0.0029	640	sp	( <sup>3</sup> F) <sup>o</sup> 3 <sup>-2</sup> C <sup>o</sup> <sub>4</sub>	6d	(5/2) <sup>-1</sup> 7/2 <sub>2</sub>		Ric		
3206.6848(13)	31175.847(12)	3206.6848(5)	-0.0000	1800	5s	(3/2) <sup>-1</sup> 3/2 <sub>2</sub>	6p	(3/2) <sup>-1</sup> 3/2 <sub>1</sub>		Ric		
3208.3026(16)	31160.127(16)	3208.3076(6)	-0.0050	1500	5s	(3/2) <sup>-1</sup> 3/2 <sub>1</sub>	6p	(3/2) <sup>-1</sup> 5/2 <sub>1</sub>		Ric		
3216.9896(14)	31075.987(14)	3216.9895(6)	0.0001	520	5p	(3/2) <sup>-1</sup> 5/2 <sub>1</sub>	7d	(3/2) <sup>-1</sup> 5/2 <sub>2</sub>		Ric		
3217.3123(22)	31072.870(21)	3217.3104(4)	0.0019	650	5p	(5/2) <sup>-1</sup> 7/2 <sub>1</sub>	7d	(3/2) <sup>-1</sup> 5/2 <sub>2</sub>		Ric		
3217.6410(17)	31069.696(17)	3217.6411(6)	-0.0001	390	7d	(3/2) <sup>-1</sup> 5/2 <sub>1</sub>	7d	(3/2) <sup>-1</sup> 5/2 <sub>2</sub>		Ric		
3218.2644(15)	31063.6384(15)	3218.2633(6)	0.0011	260	5p	( <sup>3</sup> F) <sup>o</sup> 3 <sup>-2</sup> C <sup>o</sup> <sub>4</sub>	6d	(3/2) <sup>-1</sup> 5/2 <sub>2</sub>		Ric		
3218.6278(16)	31061.170(16)	3218.6244(5)	0.0034	390	5p	(5/2) <sup>-1</sup> 7/2 <sub>1</sub>	7d	(5/2) <sup>-1</sup> 7/2 <sub>2</sub>		Ric		
3218.7642(8)	31058.854(8)	3218.7651(4)	-0.0009	2000	5p	(5/2) <sup>-1</sup> 7/2 <sub>1</sub>	7d	(5/2) <sup>-1</sup> 7/2 <sub>2</sub>		Ric		
3221.9702(22)	31027.950(21)	3221.9718(6)	-0.0016	260	5p	(3/2) <sup>-1</sup> 5/2 <sub>1</sub>	7d	(3/2) <sup>-1</sup> 3/2 <sub>2</sub>		Ric		
3225.3388(8)	30995.545(8)	3225.3392(3)	-0.0004	2100	5s	(5/2) <sup>-1</sup> 5/2 <sub>2</sub>	sp	( <sup>1</sup> G) <sup>o</sup> 3 <sup>-2</sup> F <sup>o</sup> <sub>3</sub>		Ric		
3226.3290(16)	30986.033(16)	3226.3301(12)	-0.0011	260	5p	(3/2) <sup>-1</sup> 7/2 <sub>1</sub>	7d	(3/2) <sup>-1</sup> 11/2 <sub>2</sub>		Ric		
3226.4395(9)	30984.972(9)	3226.4380(5)	0.0015	640	5p	(3/2) <sup>-1</sup> 5/2 <sub>1</sub>	7d	(3/2) <sup>-1</sup> 7/2 <sub>2</sub>		Ric		
3226.5812(10)	30983.611(9)	3226.5808(5)	0.0004	5200	5p	(5/2) <sup>-1</sup> 7/2 <sub>1</sub>	7d	(5/2) <sup>-1</sup> 7/2 <sub>2</sub>		Ric		
3229.5526(8)	30955.105(8)	3229.5524(5)	0.0003	970	5p	(5/2) <sup>-1</sup> 7/2 <sub>1</sub>	7d	(5/2) <sup>-1</sup> 7/2 <sub>2</sub>		Ric		
3233.3754(13)	30918.508(12)	3233.3722(4)	0.0032	1000	5p	(5/2) <sup>-1</sup> 7/2 <sub>1</sub>	7d	(5/2) <sup>-1</sup> 5/2 <sub>2</sub>		Ric		
3234.6710(14)	30906.125(13)	3234.6691(6)	0.0019	510	5p	(3/2) <sup>-1</sup> 11/2 <sub>1</sub>	7d	(3/2) <sup>-1</sup> 3/2 <sub>2</sub>		Ric		
3234.7336(10)	30905.527(9)	3234.7341(5)	-0.0005	950	5p	(5/2) <sup>-1</sup> 5/2 <sub>1</sub>	6p	(5/2) <sup>-1</sup> 5/2 <sub>2</sub>		Ric		
3237.1430(16)	30882.525(15)	3237.1420(7)	0.0009	250	7s	( <sup>1</sup> F) <sup>o</sup> 3 <sup>-2</sup> F <sup>o</sup> <sub>3</sub>	7s	(5/2) <sup>-1</sup> 5/2 <sub>2</sub>		Ric		
3237.2417(11)	30881.583(11)	3237.2413(5)	0.0004	1100	5p	(5/2) <sup>-1</sup> 5/2 <sub>1</sub>	7d	(5/2) <sup>-1</sup> 5/2 <sub>2</sub>		Ric		
3237.5736(12)	30878.417(11)	3237.5732(5)	-0.0016	1300	5s	(3/2) <sup>-1</sup> 3/2 <sub>2</sub>	6p	(3/2) <sup>-1</sup> 5/2 <sub>1</sub>		Ric		
3238.7160(10)	30867.526(10)	3238.7141(4)	0.0019	1900	5p	(5/2) <sup>-1</sup> 5/2 <sub>1</sub>	7d	(5/2) <sup>-1</sup> 5/2 <sub>2</sub>		Ric		
3238.8232(8)	30866.504(7)	3238.8228(6)	0.0005	5500	5p	(5/2) <sup>-1</sup> 7/2 <sub>1</sub>	7d	(5/2) <sup>-1</sup> 7/2 <sub>2</sub>		Ric		
3239.6499(13)	30858.628(12)	3239.6507(5)	-0.0008	250	sp	( <sup>1</sup> F) <sup>o</sup> 3 <sup>-2</sup> 1 <sup>o</sup> <sub>2</sub>	8s	(3/2) <sup>-1</sup> 3/2 <sub>2</sub>		Ric		
3241.8139(12)	30838.030(11)	3241.8139(5)	-0.0000	860	5p	(5/2) <sup>-1</sup> 5/2 <sub>1</sub>	7d	(5/2) <sup>-1</sup> 5/2 <sub>2</sub>		Ric		
3242.425(10)	30832.21(10)	3242.4129(5)	0.012	250	5p	(5/2) <sup>-1</sup> 5/2 <sub>1</sub>	7d	(5/2) <sup>-1</sup> 5/2 <sub>2</sub>		Ric		
3242.425(10)	30832.21(10)	3242.4252(7)	-0.004	250	5p	( <sup>1</sup> F) <sup>o</sup> 3 <sup>-2</sup> 1 <sup>o</sup> <sub>2</sub>	8s	(5/2) <sup>-1</sup> 3/2 <sub>2</sub>		Ric		
3245.9402(14)	30798.829(13)	3245.9405(6)	-0.0003	1500	5p	(3/2) <sup>-1</sup> 5/2 <sub>1</sub>	7d	(3/2) <sup>-1</sup> 5/2 <sub>2</sub>		Ric		
3246.7898(22)	30790.770(21)	3246.7839(7)	0.0059	620	5p	(3/2) <sup>-1</sup> 11/2 <sub>1</sub>	7d	(3/2) <sup>-1</sup> 11/2 <sub>2</sub>		Ric		
3250.4652(8)	30755.955(8)	3250.4650(4)	0.0003	11000	4d	(5/2) <sup>-1</sup> 3/2 <sub>1</sub>	5f	(5/2) <sup>-1</sup> 3/2 <sub>2</sub>		Ric		
3250.5739(13)	30750.089(12)	3250.5733(7)	0.0006	1200	5p	(5/2) <sup>-1</sup> 3/2 <sub>1</sub>	7d	(5/2) <sup>-1</sup> 3/2 <sub>2</sub>		Ric		
3251.726(3)	30743.7(3)	3251.7262(6)	0.00	240	sp	( <sup>1</sup> F) <sup>o</sup> 3 <sup>-2</sup> C <sup>o</sup> <sub>4</sub>	5g	(5/2) <sup>-1</sup> 11/2 <sub>2</sub>		Ric		
3251.726(3)	30743.7(3)	3251.7913(5)	-0.03	240	5p	(5/2) <sup>-1</sup> 3/2 <sub>1</sub>	7d	(5/2) <sup>-1</sup> 3/2 <sub>2</sub>		Ric		
3252.7830(8)	30734.041(8)	3252.7838(6)	-0.0008	2400	5p	(3/2) <sup>-1</sup> 5/2 <sub>1</sub>	7d	(3/2) <sup>-1</sup> 5/2 <sub>2</sub>		Ric		
3253.1078(12)	30730.972(11)	3253.1070(5)	0.0008	1200	5s	(5/2) <sup>-1</sup> 5/2 <sub>2</sub>	6p	(5/2) <sup>-1</sup> 5/2 <sub>1</sub>		Ric		
3257.1234(16)	30693.086(15)	3257.1222(5)	0.0012	240	5s	(5/2) <sup>-1</sup> 5/2 <sub>2</sub>	6p	(5/2) <sup>-1</sup> 5/2 <sub>1</sub>		Ric		

Table A1. Cont.

$\lambda_{obs}^a$ (Å)	$\sigma_{obs}^b$ (cm <sup>-1</sup> )	$\lambda_{Ritz}^c$ (Å)	$\Delta\lambda_{obs-Ritz}^d$ (Å)	$I_{obs}^d$ (arb. u.)	Char <sup>e</sup>	Lower Level	Upper Level	A (s <sup>-1</sup> )	Acc <sup>f</sup>	Line Ref. <sup>g</sup>	TP Ref. <sup>h</sup>	Notes <sup>b</sup>
3260.0249(11)	30665.770(11)	3260.0253(5)	-0.0004	2400	5p	(5/2) <sup>+</sup> 5/2 <sup>+</sup> 3	7d	(5/2) <sup>+</sup> 7/2 <sup>+</sup> 1		Ric		
3260.1697(17)	30664.4081(16)	3260.1697(4)	0.0000	240	5p	(5/2) <sup>+</sup> 5/2 <sup>+</sup> 3	7d	(5/2) <sup>+</sup> 7/2 <sup>+</sup> 1		Ric		
3261.6449(8)	30650.520(8)	3261.6474(3)	-0.0007	1800	5p	(5/2) <sup>+</sup> 5/2 <sup>+</sup> 3	8s	(5/2) <sup>+</sup> 5/2 <sup>+</sup> 1		Ric		
3263.5546(14)	30632.604(13)	3263.5530(7)	0.0017	350	5p	(5/2) <sup>+</sup> 5/2 <sup>+</sup> 3	7d	(5/2) <sup>+</sup> 5/2 <sup>+</sup> 1		Ric		
3263.9177(11)	30629.197(10)	3263.9177(4)	0.0000	3500	5p	(5/2) <sup>+</sup> 5/2 <sup>+</sup> 3	7d	(5/2) <sup>+</sup> 5/2 <sup>+</sup> 1		Ric		
3265.3948(14)	30615.342(13)	3265.3933(6)	0.0015	1100	5s	(3/2) <sup>+</sup> 3/2 <sup>+</sup> 2	6p	(3/2) <sup>+</sup> 1/2 <sup>+</sup> 1		Ric		
3268.0990(16)	30590.010(15)	3268.0988(7)	0.0002	230	5p	(3/2) <sup>+</sup> 1/2 <sup>+</sup> 0	8s	(3/2) <sup>+</sup> 3/2 <sup>+</sup> 1		Ric		
3268.1895(14)	30589.163(13)	3268.1879(5)	0.0016	450	5p	(5/2) <sup>+</sup> 5/2 <sup>+</sup> 3	7d	(5/2) <sup>+</sup> 3/2 <sup>+</sup> 1		Ric		
3268.7591(13)	30583.833(12)	3268.7589(5)	0.0002	1400	5p	(5/2) <sup>+</sup> 5/2 <sup>+</sup> 3	7d	(5/2) <sup>+</sup> 3/2 <sup>+</sup> 1		Ric		
3270.1104(16)	30571.195(15)	3270.1113(4)	-0.0008	1000	5p	( <sup>4</sup> F) <sup>+</sup> 3D <sup>+</sup> 1	6d	(3/2) <sup>+</sup> 5/2 <sup>+</sup> 1		Ric		
3275.9027(13)	30517.143(12)	3275.9057(6)	-0.0031	2200	5p	(3/2) <sup>+</sup> 3/2 <sup>+</sup> 1	7d	(3/2) <sup>+</sup> 5/2 <sup>+</sup> 1		Ric		
3278.9653(23)	30485.640(21)	3278.9636(4)	0.0017	210	5p	( <sup>4</sup> F) <sup>+</sup> 3D <sup>+</sup> 1	6d	(3/2) <sup>+</sup> 3/2 <sup>+</sup> 1		Ric		
3281.0757(23)	30469.030(21)	3281.0724(6)	0.0034	210	5p	(3/2) <sup>+</sup> 3/2 <sup>+</sup> 1	7d	(5/2) <sup>+</sup> 3/2 <sup>+</sup> 1		Ric		
3281.6964(8)	30463.268(8)	3281.6929(23)	0.0001	9700	4d	(5/2) <sup>+</sup> 3/2 <sup>+</sup> 1	5f	(5/2) <sup>+</sup> 3/2 <sup>+</sup> 1		Ric		
3282.0106(6)	30460.351(8)	3282.01019(24)	0.0005	1100	4d	(5/2) <sup>+</sup> 3/2 <sup>+</sup> 1	5f	(5/2) <sup>+</sup> 3/2 <sup>+</sup> 1		Ric		
3282.6022(11)	30454.862(10)	3282.6016(3)	0.0006	530	4d	(5/2) <sup>+</sup> 3/2 <sup>+</sup> 1	5f	(5/2) <sup>+</sup> 3/2 <sup>+</sup> 1		Ric		
3283.0958(16)	30450.283(15)	3283.0969(4)	-0.0011	210	4d	( <sup>4</sup> F) <sup>+</sup> 3D <sup>+</sup> 1	6d	(3/2) <sup>+</sup> 3/2 <sup>+</sup> 1		Ric		
3283.2431(13)	30448.917(12)	3283.2433(7)	-0.0002	940	5p	(3/2) <sup>+</sup> 3/2 <sup>+</sup> 1	7d	(3/2) <sup>+</sup> 3/2 <sup>+</sup> 1		Ric		
3290.4174(4)	30382.530(4)	3290.41683(16)	0.0005	38000	4d	(5/2) <sup>+</sup> 3/2 <sup>+</sup> 1	5f	(5/2) <sup>+</sup> 3/2 <sup>+</sup> 1		F,Re		
3291.0597(8)	30376.600(7)	3291.0592(22)	0.0002	1100	4d	(5/2) <sup>+</sup> 3/2 <sup>+</sup> 1	5f	(5/2) <sup>+</sup> 3/2 <sup>+</sup> 1	5.9e+07	D+		TW
3291.8090(16)	30369.686(15)	3291.8073(3)	0.0017	2000	4d	(5/2) <sup>+</sup> 3/2 <sup>+</sup> 1	5f	(5/2) <sup>+</sup> 3/2 <sup>+</sup> 1		Ric		
3292.1232(8)	30366.788(7)	3292.1232(3)	-0.0000	7700	4d	(5/2) <sup>+</sup> 3/2 <sup>+</sup> 1	5f	(5/2) <sup>+</sup> 3/2 <sup>+</sup> 1		Ric		
3292.7189(10)	30361.294(9)	3292.7183(3)	0.0007	3500	4d	(5/2) <sup>+</sup> 3/2 <sup>+</sup> 1	5f	(5/2) <sup>+</sup> 3/2 <sup>+</sup> 1		Ric		
3292.9965(13)	30358.735(12)	3292.9984(3)	-0.0020	1500	4d	(5/2) <sup>+</sup> 3/2 <sup>+</sup> 1	5f	(5/2) <sup>+</sup> 3/2 <sup>+</sup> 1		Ric		
3293.3326(9)	30355.637(8)	3293.3327(4)	-0.0001	2800	4d	(5/2) <sup>+</sup> 3/2 <sup>+</sup> 1	5f	(5/2) <sup>+</sup> 3/2 <sup>+</sup> 1		Ric		
3294.3354(8)	30346.397(7)	3294.3355(3)	-0.0002	3800	4d	(5/2) <sup>+</sup> 3/2 <sup>+</sup> 1	5f	(5/2) <sup>+</sup> 3/2 <sup>+</sup> 1		Ric		
3295.1019(8)	30339.338(7)	3295.1018(3)	0.0001	11000	4d	(5/2) <sup>+</sup> 3/2 <sup>+</sup> 1	5f	(5/2) <sup>+</sup> 3/2 <sup>+</sup> 1		Ric		
3297.1983(8)	30320.048(7)	3297.1986(3)	-0.0003	9300	4d	(5/2) <sup>+</sup> 3/2 <sup>+</sup> 1	5f	(5/2) <sup>+</sup> 3/2 <sup>+</sup> 1		Ric		
3297.3461(12)	30318.689(11)	3297.3492(4)	-0.0031	1200	4d	(5/2) <sup>+</sup> 3/2 <sup>+</sup> 1	5f	(5/2) <sup>+</sup> 3/2 <sup>+</sup> 1		Ric		
3297.5688(10)	30316.642(9)	3297.5686(4)	0.0002	1400	4d	(5/2) <sup>+</sup> 3/2 <sup>+</sup> 1	5f	(5/2) <sup>+</sup> 3/2 <sup>+</sup> 1		Ric		
3300.2124(14)	30292.358(13)	3300.2124(4)	0.0000	380	5p	( <sup>4</sup> F) <sup>+</sup> 3C <sup>+</sup> 3	7s	(3/2) <sup>+</sup> 3/2 <sup>+</sup> 1		Ric		
3300.4370(9)	30290.296(9)	3300.4373(4)	-0.0003	6100	4d	(5/2) <sup>+</sup> 3/2 <sup>+</sup> 1	5f	(5/2) <sup>+</sup> 3/2 <sup>+</sup> 1		Ric		
3300.6409(9)	30288.425(9)	3300.6406(3)	0.0003	9100	4d	(5/2) <sup>+</sup> 3/2 <sup>+</sup> 1	5f	(5/2) <sup>+</sup> 3/2 <sup>+</sup> 1		Ric		
3300.8815(9)	30286.218(8)	3300.8808(3)	0.0006	13000	4d	(5/2) <sup>+</sup> 3/2 <sup>+</sup> 1	5f	(5/2) <sup>+</sup> 3/2 <sup>+</sup> 1		Ric		
3301.2286(7)	30283.034(6)	3301.22844(23)	0.0001	25000	4d	(5/2) <sup>+</sup> 3/2 <sup>+</sup> 1	5f	(5/2) <sup>+</sup> 3/2 <sup>+</sup> 1	5.4e+07	D+		TW
3303.1817(12)	30265.128(11)	3303.1836(6)	-0.0018	1400	5p	(3/2) <sup>+</sup> 3/2 <sup>+</sup> 1	7d	(5/2) <sup>+</sup> 3/2 <sup>+</sup> 1	5.6e+07	D+		TW
3303.5132(21)	30262.091(20)	3303.5122(4)	0.0010	5800	4d	(5/2) <sup>+</sup> 3/2 <sup>+</sup> 1	5f	(5/2) <sup>+</sup> 3/2 <sup>+</sup> 1		Ric		
3303.8698(10)	30258.825(9)	3303.8706(6)	-0.0015	5800	4d	(5/2) <sup>+</sup> 3/2 <sup>+</sup> 1	5f	(5/2) <sup>+</sup> 3/2 <sup>+</sup> 1		Ric		
3306.3890(15)	30235.771(14)	3306.3913(4)	-0.0023	180	4d	(5/2) <sup>+</sup> 3/2 <sup>+</sup> 1	7d	(5/2) <sup>+</sup> 3/2 <sup>+</sup> 1		Ric		
3307.6576(11)	30224.175(10)	3307.6570(4)	0.0006	1200	4d	(5/2) <sup>+</sup> 3/2 <sup>+</sup> 1	5f	(5/2) <sup>+</sup> 3/2 <sup>+</sup> 1		Ric		



Table A1. Cont.

$\lambda_{\text{obs}}^a$ (Å)	$\sigma_{\text{obs}}^b$ (cm <sup>-1</sup> )	$\lambda_{\text{Ritz}}^c$ (Å)	$\Delta\lambda_{\text{obs-Ritz}}^d$ (Å)	$I_{\text{obs}}^d$ (arb. u.)	Char <sup>e</sup>	Lower Level	Upper Level	$A$ (s <sup>-1</sup> )	Acc <sup>f</sup>	Line Ref. <sup>g</sup>	TP Ref. <sup>h</sup>	Notes <sup>b</sup>
3307.872(13)	30222.210(12)	3307.8664(4)	0.0063	1200	4d	(3/2) <sup>2</sup> 7/2 <sub>1/2</sub> 5f	(3/2) <sup>2</sup> 7/2 <sub>1/2</sub> <sup>4</sup>			Ric		X
3308.1052(14)	30220.086(13)	3308.1074(5)	-0.0023	1100	sp	( <sup>4</sup> F) <sup>o</sup> -1F <sup>o</sup> <sub>3</sub> 7d	(5/2) <sup>2</sup> 7/2 <sub>1/2</sub>			Ric		
3308.2526(15)	30218.739(14)	3308.2561(4)	-0.0035	180	sp	( <sup>4</sup> F) <sup>o</sup> -1F <sup>o</sup> <sub>3</sub> 7d	(5/2) <sup>2</sup> 7/2 <sub>1/2</sub>			Ric		
3308.4337(13)	30217.085(12)	3308.4367(6)	-0.0029	360	5p	(3/2) <sup>2</sup> 3/2 <sub>1/2</sub> <sup>2</sup> 6d	(5/2) <sup>2</sup> 3/2 <sub>1/2</sub>			Ric		
3310.338(3)	30199.70(3)	3310.3389(4)	-0.001	89	sp	( <sup>3</sup> F) <sup>o</sup> 3p <sup>o</sup> 3D <sup>o</sup> <sub>3</sub> 6d	(5/2) <sup>2</sup> 5/2 <sub>1/2</sub>			Ric		
3312.0278(13)	30184.296(11)	3312.0276(4)	0.0001	550	sp	( <sup>3</sup> F) <sup>o</sup> 3p <sup>o</sup> 3D <sup>o</sup> <sub>3</sub> 6d	(5/2) <sup>2</sup> 7/2 <sub>1/2</sub>			Ric		
3312.115(14)	30183.500(13)	3312.1155(5)	-0.0004	970	sp	( <sup>3</sup> F) <sup>o</sup> 3p <sup>o</sup> 1F <sup>o</sup> <sub>3</sub> 7d	(5/2) <sup>2</sup> 5/2 <sub>1/2</sub>			Ric		
3312.677(11)	30178.380(9)	3312.6783(3)	-0.0012	610	4d	(3/2) <sup>2</sup> 7/2 <sub>1/2</sub> 5f	(3/2) <sup>2</sup> 5/2 <sub>1/2</sub> <sup>3</sup>			Ric		
3315.7440(8)	30150.467(7)	3315.7431(3)	0.0010	1300	4d	(3/2) <sup>2</sup> 7/2 <sub>1/2</sub> 5f	(3/2) <sup>2</sup> 9/2 <sub>1/2</sub> <sup>5</sup>			Ric		
3316.2756(8)	30145.634(7)	3316.2752(3)	0.0004	16000	4d	(3/2) <sup>2</sup> 7/2 <sub>1/2</sub> 5f	(3/2) <sup>2</sup> 9/2 <sub>1/2</sub> <sup>5</sup>			Ric		
3316.5116(16)	30143.489(15)	3316.5129(6)	-0.0013	260	sp	( <sup>4</sup> F) <sup>o</sup> -1F <sup>o</sup> <sub>3</sub> 7d	(5/2) <sup>2</sup> 9/2 <sub>1/2</sub>		D+	Ric	TW	
3317.1383(8)	30137.794(7)	3317.1386(4)	-0.0003	5500	4d	(3/2) <sup>2</sup> 3/2 <sub>1/2</sub> 7s	(5/2) <sup>2</sup> 5/2 <sub>1/2</sub> <sup>2</sup>			Ric		
3318.3147(23)	30122.110(21)	3318.3232(12)	-0.0085	84	sp	( <sup>3</sup> F) <sup>o</sup> 3p <sup>o</sup> 5F <sup>o</sup> <sub>4</sub> 6d	(5/2) <sup>2</sup> 5/2 <sub>1/2</sub>			Ric		
3319.028(13)	30120.706(10)	3319.0216(5)	-0.0013	840	sp	( <sup>3</sup> F) <sup>o</sup> 3p <sup>o</sup> 3D <sup>o</sup> <sub>3</sub> 6d	(5/2) <sup>2</sup> 5/2 <sub>1/2</sub>			Ric		
3321.1137(23)	30110.720(21)	3321.1144(7)	0.0023	500	5p	(3/2) <sup>2</sup> 5/2 <sub>1/2</sub> <sup>2</sup> 7d	(3/2) <sup>2</sup> 3/2 <sub>1/2</sub> <sup>1</sup>			Ric		
3321.3526(8)	30097.743(8)	3321.3528(3)	-0.0002	1400	5p	(5/2) <sup>2</sup> 7/2 <sub>1/2</sub> <sup>3</sup> 8s	(5/2) <sup>2</sup> 5/2 <sub>1/2</sub>			Ric		
3321.7168(14)	30096.255(13)	3321.7165(8)	0.0003	410	4d	(3/2) <sup>2</sup> 7/2 <sub>1/2</sub> 7p	(5/2) <sup>2</sup> 3/2 <sub>1/2</sub> <sup>2</sup>			Ric		
3322.6363(10)	30087.927(9)	3322.6351(4)	0.0012	2000	4d	(3/2) <sup>2</sup> 3/2 <sub>1/2</sub> 5f	(5/2) <sup>2</sup> 3/2 <sub>1/2</sub> <sup>1</sup>			Ric		
3324.8295(9)	30068.080(8)	3324.8292(7)	0.0003	1200	5p	(3/2) <sup>2</sup> 5/2 <sub>1/2</sub> <sup>2</sup> 8s	(5/2) <sup>2</sup> 3/2 <sub>1/2</sub>			Ric		
3325.0235(13)	30066.326(11)	3325.0210(4)	0.0025	720	5s	(5/2) <sup>2</sup> 5/2 <sub>1/2</sub> 6p	(5/2) <sup>2</sup> 7/2 <sub>1/2</sub> <sup>3</sup>			Ric		
3325.8187(14)	30059.137(12)	3325.8184(4)	0.0003	3000	4d	(3/2) <sup>2</sup> 3/2 <sub>1/2</sub> 5f	(5/2) <sup>2</sup> 3/2 <sub>1/2</sub> <sup>2</sup>			Ric		
3325.9326(13)	30058.189(11)	3325.9322(4)	-0.0006	400	5p	(5/2) <sup>2</sup> 7/2 <sub>1/2</sub> <sup>3</sup> 8s	(5/2) <sup>2</sup> 5/2 <sub>1/2</sub>			Ric		
3327.9129(16)	30040.222(15)	3327.9161(5)	-0.0032	160	sp	( <sup>4</sup> F) <sup>o</sup> 3p <sup>o</sup> 1F <sup>o</sup> <sub>3</sub> 6d	(3/2) <sup>2</sup> 3/2 <sub>1/2</sub>			Ric		
3335.4075(14)	29972.725(12)	3335.4064(5)	0.0011	520	5p	(3/2) <sup>2</sup> 1/2 <sup>1</sup> 8s	(5/2) <sup>2</sup> 3/2 <sub>1/2</sub>			Ric		
3337.5951(12)	29953.080(11)	3337.5942(4)	0.0008	3000	5p	(5/2) <sup>2</sup> 7/2 <sup>4</sup> 8s	(5/2) <sup>2</sup> 5/2 <sub>1/2</sub>			Ric		
3338.0369(14)	29949.116(12)	3338.03567(24)	0.0012	9200	4d	(5/2) <sup>2</sup> 5/2 <sub>1/2</sub> 5f	(5/2) <sup>2</sup> 9/2 <sub>1/2</sub> <sup>4</sup>			Ric		
3338.6475(9)	29943.638(8)	3338.6475(3)	0.0001	9900	4d	(5/2) <sup>2</sup> 5/2 <sub>1/2</sub> 5f	(5/2) <sup>2</sup> 9/2 <sub>1/2</sub> <sup>4</sup>			Ric		
3338.9364(9)	29941.051(8)	3338.9355(3)	0.0005	3600	4d	(5/2) <sup>2</sup> 5/2 <sub>1/2</sub> 5f	(5/2) <sup>2</sup> 7/2 <sub>1/2</sub> <sup>3</sup>		D+	Ric	TW	
3339.0850(9)	29939.715(8)	3339.0845(4)	0.0006	3600	4d	(5/2) <sup>2</sup> 5/2 <sub>1/2</sub> 5f	(5/2) <sup>2</sup> 7/2 <sub>1/2</sub> <sup>3</sup>			Ric		
3340.8308(13)	29924.070(11)	3340.8312(8)	-0.0003	720	5s	(3/2) <sup>2</sup> 3/2 <sub>1/2</sub> 5f	(3/2) <sup>2</sup> 7/2 <sub>1/2</sub> <sup>3</sup>			Ric		
3341.7610(13)	29915.741(11)	3341.7607(5)	0.0003	570	sp	( <sup>4</sup> F) <sup>o</sup> 3p <sup>o</sup> 3F <sup>o</sup> <sub>4</sub> 6d	(5/2) <sup>2</sup> 3/2 <sub>1/2</sub>			Ric		
3342.8004(10)	29906.439(9)	3342.8003(4)	0.0001	710	5p	(5/2) <sup>2</sup> 5/2 <sub>1/2</sub> 8s	(5/2) <sup>2</sup> 5/2 <sub>1/2</sub>			Ric		
3342.9641(9)	29904.975(8)	3342.9640(3)	0.0001	1800	4d	(5/2) <sup>2</sup> 5/2 <sub>1/2</sub> 5f	(5/2) <sup>2</sup> 5/2 <sub>1/2</sub> <sup>2</sup>			Ric		
3343.2140(24)	29902.740(21)	3343.2134(4)	0.0006	280	4d	(3/2) <sup>2</sup> 3/2 <sub>1/2</sub> 5f	(3/2) <sup>2</sup> 5/2 <sub>1/2</sub> <sup>2</sup>			Ric		
3343.7214(4)	29898.202(18)	3343.7215(3)	-0.0001	14000	4d	(3/2) <sup>2</sup> 3/2 <sub>1/2</sub> 5f	(3/2) <sup>2</sup> 5/2 <sub>1/2</sub> <sup>2</sup>			Ric		
3343.7515(9)	29897.933(8)	3343.7531(3)	-0.0016	14000	4d	(5/2) <sup>2</sup> 5/2 <sub>1/2</sub> 8s	(5/2) <sup>2</sup> 5/2 <sub>1/2</sub> <sup>3</sup>			Ric		
3347.2268(18)	29866.892(16)	3347.2279(4)	-0.0011	140	5p	(5/2) <sup>2</sup> 5/2 <sub>1/2</sub> <sup>2</sup> 8s	(5/2) <sup>2</sup> 5/2 <sub>1/2</sub>			Ric		
3347.6754(9)	29862.890(8)	3347.6762(3)	-0.0008	550	5p	(3/2) <sup>2</sup> 3/2 <sub>1/2</sub> 5f	(3/2) <sup>2</sup> 3/2 <sub>1/2</sub> <sup>1</sup>			Ric		
3348.7955(14)	29852.902(12)	3348.7967(4)	-0.0012	540	4d	( <sup>4</sup> F) <sup>o</sup> 3p <sup>o</sup> 3G <sup>o</sup> <sub>3</sub> 6d	(5/2) <sup>2</sup> 3/2 <sub>1/2</sub>			Ric		
3348.8824(14)	29852.127(12)	3348.8809(5)	0.0015	620	sp	( <sup>4</sup> F) <sup>o</sup> 3p <sup>o</sup> 3G <sup>o</sup> <sub>3</sub> 6d	(5/2) <sup>2</sup> 3/2 <sub>1/2</sub> <sup>2</sup>			Ric		
3349.4567(8)	29847.009(7)	3349.4569(3)	-0.0002	4200	4d	(5/2) <sup>2</sup> 5/2 <sub>1/2</sub> 5f	(5/2) <sup>2</sup> 3/2 <sub>1/2</sub> <sup>2</sup>			Ric		
3352.0324(12)	29824.075(11)	3352.0304(4)	0.0020	6400	4d	(3/2) <sup>2</sup> 3/2 <sub>1/2</sub> 5f	(3/2) <sup>2</sup> 3/2 <sub>1/2</sub> <sup>2</sup>			Ric		

Table A1. Cont.

$\lambda_{\text{obs}}^a$ (Å)	$\sigma_{\text{obs}}^b$ (cm <sup>-1</sup> )	$\lambda_{\text{Ritz}}^c$ (Å)	$\Delta\lambda_{\text{obs-Ritz}}^d$ (Å)	$I_{\text{obs}}^d$ (arb. u.)	Char <sup>e</sup>	Lower Level	Upper Level	A (s <sup>-1</sup> )	Acc <sup>f</sup>	Line Ref. <sup>g</sup>	TP Ref. <sup>h</sup>	Notes <sup>b</sup>
3352.07 <sup>9</sup>	29823.66	3352.0793(6)	-0.0005	330	5p	(3/2) <sup>+</sup> 5/2 <sup>+</sup> 3	(3/2) <sup>+</sup> 3/2 <sup>+</sup> 2 <sup>+</sup>	8s		Ric		
3354.0672(12)	29805.983(11)	3354.0677(3)	-0.0011	130	5p	( <sup>4</sup> F) <sup>+</sup> 3p <sup>+</sup> 2	(3/2) <sup>+</sup> 3/2 <sup>+</sup> 2 <sup>+</sup>	7s		Ric		
3355.3107(13)	29794.937(11)	3355.31179(19)	0.0010	64	5s	(5/2) <sup>+</sup> 5/2 <sup>+</sup> 2 <sup>+</sup>	(3/2) <sup>+</sup> 5/2 <sup>+</sup> 3	4f		Ric		
3356.8877(17)	29780.940(15)	3356.8867(3)	0.0010	60	s <sup>2</sup>	( <sup>3</sup> F) <sup>+</sup> 3p <sup>+</sup> 3	( <sup>3</sup> F) <sup>+</sup> 3p <sup>+</sup> 3	3F <sup>+</sup> 3		Ric		
3357.4722(10)	29775.756(9)	3357.4732(5)	-0.0010	64	sp	( <sup>4</sup> F) <sup>3</sup> p <sup>+</sup> 1D <sup>+</sup> 2	(5/2) <sup>+</sup> 5/2 <sup>+</sup> 2 <sup>+</sup>	7d		Ric		
3357.9368(14)	29771.636(12)	3357.9364(5)	0.0004	510	sp	( <sup>4</sup> F) <sup>3</sup> p <sup>+</sup> 3C <sup>+</sup> 3	(5/2) <sup>+</sup> 5/2 <sup>+</sup> 2 <sup>+</sup>	6d		Ric		
3359.0587(9)	29761.693(8)	3359.0575(4)	0.0012	950	sp	( <sup>4</sup> F) <sup>3</sup> p <sup>+</sup> 1D <sup>+</sup> 2	(5/2) <sup>+</sup> 5/2 <sup>+</sup> 2 <sup>+</sup>	7d		Ric		
3359.7217(9)	29755.620(8)	3359.7209(3)	0.0008	670	sp	( <sup>4</sup> F) <sup>3</sup> p <sup>+</sup> 1D <sup>+</sup> 2	(3/2) <sup>+</sup> 3/2 <sup>+</sup> 2 <sup>+</sup>	7s		Ric		
3363.8287(17)	29719.491(15)	3363.8300(10)	-0.0013	310	4d	(3/2) <sup>+</sup> 3/2 <sup>+</sup> 2 <sup>+</sup>	(5/2) <sup>+</sup> 5/2 <sup>+</sup> 2 <sup>+</sup>	7p		Ric		
3365.4414(17)	29705.430(15)	3365.4436(7)	-0.0021	610	sp	( <sup>4</sup> F) <sup>3</sup> p <sup>+</sup> 3D <sup>+</sup> 3	(3/2) <sup>+</sup> 3/2 <sup>+</sup> 2 <sup>+</sup>	5d		Ric		
3365.6475(8)	29703.431(7)	3365.6470(3)	0.0005	11000	4d	(5/2) <sup>+</sup> 7/2 <sup>+</sup> 2 <sup>+</sup>	(5/2) <sup>+</sup> 7/2 <sup>+</sup> 2 <sup>+</sup>	5f	2.9e+07	D+	TW	
3366.2696(10)	29697.942(9)	3366.2690(3)	0.0006	10000	4d	(5/2) <sup>+</sup> 7/2 <sup>+</sup> 2 <sup>+</sup>	(5/2) <sup>+</sup> 7/2 <sup>+</sup> 2 <sup>+</sup>	5f		Ric		
3366.5619(8)	29695.364(7)	3366.5618(3)	0.0001	6100	4d	(5/2) <sup>+</sup> 7/2 <sup>+</sup> 2 <sup>+</sup>	(5/2) <sup>+</sup> 7/2 <sup>+</sup> 2 <sup>+</sup>	5f		Ric		
3366.8560(24)	29692.770(21)	3366.8533(4)	0.0007	120	5s	(5/2) <sup>+</sup> 5/2 <sup>+</sup> 2 <sup>+</sup>	(5/2) <sup>+</sup> 5/2 <sup>+</sup> 2 <sup>+</sup>	4f		Ric		
3370.1508(11)	29663.742(10)	3370.1503(4)	0.0005	610	5p	(5/2) <sup>+</sup> 5/2 <sup>+</sup> 3	(5/2) <sup>+</sup> 5/2 <sup>+</sup> 2 <sup>+</sup>	8s	4.3e+07	D+	TW	
3370.4529(7)	29661.083(6)	3370.45289(23)	-0.0000	22000	4d	(5/2) <sup>+</sup> 7/2 <sup>+</sup> 2 <sup>+</sup>	(5/2) <sup>+</sup> 7/2 <sup>+</sup> 2 <sup>+</sup>	5f		F,Re		
3370.6573(11)	29659.285(10)	3370.6573(3)	-0.0001	1100	4d	(5/2) <sup>+</sup> 7/2 <sup>+</sup> 2 <sup>+</sup>	(5/2) <sup>+</sup> 5/2 <sup>+</sup> 2 <sup>+</sup>	5f		Ric		
3370.7846(8)	29658.165(7)	3370.7840(3)	0.0006	5900	4d	(5/2) <sup>+</sup> 7/2 <sup>+</sup> 2 <sup>+</sup>	(5/2) <sup>+</sup> 7/2 <sup>+</sup> 2 <sup>+</sup>	5f		Ric		
3371.4073(9)	29652.685(8)	3371.4079(3)	-0.0004	6200	4d	(5/2) <sup>+</sup> 7/2 <sup>+</sup> 2 <sup>+</sup>	(5/2) <sup>+</sup> 7/2 <sup>+</sup> 2 <sup>+</sup>	5f		Ric		
3371.7016(9)	29650.099(8)	3371.7016(3)	0.0000	870	4d	(5/2) <sup>+</sup> 7/2 <sup>+</sup> 2 <sup>+</sup>	(5/2) <sup>+</sup> 7/2 <sup>+</sup> 2 <sup>+</sup>	5f		Ric		
3373.5914(8)	29633.490(7)	3373.5912(3)	0.0002	9700	4d	(5/2) <sup>+</sup> 5/2 <sup>+</sup> 2 <sup>+</sup>	(5/2) <sup>+</sup> 5/2 <sup>+</sup> 2 <sup>+</sup>	5f		Ric		
3374.4423(13)	29626.018(11)	3374.4427(4)	-0.0005	170	5s	(3/2) <sup>+</sup> 3/2 <sup>+</sup> 2 <sup>+</sup>	( <sup>4</sup> F) <sup>3</sup> p <sup>+</sup> 3F <sup>+</sup> 2	9p		Ric		
3374.9515(8)	29621.548(7)	3374.9510(4)	0.0005	12000	4d	(3/2) <sup>+</sup> 5/2 <sup>+</sup> 2 <sup>+</sup>	(3/2) <sup>+</sup> 5/2 <sup>+</sup> 2 <sup>+</sup>	8s	4.6e+07	D+	TW	
3375.2221(12)	29619.173(11)	3375.2222(4)	-0.0000	1400	4d	(3/2) <sup>+</sup> 5/2 <sup>+</sup> 2 <sup>+</sup>	(3/2) <sup>+</sup> 5/2 <sup>+</sup> 2 <sup>+</sup>	5f		Ric		
3376.6139(8)	29606.965(7)	3376.6143(3)	-0.0004	1300	4d	(5/2) <sup>+</sup> 7/2 <sup>+</sup> 2 <sup>+</sup>	(5/2) <sup>+</sup> 5/2 <sup>+</sup> 2 <sup>+</sup>	5f		Ric		
3377.0834(17)	29602.849(15)	3377.0829(4)	0.0006	170	sp	( <sup>4</sup> F) <sup>3</sup> p <sup>+</sup> 3F <sup>+</sup> 2	(5/2) <sup>+</sup> 5/2 <sup>+</sup> 2 <sup>+</sup>	6d		Ric		
3377.2601(14)	29601.300(12)	3377.2583(3)	0.0019	110	4d	(5/2) <sup>+</sup> 7/2 <sup>+</sup> 2 <sup>+</sup>	(5/2) <sup>+</sup> 5/2 <sup>+</sup> 2 <sup>+</sup>	5f		Ric		
3377.7037(8)	29597.412(7)	3377.7038(3)	-0.0001	5300	4d	(5/2) <sup>+</sup> 7/2 <sup>+</sup> 2 <sup>+</sup>	(5/2) <sup>+</sup> 5/2 <sup>+</sup> 2 <sup>+</sup>	5f		Ric		
3378.3846(15)	29591.448(13)	3378.3831(4)	0.0015	170	sp	( <sup>4</sup> F) <sup>3</sup> p <sup>+</sup> 3F <sup>+</sup> 2	(3/2) <sup>+</sup> 5/2 <sup>+</sup> 2 <sup>+</sup>	6d		Ric		
3378.5046(8)	29590.354(7)	3378.5094(3)	0.0001	3500	4d	(5/2) <sup>+</sup> 5/2 <sup>+</sup> 2 <sup>+</sup>	(5/2) <sup>+</sup> 5/2 <sup>+</sup> 2 <sup>+</sup>	5f		Ric		
3379.4421(9)	29582.188(8)	3379.4410(4)	0.0011	500	4d	(3/2) <sup>+</sup> 5/2 <sup>+</sup> 2 <sup>+</sup>	(3/2) <sup>+</sup> 5/2 <sup>+</sup> 2 <sup>+</sup>	5f		Ric		
3379.9595(9)	29577.660(8)	3379.9602(3)	-0.0007	3800	4d	(3/2) <sup>+</sup> 5/2 <sup>+</sup> 2 <sup>+</sup>	(3/2) <sup>+</sup> 5/2 <sup>+</sup> 2 <sup>+</sup>	5f		Ric		
3380.3311(8)	29574.409(7)	3380.33017(22)	0.0009	1100	4d	(5/2) <sup>+</sup> 7/2 <sup>+</sup> 2 <sup>+</sup>	(5/2) <sup>+</sup> 7/2 <sup>+</sup> 2 <sup>+</sup>	5f		Ric		
3380.7117(8)	29571.079(10)	3380.7116(4)	0.0002	7600	4d	(3/2) <sup>+</sup> 5/2 <sup>+</sup> 2 <sup>+</sup>	(3/2) <sup>+</sup> 5/2 <sup>+</sup> 2 <sup>+</sup>	5f		Ric		
3381.1021(11)	29567.665(10)	3381.1027(4)	-0.0006	1400	4d	(5/2) <sup>+</sup> 5/2 <sup>+</sup> 2 <sup>+</sup>	(5/2) <sup>+</sup> 5/2 <sup>+</sup> 2 <sup>+</sup>	5f	3.4e+07	D+	TW	
3384.3322(8)	29539.446(7)	3384.3324(3)	-0.0002	1300	4d	(5/2) <sup>+</sup> 5/2 <sup>+</sup> 2 <sup>+</sup>	(5/2) <sup>+</sup> 5/2 <sup>+</sup> 2 <sup>+</sup>	5f		Ric		
3384.7698(14)	29533.627(12)	3384.7669(6)	0.0029	160	5p	(3/2) <sup>+</sup> 3/2 <sup>+</sup> 2 <sup>+</sup>	(3/2) <sup>+</sup> 3/2 <sup>+</sup> 2 <sup>+</sup>	8s		Ric		
3384.9450(9)	29534.098(8)	3384.9442(4)	0.0009	3600	4d	(3/2) <sup>+</sup> 5/2 <sup>+</sup> 2 <sup>+</sup>	(3/2) <sup>+</sup> 5/2 <sup>+</sup> 2 <sup>+</sup>	5f		Ric		
3385.4657(9)	29529.556(8)	3385.4650(3)	0.0006	2100	4d	(3/2) <sup>+</sup> 5/2 <sup>+</sup> 2 <sup>+</sup>	(3/2) <sup>+</sup> 5/2 <sup>+</sup> 2 <sup>+</sup>	5f		Ric		
3387.3535(17)	29513.099(15)	3387.3515(4)	0.0021	100	4d	(3/2) <sup>+</sup> 5/2 <sup>+</sup> 2 <sup>+</sup>	(5/2) <sup>+</sup> 5/2 <sup>+</sup> 2 <sup>+</sup>	5f		Ric		
3387.7986(17)	29509.222(15)	3387.8000(8)	-0.0015	210	5p	(3/2) <sup>+</sup> 3/2 <sup>+</sup> 2 <sup>+</sup>	(3/2) <sup>+</sup> 3/2 <sup>+</sup> 2 <sup>+</sup>	8s		Ric		

Table A1. Cont.

$\lambda_{\text{obs}}^a$ (Å)	$\sigma_{\text{obs}}^b$ (cm <sup>-1</sup> )	$\lambda_{\text{Ritz}}^c$ (Å)	$\Delta\lambda_{\text{obs-Ritz}}^d$ (Å)	$I_{\text{obs}}^d$ (arb. u.)	Char <sup>e</sup>	Lower Level	Upper Level	A (s <sup>-1</sup> )	Acc <sup>f</sup>	Line Ref. <sup>g</sup>	TP Ref. <sup>g</sup>	Notes <sup>h</sup>
3388.4491(14)	29503.557(12)	3388.4504(4)	-0.0013	420		4d	(3/2) <sup>+</sup> 15/2] <sub>3</sub>	5f		Ric		
		3390.6470(10)			m	4d	(3/2) <sup>+</sup> 15/2] <sub>2</sub>	7p		Ric		
3390.664(20)	29484.29(17)	3390.6678(4)	-0.004	260		4d	(3/2) <sup>+</sup> 15/2] <sub>1</sub>	5f		Ric		
3390.9325(24)	29481.950(21)	3390.9337(4)	-0.0012	100		s <sup>2</sup>	( <sup>3</sup> F) <sup>3</sup> P <sup>o</sup> - <sup>3</sup> F <sup>o</sup> - <sup>2</sup>	6d		Ric		
3392.7462(24)	29466.190(21)	3392.7444(4)	0.0019	130		sp	( <sup>3</sup> F) <sup>3</sup> P <sup>o</sup> - <sup>3</sup> D <sup>o</sup> - <sup>1</sup>			Ric		
3393.976(18)	29455.513(16)	3393.9803(13)	-0.0042	150	*	sp	( <sup>3</sup> F) <sup>3</sup> P <sup>o</sup> - <sup>5</sup> P <sup>o</sup> - <sup>2</sup>	7g		Ric		X
3393.976(18)	29455.513(16)	3393.9829(4)	-0.0069	150	*	4d	(3/2) <sup>+</sup> 15/2] <sub>2</sub>	5f		Ric		X
3393.9909(15)	29455.384(13)	3393.9914(6)	-0.0004	150		sp	( <sup>3</sup> F) <sup>3</sup> P <sup>o</sup> - <sup>3</sup> G <sup>o</sup> - <sup>4</sup>	7s		Ric		
3395.2150(9)	29444.115(9)	3395.2154(4)	-0.0004	2000		sp	( <sup>3</sup> F) <sup>3</sup> P <sup>o</sup> - <sup>3</sup> D <sup>o</sup> - <sup>2</sup>	6d		Ric		
3395.5206(10)	29442.115(9)	3395.5191(4)	0.0015	450		sp	( <sup>3</sup> F) <sup>3</sup> P <sup>o</sup> - <sup>3</sup> F <sup>o</sup> - <sup>2</sup>	6d		Ric		
3397.3752(9)	29426.043(8)	3397.3754(3)	-0.0002	740		sp	( <sup>3</sup> F) <sup>3</sup> P <sup>o</sup> - <sup>3</sup> D <sup>o</sup> - <sup>2</sup>	6d		Ric		
3400.4535(9)	29399.406(8)	3400.4535(6)	0.0000	96		4d	(3/2) <sup>+</sup> 13/2] <sub>2</sub>	7p		Ric		
3402.8301(9)	29378.873(7)	3402.8303(4)	-0.0002	1500		4d	(5/2) <sup>+</sup> 11/2] <sub>1</sub>	5f		Ric		
3406.835(2)	29344.340(2)	3406.8351(4)	-0.0001	140		5s	( <sup>3</sup> F) <sup>3</sup> P <sup>o</sup> - <sup>3</sup> F <sup>o</sup> - <sup>2</sup>			Ric		
3409.159(6)	29324.327(7)	3409.1597(4)	0.0001	1400		4d	(5/2) <sup>+</sup> 11/2] <sub>1</sub>	5f		Ric		
3410.4564(17)	29313.180(15)	3410.4549(5)	0.0015	90		5s	( <sup>3</sup> F) <sup>3</sup> P <sup>o</sup> - <sup>3</sup> D <sup>o</sup> - <sup>2</sup>			Ric		
3410.6738(13)	29311.311(11)	3410.6739(9)	-0.0000	90		5p	(3/2) <sup>+</sup> 11/2] <sub>1</sub>	7d		Ric		
3412.2696(10)	29297.604(9)	3412.2691(4)	0.0005	130		sp	( <sup>3</sup> F) <sup>3</sup> P <sup>o</sup> - <sup>3</sup> D <sup>o</sup> - <sup>2</sup>	6d		Ric		
3413.7074(14)	29285.265(12)	3413.7080(5)	-0.0007	180		sp	( <sup>3</sup> F) <sup>3</sup> P <sup>o</sup> - <sup>3</sup> D <sup>o</sup> - <sup>2</sup>	6d		Ric		
3413.8952(9)	29283.654(8)	3413.8957(6)	-0.0006	220		5p	(3/2) <sup>+</sup> 13/2] <sub>2</sub>	8s		Ric		
3416.9362(12)	29257.593(11)	3416.9349(4)	0.0012	170		sp	( <sup>3</sup> F) <sup>3</sup> P <sup>o</sup> - <sup>1</sup> F <sup>o</sup> - <sup>3</sup>	8s		Ric		
3421.5612(10)	29218.046(8)	3421.5612(4)	-0.0001	850		sp	( <sup>3</sup> F) <sup>3</sup> P <sup>o</sup> - <sup>1</sup> F <sup>o</sup> - <sup>3</sup>	8s		Ric		
3428.7688(10)	29158.654(8)	3428.7659(5)	-0.0001	330		5s	(3/2) <sup>+</sup> 13/2] <sub>1</sub>	6p		Ric		
3430.1011(12)	29145.304(10)	3430.1015(4)	-0.0004	81		s <sup>2</sup>	( <sup>3</sup> F) <sup>3</sup> P <sup>o</sup> - <sup>3</sup> D <sup>o</sup> - <sup>1</sup>			Ric		
3433.9380(9)	29112.740(8)	3433.9259(7)	0.0120	120	?	4d	(3/2) <sup>+</sup> 15/2] <sub>2</sub>	7p		Ric		
3437.1829(19)	29085.256(16)	3437.1784(5)	0.0045	78		sp	( <sup>3</sup> F) <sup>3</sup> P <sup>o</sup> - <sup>3</sup> D <sup>o</sup> - <sup>2</sup>	6d		Ric		
3444.1360(17)	29026.540(14)	3444.1368(7)	-0.0008	75		sp	( <sup>3</sup> F) <sup>3</sup> P <sup>o</sup> - <sup>3</sup> D <sup>o</sup> - <sup>2</sup>	6d		Ric		
3445.9053(16)	29011.637(13)	3445.9035(5)	0.0018	37		5p	(3/2) <sup>+</sup> 15/2] <sub>2</sub>	7d		Ric		
3451.4534(9)	28965.003(8)	3451.4543(4)	-0.0009	360		5s	(3/2) <sup>+</sup> 13/2] <sub>2</sub>	sp		Ric		
3453.9306(10)	28944.230(9)	3453.9308(6)	-0.0002	540		5s	(3/2) <sup>+</sup> 13/2] <sub>1</sub>	6p		Ric		
3460.045(5)	28895.080(21)	3460.0456(7)	-0.0000	350		sp	( <sup>3</sup> F) <sup>3</sup> P <sup>o</sup> - <sup>3</sup> F <sup>o</sup> - <sup>4</sup>	6d		Ric		
3460.4304(14)	28889.865(11)	3460.4309(5)	-0.0005	69		5p	(3/2) <sup>+</sup> 11/2] <sub>1</sub>	7d		Ric		
3461.9510(15)	28877.176(12)	3461.9515(5)	-0.0005	100		5s	(5/2) <sup>+</sup> 15/2] <sub>2</sub>	sp		Ric		
3463.4085(10)	28865.024(9)	3463.4094(3)	-0.0009	140		sp	( <sup>3</sup> F) <sup>3</sup> P <sup>o</sup> - <sup>3</sup> D <sup>o</sup> - <sup>1</sup>	7s		Ric		
3467.679(3)	28829.480(21)	3467.6793(7)	-0.001	200		sp	( <sup>3</sup> F) <sup>3</sup> P <sup>o</sup> - <sup>3</sup> F <sup>o</sup> - <sup>4</sup>	6d		Ric		
3469.4366(10)	28814.873(9)	3469.4375(4)	-0.0009	1000		sp	( <sup>3</sup> F) <sup>3</sup> P <sup>o</sup> - <sup>3</sup> D <sup>o</sup> - <sup>1</sup>	7s		Ric		
3470.7569(14)	28803.912(11)	3470.7552(8)	0.0017	130		5p	(3/2) <sup>+</sup> 11/2] <sub>1</sub>	7d		Ric		
3471.1588(10)	28800.602(8)	3471.1560(4)	-0.0003	260		5p	( <sup>3</sup> F) <sup>3</sup> P <sup>o</sup> - <sup>1</sup> D <sup>o</sup> - <sup>2</sup>	8s		Ric		
3472.0273(10)	28793.371(9)	3472.0278(3)	-0.0003	330		sp	( <sup>3</sup> F) <sup>3</sup> P <sup>o</sup> - <sup>3</sup> F <sup>o</sup> - <sup>3</sup>	7s		Ric		
3473.0008(10)	28785.302(8)	3473.0010(4)	-0.0002	130		5s	(5/2) <sup>+</sup> 15/2] <sub>2</sub>	sp		Ric		

Table A1. Cont.

$\lambda_{obs}^a$ (Å)	$\sigma_{obs}^b$ (cm <sup>-1</sup> )	$\lambda_{Ritz}^c$ (Å)	$\Delta\lambda_{obs-Ritz}^d$ (Å)	$I_{obs}^d$ (arb. u.)	Char <sup>e</sup>	Lower Level	Upper Level	A (s <sup>-1</sup> )	Acc <sup>f</sup>	Line Ref. <sup>g</sup>	TP Ref. <sup>h</sup>	Notes <sup>b</sup>
3476.470(17)	28756.571(14)	3476.470(37)	0.0005	97	sp	( <sup>3</sup> F) <sup>3</sup> P <sup>o</sup> 3P <sup>o</sup> 4	(5/2) <sup>2</sup> 19/21 <sub>4</sub>	Ric		Ric		
3478.950(3)	28736.080(21)	3478.9487(7)	0.001	640	sp	( <sup>3</sup> F) <sup>3</sup> P <sup>o</sup> 3F <sup>o</sup> 4	(5/2) <sup>2</sup> 19/21 <sub>6</sub>	Ric		Ric		
3483.830(9)	28695.825(8)	3483.8297(4)	0.0006	310	4d	(3/2) <sup>1</sup> 11/21 <sub>1</sub>	(5/2) <sup>2</sup> 11/21 <sub>2</sub>	Ric		Ric		
3487.029(19)	34869.502(7)	3487.0290(4)	0.0001	470	4d	(3/2) <sup>1</sup> 11/21 <sub>1</sub>	(5/2) <sup>2</sup> 11/21 <sub>1</sub>	Ric		Ric		
3488.021(216)	28661.348(13)	3488.0222(6)	-0.0010	31	5s	(3/2) <sup>2</sup> 13/21 <sub>1</sub>	(5/2) <sup>2</sup> 13/21 <sub>2</sub>	Ric		Ric		
3488.437(99)	34888.439(5)	3488.439(5)	0.0001	150	4d	(3/2) <sup>2</sup> 11/21 <sub>1</sub>	(5/2) <sup>2</sup> 11/21 <sub>1</sub>	Ric		Ric		
3501.612(3)	28850.110(21)	3501.6122(4)	-0.0003	59	5p	(5/2) <sup>2</sup> 13/21 <sub>2</sub>	(3/2) <sup>2</sup> 15/21 <sub>2</sub>	Ric		Ric		
3503.009(89)	28538.716(8)	3503.0101(3)	-0.0003	150	5p	(5/2) <sup>2</sup> 13/21 <sub>2</sub>	(3/2) <sup>2</sup> 15/21 <sub>2</sub>	Ric		Ric		
3504.664(315)	28825.244(12)	3504.6642(4)	0.0001	59	s <sup>2</sup>	3P <sup>1</sup> 1	( <sup>3</sup> F) <sup>3</sup> P <sup>o</sup> 3D <sup>o</sup> 2	Ric		Ric		
3506.663(11)	28507.578(9)	3506.66359(4)	0.0003	330	sp	( <sup>3</sup> F) <sup>3</sup> P <sup>o</sup> 3D <sup>o</sup> 3	(5/2) <sup>2</sup> 15/21 <sub>2</sub>	Ric		Ric		
3507.301(410)	28503.797(8)	3507.3011(4)	0.0003	58	sp	( <sup>3</sup> F) <sup>3</sup> P <sup>o</sup> 3D <sup>o</sup> 3	(5/2) <sup>2</sup> 15/21 <sub>2</sub>	Ric		Ric		
3515.229(211)	28439.515(9)	3515.2302(4)	-0.0011	850	sp	( <sup>3</sup> F) <sup>3</sup> P <sup>o</sup> 3D <sup>o</sup> 3	(5/2) <sup>2</sup> 15/21 <sub>2</sub>	Ric		Ric		
3516.1395(14)	28432.132(11)	3516.1396(4)	-0.0001	110	sp	( <sup>3</sup> F) <sup>3</sup> P <sup>o</sup> 3F <sup>o</sup> 3	(5/2) <sup>2</sup> 15/21 <sub>2</sub>	Ric		Ric		
3516.778(69)	28426.985(8)	3516.7792(3)	-0.0006	280	5s	(5/2) <sup>2</sup> 15/21 <sub>3</sub>	( <sup>3</sup> F) <sup>3</sup> P <sup>o</sup> 3F <sup>o</sup> 3	Ric		Ric		
3518.0440(10)	28416.761(8)	3518.0449(4)	-0.0009	230	sp	( <sup>3</sup> F) <sup>3</sup> P <sup>o</sup> 3F <sup>o</sup> 3	(5/2) <sup>2</sup> 17/21 <sub>4</sub>	Ric		Ric		
3518.4565(9)	28413.429(7)	3518.4562(3)	0.0003	420	sp	( <sup>3</sup> F) <sup>3</sup> P <sup>o</sup> 3F <sup>o</sup> 3	(5/2) <sup>2</sup> 17/21 <sub>5</sub>	Ric		Ric		
3522.643(3)	28379.660(21)	3522.6429(6)	0.0003	84	5s	(3/2) <sup>2</sup> 13/21 <sub>6</sub>	(5/2) <sup>2</sup> 13/21 <sub>6</sub>	Ric		Ric		
3525.5026(16)	28356.644(13)	3525.5023(5)	0.0013	55	sp	( <sup>3</sup> F) <sup>3</sup> P <sup>o</sup> 3D <sup>o</sup> 1	(5/2) <sup>2</sup> 13/21 <sub>1</sub>	Ric		Ric		
3525.9383(15)	28353.140(12)	3525.9370(4)	0.0013	140	sp	( <sup>3</sup> F) <sup>3</sup> P <sup>o</sup> 3F <sup>o</sup> 3	(5/2) <sup>2</sup> 15/21 <sub>5</sub>	Ric		Ric		
3534.6784(20)	28283.034(16)	3534.6781(9)	0.0002	27	5p	(5/2) <sup>2</sup> 13/21 <sub>1</sub>	(3/2) <sup>2</sup> 11/21 <sub>0</sub>	Ric		Ric		
3534.809(5)	28281.99(4)	3534.8076(3)	0.0002	410	4d	(3/2) <sup>2</sup> 17/21 <sub>1</sub>	(5/2) <sup>2</sup> 19/21 <sub>2</sub>	Ric		Ric		
3534.809(5)	28281.99(4)	3534.8127(5)	-0.004	410	s <sup>2</sup>	3P <sup>2</sup> 2	( <sup>3</sup> F) <sup>3</sup> P <sup>o</sup> 3G <sup>o</sup> 3	Ric		Ric		
3535.0238(14)	28280.254(11)	3535.0262(4)	-0.0003	1100	sp	( <sup>3</sup> F) <sup>3</sup> P <sup>o</sup> 3F <sup>o</sup> 3	(5/2) <sup>2</sup> 19/21 <sub>4</sub>	Ric		Ric		
3535.4942(10)	28276.508(8)	3535.4937(3)	0.0005	220	4d	(3/2) <sup>2</sup> 17/21 <sub>5</sub>	(5/2) <sup>2</sup> 17/21 <sub>4</sub>	Ric		Ric		
3535.8163(12)	28273.932(9)	3535.8167(3)	-0.0004	190	4d	(3/2) <sup>2</sup> 17/21 <sub>5</sub>	(5/2) <sup>2</sup> 17/21 <sub>3</sub>	Ric		Ric		
3535.9757(10)	28272.657(8)	3535.9767(5)	-0.0009	140	sp	( <sup>3</sup> F) <sup>3</sup> P <sup>o</sup> 3F <sup>o</sup> 3	(5/2) <sup>2</sup> 17/21 <sub>6</sub>	Ric		Ric		
3540.1850(15)	28239.042(12)	3540.1870(5)	-0.0020	110	5p	( <sup>3</sup> F) <sup>3</sup> P <sup>o</sup> 3C <sup>o</sup> 3	(5/2) <sup>2</sup> 15/21 <sub>2</sub>	Ric		Ric		
3540.3356(19)	28237.841(15)	3540.3346(4)	0.0010	110	4d	(3/2) <sup>2</sup> 17/21 <sub>5</sub>	(5/2) <sup>2</sup> 15/21 <sub>2</sub>	Ric		Ric		
3541.2200(20)	28230.789(16)	3541.2196(4)	0.0004	27	4d	(3/2) <sup>2</sup> 17/21 <sub>5</sub>	(5/2) <sup>2</sup> 15/21 <sub>3</sub>	Ric		Ric		
3546.7568(21)	28186.719(17)	3546.7551(5)	0.0017	27	5p	(3/2) <sup>2</sup> 13/21 <sub>2</sub>	(5/2) <sup>2</sup> 17/21 <sub>5</sub>	Ric		Ric		
3548.7423(11)	28170.949(9)	3548.7419(4)	0.0004	1400	sp	( <sup>3</sup> F) <sup>3</sup> P <sup>o</sup> 3C <sup>o</sup> 3	(5/2) <sup>2</sup> 15/21 <sub>5</sub>	Ric		Ric		
3551.4887(13)	28149.165(10)	3551.4887(3)	0.0001	530	4d	(3/2) <sup>2</sup> 17/21 <sub>5</sub>	(5/2) <sup>2</sup> 19/21 <sub>5</sub>	Ric		Ric		
3551.8563(10)	28146.252(8)	3551.8563(3)	-0.0000	210	4d	(3/2) <sup>2</sup> 17/21 <sub>5</sub>	(5/2) <sup>2</sup> 19/21 <sub>4</sub>	Ric		Ric		
3552.5495(12)	28140.760(9)	3552.5490(3)	0.0005	110	4d	(3/2) <sup>2</sup> 17/21 <sub>5</sub>	(5/2) <sup>2</sup> 17/21 <sub>4</sub>	Ric		Ric		
3552.8735(15)	28138.194(12)	3552.8751(3)	-0.0016	53	4d	(3/2) <sup>2</sup> 17/21 <sub>5</sub>	(5/2) <sup>2</sup> 17/21 <sub>3</sub>	Ric		Ric		
3555.4287(21)	28117.927(17)	3555.4326(15)	-0.0039	53	5s	(5/2) <sup>2</sup> 15/21 <sub>6</sub>	(5/2) <sup>2</sup> 17/21 <sub>5</sub>	Ric		Ric		
3556.915(5)	28106.22(4)	3556.9167(3)	-0.001	79	5s	(5/2) <sup>2</sup> 15/21 <sub>6</sub>	( <sup>3</sup> F) <sup>3</sup> P <sup>o</sup> 3F <sup>o</sup> 3	Ric		Ric		
3556.915(5)	28106.22(4)	3556.9231(7)	-0.008	79	5p	(3/2) <sup>2</sup> 13/21 <sub>2</sub>	(5/2) <sup>2</sup> 13/21 <sub>2</sub>	Ric		Ric		
3558.332(4)	28095.03(3)	3558.3303(4)	0.0002	52	4d	(3/2) <sup>2</sup> 17/21 <sub>5</sub>	(5/2) <sup>2</sup> 15/21 <sub>3</sub>	Ric		Ric		
3562.4574(10)	28062.497(8)	3562.4572(3)	-0.0002	100	4d	(3/2) <sup>2</sup> 17/21 <sub>5</sub>	(5/2) <sup>2</sup> 11/21 <sub>5</sub>	Ric		Ric		
3563.1578(10)	28056.981(8)	3563.1580(4)	0.0018	78	4d	(3/2) <sup>2</sup> 13/21 <sub>1</sub>	(5/2) <sup>2</sup> 15/21 <sub>2</sub>	Ric		Ric		
3565.7620(21)	28036.491(17)	3565.7601(4)	0.0018	52	5p	(3/2) <sup>2</sup> 15/21 <sub>2</sub>	(5/2) <sup>2</sup> 15/21 <sub>2</sub>	Ric		Ric		
3565.8472(10)	28035.821(8)	3565.8496(4)	-0.0024	210	5s	(3/2) <sup>2</sup> 13/21 <sub>1</sub>	(5/2) <sup>2</sup> 17/21 <sub>3</sub>	Ric		Ric		
3566.9405(11)	28027.228(9)	3566.9405(5)	-0.0000	52	4d	(3/2) <sup>2</sup> 13/21 <sub>1</sub>	(5/2) <sup>2</sup> 13/21 <sub>1</sub>	Ric		Ric		

Table A1. Cont.

$\lambda_{\text{obs}}^a$ (Å)	$\sigma_{\text{obs}}^b$ (cm <sup>-1</sup> )	$\lambda_{\text{Ritz}}^c$ (Å)	$\Delta\lambda_{\text{obs-Ritz}}^d$ (Å)	$I_{\text{obs}}^d$ (arb. u.)	Char <sup>e</sup>	Lower Level	Upper Level	A (s <sup>-1</sup> )	Acc <sup>f</sup>	Line Ref. <sup>g</sup>	TP Ref. <sup>h</sup>	Notes <sup>b</sup>
3567.801(3)	28020.470(21)	3567.79746(15)	0.003	73	5s	(5/2) <sup>1</sup> 5/2 <sub>1/2</sub>	4f	(5/2) <sup>1</sup> 5/2 <sub>1/2</sub> <sup>3</sup>		Ric		
3568.706(18)	28013.405(14)	3568.7005(4)	0.001	78	5s <sup>2</sup>	3P <sub>2</sub>	4f	( <sup>3</sup> F) <sup>3</sup> P <sup>3</sup> D <sup>3</sup>		Ric		
3573.5908(14)	27975.072(11)	3573.58964(18)	0.0011	520	5s	(5/2) <sup>1</sup> 5/2 <sub>1/2</sub>	5f	(5/2) <sup>1</sup> 7/2 <sub>1/2</sub> <sup>3</sup>		Ric		
3575.373(4)	27961.13(3)	3575.3666(24)	0.006	26	*	(1D) <sup>3</sup> P <sup>3</sup> F <sup>3</sup> D <sup>3</sup>	9s	(3/2) <sup>1</sup> 3/2 <sub>1/2</sub> <sup>1</sup>		Ric		
3575.373(4)	27961.13(3)	3575.3746(5)	-0.002	26	4d	(3/2) <sup>1</sup> 3/2 <sub>1/2</sub> <sup>1</sup>	5f	(5/2) <sup>1</sup> 1/2 <sub>1/2</sub> <sup>0</sup>		Ric		
3577.5874(19)	27943.821(15)	3577.5764(4)	0.010	5s	?	(3/2) <sup>1</sup> 3/2 <sub>1/2</sub> <sup>1</sup>	4f	(3/2) <sup>1</sup> 3/2 <sub>1/2</sub> <sup>1</sup>		Ric		X
3578.405(17)	27937.436(13)	3578.4043(6)	0.0008	130	5s	(5/2) <sup>1</sup> 5/2 <sub>1/2</sub>	sp	( <sup>3</sup> P) <sup>3</sup> P <sup>3</sup> S <sup>3</sup> D <sup>3</sup>		Ric		
3581.3166(13)	27914.724(10)	3581.3179(4)	-0.0013	26	5p	(3/2) <sup>1</sup> 7/2 <sub>1/2</sub> <sup>1</sup>	8s	(5/2) <sup>1</sup> 5/2 <sub>1/2</sub>		Ric		
3583.632(15)	27896.687(11)	3583.6328(3)	-0.0005	77	7s	( <sup>3</sup> F) <sup>3</sup> P <sup>3</sup> F <sup>3</sup> D <sup>3</sup>	5f	(3/2) <sup>1</sup> 3/2 <sub>1/2</sub>		Ric		
3588.607(9)	27858.009(7)	3588.6074(3)	0.0005	200	4d	(3/2) <sup>1</sup> 3/2 <sub>1/2</sub> <sup>1</sup>	5f	(5/2) <sup>1</sup> 7/2 <sub>1/2</sub> <sup>3</sup>		Ric		
3590.0862(10)	27830.538(8)	3590.0870(3)	-0.0008	650	5p	( <sup>3</sup> F) <sup>3</sup> P <sup>3</sup> F <sup>3</sup> D <sup>3</sup>	7s	(3/2) <sup>1</sup> 3/2 <sub>1/2</sub>		Ric		
3592.1150(19)	27830.811(15)	3592.1139(5)	0.0011	51	5p	(5/2) <sup>1</sup> 7/2 <sub>1/2</sub> <sup>3</sup>	sp	(3/2) <sup>1</sup> 7/2 <sub>1/2</sub>		Ric		
3592.3528(10)	27828.969(8)	3592.3322(4)	0.0005	770	5s	(3/2) <sup>1</sup> 3/2 <sub>1/2</sub> <sup>1</sup>	sp	( <sup>3</sup> F) <sup>3</sup> P <sup>3</sup> D <sup>3</sup>		Ric		
3593.2610(10)	27821.935(8)	3593.2613(4)	-0.0002	100	4d	(3/2) <sup>1</sup> 3/2 <sub>1/2</sub> <sup>1</sup>	5f	(5/2) <sup>1</sup> 5/2 <sub>1/2</sub> <sup>2</sup>		Ric		
3594.1722(18)	27814.882(14)	3594.1729(4)	-0.0008	130	4d	(3/2) <sup>1</sup> 3/2 <sub>1/2</sub> <sup>1</sup>	5f	(5/2) <sup>1</sup> 5/2 <sub>1/2</sub> <sup>3</sup>		Ric		
3597.100(3)	27792.240(21)	3597.1080(5)	-0.0008	51	5p	(5/2) <sup>1</sup> 5/2 <sub>1/2</sub> <sup>2</sup>	6d	(5/2) <sup>1</sup> 3/2 <sub>1/2</sub>		Ric		
3600.4380(11)	27766.477(8)	3600.4382(4)	-0.0002	76	5p	(5/2) <sup>1</sup> 5/2 <sub>1/2</sub> <sup>2</sup>	6d	(5/2) <sup>1</sup> 5/2 <sub>1/2</sub>		Ric		
3600.7635(10)	27763.967(7)	3600.7638(4)	-0.0002	130	4d	(3/2) <sup>1</sup> 3/2 <sub>1/2</sub> <sup>1</sup>	5f	(5/2) <sup>1</sup> 3/2 <sub>1/2</sub> <sup>2</sup>		Ric		
3601.9187(19)	27755.063(15)	3601.9162(4)	0.0025	200	5p	(5/2) <sup>1</sup> 5/2 <sub>1/2</sub> <sup>2</sup>	6d	(3/2) <sup>1</sup> 3/2 <sub>1/2</sub> <sup>1</sup>		Ric		
3602.2331(11)	27752.641(8)	3602.2324(3)	0.0007	1200	sp	( <sup>3</sup> F) <sup>3</sup> P <sup>3</sup> D <sup>3</sup>	7s	(5/2) <sup>1</sup> 5/2 <sub>1/2</sub> <sup>2</sup>		Ric		
3606.6576(11)	27718.596(8)	3606.6576(4)	0.0000	1900	5s	( <sup>3</sup> F) <sup>3</sup> P <sup>3</sup> D <sup>3</sup>	sp	( <sup>3</sup> F) <sup>3</sup> P <sup>3</sup> D <sup>3</sup>		Ric		
3611.0901(10)	27684.573(7)	3611.0902(3)	-0.0001	370	5p	( <sup>3</sup> F) <sup>3</sup> P <sup>3</sup> D <sup>3</sup>	7s	(5/2) <sup>1</sup> 5/2 <sub>1/2</sub>		Ric		
3611.172	27683.94	3611.1721(4)			:	(5/2) <sup>1</sup> 5/2 <sub>1/2</sub> <sup>2</sup>	6d	(5/2) <sup>1</sup> 3/2 <sub>1/2</sub>		Ric		
3615.0429(20)	27653.303(16)	3615.04192(19)	0.0010	25	5s	(5/2) <sup>1</sup> 5/2 <sub>1/2</sub> <sup>2</sup>	4f	(5/2) <sup>1</sup> 7/2 <sub>1/2</sub> <sup>3</sup>		Ric		
3616.8636(10)	27640.382(7)	3616.8630(4)	0.0007	890	5p	(5/2) <sup>1</sup> 3/2 <sub>1/2</sub> <sup>1</sup>	6d	(5/2) <sup>1</sup> 3/2 <sub>1/2</sub>		Ric		
3621.4008(19)	27605.753(15)	3621.4013(5)	-0.0005	26	4d	(5/2) <sup>1</sup> 5/2 <sub>1/2</sub> <sup>2</sup>	6d	(3/2) <sup>1</sup> 7/2 <sub>1/2</sub>		Ric		
3621.8942(11)	27601.992(8)	3621.8927(4)	0.0016	77	7f	(5/2) <sup>1</sup> 3/2 <sub>1/2</sub> <sup>1</sup>	6d	(3/2) <sup>1</sup> 3/2 <sub>1/2</sub>		Ric		
3626.350(3)	27568.080(21)	3626.3111(9)	0.039	?	?	( <sup>3</sup> F) <sup>3</sup> P <sup>3</sup> C <sup>3</sup> D <sup>3</sup>	6d	(5/2) <sup>1</sup> 7/2 <sub>1/2</sub>		Ric		X
3626.973(3)	27563.340(21)	3626.9734(4)	-0.000	51	5p	(5/2) <sup>1</sup> 5/2 <sub>1/2</sub> <sup>3</sup>	6d	(3/2) <sup>1</sup> 5/2 <sub>1/2</sub>		Ric		
3628.4741(10)	27551.940(8)	3628.4733(4)	0.0008	130	5p	(5/2) <sup>1</sup> 5/2 <sub>1/2</sub> <sup>3</sup>	6d	(3/2) <sup>1</sup> 5/2 <sub>1/2</sub>		Ric		
3629.0907(16)	27547.259(12)	3629.0858(5)	0.0049	51	5p	(3/2) <sup>1</sup> 3/2 <sub>1/2</sub> <sup>1</sup>	sp	( <sup>3</sup> F) <sup>3</sup> P <sup>3</sup> D <sup>3</sup>		Ric		
3629.3186(19)	27545.529(15)	3629.3176(3)	0.0011	26	4d	(3/2) <sup>1</sup> 5/2 <sub>1/2</sub> <sup>1</sup>	5f	(5/2) <sup>1</sup> 9/2 <sub>1/2</sub> <sup>4</sup>		Ric		
3630.0412(11)	27540.046(8)	3630.0408(3)	0.0004	100	4d	(3/2) <sup>1</sup> 5/2 <sub>1/2</sub> <sup>1</sup>	5f	(5/2) <sup>1</sup> 7/2 <sub>1/2</sub> <sup>4</sup>		Ric		
3630.6454(10)	27535.463(7)	3630.6450(4)	0.0004	380	5p	( <sup>3</sup> F) <sup>3</sup> P <sup>3</sup> F <sup>3</sup> D <sup>3</sup>	6d	(5/2) <sup>1</sup> 5/2 <sub>1/2</sub>		Ric		
3631.6198(22)	27528.075(17)	3631.61939(23)	0.0004	51	5s	(5/2) <sup>1</sup> 5/2 <sub>1/2</sub> <sup>2</sup>	4f	(5/2) <sup>1</sup> 1/2 <sub>1/2</sub> <sup>1</sup>		Ric		
3633.1159(10)	27516.740(8)	3633.1151(4)	0.0008	520	sp	(3/2) <sup>1</sup> 5/2 <sub>1/2</sub> <sup>1</sup>	6d	(5/2) <sup>1</sup> 7/2 <sub>1/2</sub>		Ric		
3635.155(17)	27501.302(13)	3635.1443(4)	0.011	210	4d	(3/2) <sup>1</sup> 5/2 <sub>1/2</sub> <sup>1</sup>	5f	(5/2) <sup>1</sup> 5/2 <sub>1/2</sub> <sup>2</sup>		Ric		X
3636.0753(17)	27494.322(13)	3636.0773(4)	0.0009	77	4d	(3/2) <sup>1</sup> 5/2 <sub>1/2</sub> <sup>1</sup>	5f	(5/2) <sup>1</sup> 5/2 <sub>1/2</sub> <sup>3</sup>		Ric		
3637.867(3)	27480.800(21)	3637.8663(4)	0.001	26	5p	(5/2) <sup>1</sup> 5/2 <sub>1/2</sub> <sup>2</sup>	6d	(5/2) <sup>1</sup> 3/2 <sub>1/2</sub>		Ric		
3641.0912(20)	27456.470(15)	3641.0918(5)	-0.0007	52	sp	( <sup>3</sup> F) <sup>3</sup> P <sup>3</sup> F <sup>3</sup> D <sup>3</sup>	6d	(5/2) <sup>1</sup> 5/2 <sub>1/2</sub>		Ric		

Table A1. Cont.

$\lambda_{\text{obs}}^a$ (Å)	$\sigma_{\text{obs}}^b$ (cm <sup>-1</sup> )	$\lambda_{\text{Ritz}}^c$ (Å)	$\Delta\lambda_{\text{obs-Ritz}}^d$ (Å)	$I_{\text{obs}}^d$ (arb. u.)	Char <sup>e</sup>	Lower Level	Upper Level	A (s <sup>-1</sup> )	Acc <sup>f</sup>	Line Ref. <sup>g</sup>	TP Ref. <sup>h</sup>	Notes <sup>b</sup>
3641.7928(11)	27451.180(8)	3641.7903(4)	0.0025	1000	s <sup>2</sup>	5p	(3/2) <sup>+</sup> [5/2] <sup>+</sup> <sub>3</sub>			Ric		
3642.4505(14)	27446.224(11)	3642.4488(4)	0.0017	77	4d	5f	(5/2) <sup>+</sup> [5/2] <sup>+</sup> <sub>3</sub>			Ric		
3642.8238(22)	27443.411(17)	3642.8229(4)	0.0009	26	4d	5f	(5/2) <sup>+</sup> [5/2] <sup>+</sup> <sub>2</sub>			Ric		
3643.0146(11)	27441.974(8)	3643.0150(5)	-0.0004	770	5p	6d	(3/2) <sup>+</sup> [3/2] <sup>+</sup> <sub>1</sub>			Ric		
3643.7566(11)	27436.386(7)	3643.7571(5)	-0.0005	1300	5p	6d	(5/2) <sup>+</sup> [5/2] <sup>+</sup> <sub>3</sub>			Ric		
3647.081(4)	27411.38(3)	3647.0800(10)	0.001	160	sp	6d	(3/2) <sup>+</sup> [5/2] <sup>+</sup> <sub>3</sub> 4d			Ric		
3648.2463(20)	27402.622(15)	3648.2475(5)	-0.0011	52	5p	6d	(5/2) <sup>+</sup> [5/2] <sup>+</sup> <sub>3</sub>			Ric		
3648.8675(15)	27397.807(11)	3648.8650(4)	0.0025	390	5s	6d	(3/2) <sup>+</sup> [5/2] <sup>+</sup> <sub>2</sub> sp			Ric		
3649.2205(22)	27395.307(17)	3649.2180(4)	0.0025	52	4d	5f	(5/2) <sup>+</sup> [5/2] <sup>+</sup> <sub>2</sub>			Ric		
3651.800(3)	27375.960(21)	3651.7900(5)	0.001	100	sp	6d	(3/2) <sup>+</sup> [3/2] <sup>+</sup> <sub>2</sub>			Ric		
3664.2913(10)	27282.636(8)	3664.2900(5)	0.0014	130	5s	6d	(3/2) <sup>+</sup> [3/2] <sup>+</sup> <sub>2</sub>			Ric		
3678.6688(20)	27176.009(15)	3678.6702(6)	-0.0014	80	sp	6d	(3/2) <sup>+</sup> [3/2] <sup>+</sup> <sub>2</sub>			Ric		
3682.4238(14)	27148.298(11)	3682.4254(7)	-0.0016	3900	sp	7s	(3/2) <sup>+</sup> [3/2] <sup>+</sup> <sub>2</sub>			Ric		
3686.5552(10)	27117.875(8)	3686.5539(4)	0.0013	16000	4p	7p	(3/2) <sup>+</sup> [5/2] <sup>+</sup> <sub>3</sub>		C+	Ric		
3693.3279(12)	27068.148(9)	3693.3271(10)	0.0009	81	4d	7p	(3/2) <sup>+</sup> [1/2] <sup>+</sup> <sub>1</sub>	9.7e+05		R2anc		O07
3703.9305(11)	26990.667(8)	3703.9285(5)	0.0020	680	sp	6d	(3/2) <sup>+</sup> [1/2] <sup>+</sup> <sub>1</sub>			Ric		
3724.1764(11)	26843.940(8)	3724.1770(3)	-0.0006	390	7s	6d	(3/2) <sup>+</sup> [3/2] <sup>+</sup> <sub>2</sub>			Ric		
3725.4537(17)	26834.737(12)	3725.4544(4)	-0.0007	110	4p	s <sup>2</sup>	1G <sub>4</sub>			Ric		
3728.6574(10)	26811.681(7)	3728.6569(4)	0.0005	280	sp	7s	(5/2) <sup>+</sup> [5/2] <sup>+</sup> <sub>2</sub>			Ric		
3730.3433(10)	26799.564(7)	3730.3437(5)	-0.0005	250	5s	7s	(5/2) <sup>+</sup> [5/2] <sup>+</sup> <sub>2</sub>			Ric		
3731.1462(13)	26793.797(9)	3731.1479(3)	-0.0018	170	5p	7s	(5/2) <sup>+</sup> [3/2] <sup>+</sup> <sub>2</sub>			Ric		
3738.6488(10)	26740.029(7)	3738.6478(3)	0.0010	1700	sp	7s	(3/2) <sup>+</sup> [3/2] <sup>+</sup> <sub>2</sub>			Ric		
3740.5281(11)	26728.024(8)	3740.5278(4)	0.0003	280	5s	7s	(3/2) <sup>+</sup> [5/2] <sup>+</sup> <sub>2</sub> sp			Ric		
3742.0597(10)	26715.656(7)	3742.0592(4)	0.0006	430	5s	7s	(3/2) <sup>+</sup> [3/2] <sup>+</sup> <sub>2</sub>			Ric		
3748.1909(10)	26671.956(7)	3748.1901(3)	0.0008	1800	sp	7s	(3/2) <sup>+</sup> [3/2] <sup>+</sup> <sub>2</sub>			Ric		
3749.782(10)	26660.64(7)	3749.7756(4)	0.006	400	5s	7s	(5/2) <sup>+</sup> [5/2] <sup>+</sup> <sub>2</sub>			Ric		
3749.782(10)	26660.64(7)	3749.7756(4)	0.006	400	5s	7s	(5/2) <sup>+</sup> [5/2] <sup>+</sup> <sub>2</sub>			Ric		
3751.3859(10)	26649.241(7)	3751.3858(4)	0.0001	310	sp	6d	(3/2) <sup>+</sup> [3/2] <sup>+</sup> <sub>2</sub>			Ric		
3761.4270(14)	26578.103(10)	3761.4269(5)	0.0001	150	sp	6d	(3/2) <sup>+</sup> [1/2] <sup>+</sup> <sub>2</sub>			Ric		
3766.8662(14)	26539.726(10)	3766.8669(5)	-0.0007	230	sp	6d	(3/2) <sup>+</sup> [3/2] <sup>+</sup> <sub>2</sub>			Ric		
3772.5256(10)	26499.913(7)	3772.5262(5)	-0.0006	480	sp	6d	(3/2) <sup>+</sup> [1/2] <sup>+</sup> <sub>2</sub>			Ric		
3774.9743(20)	26482.724(14)	3774.9751(4)	-0.0008	59	5p	6d	(5/2) <sup>+</sup> [3/2] <sup>+</sup> <sub>2</sub>			Ric		
3777.6444(10)	26464.006(7)	3777.6453(3)	-0.0011	150	5p	6d	(5/2) <sup>+</sup> [3/2] <sup>+</sup> <sub>2</sub>			Ric		
3781.9355(12)	26433.980(9)	3781.9350(4)	0.0005	3200	5s	6d	(3/2) <sup>+</sup> [3/2] <sup>+</sup> <sub>2</sub>			Ric		
3786.2696(10)	26403.721(7)	3786.2702(5)	-0.0006	2900	5p	6d	(5/2) <sup>+</sup> [3/2] <sup>+</sup> <sub>2</sub>			Ric		
3795.4413(11)	26339.919(8)	3795.4419(4)	-0.0006	450	5s	6d	(5/2) <sup>+</sup> [5/2] <sup>+</sup> <sub>2</sub>			Ric		
3796.0675(12)	26335.574(8)	3796.0687(4)	-0.0012	580	5p	6d	(5/2) <sup>+</sup> [3/2] <sup>+</sup> <sub>2</sub>			Ric		
3796.1694(12)	26334.867(9)	3796.1694(11)	-0.0000	820	5p	6d	(3/2) <sup>+</sup> [1/2] <sup>+</sup> <sub>1</sub>			Ric		
3797.8489(10)	26323.221(7)	3797.8496(5)	-0.0007	4200	5p	6d	(5/2) <sup>+</sup> [3/2] <sup>+</sup> <sub>2</sub>			Ric		
3801.5563(10)	26297.551(7)	3801.5566(5)	0.0007	670	5p	6d	(3/2) <sup>+</sup> [3/2] <sup>+</sup> <sub>2</sub>			Ric		
3806.27(5)	26265.0(3)	3806.333(3)	-0.06	7400	d <sup>10</sup>	4s	(3/2) <sup>+</sup> [1/2] <sup>+</sup> <sub>1</sub>	1.58e+00	C+	T53,M97,F84	P84	X,E2
3818.8787(11)	26178.268(7)	3818.8793(8)	-0.0006	2000	5p	6d	(5/2) <sup>+</sup> [3/2] <sup>+</sup> <sub>2</sub>			Ric		

Table A1. Cont.

$\lambda_{\text{obs}}^a$ (Å)	$\sigma_{\text{obs}}^b$ (cm <sup>-1</sup> )	$\lambda_{\text{Ritz}}^c$ (Å)	$\Delta\lambda_{\text{obs-Ritz}}^d$ (Å)	$I_{\text{obs}}^d$ (arb. u.)	Char <sup>e</sup>	Lower Level	Upper Level	A (s <sup>-1</sup> )	Acc <sup>f</sup>	Line Ref. <sup>g</sup>	TP Ref. <sup>h</sup>	Notes <sup>b</sup>
3824.8323(11)	26137.521(8)	3824.8321(6)	0.0002	1000		5p	(3/2) <sup>+</sup> 1/2 <sup>0</sup>	6d		Ric		
3826.9209(10)	26123.256(7)	3826.9216(6)	-0.0007	3000		5p	(5/2) <sup>+</sup> 3/2 <sup>1</sup>	6d		Ric		
3836.1646(11)	26060.310(7)	3836.1653(3)	-0.0010	1800		5p	(5/2) <sup>+</sup> 5/2 <sup>2</sup>	7s		Ric		
3841.4818(11)	26024.240(7)	3841.4819(4)	-0.0001	590		5s	(5/2) <sup>+</sup> 15/2 <sup>h</sup>	7s		Ric		
3842.5889(12)	26016.742(8)	3842.5882(3)	0.0007	2000		5p	(5/2) <sup>+</sup> 3/2 <sup>1</sup>	7s		Ric		
3843.5628(13)	26010.150(9)	3843.5624(3)	0.0004	150		5p	(5/2) <sup>+</sup> 5/2 <sup>2</sup>	7s		Ric		
3849.3824(13)	25969.479(9)	3849.5810(5)	0.0014	1700		5s	(5/2) <sup>+</sup> 15/2 <sup>h</sup>	sp		Ric		
3850.0921(15)	25966.600(10)	3850.0095(3)	-0.0007	1600		5p	(5/2) <sup>+</sup> 3/2 <sup>1</sup>	7s		Ric		
3851.1059(11)	25959.212(7)	3851.1020(4)	0.0030	890		s <sup>2</sup>	<sup>1</sup> G <sub>4</sub>	sp		Ric		
3859.41(6)	25903.4(4)	3859.4330(7)	-0.02	180		4d	(5/2) <sup>+</sup> 13/2 <sup>h</sup>	6p		S36c		
3861.3421(11)	25890.391(8)	3861.3424(4)	-0.0004	1300		5p	(5/2) <sup>+</sup> 7/2 <sup>1</sup>	6d		Ric		
3862.1245(11)	25885.146(8)	3862.1243(4)	0.0002	1200		5p	(3/2) <sup>+</sup> 5/2 <sup>2</sup>	6d		Ric		
3863.6403(11)	25874.991(8)	3863.6404(4)	-0.0001	1200		5p	(5/2) <sup>+</sup> 7/2 <sup>1</sup>	6d		Ric		
3864.1370(11)	25871.665(7)	3864.1365(4)	0.0005	3200		5p	(5/2) <sup>+</sup> 7/2 <sup>1</sup>	6d		Ric		
3866.3047(11)	25857.160(7)	3866.3035(3)	0.0013	1200		5p	(5/2) <sup>+</sup> 5/2 <sup>2</sup>	7s		Ric		
3868.3711(11)	25843.348(7)	3868.3707(3)	0.0004	1100		sp	( <sup>1</sup> F) <sup>+</sup> 3 <sup>+</sup>	7s		Ric		
3871.334(3)	25823.570(2.1)	3871.3321(1.0)	0.002	210		5p	( <sup>1</sup> F) <sup>+</sup> 3 <sup>+</sup> G <sup>+</sup>	7s		Ric		
3872.7645(15)	25814.031(10)	3872.7678(5)	-0.0033	550		5p	(3/2) <sup>+</sup> 5/2 <sup>2</sup>	6d		Ric		
3873.2075(11)	25811.078(7)	3873.2058(6)	0.0017	940		5s	(5/2) <sup>+</sup> 15/2 <sup>h</sup>	sp		Ric		
3878.5873(12)	25775.278(8)	3878.5875(3)	-0.0002	860		sp	( <sup>3</sup> P) <sup>+</sup> 3 <sup>+</sup> F <sup>+</sup>	7s		Ric		
3878.667	25774.75	3878.6670(5)			:	5p	(3/2) <sup>+</sup> 1/2 <sup>0</sup>	6d		Ric		
3879.8966(11)	25769.901(7)	3879.3976(4)	-0.0010	3800		5p	(5/2) <sup>+</sup> 7/2 <sup>1</sup>	6d		Ric		
3879.8973(21)	25766.576(14)	3879.8977(4)	-0.0005	140		5p	(5/2) <sup>+</sup> 7/2 <sup>1</sup>	6d		Ric		
3884.1312(9)	25738.489(6)	3884.1313(5)	-0.0001	8100		5p	(5/2) <sup>+</sup> 7/2 <sup>1</sup>	6d		Ric		
3884.5339(11)	25735.821(7)	3884.5330(5)	-0.0010	3800		5p	(3/2) <sup>+</sup> 5/2 <sup>2</sup>	6d		Ric		
3885.2865(17)	25730.836(11)	3885.2789(5)	0.0076	85		bl	(5/2) <sup>+</sup> 7/2 <sup>1</sup>	6d		Ric		
3890.0864(14)	25699.088(9)	3890.0865(4)	-0.0001	2200		5p	(5/2) <sup>+</sup> 5/2 <sup>2</sup>	6d		Ric		
3891.1277(12)	25692.211(8)	3891.1267(5)	0.0010	1500		5p	(5/2) <sup>+</sup> 1/2 <sup>0</sup>	6d		Ric		
3892.9237(11)	25680.358(7)	3892.9223(4)	0.0014	3000		5p	(5/2) <sup>+</sup> 5/2 <sup>2</sup>	6d		Ric		
3894.6198(21)	25669.175(14)	3894.61915(19)	0.0006	280		5s	(3/2) <sup>+</sup> 13/2 <sup>h</sup>	4f		Ric		
3896.6915(11)	25655.527(7)	3896.6912(4)	0.0003	1900		5p	(5/2) <sup>+</sup> 5/2 <sup>1</sup>	6d		Ric		
3896.9491(20)	25653.832(13)	3896.9487(5)	0.0004	280		5p	(3/2) <sup>+</sup> 1/2 <sup>0</sup>	6d		Ric		
3897.7292(20)	25648.698(13)	3897.7262(5)	0.0030	2500		5s	(5/2) <sup>+</sup> 15/2 <sup>h</sup>	sp		Ric		
3900.0571(11)	25633.397(7)	3900.0565(5)	-0.0008	1100		5p	(5/2) <sup>+</sup> 7/2 <sup>1</sup>	6d		Ric		
3901.2315(12)	25625.672(8)	3901.2316(5)	-0.0000	280		5p	(3/2) <sup>+</sup> 5/2 <sup>1</sup>	6d		Ric		
3902.0837(24)	25620.076(16)	3902.0821(5)	0.0016	140		5p	(5/2) <sup>+</sup> 5/2 <sup>2</sup>	6d		Ric		
3902.9667(12)	25614.280(8)	3902.9668(4)	-0.0002	2500		5p	(3/2) <sup>+</sup> 5/2 <sup>1</sup>	6d		Ric		
3903.1761(7)	25612.905(5)	3903.1759(5)	0.0002	8200		5p	(5/2) <sup>+</sup> 7/2 <sup>1</sup>	6d		F,Re	TW	
3905.1121(14)	25600.208(9)	3905.1133(6)	-0.0012	830	?	4d	(3/2) <sup>+</sup> 13/2 <sup>h</sup>	5f	3.5e+07	Ric		
3907.2743(24)	25586.042(16)	3907.2616(8)	0.0127	82		5s	( <sup>1</sup> P) <sup>+</sup> 3 <sup>+</sup> S <sup>+</sup>	2		Ric		X

Table A1. Cont.

$\lambda_{\text{obs}}^a$ (Å)	$\sigma_{\text{obs}}^b$ (cm <sup>-1</sup> )	$\lambda_{\text{Ritz}}^c$ (Å)	$\Delta\lambda_{\text{obs-Ritz}}^d$ (Å)	$I_{\text{obs}}^d$ (arb. u.)	Char <sup>e</sup>	Lower Level	Upper Level	A (s <sup>-1</sup> )	Acc <sup>f</sup>	Line Ref. <sup>g</sup>	TP Ref. <sup>h</sup>	Notes <sup>b</sup>
3912.4911(12)	25551.927(8)	3912.4900(5)	0.0011	690		5p	(5/2) <sup>+</sup> 3/2 <sup>+</sup> 1 <sup>+</sup> 2	6d		Ric		
3913.8355(14)	25543.150(9)	3913.8369(5)	-0.0014	160		5p	(3/2) <sup>+</sup> 5/2 <sup>+</sup> 3	6p		Ric		
3914.311(3)	25540.050(21)	3914.3081(9)	0.002	110	bl	4d	(5/2) <sup>+</sup> 5/2 <sup>+</sup> 3	6d		Ric		
3918.3817(12)	25513.515(8)	3918.3792(4)	0.0025	400	s <sup>2</sup>	5p	(5/2) <sup>+</sup> 3/2 <sup>+</sup> 1 <sup>+</sup> 3	6d		Ric		
3919.1725(11)	25508.366(7)	3919.1710(4)	0.0016	1000		5p	(5/2) <sup>+</sup> 3/2 <sup>+</sup> 1 <sup>+</sup> 3	6d		Ric		
3920.6546(11)	25498.724(7)	3920.6561(5)	-0.0015	4000		5p	(3/2) <sup>+</sup> 5/2 <sup>+</sup> 3	6d		Ric		
3921.071(10)	25496.02(7)	3921.0693(5)	0.002	130	*	5p	(5/2) <sup>+</sup> 3/2 <sup>+</sup> 1 <sup>+</sup> 3	6d	3.3e+07	Ric	TW	
3921.071(10)	25496.02(7)	3921.0811(4)	-0.010	130	*	5p	(5/2) <sup>+</sup> 3/2 <sup>+</sup> 1 <sup>+</sup> 3	6d		Ric		
3921.4136(15)	25493.789(10)	3921.4117(6)	0.0019	450		5p	(3/2) <sup>+</sup> 1/2 <sup>+</sup> 1 <sup>+</sup> 3	6d		Ric		
3923.4504(11)	25480.555(7)	3923.4506(5)	-0.0003	2100		5p	(5/2) <sup>+</sup> 5/2 <sup>+</sup> 3	6d		Ric		
3923.9630(12)	25477.226(8)	3923.9622(4)	0.0008	400		5p	(5/2) <sup>+</sup> 5/2 <sup>+</sup> 3	6d		Ric		
3925.8560(11)	25464.942(7)	3925.8554(5)	0.0006	390		5p	(3/2) <sup>+</sup> 5/2 <sup>+</sup> 3	6d		Ric		
3933.2684(11)	25416.953(7)	3933.2688(5)	-0.0004	2000		5p	(3/2) <sup>+</sup> 5/2 <sup>+</sup> 3	6d		Ric		
3934.1202(11)	25411.450(7)	3934.1175(3)	0.0027	470		5p	(3F <sup>+</sup> 3 <sup>+</sup> 1F <sup>+</sup> 3	7s		Ric		
3935.9626(14)	25394.555(9)	3935.9560(6)	0.0067	380	bl	5s	(3/2) <sup>+</sup> 3/2 <sup>+</sup> 1 <sup>+</sup> 3	sp		Ric		X
3940.9702(12)	25367.282(8)	3940.9707(5)	-0.0004	300		5s	(3/2) <sup>+</sup> 3/2 <sup>+</sup> 1 <sup>+</sup> 3	sp		Ric		
3944.5822(12)	25344.054(8)	3944.5826(5)	-0.0004	490		5p	(5/2) <sup>+</sup> 5/2 <sup>+</sup> 3	6d		Ric		
3945.5770(12)	25337.664(8)	3945.5767(5)	0.0004	2300		5p	(3/2) <sup>+</sup> 3/2 <sup>+</sup> 1 <sup>+</sup> 3	6d		Ric		
3945.7664(13)	25336.448(9)	3945.7662(5)	0.0002	1500		5p	(5/2) <sup>+</sup> 5/2 <sup>+</sup> 3	6d		Ric		
3952.0661(11)	25296.062(7)	3952.0660(6)	0.0001	980		5p	(5/2) <sup>+</sup> 3/2 <sup>+</sup> 1 <sup>+</sup> 3	6d		Ric		
3958.4734(13)	25255.118(8)	3958.4707(5)	0.0027	840		5p	(3/2) <sup>+</sup> 3/2 <sup>+</sup> 1 <sup>+</sup> 3	6d		Ric		
3974.3504(22)	25154.229(14)	3974.3528(7)	-0.0024	91		4d	(5/2) <sup>+</sup> 5/2 <sup>+</sup> 1 <sup>+</sup> 2	6p		Ric		
3975.5387(13)	25146.711(8)	3975.5380(9)	0.0007	90		4d	(3/2) <sup>+</sup> 1/2 <sup>+</sup> 1 <sup>+</sup> 2	7p		Ric		
3985.2145(11)	25085.657(7)	3985.2136(5)	0.0009	700		5p	(3/2) <sup>+</sup> 3/2 <sup>+</sup> 1 <sup>+</sup> 2	6d		Ric		
3987.0237(11)	25074.274(7)	3987.0244(5)	-0.0007	2300		5p	(3/2) <sup>+</sup> 3/2 <sup>+</sup> 1 <sup>+</sup> 2	6d		Ric		
3990.7807(13)	25050.670(8)	3990.7773(5)	0.0033	960		5s	(3/2) <sup>+</sup> 3/2 <sup>+</sup> 1 <sup>+</sup> 2	sp		Ric		
3993.3023(12)	25034.852(8)	3993.3022(5)	0.0001	2600		5p	(3F <sup>+</sup> 3 <sup>+</sup> 1F <sup>+</sup> 3	6d		Ric		
3998.5675(12)	25003.138(8)	3998.5684(5)	-0.0009	860		5p	(3/2) <sup>+</sup> 3/2 <sup>+</sup> 1 <sup>+</sup> 2	6d		Ric		
4003.4759(12)	24971.235(8)	4003.4736(5)	0.0023	1600		5p	(3F <sup>+</sup> 3 <sup>+</sup> 1F <sup>+</sup> 3	6d		Ric		
4004.3155(14)	24964.752(9)	4004.3160(6)	-0.0004	400		5p	(3/2) <sup>+</sup> 3/2 <sup>+</sup> 1 <sup>+</sup> 2	6d		Ric		
4006.1651(12)	24954.473(7)	4006.1666(5)	-0.0015	1500		5p	(3F <sup>+</sup> 3 <sup>+</sup> 1F <sup>+</sup> 3	6d		Ric		
4014.2364(12)	24904.301(7)	4014.2342(4)	0.0018	870		5p	(3F <sup>+</sup> 3 <sup>+</sup> 1F <sup>+</sup> 3	7s		Ric		
4015.1963(12)	24898.345(8)	4015.1954(5)	0.0009	860		5p	(3F <sup>+</sup> 3 <sup>+</sup> 1F <sup>+</sup> 3	6d		Ric		
4016.4254(14)	24890.726(9)	4016.4218(6)	0.0036	1500		5p	(3F <sup>+</sup> 3 <sup>+</sup> 1F <sup>+</sup> 3	6d		Ric		
4030.3508(21)	24804.727(13)	4030.3525(7)	-0.0018	330		5p	(3/2) <sup>+</sup> 3/2 <sup>+</sup> 1 <sup>+</sup> 2	6d		Ric		
4032.6469(12)	24790.604(7)	4032.6470(3)	-0.0001	1600		5p	(5/2) <sup>+</sup> 5/2 <sup>+</sup> 1 <sup>+</sup> 2	7s		Ric		
4042.519(3)	24729.880(21)	4042.5473(7)	0.002	67		4d	(5/2) <sup>+</sup> 1/2 <sup>+</sup> 1 <sup>+</sup> 2	6p		Ric		
4043.4879(9)	24724.139(6)	4043.4858(5)	0.0021	27000		4p	(5/2) <sup>+</sup> 3/2 <sup>+</sup> 1 <sup>+</sup> 2	7s	1.14e+06	F_Re	O07	
4043.7515(14)	24722.527(13)	4043.7521(21)	0.0008	17000		5p	(5/2) <sup>+</sup> 3/2 <sup>+</sup> 1 <sup>+</sup> 2	7s		F_Re		
4053.6529(21)	24662.142(13)	4053.6521(4)	0.0008	3100		5p	(3/2) <sup>+</sup> 1/2 <sup>+</sup> 1 <sup>+</sup> 0	7s		Ric		
4065.0094(12)	24593.244(7)	4065.0090(4)	0.0004	1600		sp	(3F <sup>+</sup> 3 <sup>+</sup> 1D <sup>+</sup> 2	6d		Ric		



Table A1. Cont.

$\lambda_{\text{obs}}^a$ (Å)	$\sigma_{\text{obs}}^b$ (cm <sup>-1</sup> )	$\lambda_{\text{Ritz}}^c$ (Å)	$\Delta\lambda_{\text{obs-Ritz}}^d$ (Å)	$I_{\text{obs}}^d$ (arb. u.)	Char <sup>e</sup>	Lower Level	Upper Level	A (s <sup>-1</sup> )	Acc <sup>f</sup>	Line Ref. <sup>g</sup>	TP Ref. <sup>h</sup>	Notes <sup>b</sup>
4065.3723(22)	24591.049(13)	4065.3730(5)	-0.0007	230	5s	(3/2) <sup>1</sup> 3/2 <sub>1</sub>	sp	( <sup>1</sup> P) <sup>3</sup> P <sup>o</sup> -3D <sup>o</sup> -2		Ric		
4068.1058(12)	24457.526(7)	4068.1056(4)	0.0001	2000	sp	( <sup>1</sup> F) <sup>3</sup> P <sup>o</sup> -1D <sup>o</sup> -2	6d	(5/2) <sup>1</sup> 7/2 <sub>1</sub>		Ric		
4089.4787(13)	24446.094(8)	4089.4788(5)	-0.0001	480	sp	( <sup>1</sup> F) <sup>3</sup> P <sup>o</sup> -1D <sup>o</sup> -2	6d	(5/2) <sup>1</sup> 7/2 <sub>1</sub>		Ric		
4112.4816(13)	24309.359(8)	4112.4801(5)	0.0015	820	5s	(3/2) <sup>1</sup> 3/2 <sub>2</sub>	sp	( <sup>3</sup> P) <sup>3</sup> P <sup>o</sup> -3D <sup>o</sup> -2		Ric		
4118.2403(24)	24275.367(14)	4118.2398(5)	0.0005	57	5s	(3/2) <sup>1</sup> 3/2 <sub>1</sub>	sp	( <sup>3</sup> P) <sup>3</sup> P <sup>o</sup> -3D <sup>o</sup> -1		Ric		
4125.171(4)	24234.580(21)	4125.1717(8)	-0.0001	11	4d	(5/2) <sup>1</sup> 11/2 <sub>1</sub>	6p	(5/2) <sup>1</sup> 8/3/2 <sub>1</sub> <sup>o</sup> -2		Ric		
4125.9552(17)	24230.094(10)	4125.9352(9)	0.0001	65	5p	(3/2) <sup>1</sup> 11/2 <sub>1</sub>	6d	(5/2) <sup>1</sup> 11/2 <sub>1</sub>		Ric		
4131.3610(4)	24198.2729(25)	4131.3610(3)	0.0000	16000	5p	(5/2) <sup>1</sup> 7/2 <sub>1</sub>	7s	(5/2) <sup>1</sup> 9/2 <sub>1</sub>		F,Re		
4132.7116(21)	24190.365(12)	4132.7109(3)	0.0007	1000	5p	(3/2) <sup>1</sup> 5/2 <sub>1</sub>	7s	(3/2) <sup>1</sup> 5/2 <sub>1</sub>		Ric		
4141.2965(5)	24140.219(3)	4141.2968(4)	-0.0003	9700	5p	(3/2) <sup>1</sup> 5/2 <sub>2</sub>	7s	(3/2) <sup>1</sup> 5/2 <sub>2</sub>		Ric		
4143.0170(13)	24130.195(7)	4143.01624(20)	0.0007	2100	5p	(5/2) <sup>1</sup> 7/2 <sub>1</sub>	7s	(5/2) <sup>1</sup> 5/2 <sub>1</sub>		F,Re		
4147.8136(20)	24102.291(11)	4147.8131(6)	0.0004	190	4d	(5/2) <sup>1</sup> 3/2 <sub>2</sub>	6p	(5/2) <sup>1</sup> 5/2 <sub>1</sub> <sup>o</sup> -3		Ric		
4151.904(3)	24078.544(15)	4151.9059(6)	-0.002	47	4d	(5/2) <sup>1</sup> 9/2 <sub>1</sub>	6p	(5/2) <sup>1</sup> 5/2 <sub>1</sub> <sup>o</sup> -3		Ric		
4153.6234(13)	24068.679(7)	4153.6236(3)	-0.0003	3600	5p	(3/2) <sup>1</sup> 11/2 <sub>1</sub>	7s	(3/2) <sup>1</sup> 3/2 <sub>1</sub>		Ric		
4154.642(4)	24062.680(21)	4154.642(4)	-0.000	9	s <sup>2</sup>	3 <sub>1</sub> <sup>2</sup>	sp	( <sup>3</sup> F) <sup>3</sup> P <sup>o</sup> -5G <sup>o</sup> -2		Ric		
4161.13984(15)	24025.1034(9)	4161.13989(14)	-0.00005	17000	5p	(5/2) <sup>1</sup> 7/2 <sub>1</sub>	7s	(5/2) <sup>1</sup> 5/2 <sub>1</sub>		F,Re		
4162.2967(14)	24018.426(8)	4162.2967(4)	0.0000	3000	5p	(3/2) <sup>1</sup> 11/2 <sub>1</sub>	7s	(3/2) <sup>1</sup> 3/2 <sub>1</sub>		Ric		
4164.2826(10)	24006.972(6)	4164.2827(3)	-0.0001	8700	5p	(5/2) <sup>1</sup> 5/2 <sub>1</sub>	7s	(5/2) <sup>1</sup> 5/2 <sub>1</sub>		F,Re		
4165.67(15)	23999.0(9)	4165.775(3)	-0.10	3	d <sup>10</sup>	1 <sub>50</sub>	4s	3D <sub>1</sub>	2.1e-12	C+		X,MI
4166.8894(23)	23993.687(13)	4166.8874(5)	0.0010	350	5s	(3/2) <sup>1</sup> 3/2 <sub>2</sub>	sp	( <sup>3</sup> P) <sup>3</sup> P <sup>o</sup> -3D <sup>o</sup> -1		Ric		
4171.8513(5)	23953.419(3)	4171.8521(3)	-0.0007	10000	5p	(5/2) <sup>1</sup> 3/2 <sub>2</sub>	7s	(5/2) <sup>1</sup> 5/2 <sub>1</sub>		F,Re		
4176.1248(12)	23938.897(7)	4176.1247(3)	0.0001	1400	5p	(5/2) <sup>1</sup> 5/2 <sub>1</sub>	7s	(5/2) <sup>1</sup> 5/2 <sub>1</sub>		Ric		
4179.3117(4)	23919.4987(21)	4179.3113(3)	0.0003	12000	5p	(3/2) <sup>1</sup> 5/2 <sub>1</sub>	7s	(3/2) <sup>1</sup> 5/2 <sub>1</sub>		F,Re		
4185.149(4)	23887.280(21)	4185.1553(11)	-0.006	8	s <sup>2</sup>	1D <sub>2</sub>	sp	( <sup>1</sup> F) <sup>3</sup> P <sup>o</sup> -D <sup>o</sup> -3		M97		
4195.3590(16)	23829.148(9)	4195.3583(5)	0.0007	210	5p	(3/2) <sup>1</sup> 5/2 <sub>1</sub>	6d	(5/2) <sup>1</sup> 5/2 <sub>1</sub>		Ric		
4195.735(13)	23826.794(8)	4195.7740(7)	-0.0005	340	4d	(5/2) <sup>1</sup> 9/2 <sub>1</sub>	6p	(5/2) <sup>1</sup> 7/2 <sub>1</sub>		Ric		
4198.6561(13)	23810.436(8)	4198.6568(4)	-0.0007	240	5p	(3/2) <sup>1</sup> 5/2 <sub>1</sub>	6d	(5/2) <sup>1</sup> 7/2 <sub>1</sub>		Ric		
4199.435(4)	23806.020(21)	4199.4464(9)	-0.011	110	4d	(3/2) <sup>1</sup> 3/2 <sub>1</sub>	6p	(3/2) <sup>1</sup> 3/2 <sub>1</sub>		Ric		
4201.735(3)	23792.990(17)	4201.7309(10)	0.004	15	5p	(3/2) <sup>1</sup> 3/2 <sub>2</sub>	6d	(3/2) <sup>1</sup> 3/2 <sub>1</sub>		Ric		
4201.888(4)	23792.120(21)	4201.8827(16)	0.001	22	sp	( <sup>1</sup> P) <sup>3</sup> P <sup>o</sup> -3D <sup>o</sup> -3	8d	(5/2) <sup>1</sup> 9/2 <sub>1</sub>		Ric		
4207.672(3)	23759.417(16)	4207.5870(9)	0.085	15	sp	( <sup>1</sup> F) <sup>3</sup> P <sup>o</sup> -G <sup>o</sup> -4	5d	(3/2) <sup>1</sup> 5/2 <sub>1</sub>		Ric		
4209.321(4)	23750.110(21)	4209.3213(10)	-0.000	29	4d	(3/2) <sup>1</sup> 11/2 <sub>1</sub>	6p	(3/2) <sup>1</sup> 11/2 <sub>1</sub>		Ric		
4211.8649(8)	23735.766(5)	4211.86561(23)	-0.0007	11000	5p	(5/2) <sup>1</sup> 5/2 <sub>1</sub>	7s	(5/2) <sup>1</sup> 5/2 <sub>1</sub>		F,Re		
4212.315(3)	23733.232(16)	4212.3160(7)	-0.001	14	4d	(5/2) <sup>1</sup> 9/2 <sub>1</sub>	6p	(5/2) <sup>1</sup> 7/2 <sub>1</sub>		Ric		
4216.9124(13)	23707.356(7)	4216.9115(5)	0.0008	640	5p	(3/2) <sup>1</sup> 11/2 <sub>1</sub>	6d	(5/2) <sup>1</sup> 5/2 <sub>1</sub>		Ric		
4219.38(20)	23693.5(11)	4219.5840(6)	-0.20	340	4d	(5/2) <sup>1</sup> 3/2 <sub>2</sub>	sp	( <sup>1</sup> G) <sup>3</sup> P <sup>o</sup> -3F <sup>o</sup> -3		S96c		
4221.021(2)	23682.000(14)	4221.0276(5)	-0.000	69	5p	(3/2) <sup>1</sup> 5/2 <sub>1</sub>	6d	(5/2) <sup>1</sup> 3/2 <sub>1</sub>		Ric		
4223.8195(14)	23668.588(8)	4223.8197(6)	-0.0002	100	4d	(5/2) <sup>1</sup> 9/2 <sub>1</sub>	6p	( <sup>1</sup> G) <sup>3</sup> P <sup>o</sup> -3F <sup>o</sup> -3		Ric		
4224.344(4)	23665.650(21)	4224.3455(3)	-0.002	14	4d	(5/2) <sup>1</sup> 11/2 <sub>1</sub>	6p	( <sup>1</sup> G) <sup>3</sup> P <sup>o</sup> -3F <sup>o</sup> -3		Ric		
4225.1956(14)	23660.880(8)	4225.1967(6)	-0.0012	140	4d	(5/2) <sup>1</sup> 15/2 <sub>1</sub>	6p	(5/2) <sup>1</sup> 5/2 <sub>1</sub> <sup>o</sup> -3		Ric		
4227.9422(14)	23645.509(8)	4227.9397(5)	0.0025	7900	4p	3 <sub>1</sub> D <sup>o</sup> -3	s <sup>2</sup>	1G <sub>4</sub>	5.1e+05	B		C07

Table A1. Cont.

$\lambda_{\text{obs}}^a$ (Å)	$\sigma_{\text{obs}}^b$ (cm <sup>-1</sup> )	$\lambda_{\text{Ritz}}^c$ (Å)	$\Delta\lambda_{\text{obs-Ritz}}^d$ (Å)	$I_{\text{obs}}^d$ (arb. u.)	Char <sup>e</sup>	Lower Level	Upper Level	$A$ (s <sup>-1</sup> )	Acc <sup>f</sup>	Line Ref. <sup>g</sup>	TP Ref. <sup>h</sup>	Notes <sup>b</sup>
4230.4486(14)	23631.5000(8)	4230.4495(4)	-0.0009	4000	5p	(3/2) <sup>+</sup> [3/2] <sup>-</sup> 1	(3/2) <sup>+</sup> [3/2] <sup>-</sup> 2			Ric		
4232.8346(15)	23618.1800(8)	4232.8362(6)	-0.0016	130	5s	(3/2) <sup>+</sup> [3/2] <sup>-</sup> 2	( <sup>2</sup> F) <sup>+</sup> 3D <sup>-</sup> 3			Ric		
4239.4445(20)	23581.3561(11)	4239.4468(4)	-0.0023	7000	5p	(3/2) <sup>+</sup> [3/2] <sup>-</sup> 1	(3/2) <sup>+</sup> [3/2] <sup>-</sup> 1			F,Re		
4240.410(3)	23570.9851(14)	4240.4120(8)	-0.002	64	4d	( <sup>2</sup> F) <sup>+</sup> 3D <sup>-</sup> 5	(5/2) <sup>+</sup> [3/2] <sup>-</sup> 1			Ric		
4241.31(4)	23570.9722(1)	4241.271(3)	0.04	48	sp	( <sup>2</sup> F) <sup>+</sup> 3D <sup>-</sup> 5	(5/2) <sup>+</sup> [7/2] <sup>-</sup> 1			Ric		
4241.31(4)	23570.9722(1)	4241.3236(9)	-0.001	48	4d	(3/2) <sup>+</sup> [3/2] <sup>-</sup> 2	(3/2) <sup>+</sup> [3/2] <sup>-</sup> 1			Ric		
4243.2516(15)	23560.1199(8)	4243.2301(5)	0.0015	320	5p	(3/2) <sup>+</sup> [1/2] <sup>+</sup> 1	(5/2) <sup>+</sup> [3/2] <sup>-</sup> 1			Ric		X
4246.9860(20)	23539.4831(11)	4246.9715(4)	0.0145	390	5p	(3/2) <sup>+</sup> [5/2] <sup>-</sup> 1	(5/2) <sup>+</sup> [7/2] <sup>-</sup> 5			Ric		
4246.9860(20)	23539.4831(11)	4246.9497(7)	0.0003	390	4d	(3/2) <sup>+</sup> [1/2] <sup>+</sup> 1	(5/2) <sup>+</sup> [3/2] <sup>-</sup> 1			Ric		
4251.0194(15)	23517.149(8)	4251.0200(6)	-0.0006	300	4d	(5/2) <sup>+</sup> [1/2] <sup>+</sup> 4f	(3/2) <sup>+</sup> [3/2] <sup>-</sup> 1			Ric		
4254.630(4)	23497.190(21)	4254.6275(11)	0.003	12	4d	(3/2) <sup>+</sup> [7/2] <sup>-</sup> 4f	(3/2) <sup>+</sup> [5/2] <sup>-</sup> 2			R2hc		
4255.6348(14)	23491.644(8)	4255.6343(4)	0.0006	11000	4d	(5/2) <sup>+</sup> [1/2] <sup>+</sup> 4f	(3/2) <sup>+</sup> [3/2] <sup>-</sup> 2			Ric		
4256.846(4)	23484.960(21)	4256.8484(7)	-0.002	30	4d	(3/2) <sup>+</sup> [1/2] <sup>+</sup> 0	(5/2) <sup>+</sup> [1/2] <sup>+</sup> 1			Ric		
4267.611(4)	23425.720(21)	4267.6128(13)	-0.002	120	s <sup>2</sup>	1G <sub>4</sub>	( <sup>2</sup> F) <sup>+</sup> 3D <sup>-</sup> 5			Ric		
4268.103(4)	23425.020(21)	4268.1012(12)	0.002	18	s <sup>2</sup>	1G <sub>4</sub>	( <sup>2</sup> F) <sup>+</sup> 3D <sup>-</sup> 5			Ric		
4276.0484(9)	23379.499(15)	4276.0496(4)	-0.0012	8700	5p	( <sup>2</sup> F) <sup>+</sup> 3D <sup>-</sup> 5	(5/2) <sup>+</sup> [9/2] <sup>-</sup> 5			Ric		
4277.805(4)	23369.900(21)	4277.8016(6)	0.003	150	4d	(3/2) <sup>+</sup> [7/2] <sup>-</sup> 4f	(3/2) <sup>+</sup> [3/2] <sup>-</sup> 2			F,Re		
4279.9621(15)	23358.120(8)	4279.9594(3)	0.0028	5100	5p	( <sup>2</sup> F) <sup>+</sup> 3D <sup>-</sup> 5	(5/2) <sup>+</sup> [5/2] <sup>-</sup> 3			Ric		
4280.845(4)	23353.300(21)	4280.8437(6)	0.002	6	4d	(5/2) <sup>+</sup> [5/2] <sup>-</sup> 6	(5/2) <sup>+</sup> [5/2] <sup>-</sup> 6			Ric		
4281.838(3)	23347.889(15)	4281.8368(8)	0.001	29	5p	(3/2) <sup>+</sup> [1/2] <sup>+</sup> 1	(5/2) <sup>+</sup> [5/2] <sup>-</sup> 3			Ric		
4285.2433(13)	23329.334(7)	4285.2420(4)	0.0012	2000	5p	(3/2) <sup>+</sup> [3/2] <sup>-</sup> 2	(3/2) <sup>+</sup> [1/2] <sup>+</sup> 1			Ric		
4286.465(3)	23322.683(16)	4286.4615(7)	0.004	11	4d	(5/2) <sup>+</sup> [5/2] <sup>-</sup> 2	( <sup>2</sup> F) <sup>+</sup> 3D <sup>-</sup> 3			Ric		
4287.15(6)	23319.1(5)	4287.04500(10)	0.08	180	4d	(3/2) <sup>+</sup> [7/2] <sup>-</sup> 4f	(5/2) <sup>+</sup> [5/2] <sup>-</sup> 2			S9cc		
4287.779(3)	23315.537(17)	4287.7744(7)	0.005	11	4d	(3/2) <sup>+</sup> [7/2] <sup>-</sup> 4f	(5/2) <sup>+</sup> [5/2] <sup>-</sup> 2			Ric		
4291.084(3)	23297.580(16)	4291.0824(24)	0.002	640	4d	(5/2) <sup>+</sup> [5/2] <sup>-</sup> 2	( <sup>2</sup> F) <sup>+</sup> 3D <sup>-</sup> 4			Ric		
4292.4705(14)	23290.055(8)	4292.4694(3)	0.0011	9000	5s	(5/2) <sup>+</sup> [5/2] <sup>-</sup> 2	( <sup>2</sup> F) <sup>+</sup> 3D <sup>-</sup> 4			Ric		
4296.123(3)	23270.256(14)	4296.1187(5)	0.004	17	5p	( <sup>2</sup> F) <sup>+</sup> 3D <sup>-</sup> 3	(5/2) <sup>+</sup> [5/2] <sup>-</sup> 2			Ric		
4299.696(3)	23250.920(16)	4299.6946(6)	0.001	11	4d	(5/2) <sup>+</sup> [5/2] <sup>-</sup> 2	( <sup>2</sup> F) <sup>+</sup> 3D <sup>-</sup> 3			Ric		
4308.710(3)	23202.274(16)	4308.7114(9)	-0.001	28	4d	(3/2) <sup>+</sup> [1/2] <sup>+</sup> 1	( <sup>2</sup> F) <sup>+</sup> 3D <sup>-</sup> 3			Ric		
4320.7611(19)	23137.564(10)	4320.7616(7)	-0.0005	270	4d	(5/2) <sup>+</sup> [1/2] <sup>+</sup> 1	( <sup>2</sup> F) <sup>+</sup> 3D <sup>-</sup> 2			Ric		
4335.639(3)	23058.167(16)	4335.6353(9)	0.004	17	4d	(3/2) <sup>+</sup> [1/2] <sup>+</sup> 1	( <sup>2</sup> F) <sup>+</sup> 3D <sup>-</sup> 2			Ric		
4341.039(3)	23029.484(15)	4341.0414(14)	-0.002	17	4d	(5/2) <sup>+</sup> [5/2] <sup>-</sup> 2	( <sup>2</sup> F) <sup>+</sup> 3D <sup>-</sup> 3			Ric		
4343.152(4)	23018.280(21)	4343.1532(5)	-0.001	11	5p	(3/2) <sup>+</sup> [3/2] <sup>-</sup> 2	(5/2) <sup>+</sup> [5/2] <sup>-</sup> 2			Ric		
4344.700(4)	23010.080(21)	4344.6972(9)	0.003	6	4d	(3/2) <sup>+</sup> [5/2] <sup>-</sup> 2	(5/2) <sup>+</sup> [5/2] <sup>-</sup> 2			Ric		
4346.687(4)	22999.580(21)	4346.6883(5)	-0.001	240	5p	(3/2) <sup>+</sup> [3/2] <sup>-</sup> 2	(5/2) <sup>+</sup> [7/2] <sup>-</sup> 5			Ric		
4357.339(4)	22943.340(21)	4357.3345(6)	0.004	6	4d	(5/2) <sup>+</sup> [5/2] <sup>-</sup> 2	( <sup>2</sup> F) <sup>+</sup> 3D <sup>-</sup> 3			Ric		
4360.102(3)	22928.797(14)	4360.0973(17)	0.005	47	5s	( <sup>2</sup> F) <sup>+</sup> 3D <sup>-</sup> 2	( <sup>2</sup> F) <sup>+</sup> 3D <sup>-</sup> 2			Ric		
4365.3705(14)	22901.127(7)	4365.3697(3)	0.0008	7300	sp	(3/2) <sup>+</sup> [3/2] <sup>-</sup> 2	(5/2) <sup>+</sup> [5/2] <sup>-</sup> 2			Ric		
4373.460(3)	22898.770(15)	4373.4591(7)	0.001	18	5p	( <sup>2</sup> F) <sup>+</sup> 3D <sup>-</sup> 2	(5/2) <sup>+</sup> [3/2] <sup>-</sup> 2			Ric		
4375.58(5)	22897.3(3)	4375.690(3)	0.1	2000	d <sup>10</sup>	1S <sub>0</sub>	(5/2) <sup>+</sup> [5/2] <sup>-</sup> 2			A73,184	A08adj	X,E2
4378.3840(14)	22833.061(7)	4378.3848(3)	-0.0007	1500	sp	( <sup>2</sup> F) <sup>+</sup> 3D <sup>-</sup> 2	(5/2) <sup>+</sup> [7/2] <sup>-</sup> 3		D+	Ric		
4396.442(3)	22739.375(15)	4396.4196(6)	0.004	13	4d	(5/2) <sup>+</sup> [9/2] <sup>-</sup> 4f	(5/2) <sup>+</sup> [7/2] <sup>-</sup> 3		9.e-02	Ric		

Table A1. Cont.

$\lambda_{\text{obs}}^a$ (Å)	$\sigma_{\text{obs}}^b$ (cm <sup>-1</sup> )	$\lambda_{\text{Ritz}}^c$ (Å)	$\Delta\lambda_{\text{obs-Ritz}}^d$ (Å)	$I_{\text{obs}}^d$ (arb. u.)	Char <sup>e</sup>	Lower Level	Upper Level	A (s <sup>-1</sup> )	Acc <sup>f</sup>	Line Ref. <sup>g</sup>	TP Ref. <sup>h</sup>	Notes <sup>b</sup>
4402.363(3)	22708.694(16)	4402.3616(15)	0.002	33	5s	(5/2) <sup>2</sup> 5/2 <sub>2</sub>	sp	( <sup>3</sup> P) <sup>3</sup> P <sup>o</sup> 5D <sup>o</sup> 3		Ric		
4410.941(3)	22664.535(17)	4410.9371(9)	0.004	7	4d	(5/2) <sup>2</sup> 1/2 <sub>0</sub>	4f	(5/2) <sup>2</sup> 1/2 <sub>1</sub>		Ric		
4419.088(4)	22622.730(21)	4419.0825(3)	0.006	4d	4d	(5/2) <sup>2</sup> 3/2 <sub>1</sub>	6p	(5/2) <sup>2</sup> 3/2 <sub>1</sub>		Ric		
4422.583(3)	22604.871(16)	4422.5816(15)	0.002	15	5s	(5/2) <sup>2</sup> 5/2 <sub>2</sub>	sp	( <sup>3</sup> P) <sup>3</sup> P <sup>o</sup> 5D <sup>o</sup> 1		Ric		
4435.693(3)	22538.066(15)	4435.6906(4)	0.002	80	4d	(5/2) <sup>2</sup> 3/2 <sub>1</sub>	4f	(5/2) <sup>2</sup> 3/2 <sub>1</sub>		Ric		
4440.8836(15)	22511.721(8)	4440.8827(4)	0.0009	520	4d	(5/2) <sup>2</sup> 3/2 <sub>1</sub>	4f	(5/2) <sup>2</sup> 3/2 <sub>1</sub>		Ric		
4441.709(14)	22507.54(7)	4441.7193(7)	-0.011	180	sp	( <sup>3</sup> F) <sup>3</sup> P <sup>o</sup> 3D <sup>o</sup> 3	5d	(3/2) <sup>2</sup> 17/2 <sub>1</sub>		Ric		
4444.8314(14)	22489.172(7)	4444.8307(3)	0.0007	1200	4d	(5/2) <sup>2</sup> 3/2 <sub>1</sub>	4f	(5/2) <sup>2</sup> 3/2 <sub>1</sub>		Ric		
4462.6902(16)	22401.721(18)	4462.6875(5)	0.0027	1600	4d	(5/2) <sup>2</sup> 19/2 <sub>1</sub>	4f	(5/2) <sup>2</sup> 19/2 <sub>1</sub>		W93		
4485.280	22288.90	4485.2800(6)						( <sup>3</sup> F) <sup>3</sup> P <sup>o</sup> 3D <sup>o</sup> 2		Ric		
4495.356(3)	22238.942(15)	4495.3577(8)	-0.002	38	sp	( <sup>3</sup> P) <sup>3</sup> P <sup>o</sup> 3C <sup>o</sup> 3	5d	(3/2) <sup>2</sup> 17/2 <sub>1</sub>	6.3e+05	F,Re	H71,N88	L
4505.9982(6)	22186.418(4)	4505.9996(4)	-0.0013	11000	4p	(5/2) <sup>2</sup> 15/2 <sub>2</sub>	5s	(5/2) <sup>2</sup> 15/2 <sub>2</sub>		Ric		
4515.5194(15)	22139.637(7)	4515.5195(3)	-0.0001	960	4d	(3/2) <sup>2</sup> 15/2 <sub>1</sub>	7s	(3/2) <sup>2</sup> 15/2 <sub>1</sub>		Ric		
4516.0192(15)	22137.040(7)	4516.0489(4)	-0.0007	2700	5p	(3/2) <sup>2</sup> 5/2 <sub>1</sub>	7s	(3/2) <sup>2</sup> 5/2 <sub>1</sub>		Ric		
4529.983(3)	22068.951(15)	4529.9803(3)	0.002	70	5p	(3/2) <sup>2</sup> 5/2 <sub>1</sub>	7s	(3/2) <sup>2</sup> 5/2 <sub>1</sub>		Ric		
4533.814(4)	22050.300(21)	4533.8122(3)	0.002	54	4d	(5/2) <sup>2</sup> 15/2 <sub>2</sub>	4f	(5/2) <sup>2</sup> 15/2 <sub>2</sub>		Ric		
4541.0325(15)	22015.251(7)	4541.0337(4)	-0.0013	6900	5p	(3/2) <sup>2</sup> 11/2 <sub>1</sub>	7s	(3/2) <sup>2</sup> 11/2 <sub>1</sub>		Ric		
4542.15(4)	22009.82(19)	4542.1167(8)	0.04	390	4d	(5/2) <sup>2</sup> 15/2 <sub>2</sub>	4f	(5/2) <sup>2</sup> 15/2 <sub>2</sub>		Ric		
4546.133(3)	21989.099(12)	4546.1333(6)	-0.002	410	4d	(5/2) <sup>2</sup> 13/2 <sub>1</sub>	sp	( <sup>3</sup> P) <sup>3</sup> P <sup>o</sup> 1D <sup>o</sup> 2		Ric		
4551.807(3)	21963.141(13)	4551.8059(8)	-0.000	260	sp	( <sup>3</sup> F) <sup>3</sup> P <sup>o</sup> 3D <sup>o</sup> 2	5d	(3/2) <sup>2</sup> 15/2 <sub>1</sub>		Ric		
4555.921(16)	21943.307(3)	4555.9193(4)	0.0018	18000	4p	(3/2) <sup>2</sup> 17/2 <sub>1</sub>	sp	( <sup>3</sup> F) <sup>3</sup> P <sup>o</sup> 3P <sup>o</sup> 2		Ric		
4557.3077(15)	21935.668(7)	4557.3079(4)	-0.0002	1100	4d	(5/2) <sup>2</sup> 17/2 <sub>1</sub>	4f	(5/2) <sup>2</sup> 17/2 <sub>1</sub>	7.1e+05	F,Re	H71,N88	L
4558.7(5)	21929.9(24)	4558.949(4)	-0.2	3000	d <sup>10</sup>	( <sup>3</sup> P) <sup>3</sup> P <sup>o</sup> 3D <sup>o</sup> 2	4f	(3/2) <sup>2</sup> 17/2 <sub>1</sub>		Ric		
4575.180(7)	21850.94(3)	4575.1748(4)	0.005	550	4d	(5/2) <sup>2</sup> 17/2 <sub>1</sub>	4f	(5/2) <sup>2</sup> 17/2 <sub>1</sub>		A73		X,HF
4575.180(7)	21850.94(3)	4575.1871(7)	-0.007	550	4d	(5/2) <sup>2</sup> 17/2 <sub>1</sub>	4f	(5/2) <sup>2</sup> 17/2 <sub>1</sub>		Ric		
4575.6529(15)	21848.681(7)	4575.6532(3)	-0.0003	850	sp	( <sup>3</sup> F) <sup>3</sup> P <sup>o</sup> 3D <sup>o</sup> 2	10s	(5/2) <sup>2</sup> 15/2 <sub>1</sub>		Ric		
4584.899(3)	21804.623(12)	4584.8994(3)	-0.001	600	4d	( <sup>3</sup> F) <sup>3</sup> P <sup>o</sup> 3D <sup>o</sup> 2	5d	(5/2) <sup>2</sup> 13/2 <sub>1</sub>		Ric		
4586.274(3)	21798.084(13)	4586.2719(3)	0.002	300	4d	(5/2) <sup>2</sup> 17/2 <sub>1</sub>	4f	(5/2) <sup>2</sup> 17/2 <sub>1</sub>		Ric		
4588.1661(15)	21789.095(7)	4588.1667(4)	-0.0006	620	5p	(3/2) <sup>2</sup> 15/2 <sub>1</sub>	7s	(3/2) <sup>2</sup> 15/2 <sub>1</sub>		Ric		
4589.401(3)	21782.285(12)	4589.4035(8)	-0.003	220	4d	(5/2) <sup>2</sup> 15/2 <sub>2</sub>	4f	(5/2) <sup>2</sup> 15/2 <sub>2</sub>		Ric		
4594.330(3)	21759.863(13)	4594.3638(14)	-0.034	200	sp	( <sup>3</sup> F) <sup>3</sup> P <sup>o</sup> 3F <sup>o</sup> 3	6s	(3/2) <sup>2</sup> 13/2 <sub>1</sub>		Ric		
4594.436(3)	21759.338(15)	4594.4374(3)	-0.001	130	4d	(5/2) <sup>2</sup> 17/2 <sub>1</sub>	4f	(5/2) <sup>2</sup> 17/2 <sub>1</sub>		Ric		
4596.9056(15)	21747.671(7)	4596.9063(5)	-0.0007	4800	4d	(5/2) <sup>2</sup> 17/2 <sub>1</sub>	4f	(5/2) <sup>2</sup> 17/2 <sub>1</sub>		Ric		
4597.9473(15)	21742.744(7)	4597.9466(3)	0.0007	3200	4d	(5/2) <sup>2</sup> 15/2 <sub>2</sub>	4f	(5/2) <sup>2</sup> 15/2 <sub>2</sub>		Ric		
4606.5041(21)	21702.356(10)	4606.4944(5)	0.0097	730	4d	(5/2) <sup>2</sup> 17/2 <sub>1</sub>	4f	(5/2) <sup>2</sup> 17/2 <sub>1</sub>		Ric		X
4608.4661(16)	21693.117(7)	4608.4662(5)	-0.0001	3100	4d	(5/2) <sup>2</sup> 17/2 <sub>1</sub>	4f	(5/2) <sup>2</sup> 17/2 <sub>1</sub>		Ric		
4609.416(3)	21688.646(14)	4609.3996(6)	0.016	560	sp	( <sup>3</sup> F) <sup>3</sup> P <sup>o</sup> 3D <sup>o</sup> 2	5d	(5/2) <sup>2</sup> 19/2 <sub>1</sub>		Ric		X
4619.659(3)	21640.559(15)	4619.6507(6)	0.008	82	4d	(5/2) <sup>2</sup> 15/2 <sub>2</sub>	4f	(5/2) <sup>2</sup> 15/2 <sub>2</sub>		Ric		
4625.097(3)	21615.114(13)	4625.1004(5)	-0.003	2100	4d	(5/2) <sup>2</sup> 15/2 <sub>2</sub>	4f	(5/2) <sup>2</sup> 15/2 <sub>2</sub>		Ric		

Table A1. Cont.

$\lambda_{\text{obs}}^a$ (Å)	$\sigma_{\text{obs}}^b$ (cm <sup>-1</sup> )	$\lambda_{\text{Ritz}}^c$ (Å)	$\Delta\lambda^{\text{obs-Ritz}}$ (Å)	$I_{\text{obs}}^d$ (arb. u.)	Char <sup>e</sup>	Lower Level	Upper Level	A (s <sup>-1</sup> )	Acc <sup>f</sup>	Line Ref. <sup>g</sup>	TP Ref. <sup>h</sup>	Notes <sup>h</sup>
4631.801(3)	21553.829(16)	4631.807(7)	-0.007	90	4d	(3/2) <sup>3</sup> F <sup>o</sup> 2/2 <sub>3</sub>	sp	( <sup>1</sup> G) <sup>3</sup> p <sup>-3</sup> F <sup>o</sup> <sub>3</sub>		Ric		
4635.260(3)	21567.722(12)	4635.259(16)	0.000	230	4d	(5/2) <sup>3</sup> F <sup>o</sup> 2/2 <sub>4</sub>	sp	( <sup>1</sup> G) <sup>3</sup> p <sup>-3</sup> F <sup>o</sup> <sub>4</sub>		Ric		
4639.583(16)	21547.616(8)	4639.583(9)	0.0019	1100	4d	(5/2) <sup>3</sup> F <sup>o</sup> 3/2 <sub>4</sub>	sp	( <sup>1</sup> G) <sup>3</sup> p <sup>-3</sup> F <sup>o</sup> <sub>2</sub>		Rinc		
4647.012(5)	21513.180(21)	4647.012(12)	-0.000	950	4d	(5/2) <sup>3</sup> F <sup>o</sup> 1/2 <sub>4</sub>	sp	( <sup>1</sup> G) <sup>3</sup> p <sup>-3</sup> F <sup>o</sup> <sub>2</sub>		Ric		
4649.2705(16)	21502.730(7)	4649.27084(23)	-0.0003	6700	4d	(5/2) <sup>3</sup> F <sup>o</sup> 1/2 <sub>4</sub>	4f	(5/2) <sup>3</sup> F <sup>o</sup> 1/2 <sub>4</sub>		Ric		
4660.304(17)	21451.820(8)	4660.3070(7)	-0.0026	5600	4d	(5/2) <sup>3</sup> F <sup>o</sup> 1/2 <sub>0</sub>	4f	(5/2) <sup>3</sup> F <sup>o</sup> 1/2 <sub>4</sub>		Ric		
4661.3627(16)	21446.950(7)	4661.3620(3)	0.0007	7100	4d	(5/2) <sup>3</sup> F <sup>o</sup> 1/2 <sub>1</sub>	4f	(5/2) <sup>3</sup> F <sup>o</sup> 1/2 <sub>1</sub>		Ric		
4662.654(5)	21441.100(12)	4662.6473(11)	0.007	13000	4d	(5/2) <sup>3</sup> F <sup>o</sup> 1/2 <sub>1</sub>	sp	( <sup>1</sup> D) <sup>3</sup> p <sup>-5</sup> S <sup>o</sup> 2		Ric		
4667.315(2)	21419.599(11)	4667.3119(12)	0.003	11000	4d	(5/2) <sup>3</sup> F <sup>o</sup> 1/2 <sub>1</sub>	sp	( <sup>1</sup> G) <sup>3</sup> p <sup>-3</sup> H <sup>o</sup> 5		Ric		
4671.7016(2)	21399.4867(11)	4671.70176(20)	-0.0002	29000	4d	(5/2) <sup>3</sup> F <sup>o</sup> 1/2 <sub>1</sub>	4f	(5/2) <sup>3</sup> F <sup>o</sup> 1/2 <sub>1</sub>		F_Re	TW	L
4673.5772(5)	21390.8989(25)	4673.5744(5)	-0.0002	20000	4d	(5/2) <sup>3</sup> F <sup>o</sup> 1/2 <sub>1</sub>	4f	(5/2) <sup>3</sup> F <sup>o</sup> 1/2 <sub>1</sub>		F_Re	TW	L
4681.9938(5)	21352.4459(22)	4681.9935(3)	0.0003	36000	4d	(5/2) <sup>3</sup> F <sup>o</sup> 1/2 <sub>1</sub>	4f	(5/2) <sup>3</sup> F <sup>o</sup> 1/2 <sub>1</sub>		F_Re	TW	L
4687.7662(18)	21326.153(8)	4687.7648(4)	0.0014	3000	5p	(3/2) <sup>3</sup> F <sup>o</sup> 3/2 <sub>2</sub>	7s	(5/2) <sup>3</sup> F <sup>o</sup> 15/2 <sub>2</sub>		Ric		
4702.125(3)	21261.032(13)	4702.1291(9)	-0.004	550	4d	(5/2) <sup>3</sup> F <sup>o</sup> 3/2 <sub>2</sub>	sp	( <sup>3</sup> P) <sup>3</sup> p <sup>-1</sup> D <sup>o</sup> 2		Ric		
4737.903(4)	21100.456(16)	4737.9023(11)	0.006	170	4d	(3/2) <sup>3</sup> F <sup>o</sup> 3/2 <sub>1</sub>	6p	(5/2) <sup>3</sup> F <sup>o</sup> 15/2 <sub>2</sub>		Ric		
4744.588(5)	21070.751(11)	4744.5892(8)	-0.001	520	5p	( <sup>1</sup> F) <sup>3</sup> p <sup>-5</sup> D <sup>o</sup> 1	5d	(5/2) <sup>3</sup> F <sup>o</sup> 15/2 <sub>2</sub>		Ric		
4753.4684(16)	21031.389(7)	4753.4691(7)	-0.0007	2100	4d	(5/2) <sup>3</sup> F <sup>o</sup> 1/2 <sub>4</sub>	sp	( <sup>1</sup> G) <sup>3</sup> p <sup>-3</sup> H <sup>o</sup> 4		Ric		
4758.4334(9)	21009.445(4)	4758.4334(7)	0.0000	15000	4p	<sup>3</sup> P <sub>1</sub>	<sup>3</sup> P <sub>0</sub>		1.3e+06	C		H71,N88
4765.913(3)	20976.472(14)	4765.9115(6)	0.002	62	sp	( <sup>3</sup> F) <sup>3</sup> p <sup>-3</sup> F <sup>o</sup> 3	5d	(3/2) <sup>3</sup> F <sup>o</sup> 15/2 <sub>3</sub>		Ric		
4766.7392(16)	20972.837(7)	4766.7394(9)	-0.0002	4500	4d	(5/2) <sup>3</sup> F <sup>o</sup> 1/2 <sub>1</sub>	sp	( <sup>3</sup> P) <sup>3</sup> p <sup>-3</sup> P <sup>o</sup> 0		Ric		
4772.9651(17)	20945.481(7)	4772.9656(5)	-0.0005	590	4d	(3/2) <sup>3</sup> F <sup>o</sup> 1/2 <sub>1</sub>	4f	(3/2) <sup>3</sup> F <sup>o</sup> 15/2 <sub>2</sub>		Ric		X
4781.0855(17)	20909.907(8)	4781.0769(8)	0.0086	670	sp	( <sup>3</sup> P) <sup>3</sup> p <sup>-3</sup> P <sup>o</sup> 1	5d	(3/2) <sup>3</sup> F <sup>o</sup> 3/2 <sub>2</sub>		Ric		
4792.769(5)	20859.194(14)	4792.7117(21)	-0.002	450	5s	(3/2) <sup>3</sup> F <sup>o</sup> 3/2 <sub>1</sub>	sp	( <sup>1</sup> P) <sup>3</sup> p <sup>-5</sup> D <sup>o</sup> 2		Ric		
4797.306(3)	20839.208(14)	4797.3080(18)	-0.002	150	5s	(5/2) <sup>3</sup> F <sup>o</sup> 1/2 <sub>3</sub>	sp	( <sup>1</sup> D) <sup>3</sup> p <sup>-5</sup> D <sup>o</sup> 2		Ric		
4800.112(3)	20827.027(11)	4800.1106(8)	0.001	590	4d	( <sup>1</sup> F) <sup>3</sup> p <sup>-3</sup> D <sup>o</sup> 1	5d	(3/2) <sup>3</sup> F <sup>o</sup> 3/2 <sub>1</sub>		Ric		
4800.584(3)	20824.980(14)	4800.5808(9)	0.003	370	4d	(5/2) <sup>3</sup> F <sup>o</sup> 15/2 <sub>2</sub>	sp	( <sup>1</sup> G) <sup>3</sup> p <sup>-3</sup> F <sup>o</sup> 2		Rinc		
4805.6557(19)	20803.001(8)	4805.6527(6)	0.0030	3600	4d	(5/2) <sup>3</sup> F <sup>o</sup> 3/2 <sub>2</sub>	sp	( <sup>3</sup> F) <sup>3</sup> p <sup>-3</sup> F <sup>o</sup> 2		Ric		
4807.0463(17)	20796.983(7)	4807.0453(8)	0.0000	7000	4d	(5/2) <sup>3</sup> F <sup>o</sup> 1/2 <sub>1</sub>	4f	(3/2) <sup>3</sup> F <sup>o</sup> 3/2 <sub>1</sub>		Ric		
4811.1487(21)	20779.250(9)	4811.1475(6)	0.0012	1000	4d	(5/2) <sup>3</sup> F <sup>o</sup> 1/2 <sub>1</sub>	sp	( <sup>3</sup> F) <sup>3</sup> p <sup>-3</sup> F <sup>o</sup> 3		Ric		
4812.9476(5)	20771.483(22)	4812.9474(4)	0.0003	36000	4d	(3/2) <sup>3</sup> F <sup>o</sup> 1/2 <sub>1</sub>	4f	(3/2) <sup>3</sup> F <sup>o</sup> 3/2 <sub>2</sub>		F_Re	TW	
4814.868(4)	20763.199(16)	4814.868(4)	0.000	310	5s	(5/2) <sup>3</sup> F <sup>o</sup> 1/2 <sub>3</sub>	sp	( <sup>1</sup> D) <sup>3</sup> p <sup>-3</sup> F <sup>o</sup> 4		Ric		
4820.269(3)	20739.934(15)	4820.2672(6)	0.002	160	5p	( <sup>1</sup> F) <sup>3</sup> p <sup>-3</sup> F <sup>o</sup> 3	5d	(5/2) <sup>3</sup> F <sup>o</sup> 17/2 <sub>4</sub>		Ric		
4829.3349(17)	20701.001(7)	4829.3340(3)	0.0009	1100	4d	(5/2) <sup>3</sup> F <sup>o</sup> 1/2 <sub>5</sub>	sp	(5/2) <sup>3</sup> F <sup>o</sup> 19/2 <sub>4</sub>		Ric		
4832.2454(17)	20688.533(7)	4832.2439(5)	0.0014	14000	4p	<sup>3</sup> P <sub>1</sub>	<sup>3</sup> P <sub>1</sub>		2.5e+05	C		H71,N88
4833.761(3)	20682.046(12)	4833.7603(9)	0.001	1000	4d	(3/2) <sup>3</sup> F <sup>o</sup> 1/2 <sub>1</sub>	s <sup>2</sup>	( <sup>3</sup> F) <sup>3</sup> p <sup>-3</sup> D <sup>o</sup> 1		Ric		
4834.673(3)	20678.146(12)	4834.6703(18)	0.002	440	5s	(3/2) <sup>3</sup> F <sup>o</sup> 3/2 <sub>2</sub>	sp	( <sup>3</sup> P) <sup>3</sup> p <sup>-5</sup> D <sup>o</sup> 3		Ric		
4836.709(2)	20669.054(11)	4836.7082(8)	0.001	790	sp	( <sup>3</sup> P) <sup>3</sup> p <sup>-3</sup> D <sup>o</sup> 3	5d	(5/2) <sup>3</sup> F <sup>o</sup> 17/2 <sub>4</sub>		Ric		
4837.434(5)	20666.341(15)	4837.4350(20)	-0.001	360	4d	(5/2) <sup>3</sup> F <sup>o</sup> 1/2 <sub>10</sub>	sp	( <sup>3</sup> P) <sup>3</sup> p <sup>-1</sup> P <sup>o</sup> 1		R2nc		
4840.1833(17)	20654.604(7)	4840.1829(8)	0.0005	1100	4d	(3/2) <sup>3</sup> F <sup>o</sup> 1/2 <sub>3</sub>	6p	(5/2) <sup>3</sup> F <sup>o</sup> 17/2 <sub>3</sub>		Ric		
4841.832(3)	20647.573(15)	4841.8320(24)	-0.000	91	4f	(5/2) <sup>3</sup> F <sup>o</sup> 1/2 <sub>3</sub>	8g	(5/2) <sup>3</sup> F <sup>o</sup> 11/2 <sub>16</sub>		R2nc		
4847.5822(17)	20625.930(7)	4847.5823(8)	-0.0000	1500	4d	(5/2) <sup>3</sup> F <sup>o</sup> 1/2 <sub>1</sub>	sp	( <sup>3</sup> P) <sup>3</sup> p <sup>-3</sup> P <sup>o</sup> 1		F_Re		
4851.2625(11)	20607.434(5)	4851.2617(4)	0.0008	12000	4d	(5/2) <sup>3</sup> F <sup>o</sup> 1/2 <sub>4</sub>	4f	(5/2) <sup>3</sup> F <sup>o</sup> 19/2 <sub>4</sub>		D+		

Table A1. Cont.

$\lambda_{\text{obs}}^a$ (Å)	$\sigma_{\text{obs}}^b$ (cm <sup>-1</sup> )	$\lambda_{\text{ritz}}^c$ (Å)	$\Delta\lambda_{\text{obs-ritz}}^d$ (Å)	$I_{\text{obs}}^d$ (arb. u.)	Char <sup>e</sup>	Lower Level	Upper Level	A (s <sup>-1</sup> )	Acc <sup>f</sup>	Line Ref. <sup>g</sup>	TP Ref. <sup>h</sup>	Notes <sup>b</sup>
4854.96733(18)	20591.6237(7)	4854.96733(17)	-0.00011	34000	4d	(5/2) <sup>-3</sup> /2]s	(5/2) <sup>-3</sup> /2]s	3.5e+07	D+	F_Re	TW	L
4859.068(7)	20574.33(3)	4859.0673(19)	0.001	97	5s	(3/2) <sup>-3</sup> /2]s	(3/2) <sup>-3</sup> /2]s			Ric		
4861.5612(18)	20563.780(8)	4861.56049(20)	0.0008	3600	4d	(5/2) <sup>-3</sup> /2]s	(5/2) <sup>-3</sup> /2]s			Ric		
4866.254(3)	20544.951(12)	4866.2530(8)	-0.001	700	sp	(3/2) <sup>-3</sup> /2]s	(3/2) <sup>-3</sup> /2]s			Ric		
4873.3056(17)	20514.223(7)	4873.3035(5)	0.0021	9900	4d	(5/2) <sup>-3</sup> /2]s	(5/2) <sup>-3</sup> /2]s	2.4e+07	D+	F_Re	TW	
4877.151(3)	20498.050(13)	4877.1492(3)	0.002	100	4d	(5/2) <sup>-3</sup> /2]s	(5/2) <sup>-3</sup> /2]s			Ric		
4883.2352(17)	20475.510(7)	4883.2351(4)	0.0001	2900	4d	(3/2) <sup>-3</sup> /2]s	(3/2) <sup>-3</sup> /2]s			Ric		
4883.7832(17)	20470.213(7)	4883.7825(3)	0.0007	2900	4d	(5/2) <sup>-3</sup> /2]s	(5/2) <sup>-3</sup> /2]s			Ric		
4889.7005(17)	20445.441(7)	4889.6998(5)	0.0008	12000	4p	(5/2) <sup>-3</sup> /2]s	(5/2) <sup>-3</sup> /2]s	1.9e+05	C	Ric	H71,N88	
4893.506(3)	20429.543(11)	4893.5089(5)	-0.003	770	4d	(3/2) <sup>-3</sup> /2]s	(3/2) <sup>-3</sup> /2]s			Ric		
4896.414(3)	20417.408(14)	4896.4163(10)	-0.002	1900	4d	(3/2) <sup>-3</sup> /2]s	(3/2) <sup>-3</sup> /2]s			Ric		
4900.472(3)	20400.501(11)	4900.4712(9)	0.001	920	sp	(3/2) <sup>-3</sup> /2]s	(3/2) <sup>-3</sup> /2]s			Ric		
4901.42635(21)	20396.5291(9)	4901.42634(15)	0.00002	26000	4d	(5/2) <sup>-3</sup> /2]s	(5/2) <sup>-3</sup> /2]s	6.2e+07	D+	F_Re	TW	X
4904.534(4)	20383.605(16)	4904.5146(21)	0.020	110	4d	(5/2) <sup>-3</sup> /2]s	(5/2) <sup>-3</sup> /2]s			Ric		
4905.768(3)	20378.478(11)	4905.7657(5)	0.001	580	4d	(3/2) <sup>-3</sup> /2]s	(3/2) <sup>-3</sup> /2]s			Ric		
4906.5663(3)	20375.1629(11)	4906.56612(16)	0.0002	21000	4d	(5/2) <sup>-3</sup> /2]s	(5/2) <sup>-3</sup> /2]s	4.4e+07	D+	F_Re	TW	
4907.1427(24)	20372.770(10)	4907.1424(4)	0.0002	1000	4d	(5/2) <sup>-3</sup> /2]s	(5/2) <sup>-3</sup> /2]s			Ric		
4908.2819(24)	20368.041(10)	4908.2838(8)	-0.0019	970	4d	(5/2) <sup>-3</sup> /2]s	(5/2) <sup>-3</sup> /2]s			F_Re		
4909.0397(13)	20364.897(5)	4909.0390(5)	0.0007	6100	4d	(5/2) <sup>-3</sup> /2]s	(5/2) <sup>-3</sup> /2]s			F_Re		
4909.7335(12)	20362.01913(10)	4909.733510(20)	0.00000	16000	4d	(5/2) <sup>-3</sup> /2]s	(5/2) <sup>-3</sup> /2]s	2.04e+08	B+	F_Re	C84	L
4912.5645(5)	20351.1138(21)	4912.5644(3)	0.0001	17000	4d	(5/2) <sup>-3</sup> /2]s	(5/2) <sup>-3</sup> /2]s			F_Re		
4912.91989(16)	20348.813(17)	4912.91987(14)	0.0002	29000	4d	(5/2) <sup>-3</sup> /2]s	(5/2) <sup>-3</sup> /2]s	6.0e+07	D+	F_Re	TW	
4915.8321(17)	20336.738(7)	4915.8312(4)	0.0009	11000	4d	(3/2) <sup>-3</sup> /2]s	(3/2) <sup>-3</sup> /2]s	2.5e+07	D+	F_Re	TW	
4918.1079(21)	20327.348(9)	4918.1061(4)	0.0019	2400	4d	(5/2) <sup>-3</sup> /2]s	(5/2) <sup>-3</sup> /2]s			Ric		
4918.3779(5)	20326.2320(20)	4918.3778(4)	0.0001	54000	4d	(5/2) <sup>-3</sup> /2]s	(5/2) <sup>-3</sup> /2]s	2.9e+08	C	F_Re	H71	
4920.0348(12)	20319.387(5)	4920.0345(4)	0.0003	6800	4d	(5/2) <sup>-3</sup> /2]s	(5/2) <sup>-3</sup> /2]s			F_Re		
4921.4627(21)	20313.492(9)	4921.4666(12)	-0.0039	5900	4d	(5/2) <sup>-3</sup> /2]s	(5/2) <sup>-3</sup> /2]s			F_Re		
4926.4228(5)	20293.0397(22)	4926.4232(3)	-0.0004	26000	4d	(5/2) <sup>-3</sup> /2]s	(5/2) <sup>-3</sup> /2]s	9.e+07	D+	F_Re	TW	
4926.811(4)	20291.440(17)	4926.8186(15)	-0.007	740	sp	(3/2) <sup>-3</sup> /2]s	(3/2) <sup>-3</sup> /2]s			Ric		
4927.860(3)	20287.121(14)	4927.8590(12)	0.001	830	4d	(5/2) <sup>-3</sup> /2]s	(5/2) <sup>-3</sup> /2]s			Ric		
4930.713(5)	20275.383(11)	4930.7110(8)	0.002	620	sp	(3/2) <sup>-3</sup> /2]s	(3/2) <sup>-3</sup> /2]s			Ric		
4931.55496(20)	20271.9213(8)	4931.55305(16)	-0.00009	28000	4d	(5/2) <sup>-3</sup> /2]s	(5/2) <sup>-3</sup> /2]s	7.1e+07	D+	F_Re	TW	
4931.6982(5)	20271.3325(20)	4931.6981(4)	0.0001	14000	4d	(5/2) <sup>-3</sup> /2]s	(5/2) <sup>-3</sup> /2]s	1.9e+08	C	F_Re	H71	L
4933.0777(24)	20265.664(10)	4933.0745(5)	0.0032	1100	4d	(5/2) <sup>-3</sup> /2]s	(5/2) <sup>-3</sup> /2]s			Ric		
4937.22029(23)	20248.660(19)	4937.22031(22)	-0.00002	26000	4d	(3/2) <sup>-3</sup> /2]s	(3/2) <sup>-3</sup> /2]s	1.1e+08	D+	F_Re	TW	
4937.516(3)	20247.449(11)	4937.5188(4)	-0.003	1100	4d	(5/2) <sup>-3</sup> /2]s	(5/2) <sup>-3</sup> /2]s			Ric		
4937.970(4)	20245.5693(16)	4937.9737(21)	-0.003	16000	4d	(5/2) <sup>-3</sup> /2]s	(5/2) <sup>-3</sup> /2]s	2.8e+07	D+	F_Re	TW	
4939.648(3)	20238.709(11)	4939.6526(6)	-0.005	1200	4d	(3/2) <sup>-3</sup> /2]s	(3/2) <sup>-3</sup> /2]s			Ric		
4940.0695(17)	20236.982(7)	4940.0693(6)	0.0002	4700	4d	(5/2) <sup>-3</sup> /2]s	(5/2) <sup>-3</sup> /2]s			Ric		
4940.912(8)	20233.53(3)	4940.9095(20)	0.003	130	5s	(1/2) <sup>-3</sup> /2]s	(1/2) <sup>-3</sup> /2]s			Ric		
4943.0240(7)	20224.886(3)	4924.0250(4)	-0.0010	20000	4d	(5/2) <sup>-3</sup> /2]s	(5/2) <sup>-3</sup> /2]s	4.0e+07	D+	F_Re	TW	
4949.4750(18)	20198.526(7)	4949.4735(4)	0.0015	3700	4d	(5/2) <sup>-3</sup> /2]s	(5/2) <sup>-3</sup> /2]s			Ric		
4951.4463(18)	20190.484(7)	4951.4464(6)	-0.0000	4200	4d	(3/2) <sup>-3</sup> /2]s	(3/2) <sup>-3</sup> /2]s			F_Re		

Table A1. Cont.

$\lambda_{\text{obs}}^a$ (Å)	$\sigma_{\text{obs}}^b$ (cm <sup>-1</sup> )	$\lambda_{\text{Ritz}}^c$ (Å)	$\Delta\lambda_{\text{obs-Ritz}}^d$ (Å)	$I_{\text{obs}}^d$ (arb. u.)	Char <sup>e</sup>	Lower Level	Upper Level	A (s <sup>-1</sup> )	Acc <sup>f</sup>	Line Ref. <sup>g</sup>	TP Ref. <sup>g</sup>	Notes <sup>h</sup>
4951.6184(14)	20189.783(6)	4951.6201(3)	-0.0016	12000	4d	(5/2) <sup>-1</sup> 5/2 <sub>1/2</sub>	4f	(5/2) <sup>-1</sup> 9/2 <sup>-1</sup> 2		F <sub>-</sub> Re		
4953.7244(5)	20181.1995(20)	4953.7246(4)	-0.0002	82000	4d	(5/2) <sup>-1</sup> 7/2 <sub>1/2</sub>	4f	(5/2) <sup>-1</sup> 9/2 <sup>-1</sup> 5	C	F <sub>-</sub> Re R1c	H71	
4955.9564(18)	20172.111(7)	4955.9566(5)	-0.0002	6300	4d	(5/2) <sup>-1</sup> 9/2 <sub>1/2</sub>	4f	( <sup>o</sup> F) <sup>-</sup> p <sup>-</sup> 3C <sup>+</sup> 4		R1c		
4969.8062(18)	20115.896(7)	4969.8064(6)	0.0016	4400	4d	(5/2) <sup>-1</sup> 7/2 <sub>1/2</sub>	4f	( <sup>o</sup> F) <sup>-</sup> p <sup>-</sup> 3F <sup>+</sup> 3	D+	R1c	TW	
4971.222(4)	20110.167(15)	4971.2261(9)	-0.004	280	5p	( <sup>o</sup> F) <sup>-</sup> 3p <sup>-</sup> 3C <sup>+</sup> 5d		(5/2) <sup>-1</sup> 3/2 <sup>-1</sup> 2		R1c		
4973.166(3)	20102.429(12)	4973.1394(7)	-0.004	280	5p	( <sup>o</sup> F) <sup>-</sup> 3p <sup>-</sup> 3F <sup>+</sup> 5d		(5/2) <sup>-1</sup> 5/2 <sup>-1</sup> 2		R1c		
4973.6975(19)	20100.158(8)	4973.6959(8)	0.0016	9000	4d	(5/2) <sup>-1</sup> 3/2 <sub>1/2</sub>	4f	(5/2) <sup>-1</sup> 3/2 <sup>-1</sup> 1	D+	F <sub>-</sub> Re	TW	
4974.1542(15)	20096.313(6)	4974.1533(5)	0.0008	9700	4d	(5/2) <sup>-1</sup> 3/2 <sub>1/2</sub>	4f	(5/2) <sup>-1</sup> 3/2 <sup>-1</sup> 3	D+	F <sub>-</sub> Re	TW	
4975.064(3)	20094.637(12)	4975.0639(8)	-0.002	560	4d	(5/2) <sup>-1</sup> 3/2 <sub>1/2</sub>	4f	( <sup>o</sup> F) <sup>-</sup> p <sup>-</sup> 3D <sup>+</sup> 3		R1c		
4980.0153(19)	20074.659(8)	4980.0135(6)	0.0018	11000	4d	(5/2) <sup>-1</sup> 3/2 <sub>1/2</sub>	4f	(5/2) <sup>-1</sup> 3/2 <sup>-1</sup> 1		R1c		
4981.0125(23)	20070.640(9)	4981.0133(6)	-0.0008	670	4d	(5/2) <sup>-1</sup> 7/2 <sub>1/2</sub>	4f	(5/2) <sup>-1</sup> 7/2 <sup>-1</sup> 2		R1c		
4985.1421(23)	20054.014(9)	4985.1381(6)	0.0040	5100	4d	(5/2) <sup>-1</sup> 5/2 <sub>1/2</sub>	4f	( <sup>o</sup> F) <sup>-</sup> p <sup>-</sup> 3F <sup>+</sup> 3	D+	R1c	TW	
4985.5049(7)	20052.5541(3)	4985.50498(7)	0.00001	70000	4d	(5/2) <sup>-1</sup> 7/2 <sub>1/2</sub>	4f	(5/2) <sup>-1</sup> 7/2 <sup>-1</sup> 4	C+	F <sub>-</sub> Re	TW	
4988.327(4)	20041.212(15)	4988.326(4)	0.000	430	5d	(5/2) <sup>-1</sup> 9/2 <sub>1/2</sub>	8f	(5/2) <sup>-1</sup> 11/2 <sup>-1</sup> 2	D+	R1c	TW	
4995.2054(22)	20013.614(19)	4995.2055(5)	-0.0001	800	4d	(5/2) <sup>-1</sup> 3/2 <sub>1/2</sub>	4f	(5/2) <sup>-1</sup> 5/2 <sup>-1</sup> 2		R1c		
4999.584(5)	19996.088(12)	4999.5826(20)	0.001	440	5d	(5/2) <sup>-1</sup> 9/2 <sub>1/2</sub>	8f	(5/2) <sup>-1</sup> 11/2 <sup>-1</sup> 5		R1c		
5002.294(3)	19985.255(12)	5002.2998(10)	-0.006	440	4d	(5/2) <sup>-1</sup> 3/2 <sub>1/2</sub>	4f	( <sup>o</sup> F) <sup>-</sup> p <sup>-</sup> 3D <sup>+</sup> 1		R1c		
5006.79983(15)	19967.2680(6)	5006.79978(15)	0.00005	46000	4d	(5/2) <sup>-1</sup> 3/2 <sub>1/2</sub>	4f	(5/2) <sup>-1</sup> 5/2 <sup>-1</sup> 3	C+	F <sub>-</sub> Re	TW	
5009.8505(3)	19955.1095(10)	5009.85058(17)	-0.0001	35000	4d	(5/2) <sup>-1</sup> 5/2 <sub>1/2</sub>	4f	(5/2) <sup>-1</sup> 5/2 <sup>-1</sup> 3	D+	F <sub>-</sub> Re	TW	
5012.6197(3)	19944.0855(12)	5012.6199(3)	-0.0002	37000	4d	(5/2) <sup>-1</sup> 7/2 <sub>1/2</sub>	4f	(5/2) <sup>-1</sup> 9/2 <sup>-1</sup> 4	C+	F <sub>-</sub> Re	TW	L
5015.2190(8)	19933.749(3)	5015.22038(21)	-0.0014	11000	4d	(5/2) <sup>-1</sup> 5/2 <sub>1/2</sub>	4f	(5/2) <sup>-1</sup> 5/2 <sup>-1</sup> 2		F <sub>-</sub> Re		
5020.126(3)	19914.266(10)	5020.1256(5)	0.000	2000	4p	3F <sup>+</sup> 5 <sup>+</sup> 2				R1c		
5021.2785(4)	19909.6939(15)	5021.27849(23)	0.0000	32000	4d	(5/2) <sup>-1</sup> 5/2 <sub>1/2</sub>	4f	(5/2) <sup>-1</sup> 7/2 <sup>-1</sup> 3	E	F <sub>-</sub> Re	TW	L
5022.599(3)	19904.459(11)	5022.6044(7)	-0.005	760	5p	( <sup>o</sup> F) <sup>-</sup> p <sup>-</sup> D <sup>+</sup> 2	5d	(5/2) <sup>-1</sup> 7/2 <sub>1/2</sub>		R1c		
5024.0251(16)	19898.810(6)	5024.0227(3)	0.0024	8700	4d	(5/2) <sup>-1</sup> 7/2 <sub>1/2</sub>	4f	(5/2) <sup>-1</sup> 9/2 <sup>-1</sup> 4		F <sub>-</sub> Re		
5030.789(3)	19872.057(11)	5030.7892(12)	-0.0000	1400	4d	(5/2) <sup>-1</sup> 5/2 <sub>1/2</sub>	4f	( <sup>o</sup> F) <sup>-</sup> p <sup>-</sup> 5S <sup>+</sup> 2		R1c		
5031.299(3)	19870.040(10)	5031.2968(8)	0.003	1400	4d	(5/2) <sup>-1</sup> 5/2 <sub>1/2</sub>	6p	(5/2) <sup>-1</sup> 7/2 <sup>-1</sup> 3		R1c		
5032.544(3)	19865.125(11)	5032.5461(8)	-0.002	1100	4d	(5/2) <sup>-1</sup> 3/2 <sub>1/2</sub>	4f	(5/2) <sup>-1</sup> 3/2 <sup>-1</sup> 1		R1c		
5034.171(3)	19858.705(13)	5034.1729(8)	-0.002	460	5p	( <sup>o</sup> F) <sup>-</sup> 3p <sup>-</sup> 3F <sup>+</sup> 2	5d	(5/2) <sup>-1</sup> 3/2 <sup>-1</sup> 1		R1c		
5036.7302(21)	19848.616(8)	5036.7320(7)	-0.0019	540	4d	(5/2) <sup>-1</sup> 11/2 <sub>1/2</sub>	4f	( <sup>o</sup> F) <sup>-</sup> 3p <sup>-</sup> 3D <sup>+</sup> 1		R1c		
5039.0109(13)	19839.652(5)	5039.0411(6)	-0.0032	17000	4d	(5/2) <sup>-1</sup> 3/2 <sub>1/2</sub>	4f	(5/2) <sup>-1</sup> 3/2 <sup>-1</sup> 3	3.9e+07	F <sub>-</sub> Re	TW	
5041.3310(9)	19830.502(4)	5041.33123(23)	-0.0003	14000	4d	(5/2) <sup>-1</sup> 5/2 <sub>1/2</sub>	4f	(5/2) <sup>-1</sup> 5/2 <sup>-1</sup> 4	1.6e+07	F <sub>-</sub> Re	TW	
5042.093(3)	19827.505(11)	5042.0348(10)	0.058	310	5p	( <sup>o</sup> F) <sup>-</sup> p <sup>-</sup> 1C <sup>+</sup> 4	5d	(5/2) <sup>-1</sup> 3/2 <sup>-1</sup> 2	D+	R1c		X
5044.2776(21)	19818.918(8)	5044.27768(10)	0.0008	940	4d	(5/2) <sup>-1</sup> 3/2 <sub>1/2</sub>	4f	( <sup>o</sup> F) <sup>-</sup> p <sup>-</sup> 3P <sup>+</sup> 0		R1c		
5047.3477(22)	19806.8629(9)	5047.34770(18)	0.00002	27000	4d	(5/2) <sup>-1</sup> 7/2 <sub>1/2</sub>	4f	(5/2) <sup>-1</sup> 7/2 <sup>-1</sup> 4		F <sub>-</sub> Re		
5051.79210(4)	19789.45784(14)	5051.79209(4)	0.00000	120000	4d	(5/2) <sup>-1</sup> 7/2 <sub>1/2</sub>	4f	(5/2) <sup>-1</sup> 9/2 <sup>-1</sup> 5	1.55e+08	F <sub>-</sub> Re	TW	L
5054.344(3)	19779.147(10)	5054.3487(6)	-0.005	950	5p	( <sup>o</sup> F) <sup>-</sup> 3p <sup>-</sup> 3F <sup>+</sup> 2	5d	(5/2) <sup>-1</sup> 7/2 <sup>-1</sup> 2		R1c		
5054.7758(20)	19777.757(8)	5054.7728(5)	0.0030	1300	4d	(5/2) <sup>-1</sup> 5/2 <sub>1/2</sub>	4f	(5/2) <sup>-1</sup> 7/2 <sup>-1</sup> 3		R1c		
5058.90906(16)	19761.5981(6)	5058.90923(14)	-0.00017	48000	4d	(5/2) <sup>-1</sup> 7/2 <sub>1/2</sub>	4f	(5/2) <sup>-1</sup> 7/2 <sup>-1</sup> 4	4.8e+07	F <sub>-</sub> Re	TW	
5059.418(5)	19759.611(21)	5059.4131(13)	0.005	160	6s	(5/2) <sup>-1</sup> 7/2 <sub>1/2</sub>	6f	(5/2) <sup>-1</sup> 5/2 <sup>-1</sup> 2		R1c		
5060.6437(9)	19754.825(4)	5060.6415(5)	0.0022	16000	4p	3P <sup>+</sup> 5 <sup>+</sup> 2		(5/2) <sup>-1</sup> 5/2 <sup>-1</sup> 3	4.4e+05	F <sub>-</sub> Re	H71	L
5065.45858(8)	19736.0471(3)	5065.45861(8)	-0.00002	70000	4d	(5/2) <sup>-1</sup> 5/2 <sub>1/2</sub>	4f	(5/2) <sup>-1</sup> 7/2 <sup>-1</sup> 4	1.61e+08	F <sub>-</sub> Re	TW	

Table A1. Cont.

$\lambda_{obs}^a$ (Å)	$\sigma_{obs}^b$ (cm <sup>-1</sup> )	$\lambda_{Ritz}^c$ (Å)	$\Delta\lambda_{obs-Ritz}^d$ (Å)	$I_{obs}^d$ (arb. u.)	Char <sup>e</sup>	Lower Level	Upper Level	A (s <sup>-1</sup> )	Acc <sup>f</sup>	Line Ref. <sup>g</sup>	TP Ref. <sup>h</sup>	Notes <sup>b</sup>
5067.09416(17)	19729.676(7)	5067.09423(17)	-0.00008	46000	4d	(3/2) <sup>1</sup> 5/2 <sub>1/2</sub> 4f	(3/2) <sup>1</sup> 7/2 <sub>1/2</sub> 3	1.23e+08	C+	F_Re	TW	
5069.431(3)	19720.584(11)	5069.4315(10)	-0.001	1600	4d	(3/2) <sup>1</sup> 3/2 <sub>1/2</sub> sp	(3/2) <sup>1</sup> 3/2 <sub>1/2</sub> 1D <sup>2</sup>			F_Re		
5072.303(4)	19709.4147(23)	5072.30253(22)	0.0008	32000	4d	(5/2) <sup>1</sup> 7/2 <sub>1/2</sub> 4f	(5/2) <sup>1</sup> 5/2 <sub>1/2</sub> 3			F_Re		
5076.5136(20)	19693.069(8)	5076.5143(5)	-0.0007	830	4d	(5/2) <sup>1</sup> 5/2 <sub>1/2</sub> 4f	(5/2) <sup>1</sup> 5/2 <sub>1/2</sub> 2			Ric		
5077.8070(18)	19688.053(7)	5077.8071(3)	-0.0001	6300	4d	(5/2) <sup>1</sup> 7/2 <sub>1/2</sub> 4f	(5/2) <sup>1</sup> 5/2 <sub>1/2</sub> 2			Ric		
5081.099(4)	19675.296(14)	5081.10531(6)	-0.006	330	5s	(3/2) <sup>1</sup> 3/2 <sub>1/2</sub> 1	(1D) <sup>3</sup> p <sup>3</sup> 3p <sup>2</sup> 1			Ric		
5082.525(4)	19669.778(14)	5082.5262(15)	-0.001	160	5p	(5/2) <sup>1</sup> 3/2 <sub>1/2</sub> 1	(3/2) <sup>1</sup> 11/2 <sub>1/2</sub> 0			Ric		
5083.9795(12)	19664.150(5)	5083.97879(22)	0.0007	21000	4d	(5/2) <sup>1</sup> 7/2 <sub>1/2</sub> 4f	(5/2) <sup>1</sup> 5/2 <sub>1/2</sub> 3			F_Re		
5084.0173(5)	19664.0034(18)	5084.0175(3)	-0.0002	14000	4d	(5/2) <sup>1</sup> 7/2 <sub>1/2</sub> 4f	(5/2) <sup>1</sup> 7/2 <sub>1/2</sub> 3			F_Re		
5088.27603(10)	19647.5455(4)	5088.27603(9)	0.0000	57000	4d	(5/2) <sup>1</sup> 5/2 <sub>1/2</sub> 4f	(5/2) <sup>1</sup> 5/2 <sub>1/2</sub> 3			F_Re		
5088.4682(8)	19644.726(3)	5088.4896(4)	-0.0013	25000	4d	(3/2) <sup>1</sup> 5/2 <sub>1/2</sub> 4f	(3/2) <sup>1</sup> 5/2 <sub>1/2</sub> 3	4.8e+07	D+	F_Re	TW	
5088.9426(11)	19644.972(4)	5088.9421(5)	0.0005	19000	4d	(5/2) <sup>1</sup> 5/2 <sub>1/2</sub> 4f	(5/2) <sup>1</sup> 5/2 <sub>1/2</sub> 2	5.2e+07	D+	F_Re	TW	
5089.492(5)	19642.851(21)	5089.4927(7)	-0.005	330	5p	(3/2) <sup>1</sup> 5/2 <sub>1/2</sub> 5d	(5/2) <sup>1</sup> 3/2 <sub>1/2</sub> 1			Ric		
5093.81535(17)	19626.1799(7)	5093.81536(14)	-0.00001	41000	4d	(5/2) <sup>1</sup> 5/2 <sub>1/2</sub> 4f	(5/2) <sup>1</sup> 5/2 <sub>1/2</sub> 2	4.9e+07	D+	F_Re	TW	
5094.442(3)	19623.766(11)	5094.4408(7)	0.001	330	5p	(3/2) <sup>1</sup> 5/2 <sub>1/2</sub> 5d	(5/2) <sup>1</sup> 3/2 <sub>1/2</sub> 2			Ric		
5095.7489(19)	19618.733(7)	5095.7478(3)	0.0011	3100	4d	(5/2) <sup>1</sup> 7/2 <sub>1/2</sub> 4f	(5/2) <sup>1</sup> 7/2 <sub>1/2</sub> 3			Ric		
5100.0629(10)	19602.138(4)	5100.0650(3)	-0.0021	12000	4d	(5/2) <sup>1</sup> 5/2 <sub>1/2</sub> 4f	(5/2) <sup>1</sup> 7/2 <sub>1/2</sub> 3			F_Re		
5100.9790(21)	19598.618(8)	5100.9762(5)	0.0028	9900	4d	(3/2) <sup>1</sup> 5/2 <sub>1/2</sub> 4f	(3/2) <sup>1</sup> 5/2 <sub>1/2</sub> 3	1.6e+07	D+	Ric	TW	
5103.283(3)	19589.770(13)	5103.2831(6)	-0.000	830	4d	(3/2) <sup>1</sup> 5/2 <sub>1/2</sub> 4f	(3/2) <sup>1</sup> 9/2 <sub>1/2</sub> 4			Ric		
5104.573(3)	19584.818(11)	5104.5755(3)	-0.002	830	4d	(5/2) <sup>1</sup> 7/2 <sub>1/2</sub> 4f	(5/2) <sup>1</sup> 3/2 <sub>1/2</sub> 2			Ric		
5108.3335(19)	19570.402(7)	5108.3328(4)	0.0007	7300	4d	(5/2) <sup>1</sup> 5/2 <sub>1/2</sub> 4f	(5/2) <sup>1</sup> 3/2 <sub>1/2</sub> 1			Ric		
5109.825(3)	19564.691(13)	5109.8270(21)	-0.002	500	5p	(1D) <sup>3</sup> p <sup>3</sup> 3p <sup>2</sup> 1	(3/2) <sup>1</sup> 5/2 <sub>1/2</sub> 1			Ric		
5109.880(6)	19564.481(21)	5109.8767(13)	0.008	330	4d	(5/2) <sup>1</sup> 5/2 <sub>1/2</sub> 4f	(3/2) <sup>1</sup> p <sup>3</sup> s <sup>2</sup> 2			Ric		
5110.3417(19)	19562.712(7)	5110.3409(5)	0.0008	1700	4d	(5/2) <sup>1</sup> 7/2 <sub>1/2</sub> 4f	(5/2) <sup>1</sup> 11/2 <sub>1/2</sub> 5			Ric		
5115.539(3)	19542.852(13)	5115.5386(11)	-0.004	170	5p	(3/2) <sup>1</sup> p <sup>3</sup> D <sup>2</sup> 1	(5/2) <sup>1</sup> 11/2 <sub>1/2</sub> 5			Ric		
5120.7535(4)	19522.9360(15)	5120.75319(19)	0.0003	20000	4d	(5/2) <sup>1</sup> 5/2 <sub>1/2</sub> 4f	(5/2) <sup>1</sup> 3/2 <sub>1/2</sub> 2	2.0e+07	D+	F_Re	TW	
5121.765(3)	19519.080(13)	5121.7672(7)	-0.002	1000	4d	(3/2) <sup>1</sup> 5/2 <sub>1/2</sub> 4f	(3/2) <sup>1</sup> 3/2 <sub>1/2</sub> 2			Ric		
5124.4745(7)	19508.760(3)	5124.4753(5)	-0.0007	30000	4d	(5/2) <sup>1</sup> 7/2 <sub>1/2</sub> sp	(3/2) <sup>1</sup> p <sup>3</sup> C <sup>2</sup> 4			F_Re		X
5127.682(3)	19496.556(13)	5127.7027(9)	-0.020	570	4d	(5/2) <sup>1</sup> 5/2 <sub>1/2</sub> 4f	(3/2) <sup>1</sup> 3/2 <sub>1/2</sub> 1			Ric		X
5127.7428(21)	19496.326(8)	5127.7327(8)	0.0101	620	4d	(5/2) <sup>1</sup> 3/2 <sub>1/2</sub> sp	(3/2) <sup>1</sup> p <sup>3</sup> 3p <sup>2</sup> 1			Ric		
5130.368(3)	19488.533(12)	5130.5829(10)	0.000	920	4d	(3/2) <sup>1</sup> 3/2 <sub>1/2</sub> sp	(3/2) <sup>1</sup> p <sup>3</sup> D <sup>2</sup> 2			Ric		
5133.123(3)	19475.890(11)	5133.1211(4)	0.002	500	4d	(5/2) <sup>1</sup> 5/2 <sub>1/2</sub> 4f	(5/2) <sup>1</sup> 11/2 <sub>1/2</sub> 1			Ric		
5134.6720(24)	19470.016(9)	5134.6725(9)	-0.0005	170	4d	(5/2) <sup>1</sup> 5/2 <sub>1/2</sub> 4f	(3/2) <sup>1</sup> 3/2 <sub>1/2</sub> 5p <sup>1</sup>			Ric		
5136.3939(14)	19463.489(7)	5136.3932(5)	0.0007	1300	4d	(5/2) <sup>1</sup> 7/2 <sub>1/2</sub> sp	(3/2) <sup>1</sup> p <sup>3</sup> C <sup>2</sup> 4			Ric		
5138.613(4)	19455.0851(7)	5138.6113(20)	0.001	340	4d	(5/2) <sup>1</sup> 5/2 <sub>1/2</sub> sp	(1G) <sup>3</sup> p <sup>3</sup> C <sup>2</sup> 4			Ric		
5151.206(2)	19407.522(9)	5151.2073(8)	-0.001	2500	4d	(5/2) <sup>1</sup> 7/2 <sub>1/2</sub> sp	(3/2) <sup>1</sup> p <sup>3</sup> D <sup>2</sup> 3			Ric		
5157.255(4)	19384.761(14)	5157.2580(9)	-0.003	340	5p	(3/2) <sup>1</sup> 3/2 <sub>1/2</sub> 0s	(3/2) <sup>1</sup> 3/2 <sub>1/2</sub> 2			Ric		
5158.0914(6)	19381.6166(21)	5158.0916(4)	-0.0002	13000	4d	(5/2) <sup>1</sup> 11/2 <sub>1/2</sub> 0f	(5/2) <sup>1</sup> 3/2 <sub>1/2</sub> 1	2.4e+07	D+	F_Re	TW	
5159.103(4)	19377.817(17)	5159.0971(13)	0.006	2300	5p	(3/2) <sup>1</sup> p <sup>3</sup> F <sup>2</sup> 4	(5/2) <sup>1</sup> 7/2 <sub>1/2</sub> 4f			Ric		
5163.252(3)	19362.244(11)	5163.2501(8)	0.002	330	4d	(5/2) <sup>1</sup> 7/2 <sub>1/2</sub> sp	(3/2) <sup>1</sup> p <sup>3</sup> D <sup>2</sup> 3			Ric		X
5167.6923(22)	19345.609(8)	5167.6825(8)	0.0098	11000	4d	(5/2) <sup>1</sup> 5/2 <sub>1/2</sub> sp	(3/2) <sup>1</sup> p <sup>3</sup> C <sup>2</sup> 3			Ric		
5171.644(3)	19330.828(12)	5171.6406(13)	0.003	570	4d	(3/2) <sup>1</sup> 7/2 <sub>1/2</sub> sp	(3/2) <sup>1</sup> p <sup>3</sup> C <sup>2</sup> 3			Ric		
5175.9651(23)	19314.689(9)	5175.9637(23)	0.0014	1400	4d	(5/2) <sup>1</sup> 3/2 <sub>1/2</sub> 1	(3/2) <sup>1</sup> p <sup>3</sup> 1p <sup>1</sup>			Ric		
5175.9651(23)	19314.689(9)	5175.9653(10)	-0.0002	1400	4d	(5/2) <sup>1</sup> 11/2 <sub>1/2</sub> sp	(3/2) <sup>1</sup> p <sup>3</sup> 3p <sup>2</sup> 1			Ric		
5183.3664(7)	19287.110(3)	5183.3664(5)	-0.0000	19000	4d	(5/2) <sup>1</sup> 11/2 <sub>1/2</sub> 4f	(5/2) <sup>1</sup> 11/2 <sub>1/2</sub> 1	2.4e+07	D+	F_Re	TW	
5184.052(3)	19284.561(11)	5184.0520(11)	-0.000	340	4d	(3/2) <sup>1</sup> 3/2 <sub>1/2</sub> 1	(1G) <sup>3</sup> p <sup>3</sup> F <sup>2</sup> 2			Ric		

Table A1. Cont.

$\lambda_{\text{obs}}^a$ (Å)	$\sigma_{\text{obs}}^b$ (cm <sup>-1</sup> )	$\lambda_{\text{Ritz}}^c$ (Å)	$\Delta\lambda_{\text{obs-Ritz}}^d$ (Å)	$I_{\text{obs}}^d$ (arb. u.)	Char <sup>e</sup>	Lower Level	Upper Level	A (s <sup>-1</sup> )	Acc <sup>f</sup>	Line Ref. <sup>g</sup>	TP Ref. <sup>h</sup>	Notes <sup>b</sup>
5192.638(6)	19252.671(21)	5192.6239(13)	0.015	240		( <sup>3</sup> F) <sup>3</sup> P <sup>3</sup> P <sup>3</sup> °	5d	(5/2) <sup>2</sup> F <sup>2</sup> 1/2	Ric			
5194.349(4)	19246.531(16)	5194.3399(17)	0.009	170		( <sup>3</sup> F) <sup>3</sup> P <sup>3</sup> F <sup>2</sup>	6s	(5/2) <sup>2</sup> F <sup>2</sup> 1/2	Ric			
5205.112(4)	19206.536(17)	5205.1059(8)	0.006	500		( <sup>3</sup> F) <sup>3</sup> P <sup>3</sup> D <sup>2</sup>	5d	(5/2) <sup>2</sup> F <sup>2</sup> 1/2	Ric			
5207.137(22)	19199.070(8)	5207.1340(15)	0.0018	29000		( <sup>3</sup> G) <sup>3</sup> P <sup>3</sup> H <sup>4</sup>	sp	( <sup>3</sup> G) <sup>3</sup> P <sup>3</sup> H <sup>4</sup>	Ric			
5229.518(3)	19116.900(18)	5229.5194(11)	-0.002	32000		( <sup>3</sup> F) <sup>3</sup> P <sup>3</sup> D <sup>2</sup>	sp	( <sup>3</sup> F) <sup>3</sup> P <sup>3</sup> D <sup>2</sup>	Ric			
5229.709(6)	19116.201(21)	5229.707(10)	-0.002	170		( <sup>3</sup> F) <sup>3</sup> P <sup>3</sup> C <sup>3</sup>	6s	(3/2) <sup>2</sup> F <sup>2</sup> 3/2	Ric			
5234.471(23)	19098.81(8)	5234.429(3)	0.042	170	*	( <sup>3</sup> F) <sup>3</sup> P <sup>3</sup> P <sup>3</sup> °	9s	(3/2) <sup>2</sup> F <sup>2</sup> 3/2	Rinc			
5234.871(23)	19098.81(8)	5234.4943(14)	-0.023	170	*	( <sup>3</sup> F) <sup>3</sup> P <sup>3</sup> F <sup>2</sup>	5d	(3/2) <sup>2</sup> F <sup>2</sup> 3/2	Ric			
5239.5473(24)	19080.307(9)	5239.5490(8)	-0.0017	330		( <sup>3</sup> F) <sup>3</sup> P <sup>3</sup> F <sup>2</sup>	4d	( <sup>3</sup> F) <sup>3</sup> P <sup>3</sup> F <sup>2</sup>	Ric			
5245.340(3)	19059.237(12)	5245.3423(13)	-0.003	19000		( <sup>3</sup> F) <sup>3</sup> P <sup>3</sup> F <sup>2</sup>	5d	(5/2) <sup>2</sup> F <sup>2</sup> 1/2	Ric			
5247.109(4)	19052.811(16)	5247.1155(9)	-0.007	160		( <sup>3</sup> F) <sup>3</sup> P <sup>3</sup> D <sup>2</sup>	4d	( <sup>3</sup> F) <sup>3</sup> P <sup>3</sup> D <sup>2</sup>	Ric			
5247.976(4)	19049.661(16)	5247.9750(7)	0.001	160		(5/2) <sup>2</sup> F <sup>2</sup> 3/2	5d	(5/2) <sup>2</sup> F <sup>2</sup> 3/2	Ric			
5251.545(3)	19036.718(9)	5251.5445(8)	0.000	330		(5/2) <sup>2</sup> F <sup>2</sup> 3/2	5d	(5/2) <sup>2</sup> F <sup>2</sup> 3/2	Ric			
5251.545(3)	19036.718(9)	5251.5445(8)	0.000	330		(5/2) <sup>2</sup> F <sup>2</sup> 3/2	5d	(5/2) <sup>2</sup> F <sup>2</sup> 3/2	Ric			
5254.2141(20)	19022.046(7)	5254.2139(6)	0.0002	350		(5/2) <sup>2</sup> F <sup>2</sup> 3/2	5d	(5/2) <sup>2</sup> F <sup>2</sup> 3/2	Ric			
5258.8249(21)	19010.364(8)	5258.8237(8)	0.0011	580		(5/2) <sup>2</sup> F <sup>2</sup> 3/2	sp	( <sup>3</sup> F) <sup>3</sup> P <sup>3</sup> D <sup>2</sup>	Ric			
5261.0461(22)	19002.338(8)	5261.0443(8)	0.0018	330		( <sup>3</sup> F) <sup>3</sup> P <sup>3</sup> D <sup>2</sup>	5d	(5/2) <sup>2</sup> F <sup>2</sup> 3/2	Ric			
5269.9892(14)	18970.091(5)	5269.9904(6)	-0.0012	23000		( <sup>3</sup> F) <sup>3</sup> P <sup>3</sup> D <sup>2</sup>	4p	( <sup>3</sup> F) <sup>3</sup> P <sup>3</sup> D <sup>2</sup>	F,Rc			
5276.5244(15)	18946.597(5)	5276.5241(9)	0.0003	16000		( <sup>3</sup> F) <sup>3</sup> P <sup>3</sup> F <sup>2</sup>	4d	(5/2) <sup>2</sup> F <sup>2</sup> 3/2	F,Rc			
5280.9333(23)	18930.707(8)	5280.9353(7)	-0.0030	480		( <sup>3</sup> F) <sup>3</sup> P <sup>3</sup> F <sup>2</sup>	sp	(5/2) <sup>2</sup> F <sup>2</sup> 3/2	Ric			
5285.360(4)	18914.923(13)	5285.3600(13)	0.000	480		( <sup>3</sup> F) <sup>3</sup> P <sup>3</sup> F <sup>2</sup>	sp	(5/2) <sup>2</sup> F <sup>2</sup> 3/2	Ric			
5289.1103(21)	18891.512(8)	5289.1096(6)	0.0007	800		( <sup>3</sup> F) <sup>3</sup> P <sup>3</sup> F <sup>2</sup>	sp	(5/2) <sup>2</sup> F <sup>2</sup> 3/2	Ric			
5291.8196(20)	18891.835(7)	5291.8216(7)	-0.0020	1600		( <sup>3</sup> F) <sup>3</sup> P <sup>3</sup> F <sup>2</sup>	sp	(5/2) <sup>2</sup> F <sup>2</sup> 3/2	Ric			
5297.4020(23)	18871.927(8)	5297.4047(9)	-0.0028	480		( <sup>3</sup> F) <sup>3</sup> P <sup>3</sup> F <sup>2</sup>	4d	( <sup>3</sup> F) <sup>3</sup> P <sup>3</sup> D <sup>2</sup>	Ric			
5310.771(3)	18824.421(11)	5310.7694(24)	0.001	310		(5/2) <sup>2</sup> F <sup>2</sup> 3/2	7g	(5/2) <sup>2</sup> F <sup>2</sup> 3/2	Ric			
5314.6020(22)	18810.851(8)	5314.6025(9)	-0.0005	480		(5/2) <sup>2</sup> F <sup>2</sup> 3/2	sp	( <sup>3</sup> G) <sup>3</sup> P <sup>3</sup> H <sup>4</sup>	Ric			
5315.989(4)	18805.942(15)	5315.9868(7)	0.003	160		(5/2) <sup>2</sup> F <sup>2</sup> 3/2	5d	(5/2) <sup>2</sup> F <sup>2</sup> 3/2	Ric			
5321.666(3)	18785.883(12)	5321.666(3)	0.000	310		(5/2) <sup>2</sup> F <sup>2</sup> 3/2	4f	(5/2) <sup>2</sup> F <sup>2</sup> 3/2	Ric			
5321.840(3)	18785.267(11)	5321.8352(21)	0.005	310		(5/2) <sup>2</sup> F <sup>2</sup> 3/2	7g	(5/2) <sup>2</sup> F <sup>2</sup> 3/2	Rinc			
5321.840(3)	18785.267(11)	5321.8386(23)	0.002	310	*	(5/2) <sup>2</sup> F <sup>2</sup> 3/2	7g	(5/2) <sup>2</sup> F <sup>2</sup> 3/2	Ric			
5324.070(4)	18777.398(13)	5324.0734(24)	-0.003	310	*	(5/2) <sup>2</sup> F <sup>2</sup> 3/2	7g	(5/2) <sup>2</sup> F <sup>2</sup> 3/2	Ric			
5324.3542(21)	18776.397(7)	5324.3531(6)	0.0011	1500		( <sup>3</sup> F) <sup>3</sup> P <sup>3</sup> F <sup>2</sup>	sp	(5/2) <sup>2</sup> F <sup>2</sup> 3/2	Ric			
5325.319(3)	18772.994(12)	5325.3132(19)	0.006	310		( <sup>3</sup> F) <sup>3</sup> P <sup>3</sup> F <sup>2</sup>	5d	(5/2) <sup>2</sup> F <sup>2</sup> 3/2	Ric			
5327.6405(8)	18763.605(8)	5327.6411(21)	0.005	920		(5/2) <sup>2</sup> F <sup>2</sup> 3/2	7g	(5/2) <sup>2</sup> F <sup>2</sup> 3/2	Ric			
5328.8109(22)	18760.694(8)	5328.8109(22)	0.000	1600		(5/2) <sup>2</sup> F <sup>2</sup> 3/2	6	(5/2) <sup>2</sup> F <sup>2</sup> 3/2	Ric			
5328.963(4)	18760.157(13)	5328.963(4)	0.000	460		(5/2) <sup>2</sup> F <sup>2</sup> 3/2	7g	(5/2) <sup>2</sup> F <sup>2</sup> 3/2	Ric			
5331.634(4)	18750.781(4)	5331.627(13)	0.008	150		(5/2) <sup>2</sup> F <sup>2</sup> 3/2	8d	(5/2) <sup>2</sup> F <sup>2</sup> 3/2	Rinc			X
5331.634(4)	18750.781(4)	5331.627(13)	0.008	150		(5/2) <sup>2</sup> F <sup>2</sup> 3/2	8d	(5/2) <sup>2</sup> F <sup>2</sup> 3/2	Rinc			X
5335.317(3)	18737.818(12)	5335.3169(21)	-0.000	300		(5/2) <sup>2</sup> F <sup>2</sup> 3/2	sp	( <sup>3</sup> D) <sup>3</sup> P <sup>3</sup> D <sup>2</sup>	Ric			
5335.318(3)	18737.112(12)	5335.3179(6)	-0.000	150		(5/2) <sup>2</sup> F <sup>2</sup> 3/2	7g	(5/2) <sup>2</sup> F <sup>2</sup> 3/2	R2nc			
5336.203(3)	18734.707(12)	5336.203(3)	0.000	300		(5/2) <sup>2</sup> F <sup>2</sup> 3/2	4f	(5/2) <sup>2</sup> F <sup>2</sup> 3/2	Ric			
5337.580(13)	18729.87(5)	5337.5664(20)	0.013	150	*	(5/2) <sup>2</sup> F <sup>2</sup> 3/2	7g	(5/2) <sup>2</sup> F <sup>2</sup> 3/2	Ric			



Table A1. Cont.

$\lambda_{\text{obs}}^a$ (Å)	$\sigma_{\text{obs}}^b$ (cm <sup>-1</sup> )	$\lambda_{\text{Ritz}}^c$ (Å)	$\Delta\lambda_{\text{obs-Ritz}}^d$ (Å)	$I_{\text{obs}}^d$ (arb. u.)	Char <sup>e</sup>	Lower Level	Upper Level	A (s <sup>-1</sup> )	Acc <sup>f</sup>	Line Ref. g	TP Ref. h	Notes <sup>b</sup>
5337.580(13)	18729.87(5)	5337.593(3)	-0.013	150	*	(5/2) <sup>3</sup> [3/2] <sup>1</sup> <sub>0</sub>	7g	(5/2) <sup>3</sup> [3/2] <sup>1</sup> <sub>1</sub>		Ric		
5338.460(3)	18726.784(10)	5338.4584(6)	0.002	300	4d	(3/2) <sup>2</sup> [1/2] <sup>1</sup> <sub>2</sub>	4f	(3/2) <sup>2</sup> [1/2] <sup>1</sup> <sub>1</sub>		Ric		
5340.098(3)	18721.041(11)	5340.0973(8)	0.001	1300	4d	(5/2) <sup>3</sup> [3/2] <sup>1</sup> <sub>2</sub>	5d	(5/2) <sup>3</sup> [3/2] <sup>1</sup> <sub>1</sub>		Ric		
5340.878(3)	18718.305(12)	5340.8750(20)	0.003	300	4f	(5/2) <sup>3</sup> [7/2] <sup>3</sup> <sub>2</sub>	7g	(5/2) <sup>3</sup> [7/2] <sup>3</sup> <sub>1</sub>		Ric		
5342.197(3)	18713.684(12)	5342.1987(24)	-0.001	150	4f	(5/2) <sup>3</sup> [7/2] <sup>3</sup> <sub>0</sub>	7g	(5/2) <sup>3</sup> [7/2] <sup>3</sup> <sub>1</sub>		Ric		
5344.366(4)	18706.091(16)	5344.3657(21)	0.000	150	m	(5/2) <sup>3</sup> [9/2] <sup>3</sup> <sub>2</sub>	7g	(5/2) <sup>3</sup> [9/2] <sup>3</sup> <sub>1</sub>		Rinc		
5344.366(4)	18706.091(16)	5344.3692(24)	-0.003	150	*	(5/2) <sup>3</sup> [7/2] <sup>3</sup> <sub>3</sub>	7g	(5/2) <sup>3</sup> [7/2] <sup>3</sup> <sub>2</sub>		Ric		
5345.160(3)	18703.332(10)	5345.154(3)	0.006	420	*	(3/2) <sup>2</sup> [9/2] <sup>1</sup> <sub>5</sub>	7g	(3/2) <sup>2</sup> [9/2] <sup>1</sup> <sub>6</sub>		Ric		
5345.576(2)	18701.857(9)	5345.5723(9)	0.003	300	sp	( <sup>3</sup> P) <sup>3</sup> 3D <sup>1</sup> <sub>1</sub>	5d	( <sup>3</sup> P) <sup>3</sup> 3D <sup>1</sup> <sub>2</sub>	1.1e+07	D+	TW	
5347.624(22)	18694.693(8)	5347.6243(8)	-0.0000	1500	4d	(5/2) <sup>3</sup> [3/2] <sup>1</sup> <sub>2</sub>	4d	(5/2) <sup>3</sup> [3/2] <sup>1</sup> <sub>1</sub>		Ric		
5347.684(3)	18694.484(11)	5347.6891(8)	-0.005	750	4d	(3/2) <sup>2</sup> [7/2] <sup>1</sup> <sub>2</sub>	sp	( <sup>3</sup> P) <sup>3</sup> 3D <sup>1</sup> <sub>1</sub>		Ric		
5347.809(3)	18694.047(12)	5347.809(3)	0.000	420	4d	(3/2) <sup>2</sup> [9/2] <sup>1</sup> <sub>2</sub>	4f	(3/2) <sup>2</sup> [9/2] <sup>1</sup> <sub>1</sub>		Ric		
5349.076(4)	18689.619(13)	5349.0730(24)	0.003	150	4f	(5/2) <sup>3</sup> [5/2] <sup>1</sup> <sub>2</sub>	7g	(5/2) <sup>3</sup> [7/2] <sup>1</sup> <sub>2</sub>	1.1e+07	D+	TW	
5351.245(4)	18682.043(14)	5351.2356(21)	-0.000	150	4f	(5/2) <sup>3</sup> [5/2] <sup>1</sup> <sub>2</sub>	7g	(5/2) <sup>3</sup> [5/2] <sup>1</sup> <sub>1</sub>		Rinc		
5351.245(4)	18682.043(14)	5351.2491(24)	-0.004	150	*	(5/2) <sup>3</sup> [5/2] <sup>1</sup> <sub>2</sub>	7g	(5/2) <sup>3</sup> [5/2] <sup>1</sup> <sub>1</sub>		Ric		
5351.379(4)	18680.878(12)	5351.5804(12)	-0.001	300	4d	(3/2) <sup>2</sup> [5/2] <sup>1</sup> <sub>2</sub>	sp	( <sup>1</sup> G) <sup>3</sup> 3F <sup>2</sup> <sub>2</sub>		Rinc		
5352.0268(21)	18679.315(7)	5352.0245(5)	0.0023	6000	4d	(3/2) <sup>2</sup> [1/2] <sup>1</sup> <sub>2</sub>	4f	(5/2) <sup>3</sup> [3/2] <sup>1</sup> <sub>2</sub>		Ric		
5353.863(4)	18675.908(12)	5353.8619(20)	-0.002	300	4f	(5/2) <sup>3</sup> [5/2] <sup>1</sup> <sub>2</sub>	7g	(5/2) <sup>3</sup> [9/2] <sup>1</sup> <sub>2</sub>		Ric		
5354.4850(20)	18670.740(7)	5354.483(8)	-0.0013	4500	4d	(3/2) <sup>2</sup> [1/2] <sup>1</sup> <sub>2</sub>	4f	(5/2) <sup>3</sup> [1/2] <sup>1</sup> <sub>0</sub>		Ric		
5355.186(3)	18668.294(11)	5355.1870(24)	-0.001	410	4f	(5/2) <sup>3</sup> [5/2] <sup>1</sup> <sub>2</sub>	7g	(5/2) <sup>3</sup> [7/2] <sup>1</sup> <sub>2</sub>	7.4e+06	D+	TW	
5356.8109(21)	18662.633(7)	5356.8091(6)	0.0018	2100	4d	(5/2) <sup>3</sup> [5/2] <sup>1</sup> <sub>2</sub>	sp	( <sup>3</sup> F) <sup>3</sup> 3F <sup>4</sup> <sub>4</sub>		Ric		
5357.374(4)	18660.670(13)	5357.3727(21)	0.002	300	4f	(5/2) <sup>3</sup> [5/2] <sup>1</sup> <sub>2</sub>	7g	(5/2) <sup>3</sup> [5/2] <sup>1</sup> <sub>1</sub>		Rinc		
5357.374(4)	18660.670(13)	5357.3761(24)	-0.002	300	4f	(5/2) <sup>3</sup> [5/2] <sup>1</sup> <sub>2</sub>	7g	(5/2) <sup>3</sup> [5/2] <sup>1</sup> <sub>1</sub>		Ric		
5361.907(4)	18644.894(12)	5361.9144(4)	-0.007	150	4f	(3/2) <sup>2</sup> [5/2] <sup>1</sup> <sub>3</sub>	7g	(3/2) <sup>2</sup> [7/2] <sup>1</sup> <sub>3</sub>		Ric		
5361.907(4)	18644.894(12)	5361.9144(4)	-0.007	150	4f	(3/2) <sup>2</sup> [5/2] <sup>1</sup> <sub>3</sub>	7g	(3/2) <sup>2</sup> [7/2] <sup>1</sup> <sub>3</sub>	9.e+06	D+	TW	
5365.5363(20)	18632.284(7)	5365.5353(6)	-0.0000	5500	4d	(3/2) <sup>2</sup> [1/2] <sup>1</sup> <sub>2</sub>	4f	(5/2) <sup>3</sup> [1/2] <sup>1</sup> <sub>1</sub>		Ric		
5366.243(3)	18629.831(11)	5366.2476(7)	-0.005	440	sp	( <sup>3</sup> P) <sup>3</sup> 3D <sup>2</sup> <sub>2</sub>	6s	(3/2) <sup>2</sup> [3/2] <sup>1</sup> <sub>2</sub>		Ric		
5368.3825(21)	18622.406(7)	5368.3839(7)	-0.0013	7400	sp	( <sup>3</sup> P) <sup>3</sup> 3F <sup>2</sup> <sub>2</sub>	5d	(5/2) <sup>3</sup> [9/2] <sup>1</sup> <sub>4</sub>		Ric		
5371.6284(21)	18611.160(7)	5371.6264(7)	0.001	880	sp	( <sup>3</sup> P) <sup>3</sup> 3F <sup>3</sup> <sub>3</sub>	5d	(5/2) <sup>3</sup> [9/2] <sup>1</sup> <sub>4</sub>		Ric		
5375.276(4)	18598.524(12)	5375.276(4)	0.000	290	4f	(3/2) <sup>2</sup> [5/2] <sup>1</sup> <sub>2</sub>	7g	(3/2) <sup>2</sup> [3/2] <sup>1</sup> <sub>2</sub>	8.1e+06	D+	TW	
5381.9479(23)	18575.468(8)	5381.9311(21)	-0.0032	430	4f	(5/2) <sup>3</sup> [7/2] <sup>1</sup> <sub>2</sub>	7g	(5/2) <sup>3</sup> [7/2] <sup>1</sup> <sub>1</sub>		Ric		
5381.9479(23)	18575.468(8)	5381.9485(20)	-0.0006	430	4f	(5/2) <sup>3</sup> [7/2] <sup>1</sup> <sub>2</sub>	7g	(5/2) <sup>3</sup> [9/2] <sup>1</sup> <sub>2</sub>		Rinc		
5382.329(4)	18574.152(15)	5382.3347(19)	-0.006	140	4f	(5/2) <sup>3</sup> [7/2] <sup>1</sup> <sub>2</sub>	7g	(5/2) <sup>3</sup> [9/2] <sup>1</sup> <sub>2</sub>	8.2e+06	D+	TW	
5383.289(4)	18570.842(12)	5383.2871(24)	0.001	140	4f	(5/2) <sup>3</sup> [7/2] <sup>1</sup> <sub>2</sub>	7g	(5/2) <sup>3</sup> [7/2] <sup>1</sup> <sub>1</sub>		Ric		
5384.518(3)	18565.569(11)	5384.8222(16)	-0.005	430	4d	(3/2) <sup>2</sup> [1/2] <sup>1</sup> <sub>2</sub>	6p	(3/2) <sup>2</sup> [1/2] <sup>1</sup> <sub>1</sub>		Ric		
5386.435(4)	18559.995(14)	5386.437(4)	-0.003	420	4f	(3/2) <sup>2</sup> [7/2] <sup>1</sup> <sub>2</sub>	7g	(3/2) <sup>2</sup> [9/2] <sup>1</sup> <sub>2</sub>		Ric		
5386.435(4)	18559.995(14)	5386.8419(10)	-0.0014	420	4f	(3/2) <sup>2</sup> [7/2] <sup>1</sup> <sub>2</sub>	7g	(3/2) <sup>2</sup> [9/2] <sup>1</sup> <sub>2</sub>	1.0e+07	D+	TW	
5386.8405(22)	18558.597(8)	5390.0296(21)	-0.001	140	4d	(5/2) <sup>3</sup> [1/2] <sup>1</sup> <sub>2</sub>	sp	( <sup>3</sup> P) <sup>3</sup> 3P <sup>1</sup> <sub>1</sub>		Ric		
5390.029(4)	18547.619(13)	5390.0296(21)	-0.001	140	4f	(5/2) <sup>3</sup> [9/2] <sup>1</sup> <sub>5</sub>	7g	(5/2) <sup>3</sup> [9/2] <sup>1</sup> <sub>5</sub>		Ric		
5390.029(4)	18547.619(13)	5390.0270(20)	0.002	140	4f	(5/2) <sup>3</sup> [9/2] <sup>1</sup> <sub>5</sub>	7g	(5/2) <sup>3</sup> [9/2] <sup>1</sup> <sub>5</sub>		Rinc		

Table A1. Cont.

$\lambda_{obs}^a$ (Å)	$\sigma_{obs}^b$ (cm <sup>-1</sup> )	$\lambda_{Ritz}^c$ (Å)	$\Delta\lambda_{obs-Ritz}^d$ (Å)	$I_{obs}^d$ (arb. u.)	Char <sup>e</sup>	Lower Level	Upper Level	A (s <sup>-1</sup> )	Acc <sup>f</sup>	Line Ref. <sup>g</sup>	TP Ref. <sup>h</sup>	Notes <sup>b</sup>
5390.4163(22)	18546.286(8)	5390.4169(13)	-0.0006	4800		4d	(3/2) <sup>1</sup> 5/2 <sub>2</sub> sp			Ric		
5391.6966(22)	18541.882(8)	5391.6987(10)	-0.0021	1700		4d	(5/2) <sup>1</sup> 9/2 <sub>2</sub> sp	( <sup>3</sup> F) <sup>3</sup> P <sup>3</sup> C <sup>3</sup>		Ric		
5393.9372(21)	18534.180(7)	5393.9372(7)	0.0001	2600		sp	( <sup>3</sup> F) <sup>3</sup> P <sup>3</sup> D <sup>2</sup> 6s	(3/2) <sup>1</sup> 3/2 <sub>1</sub>		Ric		
5397.2943(21)	18522.632(7)	5397.2952(5)	-0.0008	580		4d	(3/2) <sup>1</sup> 7/2 <sub>2</sub> 4f	(5/2) <sup>1</sup> 9/2 <sub>1</sub> <sup>4</sup>		Ric		
5397.37	18522.38	5397.3730(17)			:	sp	( <sup>3</sup> F) <sup>3</sup> P <sup>3</sup> D <sup>3</sup> 9s	(5/2) <sup>1</sup> 5/2 <sub>2</sub>			TW	
5398.573(4)	18518.266(12)	5398.573(4)	-0.000	140		4f	(3/2) <sup>1</sup> 7/2 <sub>2</sub> <sup>3</sup> 7g	(3/2) <sup>1</sup> 9/2 <sub>1</sub>	9.e+06	Ric		
5403.714(4)	18500.647(13)	5403.7093(9)	0.005	140		5p	(5/2) <sup>1</sup> 3/2 <sub>1</sub> <sup>2</sup> 5d	(3/2) <sup>1</sup> 1/2 <sub>1</sub>		Ric		
5405.652(3)	18494.013(11)	5405.6513(6)	0.001	280		4p	<sup>3</sup> F <sup>2</sup> s <sup>2</sup>	<sup>3</sup> F <sup>2</sup>		Ric		
5407.447(3)	18487.877(11)	5407.4452(23)	0.001	280		5s	(3/2) <sup>1</sup> 3/2 <sub>2</sub> sp	( <sup>1</sup> D) <sup>3</sup> P <sup>3</sup> D <sup>2</sup>		Ric		
5408.383(4)	18484.675(12)	5408.3840(24)	-0.001	280		5s	(3/2) <sup>1</sup> 3/2 <sub>1</sub> sp	( <sup>1</sup> D) <sup>3</sup> P <sup>3</sup> D <sup>2</sup>		Ric		
5422.002(3)	18438.246(12)	5422.0053(21)	-0.003	140		4f	(5/2) <sup>1</sup> 9/2 <sub>1</sub> <sup>4</sup> 7g	(5/2) <sup>1</sup> 9/2 <sub>1</sub>		Ric		
5422.392(3)	18436.920(11)	5422.3947(19)	-0.003	270		4f	(5/2) <sup>1</sup> 7/2 <sub>2</sub> 7g	(5/2) <sup>1</sup> 11/2 <sub>2</sub>	7.e+06	Ric		TW
5428.274(3)	18416.944(11)	5428.2744(9)	0.001	140		4d	(5/2) <sup>1</sup> 7/2 <sub>2</sub> sp	( <sup>3</sup> F) <sup>3</sup> P <sup>3</sup> F <sup>3</sup>		Ric		
5437.1438(21)	18386.899(7)	5437.1431(5)	0.0006	2100		4d	(3/2) <sup>1</sup> 7/2 <sub>1</sub> 4f	(5/2) <sup>1</sup> 9/2 <sub>1</sub> <sup>4</sup>		Ric		
5437.5787(23)	18385.428(8)	5437.5790(4)	-0.0002	6700		4d	(3/2) <sup>1</sup> 7/2 <sub>1</sub> 4f	(5/2) <sup>1</sup> 7/2 <sub>1</sub> <sup>4</sup>		Ric		
5441.6461(22)	18371.686(7)	5441.6471(9)	-0.0011	2100		4d	(5/2) <sup>1</sup> 7/2 <sub>1</sub> sp	( <sup>3</sup> F) <sup>3</sup> P <sup>3</sup> F <sup>3</sup>		Ric		
5448.1914(23)	18349.615(8)	5448.1938(9)	-0.0024	260		4d	(5/2) <sup>1</sup> 7/2 <sub>1</sub> sp	( <sup>3</sup> F) <sup>3</sup> P <sup>3</sup> D <sup>2</sup>		Ric		
5449.409(4)	18345.516(12)	5449.4072(10)	0.002	2700		4d	(5/2) <sup>1</sup> 3/2 <sub>2</sub> sp	( <sup>3</sup> F) <sup>3</sup> P <sup>3</sup> D <sup>2</sup>		Ric		
5458.0942(22)	18316.323(7)	5458.0941(9)	0.0001	390		4d	(3/2) <sup>1</sup> 5/2 <sub>2</sub> sp	( <sup>3</sup> F) <sup>3</sup> P <sup>3</sup> D <sup>2</sup>		Ric		
5466.57(6)	18287.94(20)	5466.5527(5)	0.01	1600	*	4d	(3/2) <sup>1</sup> 7/2 <sub>1</sub> 4f	(5/2) <sup>1</sup> 5/2 <sub>1</sub> <sup>3</sup>		Ric		
5466.57(6)	18287.94(20)	5466.6267(9)	-0.06	1600	*	4d	(5/2) <sup>1</sup> 5/2 <sub>2</sub> sp	( <sup>3</sup> F) <sup>3</sup> P <sup>3</sup> D <sup>2</sup>		Ric		
5468.563(3)	18281.260(9)	5468.5633(19)	-0.000	510		5s	(3/2) <sup>1</sup> 3/2 <sub>1</sub> sp	( <sup>1</sup> D) <sup>3</sup> P <sup>3</sup> F <sup>3</sup>		Ric		
5469.576(5)	18278.541(10)	5469.5734(6)	0.005	1300		4d	(3/2) <sup>1</sup> 3/2 <sub>2</sub> sp	( <sup>3</sup> F) <sup>3</sup> P <sup>3</sup> F <sup>3</sup>		Ric		
5469.6826(21)	18277.518(7)	5469.6819(4)	0.0006	4400		4d	(3/2) <sup>1</sup> 7/2 <sub>1</sub> 4f	(5/2) <sup>1</sup> 9/2 <sub>1</sub> <sup>5</sup>		Ric		
5472.465(3)	18268.225(11)	5472.4631(10)	0.002	130		4d	(3/2) <sup>1</sup> 5/2 <sub>2</sub> sp	( <sup>3</sup> F) <sup>3</sup> P <sup>3</sup> D <sup>2</sup>		Ric		
5472.9473(24)	18266.614(8)	5472.9467(5)	0.0007	740		4d	(3/2) <sup>1</sup> 7/2 <sub>1</sub> 4f	(5/2) <sup>1</sup> 5/2 <sub>1</sub> <sup>2</sup>		Ric		
5473.01	18266.42	5473.006(2)			:	sp	( <sup>3</sup> F) <sup>3</sup> P <sup>3</sup> F <sup>3</sup> 7g	(5/2) <sup>1</sup> 9/2 <sub>1</sub>		Ric		
5473.119(4)	18266.040(12)	5473.1211(8)	-0.002	920		4f	(5/2) <sup>1</sup> 5/2 <sub>1</sub> <sup>2</sup> 5d	(3/2) <sup>1</sup> 5/2 <sub>2</sub>		Ric		
		5473.1623(16)			m	4f	(5/2) <sup>1</sup> 7/2 <sub>1</sub> <sup>3</sup> 9s	(5/2) <sup>1</sup> 5/2 <sub>2</sub>		Ric		
5477.127(3)	18252.676(11)	5477.1275(13)	-0.001	130		4d	(3/2) <sup>1</sup> 1/2 <sub>1</sub> sp	( <sup>3</sup> F) <sup>3</sup> P <sup>3</sup> F <sup>3</sup> 0		Ric		
5478.0268(23)	18249.677(8)	5478.0262(4)	0.0006	3700		4d	(3/2) <sup>1</sup> 7/2 <sub>1</sub> 4f	(5/2) <sup>1</sup> 7/2 <sub>1</sub> <sup>5</sup>		Ric		
5479.9089(22)	18245.409(7)	5479.9071(7)	0.0018	3700		5p	(5/2) <sup>1</sup> 5/2 <sub>1</sub> <sup>2</sup> 5d	(3/2) <sup>1</sup> 5/2 <sub>2</sub>		Ric		
5480.1613(24)	18240.569(8)	5480.1619(5)	-0.0006	1900		4d	(3/2) <sup>1</sup> 7/2 <sub>1</sub> 4f	(5/2) <sup>1</sup> 7/2 <sub>1</sub> <sup>3</sup>		Ric		
5482.524(3)	18234.708(10)	5482.5262(15)	-0.002	790		sp	( <sup>3</sup> F) <sup>3</sup> P <sup>3</sup> C <sup>3</sup> 6s	(5/2) <sup>1</sup> 5/2 <sub>2</sub>		Ric		
5486.205(3)	18222.473(11)	5486.2057(8)	0.001	120		5p	(5/2) <sup>1</sup> 3/2 <sub>1</sub> <sup>2</sup> 5d	(3/2) <sup>1</sup> 5/2 <sub>2</sub>		Ric		
5493.5268(22)	18198.186(7)	5493.5289(6)	-0.0021	240		5p	(5/2) <sup>1</sup> 7/2 <sub>1</sub> <sup>3</sup> 5d	(3/2) <sup>1</sup> 7/2 <sub>1</sub>		Ric		
5495.0154(23)	18193.157(8)	5495.0146(23)	0.0008	430		5s	(3/2) <sup>1</sup> 3/2 <sub>2</sub> sp	( <sup>1</sup> D) <sup>3</sup> P <sup>3</sup> F <sup>3</sup>		Ric		
5496.868(5)	18187.126(11)	5496.8685(11)	-0.0001	510		4d	(3/2) <sup>1</sup> 3/2 <sub>1</sub> sp	( <sup>3</sup> F) <sup>3</sup> P <sup>3</sup> F <sup>3</sup> 2		Ric		
5504.021(4)	18163.488(12)	5504.0359(5)	-0.035	120	?	4d	(5/2) <sup>1</sup> 3/2 <sub>2</sub> sp	( <sup>3</sup> F) <sup>3</sup> P <sup>3</sup> D <sup>2</sup>		Ric		
5504.844(3)	18160.774(11)	5504.8442(11)	-0.000	240		4d	(5/2) <sup>1</sup> 3/2 <sub>1</sub> sp	( <sup>3</sup> F) <sup>3</sup> P <sup>3</sup> D <sup>2</sup>		Ric		
5507.428(4)	18152.254(12)	5507.4337(4)	-0.006	240		4d	(5/2) <sup>1</sup> 7/2 <sub>1</sub> 4f	(3/2) <sup>1</sup> 5/2 <sub>1</sub> <sup>2</sup>		Ric		
5512.8649(22)	18134.351(7)	5512.8650(6)	-0.0001	240		5p	(5/2) <sup>1</sup> 7/2 <sub>1</sub> <sup>3</sup> 5d	(3/2) <sup>1</sup> 7/2 <sub>1</sub>		Ric		X

Table A1. Cont.

$\lambda_{\text{obs}}^a$ (Å)	$\sigma_{\text{obs}}^b$ (cm <sup>-1</sup> )	$\lambda_{\text{Ritz}}^c$ (Å)	$\Delta\lambda_{\text{obs-Ritz}}^d$ (Å)	$I_{\text{obs}}^d$ (arb. u.)	Char <sup>e</sup>	Lower Level	Upper Level	A (s <sup>-1</sup> )	Acc <sup>f</sup>	Line Ref. <sup>g</sup>	TP Ref. <sup>h</sup>	Notes <sup>b</sup>
5521.249(3)	18106.815(9)	5521.2475(5)	0.001	230	4d	(3/2) <sup>3</sup> P <sup>o</sup> 7/2 <sub>1/2</sub>	(5/2) <sup>3</sup> F <sup>o</sup> 7/2 <sup>o</sup> <sub>3</sub>			Ric		
5521.729(3)	18105.239(9)	5521.7315(8)	-0.002	1100	5p	(5/2) <sup>3</sup> F <sup>o</sup> 7/2 <sub>1/2</sub>	(5/2) <sup>3</sup> F <sup>o</sup> 7/2 <sub>1/2</sub>			Ric		
5525.438(3)	18093.088(9)	5525.4391(6)	-0.001	230	5p	(3/2) <sup>3</sup> P <sup>o</sup> 5/2 <sub>1/2</sub>	(3/2) <sup>3</sup> P <sup>o</sup> 5/2 <sub>1/2</sub>			Ric		
5525.53	18092.78	5525.532(6)			:	( <sup>3</sup> F) <sup>3</sup> P <sup>o</sup> 3D <sup>o</sup> 7/2 <sub>1/2</sub>	( <sup>3</sup> F) <sup>3</sup> P <sup>o</sup> 3D <sup>o</sup> 7/2 <sub>1/2</sub>			Ric		
5527.1968(22)	18087.330(7)	5527.1993(7)	-0.0025	2200	4d	(3/2) <sup>3</sup> P <sup>o</sup> 7/2 <sub>1/2</sub>	( <sup>3</sup> F) <sup>3</sup> P <sup>o</sup> 3C <sup>o</sup> 4			Ric		
5527.6813(22)	18085.744(7)	5527.6804(5)	0.0009	690	4d	(3/2) <sup>3</sup> P <sup>o</sup> 7/2 <sub>1/2</sub>	(5/2) <sup>3</sup> F <sup>o</sup> 5/2 <sub>1/2</sub>			Ric		
5534.668(3)	18062.913(10)	5534.6726(8)	-0.004	230	5p	(5/2) <sup>3</sup> F <sup>o</sup> 7/2 <sub>1/2</sub>	(5/2) <sup>3</sup> F <sup>o</sup> 7/2 <sub>1/2</sub>			Ric		
5535.0494(22)	18061.669(7)	5535.0478(6)	0.0016	4100	5p	(5/2) <sup>3</sup> F <sup>o</sup> 7/2 <sub>1/2</sub>	(5/2) <sup>3</sup> F <sup>o</sup> 7/2 <sub>1/2</sub>			Ric		
5537.670(20)	18053.12(7)	5537.6662(21)	0.004	340	4d	( <sup>3</sup> F) <sup>3</sup> P <sup>o</sup> 3C <sup>o</sup> 4	(5/2) <sup>3</sup> F <sup>o</sup> 7/2 <sub>1/2</sub>			Ric		
5538.3836(22)	18050.796(7)	5538.3835(6)	0.0001	880	5p	(3/2) <sup>3</sup> P <sup>o</sup> 7/2 <sub>1/2</sub>	(5/2) <sup>3</sup> F <sup>o</sup> 7/2 <sub>1/2</sub>			Ric		
5541.6120(20)	18040.280(7)	5541.6123(6)	-0.0003	1300	5p	(5/2) <sup>3</sup> F <sup>o</sup> 7/2 <sub>1/2</sub>	(5/2) <sup>3</sup> F <sup>o</sup> 7/2 <sub>1/2</sub>			Ric		
5543.5368(22)	18034.016(7)	5543.5385(7)	-0.0016	1900	5p	( <sup>3</sup> F) <sup>3</sup> P <sup>o</sup> 3F <sup>o</sup> 2	(5/2) <sup>3</sup> F <sup>o</sup> 7/2 <sub>1/2</sub>			Ric		
5544.7815(22)	18029.968(7)	5544.7803(6)	0.0012	220	4d	(3/2) <sup>3</sup> P <sup>o</sup> 7/2 <sub>1/2</sub>	(5/2) <sup>3</sup> F <sup>o</sup> 7/2 <sub>1/2</sub>			Ric		
5555.5129(22)	17995.143(7)	5555.5123(7)	-0.0001	5500	5p	( <sup>3</sup> F) <sup>3</sup> P <sup>o</sup> 3F <sup>o</sup> 2	(5/2) <sup>3</sup> F <sup>o</sup> 7/2 <sub>1/2</sub>			Ric		
5558.314(3)	17986.072(11)	5558.3108(10)	0.003	110	4d	(3/2) <sup>3</sup> P <sup>o</sup> 7/2 <sub>1/2</sub>	( <sup>3</sup> F) <sup>3</sup> P <sup>o</sup> 3D <sup>o</sup> 3			Ric		
5559.417(4)	17982.504(11)	5559.4167(5)	0.000	110	4d	(3/2) <sup>3</sup> P <sup>o</sup> 7/2 <sub>1/2</sub>	(5/2) <sup>3</sup> F <sup>o</sup> 7/2 <sub>1/2</sub>			Ric		
5560.3761(24)	17978.755(8)	5560.3739(8)	0.0022	610	5p	(5/2) <sup>3</sup> F <sup>o</sup> 7/2 <sub>1/2</sub>	(5/2) <sup>3</sup> F <sup>o</sup> 7/2 <sub>1/2</sub>			Ric		
5562.074(3)	17973.913(11)	5562.0730(8)	0.001	110	4d	(3/2) <sup>3</sup> P <sup>o</sup> 7/2 <sub>1/2</sub>	(5/2) <sup>3</sup> F <sup>o</sup> 7/2 <sub>1/2</sub>			Ric		
5562.6460(23)	17972.065(7)	5562.6478(9)	-0.0018	770	4d	(5/2) <sup>3</sup> F <sup>o</sup> 7/2 <sub>1/2</sub>	( <sup>3</sup> F) <sup>3</sup> P <sup>o</sup> 3D <sup>o</sup> 1			Ric		
5567.002(3)	17958.004(9)	5567.0018(8)	-0.000	4d	4d	(3/2) <sup>3</sup> P <sup>o</sup> 7/2 <sub>1/2</sub>	( <sup>3</sup> F) <sup>3</sup> P <sup>o</sup> 3F <sup>o</sup> 3			Ric		
5569.670(3)	17949.401(11)	5569.6723(16)	-0.002	210	5d	(5/2) <sup>3</sup> F <sup>o</sup> 7/2 <sub>1/2</sub>	(5/2) <sup>3</sup> F <sup>o</sup> 7/2 <sub>1/2</sub>			Ric		
5571.6406(24)	17943.052(8)	5571.6415(7)	-0.0009	210	5p	(5/2) <sup>3</sup> F <sup>o</sup> 7/2 <sub>1/2</sub>	(5/2) <sup>3</sup> F <sup>o</sup> 7/2 <sub>1/2</sub>			Ric		
5578.4586(23)	17921.196(7)	5578.4537(17)	0.0019	520	5d	(3/2) <sup>3</sup> P <sup>o</sup> 7/2 <sub>1/2</sub>	(5/2) <sup>3</sup> F <sup>o</sup> 7/2 <sub>1/2</sub>	1.0e+07	D+		TW	
5579.431(4)	17917.999(12)	5579.4269(20)	0.004	210	5d	(5/2) <sup>3</sup> F <sup>o</sup> 7/2 <sub>1/2</sub>	(5/2) <sup>3</sup> F <sup>o</sup> 7/2 <sub>1/2</sub>			Ric		
5581.9475(24)	17909.921(8)	5581.9507(9)	-0.0032	310	4d	(3/2) <sup>3</sup> P <sup>o</sup> 7/2 <sub>1/2</sub>	( <sup>3</sup> F) <sup>3</sup> P <sup>o</sup> 3F <sup>o</sup> 3			Ric		
5582.173(4)	17909.196(11)	5582.1725(18)	0.001	100	5d	(5/2) <sup>3</sup> F <sup>o</sup> 7/2 <sub>1/2</sub>	(5/2) <sup>3</sup> F <sup>o</sup> 7/2 <sub>1/2</sub>			Ric		
5583.864(3)	17903.773(11)	5583.8665(11)	-0.002	210	4d	(3/2) <sup>3</sup> P <sup>o</sup> 7/2 <sub>1/2</sub>	( <sup>3</sup> F) <sup>3</sup> P <sup>o</sup> 3P <sup>o</sup> 1			Ric		
5584.346(3)	17902.330(11)	5584.3413(22)	0.004	480	5d	(3/2) <sup>3</sup> P <sup>o</sup> 7/2 <sub>1/2</sub>	(5/2) <sup>3</sup> F <sup>o</sup> 7/2 <sub>1/2</sub>	9.e+06	D+		TW	
5591.382(3)	17879.700(9)	5591.377(6)	0.005	210	5p	( <sup>3</sup> F) <sup>3</sup> P <sup>o</sup> 3F <sup>o</sup> 2	(5/2) <sup>3</sup> F <sup>o</sup> 7/2 <sub>1/2</sub>			Ric		
5592.5298(24)	17876.032(8)	5592.5272(19)	0.0026	510	5d	(5/2) <sup>3</sup> F <sup>o</sup> 7/2 <sub>1/2</sub>	(5/2) <sup>3</sup> F <sup>o</sup> 7/2 <sub>1/2</sub>	9.e+06	D+		TW	
5593.7697(13)	17872.070(4)	5593.7708(4)	-0.0011	5400	4d	(3/2) <sup>3</sup> P <sup>o</sup> 7/2 <sub>1/2</sub>	(5/2) <sup>3</sup> F <sup>o</sup> 7/2 <sub>1/2</sub>			F,Re		
5600.4662(23)	17850.701(7)	5600.4661(5)	0.0001	500	300	(3/2) <sup>3</sup> P <sup>o</sup> 7/2 <sub>1/2</sub>	(5/2) <sup>3</sup> F <sup>o</sup> 7/2 <sub>1/2</sub>			Ric		
5600.381(4)	17850.334(11)	5600.3810(10)	0.000	300	4d	(3/2) <sup>3</sup> P <sup>o</sup> 7/2 <sub>1/2</sub>	( <sup>3</sup> F) <sup>3</sup> P <sup>o</sup> 3D <sup>o</sup> 3			Ric		
5607.282(3)	17829.001(9)	5607.2823(22)	0.000	300	5d	(3/2) <sup>3</sup> P <sup>o</sup> 7/2 <sub>1/2</sub>	(5/2) <sup>3</sup> F <sup>o</sup> 7/2 <sub>1/2</sub>	8.e+06	D+		TW	
5608.027(3)	17826.635(8)	5608.0216(5)	0.005	200	4d	(3/2) <sup>3</sup> P <sup>o</sup> 7/2 <sub>1/2</sub>	(5/2) <sup>3</sup> F <sup>o</sup> 7/2 <sub>1/2</sub>			Ric		
5615.2350(23)	17803.751(7)	5615.2379(6)	-0.0030	5500	5p	(5/2) <sup>3</sup> F <sup>o</sup> 7/2 <sub>1/2</sub>	(5/2) <sup>3</sup> F <sup>o</sup> 7/2 <sub>1/2</sub>			Ric		
5618.016(3)	17794.938(11)	5618.0200(6)	-0.004	98	4d	(3/2) <sup>3</sup> P <sup>o</sup> 7/2 <sub>1/2</sub>	(5/2) <sup>3</sup> F <sup>o</sup> 7/2 <sub>1/2</sub>			Ric		
5619.885(7)	17789.021(12)	5619.8874(16)	-0.003	190	4d	(3/2) <sup>3</sup> P <sup>o</sup> 7/2 <sub>1/2</sub>	( <sup>3</sup> F) <sup>3</sup> P <sup>o</sup> 5S <sup>o</sup> 2			Ric		
5620.7814(23)	17786.183(7)	5620.7805(5)	0.0008	850	5d	(3/2) <sup>3</sup> P <sup>o</sup> 7/2 <sub>1/2</sub>	(5/2) <sup>3</sup> F <sup>o</sup> 7/2 <sub>1/2</sub>			Ric		
5621.7027(24)	17783.268(8)	5621.7019(10)	0.0009	530	4d	(5/2) <sup>3</sup> F <sup>o</sup> 7/2 <sub>1/2</sub>	( <sup>3</sup> F) <sup>3</sup> P <sup>o</sup> 3D <sup>o</sup> 1			Ric		
5629.240(3)	17759.456(11)	5629.218(3)	0.022	190	5d	(5/2) <sup>3</sup> F <sup>o</sup> 7/2 <sub>1/2</sub>	(5/2) <sup>3</sup> F <sup>o</sup> 7/2 <sub>1/2</sub>			Ric		
5630.589(4)	17755.202(11)	5630.5900(18)	-0.001	95	5d	(5/2) <sup>3</sup> F <sup>o</sup> 7/2 <sub>1/2</sub>	(5/2) <sup>3</sup> F <sup>o</sup> 7/2 <sub>1/2</sub>			Ric		X

Table A1. Cont.

$\lambda_{obs}^a$ (Å)	$\sigma_{obs}^b$ (cm <sup>-1</sup> )	$\lambda_{Ritz}^c$ (Å)	$\Delta\lambda_{obs-Ritz}^d$ (Å)	$I_{obs}^d$ (arb. u.)	Char <sup>e</sup>	Lower Level	Upper Level	A (s <sup>-1</sup> )	Acc <sup>f</sup>	Line Ref. <sup>g</sup>	TP Ref. <sup>h</sup>	Notes <sup>b</sup>
5631.153(3)	17753.425(11)	5631.156(18)	-0.003	190		5d	(5/2) <sup>3</sup> F <sub>7/2</sub> <sup>o</sup> 7f	(5/2) <sup>3</sup> F <sub>7/2</sub> <sup>o</sup> 7f		Ric		
5631.358(3)	17752.777(11)	5631.360(20)	-0.002	95		5d	(5/2) <sup>3</sup> F <sub>5/2</sub> <sup>o</sup> 7f	(5/2) <sup>3</sup> F <sub>5/2</sub> <sup>o</sup> 7f		Ric		
5633.044(23)	17747.464(7)	5633.046(15)	-0.0020	3400		4d	(3/2) <sup>3</sup> F <sub>3/2</sub> <sup>o</sup> 4f	(3/2) <sup>3</sup> F <sub>3/2</sub> <sup>o</sup> 4f		Ric		
5633.602(3)	17745.707(10)	5633.603(12)	-0.001	950		4d	(5/2) <sup>3</sup> F <sub>5/2</sub> <sup>o</sup> 3C <sup>+</sup>	( <sup>3</sup> F) <sup>3</sup> P <sup>+</sup> 3C <sup>+</sup>		Ric		
5635.5118(23)	17739.693(7)	5635.5130(11)	-0.0012	3000		4d	(5/2) <sup>3</sup> F <sub>7/2</sub> <sup>o</sup> sp	( <sup>3</sup> F) <sup>3</sup> P <sup>+</sup> 3C <sup>+</sup>		Ric		
5637.162(4)	17734.501(13)	5637.1546(21)	0.007	190		sp	( <sup>3</sup> F) <sup>3</sup> P <sup>+</sup> 3C <sup>+</sup>	(5/2) <sup>3</sup> F <sub>7/2</sub> <sup>o</sup> 5d		Ric		
5637.468(3)	17733.536(8)	5637.4686(8)	-0.000	1100		sp	( <sup>3</sup> F) <sup>3</sup> P <sup>+</sup> 3F <sup>+</sup>	(5/2) <sup>3</sup> F <sub>3/2</sub> <sup>o</sup> 5d		Ric		
5641.2645(23)	17721.603(7)	5641.26453(18)	-0.0000	2300		5p	(3/2) <sup>3</sup> F <sub>3/2</sub> <sup>o</sup> 1 5d	(3/2) <sup>3</sup> F <sub>3/2</sub> <sup>o</sup> 1/2 5d		Ric		
5643.5338(24)	17714.477(8)	5643.5346(7)	-0.0008	280		sp	( <sup>3</sup> F) <sup>3</sup> P <sup>+</sup> 3F <sup>+</sup>	(5/2) <sup>3</sup> F <sub>3/2</sub> <sup>o</sup> 2 5d		Ric		
5648.0170(24)	17700.416(8)	5648.0161(6)	0.0009	430		4d	(3/2) <sup>3</sup> F <sub>3/2</sub> <sup>o</sup> 4f	(5/2) <sup>3</sup> F <sub>3/2</sub> <sup>o</sup> 1 6s		Ric		
5651.708(4)	17688.857(11)	5651.7093(9)	-0.001	370		5p	( <sup>3</sup> F) <sup>3</sup> P <sup>+</sup> 3D <sup>+</sup>	(5/2) <sup>3</sup> F <sub>7/2</sub> <sup>o</sup> 1 5d		Ric		
5656.632(3)	17673.459(10)	5656.6271(10)	0.005	7300		5p	(5/2) <sup>3</sup> F <sub>5/2</sub> <sup>o</sup> 4f	(5/2) <sup>3</sup> F <sub>7/2</sub> <sup>o</sup> 4f		Ric		
5664.4833(23)	17648.963(7)	5664.4829(5)	0.0004	2900		4d	(3/2) <sup>3</sup> F <sub>5/2</sub> <sup>o</sup> 4f	(5/2) <sup>3</sup> F <sub>7/2</sub> <sup>o</sup> 4		Ric		TW
5667.134(3)	17639.775(11)	5667.1344(19)	-0.001	180		5d	(5/2) <sup>3</sup> F <sub>7/2</sub> <sup>o</sup> 7f	(5/2) <sup>3</sup> F <sub>7/2</sub> <sup>o</sup> 4	5.8e+06	Ric		
5668.007(3)	17637.991(10)	5668.0080(18)	-0.001	180		5d	(5/2) <sup>3</sup> F <sub>7/2</sub> <sup>o</sup> 7f	(5/2) <sup>3</sup> F <sub>7/2</sub> <sup>o</sup> 5		Ric		
5670.329(3)	17630.769(10)	5670.3245(16)	0.004	350		5d	(5/2) <sup>3</sup> F <sub>7/2</sub> <sup>o</sup> 7f	(5/2) <sup>3</sup> F <sub>7/2</sub> <sup>o</sup> 5	7.4e+06	Ric		
5674.694(4)	17617.207(12)	5674.6947(7)	-0.001	180	*	sp	( <sup>3</sup> F) <sup>3</sup> P <sup>+</sup> 3F <sup>+</sup>	(3/2) <sup>3</sup> F <sub>3/2</sub> <sup>o</sup> 6s		Ric		
5674.694(4)	17617.207(12)	5674.6968(9)	-0.003	1300	*	sp	( <sup>3</sup> F) <sup>3</sup> P <sup>+</sup> 1F <sup>+</sup>	(3/2) <sup>3</sup> F <sub>3/2</sub> <sup>o</sup> 5d		Ric		
5676.005(3)	17613.137(10)	5676.0028(11)	0.002	1300		4d	(5/2) <sup>3</sup> F <sub>7/2</sub> <sup>o</sup> sp	( <sup>3</sup> F) <sup>3</sup> P <sup>+</sup> 3D <sup>+</sup>		Ric		
5678.556(3)	17605.224(11)	5678.554(3)	0.002	87		5d	(5/2) <sup>3</sup> F <sub>5/2</sub> <sup>o</sup> 7f	(5/2) <sup>3</sup> F <sub>7/2</sub> <sup>o</sup> 3		Ric		
5681.353(3)	17596.559(11)	5681.3597(11)	-0.007	87		4d	(5/2) <sup>3</sup> F <sub>5/2</sub> <sup>o</sup> sp	( <sup>3</sup> F) <sup>3</sup> P <sup>+</sup> 3D <sup>+</sup>		Ric		
5681.998(3)	17594.559(9)	5681.9923(7)	0.006	430		sp	( <sup>3</sup> F) <sup>3</sup> P <sup>+</sup> 1F <sup>+</sup>	(3/2) <sup>3</sup> F <sub>5/2</sub> <sup>o</sup> 5d		Ric		
5682.433(3)	17593.214(9)	5682.4316(9)	0.001	2100		sp	( <sup>3</sup> F) <sup>3</sup> P <sup>+</sup> 3D <sup>+</sup>	(3/2) <sup>3</sup> F <sub>5/2</sub> <sup>o</sup> 1 6s		Ric		
5689.83(4)	17570.341(2)	5689.8869(11)	-0.06	170		4d	(3/2) <sup>3</sup> F <sub>3/2</sub> <sup>o</sup> 2 5d	( <sup>3</sup> F) <sup>3</sup> P <sup>+</sup> 3D <sup>+</sup>		S56c		
5694.526(3)	17555.852(10)	5694.5233(14)	0.001	170		4d	(3/2) <sup>3</sup> F <sub>3/2</sub> <sup>o</sup> 2 5d	( <sup>3</sup> F) <sup>3</sup> P <sup>+</sup> 3D <sup>+</sup>		Ric		
5695.931(3)	17551.521(10)	5695.9321(5)	-0.001	340		4d	(3/2) <sup>3</sup> F <sub>3/2</sub> <sup>o</sup> 4f	(5/2) <sup>3</sup> F <sub>5/2</sub> <sup>o</sup> 3		Ric		
5706.012(4)	17520.514(12)	5706.0055(7)	0.006	450		4p	1F <sup>+</sup>	3P <sub>2</sub>		Ric		
5710.7111(24)	17506.097(7)	5710.7089(5)	0.0022	250		4d	(3/2) <sup>3</sup> F <sub>5/2</sub> <sup>o</sup> 4f	(5/2) <sup>3</sup> F <sub>7/2</sub> <sup>o</sup> 3		Ric		
5711.586(4)	17503.416(11)	5711.5823(5)	0.003	250		4d	(3/2) <sup>3</sup> F <sub>5/2</sub> <sup>o</sup> 4f	(5/2) <sup>3</sup> F <sub>5/2</sub> <sup>o</sup> 3		Ric		
5721.7840(24)	17472.220(7)	5721.7856(7)	-0.0015	4100		4p	3P <sup>+</sup>	1D <sub>2</sub>		Ric		
5726.442(3)	17458.009(11)	5726.4406(6)	0.001	160		4d	(3/2) <sup>3</sup> F <sub>5/2</sub> <sup>o</sup> 4f	(5/2) <sup>3</sup> F <sub>7/2</sub> <sup>o</sup> 3		Ric		
5731.004(4)	17444.110(12)	5731.0007(11)	0.004	160		4d	(3/2) <sup>3</sup> F <sub>3/2</sub> <sup>o</sup> 1 5d	( <sup>3</sup> F) <sup>3</sup> P <sup>+</sup> 3D <sup>+</sup>		Ric		
5736.659(4)	17426.915(11)	5736.6603(5)	-0.001	160		4d	(3/2) <sup>3</sup> F <sub>5/2</sub> <sup>o</sup> 4f	(5/2) <sup>3</sup> F <sub>3/2</sub> <sup>o</sup> 2		Ric		
5752.536(4)	17378.816(11)	5752.5355(6)	0.000	580		4d	(3/2) <sup>3</sup> F <sub>5/2</sub> <sup>o</sup> 4f	(5/2) <sup>3</sup> F <sub>3/2</sub> <sup>o</sup> 2		Ric		
5759.015(4)	17359.266(11)	5759.0170(20)	-0.002	150		sp	( <sup>3</sup> F) <sup>3</sup> P <sup>+</sup> 3C <sup>+</sup>	(5/2) <sup>3</sup> F <sub>11/2</sub> <sup>o</sup> 6		Ric		
5759.4219(24)	17358.040(7)	5759.4213(7)	0.0005	6300		sp	( <sup>3</sup> F) <sup>3</sup> P <sup>+</sup> 1F <sup>+</sup>	(3/2) <sup>3</sup> F <sub>7/2</sub> <sup>o</sup> 5d		Ric		
5761.220(3)	17352.622(8)	5761.2165(10)	0.004	2200		sp	( <sup>3</sup> F) <sup>3</sup> P <sup>+</sup> 3D <sup>+</sup>	(5/2) <sup>3</sup> F <sub>5/2</sub> <sup>o</sup> 2 6s		Ric		
5761.8052(24)	17330.860(7)	5761.8056(7)	-0.0003	2200		4d	(3/2) <sup>3</sup> F <sub>5/2</sub> <sup>o</sup> 4f	( <sup>3</sup> F) <sup>3</sup> P <sup>+</sup> 3G <sup>+</sup>		Ric		
5768.143(4)	17331.796(11)	5768.1482(7)	-0.005	150		4d	(3/2) <sup>3</sup> F <sub>5/2</sub> <sup>o</sup> 4f	(5/2) <sup>3</sup> F <sub>11/2</sub> <sup>o</sup> 1		Ric		
5779.656(4)	17297.270(12)	5779.6592(8)	-0.003	360		sp	( <sup>3</sup> F) <sup>3</sup> P <sup>+</sup> 3F <sup>+</sup>	(5/2) <sup>3</sup> F <sub>11/2</sub> <sup>o</sup> 1		Ric		
5783.920(4)	17284.519(11)	5783.9194(20)	0.001	6400		5p	(3/2) <sup>3</sup> F <sub>3/2</sub> <sup>o</sup> 1 5d	(5/2) <sup>3</sup> F <sub>3/2</sub> <sup>o</sup> 1/2 5d		Ric		
5801.130(7)	17233.242(12)	5801.116(3)	0.014	140		5s	(5/2) <sup>3</sup> F <sub>5/2</sub> <sup>o</sup> 2 6s	( <sup>3</sup> F) <sup>3</sup> P <sup>+</sup> 5P <sup>+</sup>		Ric		

Table A1. Cont.

$\lambda_{\text{obs}}^a$ (Å)	$\sigma_{\text{obs}}^b$ (cm <sup>-1</sup> )	$\lambda_{\text{Ritz}}^c$ (Å)	$\Delta\lambda_{\text{obs-Ritz}}^d$ (Å)	$I_{\text{obs}}^d$ (arb. u.)	Char <sup>e</sup>	Lower Level	Upper Level	A (s <sup>-1</sup> )	Acc <sup>f</sup>	Line Ref. <sup>g</sup>	TP Ref. <sup>h</sup>	Notes <sup>b</sup>
5805.989(3)	17218.822(8)	5805.9869(11)	0.002	4700	sp	( <sup>3</sup> P) <sup>3</sup> P <sup>o</sup> 3s	(5/2) <sup>2</sup> 15/21 <sub>h</sub>			Ric		
5825.824(2)	17160.200(7)	5825.8247(9)	-0.002	9100	sp	( <sup>3</sup> P) <sup>3</sup> P <sup>o</sup> 1D <sup>o</sup> 2	(3/2) <sup>2</sup> 15/21 <sub>h</sub>	1.1e+07	D+	Ric	TW	
5833.514(1)	17137.573(7)	5833.5141(7)	0.0005	6400	sp	( <sup>3</sup> F) <sup>3</sup> P <sup>o</sup> 1D <sup>o</sup> 2	(3/2) <sup>2</sup> 15/21 <sub>h</sub>	7.9e+06	D+	Ric	TW	
5836.619(4)	17128.458(13)	5836.6234(11)	-0.004	130	4d	(3/2) <sup>2</sup> 11/21 <sub>h</sub>	( <sup>3</sup> P) <sup>3</sup> P <sup>o</sup> 3D <sup>o</sup> 1			Ric		
5842.495(3)	17111.233(8)	5842.4918(7)	0.003	1900	4p	1D <sup>o</sup> 2	3P <sub>1</sub>			Ric		
5851.787(4)	17084.062(11)	5851.7811(12)	0.006	930	sp	( <sup>3</sup> P) <sup>3</sup> P <sup>o</sup> 3C <sup>o</sup> 3	(5/2) <sup>2</sup> 15/21 <sub>h</sub>			Ric		
5858.54(1)	17064.14(3)	5858.535(5)	0.19	9100	sp	( <sup>3</sup> F) <sup>3</sup> P <sup>o</sup> 3P <sup>o</sup> 2	(3/2) <sup>2</sup> 17/21 <sub>h</sub>			Södem		X
5890.443(4)	16971.949(11)	5890.4592(12)	-0.016	1200	4d	( <sup>3</sup> F) <sup>3</sup> P <sup>o</sup> 3P <sup>o</sup> 1	( <sup>3</sup> F) <sup>3</sup> P <sup>o</sup> 3P <sup>o</sup> 1			Ric		X
5897.971(3)	16950.287(7)	5897.9758(12)	-0.005	23000	sp	( <sup>3</sup> F) <sup>3</sup> P <sup>o</sup> 3C <sup>o</sup> 3	(5/2) <sup>2</sup> 15/21 <sub>h</sub>			Ric		
5901.188(3)	16941.047(10)	5901.1910(8)	-0.003	1700	4p	3F <sup>o</sup> 3	1D <sup>o</sup> 2			Ric		
5909.753(3)	16916.494(9)	5909.7579(9)	-0.005	1500	sp	( <sup>3</sup> F) <sup>3</sup> P <sup>o</sup> 1D <sup>o</sup> 2	(3/2) <sup>2</sup> 13/21 <sub>h</sub>			Ric		
5910.813(4)	16913.460(11)	5910.8150(20)	-0.002	57	sp	( <sup>3</sup> F) <sup>3</sup> P <sup>o</sup> 3F <sup>o</sup> 4	(5/2) <sup>2</sup> 13/21 <sub>h</sub>			Ric		
5926.691(3)	16868.147(8)	5926.6916(6)	-0.000	1300	4p	1D <sup>o</sup> 2	3P <sub>2</sub>			Ric		
5929.634(3)	16859.777(10)	5929.6380(11)	-0.004	110	4d	(3/2) <sup>2</sup> 17/21 <sub>h</sub>	( <sup>3</sup> F) <sup>3</sup> P <sup>o</sup> 3F <sup>o</sup> 4			Ric		
5937.576(2)	16837.224(7)	5937.5815(7)	-0.005	2000	sp	( <sup>3</sup> F) <sup>3</sup> P <sup>o</sup> 1D <sup>o</sup> 2	(3/2) <sup>2</sup> 17/21 <sub>h</sub>	1.0e+07	D+	Ric	TW	
5939.775(7)	16830.992(21)	5939.773(20)	-0.002	54	sp	( <sup>3</sup> F) <sup>3</sup> P <sup>o</sup> 3H <sup>o</sup> 4	(3/2) <sup>2</sup> 11/21 <sub>h</sub>			Ric		
5941.1951(4)	16826.9685(10)	5941.1951(3)	-0.0001	31000	5p	(5/2) <sup>2</sup> 13/21 <sub>h</sub>	(3/2) <sup>2</sup> 11/21 <sub>h</sub>	3.6e+07	D+	F_Re	TW	
5941.826(4)	16825.183(11)	5941.8291(17)	-0.003	1600	4d	(3/2) <sup>2</sup> 11/21 <sub>h</sub>	(5/2) <sup>2</sup> 13/21 <sub>h</sub>			Ric		
5979.015(3)	16720.532(8)	5979.0193(8)	-0.004	2800	sp	( <sup>3</sup> F) <sup>3</sup> P <sup>o</sup> 3F <sup>o</sup> 2	(3/2) <sup>2</sup> 13/21 <sub>h</sub>			Ric		
5988.3141(17)	16680.567(5)	5988.3135(14)	0.0006	7600	5p	(5/2) <sup>2</sup> 13/21 <sub>h</sub>	(5/2) <sup>2</sup> 13/21 <sub>h</sub>	9.e+07	D+	F_Re	TW	
5993.259(3)	16680.793(7)	5993.2605(8)	-0.001	3200	5p	(3/2) <sup>2</sup> 11/21 <sub>h</sub>	(5/2) <sup>2</sup> 13/21 <sub>h</sub>	3.0e+07	D+	F_Re	TW	
5995.902(19)	16674.307(5)	5995.9876(10)	0.0026	4600	5p	(3/2) <sup>2</sup> 13/21 <sub>h</sub>	(3/2) <sup>2</sup> 13/21 <sub>h</sub>	7.3e+07	D+	F_Re	TW	
6000.1169(8)	16661.7272(22)	6000.1168(6)	0.0001	38000	sp	(5/2) <sup>2</sup> 15/21 <sub>h</sub>	( <sup>1</sup> D) <sup>3</sup> P <sup>o</sup> 1D <sup>o</sup> 2			Ric		
6002.304(4)	16655.656(10)	6002.305(3)	-0.000	98	6s	( <sup>3</sup> F) <sup>3</sup> P <sup>o</sup> 3F <sup>o</sup> 2	(3/2) <sup>2</sup> 13/21 <sub>h</sub>			Ric		
6013.411(3)	16624.893(7)	6013.4138(8)	-0.003	3200	sp	( <sup>3</sup> F) <sup>3</sup> P <sup>o</sup> 1D <sup>o</sup> 2	(3/2) <sup>2</sup> 11/21 <sub>h</sub>			Ric		
6018.369(5)	16611.196(13)	6018.3711(12)	-0.002	480	sp	( <sup>3</sup> F) <sup>3</sup> P <sup>o</sup> 1D <sup>o</sup> 2	(3/2) <sup>2</sup> 11/21 <sub>h</sub>			Ric		
6023.263(3)	16597.700(7)	6023.2636(9)	-0.000	3900	6s	( <sup>3</sup> P) <sup>3</sup> P <sup>o</sup> 3D <sup>o</sup> 2	(5/2) <sup>2</sup> 15/21 <sub>h</sub>			Ric		
6050.917(4)	16521.845(11)	6050.916(3)	0.001	91	sp	(5/2) <sup>2</sup> 15/21 <sub>h</sub>	( <sup>1</sup> D) <sup>3</sup> P <sup>o</sup> 1D <sup>o</sup> 2			Ric		
6071.492(4)	16465.858(10)	6071.4896(22)	0.002	130	sp	( <sup>3</sup> F) <sup>3</sup> P <sup>o</sup> 3C <sup>o</sup> 3	(3/2) <sup>2</sup> 19/21 <sub>h</sub>			Ric		
6072.217(3)	16463.891(7)	6072.2167(9)	0.001	4200	sp	( <sup>3</sup> F) <sup>3</sup> P <sup>o</sup> 3P <sup>o</sup> 2	(5/2) <sup>2</sup> 15/21 <sub>h</sub>			Ric		
6080.3334(19)	16441.915(5)	6080.3370(7)	-0.0036	11000	4p	3P <sup>o</sup> 2	3P <sup>o</sup> 2			F_Re	TW	
6083.086(4)	16434.475(10)	6083.0848(22)	0.001	130	6p	(5/2) <sup>2</sup> 17/21 <sub>h</sub>	(5/2) <sup>2</sup> 19/21 <sub>h</sub>	6.9e+06	D+	Ric		
6085.021(4)	16429.250(11)	6085.021(3)	-0.000	87	4d	(5/2) <sup>2</sup> 11/21 <sub>h</sub>	( <sup>3</sup> F) <sup>3</sup> P <sup>o</sup> 5D <sup>o</sup> 1			Ric		
6093.828(3)	16396.088(8)	6097.3235(10)	0.004	4800	5p	(3/2) <sup>2</sup> 15/21 <sub>h</sub>	(3/2) <sup>2</sup> 15/21 <sub>h</sub>	1.9e+07	D+	Ric	TW	
6099.989(3)	16388.936(7)	6099.9896(7)	-0.001	3700	5p	(3/2) <sup>2</sup> 17/21 <sub>h</sub>	(3/2) <sup>2</sup> 15/21 <sub>h</sub>	9.e+06	D+	Ric	TW	
6105.747(3)	16374.480(7)	6105.7469(8)	0.000	3600	5p	(3/2) <sup>2</sup> 11/21 <sub>h</sub>	(3/2) <sup>2</sup> 15/21 <sub>h</sub>	3.3e+07	D+	F_Re	TW	
6107.005(21)	16369.034(6)	6107.4083(12)	-0.0028	5100	5p	(3/2) <sup>2</sup> 17/21 <sub>h</sub>	(3/2) <sup>2</sup> 17/21 <sub>h</sub>			Ric		
6110.872(5)	16359.748(7)	6110.8706(7)	0.002	3700	5p	(5/2) <sup>2</sup> 17/21 <sub>h</sub>	(5/2) <sup>2</sup> 17/21 <sub>h</sub>	3.4e+07	D+	F_Re	TW	
6114.4926(14)	16350.061(4)	6114.4911(7)	0.0016	15000	5p	(5/2) <sup>2</sup> 17/21 <sub>h</sub>	(5/2) <sup>2</sup> 17/21 <sub>h</sub>	3.6e+07	D+	F_Re	TW	
6150.3818(9)	16254.6548(23)	6154.3813(6)	0.0005	16000	5p	(5/2) <sup>2</sup> 17/21 <sub>h</sub>	(5/2) <sup>2</sup> 17/21 <sub>h</sub>			F_Re	TW	
6154.2215(8)	16244.5134(21)	6154.221(7)	0.0004	25000	5p	(5/2) <sup>2</sup> 13/21 <sub>h</sub>	(5/2) <sup>2</sup> 13/21 <sub>h</sub>	1.0e+08	D+	F_Re	TW	
6157.716(4)	16235.296(10)	6157.7151(10)	0.000	4700	5p	(3/2) <sup>2</sup> 15/21 <sub>h</sub>	(3/2) <sup>2</sup> 15/21 <sub>h</sub>			Ric		
6157.956(8)	16234.662(21)	6157.9650(6)	-0.009	530	5p	(5/2) <sup>2</sup> 17/21 <sub>h</sub>	(5/2) <sup>2</sup> 15/21 <sub>h</sub>			Ric		

Table A1. Cont.

$\lambda_{\text{obs}}^a$ (Å)	$\sigma_{\text{obs}}^b$ (cm <sup>-1</sup> )	$\lambda_{\text{Ritz}}^c$ (Å)	$\Delta\lambda_{\text{obs-Ritz}}^d$ (Å)	$I_{\text{obs}}^d$ (arb. u.)	Char <sup>e</sup>	Lower Level	Upper Level	A (s <sup>-1</sup> )	Acc <sup>f</sup>	Line Ref. <sup>g</sup>	TP Ref. <sup>h</sup>	Notes <sup>h</sup>
6160.573(4)	16227.65(11)	6160.5707(14)	0.003	320		4d	(3/2) <sup>-1</sup> 7/2 <sub>1</sub> sp	( <sup>3</sup> F) <sup>-3</sup> G <sup>-5</sup>		Ric		
6172.033(3)	16197.634(7)	6172.0339(8)	-0.000	16000		5p	(5/2) <sup>-1</sup> 5/2 <sub>1</sub> 5d	(5/2) <sup>-1</sup> 5/2 <sub>1</sub> 5d	D+	F_Re	TW	
6174.296(5)	16191.698(12)	6174.2920(12)	0.004	190		4d	(3/2) <sup>-1</sup> 5/2 <sub>1</sub> 5d	( <sup>3</sup> F) <sup>-3</sup> D <sup>-2</sup>	D+	Ric		
6186.8770(14)	16158.772(4)	6186.8803(8)	-0.0033	18000		5p	(5/2) <sup>-1</sup> 5/2 <sub>1</sub> 5d	(5/2) <sup>-1</sup> 5/2 <sub>1</sub> 5d	D+	F_Re	TW	
6188.6763(11)	16154.075(3)	6188.6761(7)	0.0002	12000		5p	(5/2) <sup>-1</sup> 3/2 <sub>1</sub> 6s	(5/2) <sup>-1</sup> 5/2 <sub>1</sub> 5d	D+	F_Re	TW	
6189.317(4)	16152.402(11)	6189.3237(10)	-0.007	760		5p	(3/2) <sup>-1</sup> 5/2 <sub>1</sub> 5d	(3/2) <sup>-1</sup> 3/2 <sub>1</sub> 5d		Ric		
6192.684(4)	16143.620(11)	6192.6855(12)	-0.001	76		4d	(3/2) <sup>-1</sup> 5/2 <sub>1</sub> 5d	( <sup>3</sup> P) <sup>-3</sup> D <sup>-2</sup>	D+	Ric		
6198.091(5)	16129.537(7)	6198.0890(5)	0.002	5000		5p	(5/2) <sup>-1</sup> 7/2 <sub>1</sub> 4	(3/2) <sup>-1</sup> 5/2 <sub>1</sub> 5d		Ric		
6199.751(3)	16125.219(8)	6199.7460(10)	0.005	1700		5p	(3/2) <sup>-1</sup> 5/2 <sub>1</sub> 3	(3/2) <sup>-1</sup> 5/2 <sub>1</sub> 5d		Ric		
6203.715(4)	16114.915(11)	6203.712(3)	0.004	37		6p	(5/2) <sup>-1</sup> 7/2 <sub>1</sub> 2	(3/2) <sup>-1</sup> 5/2 <sub>1</sub> 5d		Ric		
6204.2569(19)	16113.507(5)	6204.2577(10)	-0.0008	11000		5p	(3/2) <sup>-1</sup> 1/2 <sub>1</sub> 6s	(3/2) <sup>-1</sup> 5/2 <sub>1</sub> 5d	D+	F_Re	TW	
6208.4527(19)	16102.618(5)	6208.4519(8)	-0.0022	9900		5p	(3/2) <sup>-1</sup> 5/2 <sub>1</sub> 6s	(3/2) <sup>-1</sup> 5/2 <sub>1</sub> 5d	D+	F_Re	TW	
6208.988(4)	16101.230(10)	6208.9891(14)	-0.001	75		4d	(3/2) <sup>-1</sup> 7/2 <sub>1</sub> 4	( <sup>3</sup> P) <sup>-3</sup> D <sup>-3</sup>		Ric		
6214.512(4)	16086.839(11)	6214.513(2)	0.000	150		6p	(5/2) <sup>-1</sup> 3/2 <sub>1</sub> 8d	(5/2) <sup>-1</sup> 3/2 <sub>1</sub> 2d		Ric		
6216.5366(8)	16080.6383(21)	6216.9385(6)	0.0001	39000		5p	(5/2) <sup>-1</sup> 7/2 <sub>1</sub> 3	(5/2) <sup>-1</sup> 9/2 <sub>1</sub> 4d	C+	F_Re	TW	
6219.8492(9)	16073.1134(22)	6219.8488(7)	0.0005	24000		5p	(3/2) <sup>-1</sup> 5/2 <sub>1</sub> 2	(3/2) <sup>-1</sup> 7/2 <sub>1</sub> 5d	C+	F_Re	TW	
6221.288(4)	16069.396(11)	6221.2875(7)	0.001	740		5p	(5/2) <sup>-1</sup> 7/2 <sub>1</sub> 3	(5/2) <sup>-1</sup> 7/2 <sub>1</sub> 5d		Ric		
6231.396(3)	16043.331(8)	6231.3934(6)	0.002	290		5p	(5/2) <sup>-1</sup> 5/2 <sub>1</sub> 2	(5/2) <sup>-1</sup> 5/2 <sub>1</sub> 5d		Ric		
6236.344(3)	16030.601(7)	6236.3471(10)	-0.003	1200		5p	(3/2) <sup>-1</sup> 1/2 <sub>1</sub> 5d	(3/2) <sup>-1</sup> 3/2 <sub>1</sub> 2d		Ric		
6250.417(3)	15994.508(8)	6250.4216(8)	-0.005	720		5p	(5/2) <sup>-1</sup> 5/2 <sub>1</sub> 6s	(5/2) <sup>-1</sup> 5/2 <sub>1</sub> 5d		Ric		
6257.838(3)	15975.542(7)	6257.8374(7)	0.000	3400		5p	(5/2) <sup>-1</sup> 7/2 <sub>1</sub> 3	(5/2) <sup>-1</sup> 7/2 <sub>1</sub> 5d	D+	F_Re	TW	
6261.8477(13)	15965.311(3)	6261.8464(6)	0.0013	19000		5p	(5/2) <sup>-1</sup> 5/2 <sub>1</sub> 3	(5/2) <sup>-1</sup> 7/2 <sub>1</sub> 4	D+	F_Re	TW	
6265.650(5)	15955.623(7)	6265.6480(6)	0.002	2800		5p	(5/2) <sup>-1</sup> 5/2 <sub>1</sub> 4	(5/2) <sup>-1</sup> 7/2 <sub>1</sub> 5d		Ric		
6273.34762(8)	15936.04484(21)	6273.34763(8)	-0.00000	47000		5p	(5/2) <sup>-1</sup> 7/2 <sub>1</sub> 4	(5/2) <sup>-1</sup> 9/2 <sub>1</sub> 2d	C+	F_Re	TW	
6276.660(5)	15927.6361(14)	6276.6713(19)	-0.012	14000		5p	( <sup>3</sup> F) <sup>-3</sup> F <sup>-4</sup>	(5/2) <sup>-1</sup> 5/2 <sub>1</sub> 5d		Ric		
6288.695(3)	15897.154(7)	6288.6936(9)	0.001	6600		5p	(5/2) <sup>-1</sup> 5/2 <sub>1</sub> 2	(5/2) <sup>-1</sup> 3/2 <sub>1</sub> 2d	D+	Ric		
6296.239(4)	15878.107(11)	6296.2430(8)	-0.004	34		5p	(5/2) <sup>-1</sup> 5/2 <sub>1</sub> 6s	(5/2) <sup>-1</sup> 3/2 <sub>1</sub> 2d		Ric		
6299.864(5)	15868.969(11)	6299.810(3)	0.054	34	?	sp	( <sup>3</sup> P) <sup>-3</sup> 1P <sup>-2</sup>	(5/2) <sup>-1</sup> 5/2 <sub>1</sub> 5d		Ric		
6301.0135(6)	15866.0749(21)	6301.0137(7)	-0.0001	27000		5p	(3/2) <sup>-1</sup> 5/2 <sub>1</sub> 3	(5/2) <sup>-1</sup> 5/2 <sub>1</sub> 5d	C+	F_Re	TW	X
6305.9712(10)	15855.601(3)	6305.9718(8)	-0.0006	12000		5p	(5/2) <sup>-1</sup> 5/2 <sub>1</sub> 3	(5/2) <sup>-1</sup> 7/2 <sub>1</sub> 5d		Ric		
6311.3006(21)	15840.214(5)	6311.3059(5)	-0.0053	18000		5p	(5/2) <sup>-1</sup> 5/2 <sub>1</sub> 3	(5/2) <sup>-1</sup> 9/2 <sub>1</sub> 2d	D+	F_Re	TW	
6312.491(3)	15837.227(7)	6312.4915(11)	0.001	14000		5p	(5/2) <sup>-1</sup> 3/2 <sub>1</sub> 5d	(5/2) <sup>-1</sup> 5/2 <sub>1</sub> 5d		Ric		
6313.564(3)	15834.535(7)	6313.5627(7)	0.001	1000		5p	(5/2) <sup>-1</sup> 3/2 <sub>1</sub> 5d	(5/2) <sup>-1</sup> 3/2 <sub>1</sub> 5d	D+	F_Re	TW	
6317.788(3)	15823.950(7)	6317.7831(12)	0.004	1300		4p	( <sup>3</sup> P) <sup>-3</sup> 1P <sup>-2</sup>	(5/2) <sup>-1</sup> 3/2 <sub>1</sub> 5d	D+	Ric		
6318.944(5)	15821.0531(3)	6318.9422(15)	0.002	33		4d	(3/2) <sup>-1</sup> 3/2 <sub>1</sub> 6s	( <sup>3</sup> P) <sup>-3</sup> D <sup>-3</sup>		Ric		
6326.464(3)	15802.245(7)	6326.4649(8)	0.000	2500		5p	(3/2) <sup>-1</sup> 5/2 <sub>1</sub> 6s	(3/2) <sup>-1</sup> 7/2 <sub>1</sub> 5d	D+	Ric		
6357.318(3)	15725.318(7)	6357.4192(13)	-0.005	16000		5p	(3/2) <sup>-1</sup> 1/2 <sub>1</sub> 3	(3/2) <sup>-1</sup> 1/2 <sub>1</sub> 2d	D+	F_Re	TW	
6363.566(5)	15710.115(11)	6363.568(4)	-0.001	32		6p	(5/2) <sup>-1</sup> 5/2 <sub>1</sub> 3	(5/2) <sup>-1</sup> 9/2 <sub>1</sub> 2d	D+	Ric		
6373.267(3)	15686.203(8)	6373.2678(7)	-0.001	6900		5p	(5/2) <sup>-1</sup> 5/2 <sub>1</sub> 3	(5/2) <sup>-1</sup> 9/2 <sub>1</sub> 2d	D+	Ric		
6377.248(7)	15676.410(17)	6377.2432(12)	0.005	13000		5p	(3/2) <sup>-1</sup> 5/2 <sub>1</sub> 3	(3/2) <sup>-1</sup> 3/2 <sub>1</sub> 2d		Ric		
6377.842(3)	15674.951(7)	6377.8383(7)	0.004	19000		5p	(5/2) <sup>-1</sup> 5/2 <sub>1</sub> 3	(5/2) <sup>-1</sup> 3/2 <sub>1</sub> 2d	D+	F_Re	TW	
6380.758(4)	15667.788(9)	6380.7645(7)	-0.007	1300		5p	(5/2) <sup>-1</sup> 5/2 <sub>1</sub> 2	(5/2) <sup>-1</sup> 3/2 <sub>1</sub> 2d		Ric		
6385.263(3)	15656.734(7)	6385.2618(10)	0.001	1200		sp	( <sup>3</sup> F) <sup>-3</sup> D <sup>-1</sup>	(5/2) <sup>-1</sup> 5/2 <sub>1</sub> 2d		Ric		

Table A1. Cont.

$\lambda_{\text{obs}}^a$ (Å)	$\sigma_{\text{obs}}^b$ (cm <sup>-1</sup> )	$\lambda_{\text{Ritz}}^c$ (Å)	$\Delta\lambda_{\text{obs-Ritz}}^d$ (Å)	$I_{\text{obs}}^d$ (arb. u.)	Char <sup>e</sup>	Lower Level	Upper Level	A (s <sup>-1</sup> )	Acc <sup>f</sup>	Line Ref. <sup>g</sup>	TP Ref. <sup>h</sup>	Notes <sup>b</sup>
6393.074(6)	15637.604(15)	6393.079(20)	-0.005	130	*	( <sup>1</sup> P) <sup>3</sup> C <sup>o</sup> , 4 6g	(5/2) <sup>2</sup> 19/21 <sub>4</sub>			Ric		
6393.074(6)	15637.604(15)	6393.0735(21)	0.001	130	*	( <sup>1</sup> F) <sup>3</sup> P <sup>o</sup> , 3C <sup>o</sup> , 4 6g	(5/2) <sup>2</sup> 19/21 <sub>5</sub>			Rinc		
6393.957(3)	15635.446(8)	6393.9587(13)	-0.002	2100	sp	( <sup>3</sup> F) <sup>3</sup> P <sup>o</sup> , 3C <sup>o</sup> , 4 6g	(5/2) <sup>2</sup> 11/21 <sub>5</sub>		D+	Ric	TW	
6403.384(3)	15612.428(8)	6403.3840(15)	-0.000	9600	4d	(3/2) <sup>2</sup> 11/21 <sub>0</sub>	(3/2) <sup>2</sup> 11/21 <sub>1</sub>		D+	Ric	TW	
6411.142(4)	15593.535(10)	6411.1518(12)	-0.010	10000	5p	(3/2) <sup>2</sup> 3/21 <sup>o</sup> , 1 5d	(3/2) <sup>2</sup> 3/21 <sub>1</sub>		D+	F,Re	TW	
6414.569(3)	15585.204(7)	6414.5612(11)	0.008	12000	5p	(3/2) <sup>2</sup> 3/21 <sup>o</sup> , 2 5d	(3/2) <sup>2</sup> 15/21 <sub>2</sub>		D+	Ric	TW	
6414.625(3)	15583.069(7)	6414.6165(8)	0.008	16000	sp	( <sup>3</sup> F) <sup>3</sup> P <sup>o</sup> , 3P <sup>o</sup> , 3 6s	(5/2) <sup>2</sup> 15/21 <sub>2</sub>		D+	Ric	TW	
6418.160(4)	15576.483(10)	6418.1596(24)	0.004	2100	4f	(5/2) <sup>2</sup> 11/21 <sup>o</sup> , 1 6g	(5/2) <sup>2</sup> 3/21 <sub>2</sub>		D+	Ric	TW	
6419.941(9)	15571.162(21)	6419.9515(7)	-0.010	62	m	(5/2) <sup>2</sup> 11/21 <sup>o</sup> , 1 6g	(5/2) <sup>2</sup> 3/21 <sub>1</sub>			Rinc		
6423.8842(11)	15562.604(3)	6423.8846(8)	-0.0003	19000	5p	(5/2) <sup>2</sup> 3/21 <sup>o</sup> , 2 6s	(3/2) <sup>2</sup> 3/21 <sub>2</sub>		C+	Ric	TW	
6427.416(9)	15554.032(21)	6427.411(3)	0.005	31	4f	(5/2) <sup>2</sup> 3/21 <sup>o</sup> , 2 6s	(3/2) <sup>2</sup> 15/21 <sub>2</sub>			F,Re		
6432.416(3)	15539.196(7)	6432.415(3)	0.001	5600	4f	(5/2) <sup>2</sup> 3/21 <sup>o</sup> , 2 6g	(5/2) <sup>2</sup> 17/21 <sub>5</sub>		D+	Ric	TW	
6433.597(4)	15539.109(10)	6433.5944(22)	0.003	920	4f	(5/2) <sup>2</sup> 3/21 <sup>o</sup> , 2 6g	(5/2) <sup>2</sup> 15/21 <sub>2</sub>		D+	Ric	TW	
6434.081(5)	15537.941(12)	6434.075(3)	0.006	610	4f	(5/2) <sup>2</sup> 11/21 <sup>o</sup> , 0 6g	(5/2) <sup>2</sup> 3/21 <sub>2</sub>		D+	Ric	TW	
6434.799(3)	15536.208(8)	6434.7944(13)	0.004	4f	4f	(5/2) <sup>2</sup> 11/21 <sup>o</sup> , 2 6g	(5/2) <sup>2</sup> 3/21 <sub>1</sub>		D+	Ric	TW	
6437.596(3)	15529.458(8)	6437.5974(24)	-0.002	460	4f	(5/2) <sup>2</sup> 11/21 <sup>o</sup> , 2 6g	(5/2) <sup>2</sup> 13/21 <sub>2</sub>		D+	Ric	TW	
6441.202(5)	15520.764(12)	6441.1920(9)	0.010	1200	4p	( <sup>3</sup> F) <sup>3</sup> P <sup>o</sup> , 3F <sup>o</sup> , 2 5s <sup>2</sup>	(5/2) <sup>2</sup> 13/21 <sub>2</sub>			Ric		
6441.677(3)	15519.618(8)	6441.6790(8)	-0.002	13000	sp	( <sup>3</sup> F) <sup>3</sup> P <sup>o</sup> , 3F <sup>o</sup> , 2 5d	(5/2) <sup>2</sup> 7/21 <sub>4</sub>			Ric		
6442.964(3)	15516.519(7)	6442.964(3)	-0.000	10000	4f	(5/2) <sup>2</sup> 11/21 <sup>o</sup> , 6 6g	(5/2) <sup>2</sup> 7/21 <sub>4</sub>			Ric		
6443.587(3)	15515.019(8)	6443.587(3)	0.000	4900	4f	(5/2) <sup>2</sup> 11/21 <sup>o</sup> , 6 6g	(5/2) <sup>2</sup> 13/21 <sub>2</sub>		D+	F,Re	TW	
6445.695(20)	15509.95(5)	6445.673(3)	0.020	1400	6p	(3/2) <sup>2</sup> 3/21 <sup>o</sup> , 2 9s	(3/2) <sup>2</sup> 13/21 <sub>2</sub>		D+	Ric	TW	
6445.692(20)	15509.95(5)	6445.7022(9)	-0.010	1400	sp	( <sup>1</sup> F) <sup>3</sup> P <sup>o</sup> , 3F <sup>o</sup> , 2 9s	(3/2) <sup>2</sup> 15/21 <sub>5</sub>		D+	Ric	TW	
6448.558(3)	15503.059(8)	6447.632(3)	-0.005	61	4p	( <sup>1</sup> F) <sup>3</sup> P <sup>o</sup> , 3F <sup>o</sup> , 3 8d	(5/2) <sup>2</sup> 19/21 <sub>5</sub>			Rinc		
6449.63(3)	15500.49(7)	6449.6175(15)	0.01	20000	3p	( <sup>1</sup> G) <sup>3</sup> P <sup>o</sup> , 3F <sup>o</sup> , 3 8d	(5/2) <sup>2</sup> 19/21 <sub>4</sub>			Ric		
6449.63(3)	15500.49(7)	6449.635(3)	-0.03	30	4d	( <sup>3</sup> P) <sup>3</sup> P <sup>o</sup> , 3D <sup>o</sup> , 3 8d	( <sup>3</sup> P) <sup>3</sup> P <sup>o</sup> , 3D <sup>o</sup> , 3 8d			Ric		
6449.63(3)	15500.49(7)	6449.635(3)	-0.03	30	sp	( <sup>3</sup> P) <sup>3</sup> P <sup>o</sup> , 5S <sup>o</sup> , 2 6g	(5/2) <sup>2</sup> 15/21 <sub>2</sub>			Ric		
6449.63(3)	15500.49(7)	6449.639(4)	-0.03	30	sp	( <sup>3</sup> P) <sup>3</sup> P <sup>o</sup> , 5S <sup>o</sup> , 2 6g	(5/2) <sup>2</sup> 15/21 <sub>2</sub>			Rinc		
6450.874(3)	15497.493(8)	6450.8738(17)	-0.000	610	4d	( <sup>3</sup> F) <sup>3</sup> P <sup>o</sup> , 3D <sup>o</sup> , 1 5p	( <sup>3</sup> F) <sup>3</sup> P <sup>o</sup> , 3D <sup>o</sup> , 1 5p			Ric		
6452.116(3)	15494.508(7)	6452.1161(24)	0.000	1300	4f	(5/2) <sup>2</sup> 3/21 <sup>o</sup> , 1 6g	(5/2) <sup>2</sup> 3/21 <sub>2</sub>		D+	Ric	TW	
6454.161(3)	15489.601(8)	6454.895(3)	-0.001	910	4f	(5/2) <sup>2</sup> 3/21 <sup>o</sup> , 1 6g	(3/2) <sup>2</sup> 3/21 <sub>1</sub>			Ric		
6454.894(9)	15487.842(21)	6456.140(9)	-0.021	30	6p	(5/2) <sup>2</sup> 7/21 <sup>o</sup> , 1 8d	(5/2) <sup>2</sup> 7/21 <sub>4</sub>			Ric		
6456.119(13)	15484.90(3)	6456.1848(19)	0.002	2600	5s	(3/2) <sup>2</sup> 13/21 <sub>1</sub>	( <sup>3</sup> P) <sup>3</sup> P <sup>o</sup> , 5P <sup>o</sup> , 1 6g			Ric		
6457.187(3)	15482.342(7)	6457.1848(19)	0.002	2600	4f	(5/2) <sup>2</sup> 7/21 <sup>o</sup> , 3 6g	(5/2) <sup>2</sup> 19/21 <sub>4</sub>			Ric		
6457.568(4)	15481.908(10)	6457.371(3)	-0.004	1600	4f	(5/2) <sup>2</sup> 3/21 <sup>o</sup> , 1 6g	(5/2) <sup>2</sup> 3/21 <sub>1</sub>			Ric		
6458.263(9)	15479.762(21)	6458.259(3)	0.004	61	4f	(5/2) <sup>2</sup> 3/21 <sup>o</sup> , 1 6g	(3/2) <sup>2</sup> 19/21 <sub>5</sub>			Ric		
6460.304(3)	15474.870(8)	6460.304(3)	0.001	1000	4f	(5/2) <sup>2</sup> 7/21 <sup>o</sup> , 2 6g	(5/2) <sup>2</sup> 7/21 <sub>5</sub>			Ric		
6462.140(3)	15470.475(8)	6462.1413(20)	-0.002	60	4f	(3/2) <sup>2</sup> 19/21 <sup>o</sup> , 4 6g	(3/2) <sup>2</sup> 19/21 <sub>4</sub>			Ric		
6462.70(10)	15469.13(24)	6462.6086(21)	0.09	1000	4f	(3/2) <sup>2</sup> 7/21 <sup>o</sup> , 2 7d	(3/2) <sup>2</sup> 7/21 <sub>5</sub>			S36c		
6465.342(15)	15462.81(4)	6465.3543(24)	-0.012	30	4f	(5/2) <sup>2</sup> 7/21 <sup>o</sup> , 3 6g	(5/2) <sup>2</sup> 7/21 <sub>5</sub>			Ric		
6465.342(15)	15462.81(4)	6465.359(3)	-0.017	30	4f	(5/2) <sup>2</sup> 7/21 <sup>o</sup> , 3 6g	(5/2) <sup>2</sup> 15/21 <sub>2</sub>			Ric		
6466.245(3)	15460.653(7)	6466.245(3)	0.000	5600	4f	(3/2) <sup>2</sup> 7/21 <sup>o</sup> , 5 6g	(3/2) <sup>2</sup> 11/21 <sub>4</sub>		D+	Ric	TW	

Table A1. Cont.

$\lambda_{\text{obs}}^a$ (Å)	$\sigma_{\text{obs}}^b$ (cm <sup>-1</sup> )	$\lambda_{\text{Ritz}}^c$ (Å)	$\Delta\lambda^{\text{obs-Ritz}}$ (Å)	$I_{\text{obs}}^d$ (arb. u.)	Char <sup>e</sup>	Lower Level	Upper Level	A (s <sup>-1</sup> )	Acc <sup>f</sup>	Line Ref. <sup>g</sup>	TP Ref. <sup>h</sup>	Notes <sup>b</sup>
6470.1386(19)	15451.350(5)	6470.1383(19)	0.0003	8600	4f	(3/2) <sup>2</sup> 1/2 <sub>1</sub> 4g	(3/2) <sup>2</sup> 11/2 <sub>1</sub>	2.3e+07	D+	F,Rc	TW	
6470.160(3)	15451.298(7)	6470.1668(8)	-0.006	15000	sp	( <sup>3</sup> F) <sup>o</sup> -3F <sub>3</sub> 6s	(5/2) <sup>2</sup> 15/2 <sub>1</sub>	7.5e+06	D+	F,Rc	TW	
6475.426(4)	15438.734(9)	6475.4257(24)	-0.000	1000	4f	(5/2) <sup>2</sup> 15/2 <sub>1</sub> 2	(5/2) <sup>2</sup> 15/2 <sub>1</sub> 2			Rlc		
6476.184(4)	15436.925(9)	6476.1819(19)	0.003	1000	4f	(5/2) <sup>2</sup> 17/2 <sub>1</sub> 3	(5/2) <sup>2</sup> 19/2 <sub>1</sub> 4			Rlc		
6477.868(9)	15432.912(21)	6477.860(3)	0.008	120	6p	(5/2) <sup>2</sup> 7/2 <sub>1</sub> 3	(5/2) <sup>2</sup> 19/2 <sub>1</sub> 4			Rlc		
6479.316(3)	15429.463(7)	6479.3164(21)	-0.000	4100	4f	(5/2) <sup>2</sup> 15/2 <sub>1</sub> 3	(5/2) <sup>2</sup> 17/2 <sub>1</sub> 3	1.5e+07	D+	Rlc	TW	
6481.436(3)	15424.118(7)	6481.4350(12)	0.001	15000	5p	(3/2) <sup>2</sup> 13/2 <sub>1</sub> 2	(3/2) <sup>2</sup> 13/2 <sub>1</sub> 2			Rlc	TW	
		6484.409(3)				(5/2) <sup>2</sup> 15/2 <sub>1</sub> 3	(3/2) <sup>2</sup> 15/2 <sub>1</sub> 3	6.5e+06	D+	Rinc	TW	
6484.417(3)	15417.326(8)	6484.4174(9)	-0.000	7800	5p	(5/2) <sup>2</sup> 15/2 <sub>1</sub> 3	(5/2) <sup>2</sup> 15/2 <sub>1</sub> 3			F,Rc	TW	
6488.816(3)	15406.875(7)	6488.814(3)	0.002	2700	4f	(3/2) <sup>2</sup> 15/2 <sub>1</sub> 3	(3/2) <sup>2</sup> 17/2 <sub>1</sub> 4	1.4e+07	D+	Rlc	TW	
6494.029(3)	15394.507(6)	6494.0320(6)	-0.003	18000	sp	( <sup>3</sup> F) <sup>o</sup> -F <sub>3</sub> 5d	(5/2) <sup>2</sup> 15/2 <sub>1</sub> 3	1.9e+07	D+	F,Rc	TW	
6497.040(9)	15387.372(21)	6497.041(3)	-0.001	89	4f	(3/2) <sup>2</sup> 15/2 <sub>1</sub> 3	(5/2) <sup>2</sup> 15/2 <sub>1</sub> 3			F,Rc		
6508.401(3)	15360.514(7)	6508.400(3)	0.001	2700	4f	(3/2) <sup>2</sup> 15/2 <sub>1</sub> 3	(3/2) <sup>2</sup> 15/2 <sub>1</sub> 3	1.7e+07	D+	Rlc	TW	
6516.458(3)	15341.522(8)	6516.4637(12)	-0.006	6600	5p	(3/2) <sup>2</sup> 15/2 <sub>1</sub> 2	(3/2) <sup>2</sup> 17/2 <sub>1</sub> 3			Rlc	TW	
6517.316(3)	15339.501(7)	6517.3166(21)	-0.000	6600	4f	(5/2) <sup>2</sup> 17/2 <sub>1</sub> 4	(5/2) <sup>2</sup> 19/2 <sub>1</sub> 5	1.7e+07	D+	Rlc	TW	
6518.236(4)	15337.337(9)	6518.2366(12)	-0.001	150	4f	(5/2) <sup>2</sup> 17/2 <sub>1</sub> 4	(5/2) <sup>2</sup> 17/2 <sub>1</sub> 4			Rlc	TW	
6520.497(3)	15330.019(8)	6520.4970(21)	-0.000	1000	4f	(5/2) <sup>2</sup> 17/2 <sub>1</sub> 4	(5/2) <sup>2</sup> 17/2 <sub>1</sub> 4	5.7e+06	D+	Rlc	TW	
6521.270(6)	15321.2756(14)	6521.2756(14)	-0.005	480	4p	<sup>3</sup> P <sub>0</sub>	(5/2) <sup>2</sup> 17/2 <sub>1</sub> 4			Rlc	TW	
6523.820(3)	15320.209(7)	6523.820(3)	-0.000	4500	4f	(3/2) <sup>2</sup> 17/2 <sub>1</sub> 4	(3/2) <sup>2</sup> 19/2 <sub>1</sub> 5	2.1e+07	D+	Rlc	TW	
6525.641(9)	15319.932(21)	6525.650(3)	-0.008	29	4f	(5/2) <sup>2</sup> 17/2 <sub>1</sub> 4	(5/2) <sup>2</sup> 15/2 <sub>1</sub> 3			Rlc		
6526.646(6)	15317.574(13)	6526.655(3)	-0.009	88	4f	(3/2) <sup>2</sup> 17/2 <sub>1</sub> 4	(3/2) <sup>2</sup> 17/2 <sub>1</sub> 4			Rlc		
6529.167(3)	15311.658(8)	6529.1668(21)	0.001	1000	4f	(5/2) <sup>2</sup> 19/2 <sub>1</sub> 5	(5/2) <sup>2</sup> 19/2 <sub>1</sub> 5	4.6e+06	D+	Rlc	TW	
6530.082(3)	15309.514(7)	6530.0829(22)	-0.001	13000	4f	(5/2) <sup>2</sup> 17/2 <sub>1</sub> 4	(5/2) <sup>2</sup> 17/2 <sub>1</sub> 4	2.0e+07	D+	Rlc	TW	
6536.679(9)	15294.062(21)	6536.6999(17)	-0.017	29	4d	( <sup>3</sup> P) <sup>o</sup> -3P <sub>2</sub>	( <sup>3</sup> P) <sup>o</sup> -3P <sub>2</sub>			Rlc		
6541.637(3)	15282.471(7)	6541.6569(20)	0.000	3400	4f	(3/2) <sup>2</sup> 15/2 <sub>1</sub> 3	(3/2) <sup>2</sup> 19/2 <sub>1</sub> 4	1.9e+07	D+	Rlc	TW	
6544.485(6)	15275.822(14)	6544.480(3)	0.004	58	4f	(3/2) <sup>2</sup> 17/2 <sub>1</sub> 3	(3/2) <sup>2</sup> 17/2 <sub>1</sub> 3			Rinc		
6544.485(6)	15275.822(14)	6544.489(3)	-0.004	58	4f	(3/2) <sup>2</sup> 17/2 <sub>1</sub> 3	(3/2) <sup>2</sup> 17/2 <sub>1</sub> 3			Rlc		
6550.304(5)	15262.251(12)	6550.3097(9)	-0.006	150	5p	(3/2) <sup>2</sup> 17/2 <sub>1</sub> 3	(3/2) <sup>2</sup> 17/2 <sub>1</sub> 3			Rlc		
6551.286(3)	15259.964(8)	6551.2873(8)	-0.002	1900	4p	( <sup>3</sup> P) <sup>o</sup> -3P <sub>2</sub>	( <sup>3</sup> P) <sup>o</sup> -3P <sub>2</sub>			Rlc		
6554.291(6)	15251.804(13)	6554.7923(9)	-0.002	5100	4p	<sup>3</sup> P <sub>1</sub>	( <sup>3</sup> P) <sup>o</sup> -3P <sub>1</sub>			Rlc		
6556.193(6)	15248.542(14)	6556.206(3)	-0.013	430	4d	( <sup>3</sup> P) <sup>o</sup> -3P <sub>1</sub>	( <sup>3</sup> P) <sup>o</sup> -3P <sub>1</sub>			Rlc		
6559.657(4)	15240.489(9)	6559.6523(8)	0.005	13000	5p	(5/2) <sup>2</sup> 11/2 <sub>1</sub> sp	(5/2) <sup>2</sup> 11/2 <sub>1</sub> sp	4.9e+06	D+	Rlc	TW	
6564.492(3)	15229.264(8)	6564.4941(8)	-0.002	10000	sp	( <sup>3</sup> F) <sup>o</sup> -F <sub>3</sub> 5d	(5/2) <sup>2</sup> 19/2 <sub>1</sub> 4			Rlc		
6567.949(6)	15221.249(13)	6567.9621(7)	-0.013	290	5s	( <sup>3</sup> F) <sup>o</sup> -F <sub>3</sub> 5d	(5/2) <sup>2</sup> 13/2 <sub>1</sub> 2			Rlc	B00	
6576.147(6)	15202.273(13)	6576.1510(20)	-0.004	1000	4f	(5/2) <sup>2</sup> 15/2 <sub>1</sub> 2	(5/2) <sup>2</sup> 19/2 <sub>1</sub> 4	5.1e+05	C	Rlc	TW	
6577.0812(15)	15200.114(3)	6577.0816(12)	-0.0003	5700	4f	(5/2) <sup>2</sup> 19/2 <sub>1</sub> 4	(5/2) <sup>2</sup> 19/2 <sub>1</sub> 4	4.3e+06	D+	Rlc	TW	
6579.576(9)	15194.812(21)	6579.586(3)	-0.010	500	4f	(5/2) <sup>2</sup> 19/2 <sub>1</sub> 4	(5/2) <sup>2</sup> 17/2 <sub>1</sub> 3	1.5e+07	D+	F,Rc	TW	
6592.896(9)	15163.632(21)	6592.900(3)	-0.004	120	5s	( <sup>3</sup> F) <sup>o</sup> -5P <sub>2</sub>	( <sup>3</sup> F) <sup>o</sup> -5P <sub>2</sub>			Rlc		
6602.096(9)	15142.522(21)	6602.094(3)	0.003	57	6p	(5/2) <sup>2</sup> 13/2 <sub>1</sub> 2	(5/2) <sup>2</sup> 17/2 <sub>1</sub> 3			Rlc		
6603.527(9)	15139.242(21)	6603.523(4)	0.003	29	6p	(3/2) <sup>2</sup> 15/2 <sub>1</sub> 3	(3/2) <sup>2</sup> 13/2 <sub>1</sub> 2			Rlc		
6612.087(9)	15119.642(21)	6612.086(3)	0.001	87	6p	(5/2) <sup>2</sup> 15/2 <sub>1</sub> 3	(5/2) <sup>2</sup> 15/2 <sub>1</sub> 3			Rlc		
6624.291(3)	15091.787(7)	6624.2890(9)	0.002	5200	sp	( <sup>3</sup> F) <sup>o</sup> -1D <sub>2</sub>	(5/2) <sup>2</sup> 15/2 <sub>1</sub> 2	2.2e+07	D+	Rlc	TW	



Table A1. Cont.

$\lambda_{\text{obs}}^a$ (Å)	$\sigma_{\text{obs}}^b$ (cm <sup>-1</sup> )	$\lambda_{\text{Ritz}}^c$ (Å)	$\Delta\lambda_{\text{obs-Ritz}}^d$ (Å)	$I_{\text{obs}}^d$ (arb. u.)	Char <sup>e</sup>	Lower Level	Upper Level	A (s <sup>-1</sup> )	Acc <sup>f</sup>	Line Ref. <sup>g</sup>	TP Ref. <sup>h</sup>	Notes <sup>h</sup>
6626.243(3)	15087.341(8)	6626.2420(20)	0.001	710	5d	(5/2) <sup>-1</sup> [1/2] <sub>1</sub>	8p			Ric		
6631.476(3)	15075.436(7)	6631.4733(7)	0.003	330	5p	(5/2) <sup>-1</sup> [7/2] <sub>3</sub>	6s			Ric		
6635.173(7)	15067.037(17)	6635.1692(18)	0.003	850	5d	(5/2) <sup>-1</sup> [1/2] <sub>1</sub>	6s			Ric		
6641.395(3)	15052.920(17)	6641.3938(9)	0.002	8000	5p	( <sup>3</sup> P) <sup>3</sup> P <sup>-1</sup> D <sup>2</sup>	5d	2.6e+07	D+	Ric	TW	
6647.796(4)	15038.427(10)	6647.7986(18)	-0.003	850	5d	(5/2) <sup>-1</sup> [1/2] <sub>1</sub>	5d			Ric		
6648.764(5)	15036.321(11)	6648.7717(14)	-0.008	7300	5p	(3/2) <sup>-1</sup> [3/2] <sup>o</sup>	5d	1.1e+07	D+	Ric	TW	
6651.322(4)	15030.453(10)	6651.3254(21)	-0.003	700	5p	( <sup>3</sup> F) <sup>1</sup> P <sup>3</sup> F <sup>3</sup>	6g	3.8e+06	D+	Ric	TW	
6654.635(9)	15022.972(21)	6654.6353(3)	-0.000	56	5p	( <sup>3</sup> F) <sup>1</sup> P <sup>3</sup> F <sup>3</sup>	6g			Ric		
6660.961(3)	15008.705(7)	6660.9606(8)	0.000	9200	4p	3D <sup>2</sup>	5s <sup>2</sup>			Ric		
6663.950(9)	15001.972(21)	6663.9466(8)	0.004	560	5s	(5/2) <sup>-1</sup> [5/2] <sub>3</sub>	5p			Ric		
6692.710(6)	14997.507(14)	6692.7144(7)	-0.005	700	5p	( <sup>3</sup> F) <sup>3</sup> P <sup>-1</sup> D <sup>2</sup>	5d			Ric		
6711.983(6)	14894.615(12)	6711.980(3)	0.003	56	5d	(3/2) <sup>-1</sup> [1/2] <sub>1</sub>	6f			Ric		
6716.700(3)	14884.155(7)	6716.7062(8)	-0.007	1300	5p	(5/2) <sup>-1</sup> [5/2] <sup>o</sup>	6s			Ric		
6717.687(6)	14881.968(12)	6717.687(4)	-0.001	280	5s	(3/2) <sup>-1</sup> [3/2] <sub>2</sub>	5p			Ric		
6725.481(10)	14864.722(21)	6725.490(4)	-0.010	28	5d	(3/2) <sup>-1</sup> [1/2] <sub>1</sub>	6f			R2c		
6725.834(10)	14863.942(21)	6725.850(8)	-0.016	28	5s	(3/2) <sup>-1</sup> [3/2] <sub>2</sub>	5p			R1nc		
6736.397(5)	14850.633(10)	6736.420(7)	-0.023	6300	5p	(5/2) <sup>-1</sup> [3/2] <sup>o</sup>	6s			Ric		
6739.599(3)	14833.582(7)	6739.598(3)	0.002	140	5d	(3/2) <sup>-1</sup> [1/2] <sub>1</sub>	6f	7.4e+06	D+	Ric	TW	X
6743.740(7)	14824.474(16)	6743.737(3)	0.003	56	5d	(5/2) <sup>-1</sup> [1/2] <sub>1</sub>	6f			R2hc		
6758.855(4)	14791.323(8)	6758.8577(10)	-0.003	6300	5p	( <sup>3</sup> F) <sup>3</sup> P <sup>-1</sup> D <sup>2</sup>	5d	1.0e+07	D+	Ric	TW	
6760.142(5)	14788.506(11)	6760.1422(8)	0.000	56	5p	(5/2) <sup>-1</sup> [5/2] <sup>o</sup>	6s			Ric		
6765.794(10)	14776.153(21)	6765.7884(19)	0.006	28	5p	( <sup>3</sup> G) <sup>3</sup> P <sup>-3</sup> H <sup>4</sup>	6g			Ric		
6767.561(7)	14772.294(16)	6767.5789(9)	-0.018	28	5p	( <sup>3</sup> F) <sup>3</sup> P <sup>-1</sup> D <sup>2</sup>	5d			Ric		
6770.361(3)	14766.186(7)	6770.3694(10)	0.000	3100	4p	<sup>3</sup> P <sup>-1</sup>	5s <sup>2</sup>			Ric		
6779.440(7)	14746.410(15)	6779.4453(18)	-0.005	28	5p	(3/2) <sup>-1</sup> [1/2] <sub>1</sub>	5d			Ric		
6780.114(4)	14744.945(9)	6780.1122(7)	0.002	4900	5p	(5/2) <sup>-1</sup> [3/2] <sup>o</sup>	6s			Ric		
6786.482(5)	14731.110(11)	6786.4808(7)	0.001	84	5s	(5/2) <sup>-1</sup> [5/2] <sub>3</sub>	5p			Ric		
6802.138(3)	14697.204(7)	6802.1387(19)	-0.001	220	5d	(5/2) <sup>-1</sup> [9/2] <sub>5</sub>	6f	3.5e+06	D+	Ric	TW	
6806.215(3)	14688.401(7)	6806.2136(9)	0.001	4100	5p	( <sup>3</sup> F) <sup>3</sup> P <sup>-3</sup> F <sup>3</sup>	6s			Ric		
6809.6453(23)	14681.001(5)	6809.6436(8)	0.0016	5200	5p	(5/2) <sup>-1</sup> [5/2] <sup>o</sup>	6s			F <sub>2</sub> Ric		
6814.690(14)	14670.13(3)	6814.69132(2)	-0.001	28	5d	(3/2) <sup>-1</sup> [3/2] <sub>2</sub>	5p			Ric		
6821.060(5)	14656.434(11)	6821.0571(19)	0.002	140	5d	(5/2) <sup>-1</sup> [3/2] <sub>2</sub>	5p	3.2e+06	D+	Ric	TW	
6822.342(8)	14653.679(17)	6822.3460(19)	-0.004	28	5d	(5/2) <sup>-1</sup> [9/2] <sub>5</sub>	6f			Ric		
6823.201(3)	14651.833(7)	6823.2010(23)	0.001	6400	5d	(5/2) <sup>-1</sup> [9/2] <sub>5</sub>	6f	1.8e+07	D+	Ric	TW	
6824.750(4)	14648.508(8)	6824.7493(19)	0.001	700	5d	(5/2) <sup>-1</sup> [9/2] <sub>5</sub>	6f	7.2e+06	D+	Ric	TW	
6830.531(3)	14636.112(7)	6830.5296(22)	0.001	1300	5d	(5/2) <sup>-1</sup> [7/2] <sub>3</sub>	6f	1.8e+07	D+	Ric	TW	
6833.026(4)	14630.766(9)	6833.0244(19)	0.002	560	5d	(5/2) <sup>-1</sup> [3/2] <sub>2</sub>	6f	8.1e+06	D+	Ric	TW	
6837.491(4)	14621.212(8)	6837.4936(18)	-0.002	720	5d	(5/2) <sup>-1</sup> [3/2] <sub>2</sub>	6f	9.4e+06	D+	Ric	TW	
6844.156(3)	14606.974(7)	6844.1542(20)	0.000	3200	5p	( <sup>3</sup> F) <sup>3</sup> P <sup>-1</sup> G <sup>4</sup>	6s	1.8e+07	D+	Ric		
6846.104(20)	14602.82(4)	6846.065(3)	0.039	880	5p	( <sup>3</sup> F) <sup>3</sup> P <sup>-1</sup> G <sup>4</sup>	6s			Ric		
6847.112(7)	14600.669(14)	6847.112(3)	-0.000	170	5d	(5/2) <sup>-1</sup> [3/2] <sub>2</sub>	6f			Ric		
6849.991(6)	14594.532(13)	6849.988(4)	0.003	56	4d	( <sup>1</sup> D) <sup>3</sup> P <sup>-3</sup> P <sup>o</sup>	5p			Ric		
6852.428(7)	14589.342(14)	6852.432(3)	-0.004	84	5d	(3/2) <sup>-1</sup> [3/2] <sub>2</sub>	6f			Ric		

Table A1. Cont.

$\lambda_{\text{obs}}^a$ (Å)	$\sigma_{\text{obs}}^b$ (cm <sup>-1</sup> )	$\lambda_{\text{ritz}}^c$ (Å)	$\Delta\lambda_{\text{obs-ritz}}^d$ (Å)	$I_{\text{obs}}^d$ (arb. u.)	Char <sup>e</sup>	Lower Level	Upper Level	A (s <sup>-1</sup> )	Acc <sup>f</sup>	Line Ref. <sup>g</sup>	TP Ref. <sup>g</sup>	Notes <sup>h</sup>
6863.061(3)	14566.739(7)	6863.0599(23)	0.001	2100	5d	(3/2) <sup>-1</sup> 7/21 <sub>6</sub>	6f	(3/2) <sup>-1</sup> 9/21 <sup>-5</sup>	D+	Ric	TW	
6867.88(2)	14556.5(4)	6868.184(4)	-0.30	470	4d	(3/2) <sup>-1</sup> 5/21 <sub>6</sub>	sp	(3/2) <sup>-1</sup> 5/21 <sup>-6</sup>		S36c		
6868.790(3)	14554.589(7)	6868.7864(9)	0.004	2900	sp	( <sup>3</sup> F) <sup>-1</sup> 3F <sup>-2</sup>		( <sup>3</sup> F) <sup>-1</sup> 5/21 <sup>-6</sup>		Ric		
6872.230(3)	14547.303(7)	6872.2293(10)	0.001	3200	4p	1F <sup>-3</sup>	s <sup>2</sup>	1D <sup>2</sup>		Ric		
6879.403(3)	14532.136(7)	6879.4043(7)	-0.001	2500	5s	(5/2) <sup>+1</sup> 5/21 <sub>6</sub>	5p	(3/2) <sup>+1</sup> 1/21 <sup>-1</sup>	C	Ric	B00	
6883.496(6)	14502.427(12)	6883.4896(18)	0.006	2200	5d	(5/2) <sup>+1</sup> 5/21 <sub>6</sub>	6f	(5/2) <sup>+1</sup> 9/21 <sup>-4</sup>		Ric		
6894.810(4)	14499.663(9)	6894.8061(18)	0.004	700	5d	(5/2) <sup>+1</sup> 5/21 <sub>6</sub>	6f	(5/2) <sup>+1</sup> 9/21 <sup>-4</sup>		Ric	TW	
6902.817(4)	14483.263(9)	6902.8139(19)	0.005	560	5d	(5/2) <sup>+1</sup> 5/21 <sub>6</sub>	6f	(5/2) <sup>+1</sup> 9/21 <sup>-4</sup>		Ric	TW	
6915.653(10)	14455.962(21)	6915.6598(18)	0.002	56	5d	(5/2) <sup>+1</sup> 5/21 <sub>6</sub>	6f	(5/2) <sup>+1</sup> 9/21 <sup>-4</sup>		Ric	TW	
6928.602(6)	14428.946(12)	6928.592(3)	0.009	340	5d	(5/2) <sup>+1</sup> 5/21 <sub>6</sub>	6f	(5/2) <sup>+1</sup> 9/21 <sup>-4</sup>		Ric	B00	
6937.552(4)	14410.331(8)	6937.5472(7)	0.005	2100	3d	(5/2) <sup>+1</sup> 5/21 <sub>6</sub>	5p	(5/2) <sup>+1</sup> 9/21 <sup>-4</sup>		Ric	B00	
6939.099(7)	14407.119(14)	6939.098(3)	0.001	280	5d	(5/2) <sup>+1</sup> 7/21 <sub>6</sub>	6f	(5/2) <sup>+1</sup> 7/21 <sup>-3</sup>		Ric	TW	
6948.795(7)	14387.015(15)	6948.7944(20)	-0.001	2000	5d	(5/2) <sup>+1</sup> 7/21 <sub>6</sub>	6f	(5/2) <sup>+1</sup> 7/21 <sup>-3</sup>		Ric	TW	
6950.139(6)	14384.234(13)	6950.1341(20)	0.005	1700	5d	(5/2) <sup>+1</sup> 7/21 <sub>6</sub>	6f	(5/2) <sup>+1</sup> 7/21 <sup>-3</sup>		Ric	TW	
6952.870(4)	14378.583(7)	6952.8664(20)	0.004	4200	5d	(5/2) <sup>+1</sup> 7/21 <sub>6</sub>	6f	(5/2) <sup>+1</sup> 9/21 <sup>-5</sup>		Ric	TW	
6953.480(10)	14377.322(21)	6953.4782(20)	0.002	110	5d	(5/2) <sup>+1</sup> 7/21 <sub>6</sub>	6f	(5/2) <sup>+1</sup> 9/21 <sup>-4</sup>		Ric	TW	
6953.930(6)	14374.391(13)	6953.914(3)	0.016	2100	5d	(5/2) <sup>+1</sup> 5/21 <sub>6</sub>	6f	(5/2) <sup>+1</sup> 7/21 <sup>-4</sup>		Ric	TW	
6954.820(10)	14374.552(21)	6954.8176(19)	0.002	230	5d	(5/2) <sup>+1</sup> 5/21 <sub>6</sub>	6f	(5/2) <sup>+1</sup> 7/21 <sup>-4</sup>		Ric	TW	
6957.884(10)	14368.222(20)	6957.869(3)	0.015	1800	5d	(5/2) <sup>+1</sup> 5/21 <sub>6</sub>	6f	(5/2) <sup>+1</sup> 7/21 <sup>-3</sup>		Ric	TW	
6957.884(10)	14368.222(20)	6957.876(4)	0.008	1800	sp	( <sup>3</sup> G) <sup>-1</sup> 3H <sup>-5</sup>	6g	(5/2) <sup>+1</sup> 13/21 <sub>6</sub>		Ric		
6957.884(10)	14368.222(20)	6957.876(3)	0.008	1800	5d	(5/2) <sup>+1</sup> 5/21 <sub>6</sub>	6f	(5/2) <sup>+1</sup> 13/21 <sup>-6</sup>		Ric		
6963.433(10)	14356.772(21)	6963.427(3)	0.006	230	5d	(5/2) <sup>+1</sup> 5/21 <sub>6</sub>	6f	(5/2) <sup>+1</sup> 7/21 <sup>-3</sup>		Ric	TW	
6968.846(10)	14345.622(21)	6968.847(3)	-0.002	57	5d	(5/2) <sup>+1</sup> 5/21 <sub>6</sub>	6f	(5/2) <sup>+1</sup> 5/21 <sup>-2</sup>		Ric		
6976.305(10)	14330.282(21)	6976.2990(20)	0.006	230	5d	(5/2) <sup>+1</sup> 5/21 <sub>6</sub>	6f	(5/2) <sup>+1</sup> 5/21 <sup>-2</sup>		Ric	TW	
6977.571(4)	14327.683(8)	6977.5641(10)	0.007	4300	5p	(3/2) <sup>+1</sup> 5/21 <sup>-2</sup>	5d	(5/2) <sup>+1</sup> 5/21 <sup>-2</sup>		Ric		
6986.548(8)	14309.273(17)	6986.5269(20)	0.021	2100	10p	(3/2) <sup>+1</sup> 5/21 <sup>-2</sup>	5d	(5/2) <sup>+1</sup> 1/21 <sub>6</sub>		Ric		
6996.556(5)	14288.805(9)	6996.5446(10)	0.012	1400	6p	(3/2) <sup>+1</sup> 5/21 <sup>-2</sup>	5d	(5/2) <sup>+1</sup> 7/21 <sub>6</sub>		Ric		
7022.859(4)	14235.289(7)	7022.8519(9)	0.007	2800	sp	( <sup>3</sup> F) <sup>-1</sup> 3F <sup>-3</sup>	6s	(5/2) <sup>+1</sup> 9/21 <sub>6</sub>		Ric		
7037.388(4)	14205.899(8)	7037.3853(10)	0.003	2900	5p	(3/2) <sup>+1</sup> 1/21 <sup>-1</sup>	5d	(5/2) <sup>+1</sup> 15/21 <sub>6</sub>		Ric		
7083.772(6)	14112.882(12)	7083.7743(13)	-0.003	730	5p	(3/2) <sup>+1</sup> 1/21 <sup>-1</sup>	5d	(5/2) <sup>+1</sup> 11/21 <sub>6</sub>		Ric		
7123.112(11)	14034.939(21)	7123.106(3)	0.006	59	6s	(5/2) <sup>+1</sup> 5/21 <sub>6</sub>	7p	(5/2) <sup>+1</sup> 5/21 <sup>-3</sup>		Ric		
7123.112(11)	14034.939(21)	7123.1061(21)	0.006	59	sp	( <sup>3</sup> F) <sup>-1</sup> 3C <sup>-5</sup>	5g	(5/2) <sup>+1</sup> 11/21 <sub>6</sub>		Ric		
7123.112(11)	14034.939(21)	7123.1212(21)	-0.010	59	sp	( <sup>3</sup> F) <sup>-1</sup> 3C <sup>-5</sup>	5g	(5/2) <sup>+1</sup> 11/21 <sub>6</sub>		Ric		
7127.032(8)	14027.030(11)	7127.0305(11)	0.002	150	5p	(3/2) <sup>+1</sup> 5/21 <sup>-2</sup>	5d	(5/2) <sup>+1</sup> 3/21 <sub>6</sub>		Ric		
7139.649(5)	14002.431(10)	7139.653(3)	-0.004	1500	5s	(5/2) <sup>+1</sup> 5/21 <sub>6</sub>	7p	(5/2) <sup>+1</sup> 7/21 <sup>-4</sup>		Ric		
7157.757(5)	13967.006(10)	7157.7517(8)	0.006	1500	6s	(5/2) <sup>+1</sup> 5/21 <sub>6</sub>	sp	( <sup>3</sup> F) <sup>-1</sup> 3F <sup>-1</sup> D <sup>-2</sup>		Ric	B00	
7182.106(7)	13919.655(14)	7182.104(5)	0.002	60	6s	(5/2) <sup>+1</sup> 5/21 <sub>6</sub>	7p	(5/2) <sup>+1</sup> 5/21 <sup>-2</sup>		Ric		
7189.458(4)	13905.422(7)	7189.4534(12)	0.004	1300	5p	(3/2) <sup>+1</sup> 1/21 <sup>-1</sup>	5d	(5/2) <sup>+1</sup> 3/21 <sub>6</sub>		Ric		
7194.900(3)	13894.903(6)	7194.8933(10)	0.007	6800	4p	1D <sup>2</sup>	s <sup>2</sup>	(3/2) <sup>+1</sup> 3/21 <sub>6</sub>		F <sub>2</sub> Re	TW	
7255.7937(20)	13778.293(4)	7255.7899(9)	0.0038	6400	sp	( <sup>3</sup> F) <sup>-1</sup> 1D <sup>-2</sup>	6s	(3/2) <sup>+1</sup> 9/21 <sub>6</sub>	D+	Ric		
7271.507(6)	13748.519(11)	7271.4991(10)	0.007	460	5p	(5/2) <sup>+1</sup> 5/21 <sup>-3</sup>	5d	(3/2) <sup>+1</sup> 3/21 <sub>6</sub>		Ric		
7306.511(4)	13682.653(7)	7306.5042(9)	0.007	3700	5p	( <sup>3</sup> F) <sup>-1</sup> 1D <sup>-2</sup>	6s	( <sup>3</sup> F) <sup>-1</sup> 3/21 <sub>6</sub>		Ric		
7326.007(4)	13646.242(7)	7326.0039(8)	0.003	6900	5s	(5/2) <sup>+1</sup> 5/21 <sub>6</sub>	sp	( <sup>3</sup> F) <sup>-1</sup> 1D <sup>-2</sup>	B	Ric	B00	

Table A1. Cont.

$\lambda_{obs}^a$ (Å)	$\sigma_{obs}^b$ (cm <sup>-1</sup> )	$\lambda_{Ritz}^c$ (Å)	$\Delta\lambda_{obs-Ritz}^d$ (Å)	$I_{obs}^d$ (arb. u.)	Char <sup>e</sup>	Lower Level	Upper Level	A (s <sup>-1</sup> )	Acc <sup>f</sup>	Line Ref. <sup>g</sup>	TP Ref. <sup>h</sup>	Notes <sup>h</sup>
7331.6940(19)	13635.656(4)	7331.6941(7)	-0.0001	5100		5p	6s			F <sub>1</sub> Re		
7382.275(3)	13542.229(16)	7382.2720(14)	0.003	3500		4d	(5/2) <sup>2</sup> [3/2] <sup>1</sup> <sub>2</sub>	1.6e+07	D+	F <sub>1</sub> Re	TW	
7396.156(6)	13516.615(11)	7396.1523(12)	0.003	1900		5p	(3/2) <sup>2</sup> [3/2] <sup>1</sup> <sub>2</sub>			R1c		
7399.8836(16)	13510.005(3)	7399.8787(7)	0.0049	14000		5s	(5/2) <sup>2</sup> [5/2] <sup>1</sup> <sub>2</sub>	2.57e+07	B	F <sub>1</sub> Re	B00	
7404.3561(11)	13501.8442(20)	7404.3532(6)	0.0029	55000		5s	(5/2) <sup>2</sup> [5/2] <sup>1</sup> <sub>2</sub>	2.0e+07	D+	F <sub>1</sub> Re	TW	L
7417.483(5)	13477.950(9)	7417.4819(12)	0.001	2400		5p	(3/2) <sup>2</sup> [3/2] <sup>1</sup> <sub>2</sub>			R1c		
7420.556(4)	13473.368(7)	7420.5668(9)	-0.010	4100		5s	(3/2) <sup>2</sup> [3/2] <sup>1</sup> <sub>2</sub>	3.1e+06	C	R1c	B00	
7422.602(5)	13468.656(9)	7422.5904(11)	0.011	790		4p	3p <sup>3</sup>			R1c		
7434.155(4)	13447.725(7)	7434.1525(15)	0.002	3700		4d	(3/2) <sup>2</sup> [1/2] <sup>1</sup> <sub>2</sub>	1.3e+07	D+	R1c	TW	
7438.1504(13)	13440.5007(24)	7438.1505(10)	-0.0001	11000		5p	(3/2) <sup>2</sup> [1/2] <sup>1</sup> <sub>2</sub>	1.0e+07	D+	F <sub>1</sub> Re	TW	
7481.554(8)	13362.5281(15)	7481.5532(10)	-0.001	190		5p	(5/2) <sup>2</sup> [5/2] <sup>1</sup> <sub>2</sub>	3.0e+06	D+	R1c		
7493.289(8)	13341.6021(14)	7493.2883(20)	0.000	130		6p	(5/2) <sup>2</sup> [7/2] <sup>1</sup> <sub>3</sub>	3.0e+06	D+	R1c	TW	
7562.0141(17)	13220.350(3)	7562.0167(9)	-0.0026	16000		5s	(3/2) <sup>2</sup> [3/2] <sup>1</sup> <sub>2</sub>	3.8e+07	B	F <sub>1</sub> Re	B00	
7564.324(8)	13216.314(4)	7564.3057(14)	0.018	64		5p	(3/2) <sup>2</sup> [3/2] <sup>1</sup> <sub>2</sub>			R1c		
7575.242(7)	13197.266(12)	7575.2394(12)	0.011	220		5p	(3/2) <sup>2</sup> [3/2] <sup>1</sup> <sub>2</sub>			R1c		
7579.023(5)	13190.681(5)	7579.0283(10)	-0.005	20000		5s	(3/2) <sup>2</sup> [3/2] <sup>1</sup> <sub>2</sub>	4.1e+07	B	F <sub>1</sub> Re	B00	
7579.850(5)	13189.242(9)	7579.8494(9)	0.001	8400		5s	(3/2) <sup>2</sup> [3/2] <sup>1</sup> <sub>2</sub>	1.15e+07	B	F <sub>1</sub> Re	B00	
7583.273(8)	13183.289(13)	7583.339(4)	-0.066	64	?	4d	(5/2) <sup>2</sup> [1/2] <sup>1</sup> <sub>2</sub>			R1c		X
7652.326(7)	13064.3147(12)	7652.337(5)	-0.0011	26000		5s	(5/2) <sup>2</sup> [5/2] <sup>1</sup> <sub>2</sub>	2.35e+07	B	F <sub>1</sub> Re	B00	
7664.6151(12)	13014.3283(20)	7664.6465(7)	-0.0014	52000		5p	(5/2) <sup>2</sup> [7/2] <sup>1</sup> <sub>3</sub>	3.5e+07	D+	F <sub>1</sub> Re	TW	L
7681.787(4)	13014.223(7)	7681.7968(10)	-0.010	570		5p	(3/2) <sup>2</sup> [5/2] <sup>1</sup> <sub>2</sub>			R1c		
7712.118(6)	12962.535(9)	7712.121(3)	-0.003	640		6p	(5/2) <sup>2</sup> [3/2] <sup>1</sup> <sub>2</sub>	3.7e+06	D+	R1c	TW	
7726.637(4)	12938.681(6)	7726.6439(10)	-0.007	9000		5s	(3/2) <sup>2</sup> [3/2] <sup>1</sup> <sub>2</sub>	1.70e+07	B	F <sub>1</sub> Re	B00	
7738.6656(12)	12918.5693(21)	7738.6644(9)	0.0012	30000		5p	(3/2) <sup>2</sup> [5/2] <sup>1</sup> <sub>2</sub>	4.5e+07	D+	F <sub>1</sub> Re	TW	L
7739.499(8)	12917.179(14)	7739.505(4)	-0.006	1600		6p	(5/2) <sup>2</sup> [5/2] <sup>1</sup> <sub>2</sub>	7.1e+06	D+	R1c	TW	
7744.0889(18)	12909.522(3)	7744.0905(8)	-0.0016	7800		5p	(5/2) <sup>2</sup> [7/2] <sup>1</sup> <sub>3</sub>			R1c		
7754.3688(20)	12892.408(3)	7754.3653(10)	0.0035	11000		5p	(3/2) <sup>2</sup> [1/2] <sup>1</sup> <sub>2</sub>	9.e+06	D+	F <sub>1</sub> Re	TW	
7766.516(9)	12862.244(16)	7766.511(7)	0.006	32		6p	(3/2) <sup>2</sup> [1/2] <sup>1</sup> <sub>2</sub>			R1c		
7773.196(7)	12861.182(12)	7773.192(9)	-0.003	3200		5s	(5/2) <sup>2</sup> [5/2] <sup>1</sup> <sub>2</sub>	1.08e+06	C	R1c	B00	
7778.7353(13)	12851.023(22)	7778.7347(8)	0.006	25000		5p	(5/2) <sup>2</sup> [5/2] <sup>1</sup> <sub>2</sub>	1.3e+07	D+	F <sub>1</sub> Re	TW	L
7805.1886(13)	12808.4659(21)	7805.1878(7)	0.008	26000		5p	(5/2) <sup>2</sup> [5/2] <sup>1</sup> <sub>2</sub>	1.6e+07	D+	F <sub>1</sub> Re	TW	L
7807.6534(12)	12794.4224(20)	7807.6526(7)	0.0007	82000		5p	(5/2) <sup>2</sup> [5/2] <sup>1</sup> <sub>2</sub>	3.6e+07	D+	F <sub>1</sub> Re	TW	L
7812.3182(19)	12790.777(3)	7812.3164(10)	0.0018	10000		5p	(3/2) <sup>2</sup> [1/2] <sup>1</sup> <sub>2</sub>			F <sub>1</sub> Re	TW	
7820.577(4)	12783.646(16)	7820.5768(10)	-0.0000	7300		5s	(3/2) <sup>2</sup> [3/2] <sup>1</sup> <sub>2</sub>	1.51e+07	B	F <sub>1</sub> Re	B00	
7825.6528(12)	12774.9718(20)	7825.6530(7)	-0.0002	59000		5p	(5/2) <sup>2</sup> [7/2] <sup>1</sup> <sub>3</sub>	5.2e+07	B	F <sub>1</sub> Re	B00	L
7845.0720(12)	12748.3378(20)	7845.0795(9)	-0.0003	24000		5p	(3/2) <sup>2</sup> [3/2] <sup>1</sup> <sub>2</sub>	3.8e+07	D+	F <sub>1</sub> Re	TW	L
7853.984(9)	12728.890(15)	7853.980(4)	0.004	190		6p	(5/2) <sup>2</sup> [5/2] <sup>1</sup> <sub>2</sub>			R1c		
7860.576(5)	12718.216(7)	7860.5740(10)	0.002	5700		6p	(3/2) <sup>2</sup> [5/2] <sup>1</sup> <sub>2</sub>			R1c		
7862.652(9)	12714.857(14)	7862.654(3)	-0.002	250		6p	(5/2) <sup>2</sup> [5/2] <sup>1</sup> <sub>2</sub>	2.9e+06	D+	R1c	TW	
7886.076(9)	12677.091(15)	7886.097(5)	-0.021	61		6p	(3/2) <sup>2</sup> [1/2] <sup>1</sup> <sub>2</sub>			R1c		
7890.568(4)	12669.874(16)	7890.5666(8)	0.001	3500		5s	(5/2) <sup>2</sup> [5/2] <sup>1</sup> <sub>2</sub>	5.8e+06	B	F <sub>1</sub> Re	B00	
7895.8050(13)	12661.4700(22)	7895.8039(8)	0.0011	21000		5s	(3/2) <sup>2</sup> [5/2] <sup>1</sup> <sub>2</sub>	4.3e+07	B	F <sub>1</sub> Re	B00	L
7902.5482(13)	12650.6660(21)	7902.5499(8)	-0.0017	25000		5s	(3/2) <sup>2</sup> [5/2] <sup>1</sup> <sub>3</sub>	4.9e+07	B	F <sub>1</sub> Re	B00	L

Table A1. Cont.

$\lambda_{\text{obs}}^a$ (Å)	$\sigma_{\text{obs}}^b$ (cm <sup>-1</sup> )	$\lambda_{\text{Ritz}}^c$ (Å)	$\Delta\lambda_{\text{obs-Ritz}}^d$ (Å)	$I_{\text{obs}}^d$ (arb. u.)	Char <sup>e</sup>	Lower Level	Upper Level	A (s <sup>-1</sup> )	Acc <sup>f</sup>	Line Ref. <sup>g</sup>	TP Ref. <sup>h</sup>	Notes <sup>h</sup>
7907.351(10)	12642.983(16)	7907.364(5)	-0.014	61	6p	(5/2) <sup>+</sup> 5/2 <sub>1/2</sub>	(5/2) <sup>+</sup> 3/2 <sub>1/2</sub>	4.7e+07	B	Ric	B00	L
7944.4368(6)	12583.963(10)	7944.4363(5)	0.003	17000	5s	(5/2) <sup>+</sup> 15/2 <sub>3/2</sub>	(5/2) <sup>+</sup> 17/2 <sub>1/2</sub>	1.0e+07	D+	F_Re	TW	
7967.067(5)	12548.220(8)	7967.065(4)	0.002	2100	6p	(3/2) <sup>+</sup> 5/2 <sub>1/2</sub>	(3/2) <sup>+</sup> 7/2 <sub>1/2</sub>	2.9e+07	B	Ric	B00	
7972.031(5)	12540.406(7)	7972.0306(10)	0.000	7800	5s	(5/2) <sup>+</sup> 15/2 <sub>3/2</sub>	(5/2) <sup>+</sup> 17/2 <sub>1/2</sub>	1.7e+07	D+	F_Re	TW	X
7981.574(9)	12525.413(15)	7981.4451(23)	0.128	59	4f	(5/2) <sup>+</sup> 17/2 <sub>1/2</sub>	(5/2) <sup>+</sup> 19/2 <sub>1/2</sub>	3.2e+07	D+	F_Re	B00	L
7988.1598(13)	12515.0857(20)	7988.1620(7)	-0.0022	47000	5p	(5/2) <sup>+</sup> 5/2 <sub>3/2</sub>	(5/2) <sup>+</sup> 5/2 <sub>1/2</sub>	1.2e+07	B	F_Re	B00	
7996.793(3)	12501.575(5)	7996.7854(10)	0.007	9000	5s	(3/2) <sup>+</sup> 13/2 <sub>1/2</sub>	(3/2) <sup>+</sup> 11/2 <sub>1/2</sub>	8.2e+06	D+	R2nc	TW	
8006.515(5)	12486.394(8)	8006.525(4)	-0.009	440	6p	(3/2) <sup>+</sup> 15/2 <sub>1/2</sub>	(3/2) <sup>+</sup> 17/2 <sub>1/2</sub>	5.9e+06	D+	F_Re	TW	
8026.479(3)	12465.338(5)	8026.4828(12)	-0.004	7100	5p	(3/2) <sup>+</sup> 13/2 <sub>1/2</sub>	(3/2) <sup>+</sup> 13/2 <sub>1/2</sub>	5.9e+06	D+	F_Re	TW	
8042.489(7)	12430.544(11)	8042.494(4)	-0.005	230	7d	(5/2) <sup>+</sup> 3/2 <sub>1/2</sub>	(5/2) <sup>+</sup> 3/2 <sub>1/2</sub>	8.2e+06	D+	Ric		
		8053.200(6)			6p	(3/2) <sup>+</sup> 15/2 <sub>1/2</sub>	(3/2) <sup>+</sup> 17/2 <sub>1/2</sub>	2.3e+06	D+	Ric	TW	
8053.339(16)	12413.796(24)	8053.338(4)	-0.019	230	sp	( <sup>1</sup> G) <sup>3</sup> pc <sup>+</sup> 3F <sup>+</sup> <sub>3/2</sub>	( <sup>1</sup> G) <sup>3</sup> pc <sup>+</sup> 3F <sup>+</sup> <sub>3/2</sub>			Ric		
8054.227(7)	12412.428(11)	8054.239(3)	-0.012	110	sp	( <sup>1</sup> G) <sup>3</sup> pc <sup>+</sup> 3F <sup>+</sup> <sub>3/2</sub>	( <sup>1</sup> G) <sup>3</sup> pc <sup>+</sup> 3F <sup>+</sup> <sub>3/2</sub>			Ric		
8074.999(7)	12380.498(11)	8074.999(3)	0.000	420	6p	(5/2) <sup>+</sup> 17/2 <sub>3/2</sub>	(5/2) <sup>+</sup> 15/2 <sub>1/2</sub>	3.5e+06	D+	Ric	TW	
8075.456(7)	12379.797(11)	8075.4576(10)	-0.001	2300	5s	(3/2) <sup>+</sup> 13/2 <sub>1/2</sub>	(3/2) <sup>+</sup> 15/2 <sub>1/2</sub>	2.8e+05	C	Ric	B00	
8088.5846(15)	12359.7038(23)	8088.5888(11)	-0.0042	13000	5p	(3/2) <sup>+</sup> 15/2 <sub>1/2</sub>	(3/2) <sup>+</sup> 17/2 <sub>1/2</sub>	1.6e+07	D+	F_Re	TW	
8095.5267(14)	12349.1051(21)	8095.5268(8)	-0.0001	26000	5s	(5/2) <sup>+</sup> 15/2 <sub>3/2</sub>	(5/2) <sup>+</sup> 17/2 <sub>1/2</sub>	3.7e+07	B	F_Re	B00	
8098.519(7)	12344.542(11)	8098.5396(14)	-0.020	550	sp	( <sup>3</sup> F) <sup>3</sup> pc <sup>+</sup> 3C <sup>+</sup> <sub>3/2</sub>	( <sup>3</sup> F) <sup>3</sup> pc <sup>+</sup> 3C <sup>+</sup> <sub>3/2</sub>			Ric		
8100.868(7)	12340.963(11)	8100.883(3)	-0.015	830	6p	(5/2) <sup>+</sup> 17/2 <sub>1/2</sub>	(5/2) <sup>+</sup> 15/2 <sub>1/2</sub>	2.7e+06	D+	Ric	TW	
8103.352(7)	12337.180(11)	8103.353(4)	-0.001	550	sp	( <sup>1</sup> G) <sup>3</sup> pc <sup>+</sup> 3F <sup>+</sup> <sub>3/2</sub>	( <sup>1</sup> G) <sup>3</sup> pc <sup>+</sup> 3F <sup>+</sup> <sub>3/2</sub>			Ric		
8154.003(6)	12260.545(9)	8154.012(4)	-0.009	2000	6p	(5/2) <sup>+</sup> 17/2 <sub>3/2</sub>	(5/2) <sup>+</sup> 19/2 <sub>1/2</sub>	5.4e+06	D+	Ric	TW	
8192.221(6)	12203.347(9)	8192.2333(13)	-0.012	10700	5p	(3/2) <sup>+</sup> 13/2 <sub>1/2</sub>	(3/2) <sup>+</sup> 15/2 <sub>1/2</sub>	2.0e+07	D+	F_Re	TW	
8192.330(3)	12203.185(4)	8192.3279(10)	0.002	3300	sp	( <sup>3</sup> F) <sup>3</sup> pc <sup>+</sup> 3F <sup>+</sup> <sub>3/2</sub>	( <sup>3</sup> F) <sup>3</sup> pc <sup>+</sup> 3F <sup>+</sup> <sub>3/2</sub>	5.9e+06	D+	F_Re	TW	
8201.998(7)	12188.949(11)	8201.908(4)	-0.010	52	6p	(3/2) <sup>+</sup> 15/2 <sub>1/2</sub>	(3/2) <sup>+</sup> 17/2 <sub>1/2</sub>	4.6e+07	B	Ric	B00	
8235.272(4)	12139.553(6)	8235.2788(14)	-0.007	5600	5s	(3/2) <sup>+</sup> 13/2 <sub>1/2</sub>	(3/2) <sup>+</sup> 11/2 <sub>1/2</sub>			F_Re		
8256.944(6)	12107.691(9)	8256.9412(13)	0.002	3000	5p	(5/2) <sup>+</sup> 15/2 <sub>1/2</sub>	(5/2) <sup>+</sup> 13/2 <sub>1/2</sub>			F_Re		
8277.5525(14)	12069.5460(21)	8277.5527(8)	-0.0003	20000	5s	(5/2) <sup>+</sup> 15/2 <sub>3/2</sub>	(5/2) <sup>+</sup> 13/2 <sub>1/2</sub>	4.3e+07	B	F_Re	B00	
8283.1521(14)	12067.3813(21)	8283.1520(9)	0.0000	23000	sp	( <sup>3</sup> F) <sup>3</sup> pc <sup>+</sup> 1F <sup>+</sup> <sub>3/2</sub>	( <sup>3</sup> F) <sup>3</sup> pc <sup>+</sup> 1F <sup>+</sup> <sub>3/2</sub>			F_Re		
8298.461(7)	12047.116(11)	8298.465(3)	-0.004	72	sp	( <sup>3</sup> F) <sup>3</sup> pc <sup>+</sup> 3F <sup>+</sup> <sub>3/2</sub>	( <sup>3</sup> F) <sup>3</sup> pc <sup>+</sup> 3F <sup>+</sup> <sub>3/2</sub>			Ric		
8306.475(5)	12035.493(7)	8306.4866(14)	-0.011	890	4p	3D <sub>2</sub>	3D <sub>2</sub>			Ric		
8308.148(7)	12033.070(11)	8308.150(3)	-0.002	120	sp	( <sup>3</sup> F) <sup>3</sup> pc <sup>+</sup> 3F <sup>+</sup> <sub>3/2</sub>	( <sup>3</sup> F) <sup>3</sup> pc <sup>+</sup> 3F <sup>+</sup> <sub>3/2</sub>			Ric		
8328.395(6)	12003.817(8)	8328.393(3)	0.001	470	6p	(5/2) <sup>+</sup> 15/2 <sub>1/2</sub>	(5/2) <sup>+</sup> 17/2 <sub>1/2</sub>	3.1e+06	D+	Ric	TW	
8333.074(7)	11997.077(10)	8333.072(4)	0.001	470	6p	(5/2) <sup>+</sup> 15/2 <sub>3/2</sub>	(5/2) <sup>+</sup> 15/2 <sub>1/2</sub>	2.3e+06	D+	Ric	TW	
8333.617(8)	11996.294(12)	8333.6418(20)	-0.024	580	sp	( <sup>3</sup> F) <sup>3</sup> pc <sup>+</sup> 3C <sup>+</sup> <sub>3/2</sub>	( <sup>3</sup> F) <sup>3</sup> pc <sup>+</sup> 3C <sup>+</sup> <sub>3/2</sub>			Ric		
8336.333(5)	11992.386(8)	8336.3323(20)	0.001	3500	sp	( <sup>3</sup> F) <sup>3</sup> pc <sup>+</sup> 1F <sup>+</sup> <sub>3/2</sub>	( <sup>3</sup> F) <sup>3</sup> pc <sup>+</sup> 1F <sup>+</sup> <sub>3/2</sub>	1.4e+06	D+	Ric	TW	
8353.837(7)	11967.259(10)	8353.843(3)	-0.006	230	6p	(5/2) <sup>+</sup> 15/2 <sub>3/2</sub>	(5/2) <sup>+</sup> 15/2 <sub>1/2</sub>	3.1e+06	D+	Ric	TW	
8381.848(7)	11927.237(11)	8381.872(4)	-0.004	45	6p	(5/2) <sup>+</sup> 15/2 <sub>1/2</sub>	(5/2) <sup>+</sup> 19/2 <sub>1/2</sub>			Ric		
8385.624(7)	11921.895(11)	8385.629(4)	-0.005	67	4f	(5/2) <sup>+</sup> 15/2 <sub>1/2</sub>	(5/2) <sup>+</sup> 13/2 <sub>1/2</sub>			Ric		
8394.566(8)	11909.195(11)	8394.5743(12)	-0.008	110	5s	(5/2) <sup>+</sup> 19/2 <sub>1/2</sub>	(5/2) <sup>+</sup> 19/2 <sub>1/2</sub>			Ric		
8402.897(7)	11897.388(9)	8402.9047(11)	-0.007	1600	4f	( <sup>3</sup> F) <sup>3</sup> pc <sup>+</sup> 1D <sup>+</sup> <sub>2</sub>	( <sup>3</sup> F) <sup>3</sup> pc <sup>+</sup> 1D <sup>+</sup> <sub>2</sub>	3.9e+06	C	Ric	B00	
8450.062(8)	11830.982(11)	8450.078(3)	-0.016	63	sp	( <sup>3</sup> F) <sup>3</sup> pc <sup>+</sup> 3D <sup>+</sup> <sub>2</sub>	( <sup>3</sup> F) <sup>3</sup> pc <sup>+</sup> 3D <sup>+</sup> <sub>2</sub>			Ric		
8477.298(5)	11792.971(7)	8477.3077(17)	-0.009	3900	4p	1P <sup>+</sup> <sub>1</sub> s <sup>2</sup>	<sup>1</sup> D textsubscript2			Ric		

Table A1. Cont.

$\lambda_{\text{obs}}^a$ (Å)	$\sigma_{\text{res}}^b$ (cm <sup>-1</sup> )	$\lambda_{\text{Ritz}}^c$ (Å)	$\Delta\lambda_{\text{obs-Ritz}}^d$ (Å)	$I_{\text{obs}}^d$ (arb. u.)	Char <sup>e</sup>	Lower Level	Upper Level	A (s <sup>-1</sup> )	Acc <sup>f</sup>	Line Ref. <sup>g</sup>	TP Ref. <sup>h</sup>	Notes <sup>b</sup>
8503.394(5)	11756.780(7)	8503.397(9)	-0.004	3600	5s	(5/2) <sup>3</sup> F <sup>o</sup> 5/2 <sub>2</sub>	5p	1.6e+06	C	R1c	B00	
8511.0626(20)	11746.187(3)	8511.0647(10)	-0.0021	11000	sp	( <sup>4</sup> F) <sup>o</sup> 3D <sup>o</sup> 2	6s	(5/2) <sup>3</sup> F <sup>o</sup> 5/2 <sub>2</sub>	D+	F,R1c	TW	
8535.196(11)	11712.975(15)	8535.2020(23)	-0.006	77	sp	( <sup>4</sup> F) <sup>o</sup> 3P <sup>o</sup> 3D <sup>o</sup> 1	5g	(5/2) <sup>3</sup> F <sup>o</sup> 5/2 <sub>2</sub>		R1c		
8574.093(11)	11659.838(15)	8574.083(5)	0.010	690	5s	(3/2) <sup>3</sup> F <sup>o</sup> 3F <sup>o</sup> 4	6d	(5/2) <sup>3</sup> F <sup>o</sup> 5/2 <sub>2</sub>	B	R1c	B00	
8606.681(10)	11615.690(13)	8606.6732(12)	0.008	1100	sp	(3/2) <sup>3</sup> F <sup>o</sup> 3D <sup>o</sup> 2	sp	(5/2) <sup>3</sup> F <sup>o</sup> 5/2 <sub>2</sub>		R1c		
8609.132(5)	11612.384(7)	8609.1359(12)	-0.004	1100	sp	( <sup>4</sup> F) <sup>o</sup> 3P <sup>o</sup> 1D <sup>o</sup> 2	6s	(5/2) <sup>3</sup> F <sup>o</sup> 5/2 <sub>2</sub>		R1c		
8729.820(9)	11451.845(12)	8729.822(3)	-0.002	160	sp	( <sup>4</sup> G) <sup>o</sup> 3P <sup>o</sup> 3P <sup>o</sup> 2	5g	(3/2) <sup>3</sup> F <sup>o</sup> 5/2 <sub>2</sub>		R1c		
8730.233(7)	11451.303(9)	8730.232(3)	0.002	110	sp	( <sup>4</sup> G) <sup>o</sup> 3P <sup>o</sup> 3P <sup>o</sup> 3	8s	(3/2) <sup>3</sup> F <sup>o</sup> 5/2 <sub>2</sub>		R1c		
8797.094(7)	11364.269(9)	8797.0968(22)	-0.002	380	sp	( <sup>4</sup> F) <sup>o</sup> 1P <sup>o</sup> 3F <sup>o</sup> 3	5g	(5/2) <sup>3</sup> F <sup>o</sup> 5/2 <sub>2</sub>	D+	R1c	TW	
8800.120(8)	11360.362(10)	8800.122(3)	-0.002	74	5g	( <sup>4</sup> F) <sup>o</sup> 1P <sup>o</sup> 3F <sup>o</sup> 4	5g	(5/2) <sup>3</sup> F <sup>o</sup> 5/2 <sub>2</sub>		R1c		
8801.397(8)	11347.110(10)	8810.397(4)	0.000	290	6p	(5/2) <sup>3</sup> F <sup>o</sup> 7/2 <sup>o</sup> 1	8s	(5/2) <sup>3</sup> F <sup>o</sup> 5/2 <sub>2</sub>	D+	R1c	TW	
8937.241(8)	11186.064(10)	8937.281(3)	-0.039	13	5d	(5/2) <sup>3</sup> F <sup>o</sup> 5/2 <sub>2</sub>	5f	(3/2) <sup>3</sup> F <sup>o</sup> 7/2 <sup>o</sup> 1		R1c		X
8959.159(9)	11158.698(11)	8959.1604(12)	-0.001	1300	5s	(3/2) <sup>3</sup> F <sup>o</sup> 3D <sup>o</sup> 2	sp	( <sup>4</sup> F) <sup>o</sup> 3P <sup>o</sup> 1F <sup>o</sup> 3	C	R1c	B00	
8967.150(9)	11148.754(11)	8967.143(4)	0.007	250	sp	( <sup>4</sup> G) <sup>o</sup> 3P <sup>o</sup> 3P <sup>o</sup> 2	6d	(3/2) <sup>3</sup> F <sup>o</sup> 5/2 <sub>2</sub>		R1c		
8991.446(9)	11118.629(11)	8991.447(7)	-0.001	12	sp	( <sup>4</sup> P) <sup>o</sup> 3P <sup>o</sup> 1P <sup>o</sup> 1	6d	(3/2) <sup>3</sup> F <sup>o</sup> 5/2 <sub>2</sub>		R2nc		
9001.419(8)	11106.311(9)	9001.428(5)	-0.009	25	6p	(3/2) <sup>3</sup> F <sup>o</sup> 5/2 <sub>2</sub>	8s	(3/2) <sup>3</sup> F <sup>o</sup> 5/2 <sub>2</sub>		R1c		
9005.757(8)	11100.961(9)	9005.754(4)	0.003	4300	sp	( <sup>4</sup> F) <sup>o</sup> 1P <sup>o</sup> 3G <sup>o</sup> 3	5g	(3/2) <sup>3</sup> F <sup>o</sup> 5/2 <sub>2</sub>	D+	R1c	TW	X
9015.187(9)	11089.349(11)	9015.144(4)	0.043	310	sp	( <sup>4</sup> F) <sup>o</sup> 1P <sup>o</sup> 3G <sup>o</sup> 4	5g	(3/2) <sup>3</sup> F <sup>o</sup> 5/2 <sub>2</sub>		R1c		
9029.347(8)	11071.959(9)	9029.343(4)	0.003	300	sp	( <sup>4</sup> F) <sup>o</sup> 1P <sup>o</sup> 3F <sup>o</sup> 2	8s	(5/2) <sup>3</sup> F <sup>o</sup> 5/2 <sub>2</sub>		R1c		
9036.147(8)	11036.627(9)	9036.132(4)	0.015	600	sp	( <sup>4</sup> G) <sup>o</sup> 3P <sup>o</sup> 3H <sup>o</sup> 5	5g	(3/2) <sup>3</sup> F <sup>o</sup> 5/2 <sub>2</sub>	D+	R1c	TW	
9067.974(8)	11024.796(10)	9067.9717(16)	0.002	180	5s	(5/2) <sup>3</sup> F <sup>o</sup> 5/2 <sub>2</sub>	sp	( <sup>4</sup> F) <sup>o</sup> 3P <sup>o</sup> 3P <sup>o</sup> 2	C	R1c	B00	
9086.933(9)	11001.793(11)	9086.938(4)	0.005	1200	6p	(5/2) <sup>3</sup> F <sup>o</sup> 5/2 <sub>2</sub>	8s	(5/2) <sup>3</sup> F <sup>o</sup> 5/2 <sub>2</sub>	D+	R1c	TW	
9089.413(9)	10998.792(11)	9089.4094(24)	0.005	46	5d	(5/2) <sup>3</sup> F <sup>o</sup> 7/2 <sup>o</sup> 1	5f	(3/2) <sup>3</sup> F <sup>o</sup> 5/2 <sub>2</sub>		R1c		X
9093.704(9)	10993.602(11)	9093.632(4)	0.072	12	sp	( <sup>4</sup> P) <sup>o</sup> 1P <sup>o</sup> 2	6d	(3/2) <sup>3</sup> F <sup>o</sup> 5/2 <sub>2</sub>		R1c		
9096.064(9)	10990.749(11)	9096.054(6)	0.011	81	5d	(5/2) <sup>3</sup> F <sup>o</sup> 5/2 <sub>2</sub>	7p	(5/2) <sup>3</sup> F <sup>o</sup> 5/2 <sub>2</sub>		R1c		
9097.529(9)	10988.980(11)	9097.525(3)	0.004	460	sp	( <sup>4</sup> P) <sup>o</sup> 1P <sup>o</sup> 3P <sup>o</sup> 2	7s	(5/2) <sup>3</sup> F <sup>o</sup> 5/2 <sub>2</sub>		R1c		
9098.493(9)	10987.815(11)	9098.489(3)	0.005	69	5d	(5/2) <sup>3</sup> F <sup>o</sup> 5/2 <sub>2</sub>	5f	(3/2) <sup>3</sup> F <sup>o</sup> 5/2 <sub>2</sub>		R1c		
9101.459(12)	10984.235(15)	9101.4285(22)	0.030	23	5d	(5/2) <sup>3</sup> F <sup>o</sup> 5/2 <sub>2</sub>	5f	(3/2) <sup>3</sup> F <sup>o</sup> 5/2 <sub>2</sub>		R1c		
9103.234(6)	10982.083(8)	9103.2366(12)	-0.003	2600	5p	(3/2) <sup>3</sup> F <sup>o</sup> 5/2 <sub>2</sub>	6s	(5/2) <sup>3</sup> F <sup>o</sup> 5/2 <sub>2</sub>		R1c		
9107.895(9)	10976.473(11)	9107.878(6)	0.016	230	5s	(5/2) <sup>3</sup> F <sup>o</sup> 5/2 <sub>2</sub>	6s	(5/2) <sup>3</sup> F <sup>o</sup> 5/2 <sub>2</sub>	C	R1c	B00	
9115.200(9)	10967.075(11)	9115.643(10)	0.057	46	5f	(5/2) <sup>3</sup> F <sup>o</sup> 5/2 <sub>2</sub>	9d	(5/2) <sup>3</sup> F <sup>o</sup> 5/2 <sub>2</sub>	9.1e+04	R1c		X
9125.941(9)	10954.767(11)	9125.932(4)	0.009	340	sp	( <sup>4</sup> G) <sup>o</sup> 3P <sup>o</sup> 3P <sup>o</sup> 2	5g	(3/2) <sup>3</sup> F <sup>o</sup> 5/2 <sub>2</sub>		R2nc		
9154.181(18)	10920.973(21)	9154.160(4)	0.021	170	5p	( <sup>4</sup> G) <sup>o</sup> 3P <sup>o</sup> 3P <sup>o</sup> 2	5g	(3/2) <sup>3</sup> F <sup>o</sup> 5/2 <sub>2</sub>		R2c		
9158.409(9)	10915.931(11)	9158.393(4)	0.016	450	sp	( <sup>4</sup> P) <sup>o</sup> 3P <sup>o</sup> 3P <sup>o</sup> 1	5g	(5/2) <sup>3</sup> F <sup>o</sup> 5/2 <sub>2</sub>		R1c		
9179.306(12)	10891.081(14)	9179.319(7)	-0.014	610	5d	(3/2) <sup>3</sup> F <sup>o</sup> 5/2 <sub>2</sub>	7p	(3/2) <sup>3</sup> F <sup>o</sup> 5/2 <sub>2</sub>		R2nc		
9205.3214(22)	10860.301(3)	9205.3242(12)	-0.0028	5800	5p	(3/2) <sup>3</sup> F <sup>o</sup> 5/2 <sub>2</sub>	6s	(5/2) <sup>3</sup> F <sup>o</sup> 5/2 <sub>2</sub>		F,R1c		
9219.491(10)	10843.610(12)	9219.466(5)	0.025	32	5d	(5/2) <sup>3</sup> F <sup>o</sup> 5/2 <sub>2</sub>	7p	(5/2) <sup>3</sup> F <sup>o</sup> 5/2 <sub>2</sub>	1.3e+06	R1c	B00	
9226.742(10)	10835.088(12)	9226.7371(12)	0.005	730	sp	(5/2) <sup>3</sup> F <sup>o</sup> 5/2 <sub>2</sub>	5p	(5/2) <sup>3</sup> F <sup>o</sup> 5/2 <sub>2</sub>		R1c		
9230.567(11)	10830.599(13)	9230.577(3)	-0.010	370	sp	( <sup>4</sup> P) <sup>o</sup> 1P <sup>o</sup> 3D <sup>o</sup> 3	7s	(5/2) <sup>3</sup> F <sup>o</sup> 5/2 <sub>2</sub>		R1c		
9234.272(8)	10826.253(10)	9234.258(3)	0.014	1300	sp	( <sup>4</sup> F) <sup>o</sup> 1P <sup>o</sup> 3D <sup>o</sup> 3	6d	(5/2) <sup>3</sup> F <sup>o</sup> 5/2 <sub>2</sub>		R1c		
9277.399(12)	10775.926(14)	9277.400(9)	-0.000	11	5f	(5/2) <sup>3</sup> F <sup>o</sup> 5/2 <sub>2</sub>	8g	(5/2) <sup>3</sup> F <sup>o</sup> 5/2 <sub>2</sub>	4.6e+06	R1nc		

Table A1. Cont.

$\lambda_{\text{obs}}^{\text{a}}$ (Å)	$\sigma_{\text{obs}}^{\text{b}}$ (cm <sup>-1</sup> )	$\lambda_{\text{Ritz}}^{\text{c}}$ (Å)	$\Delta\lambda_{\text{obs-Ritz}}^{\text{d}}$ (Å)	$I_{\text{obs}}^{\text{d}}$ (arb. u.)	Char <sup>e</sup>	Lower Level	Upper Level	A (s <sup>-1</sup> )	Acc <sup>f</sup>	Line Ref. g	TP Ref. h	Notes <sup>h</sup>
9296.634(12)	10753.631(14)	9296.580(6)	0.054	21	sp	(1D) <sup>3</sup> P <sup>o</sup> 3P <sup>o</sup> 2	5d	(3/2) <sup>2</sup> F <sup>o</sup> 5/2 <sup>b</sup>		R1c		X
9312.387(13)	10735.440(15)	9312.450(9)	-0.064	21	5f	(5/2) <sup>2</sup> F <sup>o</sup> 2/1 <sup>s</sup>	7g	(3/2) <sup>2</sup> F <sup>o</sup> 11/2 <sup>b</sup>		R1c		X
9317.944(9)	10729.037(10)	9317.943(4)	0.002	260	sp	( <sup>3</sup> F) <sup>3</sup> D <sup>+</sup> 4	6d	(3/2) <sup>2</sup> F <sup>o</sup> 5/2 <sup>b</sup>		R1c		
9324.302(9)	10721.722(10)	9323.128(20)	-0.011	21	sp	( <sup>3</sup> F) <sup>3</sup> C <sup>+</sup> 4	6d	(5/2) <sup>2</sup> F <sup>o</sup> 7/2 <sup>b</sup>		R1c		
9331.893(6)	10713.000(7)	9331.8965(12)	-0.004	2400	5s	(3/2) <sup>2</sup> F <sup>o</sup> 3/2 <sup>b</sup>	5p	(5/2) <sup>2</sup> F <sup>o</sup> 2/1 <sup>s</sup>	1.2e+06	R1c	B00	
9339.711(8)	10704.032(9)	9339.7151(17)	-0.004	360	5s	(5/2) <sup>2</sup> F <sup>o</sup> 5/2 <sup>b</sup>	5p	( <sup>3</sup> F) <sup>3</sup> P <sup>o</sup> 3P <sup>o</sup> 2	6.8e+05	R1c	B00	
9364.118(14)	10676.133(16)	9364.046(7)	0.072	10	4d	(3/2) <sup>2</sup> F <sup>o</sup> 7/2 <sup>b</sup>	5p	(1D) <sup>3</sup> P <sup>o</sup> 3P <sup>o</sup> 2		R1c		X
9374.435(19)	10664.383(21)	9374.447(23)	-0.006	10	4f	(5/2) <sup>2</sup> F <sup>o</sup> 7/2 <sup>b</sup>	6d	(3/2) <sup>2</sup> F <sup>o</sup> 5/2 <sup>b</sup>		R1c		
9391.049(12)	10645.517(14)	9390.959(21)	0.123	21	4f	(5/2) <sup>2</sup> F <sup>o</sup> 7/2 <sup>b</sup>	6d	(5/2) <sup>2</sup> F <sup>o</sup> 7/2 <sup>b</sup>		R1c		X
9415.060(9)	10618.368(10)	9415.044(6)	0.016	21	4d	(3/2) <sup>2</sup> F <sup>o</sup> 7/2 <sup>b</sup>	6d	(1D) <sup>3</sup> P <sup>o</sup> 3P <sup>o</sup> 2		R1c		
9424.164(12)	10608.110(14)	9424.151(4)	0.013	100	sp	( <sup>3</sup> F) <sup>3</sup> D <sup>+</sup> 4	6d	(3/2) <sup>2</sup> F <sup>o</sup> 3/2 <sup>b</sup>		R1c		
9444.862(10)	10444.863(11)	9444.858(11)	0.005	10	4d	(1D) <sup>3</sup> P <sup>o</sup> 3D <sup>+</sup> 3	6d	(1D) <sup>3</sup> P <sup>o</sup> 3D <sup>+</sup> 3		R1c		
9451.495(11)	10577.435(12)	9451.5130(13)	-0.018	1400	5p	(3/2) <sup>2</sup> F <sup>o</sup> 5/2 <sup>b</sup>	6s	(3/2) <sup>2</sup> F <sup>o</sup> 5/2 <sup>b</sup>		R1c		
9458.336(9)	10569.285(10)	9458.335(3)	0.000	72	4f	(5/2) <sup>2</sup> F <sup>o</sup> 7/2 <sup>b</sup>	6d	(5/2) <sup>2</sup> F <sup>o</sup> 7/2 <sup>b</sup>		R1c		
9459.889(10)	10565.049(11)	9459.895(4)	-0.005	31	sp	( <sup>3</sup> P) <sup>3</sup> P <sup>o</sup> 3C <sup>+</sup> 4	6d	(5/2) <sup>2</sup> F <sup>o</sup> 9/2 <sup>b</sup>		R1c		
9460.291(9)	10567.042(10)	9460.290(5)	0.001	1000	sp	( <sup>3</sup> P) <sup>3</sup> P <sup>o</sup> 3P <sup>o</sup> 0	5g	(5/2) <sup>2</sup> F <sup>o</sup> 3/2 <sup>b</sup>		R1c		
9461.294(10)	10566.480(11)	9461.3089(22)	-0.015	10	4f	(5/2) <sup>2</sup> F <sup>o</sup> 7/2 <sup>b</sup>	6d	(5/2) <sup>2</sup> F <sup>o</sup> 7/2 <sup>b</sup>		R1c		
9473.011(12)	10553.411(13)	9473.0050(12)	0.006	1300	5s	(3/2) <sup>2</sup> F <sup>o</sup> 3/2 <sup>b</sup>	7p	(5/2) <sup>2</sup> F <sup>o</sup> 3/2 <sup>b</sup>	1.13e+06	C	B00	
9474.119(10)	10552.176(11)	9474.106(5)	0.013	10	5d	(5/2) <sup>2</sup> F <sup>o</sup> 7/2 <sup>b</sup>	5p	(5/2) <sup>2</sup> F <sup>o</sup> 7/2 <sup>b</sup>		R1c		
9485.256(10)	10539.787(11)	9485.2726(23)	-0.017	21	10	(5/2) <sup>2</sup> F <sup>o</sup> 5/2 <sup>b</sup>	6d	(3/2) <sup>2</sup> F <sup>o</sup> 5/2 <sup>b</sup>		R1c		
9492.663(19)	10531.563(21)	9492.653(4)	0.010	10	4f	(3/2) <sup>2</sup> F <sup>o</sup> 5/2 <sup>b</sup>	6d	(3/2) <sup>2</sup> F <sup>o</sup> 5/2 <sup>b</sup>		R2c		X
9493.808(21)	10530.293(23)	9493.987(16)	-0.179	10	sp	( <sup>3</sup> P) <sup>3</sup> P <sup>o</sup> 3P <sup>o</sup> 3	6s	(3/2) <sup>2</sup> F <sup>o</sup> 3/2 <sup>b</sup>		R1c		
9500.248(10)	10523.154(11)	9500.262(3)	-0.014	52	sp	( <sup>3</sup> P) <sup>3</sup> P <sup>o</sup> 3P <sup>o</sup> 1	7s	(3/2) <sup>2</sup> F <sup>o</sup> 3/2 <sup>b</sup>		R1c		
9502.093(10)	10521.111(11)	9502.1498(21)	-0.057	10	4f	(5/2) <sup>2</sup> F <sup>o</sup> 5/2 <sup>b</sup>	6d	(5/2) <sup>2</sup> F <sup>o</sup> 7/2 <sup>b</sup>		R1c		X
9504.184(9)	10518.796(10)	9504.220(4)	-0.035	360	sp	( <sup>3</sup> P) <sup>3</sup> P <sup>o</sup> 1D <sup>+</sup> 2	5g	(3/2) <sup>2</sup> F <sup>o</sup> 7/2 <sup>b</sup>		R1c		X
9505.598(10)	10517.232(11)	9505.605(3)	-0.008	10	4f	(5/2) <sup>2</sup> F <sup>o</sup> 3/2 <sup>b</sup>	6d	(5/2) <sup>2</sup> F <sup>o</sup> 3/2 <sup>b</sup>		R1c		X
9510.299(19)	10512.033(21)	9510.298(7)	0.001	42	sp	( <sup>3</sup> P) <sup>3</sup> P <sup>o</sup> 5P <sup>o</sup> 2	6d	(3/2) <sup>2</sup> F <sup>o</sup> 3/2 <sup>b</sup>		R1c		
9512.762(8)	10509.864(9)	9512.2653(15)	-0.004	2900	5s	(3/2) <sup>2</sup> F <sup>o</sup> 3/2 <sup>b</sup>	5p	(5/2) <sup>2</sup> F <sup>o</sup> 5/2 <sup>b</sup>	1.3e+06	C	B00	
9515.588(11)	10506.190(12)	9515.595(3)	-0.007	210	4f	(5/2) <sup>2</sup> F <sup>o</sup> 7/2 <sup>b</sup>	6d	(5/2) <sup>2</sup> F <sup>o</sup> 5/2 <sup>b</sup>		R1c		
9527.379(10)	10493.188(11)	9527.376(4)	0.003	31	4f	(3/2) <sup>2</sup> F <sup>o</sup> 7/2 <sup>b</sup>	6d	(3/2) <sup>2</sup> F <sup>o</sup> 3/2 <sup>b</sup>		R1c		
9530.897(10)	10489.315(11)	9530.905(3)	-0.008	160	4f	(5/2) <sup>2</sup> F <sup>o</sup> 11/2 <sup>b</sup>	5d	(3/2) <sup>2</sup> F <sup>o</sup> 9/2 <sup>b</sup>		R1c		
9546.928(10)	10471.701(11)	9546.928(3)	-0.000	210	4f	(5/2) <sup>2</sup> F <sup>o</sup> 11/2 <sup>b</sup>	6d	(5/2) <sup>2</sup> F <sup>o</sup> 9/2 <sup>b</sup>		R1c		
9548.691(10)	10469.768(11)	9548.702(3)	-0.011	21	4f	(5/2) <sup>2</sup> F <sup>o</sup> 3/2 <sup>b</sup>	6d	(5/2) <sup>2</sup> F <sup>o</sup> 3/2 <sup>b</sup>		R1c		
9565.600(10)	10451.261(11)	9565.623(4)	-0.024	53	4f	(3/2) <sup>2</sup> F <sup>o</sup> 9/2 <sup>b</sup>	6d	(3/2) <sup>2</sup> F <sup>o</sup> 7/2 <sup>b</sup>		R1c		
9585.611(10)	10429.442(11)	9585.628(3)	-0.017	32	4f	(3/2) <sup>2</sup> F <sup>o</sup> 5/2 <sup>b</sup>	6s	(3/2) <sup>2</sup> F <sup>o</sup> 3/2 <sup>b</sup>		R1c		
9597.666(20)	10416.043(21)	9597.614(7)	0.052	11	sp	( <sup>3</sup> P) <sup>3</sup> P <sup>o</sup> 5P <sup>o</sup> 2	6s	(3/2) <sup>2</sup> F <sup>o</sup> 3/2 <sup>b</sup>		R1c		
9599.817(10)	10414.009(11)	9599.843(3)	-0.026	11	4f	(5/2) <sup>2</sup> F <sup>o</sup> 5/2 <sup>b</sup>	6d	(5/2) <sup>2</sup> F <sup>o</sup> 3/2 <sup>b</sup>		R1c		
9602.377(10)	10411.232(11)	9602.374(3)	0.003	22	4f	(3/2) <sup>2</sup> F <sup>o</sup> 7/2 <sup>b</sup>	6d	(3/2) <sup>2</sup> F <sup>o</sup> 3/2 <sup>b</sup>		R1c		
9605.15(9)	10408.22(10)	9605.075(6)	0.08	54	5d	(5/2) <sup>2</sup> F <sup>o</sup> 5/2 <sup>b</sup>	7p	(5/2) <sup>2</sup> F <sup>o</sup> 3/2 <sup>b</sup>		R1c		
9605.15(9)	10408.22(10)	9605.193(4)	-0.04	54	4f	(3/2) <sup>2</sup> F <sup>o</sup> 9/2 <sup>b</sup>	6d	(3/2) <sup>2</sup> F <sup>o</sup> 7/2 <sup>b</sup>		R1c		
9610.896(10)	10402.004(11)	9610.884(5)	0.012	430	5d	(5/2) <sup>2</sup> F <sup>o</sup> 7/2 <sup>b</sup>	5f	(3/2) <sup>2</sup> F <sup>o</sup> 3/2 <sup>b</sup>		R1c	TW	
9613.596(20)	10399.083(21)	9613.594(3)	0.002	65	4f	(5/2) <sup>2</sup> F <sup>o</sup> 9/2 <sup>b</sup>	6d	(5/2) <sup>2</sup> F <sup>o</sup> 7/2 <sup>b</sup>	5.9e+06	D+		
9630.420(10)	10380.916(11)	9630.428(3)	-0.009	11	4f	(3/2) <sup>2</sup> F <sup>o</sup> 7/2 <sup>b</sup>	6d	(3/2) <sup>2</sup> F <sup>o</sup> 5/2 <sup>b</sup>		R1c		

Table A1. Cont.

$\lambda_{\text{obs}}^a$ (Å)	$\sigma_{\text{obs}}^b$ (cm <sup>-1</sup> )	$\lambda_{\text{Ritz}}^c$ (Å)	$\Delta\lambda_{\text{obs-Ritz}}^d$ (Å)	$I_{\text{obs}}^d$ (arb. u.)	Char <sup>e</sup>	Lower Level	Upper Level	A (s <sup>-1</sup> )	Acc <sup>f</sup>	Line Ref. <sup>g</sup>	TP Ref. <sup>h</sup>	Notes <sup>h</sup>
9630.969(11)	10380.324(11)	9631.023(3)	-0.054	11	4f	(5/2) <sup>+</sup> 5/2 <sup>-</sup> 3	6d			Ric		X
9637.149(11)	10373.668(12)	9637.148(3)	0.000	1100	3p	( <sup>1</sup> F)P <sup>-</sup> 3D <sup>+</sup>	5g			Ric		
9646.751(10)	10363.342(11)	9646.770(3)	-0.019	22	4f	(5/2) <sup>+</sup> 7/2 <sup>-</sup> 4	6d			Ric		
9649.361(10)	10360.539(11)	9649.378(3)	-0.017	110	sp	( <sup>3</sup> F)P <sup>-</sup> 3D <sup>+</sup>	5g			Ric		X
9649.361(10)	10360.539(11)	9649.399(3)	-0.038	110	sp	( <sup>3</sup> F)P <sup>-</sup> 3D <sup>+</sup>	5g			Ric		X
9651.107(10)	10358.665(11)	9651.115(4)	-0.008	22	4f	(3/2) <sup>+</sup> 3/2 <sup>-</sup> 2	6d			Ric		
9657.363(11)	10351.954(11)	9657.369(4)	-0.005	22	4f	(5/2) <sup>+</sup> 1/2 <sup>-</sup> 1	6d			Ric		
9664.119(10)	10344.717(11)	9664.140(3)	-0.020	11	4f	(3/2) <sup>+</sup> 5/2 <sup>-</sup> 2	6d			Ric		
9670.167(10)	10338.248(11)	9670.172(8)	-0.006	11	6d	(5/2) <sup>+</sup> 9/2 <sup>-</sup> 4	5f			Ric		
9688.602(8)	10331.577(8)	9688.6189(13)	-0.017	1600	5s	(3/2) <sup>+</sup> 13/2 <sup>-</sup> 2	8p			Ric		
9715.855(20)	10289.633(21)	9715.789(3)	0.066	12	4f	(5/2) <sup>+</sup> 9/2 <sup>-</sup> 1	6d			Ric		X
9718.927(10)	10286.381(11)	9718.9263(24)	0.000	23	4f	(5/2) <sup>+</sup> 9/2 <sup>-</sup> 1	6d			Ric		
9732.121(21)	10272.435(22)	9732.1007(17)	0.021	1100	sp	( <sup>3</sup> F)P <sup>-</sup> 3C <sup>+</sup>	5g			Ric		
9732.148(13)	10272.407(13)	9732.1264(21)	0.022	1100	sp	( <sup>3</sup> F)P <sup>-</sup> 3C <sup>+</sup>	5g			Ric		
9734.473(10)	10269.953(11)	9734.488(3)	-0.015	24	4f	(5/2) <sup>+</sup> 7/2 <sup>-</sup> 4	6d			Ric		
9735.802(4)	10268.551(4)	9735.8031(20)	-0.001	6700	sp	( <sup>1</sup> F)P <sup>-</sup> 3C <sup>+</sup>	5g			F_Re		
		9781.688(5)			sp	( <sup>1</sup> F)P <sup>-</sup> 3D <sup>+</sup>	5g			Ric		
9781.844(13)	10220.219(13)	9781.880(4)	-0.037	120	4f	(3/2) <sup>+</sup> 7/2 <sup>-</sup> 3	6d			Ric		X
9792.465(10)	10209.134(11)	9792.4709(19)	-0.006	50	4f	(5/2) <sup>+</sup> 1/2 <sup>-</sup> 1	5g			Ric		
9794.085(10)	10207.445(10)	9794.067(3)	0.018	38	sp	( <sup>3</sup> F)P <sup>-</sup> 3D <sup>+</sup>	7s			Ric		
9813.2038(22)	10187.5583(23)	9813.2047(20)	-0.0009	8600	4f	(5/2) <sup>+</sup> 1/2 <sup>-</sup> 1	5g			F_Re		
9813.334(8)	10187.423(8)	9813.325(4)	0.009	2600	4f	(5/2) <sup>+</sup> 1/2 <sup>-</sup> 1	5g			Ric		
9817.398(9)	10183.206(9)	9817.3974(12)	0.001	240	4f	(5/2) <sup>+</sup> 1/2 <sup>-</sup> 1	5g			Ric		
9824.237(10)	10176.117(11)	9824.2394(9)	-0.002	100	4f	(5/2) <sup>+</sup> 11/2 <sup>-</sup> 6	5g			Ric		
9827.041(12)	10172.213(12)	9827.0477(21)	-0.006	78	4f	(5/2) <sup>+</sup> 11/2 <sup>-</sup> 6	5g			Ric		
9827.982(4)	10172.240(4)	9827.9787(7)	0.003	3200	4f	(5/2) <sup>+</sup> 11/2 <sup>-</sup> 6	5g			F_Re		
9828.973(10)	10171.214(10)	9828.9743(16)	-0.001	710	5p	(3/2) <sup>+</sup> 3/2 <sup>-</sup> 2	6s			Ric		
9830.795(4)	10169.329(4)	9830.7965(20)	-0.001	2700	4f	(5/2) <sup>+</sup> 11/2 <sup>-</sup> 6	5g			F_Re		
9835.299(10)	10164.672(11)	9835.299(3)	-0.001	100	4f	(3/2) <sup>+</sup> 3/2 <sup>-</sup> 2	5g			Ric		
9837.8361(21)	10162.065(22)	9837.8372(17)	-0.0011	10000	4f	(5/2) <sup>+</sup> 3/2 <sup>-</sup> 2	5g			F_Re		
9850.955(5)	10148.991(6)	9850.504(4)	-0.010	2400	4f	(5/2) <sup>+</sup> 1/2 <sup>-</sup> 0	5g			F_Re		
9858.723(7)	10140.521(8)	9858.7254(24)	-0.002	21000	4f	(5/2) <sup>+</sup> 1/2 <sup>-</sup> 0	5g			Ric		
9861.28027(17)	10137.89135(18)			19000	4f	(5/2) <sup>+</sup> 11/2 <sup>-</sup> 6	5g			Ric		
9864.13643(18)	10134.9593(22)			19000	4f	(5/2) <sup>+</sup> 11/2 <sup>-</sup> 6	5g			F_Re		
9868.0934(21)	10130.8920(19)			9100	4f	(3/2) <sup>+</sup> 3/2 <sup>-</sup> 2	5g			F_Re		
9870.8161(16)	10128.0981(7)			97	5s	(5/2) <sup>+</sup> 15/2 <sup>-</sup> 3	5p			Ric		
9878.465(8)	10120.255(9)	9878.193(5)	0.273	280	3p	( <sup>3</sup> F)P <sup>-</sup> 5S <sup>+</sup>	5p			Ric		X
9881.464(3)	10117.184(3)	9881.4639(15)	0.000	8400	4f	(5/2) <sup>+</sup> 7/2 <sup>-</sup> 3	5g			F_Re		
9883.730(9)	10114.864(9)	9883.7091(24)	0.021	560	4f	(3/2) <sup>+</sup> 9/2 <sup>-</sup> 1	5g			Ric		
9883.9672(10)	10114.6216(10)	9883.9674(10)	-0.0001	5100	4f	(5/2) <sup>+</sup> 9/2 <sup>-</sup> 1	5g			F_Re		
9884.996(11)	10113.569(11)	9884.989(4)	0.007	28	6p	(5/2) <sup>+</sup> 7/2 <sup>-</sup> 3	6d			Ric		
9892.939(4)	10105.448(4)	9892.940(4)	-0.000	4800	4f	(3/2) <sup>+</sup> 3/2 <sup>-</sup> 2	5g			F_Re		
9894.337(7)	10104.021(7)	9894.3443(14)	-0.007	5300	4f	(5/2) <sup>+</sup> 7/2 <sup>-</sup> 3	5g			Ric		

Table A1. Cont.

$\lambda_{\text{obs}}^a$ (Å)	$\sigma_{\text{obs}}^b$ (cm <sup>-1</sup> )	$\lambda_{\text{Ritz}}^c$ (Å)	$\Delta\lambda_{\text{obs-Ritz}}^d$ (Å)	$I_{\text{obs}}^d$ (arb. u.)	Char <sup>e</sup>	Lower Level	Upper Level	A (s <sup>-1</sup> )	Acc <sup>f</sup>	Line Ref. <sup>g</sup>	TP Ref. <sup>h</sup>	Notes <sup>b</sup>
9899.567(11)	10096.683(11)	9899.414(6)	0.153	57	?	( <sup>1</sup> S) <sup>o</sup> 3s <sup>2</sup> 5s <sup>2</sup>	(5/2) <sup>o</sup> 3/2(21)	3.7e+06	D+	Ric	TW	X
9905.136(23)	10095.005(24)	9905.091(3)	0.045	1800	4f	(5/2) <sup>o</sup> 3/2(1 <sup>o</sup> )	(5/2) <sup>o</sup> 3/2(21)	1.5e+07	D+	F,Re	TW	
9905.18(8)	10092.97(6)	9905.214(4)	-0.04	1800	*	(5/2) <sup>o</sup> 3/2(1 <sup>o</sup> )	(5/2) <sup>o</sup> 3/2(21)			Ric		
9911.988(12)	10086.028(12)	9911.986(3)	0.002	58	sp	( <sup>3</sup> F) <sup>o</sup> 3D <sup>o</sup> 7s	(3/2) <sup>o</sup> 3/2(21)			Ric		
9915.090(21)	10082.873(22)	9915.0672(18)	0.022	630	4f	(5/2) <sup>o</sup> 7/2(1 <sup>o</sup> )	(5/2) <sup>o</sup> 7/2(21)			Ric		
9915.090(21)	10082.873(22)	9915.1061(20)	-0.017	630	4f	(5/2) <sup>o</sup> 7/2(1 <sup>o</sup> )	(5/2) <sup>o</sup> 7/2(21)			Ric		
9916.417(13)	10081.523(3)	9916.4172(3)	-0.0001	15000	4f	(3/2) <sup>o</sup> 7/2(1 <sup>o</sup> )	(3/2) <sup>o</sup> 7/2(21)	6.6e+07	B	F,Re	TW	
9917.959(10)	10079.9642(10)	9917.9510(10)	-0.0001	9600	4f	(5/2) <sup>o</sup> 7/2(1 <sup>o</sup> )	(5/2) <sup>o</sup> 7/2(21)	3.8e+07	C+	F,Re	TW	
9925.5883(4)	10072.2080(4)	9925.5883(4)	-0.0000	13000	4f	(3/2) <sup>o</sup> 7/2(1 <sup>o</sup> )	(3/2) <sup>o</sup> 7/2(21)	6.5e+07	B	F,Re	TW	
9926.0209(15)	10071.690(16)	9926.0211(13)	-0.0002	4900	4f	(5/2) <sup>o</sup> 7/2(1 <sup>o</sup> )	(5/2) <sup>o</sup> 7/2(21)			F,Re		
9938.844(4)	10058.844(4)	9938.7730(16)	0.002	5300	4f	(5/2) <sup>o</sup> 5/2(1 <sup>o</sup> )	(5/2) <sup>o</sup> 5/2(21)	2.1e+07	C+	F,Re	TW	
9938.9960(6)	10058.6207(6)	9938.9960(6)	0.0000	11000	4f	(5/2) <sup>o</sup> 5/2(1 <sup>o</sup> )	(5/2) <sup>o</sup> 5/2(21)	4.4e+07	C+	F,Re	TW	
9948.895(11)	10048.612(11)	9948.8880(21)	0.007	61	4f	(5/2) <sup>o</sup> 5/2(1 <sup>o</sup> )	(5/2) <sup>o</sup> 5/2(21)			Ric		
9959.970(3)	10037.439(3)	9959.9679(18)	0.002	5800	4f	(5/2) <sup>o</sup> 5/2(1 <sup>o</sup> )	(5/2) <sup>o</sup> 5/2(21)	1.9e+07	C+	F,Re	TW	
9960.3485(8)	10037.0573(8)	9960.3485(8)	-0.0000	11000	4f	(3/2) <sup>o</sup> 5/2(1 <sup>o</sup> )	(3/2) <sup>o</sup> 5/2(21)	5.6e+07	B	F,Re	TW	
9981.3599(12)	10015.890(12)	9981.379(3)	0.020	130	4f	(5/2) <sup>o</sup> 5/2(1 <sup>o</sup> )	(5/2) <sup>o</sup> 5/2(21)	1.9e+06	D+	Ric	TW	
9994.027(11)	10003.234(11)	9994.019(3)	0.008	900	4f	(3/2) <sup>o</sup> 5/2(1 <sup>o</sup> )	(3/2) <sup>o</sup> 5/2(21)	9e+06	D+	Ric	TW	
10006.588(3)	9990.678(3)	10006.5881(24)	-0.001	8400	4f	(5/2) <sup>o</sup> 7/2(1 <sup>o</sup> )	(5/2) <sup>o</sup> 7/2(21)	4.9e+07	C+	F,Re	TW	
10022.9672(3)	9974.3510(3)	10022.9672(3)	-0.0000	20000	4f	(5/2) <sup>o</sup> 7/2(1 <sup>o</sup> )	(5/2) <sup>o</sup> 7/2(21)	4.9e+07	C+	F,Re	TW	
10026.894(4)	9970.445(4)	10026.8943(17)	-0.001	1500	4f	(5/2) <sup>o</sup> 7/2(1 <sup>o</sup> )	(5/2) <sup>o</sup> 7/2(21)	4.9e+07	B	F,Re	TW	
10036.224(3)	9961.176(3)	10036.2243(9)	-0.000	5700	4f	(5/2) <sup>o</sup> 7/2(1 <sup>o</sup> )	(5/2) <sup>o</sup> 7/2(21)			F,Re		
10038.0920(5)	9959.3223(5)	10038.0919(5)	0.001	14000	4f	(5/2) <sup>o</sup> 7/2(1 <sup>o</sup> )	(5/2) <sup>o</sup> 7/2(21)	1.64e+07	C+	F,Re	TW	
10040.499(13)	9956.9330(13)	10040.481(5)	0.017	560	4f	(3/2) <sup>o</sup> 7/2(1 <sup>o</sup> )	(3/2) <sup>o</sup> 7/2(21)	6.0e+07	B	F,Re	TW	
10049.773(12)	9947.746(12)	10049.7881(19)	-0.015	1200	4f	(3/2) <sup>o</sup> 7/2(1 <sup>o</sup> )	(3/2) <sup>o</sup> 7/2(21)	9e+06	D+	Ric	TW	
10051.0231(20)	9946.5092(20)	10051.0218(6)	0.0014	5100	4f	(5/2) <sup>o</sup> 7/2(1 <sup>o</sup> )	(5/2) <sup>o</sup> 7/2(21)	1.32e+07	C+	F,Re	TW	
10054.93572(22)	9942.63880(21)	10054.93573(22)	-0.00001	24000	4f	(5/2) <sup>o</sup> 7/2(1 <sup>o</sup> )	(5/2) <sup>o</sup> 7/2(21)	5.8e+07	B	F,Re	TW	
10057.609(11)	9939.996(11)	10057.6090(20)	-0.000	180	4f	(5/2) <sup>o</sup> 7/2(1 <sup>o</sup> )	(5/2) <sup>o</sup> 7/2(21)	1.7e+06	D+	Ric	TW	
10080.3499(10)	9917.5719(10)	10080.3499(10)	-0.0000	11000	4f	(5/2) <sup>o</sup> 7/2(1 <sup>o</sup> )	(5/2) <sup>o</sup> 7/2(21)	5.5e+07	B	F,Re	TW	
10092.14(3)	9902.99(3)	10092.1155(21)	0.02	990	4f	(3/2) <sup>o</sup> 7/2(1 <sup>o</sup> )	(3/2) <sup>o</sup> 7/2(21)	7.3e+06	D+	Ric	TW	
10092.14(3)	9905.99(3)	10092.151(3)	-0.01	990	4f	(3/2) <sup>o</sup> 7/2(1 <sup>o</sup> )	(3/2) <sup>o</sup> 7/2(21)	1.25e+07	C+	F,Re	TW	
10092.808(8)	9837.103(8)	10062.8099(18)	-0.001	3600	4f	(5/2) <sup>o</sup> 7/2(1 <sup>o</sup> )	(5/2) <sup>o</sup> 7/2(21)	4.4e+07	B	F,Re	TW	
10166.8202(21)	9833.2217(20)	10166.8192(16)	0.0010	18000	4f	(5/2) <sup>o</sup> 7/2(1 <sup>o</sup> )	(5/2) <sup>o</sup> 7/2(21)	4.4e+07	B	Ric	TW	
10176.433(12)	9823.933(12)	10176.4346(17)	-0.002	1700	4f	(5/2) <sup>o</sup> 7/2(1 <sup>o</sup> )	(5/2) <sup>o</sup> 7/2(21)			Ric		
10193.660(10)	9807.331(10)	10193.6484(21)	0.012	1100	5s	(5/2) <sup>o</sup> 7/2(1 <sup>o</sup> )	(5/2) <sup>o</sup> 7/2(21)			Ric		
10225.073(10)	9777.201(10)	10225.077(4)	-0.003	1700	6p	(5/2) <sup>o</sup> 7/2(1 <sup>o</sup> )	(5/2) <sup>o</sup> 7/2(21)			Ric		
10237.22(3)	9765.60(3)	10237.183(4)	0.03	120	6p	(5/2) <sup>o</sup> 7/2(1 <sup>o</sup> )	(5/2) <sup>o</sup> 7/2(21)			Ric		
10237.22(3)	9765.60(3)	10237.219(4)	-0.00	120	6p	( <sup>3</sup> F) <sup>o</sup> 3H <sup>o</sup> 2	(5/2) <sup>o</sup> 7/2(21)	1.9e+06	D+	Ric	TW	
10247.043(10)	9736.2394(9)	10247.038(4)	0.005	1300	sp	(3/2) <sup>o</sup> 7/2(21)	(5/2) <sup>o</sup> 7/2(21)			Ric		
10278.686(16)	9726.204(15)	10278.6604(14)	0.026	540	sp	( <sup>1</sup> G) <sup>o</sup> 3H <sup>o</sup> 4	(5/2) <sup>o</sup> 7/2(21)	1.17e+07	C+	Ric	TW	X
10297.40(3)	9708.53(3)	10297.147(5)	0.25	56	sp	( <sup>3</sup> F) <sup>o</sup> 3F <sup>o</sup> 3	(5/2) <sup>o</sup> 7/2(21)			Ric		
10343.469(10)	9665.287(9)	10343.472(3)	-0.003	6100	sp	( <sup>3</sup> F) <sup>o</sup> 3F <sup>o</sup> 3	(5/2) <sup>o</sup> 7/2(21)			Ric		
10357.603(10)	9652.098(9)	10357.586(3)	0.017	780	sp	( <sup>3</sup> F) <sup>o</sup> 3F <sup>o</sup> 3	(5/2) <sup>o</sup> 7/2(21)	4.8e+06	D+	Ric	TW	



Table A1. Cont.

$\lambda_{\text{obs}}^a$ (Å)	$\sigma_{\text{obs}}^b$ (cm <sup>-1</sup> )	$\lambda_{\text{ritz}}^c$ (Å)	$\Delta\lambda_{\text{obs-ritz}}^d$ (Å)	$I_{\text{obs}}^d$ (arb. u.)	Char <sup>e</sup>	Lower Level	Upper Level	A (s <sup>-1</sup> )	Acc <sup>f</sup>	Line Ref. <sup>g</sup>	TP Ref. <sup>h</sup>	Notes <sup>b</sup>
10380.323(21)	9630.972(20)	10380.297(3)	0.026	130	*	sp	(5/2) <sup>2</sup> 5/2 <sub>1/2</sub>	5g		Ric		
10380.323(21)	9630.972(20)	10380.340(3)	-0.016	130	*	sp	(3/2) <sup>2</sup> 5/2 <sub>1/2</sub>	5g		Ric		
10424.302(8)	9590.341(7)	10424.309(3)	-0.007	3700		5d	(5/2) <sup>2</sup> 11/2 <sub>1</sub>	5f	D+	F_Re	TW	
10465.012(7)	9543.000(7)	10465.004(4)	0.008	3800		5d	(5/2) <sup>2</sup> 11/2 <sub>1</sub>	5f	D+	F_Re	TW	
10465.012(7)	9552.438(10)	10465.665(4)	-0.002	4800		5d	(5/2) <sup>2</sup> 11/2 <sub>1</sub>	5f	D+	F_Re	TW	
10575.703(11)	9453.046(10)	10575.690(6)	0.013	180		6p	(5/2) <sup>2</sup> 15/2 <sub>1/2</sub>	6d	D+	Ric	TW	
10609.294(11)	9423.116(10)	10609.300(5)	-0.006	240		5d	(3/2) <sup>2</sup> 11/2 <sub>1</sub>	5f	D+	Ric	TW	
10624.895(12)	9409.280(11)	10624.901(4)	-0.007	96		sp	(3/2) <sup>2</sup> 3 <sup>1</sup> H <sub>1</sub>	5g		Ric		
10641.797(11)	9394.335(9)	10641.822(5)	-0.025	3600		5d	(3/2) <sup>2</sup> 11/2 <sub>1</sub>	5f	D+	F_Re	TW	
10742.332(8)	9306.416(7)	10742.339(23)	-0.007	4800		5d	(5/2) <sup>2</sup> 9/2 <sub>1/2</sub>	5f	D+	F_Re	TW	
10745.703(12)	9303.497(11)	10745.703(3)	-0.001	110		5d	(5/2) <sup>2</sup> 9/2 <sub>1/2</sub>	5f	D+	Ric		
10752.044(14)	9298.010(12)	10752.046(3)	-0.002	53		5d	(5/2) <sup>2</sup> 9/2 <sub>1/2</sub>	5f	D+	Ric		
10768.359(14)	9283.923(12)	10768.360(4)	-0.001	210		5d	(5/2) <sup>2</sup> 13/2 <sub>1/2</sub>	5f	D+	Ric	TW	
10787.828(10)	9267.168(9)	10787.827(3)	0.001	210		5d	(5/2) <sup>2</sup> 9/2 <sub>1/2</sub>	5f	D+	Ric	TW	
10791.529(10)	9263.990(9)	10791.519(3)	0.010	1400		5d	(5/2) <sup>2</sup> 9/2 <sub>1/2</sub>	5f	D+	Ric	TW	
10797.923(12)	9258.504(11)	10797.915(3)	0.008	160		5d	(5/2) <sup>2</sup> 9/2 <sub>1/2</sub>	5f	D+	Ric		
10800.96(3)	9255.90(3)	10800.928(3)	0.03	110	*	5d	(5/2) <sup>2</sup> 17/2 <sub>1/2</sub>	5f		Ric		
10800.985(12)	9255.879(10)	10800.972(7)	0.014	110	*	sp	(5/2) <sup>2</sup> 3 <sup>1</sup> D <sub>3</sub>	4d		F_Re		
10836.3452(6)	9225.6765(5)	10836.3453(6)	-0.0001	8300		5d	(5/2) <sup>2</sup> 19/2 <sub>1/2</sub>	5f	D+	F_Re	TW	
10849.473(3)	9214.514(5)	10849.477(3)	-0.004	6300		5d	(3/2) <sup>2</sup> 17/2 <sub>1/2</sub>	5f	D+	F_Re	TW	
10852.407(10)	9212.022(9)	10852.401(4)	0.007	2100		5d	(5/2) <sup>2</sup> 13/2 <sub>1/2</sub>	5f	D+	Ric	TW	
10865.050(17)	9201.303(15)	10865.010(5)	0.039	100		5d	(5/2) <sup>2</sup> 13/2 <sub>1/2</sub>	5f	D+	Ric		
10885.074(16)	9184.376(14)	10885.064(5)	0.008	200	*	sp	(3/2) <sup>2</sup> 3 <sup>1</sup> F <sub>3</sub>	6d		Ric		
10885.074(16)	9184.376(14)	10885.064(8)	0.010	200	*	sp	(3/2) <sup>2</sup> 3 <sup>1</sup> D <sub>1</sub>	6d		Ric		
10889.9718(12)	9180.2457(11)	10889.9720(12)	-0.0003	6800		5d	(5/2) <sup>2</sup> 19/2 <sub>1/2</sub>	5f	D+	F_Re	TW	
10904.886(9)	9167.691(7)	10904.902(5)	-0.016	2600		5d	(3/2) <sup>2</sup> 13/2 <sub>1/2</sub>	5f	D+	F_Re	TW	
10925.167(13)	9150.672(11)	10925.155(4)	0.012	97		5d	(3/2) <sup>2</sup> 17/2 <sub>1/2</sub>	5f	D+	Ric	TW	
10929.791(10)	9146.800(9)	10929.799(4)	-0.008	480		5d	(5/2) <sup>2</sup> 13/2 <sub>1/2</sub>	5f	D+	Ric	TW	
10930.9327(21)	9145.8452(17)	10930.9342(19)	-0.0015	5300		5d	(3/2) <sup>2</sup> 17/2 <sub>1/2</sub>	5f	D+	F_Re	TW	
10959.809(11)	9121.748(6)	10959.819(5)	-0.010	4600		5d	(3/2) <sup>2</sup> 13/2 <sub>1/2</sub>	5f	D+	Ric	TW	
10964.502(11)	9117.844(9)	10964.527(5)	-0.025	3200		5d	(3/2) <sup>2</sup> 13/2 <sub>1/2</sub>	5f	D+	Ric	TW	
10966.532(11)	9116.156(9)	10966.524(5)	0.008	900		5d	(5/2) <sup>2</sup> 13/2 <sub>1/2</sub>	5f	D+	Ric	TW	
10973.938(5)	9110.004(4)	10973.944(3)	-0.006	3100		5d	(5/2) <sup>2</sup> 15/2 <sub>1/2</sub>	5f	D+	F_Re	TW	
10980.553(5)	9104.516(4)	10980.559(3)	-0.006	4700		5d	(5/2) <sup>2</sup> 15/2 <sub>1/2</sub>	5f	D+	F_Re	TW	
10983.677(10)	9101.926(8)	10983.675(3)	0.002	1600		5d	(5/2) <sup>2</sup> 15/2 <sub>1/2</sub>	5f	D+	F_Re	TW	
11008.410(12)	9081.477(10)	11008.408(4)	0.002	3300		sp	(3/2) <sup>2</sup> 3 <sup>1</sup> D <sub>3</sub>	7s	D+	Ric	TW	
11009.932(6)	9080.221(5)	11009.932(4)	-0.000	3200		5d	(3/2) <sup>2</sup> 13/2 <sub>1/2</sub>	5f	D+	F_Re	TW	
11027.380(13)	9065.854(11)	11027.388(3)	-0.008	190		5d	(3/2) <sup>2</sup> 15/2 <sub>1/2</sub>	5f	D+	Ric	TW	
11035.792(10)	9058.792(8)	11035.978(4)	-0.002	2700		5d	(5/2) <sup>2</sup> 15/2 <sub>1/2</sub>	5f	D+	Ric	TW	
11098.345(11)	9007.885(9)	11098.352(3)	-0.006	150		5d	(5/2) <sup>2</sup> 15/2 <sub>1/2</sub>	5f	D+	Ric	TW	
11100.523(11)	9006.118(9)	11100.529(5)	-0.006	150		5d	(3/2) <sup>2</sup> 13/2 <sub>1/2</sub>	5f	D+	Ric	TW	
11114.771(5)	8994.573(4)	11114.773(3)	-0.001	2500		5d	(5/2) <sup>2</sup> 17/2 <sub>1/2</sub>	5f	D+	F_Re	TW	

Table A1. Cont.

$\lambda_{\text{obs}}^a$ (Å)	$\sigma_{\text{obs}}^b$ (cm <sup>-1</sup> )	$\lambda_{\text{Ritz}}^c$ (Å)	$\Delta\lambda_{\text{obs-Ritz}}^d$ (Å)	Char <sup>e</sup>	Lower Level	Upper Level	A (s <sup>-1</sup> )	Acc <sup>f</sup>	Line Ref. <sup>g</sup>	TP Ref. <sup>h</sup>	Notes <sup>h</sup>
11121.559(10)	8989.083(8)	11121.558(3)	0.001		5d	(5/2) <sup>3</sup> [7/2] <sub>3</sub> 5f	(5/2) <sup>3</sup> [7/2] <sub>3</sub> 4	9.e+06	E	Ric	TW
11123.1488(20)	8987.7987(16)	11123.1487(18)	0.0001		5d	(5/2) <sup>3</sup> [7/2] <sub>3</sub> 5f	(5/2) <sup>3</sup> [9/2] <sub>3</sub> 5	3.3e+07	D+	F,Re	TW
11124.761(11)	8986.496(9)	11124.755(4)	0.006		5d	(5/2) <sup>3</sup> [7/2] <sub>3</sub> 5f	(5/2) <sup>3</sup> [7/2] <sub>3</sub> 3	1.2e+07	D+	Ric	TW
11125.451(5)	8985.939(4)	11125.454(4)	-0.003		5d	(3/2) <sup>3</sup> [5/2] <sub>1</sub> 5f	(3/2) <sup>3</sup> [7/2] <sub>3</sub> 4	3.5e+07	D+	F,Re	TW
11126.754(11)	8984.886(9)	11126.756(3)	-0.001		5d	(5/2) <sup>3</sup> [7/2] <sub>3</sub> 5f	(5/2) <sup>3</sup> [9/2] <sub>3</sub> 4	4.5e+06	D+	Ric	TW
11133.556(12)	8979.397(9)	11133.556(3)	0.000		5d	(5/2) <sup>3</sup> [7/2] <sub>3</sub> 5f	(5/2) <sup>3</sup> [7/2] <sub>3</sub> 4	9.e+06	D+	Ric	TW
11141.872(21)	8972.695(17)	11141.845(5)	0.027		9p	(3/2) <sup>3</sup> [3/2] <sub>1</sub> 7s	(3/2) <sup>3</sup> [3/2] <sub>1</sub> 2			Ric	
11156.494(10)	8960.935(8)	11156.492(5)	0.002		5d	(3/2) <sup>3</sup> [5/2] <sub>1</sub> 5f	(3/2) <sup>3</sup> [7/2] <sub>3</sub> 3	3.2e+07	D+	Ric	TW
11173.078(11)	8947.635(8)	11173.081(4)	-0.003		5d	(5/2) <sup>3</sup> [5/2] <sub>1</sub> 5f	(5/2) <sup>3</sup> [7/2] <sub>3</sub> 3	2.2e+07	D+	F,Re	TW
11180.070(13)	8942.039(11)	11180.072(4)	-0.002		5d	(3/2) <sup>3</sup> [5/2] <sub>1</sub> 5f	(3/2) <sup>3</sup> [5/2] <sub>1</sub> 3	1.0e+07	D+	Ric	TW
11190.534(13)	8933.663(11)	11190.534(4)	0.018		5d	(5/2) <sup>3</sup> [7/2] <sub>3</sub> 5f	(5/2) <sup>3</sup> [5/2] <sub>1</sub> 3	2.0e+06	D+	Ric	TW
11202.751(12)	8923.935(9)	11202.717(5)	0.034		5d	(3/2) <sup>3</sup> [5/2] <sub>1</sub> 5f	(3/2) <sup>3</sup> [5/2] <sub>1</sub> 3	1.1e+07	D+	Ric	TW
11208.490(13)	8919.366(11)	11208.425(5)	0.065		5d	(5/2) <sup>3</sup> [5/2] <sub>1</sub> 5f	(5/2) <sup>3</sup> [5/2] <sub>1</sub> 3	1.2e+06	D+	Ric	TW X
11218.324(11)	8911.547(9)	11218.317(4)	0.007		5d	(5/2) <sup>3</sup> [5/2] <sub>1</sub> 5f	(5/2) <sup>3</sup> [5/2] <sub>1</sub> 2	1.6e+07	D+	Ric	TW
11227.209(11)	8904.495(9)	11227.208(4)	0.000		5d	(5/2) <sup>3</sup> [5/2] <sub>1</sub> 5f	(5/2) <sup>3</sup> [5/2] <sub>1</sub> 3	5.4e+06	D+	Ric	TW
23063.7	4335.82	23063.701(9)		:	4s	<sup>3</sup> D <sub>2</sub> 4s	<sup>1</sup> D <sub>2</sub> 2.0e-01	C+	C+		TW,G64 M1
29261.7	3417.43	29261.733(10)		:	4s	<sup>3</sup> D <sub>2</sub> 4s	<sup>1</sup> D <sub>2</sub> 1.55e-02	C+	C+		TW,G64 M1
44127.2	2266.18	44127.15(3)		:	4s	<sup>3</sup> D <sub>1</sub> 4s	<sup>1</sup> D <sub>2</sub> 2.7e-02	C+	C+		TW,G64 M1
48317.6	2069.639	48317.60(4)		:	4s	<sup>3</sup> D <sub>1</sub> 4s	<sup>3</sup> D <sub>1</sub> 9.e-08	E	E		TW E2
86861.8	1151.254	86861.79(7)		:	4s	<sup>3</sup> D <sub>2</sub> 4s	<sup>3</sup> D <sub>1</sub> 5.6e-02	C+	C+		TW,G64 M1
108887	918.385	108886.80(16)		:	4s	<sup>3</sup> D <sub>3</sub> 4s	<sup>3</sup> D <sub>2</sub> 1.8e-02	C+	C+		TW,G64 M1

<sup>a</sup> Observed wavelength between 2000 Å and 20000 Å is given in standard air; outside of this region, it is in vacuum. The standard uncertainty in the last decimal place is given in parentheses after the value. Conversion from air to vacuum was made using the five-parameter formula from Peck and Reeder [38];

<sup>b</sup> Observed wavenumber in vacuum;

<sup>c</sup> Ritz wavelength and its uncertainty were obtained in the least-squares level optimization procedure using the LOPT code [39]. For lines that alone determine one of the energy levels of the transition, this column is blank;

<sup>d</sup> Observed intensities from different experiments have been normalized to a uniform scale (see text). They are proportional to the energy flux under the line profile and have uncertainties of a factor of three on average. Intensities of parity-forbidden transitions are given on a different scale, since most of them were observed only in nebulas;

<sup>e</sup> Line character code: b—blended line; p—perturbed by a close line; \*—the given intensity value is shared by two or more transitions; n—masked by another strong line (no wavelength measurement available)—the value given in the observed wavelength column is a rounded Ritz wavelength (no wavelength measurement available); ?—questionable identification;

<sup>f</sup> Transition probability accuracy code: A+—transition probability uncertainty is likely ≤2%; B—≤7%; C—≤18%; D—≤25%; E—≤50%;

<sup>g</sup> Key to observed wavelength and transition probability references: A73—Aller et al. [4]; A08—Andersson et al. [40]; B00—Blomont et al. [41]; B09—Brown et al. [42]; C84—Cederquist et al. [43]; C94—Crespo Lopez-Urrutia et al. [44]; D05—Dong and Fritzsche [45]; G64—Garstang [46]; H71—Hefferlin et al. [47]; K66—Kaufman and Ward [15]; K82—Kono and Hattori [48]; M97—McKeena et al. [5]; N88—Neger and Jäger [49]; O07—Ortiz et al. [50]; P84—Prior [37]; P97—Pinnington et al. [51]; R1—Ross [2]; R2—Ross [16]; S36—Shenstone [1]; T53—Thackeray [3]; W93—Wagatsuma and Hirokawa [36]; F—this work, FITS measurements with Cu/Ge/Pt/Ar hollow cathode; F, Re—this work, measurements with Cu/Re/Ar hollow cathode; TW—this work, grating measurements. Lower-case letters after the reference have the following meaning: c—corrected in this work; n—new identification; r—revised identification; cal—calculated A-value; se—A-value was semiempirically adjusted by ratio of observed and calculated lifetime;

<sup>h</sup> Notes: X—excluded from level-optimization procedure; L—lasing line; M1—magnetic-dipole transition; E2—electric-quadrupole transition; HF—hyperfine-induced transition.

Table A2. Energy levels of Cu II.

Label <sup>a</sup>	Configuration	Term	J	Level <sup>b</sup> , cm <sup>-1</sup>	Unc. <sup>c</sup> , cm <sup>-1</sup>	Landé g <sup>d</sup>	Leading Percentages <sup>e</sup>	Note <sup>f</sup>	N <sub>lines</sub> <sup>g</sup>
d <sup>10</sup>	3d <sup>10</sup>	1S	0	0.000	0.0017		97% + 2% 4d <sup>1</sup> S		15
4s	3d <sup>9</sup> 4s	3D	3	21928.7326	0.0014	1.32		98%	59
4s	3d <sup>9</sup> 4s	3D	2	22847.1176	—	1.16	89% + 9% 4s <sup>1</sup> D		77
4s	3d <sup>9</sup> 4s	3D	1	23998.3718	0.0009	0.48	98%		48
4s	3d <sup>9</sup> 4s	1D	1	26264.5502	0.0012	1.00	89% + 9% 4s <sup>3</sup> D		64
4p	3d <sup>9</sup> 4p	3P <sup>o</sup>	2	66418.6849	0.0014	1.49	96% + 2% 4p <sup>3</sup> D <sup>o</sup>		31
4p	3d <sup>9</sup> 4p	3P <sup>o</sup>	1	67916.5572	0.0011	1.49	95% + 2% 4p <sup>1</sup> P <sup>o</sup>		42
4p	3d <sup>9</sup> 4p	3F <sup>o</sup>	3	68447.7349	0.0013	1.06	62% + 34% 4p <sup>1</sup> F <sup>o</sup>		32
4p	3d <sup>9</sup> 4p	3F <sup>o</sup>	4	68730.8876	0.0017	1.23	98%		23
4p	3d <sup>9</sup> 4p	3P <sup>o</sup>	0	68850.2628	0.0014		98%		12
s <sup>2</sup>	3d <sup>8</sup> 4s <sup>2</sup>	3F	4	69704.7015	0.0019		95% + 4% p <sup>2</sup> (F)S <sup>3</sup> F		32
4p	3d <sup>9</sup> 4p	3F <sup>o</sup>	4	69867.9849	0.0011	0.67	88% + 6% 4p <sup>3</sup> D <sup>o</sup>		37
4p	3d <sup>9</sup> 4p	1F <sup>o</sup>	3	70841.4669	0.0014		49% + 31% 4p <sup>3</sup> D <sup>o</sup> + 17% 4p <sup>3</sup> F <sup>o</sup>		40
4p	3d <sup>9</sup> 4p	1D <sup>o</sup>	2	71493.8548	0.0007	1.08	54% + 35% 4p <sup>3</sup> D <sup>o</sup> + 9% 4p <sup>3</sup> F <sup>o</sup>		36
s <sup>2</sup>	3d <sup>8</sup> 4s <sup>2</sup>	3F	3	71531.542	0.0003		95% + 4% p <sup>2</sup> (F)S <sup>3</sup> F		57
4p	3d <sup>9</sup> 4p	3D <sup>o</sup>	3	71920.0961	0.0008		64% + 19% 4p <sup>3</sup> F <sup>o</sup> + 15% 4p <sup>1</sup> F <sup>o</sup>		36
s <sup>2</sup>	3d <sup>8</sup> 4s <sup>2</sup>	3F	2	72723.817	0.004		94% + 4% p <sup>2</sup> (F)S <sup>3</sup> F		52
4p	3d <sup>9</sup> 4p	3D <sup>o</sup>	1	73102.0408	0.0007	0.47	92% + 3% 4p <sup>1</sup> P <sup>o</sup>		31
4p	3d <sup>9</sup> 4p	3D <sup>o</sup>	2	73353.2957	0.0008	0.99	54% + 41% 4p <sup>1</sup> D <sup>o</sup>		39
4p	3d <sup>9</sup> 4p	1P <sup>o</sup>	1	73595.8143	0.0018	1.04	93% + 4% 4p <sup>3</sup> D <sup>o</sup>		36
s <sup>2</sup>	3d <sup>8</sup> 4s <sup>2</sup>	1D	2	85388.772	0.003		73% + 21% s <sup>2</sup> 3P		49
s <sup>2</sup>	3d <sup>8</sup> 4s <sup>2</sup>	3P	2	88362.001	0.003		74% + 21% s <sup>2</sup> 1D		44
s <sup>2</sup>	3d <sup>8</sup> 4s <sup>2</sup>	3P	1	88605.096	0.004		95% + 4% p <sup>2</sup> (P)S <sup>3</sup> P		38
s <sup>2</sup>	3d <sup>8</sup> 4s <sup>2</sup>	3P	0	88926.002	0.003		95% + 4% p <sup>2</sup> (P)S <sup>3</sup> P		17
s <sup>2</sup>	3d <sup>8</sup> 4s <sup>2</sup>	1G	4	95565.619	0.003	0.98	95% + 4% p <sup>2</sup> (G)S <sup>1</sup> G		18
sp	3d <sup>8</sup> ( <sup>3</sup> P) <sup>4</sup> s4p( <sup>3</sup> P <sup>o</sup> )	5D <sup>o</sup>	4	107942.795	0.010		93% + 4% sp ( <sup>3</sup> P) <sup>3</sup> P <sup>o</sup> 5D <sup>o</sup>		2
5s	(5/2) <sup>2</sup> [5/2]	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )5s	2[5/2]	108014.8372	0.0012		100%		48
5s	(5/2) <sup>2</sup> [5/2]	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )5s	2[5/2]	108355.6078	0.0012		98% + 2% 5s (3/2) <sup>2</sup> [3/2]		48
sp	( <sup>3</sup> F) <sup>3</sup> P <sup>o</sup> 5D <sup>o</sup>	5D <sup>o</sup>	3	109276.015	0.006		91% + 4% sp ( <sup>3</sup> P) <sup>3</sup> P <sup>o</sup> 5D <sup>o</sup>		8
5s	(3/2) <sup>2</sup> [3/2]	3d <sup>8</sup> ( <sup>3</sup> D <sub>3/2</sub> )5s	2[3/2]	110084.4773	0.0011		100%		34
sp	( <sup>3</sup> F) <sup>3</sup> P <sup>o</sup> 5D <sup>o</sup>	5D <sup>o</sup>	2	110363.725	0.008		91% + 5% sp ( <sup>3</sup> P) <sup>3</sup> P <sup>o</sup> 5D <sup>o</sup>		4
5s	(3/2) <sup>2</sup> [3/2]	3d <sup>8</sup> ( <sup>2</sup> D <sub>3/2</sub> )5s	2[3/2]	110366.1542	0.0011		98% + 2% 5s (5/2) <sup>2</sup> [5/2]		47
sp	( <sup>3</sup> F) <sup>3</sup> P <sup>o</sup> 5G <sup>o</sup>	5G <sup>o</sup>	5	110631.196	0.009		82% + 13% sp ( <sup>3</sup> F) <sup>3</sup> P <sup>o</sup> 5F <sup>o</sup>		1
sp	( <sup>3</sup> F) <sup>3</sup> P <sup>o</sup> 5D <sup>o</sup>	5D <sup>o</sup>	1	111124.39	0.14		93% + 5% sp ( <sup>3</sup> P) <sup>3</sup> P <sup>o</sup> 5D <sup>o</sup>		1
sp	( <sup>3</sup> F) <sup>3</sup> P <sup>o</sup> 5G <sup>o</sup>	5G <sup>o</sup>	4	111218.705	0.008		83% + 10% sp ( <sup>3</sup> F) <sup>3</sup> P <sup>o</sup> 5F <sup>o</sup> + 5% sp ( <sup>3</sup> F) <sup>3</sup> P <sup>o</sup> 3G <sup>o</sup>		2
sp	( <sup>3</sup> F) <sup>3</sup> P <sup>o</sup> 5G <sup>o</sup>	5G <sup>o</sup>	3	111876.412	0.008		89% + 7% sp ( <sup>3</sup> F) <sup>3</sup> P <sup>o</sup> 3F <sup>o</sup>		3
sp	( <sup>3</sup> F) <sup>3</sup> P <sup>o</sup> 5F <sup>o</sup>	5F <sup>o</sup>	5	112401.632	0.022		86% + 12% sp ( <sup>3</sup> F) <sup>3</sup> P <sup>o</sup> 5G <sup>o</sup>		1
sp	( <sup>3</sup> F) <sup>3</sup> P <sup>o</sup> 5C <sup>o</sup>	5C <sup>o</sup>	2	112424.679	0.023		95% + 3% sp ( <sup>3</sup> F) <sup>3</sup> P <sup>o</sup> 5F <sup>o</sup>		2
sp	( <sup>3</sup> F) <sup>3</sup> P <sup>o</sup> 5F <sup>o</sup>	5F <sup>o</sup>	4	113302.823	0.026		84% + 9% sp ( <sup>3</sup> F) <sup>3</sup> P <sup>o</sup> 5G <sup>o</sup>		5
sp	( <sup>3</sup> F) <sup>3</sup> P <sup>o</sup> 5F <sup>o</sup>	5F <sup>o</sup>	3	114000.452	0.007		86% + 7% sp ( <sup>3</sup> F) <sup>3</sup> P <sup>o</sup> 3C <sup>o</sup>		5

Table A2. Cont.

Label <sup>a</sup>	Configuration	Term	<i>J</i>	Level <sup>b</sup> , cm <sup>-1</sup>	Unc. <sup>c</sup> , cm <sup>-1</sup>	Landé <sup>d</sup> , g <sup>d</sup>	Leading Percentages <sup>e</sup>	Note <sup>f</sup>	<i>N</i> <sub>lines</sub> <sup>g</sup>
sp	3d <sup>8</sup> ( <sup>3</sup> F)4s4p( <sup>3</sup> P <sup>o</sup> )	5P <sup>o</sup>	2	114481.674	0.006		92% + 3% sp ( <sup>3</sup> F) <sup>3</sup> P <sup>o</sup> 3C <sup>o</sup>		6
4d	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )4d	2 <sup>1</sup> [1/2]	1	114511.2386	0.0012		91% + 7% 4d (3/2) <sup>2</sup> [1/2] + 1% 4d2		39
sp	3d <sup>8</sup> ( <sup>3</sup> F)4s4p( <sup>3</sup> P <sup>o</sup> )	5P <sup>o</sup>	1	114755.953	0.011		97%		3
sp	3d <sup>8</sup> ( <sup>3</sup> F)4s4p( <sup>1</sup> P <sup>o</sup> )	3G <sup>o</sup>	5	115359.532	0.005		71% + 20% sp ( <sup>3</sup> F) <sup>3</sup> P <sup>o</sup> 1C <sup>o</sup> + 6% sp ( <sup>3</sup> F) <sup>3</sup> P <sup>o</sup> 5C <sup>o</sup>		7
sp	3d <sup>8</sup> ( <sup>3</sup> F)4s4p( <sup>3</sup> P <sup>o</sup> )	3G <sup>o</sup>	4	115546.114	0.011		93% + 6% sp ( <sup>3</sup> F) <sup>3</sup> P <sup>o</sup> 3C <sup>o</sup>		1
4d	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )4d	2 <sup>1</sup> [9/2]	5	115568.99497	0.0012		99%		22
4d	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )4d	2 <sup>3</sup> [2]	2	115638.8036	0.0011		93% + 4% 4d (5/2) <sup>2</sup> [5/2] + 2% 4d (3/2) <sup>2</sup> [3/2]		42
4d	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )4d	2 <sup>1</sup> [9/2]	4	115662.5622	0.0014		97% + 1% 4d (5/2) <sup>2</sup> [7/2]		32
4d	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )4d	2 <sup>3</sup> [2]	4	115665.1539	0.0011		97% + 1% 4d (3/2) <sup>2</sup> [1/2] + 1% 4d (3/2) <sup>2</sup> [3/2]		30
4d	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )4d	2 <sup>1</sup> [5/2]	3	116080.2237	0.0010		97% + 1% 4d (5/2) <sup>2</sup> [7/2] + 1% 4d (3/2) <sup>2</sup> [5/2]		35
4d	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )4d	2 <sup>1</sup> [7/2]	3	116325.9148	0.0011		95% + 4% 4d (3/2) <sup>2</sup> [7/2] + 1% 4d (5/2) <sup>2</sup> [5/2]		37
4d	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )4d	2 <sup>1</sup> [7/2]	4	116371.18040	0.0011		95% + 2% 4d (3/2) <sup>2</sup> [7/2] + 1% 4d (5/2) <sup>2</sup> [9/2]		35
sp	3d <sup>8</sup> ( <sup>3</sup> F)4s4p( <sup>3</sup> P <sup>o</sup> )	3D <sup>o</sup>	3	116375.406	0.003		44% + 35% sp ( <sup>3</sup> F) <sup>3</sup> P <sup>o</sup> 3C <sup>o</sup> + 13% sp ( <sup>3</sup> F) <sup>3</sup> P <sup>o</sup> 3P <sup>o</sup>		17
4d	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )4d	2 <sup>1</sup> [5/2]	2	116387.7873	0.0010		92% + 3% 4d (3/2) <sup>2</sup> [3/2] + 3% 4d (5/2) <sup>2</sup> [3/2]		43
4d	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )4d	2 <sup>1</sup> [1/2]	0	116576.5758	0.0018		53% + 45% 4d (3/2) <sup>2</sup> [1/2]		16
sp	3d <sup>8</sup> ( <sup>3</sup> F)4s4p( <sup>3</sup> P <sup>o</sup> )	3G <sup>o</sup>	3	116643.960	0.003		57% + 36% sp ( <sup>3</sup> F) <sup>3</sup> P <sup>o</sup> 3D <sup>o</sup>		17
sp	3d <sup>8</sup> ( <sup>3</sup> F)4s4p( <sup>1</sup> P <sup>o</sup> )	3D <sup>o</sup>	2	117130.340	0.003		75% + 10% sp ( <sup>3</sup> F) <sup>3</sup> P <sup>o</sup> 3P <sup>o</sup>		27
4d	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )4d	2 <sup>1</sup> [1/2]	1	117231.4014	0.0019		91% + 7% 4d (5/2) <sup>2</sup> [1/2]		28
sp	3d <sup>8</sup> ( <sup>3</sup> F)4s4p( <sup>3</sup> P <sup>o</sup> )	3P <sup>o</sup>	4	117666.626	0.005		88% + 3% sp ( <sup>3</sup> F) <sup>3</sup> P <sup>o</sup> 3P <sup>o</sup>		15
4d	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )4d	2 <sup>1</sup> [7/2]	3	117747.3504	0.0015		95% + 4% 4d (5/2) <sup>2</sup> [7/2]		37
4d	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )4d	2 <sup>1</sup> [7/2]	4	117883.0985	0.0013		96% + 2% 4d (5/2) <sup>2</sup> [7/2]		35
4d	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )4d	2 <sup>3</sup> [2]	1	117928.2197	0.0018		98%		31
sp	3d <sup>8</sup> ( <sup>3</sup> F)4s4p( <sup>3</sup> P <sup>o</sup> )	3D <sup>o</sup>	1	118071.302	0.003		87% + 6% sp ( <sup>1</sup> D) <sup>3</sup> P <sup>o</sup> 3D <sup>o</sup>		22
sp	3d <sup>8</sup> ( <sup>3</sup> F)4s4p( <sup>3</sup> P <sup>o</sup> )	3P <sup>o</sup>	3	118142.950	0.003		63% + 14% sp ( <sup>3</sup> F) <sup>3</sup> P <sup>o</sup> 1P <sup>o</sup> + 10% sp ( <sup>3</sup> F) <sup>3</sup> P <sup>o</sup> 3D <sup>o</sup>		42
4d	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )4d	2 <sup>3</sup> [2]	2	118163.2663	0.0015		82% + 12% 4d (3/2) <sup>2</sup> [5/2] + 2% 4d (5/2) <sup>2</sup> [5/2]		32
4d	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )4d	2 <sup>1</sup> [5/2]	3	118483.8135	0.0015		98% + 1% 4d (5/2) <sup>2</sup> [5/2]		37
4d	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )4d	2 <sup>1</sup> [5/2]	2	118531.9058	0.0016		86% + 12% 4d (3/2) <sup>2</sup> [3/2] + 1% 4d (5/2) <sup>2</sup> [3/2]		35
sp	3d <sup>8</sup> ( <sup>3</sup> F)4s4p( <sup>1</sup> P <sup>o</sup> )	1G <sup>o</sup>	4	118991.330	0.007		75% + 20% sp ( <sup>3</sup> F) <sup>3</sup> P <sup>o</sup> 3G <sup>o</sup>		9
sp	3d <sup>8</sup> ( <sup>3</sup> F)4s4p( <sup>3</sup> P <sup>o</sup> )	3P <sup>o</sup>	2	119039.6355	0.0019		82% + 8% sp ( <sup>3</sup> F) <sup>3</sup> P <sup>o</sup> 3P <sup>o</sup>		34
5p	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )5p	2 <sup>3</sup> [2] <sup>o</sup>	2	120092.3828	0.0012		96% + 2% sp + 1% 5p (3/2) <sup>2</sup> [3/2] <sup>o</sup>		40
5p	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )5p	2 <sup>1</sup> [7/2] <sup>o</sup>	3	120684.7128	0.0013		86% + 13% sp		33
5p	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )5p	2 <sup>1</sup> [7/2] <sup>o</sup>	4	120789.80865	0.0013		95% + 4% sp		20
5p	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )5p	2 <sup>1</sup> [5/2] <sup>o</sup>	2	120876.0141	0.0015		51% + 41% sp + 3% 5p (3/2) <sup>2</sup> [3/2] <sup>o</sup>		41
5p	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )5p	2 <sup>3</sup> [2] <sup>o</sup>	1	120919.5715	0.0012		83% + 15% 5p (3/2) <sup>2</sup> [1/2] <sup>o</sup> + 1% sp		43
5p	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )5p	2 <sup>1</sup> [5/2] <sup>o</sup>	3	121079.1501	0.0012		54% + 35% sp + 3% 5p (3/2) <sup>2</sup> [5/2] <sup>o</sup>		45
sp	3d <sup>8</sup> ( <sup>3</sup> F)4s4p( <sup>3</sup> P <sup>o</sup> )	1P <sup>o</sup>	3	121524.8509	0.0014		39% + 43% 5p 3D <sup>o</sup> + 6% sp ( <sup>3</sup> F) <sup>3</sup> P <sup>o</sup> 3P <sup>o</sup>		37
sp	3d <sup>8</sup> ( <sup>3</sup> F)4s4p( <sup>1</sup> P <sup>o</sup> )	1D <sup>o</sup>	2	121981.8546	0.0015		36% + 32% 5p 3D <sup>o</sup> + 22% 5p 3P <sup>o</sup>	cd	44
5p	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )5p	2 <sup>1</sup> [1/2] <sup>o</sup>	0	122224.0199	0.0020		99%		13
4d	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )4d	2 <sup>1</sup> [1/2]	0	122415.957	0.0013		45% + 34% 4d (5/2) <sup>2</sup> [1/2] + 10% 5d (5/2) <sup>2</sup> [1/2]		12
5p	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )5p	2 <sup>1</sup> [5/2] <sup>o</sup>	2	122745.9491	0.0013		85% + 4% 5p (3/2) <sup>2</sup> [3/2] <sup>o</sup> + 4% 5p (5/2) <sup>2</sup> [5/2] <sup>o</sup>		39

Table A2. Cont.

Label <sup>a</sup>	Configuration	Term	<i>J</i>	Level <sup>b</sup> , cm <sup>-1</sup>	Unc. <sup>c</sup> , cm <sup>-1</sup>	Landé <sup>d</sup> <i>g<sup>d</sup></i>	Leading Percentages <sup>e</sup>	Note <sup>f</sup>	<i>N<sub>lines</sub></i> <sup>g</sup>
5p	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> ) <sup>5</sup> p	2[1/2] <sup>o</sup>	1	122867.4707	0.0015		75% + 14% 5p (5/2) <sup>3</sup> (3/2) <sup>1</sup> + 9% 5p (3/2) <sup>2</sup> (3/2) <sup>o</sup>		39
5p	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> ) <sup>5</sup> p	2[5/2] <sup>o</sup>	3	123016.8175	0.0014		91% + 7% sp + 1% 5p (5/2) <sup>2</sup> (7/2) <sup>o</sup>		27
5p	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> ) <sup>5</sup> p	2[3/2] <sup>o</sup>	1	123304.823	0.003		86% + 9% 5p (3/2) <sup>2</sup> (1/2) <sup>1</sup> + 4% sp		27
5p	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> ) <sup>5</sup> p	3[2/2] <sup>o</sup>	1	123530.061	0.0016		76% + 13% sp + 3% 5p (5/2) <sup>1</sup> (5/2) <sup>o</sup>		43
5p	3d <sup>8</sup> ( <sup>3</sup> P) <sup>4</sup> s4p(3p <sup>o</sup> )	5p <sup>o</sup>	3	125326.8261	0.017		88% + 8% sp (1D) <sup>3</sup> p <sup>o</sup> 3D <sup>o</sup>		6
5p	3d <sup>8</sup> ( <sup>3</sup> P) <sup>4</sup> s4p(3p <sup>o</sup> )	5p <sup>o</sup>	2	125248.121	0.008		88% + 3% sp (1D) <sup>3</sup> p <sup>o</sup> 3p <sup>o</sup>		11
5p	3d <sup>8</sup> ( <sup>3</sup> P) <sup>4</sup> s4p(3p <sup>o</sup> )	5p <sup>o</sup>	1	125569.33	0.04		94% + 2% sp (1D) <sup>3</sup> p <sup>o</sup> 3p <sup>o</sup>		5
5p	3d <sup>8</sup> (1D) <sup>4</sup> s4p(3p <sup>o</sup> )	3p <sup>o</sup>	2	128365.736	0.006		69% + 15% sp (1D) <sup>3</sup> p <sup>o</sup> 3D <sup>o</sup>		10
5p	3d <sup>8</sup> (1D) <sup>4</sup> s4p(3p <sup>o</sup> )	3p <sup>o</sup>	3	128559.314	0.008		68% + 11% sp (3P) <sup>3</sup> p <sup>o</sup> 5D <sup>o</sup> + 9% sp (1D) <sup>3</sup> p <sup>o</sup> 3D <sup>o</sup>		6
5p	3d <sup>8</sup> (1D) <sup>4</sup> s4p(3p <sup>o</sup> )	3D <sup>o</sup>	1	128569.150	0.008		66% + 9% sp (1D) <sup>3</sup> p <sup>o</sup> 3p <sup>o</sup> + 9% sp (3P) <sup>3</sup> p <sup>o</sup> 3p <sup>o</sup>		7
5p	3d <sup>8</sup> (1D) <sup>4</sup> s4p(3p <sup>o</sup> )	3p <sup>o</sup>	4	128778.037	0.017		64% + 28% sp (3P) <sup>3</sup> p <sup>o</sup> 5D <sup>o</sup>		2
5p	3d <sup>8</sup> (1D) <sup>4</sup> s4p(3p <sup>o</sup> )	3D <sup>o</sup>	2	128854.036	0.008		59% + 19% sp (1D) <sup>3</sup> p <sup>o</sup> 3p <sup>o</sup>		8
5s <sup>2</sup>	3d <sup>8</sup> 4s <sup>2</sup>	1s	0	128910.03	0.06		94% + 5% p <sup>2</sup> (s) <sup>1</sup> s <sup>1</sup>	N	1
5p	3d <sup>8</sup> (1D) <sup>4</sup> s4p(3p <sup>o</sup> )	3p <sup>o</sup>	0	129105.778	0.009		63% + 32% sp (3P) <sup>3</sup> p <sup>o</sup> 3p <sup>o</sup>		3
5p	3d <sup>8</sup> (1D) <sup>4</sup> s4p(3p <sup>o</sup> )	3D <sup>o</sup>	3	129116.774	0.011		69% + 10% sp (1D) <sup>3</sup> p <sup>o</sup> 3p <sup>o</sup> + 7% sp (3P) <sup>3</sup> p <sup>o</sup> 5p <sup>o</sup>		6
5p	3d <sup>8</sup> (1D) <sup>4</sup> s4p(3p <sup>o</sup> )	3p <sup>o</sup>	1	129759.750	0.006		56% + 19% sp (1D) <sup>3</sup> p <sup>o</sup> 3D <sup>o</sup> + 18% sp (3P) <sup>3</sup> p <sup>o</sup> 3p <sup>o</sup>		9
5p	3d <sup>8</sup> (1D) <sup>4</sup> s4p(3p <sup>o</sup> )	3p <sup>o</sup>	2	130386.404	0.016		74% + 12% sp (3P) <sup>3</sup> p <sup>o</sup> 3p <sup>o</sup> + 8% sp (1D) <sup>3</sup> p <sup>o</sup> 3D <sup>o</sup>		8
5p	3d <sup>8</sup> ( <sup>3</sup> P) <sup>4</sup> s4p(3p <sup>o</sup> )	5D <sup>o</sup>	1	130940.488	0.008		91% + 5% sp (3P) <sup>3</sup> p <sup>o</sup> 5D <sup>o</sup>		8
5p	3d <sup>8</sup> ( <sup>3</sup> P) <sup>4</sup> s4p(3p <sup>o</sup> )	5D <sup>o</sup>	2	130943.661	0.009		88% + 5% sp (3P) <sup>3</sup> p <sup>o</sup> 5D <sup>o</sup>		9
5p	3d <sup>8</sup> ( <sup>3</sup> P) <sup>4</sup> s4p(3p <sup>o</sup> )	5D <sup>o</sup>	0	130953.558	0.016		91% + 6% sp (3P) <sup>3</sup> p <sup>o</sup> 5D <sup>o</sup>		2
5p	3d <sup>8</sup> ( <sup>3</sup> P) <sup>4</sup> s4p(3p <sup>o</sup> )	5D <sup>o</sup>	3	131044.310	0.008		81% + 11% sp (1D) <sup>3</sup> p <sup>o</sup> 3p <sup>o</sup>	N	10
5p	3d <sup>8</sup> ( <sup>3</sup> P) <sup>4</sup> s4p(3p <sup>o</sup> )	5D <sup>o</sup>	4	131312.426	0.013		66% + 25% sp (1D) <sup>3</sup> p <sup>o</sup> 3p <sup>o</sup> + 5% sp (1G) <sup>3</sup> p <sup>o</sup> 3p <sup>o</sup>		5
6s	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> ) <sup>6</sup> s	2[5/2]	3	133594.2323	0.0013		100%		27
6s	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> ) <sup>6</sup> s	2[5/2]	2	133728.0387	0.0013		100%		29
5p	3d <sup>8</sup> ( <sup>3</sup> P) <sup>4</sup> s4p(3p <sup>o</sup> )	3p <sup>o</sup>	2	133825.927	0.004		55% + 22% sp (3P) <sup>3</sup> p <sup>o</sup> 3D <sup>o</sup> + 9% sp (1D) <sup>3</sup> p <sup>o</sup> 3p <sup>o</sup>		13
5p	3d <sup>8</sup> ( <sup>3</sup> P) <sup>4</sup> s4p(3p <sup>o</sup> )	3D <sup>o</sup>	3	133984.325	0.004		47% + 31% sp (3F) <sup>3</sup> p <sup>o</sup> 3D <sup>o</sup> + 6% sp (1D) <sup>3</sup> p <sup>o</sup> 3D <sup>o</sup>		14
5p	3d <sup>8</sup> ( <sup>3</sup> P) <sup>4</sup> s4p(1p <sup>o</sup> )	3G <sup>o</sup>	5	134110.870	0.004		93% + 2% 4f <sup>3</sup> G <sup>o</sup>		9
5p	3d <sup>8</sup> ( <sup>3</sup> P) <sup>4</sup> s4p(3p <sup>o</sup> )	3D <sup>o</sup>	1	134359.847	0.003		52% + 24% sp (3P) <sup>3</sup> p <sup>o</sup> 3p <sup>o</sup> + 10% sp (1D) <sup>3</sup> p <sup>o</sup> 3p <sup>o</sup>		16
5p	3d <sup>8</sup> ( <sup>3</sup> P) <sup>4</sup> s4p(3p <sup>o</sup> )	3p <sup>o</sup>	2	134675.522	0.003		50% + 22% sp (3P) <sup>3</sup> p <sup>o</sup> 3p <sup>o</sup> + 7% sp (3F) <sup>3</sup> p <sup>o</sup> 3D <sup>o</sup>		18
5p	3d <sup>8</sup> ( <sup>3</sup> P) <sup>4</sup> s4p(1p <sup>o</sup> )	3p <sup>o</sup>	4	134742.863	0.003		50% + 31% sp (3F) <sup>3</sup> p <sup>o</sup> 3G <sup>o</sup> + 7% sp (1G) <sup>3</sup> p <sup>o</sup> 3p <sup>o</sup>	cd	13
5p	3d <sup>8</sup> ( <sup>3</sup> P) <sup>4</sup> s4p(3p <sup>o</sup> )	3p <sup>o</sup>	1	135135.168	0.003		38% + 32% sp (3P) <sup>3</sup> p <sup>o</sup> 3D <sup>o</sup> + 14% sp (1D) <sup>3</sup> p <sup>o</sup> 3p <sup>o</sup>		10
5p	3d <sup>8</sup> ( <sup>3</sup> P) <sup>4</sup> s4p(3p <sup>o</sup> )	3p <sup>o</sup>	0	135484.575	0.004		60% + 31% sp (1D) <sup>3</sup> p <sup>o</sup> 3p <sup>o</sup> + 5% 4f <sup>3</sup> p <sup>o</sup>		6
6s	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> ) <sup>6</sup> s	2[3/2]	1	135664.0204	0.0015		100%		21
5p	3d <sup>8</sup> ( <sup>3</sup> P) <sup>4</sup> s4p(1p <sup>o</sup> )	3D <sup>o</sup>	3	135733.433	0.003		26% sp (3P) <sup>3</sup> p <sup>o</sup> 3D <sup>o</sup> + 14% sp (3F) <sup>3</sup> p <sup>o</sup> 3p <sup>o</sup> + 13% sp (3F) <sup>1</sup> p <sup>o</sup> 3D <sup>o</sup>		20
6s	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> ) <sup>6</sup> s	2[3/2]	3	135760.1548	0.0016		99%		27
4f	3d <sup>8</sup> ( <sup>3</sup> P) <sup>4</sup> s4p(1p <sup>o</sup> )	3G <sup>o</sup>	4	135834.6720	0.0019		49% + 22% sp (3F) <sup>3</sup> p <sup>o</sup> 3p <sup>o</sup> + 9% 4f <sup>3</sup> G <sup>o</sup>		17
4f	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> ) <sup>7</sup> f	2[1/2] <sup>o</sup>	1	135863.6857	0.0016		97% + 2% sp + 1% 4f (5/2) <sup>2</sup> (3/2) <sup>1</sup>		19
4f	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> ) <sup>7</sup> f	2[1/2] <sup>o</sup>	0	135902.1365	0.0023		94% + 4% sp		8
4f	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> ) <sup>7</sup> f	2[3/2] <sup>o</sup>	2	135910.7245	0.0011		94% + 4% 4f (5/2) <sup>2</sup> (5/2) <sup>1</sup> + 2% sp		23

Table A2. Cont.

Label <sup>a</sup>	Configuration	Term	J	Level <sup>b</sup> , cm <sup>-1</sup>	Unc. <sup>c</sup> , cm <sup>-1</sup>	Landé <sup>d</sup> g <sup>d</sup>	Leading Percentages <sup>e</sup>	Note <sup>f</sup>	N <sub>lines</sub> <sup>g</sup>
4f	(5/2) <sup>3</sup> [11/2] <sup>o</sup>	2[11/2] <sup>o</sup>	6	135931.01412	0.0012		99% + 1% sp		5
4f	(5/2) <sup>2</sup> D <sub>3/2</sub> Hf	2[11/2] <sup>o</sup>	5	135933.89499	0.0019		98% + 1% sp		11
sp	3d <sup>8</sup> ( <sup>3</sup> P) <sup>3</sup> S <sup>o</sup>	5S <sup>o</sup>	2	135952.279	0.005		83% + 4% 4f <sup>1</sup> D <sup>o</sup>		12
4f	(5/2) <sup>2</sup> [1/2] <sup>o</sup>	2[3/2] <sup>o</sup>	1	135958.1919	0.0016		97% + 2% sp + 1% 4f(5/2) <sup>2</sup> [1/2] <sup>o</sup>		20
4f	(5/2) <sup>2</sup> [7/2] <sup>o</sup>	2[7/2] <sup>o</sup>	3	135989.9176	0.0012		41% + 37% sp + 11% 4f(5/2) <sup>2</sup> [5/2] <sup>o</sup>		33
4f	(5/2) <sup>2</sup> [5/2] <sup>o</sup>	2[5/2] <sup>o</sup>	2	136013.9671	0.0011		84% + 9% sp + 5% 4f(5/2) <sup>2</sup> [3/2] <sup>o</sup>		17
4f	(5/2) <sup>2</sup> [5/2] <sup>o</sup>	2[5/2] <sup>o</sup>	3	136035.3328	0.0010		86% + 11% 4f(5/2) <sup>2</sup> [7/2] <sup>o</sup> + 3% sp		28
4f	(5/2) <sup>2</sup> [7/2] <sup>o</sup>	2[7/2] <sup>o</sup>	4	136132.77781	0.0010		88% + 8% 4f(5/2) <sup>2</sup> [9/2] <sup>o</sup> + 3% sp		26
4f	(5/2) <sup>2</sup> [9/2] <sup>o</sup>	2[9/2] <sup>o</sup>	5	136160.61825	0.0011		98% + 2% sp		14
4f	(5/2) <sup>2</sup> [9/2] <sup>o</sup>	2[9/2] <sup>o</sup>	4	136269.9996	0.0014		75% + 14% sp + 9% 4f(5/2) <sup>2</sup> [7/2] <sup>o</sup>		20
5d	(5/2) <sup>2</sup> [1/2] <sup>o</sup>	2[1/2] <sup>o</sup>	1	136336.8971	0.0020		98% + 1% 5d(3/2) <sup>2</sup> [1/2] <sup>o</sup>		17
sp	( <sup>1</sup> G) <sup>3</sup> P <sup>o</sup> 3F <sup>o</sup>	3F <sup>o</sup>	3	136441.817	0.003		97% + 25% sp( <sup>3</sup> F) <sup>1</sup> P <sup>o</sup> 3G <sup>o</sup> + 11% sp( <sup>1</sup> G) <sup>3</sup> P <sup>o</sup> 3F <sup>o</sup>		21
sp	( <sup>1</sup> G) <sup>3</sup> P <sup>o</sup> 3H <sup>o</sup>	3H <sup>o</sup>	4	136441.817	0.003		97%		10
5d	(5/2) <sup>2</sup> [9/2] <sup>o</sup>	2[9/2] <sup>o</sup>	5	136725.85349	0.0013		100%		14
5d	(5/2) <sup>2</sup> [9/2] <sup>o</sup>	2[9/2] <sup>o</sup>	2	136754.1104	0.0018		97% + 2% 5d(5/2) <sup>2</sup> [5/2] <sup>o</sup>		25
5d	(5/2) <sup>2</sup> [9/2] <sup>o</sup>	2[9/2] <sup>o</sup>	4	136765.3514	0.0018		99%		20
5d	(5/2) <sup>2</sup> [3/2] <sup>o</sup>	2[3/2] <sup>o</sup>	1	136773.1713	0.0021		99%		19
sp	( <sup>3</sup> F) <sup>3</sup> P <sup>o</sup> 3D <sup>o</sup>	3D <sup>o</sup>	2	136800.137	0.003		41% + 18% sp( <sup>3</sup> P) <sup>3</sup> P <sup>o</sup> 1D <sup>o</sup> + 14% 6p		14
5d	(5/2) <sup>2</sup> [5/2] <sup>o</sup>	2[5/2] <sup>o</sup>	3	136919.3511	0.0014		99% + 1% 5d(5/2) <sup>2</sup> [7/2] <sup>o</sup>		36
5d	(5/2) <sup>2</sup> [7/2] <sup>o</sup>	2[7/2] <sup>o</sup>	3	137034.778	0.003		99% + 1% 5d(5/2) <sup>2</sup> [5/2] <sup>o</sup> + 1% 5d(3/2) <sup>2</sup> [7/2] <sup>o</sup>		23
5d	(5/2) <sup>2</sup> [7/2] <sup>o</sup>	2[7/2] <sup>o</sup>	4	137044.4647	0.0017		99%		22
5d	(5/2) <sup>2</sup> [5/2] <sup>o</sup>	2[5/2] <sup>o</sup>	2	137073.6465	0.0019		97% + 2% 5d(5/2) <sup>2</sup> [3/2] <sup>o</sup>		24
sp	( <sup>1</sup> G) <sup>3</sup> P <sup>o</sup> 3G <sup>o</sup>	3G <sup>o</sup>	3	137078.190	0.005		52% + 19% sp( <sup>3</sup> F) <sup>1</sup> P <sup>o</sup> 3F <sup>o</sup> + 14% sp( <sup>1</sup> G) <sup>3</sup> P <sup>o</sup> 3F <sup>o</sup>		7
sp	( <sup>1</sup> G) <sup>3</sup> P <sup>o</sup> 3H <sup>o</sup>	3H <sup>o</sup>	5	137082.175	0.005		96% + 2% 4f1H <sup>o</sup>		6
sp	( <sup>1</sup> G) <sup>3</sup> P <sup>o</sup> 3F <sup>o</sup>	3F <sup>o</sup>	2	137212.779	0.004		36% + 36% sp( <sup>3</sup> F) <sup>1</sup> P <sup>o</sup> 3F <sup>o</sup> + 14% sp( <sup>3</sup> P) <sup>3</sup> P <sup>o</sup> 1D <sup>o</sup>	RJ	12
sp	( <sup>3</sup> P) <sup>3</sup> P <sup>o</sup> 1P <sup>o</sup>	1P <sup>o</sup>	0	137242.914	0.008		82% + 5% sp( <sup>3</sup> P) <sup>3</sup> P <sup>o</sup> 3P <sup>o</sup>	N	6
5d	(5/2) <sup>2</sup> [1/2] <sup>o</sup>	2[1/2] <sup>o</sup>	1	137614.140	0.004		60% + 37% 5d(3/2) <sup>2</sup> [1/2] <sup>o</sup> + 1% 6d(5/2) <sup>2</sup> [1/2] <sup>o</sup>		7
sp	( <sup>3</sup> P) <sup>3</sup> P <sup>o</sup> 1D <sup>o</sup>	1D <sup>o</sup>	2	137648.800	0.004		50% + 9% sp( <sup>3</sup> P) <sup>3</sup> P <sup>o</sup> 3D <sup>o</sup> + 9% sp( <sup>3</sup> F) <sup>1</sup> P <sup>o</sup> 3D <sup>o</sup>		15
sp	( <sup>1</sup> G) <sup>3</sup> P <sup>o</sup> 3D <sup>o</sup>	3D <sup>o</sup>	1	137913.450	0.004		28% + 16% 4f <sup>1</sup> D <sup>o</sup> + 16% 4f		13
sp	( <sup>1</sup> G) <sup>3</sup> P <sup>o</sup> 3F <sup>o</sup>	3F <sup>o</sup>	4	137938.904	0.007		49% + 39% 6p <sup>3</sup> F <sup>o</sup> + 5% sp( <sup>3</sup> F) <sup>1</sup> P <sup>o</sup> 3F <sup>o</sup>	cd	6
4f	(3/2) <sup>2</sup> [3/2] <sup>o</sup>	2[3/2] <sup>o</sup>	2	138002.8856	0.0023		94% + 3% sp + 2% 4f(3/2) <sup>2</sup> [5/2] <sup>o</sup>		10
4f	(3/2) <sup>2</sup> [3/2] <sup>o</sup>	2[3/2] <sup>o</sup>	1	138028.384	0.003		59% + 26% sp + 10% 6p		14
4f	(3/2) <sup>2</sup> [9/2] <sup>o</sup>	2[9/2] <sup>o</sup>	5	138064.2971	0.0021		99% + 1% sp		10
4f	(3/2) <sup>2</sup> [9/2] <sup>o</sup>	2[9/2] <sup>o</sup>	4	138073.5826	0.0022		98% + 1% sp		10
4f	(3/2) <sup>2</sup> [5/2] <sup>o</sup>	2[5/2] <sup>o</sup>	3	138130.5345	0.0015		97% + 1% 4f(3/2) <sup>2</sup> [7/2] <sup>o</sup>		17
4f	(3/2) <sup>2</sup> [5/2] <sup>o</sup>	2[5/2] <sup>o</sup>	2	138176.8797	0.0018		89% + 7% sp + 1% 4f(3/2) <sup>2</sup> [3/2] <sup>o</sup>		17
4f	(3/2) <sup>2</sup> [7/2] <sup>o</sup>	2[7/2] <sup>o</sup>	4	138219.8605	0.0015		98%		12
4f	(3/2) <sup>2</sup> [7/2] <sup>o</sup>	2[7/2] <sup>o</sup>	3	138261.5822	0.0017		93% + 1% sp + 1% 4f(3/2) <sup>2</sup> [5/2] <sup>o</sup>		19
6p	(5/2) <sup>2</sup> [7/2] <sup>o</sup>	2[7/2] <sup>o</sup>	3	138401.956	0.003		62% + 29% sp + 2% 6p(5/2) <sup>2</sup> [5/2] <sup>o</sup>		21
sp	( <sup>3</sup> P) <sup>3</sup> S <sup>o</sup>	3S <sup>o</sup>	1	138516.49	0.03		97%	N	5

Table A2. Cont.

Label <sup>a</sup>	Configuration	Term	<i>J</i>	Level <i>b</i> , cm <sup>-1</sup>	Unc. <i>c</i> , cm <sup>-1</sup>	Landé <i>g</i> <sup>d</sup>	Leading Percentages <sup>e</sup>	Note <i>f</i>	<i>N</i> <sub>lines</sub> <sup>g</sup>
5d	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )5d	2 <sup>1</sup> /2 <sup>1</sup>	1	138593.046	0.003		98% + 1% 5d (5/2) <sup>2</sup> [1/2]		17
6p	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )6p	2 <sup>3</sup> /2 <sup>1</sup>	2	138745.817	0.005		91% + 4% sp + 3% 6p (5/2) <sup>2</sup> [5/2] <sup>o</sup>		14
5d	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )5d	2 <sup>1</sup> /2 <sup>1</sup>	3	138819.0637	0.0019		99% + 1% 5d (5/2) <sup>2</sup> [7/2]		15
5d	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )5d	2 <sup>1</sup> /2 <sup>1</sup>	4	138882.8921	0.0019		99%		15
5d	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )5d	2 <sup>3</sup> /2 <sup>1</sup>	1	138898.334	0.003		99%		18
5d	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )5d	2 <sup>3</sup> /2 <sup>1</sup>	2	138981.246	0.003		97% + 2% 5d (3/2) <sup>2</sup> [5/2] + 1% 5d (5/2) <sup>2</sup> [3/2]		19
6p	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )6p	2 <sup>5</sup> /2 <sup>1</sup>	2	139028.705	0.005		41% + 40% sp + 11% 6p (3/2) <sup>2</sup> [5/2] <sup>o</sup>		11
5d	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )5d	2 <sup>5</sup> /2 <sup>1</sup>	3	139119.4295	0.003		100%		18
5d	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )5d	2 <sup>3</sup> /2 <sup>1</sup>	3	139241.130	0.003		97% + 2% 5d (3/2) <sup>2</sup> [3/2]		24
6p	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )6p	2 <sup>3</sup> /2 <sup>1</sup>	1	139241.130	0.005		73% + 7% 6p (3/2) <sup>2</sup> [3/2] <sup>o</sup> + 4% 6p (3/2) <sup>2</sup> [1/2] <sup>o</sup>		21
sp	3d <sup>8</sup> ( <sup>1</sup> G <sub>3/2</sub> sp( <sup>2</sup> P <sup>o</sup> ))	3 <sup>1</sup> F <sup>o</sup>	3	139331.149	0.003		21% + 46% 6p <sup>1</sup> F <sup>o</sup> + 15% 6p <sup>3</sup> D <sup>o</sup>	cd	23
6p	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )6p	2 <sup>7</sup> /2 <sup>1</sup>	4	139395.786	0.004		59% + 37% sp		11
6p	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )6p	3 <sup>1</sup> F <sup>o</sup>	4	139710.491	0.004		19% + 42% 6p <sup>1</sup> D <sup>o</sup> + 15% sp ( <sup>1</sup> G <sub>3</sub> <sup>o</sup> 3 <sup>1</sup> F <sup>o</sup> )		15
sp	3d <sup>8</sup> ( <sup>3</sup> F)4sp( <sup>1</sup> P <sup>o</sup> )	3 <sup>1</sup> F <sup>o</sup>	3	139741.097	0.003		59% + 31% sp + 4% 6p (5/2) <sup>2</sup> [7/2] <sup>o</sup>		18
6p	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )6p	2 <sup>1</sup> /2 <sup>1</sup>	0	140589.344	0.006		47% + 20% 6d (5/2) <sup>2</sup> [1/2] + 17% 5d (5/2) <sup>2</sup> [1/2]		4
5d	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )5d	2 <sup>1</sup> /2 <sup>1</sup>	1	140981.510	0.005		94% + 3% 6p (5/2) <sup>2</sup> [3/2] <sup>o</sup> + 2% sp		8
6p	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )6p	2 <sup>5</sup> /2 <sup>1</sup>	3	141202.628	0.006		89% + 8% sp		12
6p	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )6p	2 <sup>5</sup> /2 <sup>1</sup>	2	141244.556	0.006		62% + 22% sp + 13% 6p (3/2) <sup>2</sup> [3/2] <sup>o</sup>	ci	9
6p	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )6p	2 <sup>3</sup> /2 <sup>1</sup>	2	141542.001	0.005		73% + 13% 6p (3/2) <sup>2</sup> [5/2] <sup>o</sup> + 10% sp		13
6p	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )6p	2 <sup>3</sup> /2 <sup>1</sup>	1	141734.175	0.005		79% + 16% sp + 1% 5p	ci	10
sp	3d <sup>8</sup> ( <sup>1</sup> G <sub>3/2</sub> sp( <sup>1</sup> P <sup>o</sup> ))	3 <sup>3</sup> G <sup>o</sup>	3	143423.319	0.020		99%	N	4
7s	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )7s	2 <sup>5</sup> /2 <sup>1</sup>	3	144814.9118	0.0014		100%		26
7s	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )7s	2 <sup>5</sup> /2 <sup>1</sup>	2	144882.9859	0.0016		100%		26
5f	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )5f	2 <sup>1</sup> /2 <sup>1</sup>	0	145889.334	0.004		100%		6
5f	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )5f	2 <sup>1</sup> /2 <sup>1</sup>	1	145900.904	0.003		84% + 16% 5f (5/2) <sup>2</sup> [3/2] <sup>o</sup>		10
5f	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )5f	2 <sup>3</sup> /2 <sup>1</sup>	2	145927.231	0.003		100%		13
5f	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )5f	2 <sup>1</sup> /2 <sup>1</sup>	5	145945.5969	0.0019		100%		5
5f	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )5f	2 <sup>1</sup> /2 <sup>1</sup>	6	145951.5299	0.0014		100%		2
5f	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )5f	2 <sup>3</sup> /2 <sup>1</sup>	1	145955.447	0.004		84% + 16% 5f (5/2) <sup>2</sup> [1/2] <sup>o</sup>		10
5f	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )5f	2 <sup>5</sup> /2 <sup>1</sup>	3	145978.142	0.003		98% + 2% 5f (5/2) <sup>2</sup> [7/2] <sup>o</sup>		12
5f	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )5f	2 <sup>5</sup> /2 <sup>1</sup>	2	145985.199	0.003		100%		12
5f	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )5f	2 <sup>7</sup> /2 <sup>1</sup>	3	146021.279	0.003		98% + 2% 5f (5/2) <sup>2</sup> [5/2] <sup>o</sup>		13
5f	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )5f	2 <sup>7</sup> /2 <sup>1</sup>	4	146023.862	0.003		86% + 14% 5f (5/2) <sup>2</sup> [9/2] <sup>o</sup>		13
5f	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )5f	2 <sup>9</sup> /2 <sup>1</sup>	4	146029.350	0.003		86% + 14% 5f (5/2) <sup>2</sup> [7/2] <sup>o</sup>		13
5f	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )5f	2 <sup>9</sup> /2 <sup>1</sup>	5	146032.2635	0.0021		100%		7
5f	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )5f	2 <sup>3</sup> /2 <sup>1</sup>	1	146051.118	0.004		100%		5
5g	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )5g	2 <sup>3</sup> /2 <sup>1</sup>	2	146051.2431	0.003		100%		4
5g	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )5g	2 <sup>1</sup> /2 <sup>1</sup>	6	146068.85092	0.0019		100%		1
5g	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )5g	2 <sup>1</sup> /2 <sup>1</sup>	7	146068.90547	0.0012		100%		1
5g	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )5g	2 <sup>5</sup> /2 <sup>1</sup>	3	146072.7739	0.0020		100%		5
5g	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )5g	2 <sup>5</sup> /2 <sup>1</sup>	2	146072.8134	0.0018		100%		6

Table A2. Cont.

Label <sup>a</sup>	Configuration	Term	J	Level <sup>b</sup> , cm <sup>-1</sup>	Unc. c, cm <sup>-1</sup>	Landé g <sup>d</sup>	Leading Percentages <sup>e</sup>	Note f	N <sub>lines</sub> <sup>g</sup>
5g	(5/2) <sup>2</sup> [7/2]	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )5g	2[7/2]	146093.9312	0.0014		100%		5
5g	(5/2) <sup>2</sup> [7/2]	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )5g	2[7/2]	146093.9535	0.0012		100%		2
5g	(5/2) <sup>2</sup> [11/2]	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )5g	2[11/2]	146103.2223	0.0018		100%		7
5g	(5/2) <sup>2</sup> [11/2]	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )5g	2[11/2]	146103.25704	0.0011		100%		3
5g	(5/2) <sup>2</sup> [9/2]	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )5g	2[9/2]	146107.1016	0.0016		100%		7
5g	(5/2) <sup>2</sup> [9/2]	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )5g	2[9/2]	146107.1288	0.0010		100%		6
6d	(5/2) <sup>2</sup> [1/2]	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )6d	2[1/2]	146215.634	0.004		98% + 1% 6d (5/2) <sup>2</sup> [3/2]		7
6d	(5/2) <sup>2</sup> [9/2]	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )6d	2[9/2]	146402.715	0.004		100%		8
6d	(5/2) <sup>2</sup> [3/2]	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )6d	2[3/2]	146415.599	0.003		97% + 2% 6d (5/2) <sup>2</sup> [5/2]		12
6d	(5/2) <sup>2</sup> [9/2]	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )6d	2[9/2]	146423.201	0.003		100%		10
6d	(5/2) <sup>2</sup> [1/2]	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )6d	2[1/2]	146427.948	0.003		99% + 1% 6d (5/2) <sup>2</sup> [1/2]		12
6d	(5/2) <sup>2</sup> [5/2]	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )6d	2[5/2]	146496.100	0.003		99% + 1% 6d (5/2) <sup>2</sup> [7/2]		16
6d	(5/2) <sup>2</sup> [7/2]	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )6d	2[7/2]	146556.381	0.003		99% + 1% 6d (5/2) <sup>2</sup> [5/2]		19
6d	(5/2) <sup>2</sup> [7/2]	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )6d	2[7/2]	146559.703	0.003		100%		14
6d	(5/2) <sup>2</sup> [1/2]	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )6d	2[1/2]	146575.101	0.0021		97% + 2% 6d (5/2) <sup>2</sup> [3/2] + 1% 7s (3/2) <sup>2</sup> [3/2]		23
7s	(3/2) <sup>2</sup> [3/2]	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )7s	2[3/2]	146886.1667	0.0021		100%		20
7s	(3/2) <sup>2</sup> [3/2]	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )7s	2[3/2]	146936.3180	0.0018		99%		24
6d	(5/2) <sup>2</sup> [1/2]	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )6d	2[1/2]	147097.835	0.005		60% + 29% 6d (3/2) <sup>2</sup> [1/2] + 4% 7d (5/2) <sup>2</sup> [1/2]		6
7p	(5/2) <sup>2</sup> [3/2]	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )7p	2[3/2]	147327.659	0.007		94% + 4% sp + 1% 7p (5/2) <sup>2</sup> [5/2] <sup>o</sup>	R	10
7p	(5/2) <sup>2</sup> [7/2]	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )7p	2[7/2]	147525.93	0.06		98% + 1% sp		3
7p	(5/2) <sup>2</sup> [3/2]	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )7p	2[3/2]	147562.672	0.006		94% + 3% sp + 1% 5f (3/2) <sup>2</sup> [3/2] <sup>o</sup>		8
7p	(5/2) <sup>2</sup> [7/2]	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )7p	2[7/2]	147596.655	0.006		100%		4
7p	(5/2) <sup>2</sup> [5/2]	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )7p	2[5/2]	147647.699	0.009		94% + 3% sp + 2% 7p (5/2) <sup>2</sup> [3/2] <sup>o</sup>		7
7p	(5/2) <sup>2</sup> [5/2]	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )7p	2[5/2]	147762.990	0.005		98%		8
5f	(3/2) <sup>2</sup> [3/2]	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )5f	2[3/2]	147987.359	0.004		99%		9
5f	(3/2) <sup>2</sup> [3/2]	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )5f	2[3/2]	148016.157	0.004		99% + 1% 7p (5/2) <sup>2</sup> [3/2] <sup>o</sup>		11
5f	(3/2) <sup>2</sup> [9/2]	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )5f	2[9/2]	148028.7360	0.0023		100%		5
5f	(3/2) <sup>2</sup> [9/2]	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )5f	2[9/2]	148033.574	0.003		100%		6
5f	(3/2) <sup>2</sup> [5/2]	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )5f	2[5/2]	148061.467	0.003		97% + 2% 5f (3/2) <sup>2</sup> [7/2] <sup>o</sup>		11
5f	(3/2) <sup>2</sup> [5/2]	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )5f	2[5/2]	148066.011	0.003		99%		9
5f	(3/2) <sup>2</sup> [7/2]	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )5f	2[7/2]	148102.986	0.003		97% + 3% 5f (3/2) <sup>2</sup> [5/2] <sup>o</sup>		5
5f	(3/2) <sup>2</sup> [7/2]	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )5f	2[7/2]	148105.366	0.003		100%		3
5g	(3/2) <sup>2</sup> [5/2]	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )5g	2[5/2]	148133.777	0.003		100%		3
5g	(3/2) <sup>2</sup> [5/2]	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )5g	2[5/2]	148133.832	0.005		100%		3
5g	(3/2) <sup>2</sup> [11/2]	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )5g	2[11/2]	148145.7906	0.0021		100%		3
5g	(3/2) <sup>2</sup> [11/2]	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )5g	2[11/2]	148145.8203	0.0021		100%		3
5g	(3/2) <sup>2</sup> [7/2]	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )5g	2[7/2]	148167.557	0.003		100%		5
5g	(3/2) <sup>2</sup> [7/2]	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )5g	2[7/2]	148167.5920	0.0017		100%		4
5g	(3/2) <sup>2</sup> [9/2]	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )5g	2[9/2]	148179.1541	0.0019		100%		4
5g	(3/2) <sup>2</sup> [9/2]	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )5g	2[9/2]	148179.1829	0.0016		100%		4



Table A2. Cont.

Label <sup>a</sup>	Configuration	Term	J	Level <sup>b</sup> , cm <sup>-1</sup>	Unc. <sup>c</sup> , cm <sup>-1</sup>	Landé g <sup>d</sup>	Leading Percentages <sup>e</sup>	Note <sup>f</sup>	N <sub>lines</sub> <sup>g</sup>
6d	(3/2) <sup>2</sup> [1/2]	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )6d	2 <sup>1</sup> [1/2]	148361.542	0.004		99%		10
6d	(3/2) <sup>2</sup> [7/2]	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )6d	3	148481.763	0.003		100%		11
6d	(3/2) <sup>2</sup> [7/2]	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )6d	4	148515.552	0.004		100%		9
6d	(3/2) <sup>2</sup> [3/2]	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )6d	2 <sup>3</sup> [3/2]	148521.575	0.003		100%		12
6d	(3/2) <sup>2</sup> [3/2]	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )6d	1	148559.958	0.003		99% + 1% 6d (3/2) <sup>2</sup> [5/2]		15
6d	(3/2) <sup>2</sup> [5/2]	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )6d	3	148631.096	0.003		100%		13
6d	(3/2) <sup>2</sup> [5/2]	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )6d	2	148642.489	0.003		99% + 1% 6d (3/2) <sup>2</sup> [3/2]		13
6d	(3/2) <sup>2</sup> [1/2]	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )6d	2 <sup>1</sup> [1/2]	149202.607	0.007		51% + 28% 7d (5/2) <sup>2</sup> [1/2] + 6% 6d (5/2) <sup>2</sup> [1/2]		3
7p	(3/2) <sup>2</sup> [1/2] <sup>o</sup>	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )7p	2 <sup>1</sup> [1/2] <sup>o</sup>	149371.08	0.008		94% + 5% sp		2
7p	(3/2) <sup>2</sup> [1/2] <sup>o</sup>	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )7p	1	149484.111	0.008		95% + 4% sp + 1% 7p (5/2) <sup>2</sup> [3/2] <sup>o</sup>		5
7p	(3/2) <sup>2</sup> [5/2] <sup>o</sup>	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )7p	2 <sup>5</sup> [2] <sup>o</sup>	149525.97	0.005		64% + 26% 7p (3/2) <sup>2</sup> [3/2] <sup>o</sup> + 8% sp		4
7p	(3/2) <sup>2</sup> [5/2] <sup>o</sup>	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )7p	3	149624.47	0.005		92% + 6% sp		2
7p	(3/2) <sup>2</sup> [3/2] <sup>o</sup>	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )7p	2 <sup>3</sup> [3/2] <sup>o</sup>	149726.69	0.005		63% + 33% 7p (3/2) <sup>2</sup> [5/2] <sup>o</sup> + 3% sp		3
7p	(3/2) <sup>2</sup> [3/2] <sup>o</sup>	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )7p	2 <sup>3</sup> [2] <sup>o</sup>	149765.88	0.005		95% + 4% sp		4
sp	(D) <sup>1</sup> p <sup>o</sup> - 1p <sup>o</sup>	3d <sup>8</sup> ( <sup>1</sup> D)4s4p( <sup>1</sup> P <sup>o</sup> )	1D <sup>o</sup>	150249.887	0.008		38% + 28% sp (1p <sup>o</sup> ) 3p <sup>o</sup> + 11% 7p 1D <sup>o</sup>		8
8s	(5/2) <sup>2</sup> [5/2]	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )8s	2 <sup>5</sup> [2]	150742.896	0.003		100%		13
8s	(5/2) <sup>2</sup> [5/2]	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )8s	2	150782.454	0.003		100%		13
6f	(5/2) <sup>2</sup> [1/2] <sup>o</sup>	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )6f	2 <sup>1</sup> [1/2] <sup>o</sup>	151161.379	0.007		63% + 21% sp + 5% 8p (5/2) <sup>2</sup> [3/2] <sup>o</sup>		6
6f	(5/2) <sup>2</sup> [1/2] <sup>o</sup>	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )6f	0	151327.262	0.008		98% + 1% sp		2
6f	(5/2) <sup>2</sup> [11/2] <sup>o</sup>	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )6f	2 <sup>11</sup> [1/2] <sup>o</sup>	151372.330	0.004		100%		4
6f	(5/2) <sup>2</sup> [3/2] <sup>o</sup>	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )6f	2 <sup>3</sup> [2] <sup>o</sup>	151373.840	0.006		96% + 3% 6f (5/2) <sup>2</sup> [1/2] <sup>o</sup>		5
6f	(5/2) <sup>2</sup> [3/2] <sup>o</sup>	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )6f	2 <sup>3</sup> [2] <sup>o</sup>	151375.318	0.004		52% + 46% 6f (5/2) <sup>2</sup> [5/2] <sup>o</sup>		7
6f	(5/2) <sup>2</sup> [11/2] <sup>o</sup>	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )6f	2 <sup>11</sup> [1/2] <sup>o</sup>	151377.688	0.005		100%		2
6f	(5/2) <sup>2</sup> [5/2] <sup>o</sup>	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )6f	3	151402.621	0.004		71% + 28% 6f (5/2) <sup>2</sup> [7/2] <sup>o</sup>		7
6f	(5/2) <sup>2</sup> [5/2] <sup>o</sup>	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )6f	2	151403.942	0.004		53% + 44% 6f (5/2) <sup>2</sup> [3/2] <sup>o</sup>		8
6f	(5/2) <sup>2</sup> [7/2] <sup>o</sup>	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )6f	2 <sup>7</sup> [2] <sup>o</sup>	151419.022	0.004		90% + 10% 6f (5/2) <sup>2</sup> [9/2] <sup>o</sup>		8
6f	(5/2) <sup>2</sup> [9/2] <sup>o</sup>	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )6f	2 <sup>9</sup> [2] <sup>o</sup>	151421.791	0.004		90% + 10% 6f (5/2) <sup>2</sup> [7/2] <sup>o</sup>		9
6f	(5/2) <sup>2</sup> [9/2] <sup>o</sup>	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )6f	2 <sup>9</sup> [2] <sup>o</sup>	151423.056	0.004		100%		4
8p	(5/2) <sup>2</sup> [3/2] <sup>o</sup>	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )8p	2 <sup>3</sup> [2] <sup>o</sup>	151424.241	0.004		33% 6f (5/2) <sup>2</sup> [1/2] <sup>o</sup> + 36% sp + 20% 8p (5/2) <sup>2</sup> [3/2] <sup>o</sup>		8
6g	(5/2) <sup>2</sup> [3/2] <sup>o</sup>	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )6g	2 <sup>3</sup> [2] <sup>o</sup>	151440.091	0.008		100%		2
6g	(5/2) <sup>2</sup> [3/2] <sup>o</sup>	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )6g	2	151440.178	0.006		100%		2
6g	(5/2) <sup>2</sup> [7/2] <sup>o</sup>	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )6g	2 <sup>7</sup> [2] <sup>o</sup>	151441.899	0.006		70% + 27% 6f (5/2) <sup>2</sup> [5/2] <sup>o</sup> + 2% sp		7
6g	(5/2) <sup>2</sup> [13/2]	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )6g	2 <sup>13</sup> [2]	151450.414	0.007		100%		2
6g	(5/2) <sup>2</sup> [13/2]	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )6g	2 <sup>13</sup> [2]	151450.488	0.003		100%		1
6g	(5/2) <sup>2</sup> [15/2]	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )6g	2 <sup>15</sup> [2]	151452.690	0.007		100%		4
6g	(5/2) <sup>2</sup> [15/2]	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )6g	2 <sup>15</sup> [2]	151452.701	0.006		100%		4
6h	(5/2) <sup>2</sup> [5/2] <sup>o</sup>	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )6h	2 <sup>5</sup> [2] <sup>o</sup>	[151458.3]	6		100%	pf	0
6h	(5/2) <sup>2</sup> [5/2] <sup>o</sup>	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )6h	3	[151458.4]	6		100%	pf	0
6h	(5/2) <sup>2</sup> [15/2] <sup>o</sup>	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )6h	2 <sup>15</sup> [2] <sup>o</sup>	[151461.7]	6		100%	pf	0
6h	(5/2) <sup>2</sup> [15/2] <sup>o</sup>	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )6h	2 <sup>15</sup> [2] <sup>o</sup>	[151461.8]	6		100%	pf	0
6h	(5/2) <sup>2</sup> [7/2] <sup>o</sup>	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )6h	2 <sup>7</sup> [2] <sup>o</sup>	[151463.9]	6		100%	pf	0

Table A2. Cont.

Label <sup>a</sup>	Configuration	Term	J	Level <sup>b</sup> , cm <sup>-1</sup>	Unc. <sup>c</sup> , cm <sup>-1</sup>	Landé <sup>d</sup> g <sup>d</sup>	Leading Percentages <sup>e</sup>	Note <sup>f</sup>	N <sub>lines</sub> <sup>g</sup>
6h	(5/2) <sup>3</sup> [7/2] <sup>o</sup>	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )6h	4	151464.01	6		100%	pf	0
6g	(5/2) <sup>2</sup> [7/2] <sup>o</sup>	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )6g	3	151464.789	0.006		100%		4
6g	(5/2) <sup>2</sup> [7/2] <sup>o</sup>	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )6g	4	151464.796	0.005		100%		2
6h	(5/2) <sup>2</sup> [9/2] <sup>o</sup>	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )6h	4	151468.51	6		100%	pf	0
6h	(5/2) <sup>2</sup> [9/2] <sup>o</sup>	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )6h	5	151468.51	6		100%	pf	0
6h	(5/2) <sup>2</sup> [13/2] <sup>o</sup>	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )6h	6	151469.81	6		100%	pf	0
6h	(5/2) <sup>2</sup> [13/2] <sup>o</sup>	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )6h	7	151470.01	6		100%	pf	0
6g	(5/2) <sup>2</sup> [11/2] <sup>o</sup>	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )6g	5	151470.113	0.003		100%		5
6g	(5/2) <sup>2</sup> [11/2] <sup>o</sup>	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )6g	6	151470.130	0.005		100%		3
6h	(5/2) <sup>2</sup> [11/2] <sup>o</sup>	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )6h	5	151471.41	6		100%	pf	0
6h	(5/2) <sup>2</sup> [11/2] <sup>o</sup>	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )6h	6	151471.51	6		100%	pf	0
6g	(5/2) <sup>2</sup> [9/2] <sup>o</sup>	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )6g	4	151472.264	0.005		100%		5
6g	(5/2) <sup>2</sup> [9/2] <sup>o</sup>	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )6g	5	151472.278	0.005		100%		3
7d	(5/2) <sup>2</sup> [1/2] <sup>o</sup>	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )7d	1	151552.191	0.007		98% + 1% 7d (5/2) <sup>2</sup> [3/2]		2
7d	(5/2) <sup>2</sup> [9/2] <sup>o</sup>	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )7d	2	151552.191	0.005		100%		5
7d	(5/2) <sup>2</sup> [3/2] <sup>o</sup>	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )7d	3	151662.985	0.005		96% + 4% 7d (5/2) <sup>2</sup> [5/2]		6
7d	(5/2) <sup>2</sup> [9/2] <sup>o</sup>	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )7d	4	151668.328	0.005		99%		7
7d	(5/2) <sup>2</sup> [3/2] <sup>o</sup>	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )7d	1	151671.666	0.006		99% + 1% 7d (5/2) <sup>2</sup> [1/2]		4
7d	(5/2) <sup>2</sup> [5/2] <sup>o</sup>	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )7d	3	151708.347	0.004		99% + 1% 7d (5/2) <sup>2</sup> [7/2]		8
7d	(5/2) <sup>2</sup> [7/2] <sup>o</sup>	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )7d	3	151743.558	0.003		99% + 1% 7d (5/2) <sup>2</sup> [5/2]		13
7d	(5/2) <sup>2</sup> [7/2] <sup>o</sup>	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )7d	4	151744.916	0.005		99%		8
7d	(5/2) <sup>2</sup> [5/2] <sup>o</sup>	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )7d	2	151757.601	0.004		96% + 4% 7d (5/2) <sup>2</sup> [3/2]		8
8p	(5/2) <sup>2</sup> [1/2] <sup>o</sup>	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )8p	2	152054.78	0.03		53% + 21% 8p (5/2) <sup>2</sup> [5/2] <sup>o</sup> + 20% sp	N	5
7d	(5/2) <sup>2</sup> [1/2] <sup>o</sup>	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )7d	0	152179.051	0.007		52% + 28% 7d (3/2) <sup>2</sup> [1/2] <sup>o</sup> + 9% 8d (5/2) <sup>2</sup> [1/2]		2
8p	(5/2) <sup>2</sup> [5/2] <sup>o</sup>	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )8p	2	152580.19	0.05		65% + 27% 8p (5/2) <sup>2</sup> [3/2] <sup>o</sup> + 7% sp	N	2
8s	(3/2) <sup>2</sup> [3/2] <sup>o</sup>	3d <sup>8</sup> ( <sup>3</sup> P)4s4p( <sup>1</sup> P <sup>o</sup> )	0	152783.41	0.05		77% + 9% 8p <sup>3</sup> p <sup>o</sup> + 5% 7p <sup>3</sup> p <sup>o</sup>	N	2
8s	(3/2) <sup>2</sup> [3/2] <sup>o</sup>	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )8s	1	152814.032	0.007		100%	N	4
8s	(3/2) <sup>2</sup> [3/2] <sup>o</sup>	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )8s	2	152840.475	0.005		100%	N	4
sp	( <sup>1</sup> D) <sup>o</sup> p <sup>o</sup> 3p <sup>o</sup>	3d <sup>8</sup> ( <sup>3</sup> P)4s4p( <sup>1</sup> P <sup>o</sup> )	3p <sup>o</sup>	152944.11	0.05		39% + 19% sp ( <sup>1</sup> D) <sup>o</sup> p <sup>o</sup> 1D <sup>o</sup> + 16% 8p <sup>3</sup> p <sup>o</sup>	N	4
sp	( <sup>1</sup> D) <sup>o</sup> p <sup>o</sup> 1p <sup>o</sup>	3d <sup>8</sup> ( <sup>1</sup> D)4s4p( <sup>1</sup> P <sup>o</sup> )	1p <sup>o</sup>	152944.11	0.04		22% + 18% 6f <sup>3</sup> D <sup>o</sup> + 17% 6f <sup>3</sup> P <sup>o</sup>	N	5
6f	(3/2) <sup>2</sup> [5/2] <sup>o</sup>	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )6f	3	153410.212	0.006		89% + 8% sp + 1% 6f (3/2) <sup>2</sup> [7/2] <sup>o</sup>		5
6f	(3/2) <sup>2</sup> [3/2] <sup>o</sup>	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )6f	2	153426.632	0.006		52% + 42% 6f (3/2) <sup>2</sup> [5/2] <sup>o</sup> + 5% sp		7
6f	(3/2) <sup>2</sup> [9/2] <sup>o</sup>	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )6f	5	153449.633	0.005		100%		2
6f	(3/2) <sup>2</sup> [9/2] <sup>o</sup>	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )6f	4	153455.178	0.005		100%		4
6f	(3/2) <sup>2</sup> [3/2] <sup>o</sup>	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )6f	1	153457.747	0.009		55% + 23% sp + 15% 8p (3/2) <sup>2</sup> [1/2] <sup>o</sup>		6
6f	(3/2) <sup>2</sup> [3/2] <sup>o</sup>	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )6f	2	153487.668	0.006		56% + 37% 6f (3/2) <sup>2</sup> [3/2] <sup>o</sup> + 5% sp		8
6f	(3/2) <sup>2</sup> [7/2] <sup>o</sup>	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )6f	4	153495.854	0.006		100%		3
6f	(3/2) <sup>2</sup> [7/2] <sup>o</sup>	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )6f	3	153498.834	0.007		98% + 2% 6f (3/2) <sup>2</sup> [5/2] <sup>o</sup>		3
6g	(3/2) <sup>2</sup> [5/2] <sup>o</sup>	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )6g	2	153517.905	0.008		100%		2
6g	(3/2) <sup>2</sup> [5/2] <sup>o</sup>	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )6g	1	153517.985	0.008		100%		1
6g	(3/2) <sup>2</sup> [11/2] <sup>o</sup>	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )6g	5	153524.933	0.005		100%		2

Table A2. Cont.

Label <sup>a</sup>	Configuration	Term	J	Level <sup>b</sup> , cm <sup>-1</sup>	Unc. <sup>c</sup> , cm <sup>-1</sup>	Landé <sup>e</sup> g <sup>d</sup>	Leading Percentages <sup>e</sup>	Note <sup>f</sup>	N <sub>lines</sub> <sup>g</sup>
6g	(3/2) <sup>2</sup> [11/2]	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )6g	2[11/2]	153524.950	0.007	100%	100%		1
6g	(3/2) <sup>2</sup> [7/2]	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )6g	2[7/2]	153537.395	0.007	100%	100%		2
6g	(3/2) <sup>2</sup> [7/2]	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )6g	2[7/2]	153537.414	0.006	100%	100%		3
6h	(3/2) <sup>2</sup> [7/2] <sup>o</sup>	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )6h	2[7/2] <sup>o</sup>	153543.71	6	100%	100%	pf	0
6h	(3/2) <sup>2</sup> [7/2] <sup>o</sup>	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )6h	2[7/2] <sup>o</sup>	153543.81	6	100%	100%	pf	0
6g	(3/2) <sup>2</sup> [9/2]	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )6g	2[9/2]	153544.054	0.005	100%	100%		3
6g	(3/2) <sup>2</sup> [9/2]	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )6g	2[9/2]	153544.069	0.007	100%	100%		2
6h	(3/2) <sup>2</sup> [13/2] <sup>o</sup>	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )6h	2[13/2] <sup>o</sup>	153546.01	6	100%	100%	pf	0
6h	(3/2) <sup>2</sup> [13/2] <sup>o</sup>	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )6h	2[13/2] <sup>o</sup>	153546.21	6	100%	100%	pf	0
6h	(3/2) <sup>2</sup> [9/2] <sup>o</sup>	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )6h	2[9/2] <sup>o</sup>	153552.01	6	100%	100%	pf	0
6h	(3/2) <sup>2</sup> [9/2] <sup>o</sup>	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )6h	2[9/2] <sup>o</sup>	153552.11	6	100%	100%	pf	0
6h	(3/2) <sup>2</sup> [11/2] <sup>o</sup>	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )6h	2[11/2] <sup>o</sup>	153554.31	6	100%	100%	pf	0
6h	(3/2) <sup>2</sup> [11/2] <sup>o</sup>	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )6h	2[11/2] <sup>o</sup>	153554.41	6	100%	100%	pf	0
7d	(3/2) <sup>2</sup> [1/2]	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )7d	2[1/2]	153688.567	0.006	99%	97%		5
7d	(3/2) <sup>2</sup> [7/2]	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )7d	2[7/2]	153730.935	0.005	100%	100%		5
7d	(3/2) <sup>2</sup> [7/2]	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )7d	2[7/2]	153730.851	0.005	100%	100%		3
7d	(3/2) <sup>2</sup> [3/2]	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )7d	2[3/2]	153753.738	0.007	100%	100%		2
7d	(3/2) <sup>2</sup> [5/2]	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )7d	2[5/2]	153773.884	0.006	100%	97% + 3% 7d (3/2) <sup>2</sup> [5/2]		5
7d	(3/2) <sup>2</sup> [5/2]	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )7d	2[5/2]	153815.644	0.006	100%	97% + 3% 7d (3/2) <sup>2</sup> [3/2]		5
7d	(3/2) <sup>2</sup> [5/2]	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )7d	2[5/2]	153821.937	0.006	100%	97% + 9% sp (1D) <sup>1</sup> P <sup>o</sup> 1F <sup>o</sup> + 8% 8p 3P <sup>o</sup>	N	4
sp	(3P) <sup>o</sup> 3D <sup>o</sup>	3d <sup>8</sup> ( <sup>3</sup> P)4sp(1P <sup>o</sup> )	3D <sup>o</sup>	153850.18	0.04	100%	49% + 44% 8d (5/2) <sup>2</sup> [1/2] + 2% 8d (3/2) <sup>2</sup> [1/2]	N	2
7d	(3/2) <sup>2</sup> [1/2]	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )7d	2[1/2]	153853.763	0.011	100%	38% + 44% sp + 6% 7f (5/2) <sup>2</sup> [3/2] <sup>o</sup>	N	2
8p	(3/2) <sup>2</sup> [3/2] <sup>o</sup>	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )8p	2[3/2] <sup>o</sup>	154225.21	0.04	100%	100%		2
9s	(5/2) <sup>2</sup> [5/2]	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )9s	2[5/2]	154255.815	0.005	100%	100%		4
9s	(5/2) <sup>2</sup> [5/2]	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )9s	2[5/2]	154281.251	0.008	100%	100%		4
7f	(5/2) <sup>2</sup> [11/2] <sup>o</sup>	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )7f	2[11/2] <sup>o</sup>	154641.392	0.006	99%	99%		2
7f	(5/2) <sup>2</sup> [11/2] <sup>o</sup>	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )7f	2[11/2] <sup>o</sup>	154647.056	0.005	100%	100%		2
7f	(5/2) <sup>2</sup> [9/2] <sup>o</sup>	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )7f	2[9/2] <sup>o</sup>	154653.777	0.07	100%	51% + 25% 8p (3/2) <sup>2</sup> [3/2] <sup>o</sup> + 12% 8p (3/2) <sup>2</sup> [1/2] <sup>o</sup>	N	2
7f	(5/2) <sup>2</sup> [5/2] <sup>o</sup>	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )7f	2[5/2] <sup>o</sup>	154672.123	0.006	100%	62% + 37% 7f (5/2) <sup>2</sup> [7/2] <sup>o</sup>		4
7f	(5/2) <sup>2</sup> [7/2] <sup>o</sup>	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )7f	2[7/2] <sup>o</sup>	154672.766	0.006	100%	91% + 9% 7f (5/2) <sup>2</sup> [9/2] <sup>o</sup>		5
7f	(5/2) <sup>2</sup> [9/2] <sup>o</sup>	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )7f	2[9/2] <sup>o</sup>	154674.551	0.006	100%	91% + 9% 7f (5/2) <sup>2</sup> [7/2] <sup>o</sup>		4
7f	(5/2) <sup>2</sup> [9/2] <sup>o</sup>	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )7f	2[9/2] <sup>o</sup>	154675.247	0.005	100%	100%		4
7f	(5/2) <sup>2</sup> [7/2] <sup>o</sup>	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )7f	2[7/2] <sup>o</sup>	154678.877	0.008	100%	62% + 36% 7f (5/2) <sup>2</sup> [5/2] <sup>o</sup> + 1% sp		3
7g	(5/2) <sup>2</sup> [3/2]	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )7g	2[3/2]	154688.020	0.011	100%	100%		2
7g	(5/2) <sup>2</sup> [3/2]	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )7g	2[3/2]	154688.112	0.009	100%	100%		3
7g	(5/2) <sup>2</sup> [13/2]	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )7g	2[13/2]	154694.589	0.008	100%	100%		1
7g	(5/2) <sup>2</sup> [13/2]	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )7g	2[13/2]	154694.619	0.008	100%	100%		1
7g	(5/2) <sup>2</sup> [15/2]	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )7g	2[15/2]	154695.997	0.008	100%	100%		4
7g	(5/2) <sup>2</sup> [15/2]	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )7g	2[15/2]	154696.009	0.007	100%	100%	N	4
7f	(5/2) <sup>2</sup> [5/2] <sup>o</sup>	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )7f	2[5/2] <sup>o</sup>	154698.288	0.020	100%	39% + 28% 8p (3/2) <sup>2</sup> [3/2] <sup>o</sup> + 15% 7f (5/2) <sup>2</sup> [3/2] <sup>o</sup>	N	3
7h	(5/2) <sup>2</sup> [5/2] <sup>o</sup>	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )7h	2[5/2] <sup>o</sup>	[154702.4]	2.0	100%	100%	pf	0

Table A2. Cont.

Label <sup>a</sup>	Configuration	Term	J	Level <sup>b</sup> , cm <sup>-1</sup>	Unc. <sup>c</sup> , cm <sup>-1</sup>	Landé <sup>d</sup> g <sup>d</sup>	Leading Percentages <sup>e</sup>	Note <sup>f</sup>	N <sub>lines</sub> <sup>g</sup>
7h	(5/2) <sup>3</sup> [5/2] <sup>o</sup>	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )7h	2[5/2] <sup>o</sup>	154702.5	2.0		100%	pf	0
7g	(5/2) <sup>2</sup> [7/2]	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )7g	2[7/2]	154703.597	0.008		100%		2
7g	(5/2) <sup>2</sup> [7/2]	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )7g	2[7/2]	154703.625	0.008		100%		2
7h	(5/2) <sup>2</sup> [15/2] <sup>o</sup>	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )7h	2[15/2] <sup>o</sup>	154704.6	2.0		100%	pf	0
7h	(5/2) <sup>2</sup> [15/2] <sup>o</sup>	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )7h	2[15/2] <sup>o</sup>	154704.6	2.0		100%	pf	0
7h	(5/2) <sup>2</sup> [7/2] <sup>o</sup>	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )7h	2[7/2] <sup>o</sup>	154706.01	2.0		100%	pf	0
7h	(5/2) <sup>2</sup> [7/2] <sup>o</sup>	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )7h	2[7/2] <sup>o</sup>	154706.11	2.0		100%	pf	0
7g	(5/2) <sup>2</sup> [11/2]	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )7g	2[11/2]	154706.911	0.007		100%		3
7g	(5/2) <sup>2</sup> [9/2]	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )7g	2[9/2]	154708.235	0.007		100%	N	5
7g	(5/2) <sup>2</sup> [9/2]	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )7g	2[9/2]	154708.244	0.007		100%		2
7h	(5/2) <sup>2</sup> [9/2]	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )7h	2[9/2]	154709.1	2.0		100%	pf	0
7h	(5/2) <sup>2</sup> [9/2]	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )7h	2[9/2]	154709.1	2.0		100%	pf	0
7h	(5/2) <sup>2</sup> [13/2] <sup>o</sup>	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )7h	2[13/2] <sup>o</sup>	154709.71	2.0		100%	pf	0
7h	(5/2) <sup>2</sup> [13/2] <sup>o</sup>	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )7h	2[13/2] <sup>o</sup>	154709.8	2.0		100%	pf	0
7h	(5/2) <sup>2</sup> [11/2] <sup>o</sup>	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )7h	2[11/2] <sup>o</sup>	154710.71	2.0		100%	pf	0
7h	(5/2) <sup>2</sup> [11/2] <sup>o</sup>	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )7h	2[11/2] <sup>o</sup>	154710.81	2.0		100%	pf	0
8p	(3/2) <sup>2</sup> [1/2] <sup>o</sup>	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )8p	2[1/2] <sup>o</sup>	154719.09	0.03		29% + 32% 8p (3/2) <sup>2</sup> [3/2] <sup>o</sup> + 19% sp	N	3
8d	(5/2) <sup>2</sup> [1/2]	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )8d	2[1/2]	154766.034	0.022		98% + 1% 8d (5/2) <sup>2</sup> [3/2]		1
8d	(5/2) <sup>2</sup> [9/2]	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )8d	2[9/2]	154828.718	0.008		100%		2
8d	(5/2) <sup>2</sup> [3/2]	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )8d	2[3/2]	154832.657	0.011		95% + 5% 8d (5/2) <sup>2</sup> [5/2]		1
8d	(5/2) <sup>2</sup> [9/2]	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )8d	2[9/2]	154836.434	0.006		100%		4
8d	(5/2) <sup>2</sup> [3/2]	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )8d	2[3/2]	154838.9737	0.013		98% + 1% 8d (5/2) <sup>2</sup> [1/2]		2
8d	(5/2) <sup>2</sup> [5/2]	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )8d	2[5/2]	154860.741	0.006		98% + 1% 8d (5/2) <sup>2</sup> [7/2]		5
8d	(5/2) <sup>2</sup> [7/2]	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )8d	2[7/2]	154883.104	0.009		98% + 1% 8d (5/2) <sup>2</sup> [5/2]		2
8d	(5/2) <sup>2</sup> [7/2]	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )8d	2[7/2]	154883.625	0.007		100%		6
8d	(5/2) <sup>2</sup> [5/2]	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )8d	2[5/2]	154892.916	0.020		95% + 5% 8d (5/2) <sup>2</sup> [3/2]		2
8d	(5/2) <sup>2</sup> [1/2]	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )8d	2[1/2]	155244.8422	0.021		32% + 29% 9d (5/2) <sup>2</sup> [1/2] + 20% 8d (3/2) <sup>2</sup> [1/2]		1
9s	(3/2) <sup>2</sup> [3/2]	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )9s	2[3/2]	156326.913	0.018		100%		4
9s	(3/2) <sup>2</sup> [3/2]	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )9s	2[3/2]	156341.878	0.009		99% + 1% 10s (5/2) <sup>2</sup> [5/2]		5
10s	(5/2) <sup>2</sup> [5/2]	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )10s	2[5/2]	156508.501	0.022		100%		1
10s	(5/2) <sup>2</sup> [5/2]	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )10s	2[5/2]	156526.436	0.015		99% + 1% 9s (3/2) <sup>2</sup> [3/2]		2
7f	(3/2) <sup>2</sup> [9/2] <sup>o</sup>	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )7f	2[9/2] <sup>o</sup>	156711.894	0.007		91% + 6% 8f (5/2) <sup>2</sup> [11/2] <sup>o</sup> + 3% 8f (5/2) <sup>2</sup> [9/2] <sup>o</sup>		2
7f	(3/2) <sup>2</sup> [9/2] <sup>o</sup>	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )7f	2[9/2] <sup>o</sup>	156721.308	0.007		97% + 3% 8f (5/2) <sup>2</sup> [9/2] <sup>o</sup>		2
7f	(3/2) <sup>2</sup> [7/2] <sup>o</sup>	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )7f	2[7/2] <sup>o</sup>	156754.91	7		99% + 1% 8f (5/2) <sup>2</sup> [7/2] <sup>o</sup>	sf	0
8f	(5/2) <sup>2</sup> [11/2] <sup>o</sup>	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )8f	2[11/2] <sup>o</sup>	156761.443	0.008		94% + 6% 7f (3/2) <sup>2</sup> [9/2] <sup>o</sup>		3
7g	(3/2) <sup>2</sup> [5/2]	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )7g	2[5/2]	156763.090	0.011		99% + 1% 8g (5/2) <sup>2</sup> [5/2]		1
8f	(5/2) <sup>2</sup> [11/2] <sup>o</sup>	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )8f	2[11/2] <sup>o</sup>	156767.066	0.016		99% + 1% 8g (5/2) <sup>2</sup> [5/2]		2
7g	(3/2) <sup>2</sup> [11/2]	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )7g	2[11/2]	156767.609	0.011		99% + 1% 8g (5/2) <sup>2</sup> [11/2]	N	1
7g	(3/2) <sup>2</sup> [11/2]	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )7g	2[11/2]	156767.630	0.011		99% + 1% 8g (5/2) <sup>2</sup> [11/2]		2
7g	(3/2) <sup>2</sup> [7/2]	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )7g	2[7/2]	156775.405	0.014		99% + 1% 8g (5/2) <sup>2</sup> [7/2]		2

Table A2. Cont.

Label <sup>a</sup>	Configuration	Term	J	Level <sup>b</sup> , cm <sup>-1</sup>	Unc. <sup>c</sup> , cm <sup>-1</sup>	Landé g <sup>d</sup>	Leading Percentages <sup>e</sup>	Note <sup>f</sup>	N <sub>lines</sub> <sup>g</sup>
7g	(3/2) <sup>2</sup> [7/2] <sup>o</sup>	2 <sup>1</sup> [7/2]	4	156775.430	0.014		99% + 1% 8g (5/2) <sup>2</sup> [7/2]	N	1
8f	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> ) <sup>2</sup> 8f	2 <sup>1</sup> [7/2] <sup>o</sup>	4	156779.71	7		94% + 5% 8f (5/2) <sup>2</sup> [9/2] <sup>o</sup> + 1% 7f (3/2) <sup>2</sup> [7/2] <sup>o</sup>	sf	0
7g	(3/2) <sup>2</sup> [9/2]	2 <sup>1</sup> [9/2]	4	156779.847	0.014		100%		2
7g	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> ) <sup>2</sup> 7g	2 <sup>1</sup> [9/2]	5	156779.855	0.014			N	1
8f	(5/2) <sup>2</sup> [9/2] <sup>o</sup>	2 <sup>1</sup> [9/2] <sup>o</sup>	4	156781.71	7		92% + 5% 8f (5/2) <sup>2</sup> [7/2] <sup>o</sup> + 2% 7f (3/2) <sup>2</sup> [9/2] <sup>o</sup>	sf	0
8f	(5/2) <sup>2</sup> [9/2] <sup>o</sup>	2 <sup>1</sup> [9/2] <sup>o</sup>	5	156782.41	7		97% + 3% 7f (3/2) <sup>2</sup> [9/2] <sup>o</sup>	sf	0
8g	(5/2) <sup>2</sup> [3/2]	2 <sup>1</sup> [3/2]	2	156797.31	2.0		100%	pf	0
8g	(5/2) <sup>2</sup> [7/2]	2 <sup>1</sup> [7/2]	3	156805.71	2.0		99% + 1% 7g (3/2) <sup>2</sup> [7/2]	pf	0
8g	(5/2) <sup>2</sup> [9/2]	2 <sup>1</sup> [9/2]	5	156807.81	2.0		100%	pf	0
8g	(5/2) <sup>2</sup> [11/2]	2 <sup>1</sup> [11/2]	6	156808.1897	0.010		99% + 1% 7g (3/2) <sup>2</sup> [11/2]	N	2
9d	(5/2) <sup>2</sup> [9/2]	2 <sup>1</sup> [9/2]	5	156888.51	2.0		100%	sf	0
9d	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> ) <sup>2</sup> 9d	2 <sup>1</sup> [9/2]	4	156912.740	0.011		51% + 44% 8d (3/2) <sup>2</sup> [7/2] + 5% 9d (5/2) <sup>2</sup> [7/2]		2
8d	(3/2) <sup>2</sup> [5/2]	2 <sup>1</sup> [5/2]	2	156958.117	0.06		42% + 38% 9d (5/2) <sup>2</sup> [5/2] + 16% 8d (3/2) <sup>2</sup> [3/2]		1
9g	(5/2) <sup>2</sup> [3/2]	2 <sup>1</sup> [3/2]	2	158241.1	2.0		100%	pf	0
9g	(5/2) <sup>2</sup> [7/2]	2 <sup>1</sup> [7/2]	3	158246.81	4		100%	pf	0
10d	(5/2) <sup>2</sup> [1/2]	2 <sup>1</sup> [1/2]	1	158285.31	4		98% + 2% 10d (5/2) <sup>2</sup> [3/2]	sf	0
10d	(5/2) <sup>2</sup> [3/2]	2 <sup>1</sup> [3/2]	2	158306.01	5		95% + 4% 10d (5/2) <sup>2</sup> [5/2]	sf	0
10d	(5/2) <sup>2</sup> [9/2]	2 <sup>1</sup> [9/2]	5	158306.91	2.0		100%	sf	0
10d	(5/2) <sup>2</sup> [11/2]	2 <sup>1</sup> [11/2]	4	158308.91	2.0		100%	sf	0
10d	(5/2) <sup>2</sup> [1/2]	2 <sup>1</sup> [1/2]	1	158310.41	4		98% + 2% 10d (5/2) <sup>2</sup> [1/2]	sf	0
10d	(5/2) <sup>2</sup> [3/2]	2 <sup>1</sup> [3/2]	2	158333.31	4		98% + 2% 10d (5/2) <sup>2</sup> [7/2]	sf	0
10d	(5/2) <sup>2</sup> [5/2]	2 <sup>1</sup> [5/2]	3	158333.31	4		95% + 4% 10d (5/2) <sup>2</sup> [3/2]	sf	0
10d	(5/2) <sup>2</sup> [7/2]	2 <sup>1</sup> [7/2]	3	158334.11	5		98% + 2% 10d (5/2) <sup>2</sup> [5/2]	sf	0
10d	(5/2) <sup>2</sup> [9/2]	2 <sup>1</sup> [9/2]	4	158334.21	4		100%	sf	0
10s	(3/2) <sup>2</sup> [3/2]	2 <sup>1</sup> [3/2]	1	158579.33	0.14		100%	N	1
8f	(3/2) <sup>2</sup> [9/2] <sup>o</sup>	2 <sup>1</sup> [9/2] <sup>o</sup>	4	158851.11	8		100%	sf	0
8f	(3/2) <sup>2</sup> [7/2] <sup>o</sup>	2 <sup>1</sup> [7/2] <sup>o</sup>	4	158864.41	8		100%	sf	0
8g	(3/2) <sup>2</sup> [5/2]	2 <sup>1</sup> [5/2]	3	158869.31	2.0		100%	pf	0
8g	(3/2) <sup>2</sup> [11/2]	2 <sup>1</sup> [11/2]	6	158871.71	2.0		100%	pf	0
8g	(3/2) <sup>2</sup> [7/2]	2 <sup>1</sup> [7/2]	4	158875.81	2.0		100%	pf	0
8h	(3/2) <sup>2</sup> [7/2] <sup>o</sup>	2 <sup>1</sup> [7/2] <sup>o</sup>	3	158876.91	2.0		100%	pf	0
8h	(3/2) <sup>2</sup> [7/2]	2 <sup>1</sup> [7/2]	4	158877.01	2.0		100%	pf	0
8h	(3/2) <sup>2</sup> [13/2]	2 <sup>1</sup> [13/2]	6	158877.91	2.0		100%	pf	0
8g	(3/2) <sup>2</sup> [9/2]	2 <sup>1</sup> [9/2]	5	158878.01	2.0		100%	pf	0
8h	(3/2) <sup>2</sup> [13/2]	2 <sup>1</sup> [13/2]	7	158878.01	2.0		100%	pf	0
8h	(3/2) <sup>2</sup> [9/2]	2 <sup>1</sup> [9/2]	4	158880.41	2.0		100%	pf	0
8h	(3/2) <sup>2</sup> [9/2]	2 <sup>1</sup> [9/2]	5	158880.51	2.0		100%	pf	0
8h	(3/2) <sup>2</sup> [11/2]	2 <sup>1</sup> [11/2]	5	158880.51	2.0		100%	pf	0
8h	(3/2) <sup>2</sup> [11/2]	2 <sup>1</sup> [11/2]	6	158881.41	2.0		100%	pf	0
9d	(3/2) <sup>2</sup> [11/2]	2 <sup>1</sup> [11/2]	1	158935.91	4		99%	sf	0

Table A2. Cont.

Label <sup>a</sup>	Configuration	Term	J	Level <sup>b</sup> , cm <sup>-1</sup>	Unc. <sup>c</sup> , cm <sup>-1</sup>	Landé g <sup>d</sup>	Leading Percentages <sup>e</sup>	Note <sup>f</sup>	N <sub>lines</sub> <sup>g</sup>
9d	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )9d	2 <sup>7</sup> /2	3	158961.1	2.0	100%	100%	sf	0
9d	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )9d	2 <sup>7</sup> /2	4	158966.7	2.0	100%	100%	sf	0
9d	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )9d	2 <sup>5</sup> /2	1	158970.8	2.0	100%	100%	sf	0
9d	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )9d	2 <sup>5</sup> /2	2	158977.0	5	96% + 4% 9d (3/2) <sup>2</sup> [5/2]		sf	0
9d	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )9d	2 <sup>5</sup> /2	3	158999.4	2.0	100%	100%	sf	0
9d	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )9d	2 <sup>5</sup> /2	2	159000.4	5	96% + 4% 9d (3/2) <sup>2</sup> [3/2]		sf	0
10g	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )10g	2 <sup>3</sup> /2	2	159273.3	2.0	100%	100%	pf	0
10g	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )10g	2 <sup>7</sup> /2	3	159277.4	2.0	100%	100%	pf	0
9g	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )9g	2 <sup>5</sup> /2	3	160312.5	2.0	100%	100%	pf	0
9g	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )9g	2 <sup>11</sup> /2	6	160314.1	2.0	100%	100%	pf	0
9g	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )9g	2 <sup>7</sup> /2	4	160317.0	2.0	100%	100%	pf	0
9g	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )9g	2 <sup>9</sup> /2	5	160318.5	2.0	100%	100%	pf	0
10d	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )10d	2 <sup>11</sup> /2	1	160361.5	4	99%		sf	0
10d	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )10d	2 <sup>7</sup> /2	3	160378.4	2.0	100%	100%	sf	0
10d	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )10d	2 <sup>7</sup> /2	4	160382.2	2.0	100%	100%	sf	0
10d	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )10d	2 <sup>3</sup> /2	1	160385.0	2.0	100%	96% + 3% 10d (3/2) <sup>2</sup> [5/2]	sf	0
10d	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )10d	2 <sup>3</sup> /2	2	160388.7	5	100%		sf	0
10d	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )10d	2 <sup>5</sup> /2	3	160404.5	2.0	100%	96% + 3% 10d (3/2) <sup>2</sup> [3/2]	sf	0
10d	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )10d	2 <sup>5</sup> /2	2	160405.1	5	100%		sf	0
10g	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )10g	2 <sup>5</sup> /2	3	161344.3	2.0	100%	100%	pf	0
10g	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )10g	2 <sup>11</sup> /2	6	161345.4	2.0	100%	100%	pf	0
10g	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )10g	2 <sup>7</sup> /2	4	161347.6	2.0	100%	100%	pf	0
10g	3d <sup>9</sup> ( <sup>2</sup> D <sub>3/2</sub> )10g	2 <sup>9</sup> /2	5	161348.6	2.0	100%	100%	pf	0
	Cu III								
	(3d <sup>9</sup> 2D <sub>5/2</sub> )	Limit		163669.2	0.5				

<sup>a</sup> Label used in the column of Leading Percentages;  
<sup>b</sup> Level values were obtained in the least-squares optimization procedure using the LOPT code [39] (see text), except the following: (1) Values in square brackets were obtained using extrapolations along level series (see column "Notes"); (2) The ionization limit is quoted from Ross [2] (see text). A question mark after the value indicates an uncertain identification;  
<sup>c</sup> Uncertainties (one standard deviation) are specified for separations from the 3d<sup>9</sup>4s<sup>3</sup>D<sub>3</sub> level (at 22847.1176 cm<sup>-1</sup>). To determine uncertainties relative to the ground level, the given values should be combined in quadrature with the uncertainty of the ground level, 0.017 cm<sup>-1</sup>;  
<sup>d</sup> Experimental Landé g-factors are quoted from Sugar and Musgrove [17];  
<sup>e</sup> The three leading contributions to the eigenvector are given, if their rounded value is ≥ 1%. The first percentage refers to the configuration and term given in the second and third columns, unless otherwise specified after the percentage value. For the 3d<sup>9</sup>nl levels designated in the J<sub>1</sub>/I (a.k.a. JK) coupling scheme, the percentage value of the 3d<sup>8</sup>4s4p configuration is the sum of percentage contributions of all terms of this configuration;  
<sup>f</sup> Key to the notes: N—newly identified level; R—revised level value (new identification); Rj—revised J value (was 1 in Sugar and Musgrove [17] and Ross [2]); ci—the two previously known levels, for which the identifications have been interchanged; cd—previously known levels, for which the configuration and/or term designations have been revised; sf, pf—level values found by extrapolation using the Ritz quantum-defect or polarization formulas, respectively (see text in Section 4), in combination with the least-squares parametric fitting (see text);  
<sup>g</sup> Number of connecting lines included in the level optimization procedure for this level.

Table 3. Least-squares fitting parameters for Cu II.

Configuration	Parameter <sup>a</sup>	LSF <sup>b</sup>	STD <sup>c</sup>	Group <sup>d</sup>	HFR <sup>e</sup>	LSF/HF	
<b>Even parity</b>							
3d <sup>10</sup>	$E_{av}$	5775.8	52		0.0		
3d <sup>9</sup> 4s	$E_{av}$	26843.5	21		9367.0	2.8658	
	$\zeta(3d)$	819.9	2.0	1	814.7	1.0064	
	$G^2(3d,4s)$	8519.5	132	2	9945.5	0.8566	
3d <sup>9</sup> 4d	$E_{av}$	119071.8	12		98893.7	1.2040	
	$\zeta(3d)$	827.0	2.0	1	821.7	1.0064	
	$\zeta(4d)$	13.7	fixed		13.7	1.0000	
	$F^2(3d,4d)$	3237.5	96		4085.1	0.7925	
	$F^4(3d,4d)$	1109.0	fixed		1386.3	0.8000	
	$C^0(3d,4d)$	1426.8	47		1440.0	0.9908	
	$G^2(3d,4d)$	705.6	152		1276.5	0.5528	
	$C^4(3d,4d)$	538.0	228		890.6	0.6041	
	3d <sup>9</sup> 5s	$E_{av}$	109078.5	20		92286.1	1.1820
		$\zeta(3d)$	826.4	2.0	1	821.1	1.0064
$G^2(3d,5s)$		1537.1	24	2	1794.4	0.8566	
3d <sup>9</sup> 5d	$E_{av}$	137813.1	10		120253.4	1.1460	
	$\zeta(3d)$	827.6	2.0	1	822.3	1.0064	
	$\zeta(5d)$	6.1	fixed		6.1	1.0000	
	$F^2(3d,5d)$	1905.2	73	5	1567.9	1.2152	
	$F^4(3d,5d)$	463.5	fixed		579.4	0.8000	
	$C^0(3d,5d)$	455.2	20	8	616.8	0.7380	
	$G^2(3d,5d)$	412.6	18	8	559.0	0.7380	
	$C^4(3d,5d)$	290.1	13	8	393.0	0.7380	
	3d <sup>9</sup> 5g	$E_{av}$	146914.9	9		129486.8	1.1346
		$\zeta(3d)$	828.0	2.0	1	822.7	1.0064
$F^2(3d,5g)$		133.4	fixed		166.7	0.8000	
$F^4(3d,5g)$		5.2	fixed		6.5	0.8000	
3d <sup>9</sup> 6s	$E_{av}$	134521.0	20		117385.5	1.1460	
	$\zeta(3d)$	827.4	2.0	1	822.1	1.0064	
	$G^2(3d,6s)$	564.8	9	2	659.4	0.8566	
3d <sup>9</sup> 6d	$E_{av}$	147347.9	10		129891.5	1.1344	
	$\zeta(3d)$	827.8	2.0	1	822.5	1.0064	
	$\zeta(6d)$	3.2	fixed		3.2	1.0000	
	$F^2(3d,6d)$	952.5	36	5	783.9	1.2152	
	$F^4(3d,6d)$	240.4	fixed		300.5	0.8000	
	$C^0(3d,6d)$	182.2	17	9	320.8	0.5680	
	$G^2(3d,6d)$	166.8	15	9	293.6	0.5680	
	$C^4(3d,6d)$	117.6	11	9	207.0	0.5680	
	3d <sup>9</sup> 6g	$E_{av}$	152289.1	9		134856.3	1.1293
		$\zeta(3d)$	828.0	2.0	1	822.7	1.0064
$F^2(3d,6g)$		77.6	fixed		97.0	0.8000	
$F^4(3d,6g)$		3.9	fixed		4.9	0.8000	
3d <sup>9</sup> 7s	$E_{av}$	145697.1	20		128417.0	1.1346	
	$\zeta(3d)$	827.7	2.0	1	822.4	1.0064	
	$G^2(3d,7s)$	273.2	4	2	318.9	0.8566	
3d <sup>9</sup> 7d	$E_{av}$	152539.1	10		135114.4	1.1290	
	$\zeta(3d)$	827.9	2.0	1	822.6	1.0064	
	$\zeta(7d)$	1.9	fixed		1.9	1.0000	
	$F^2(3d,7d)$	546.1	21	5	449.4	1.2152	
	$F^4(3d,7d)$	140.5	fixed		175.6	0.8000	
	$C^0(3d,7d)$	149.8	fixed		187.2	0.8000	
	$G^2(3d,7d)$	166.8	fixed		172.4	0.8000	
	$C^4(3d,7d)$	117.6	fixed		121.8	0.8000	
	3d <sup>9</sup> 7g	$E_{av}$	155529.5	10		138096.9	1.1262
		$\zeta(3d)$	828.0	2.0	1	822.7	1.0064
$F^2(3d,7g)$		49.0	fixed		61.3	0.8000	
$F^4(3d,7g)$		2.7	fixed		3.4	0.8000	

Table 3. Cont.

Configuration	Parameter <sup>a</sup>	LSF <sup>b</sup>	STD <sup>c</sup>	Group <sup>d</sup>	HFR <sup>e</sup>	LSF/HF
<b>Even parity</b>						
3d <sup>9</sup> 8s	$E_{av}$	151604.1	20		134260.1	1.1292
	$\zeta(3d)$	827.8	2.0	1	822.5	1.0064
	$G^2(3d,8s)$	153.2	2.0	2	178.9	0.8566
3d <sup>9</sup> 8d	$E_{av}$	155694.0	14		138268.4	1.1260
	$\zeta(3d)$	827.9	2.0	1	822.6	1.0064
	$\zeta(8d)$	1.2	fixed		1.2	1.0000
	$F^2(3d,8d)$	342.5	13	5	281.9	1.2152
	$F^4(3d,8d)$	89.1	fixed		111.4	0.8000
	$G^0(3d,8d)$	95.0	fixed		118.8	0.8000
	$G^2(3d,8d)$	87.7	fixed		109.6	0.8000
	$G^4(3d,8d)$	62.0	fixed		77.5	0.8000
3d <sup>9</sup> 8g	$E_{av}$	157632.2	17		140200.6	1.1243
	$\zeta(3d)$	828.0	2.0	1	822.7	1.0064
	$F^2(3d,8g)$	32.9	fixed		41.1	0.8000
	$F^4(3d,8g)$	2.0	fixed		2.5	0.8000
3d <sup>9</sup> 9s	$E_{av}$	155106.1	20		137730.5	1.1262
	$\zeta(3d)$	827.9	2.0	1	822.6	1.0064
	$G^2(3d,9s)$	94.7	1.0	2	110.5	0.8566
3d <sup>9</sup> 9d	$E_{av}$	157752.1	14		140319.6	1.1242
	$\zeta(3d)$	828.0	2.0	1	822.7	1.0064
	$\zeta(9d)$	0.8	fixed		0.8	1.0000
	$F^2(3d,9d)$	229.1	9	5	188.5	1.2152
	$F^4(3d,9d)$	60.0	fixed		75.0	0.8000
	$G^0(3d,9d)$	64.0	fixed		80.0	0.8000
	$G^2(3d,9d)$	59.2	fixed		74.0	0.8000
	$G^4(3d,9d)$	41.8	fixed		52.2	0.8000
	3d <sup>9</sup> 9g	$E_{av}$	159073.9	17		141643.1
$\zeta(3d)$		828.0	2.0	1	822.7	1.0064
$F^2(3d,9g)$		23.1	fixed		28.9	0.8000
$F^4(3d,9g)$		1.4	fixed		1.7	0.8000
3d <sup>9</sup> 10s	$E_{av}$	157351.8	23		139959.4	1.1243
	$\zeta(3d)$	827.9	2.0	1	822.6	1.0064
	$G^2(3d,10s)$	62.5	1.0	2	73.0	0.8566
3d <sup>9</sup> 10d	$E_{av}$	159159.7	10		141729.3	1.1230
	$\zeta(3d)$	828.0	2.0	1	822.7	1.0064
	$\zeta(10d)$	0.6	fixed		0.6	1.0000
	$F^2(3d,10d)$	160.7	6	5	132.3	1.2152
	$F^4(3d,10d)$	42.3	fixed		52.9	0.8000
	$G^0(3d,10d)$	45.1	fixed		56.4	0.8000
	$G^2(3d,10d)$	41.8	fixed		52.2	0.8000
	$G^4(3d,10d)$	29.5	fixed		36.9	0.8000
3d <sup>9</sup> 10g	$E_{av}$	160104.8	17		142674.4	1.1222
	$\zeta(3d)$	828.0	2.0	1	822.7	1.0064
	$F^2(3d,10g)$	16.8	fixed		21.0	0.8000
	$F^4(3d,10g)$	1.1	fixed		1.4	0.8000
3d <sup>8</sup> 4s <sup>2</sup>	$E_{av}$	88372.4	16		62522.0	1.4135
	$F^2(3d,3d)$	91560.3	114	3	109696.0	0.8347
	$F^4(3d,3d)$	58255.9	103	4	68373.1	0.8520
	$\alpha(3d)$	93.8	3	7	0.0	
3d <sup>8</sup> 4p <sup>2</sup>	$\zeta(3d)$	892.2	3	1	886.5	1.0064
	$E_{av}$	188427.0	fixed		162579.7	1.1590
	$F^2(3d,3d)$	92340.0	115	3	110630.1	0.8347
	$F^4(3d,3d)$	58793.9	104	4	69004.6	0.8520
	$\alpha(3d)$	93.8	3	7	0.0	
	$F^2(4p,4p)$	28518.8	fixed		35648.5	0.8000
	$\zeta(3d)$	898.5	3	1	892.8	1.0064
	$\zeta(4p)$	619.0	fixed		619.0	1.0000
	$F^2(3d,4p)$	12983.5	fixed		16229.4	0.8000
	$G^1(3d,4p)$	4628.9	fixed		5786.1	0.8000
	$G^3(3d,4p)$	3922.3	fixed		4902.9	0.8000



Table 3. Cont.

Configuration	Parameter <sup>a</sup>	LSF <sup>b</sup>	STD <sup>c</sup>	Group <sup>d</sup>	HFR <sup>e</sup>	LSF/HF
<b>Even parity</b>						
3d <sup>8</sup> 4s4d	$E_{av}$	186352.1	fixed		160504.8	1.1610
	$F^2(3d,3d)$	92375.3	115	3	110672.4	0.8347
	$F^4(3d,3d)$	58816.8	104	4	69031.5	0.8520
	$\alpha(3d)$	93.8	3	7	0.0	
	$\zeta(3d)$	898.6	3	1	892.9	1.0064
	$F^2(3d,4d)$	5461.6	208	5	4494.5	1.2152
	$G^2(3d,4s)$	9256.3	144	2	10805.6	0.8566
3d <sup>8</sup> 4s5s	$E_{av}$	178348.4	fixed		152501.1	1.1695
	$F^2(3d,3d)$	92277.5	115	3	110555.2	0.8347
	$F^4(3d,3d)$	58748.9	104	4	68951.7	0.8520
	$\alpha(3d)$	93.8	3	7	0.0	
	$\zeta(3d)$	897.8	3	1	892.1	1.0064
	$G^2(3d,4s)$	9552.4	148	2	11151.3	0.8566
	$G^2(3d,5s)$	1270.3	20	2	1482.9	0.8566
3d <sup>8</sup> 4d <sup>2</sup>	$E_{av}$	307518.0	fixed		281670.7	1.0918
	$F^2(3d,3d)$	93279.6	116	3	111755.9	0.8347
	$F^4(3d,3d)$	59441.2	105	4	69764.2	0.8520
	$\alpha(3d)$	93.8	3	7	0.0	
	$\zeta(3d)$	906.0	3	1	900.2	1.0064
	$F^2(3d,4d)$	7552.1	288	5	6214.9	1.2152
	$E_{av}$	209861.7	fixed		184014.4	1.1405
3d <sup>8</sup> 4s5d	$F^2(3d,3d)$	92407.3	115	3	110710.8	0.8347
	$F^4(3d,3d)$	58838.5	104	4	69056.9	0.8520
	$\alpha(3d)$	93.8	3	7	0.0	
	$\zeta(3d)$	899.0	3	1	893.3	1.0064
	$F^2(3d,5d)$	1997.4	76	5	1643.7	1.2152
	$G^2(3d,4s)$	9429.0	147	2	11007.3	0.8566
	<b>Configuration interaction</b>					
3d <sup>9</sup> 4d-3d <sup>9</sup> 5d	$R_d^0(3d4d,3d5d)$	147.8	7	6	135.3	1.0921
	$R_d^2(3d4d,3d5d)$	2400.9	108	6	2198.4	1.0921
	$R_d^4(3d4d,3d5d)$	959.9	43	6	879.0	1.0921
	$R_e^0(3d4d,3d5d)$	1028.7	46	6	942.0	1.0921
	$R_e^2(3d4d,3d5d)$	921.6	41	6	843.9	1.0921
	$R_e^4(3d4d,3d5d)$	645.4	29	6	591.0	1.0921
3d <sup>9</sup> 4d-3d <sup>9</sup> 6d	$R_d^0(3d4d,3d6d)$	106.6	5	6	97.6	1.0921
	$R_d^2(3d4d,3d6d)$	1631.1	73	6	1493.6	1.0921
	$R_d^4(3d4d,3d6d)$	684.3	31	6	626.6	1.0921
	$R_e^0(3d4d,3d6d)$	741.5	33	6	679.0	1.0921
	$R_e^2(3d4d,3d6d)$	667.2	30	6	610.9	1.0921
	$R_e^4(3d4d,3d6d)$	467.9	21	6	428.4	1.0921
3d <sup>9</sup> 4d-3d <sup>9</sup> 7d	$R_d^0(3d4d,3d7d)$	81.5	4	6	74.6	1.0921
	$R_d^2(3d4d,3d7d)$	1212.2	54	6	1110.0	1.0921
	$R_d^4(3d4d,3d7d)$	520.2	23	6	476.3	1.0921
	$R_e^0(3d4d,3d7d)$	566.5	25	6	518.7	1.0921
	$R_e^2(3d4d,3d7d)$	510.8	23	6	467.7	1.0921
	$R_e^4(3d4d,3d7d)$	358.5	16	6	328.3	1.0921
3d <sup>9</sup> 4d-3d <sup>9</sup> 8d	$R_d^0(3d4d,3d8d)$	64.9	3	6	59.4	1.0921
	$R_d^2(3d4d,3d8d)$	950.0	43	6	869.9	1.0921
	$R_d^4(3d4d,3d8d)$	412.8	18	6	378.0	1.0921
	$R_e^0(3d4d,3d8d)$	451.0	20	6	413.0	1.0921
	$R_e^2(3d4d,3d8d)$	407.2	18	6	372.9	1.0921
	$R_e^4(3d4d,3d8d)$	286.0	13	6	261.9	1.0921
3d <sup>9</sup> 4d-3d <sup>9</sup> 9d	$R_d^0(3d4d,3d9d)$	53.2	2.0	6	48.7	1.0921
	$R_d^2(3d4d,3d9d)$	771.9	35	6	706.8	1.0921
	$R_d^4(3d4d,3d9d)$	338.0	15	6	309.5	1.0921
	$R_e^0(3d4d,3d9d)$	370.1	17	6	338.9	1.0921
	$R_e^2(3d4d,3d9d)$	334.4	15	6	306.2	1.0921
	$R_e^4(3d4d,3d9d)$	234.9	11	6	215.1	1.0921

Table 3. Cont.

Configuration	Parameter <sup>a</sup>	LSF <sup>b</sup>	STD <sup>c</sup>	Group <sup>d</sup>	HFR <sup>e</sup>	LSF/HF
<b>Configuration interaction</b>						
3d <sup>9</sup> 4d-3d <sup>9</sup> 10d	R <sub>d</sub> <sup>0</sup> (3d4d,3d10d)	44.8	2.0	6	41.0	1.0921
	R <sub>d</sub> <sup>2</sup> (3d4d,3d10d)	643.8	29	6	589.5	1.0921
	R <sub>d</sub> <sup>4</sup> (3d4d,3d10d)	283.4	13	6	259.5	1.0921
	R <sub>e</sub> <sup>0</sup> (3d4d,3d10d)	310.7	14	6	284.5	1.0921
	R <sub>e</sub> <sup>2</sup> (3d4d,3d10d)	281.0	13	6	257.3	1.0921
	R <sub>e</sub> <sup>4</sup> (3d4d,3d10d)	197.5	9	6	180.8	1.0921
3d <sup>9</sup> 5d-3d <sup>9</sup> 6d	R <sub>d</sub> <sup>2</sup> (3d5d,3d6d)	1147.0	51	6	1050.3	1.0921
	R <sub>d</sub> <sup>4</sup> (3d5d,3d6d)	454.3	20	6	416.0	1.0921
	R <sub>e</sub> <sup>0</sup> (3d5d,3d6d)	485.8	22	6	444.8	1.0921
	R <sub>e</sub> <sup>2</sup> (3d5d,3d6d)	442.4	20	6	405.1	1.0921
	R <sub>e</sub> <sup>4</sup> (3d5d,3d6d)	311.5	14	6	285.2	1.0921
	R <sub>d</sub> <sup>2</sup> (3d5d,3d7d)	850.8	38	6	779.1	1.0921
3d <sup>9</sup> 5d-3d <sup>9</sup> 7d	R <sub>d</sub> <sup>4</sup> (3d5d,3d7d)	346.3	16	6	317.1	1.0921
	R <sub>e</sub> <sup>0</sup> (3d5d,3d7d)	371.2	17	6	339.9	1.0921
	R <sub>e</sub> <sup>2</sup> (3d5d,3d7d)	339.0	15	6	310.4	1.0921
	R <sub>e</sub> <sup>4</sup> (3d5d,3d7d)	238.7	11	6	218.6	1.0921
	R <sub>d</sub> <sup>2</sup> (3d5d,3d8d)	666.6	30	6	610.4	1.0921
	R <sub>d</sub> <sup>4</sup> (3d5d,3d8d)	275.3	12	6	252.1	1.0921
3d <sup>9</sup> 5d-3d <sup>9</sup> 8d	R <sub>e</sub> <sup>0</sup> (3d5d,3d8d)	295.5	13	6	270.6	1.0921
	R <sub>e</sub> <sup>2</sup> (3d5d,3d8d)	270.3	12	6	247.5	1.0921
	R <sub>e</sub> <sup>4</sup> (3d5d,3d8d)	190.6	9	6	174.5	1.0921
	R <sub>d</sub> <sup>2</sup> (3d5d,3d9d)	541.3	24	6	495.7	1.0921
	R <sub>d</sub> <sup>4</sup> (3d5d,3d9d)	225.8	10	6	206.8	1.0921
	R <sub>e</sub> <sup>0</sup> (3d5d,3d9d)	242.4	11	6	222.0	1.0921
3d <sup>9</sup> 5d-3d <sup>9</sup> 9d	R <sub>e</sub> <sup>2</sup> (3d5d,3d9d)	222.0	10	6	203.3	1.0921
	R <sub>e</sub> <sup>4</sup> (3d5d,3d9d)	156.6	7	6	143.4	1.0921
	R <sub>d</sub> <sup>2</sup> (3d5d,3d10d)	451.6	20	6	413.5	1.0921
	R <sub>d</sub> <sup>4</sup> (3d5d,3d10d)	189.4	8	6	173.4	1.0921
	R <sub>e</sub> <sup>0</sup> (3d5d,3d10d)	203.7	9	6	186.5	1.0921
	R <sub>e</sub> <sup>2</sup> (3d5d,3d10d)	186.4	8	6	170.7	1.0921
3d <sup>9</sup> 6d-3d <sup>9</sup> 7d	R <sub>e</sub> <sup>4</sup> (3d5d,3d10d)	131.6	6	6	120.5	1.0921
	R <sub>d</sub> <sup>2</sup> (3d6d,3d7d)	631.0	28	6	577.8	1.0921
	R <sub>d</sub> <sup>4</sup> (3d6d,3d7d)	250.7	11	6	229.6	1.0921
	R <sub>e</sub> <sup>0</sup> (3d6d,3d7d)	267.7	12	6	245.1	1.0921
	R <sub>e</sub> <sup>2</sup> (3d6d,3d7d)	245.7	11	6	225.0	1.0921
	R <sub>e</sub> <sup>4</sup> (3d6d,3d7d)	173.4	8	6	158.8	1.0921
3d <sup>9</sup> 6d-3d <sup>9</sup> 8d	R <sub>d</sub> <sup>2</sup> (3d6d,3d8d)	494.0	22	6	452.3	1.0921
	R <sub>d</sub> <sup>4</sup> (3d6d,3d8d)	199.6	9	6	182.8	1.0921
	R <sub>e</sub> <sup>0</sup> (3d6d,3d8d)	213.3	10	6	195.3	1.0921
	R <sub>e</sub> <sup>2</sup> (3d6d,3d8d)	196.0	9	6	179.5	1.0921
	R <sub>e</sub> <sup>4</sup> (3d6d,3d8d)	138.5	6	6	126.8	1.0921
	R <sub>d</sub> <sup>2</sup> (3d6d,3d9d)	401.0	18	6	367.2	1.0921
3d <sup>9</sup> 6d-3d <sup>9</sup> 9d	R <sub>d</sub> <sup>4</sup> (3d6d,3d9d)	163.7	7	6	149.9	1.0921
	R <sub>e</sub> <sup>0</sup> (3d6d,3d9d)	175.1	8	6	160.3	1.0921
	R <sub>e</sub> <sup>2</sup> (3d6d,3d9d)	161.0	7	6	147.4	1.0921
	R <sub>e</sub> <sup>4</sup> (3d6d,3d9d)	113.7	5	6	104.1	1.0921
	R <sub>d</sub> <sup>2</sup> (3d6d,3d10d)	334.6	15	6	306.4	1.0921
	R <sub>d</sub> <sup>4</sup> (3d6d,3d10d)	137.3	6	6	125.7	1.0921
3d <sup>9</sup> 6d-3d <sup>9</sup> 10d	R <sub>e</sub> <sup>0</sup> (3d6d,3d10d)	146.9	7	6	134.5	1.0921
	R <sub>e</sub> <sup>2</sup> (3d6d,3d10d)	135.3	6	6	123.9	1.0921
	R <sub>e</sub> <sup>4</sup> (3d6d,3d10d)	95.6	4	6	87.5	1.0921
	R <sub>d</sub> <sup>2</sup> (3d7d,3d8d)	382.7	17	6	350.4	1.0921
	R <sub>d</sub> <sup>4</sup> (3d7d,3d8d)	152.8	7	6	139.9	1.0921
	R <sub>e</sub> <sup>0</sup> (3d7d,3d8d)	163.0	7	6	149.3	1.0921
3d <sup>9</sup> 7d-3d <sup>9</sup> 8d	R <sub>e</sub> <sup>2</sup> (3d7d,3d8d)	150.2	7	6	137.5	1.0921
	R <sub>e</sub> <sup>4</sup> (3d7d,3d8d)	106.0	5	6	97.1	1.0921

Table 3. Cont.

Configuration	Parameter <sup>a</sup>	LSF <sup>b</sup>	STD <sup>c</sup>	Group <sup>d</sup>	HFR <sup>e</sup>	LSF/HF
<b>Configuration interaction</b>						
3d <sup>9</sup> 7d-3d <sup>9</sup> d	R <sub>d</sub> <sup>2</sup> (3d7d,3d9d)	310.7	14	6	284.5	1.0921
	R <sub>d</sub> <sup>4</sup> (3d7d,3d9d)	125.4	6	6	114.8	1.0921
	R <sub>e</sub> <sup>0</sup> (3d7d,3d9d)	133.7	6	6	122.4	1.0921
	R <sub>e</sub> <sup>2</sup> (3d7d,3d9d)	123.4	6	6	113.0	1.0921
	R <sub>e</sub> <sup>4</sup> (3d7d,3d9d)	87.3	4	6	79.9	1.0921
3d <sup>9</sup> 7d-3d <sup>9</sup> 10d	R <sub>d</sub> <sup>2</sup> (3d7d,3d10d)	259.2	12	6	237.3	1.0921
	R <sub>d</sub> <sup>4</sup> (3d7d,3d10d)	105.3	5	6	96.4	1.0921
	R <sub>e</sub> <sup>0</sup> (3d7d,3d10d)	112.3	5	6	102.8	1.0921
	R <sub>e</sub> <sup>2</sup> (3d7d,3d10d)	103.6	5	6	94.9	1.0921
	R <sub>e</sub> <sup>4</sup> (3d7d,3d10d)	73.3	3	6	67.1	1.0921
3d <sup>9</sup> 8d-3d <sup>9</sup> d	R <sub>d</sub> <sup>2</sup> (3d8d,3d9d)	249.3	11	6	228.3	1.0921
	R <sub>d</sub> <sup>4</sup> (3d8d,3d9d)	99.9	4	6	91.5	1.0921
	R <sub>e</sub> <sup>0</sup> (3d8d,3d9d)	106.5	5	6	97.5	1.0921
	R <sub>e</sub> <sup>2</sup> (3d8d,3d9d)	98.4	4	6	90.1	1.0921
	R <sub>e</sub> <sup>4</sup> (3d8d,3d9d)	69.6	3	6	63.7	1.0921
3d <sup>9</sup> 8d-3d <sup>9</sup> 10d	R <sub>d</sub> <sup>2</sup> (3d8d,3d10d)	207.8	9	6	190.3	1.0921
	R <sub>d</sub> <sup>4</sup> (3d8d,3d10d)	83.9	4	6	76.8	1.0921
	R <sub>e</sub> <sup>0</sup> (3d8d,3d10d)	89.4	4	6	81.9	1.0921
	R <sub>e</sub> <sup>2</sup> (3d8d,3d10d)	82.8	4	6	75.8	1.0921
	R <sub>e</sub> <sup>4</sup> (3d8d,3d10d)	58.5	3	6	53.6	1.0921
3d <sup>9</sup> 9d-3d <sup>9</sup> 10d	R <sub>d</sub> <sup>2</sup> (3d9d,3d10d)	171.3	8	6	156.9	1.0921
	R <sub>d</sub> <sup>4</sup> (3d9d,3d10d)	68.8	3	6	63.0	1.0921
	R <sub>e</sub> <sup>0</sup> (3d9d,3d10d)	73.3	3	6	67.1	1.0921
	R <sub>e</sub> <sup>2</sup> (3d9d,3d10d)	67.9	3	6	62.2	1.0921
	R <sub>e</sub> <sup>4</sup> (3d9d,3d10d)	48.1	2.0	6	44.0	1.0921
<b>Odd parity</b>						
3d <sup>9</sup> 4p	E <sub>av</sub>	73281.0	22		53995.6	1.3572
	ζ(3d)	828.8	5	1	818.3	1.0128
	ζ(4p)	538.0	20	9	444.2	1.2112
	F <sup>2</sup> (3d,4p)	13098.9	152		13901.7	0.9423
	G <sup>1</sup> (3d,4p)	4368.5	65		5338.7	0.8183
3d <sup>9</sup> 4f	C <sup>3</sup> (3d,4p)	3615.9	363		4299.1	0.8411
	E <sub>av</sub>	136895.6	17		119289.7	1.1476
3d <sup>9</sup> 5p	ζ(3d)	833.2	5	1	822.7	1.0128
	E <sub>av</sub>	121911.6	24		104871.2	1.1625
	ζ(3d)	832.0	5	1	821.5	1.0128
	ζ(5p)	159.8	6	9	131.9	1.2112
	F <sup>2</sup> (3d,5p)	3512.5	21	2	3548.4	0.9899
3d <sup>9</sup> 5f	C <sup>1</sup> (3d,5p)	1262.1	94	3	1287.6	0.9802
	C <sup>3</sup> (3d,5p)	1174.4	306	10	1102.4	1.0653
	E <sub>av</sub>	146833.4	16		129308.6	1.1355
3d <sup>9</sup> 6p	ζ(3d)	833.2	5	1	822.7	1.0128
	E <sub>av</sub>	139748.8	29		122652.3	1.1394
	ζ(3d)	832.7	5	1	822.2	1.0128
	ζ(6p)	69.9	3	9	57.7	1.2112
	F <sup>2</sup> (3d,6p)	1443.6	9	2	1458.4	0.9899
3d <sup>9</sup> 6f	C <sup>1</sup> (3d,6p)	521.8	39	3	532.4	0.9802
	C <sup>3</sup> (3d,6p)	493.4	129	10	463.1	1.0653
	E <sub>av</sub>	152224.4	17		134753.4	1.1297
3d <sup>9</sup> 6h	ζ(3d)	833.2	5	1	822.7	1.0128
	E <sub>av</sub>	152299.5	16		134875.8	1.1292
3d <sup>9</sup> 7p	ζ(3d)	833.2	5	1	822.7	1.0128
	E <sub>av</sub>	148438.8	22		131122.8	1.1321
	ζ(3d)	833.0	5	1	822.5	1.0128
	ζ(7p)	36.8	1.0	9	30.4	1.2112
	F <sup>2</sup> (3d,7p)	738.7	4	2	746.3	0.9899
	C <sup>1</sup> (3d,7p)	268.6	20	3	274.0	0.9802
	C <sup>3</sup> (3d,7p)	255.8	67	10	240.1	1.0653

Table 3. Cont.

Configuration	Parameter <sup>a</sup>	LSF <sup>b</sup>	STD <sup>c</sup>	Group <sup>d</sup>	HFR <sup>e</sup>	LSF/HF
<b>Odd parity</b>						
3d <sup>9</sup> 7f	$E_{av}$	155498.8	22		138032.9	1.1265
	$\zeta(3d)$	833.2	5	1	822.7	1.0128
3d <sup>9</sup> 7h	$E_{av}$	155540.7	21		138110.8	1.1262
	$\zeta(3d)$	833.2	5	1	822.7	1.0128
3d <sup>9</sup> 8p	$E_{av}$	153145.3	54		135833.1	1.1275
	$\zeta(3d)$	833.1	5	1	822.6	1.0128
	$\zeta(8p)$	21.8	1.0	9	18.0	1.2112
	$F^2(3d,8p)$	429.6	3	2	434.0	0.9899
	$G^1(3d,8p)$	156.8	12	3	160.0	0.9802
	$G^3(3d,8p)$	150.0	39	10	140.8	1.0653
	$E_{av}$	157610.4	28		140157.8	1.1245
3d <sup>9</sup> 8f	$\zeta(3d)$	833.2	5	1	822.7	1.0128
	$E_{av}$	157629.5	26		140210.6	1.1242
3d <sup>9</sup> 8h	$\zeta(3d)$	833.2	5	1	822.7	1.0128
	$E_{av}$	132837.3	12		104548.6	1.2706
3d <sup>8</sup> 4s4p	$F^2(3d,3d)$	92783.8	119	4	110131.5	0.8425
	$F^4(3d,3d)$	59745.4	207	5	68667.5	0.8701
	$\alpha(3d)$	84.8	3	8	0.0	
	$\zeta(3d)$	900.8	5	1	889.4	1.0128
	$\zeta(4p)$	732.4	27	9	604.7	1.2112
	$F^2(3d,4p)$	15857.7	94	2	16019.7	0.9899
	$G^2(3d,4s)$	8059.3	145	7	10125.0	0.7960
	$G^1(3d,4p)$	5532.7	82	11	5751.7	0.9619
	$G^3(3d,4p)$	4703.6	208	12	4854.4	0.9689
	$G^1(4s,4p)$	37321.3	52	6	47726.6	0.7820
	$E_{av}$	211778.8	fixed		183501.6	1.1541
	$F^2(3d,3d)$	93301.4	119	4	110745.9	0.8425
	$F^4(3d,3d)$	60104.6	208	5	69080.2	0.8701
	$\alpha(3d)$	84.8	3	8	0.0	
$\zeta(3d)$	905.0	5	1	893.6	1.0128	
$G^2(3d,4s)$	8816.3	158	7	11076.0	0.7960	
3d <sup>8</sup> 4p4d	$E_{av}$	244758.6	fixed		216481.4	1.1306
	$F^2(3d,3d)$	93638.6	120	4	111146.1	0.8425
	$F^4(3d,3d)$	60341.3	209	5	69352.4	0.8701
	$\alpha(3d)$	84.8	3	8	0.0	
	$\zeta(3d)$	907.5	5	1	896.1	1.0128
	$\zeta(4p)$	873.4	33	9	721.1	1.2112
	$F^2(3d,4p)$	17746.3	105	2	17927.6	0.9899
	$G^1(3d,4p)$	6222.8	92	11	6469.1	0.9619
	$G^3(3d,4p)$	5367.4	237	12	5539.4	0.9689
	$E_{av}$	195045.6	fixed		166768.4	1.1696
	$F^2(3d,3d)$	93179.2	119	4	110600.7	0.8425
	$F^4(3d,3d)$	60019.6	208	5	68982.6	0.8701
	$\alpha(3d)$	84.8	3	8	0.0	
	$\zeta(3d)$	903.9	5	1	892.5	1.0128
$\zeta(5p)$	182.9	7	9	151.0	1.2112	
$F^2(3d,5p)$	3559.6	21	2	3596.0	0.9899	
$G^2(3d,4s)$	8773.2	158	7	11021.9	0.7960	
$G^1(3d,5p)$	1184.8	89	3	1208.8	0.9802	
$G^3(3d,5p)$	1145.1	298	10	1074.9	1.0653	
$G^1(4s,5p)$	4181.2	6	6	5346.9	0.7820	

Table 3. Cont.

Configuration	Parameter <sup>a</sup>	LSF <sup>b</sup>	STD <sup>c</sup>	Group <sup>d</sup>	HFR <sup>e</sup>	LSF/HF
<b>Odd parity</b>						
3d <sup>8</sup> 4s5f	$E_{av}$	222119.6	fixed		193842.4	1.1459
	$F^2(3d,3d)$	93300.7	119	4	110745.0	0.8425
	$F^4(3d,3d)$	60104.1	208	5	69079.8	0.8701
	$\alpha(3d)$	84.8	3	8	0.0	
	$\zeta(3d)$	905.0	5	1	893.6	1.0128
	$G^2(3d,4s)$	8827.6	159	7	11090.3	0.7960

<sup>a</sup> All omitted single-configuration parameters were fixed at HFR values scaled by a factor of 0.80 for the direct and exchange electrostatic parameters  $F^k$  and  $G^k$ , and 1.0 for spin-orbit parameters  $\zeta$ . All omitted configuration-interaction parameters were fixed at HFR values scaled by a factor of 0.94 in both parities;

<sup>b</sup> Parameter values determined in the least-squares fitting procedure (see Section 3);

<sup>c</sup> Standard deviation of the least-squares fitting;

<sup>d</sup> Parameters within each numbered group were linked together in the LSF procedure, so that the ratios to ab initio HFR values were the same for each parameter in the group;

<sup>e</sup> The ab initio Hartree-Fock-Relativistic parameter values as computed by Cowan's codes [52]. In this calculation, we included both relativistic and Breit corrections (in Cowan's codes, the latter affect only the average energies of configurations) and used the scaling factor of 1.0 for the exchange contribution.

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# The Third Spectrum of Indium: In III

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Academic Editor: Joseph Reader

Received: 1 February 2017; Accepted: 5 June 2017; Published: 13 June 2017

**Abstract:** The present investigation reports on the extended study of the third spectrum of indium (In III). This spectrum was previously analyzed in many articles, but, nevertheless, this study represents a significant extension of the previous analyses. The main new contribution is connected to the observation of transitions involving core-excited configurations. Previous data are critically evaluated and in some cases are corrected. The spectra were recorded on 3-m as well as on 10.7-m normal incidence spectrographs using a triggered spark source. Theoretical calculations were made with Cowan's code. The analysis results in the identifications of 70 spectral lines and determination of 24 new energy levels. In addition, the manuscript represents a compilation of all presently available data on In III.

**Keywords:** spectra; ionized atoms; wavelengths; energy levels; ionization energies

## 1. Introduction

The third spectrum of indium (In III) belongs to the Ag I isoelectronic sequence with the ground state  $[\text{Kr}] 4d^{10}5s^2S_{1/2}$ . The outer electronic excitation gives rise to the  $[\text{Kr}] 4d^{10}n\ell$  ( $n \geq 5$ , for  $\ell \leq 2$ ;  $n \geq \ell + 1$  otherwise) type of configurations with a simple doublet structure, while core excitation involving the configurations such as  $4d^95s$  ( $5p + 4f$ ),  $4d^95s^2$  and  $4d^95p^2$  makes a complex three-electron system having both doublet and quartet terms.

Several authors studied the In III spectrum, and it is appropriate to summarize their work briefly. The first work on the third spectrum of indium was done by Rao et al. [1], followed by Lang [2], Douglas [3] and Nodwell [4]. Rao et al. [1] identified 12 lines in the wavelength region 2983–5918 Å and established 13 levels belonging to the  $4d^{10}(5s, 6s, 7s, 5p, 6p, 5d, 6d, 4f, 5f \text{ and } 5g)$  configurations. However, only six of those levels could be verified by later workers [2–4]. Nodwell [4] studied the indium spectrum in more detail. He recorded the indium spectra on a 2-m vacuum grating spectrograph and identified 56 lines of In III in the wavelength region 685–6198 Å. He established 27 energy levels including six doubtful. This work is listed in the Atomic Energy Levels (AEL) compilation [5]. Bhatia [6] investigated the In III spectrum more comprehensively using a 3-m normal incidence vacuum spectrograph in the range 340–2300 Å with a 1200 lines/mm grating giving a reciprocal dispersion of 2.775 Å/mm and a prism spectrograph in the region 2300 Å to 9500 Å with a disruptive electrodeless discharge. He revised and extended the earlier analysis and established the levels of the  $4d^{10}ns$  ( $n = 5-12$ ),  $4d^{10}np$  ( $n = 5-9$ ),  $4d^{10}nd$  ( $n = 5-9$ ),  $4d^{10}nf$  ( $n = 4-7$ ),  $4d^{10}ng$  ( $n = 5-9$ ),  $4d^{10}nh$  ( $n = 6-9$ ),  $4d^95s^2$ , and  $4d^95s5p$  configurations. Kaufman et al. [7] studied the core-excited transition array  $4d^{10}5s-4d^95s5p$  in the isoelectronic sequence from In III to Te VI. The spectra were recorded on 10.7-m normal and grazing incidence spectrographs using a sliding spark source. Out of 23 possible levels of the  $4d^95s5p$  configuration, they reported only 10 that can combine with the ground level  $4d^{10}5s^2S_{1/2}$ . Kilbane et al. [8] studied photoabsorption spectra of In II–IV with a dual laser plasma (DLP) technique. They reported the  $4d^{10}5s-\{4d^95snp$  ( $n = 6-11$ ) +  $4d^95snf$  ( $n = 4-11$ ) transition array. They could not observe the  $4d^{10}5s-4d^95s5p$  transitions as they lie beyond the region



of their investigation. Recently, Ryabtsev et al. [9] added a new configuration  $4d^9 5p^2$  to the In III-Te VI sequence and observed the  $4d^{10} 5p-4d^9 5p^2$  transition array in the range 250–600 Å using a 6.65-m normal incidence spectrograph equipped with a 1200 lines/mm grating giving a reciprocal linear dispersion of 1.25 Å/mm. They were able to determine only 13 levels out of 28 levels of the  $4d^9 5p^2$  configuration. Skočić et al. [10] studied Stark shifts of some prominent lines of In III ( $6s-6p$ ,  $6p-6d$ , and  $4f-5d$ ).

As mentioned above, a number of publications on In III appeared in the literature [1–11]. Among these, Bhatia’s [6] analysis was the most comprehensive and contained a large number of one-electron configurations. However, after careful examination of these results, a number of irregularities were noticed in Bhatia’s results, for example, many lines classified did not match the In III characteristics on our recorded spectra and 17 reported lines have incorrect conversion between wavenumbers and wavelengths. Moreover, the levels of the  $4d^9 5s 5p$  configuration reported by Kaufman et al. [7] and the levels of  $4d^9 5p^2$  configuration established by Ryabtsev et al. [9] are still incomplete. These facts prompted us to re-investigate the In III spectrum in detail. A Grotrian energy level diagram of In III is illustrated in Figure 1 showing the basic configurations and possible transition between them.

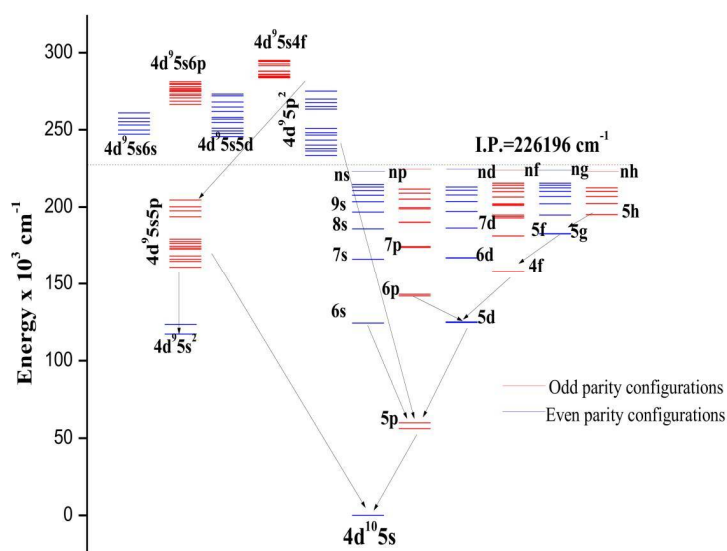


Figure 1. Grotrian diagram of In III. “I.P.” denotes the ionization potential (see Section 6). Arrows denote the observed transition arrays.

## 2. Experiment Detail

The spectra were recorded at two different places. A 3-m vacuum spectrograph equipped with 2400 lines per mm holographic grating was employed at Antigonish laboratory in Nova Scotia, Canada with a triggered spark source to cover the wavelength region 350–2080 Å. This spectrograph gives the first order inverse dispersion of 1.385 Å/mm. For ionization separation of the spectral lines, either the charging potential of the source was varied or an inductance with a varying number of turns was inserted in series in the circuit. The charging unit was a 14.5 μF low inductance fast charging capacitor and the charging potential was varied between 2 and 6 kV. Y.N. Joshi of St. Francis Xavier University, Antigonish (Canada) provided the indium spectra that were recorded on the 10.7-m normal incidence vacuum spectrograph of the National Institute of Standards and Technology (NIST) also using a triggered spark source. The NIST spectrograph was equipped with 1200 lines/mm grating with

an inverse dispersion 0.78 Å/mm. The spectrograms were measured either on an *Abbec* comparator at Aligarh or on a semi-automatic Grant’s comparator in Antigonish, Canada. Known standard lines of oxygen, carbon, aluminium and silicon [11] were used as internal standards for the calibration of wavelengths. We estimated our measurements uncertainty for sharp and unblended lines to be within ±0.006 Å for wavelength below 900 Å and ±0.008 Å above that.

### 3. Theoretical Calculations

The ab initio calculations were performed by the Hartree–Fock method with relativistic corrections using Cowan code [12] with superposition of configurations including 4d<sup>10</sup>*ns* (*n* = 5–12), 4d<sup>10</sup>*nd* (*n* = 5–9), 4d<sup>10</sup>*ng* (*n* = 5–9), 4d<sup>9</sup>(5s<sup>2</sup> + 5p<sup>2</sup>), 4d<sup>9</sup>5s(5d + 6s) configurations for the even parity system and 4d<sup>10</sup>*np* (*n* = 5–9), 4d<sup>10</sup>*nf* (*n* = 4–7), 4d<sup>10</sup>*nh* (*n* = 6–9), 4d<sup>9</sup>5s*np* (*n* = 5–11), 4d<sup>9</sup>5s*nf* (*n* = 4–12), 4d<sup>8</sup>5s<sup>2</sup>5p for the odd parity matrix involving a total of 52 configurations in our calculations. The initial scaling of the Slater energy parameters was kept at 100% of the Hartree–Fock values for *E*<sub>av</sub> and ζ<sub>*nl*</sub>, 85% for *F*<sup>*k*</sup>, and 80% for the *G*<sup>*k*</sup> as well as *R*<sup>*k*</sup> integrals. These parameters were more refined at a later stage as least squares fitted parametric calculations were performed. The main output from these programs includes the values of energy levels, wavelengths, weighted transition rates and weighted oscillator strengths. The transition probability of lines depends on the line strength and is greatly affected by the cancellation factor [13], is also calculated by Cowan’s code programs [12]. The Hartree–Fock (HFR) and least-squares-fitted (LSF) energy parameters used in the present calculations are given in Table 1 along with their scaling factor (ratio of the LSF value to the HFR value) of the parameters. The standard deviations for the even and odd parity systems are 172 cm<sup>−1</sup> and 216 cm<sup>−1</sup>, respectively.

**Table 1.** Least Square Fitted (LSF) Energy Parameters (in cm<sup>−1</sup>) for In III.

Configuration	Parameters <sup>a</sup>	LSF	STD <sup>#</sup>	Group <sup>b</sup>	HFR	LSF/HFR
<b>Even Parity</b>						
5s	<i>E</i> <sub>av</sub>	1525.6	247		1560.9	0.9774
6s	<i>E</i> <sub>av</sub>	126,947.0	245		124,323.4	1.0211
7s	<i>E</i> <sub>av</sub>	169,472.1	245		166,231.3	1.0195
8s	<i>E</i> <sub>av</sub>	189,397.9	245		185,887.2	1.0189
9s	<i>E</i> <sub>av</sub>	200,378.4	245		196,742.7	1.0185
10s	<i>E</i> <sub>av</sub>	207,041.1	139	1	203,380.9	1.0180
11s	<i>E</i> <sub>av</sub>	211,473.3	142	1	207,734.7	1.0180
12s	<i>E</i> <sub>av</sub>	214,537.1	144	1	210,744.4	1.0180
13s	<i>E</i> <sub>av</sub>	216,749.1	145	1	212,917.3	1.0180
14s	<i>E</i> <sub>av</sub>	218,395.3	147	1	214,534.4	1.0180
5d	<i>E</i> <sub>av</sub>	128,785.8	179		124,706.2	1.0327
	ζ(5d)	149.6	125	3	120.5	1.2415
6d	<i>E</i> <sub>av</sub>	170,730.6	174		167,143.9	1.0215
	ζ(6d)	65.7	55	3	52.9	1.2420
7d	<i>E</i> <sub>av</sub>	190,146.5	174		186,483.2	1.0196
	ζ(7d)	35.0	29	3	28.2	1.2411
8d	<i>E</i> <sub>av</sub>	200,844.9	174		197,127.9	1.0189
	ζ(8d)	20.9	17	3	16.8	1.2440
9d	<i>E</i> <sub>av</sub>	207,385.2	174	2	203,639.2	1.0184
	ζ(9d)	13.4	11	3	10.8	1.2407
10d	<i>E</i> <sub>av</sub>	211,739.0	177	2	207,914.3	1.0184
	ζ(10d)	9.1	8	3	7.3	1.2466
11d	<i>E</i> <sub>av</sub>	214,754.5	180	2	210,875.3	1.0184
	ζ(11d)	6.5	5	3	5.2	1.2500
12d	<i>E</i> <sub>av</sub>	216,933.8	182	2	213,015.3	1.0184
	ζ(12d)	4.7	4	3	3.8	1.2368
5g	<i>E</i> <sub>av</sub>	186,530.4	173		182,689.5	1.0210
	ζ(5d)	0.3	Fixed		0.3	1.0000
6g	<i>E</i> <sub>av</sub>	198,656.5	173		194,809.9	1.0197
	ζ(5d)	0.2	Fixed		0.2	1.0000

Table 1. Cont.

Configuration	Parameters <sup>a</sup>	LSF	STD #	Group <sup>b</sup>	HFR	LSF/HFR
7g	$E_{av}$	205,968.6	173		202,130.8	1.0190
	$\zeta(5d)$	0.1	Fixed		0.1	1.0000
8g	$E_{av}$	210,713.4	173		206,885.7	1.0185
	$\zeta(5d)$	0.1	Fixed		0.1	1.0000
9g	$E_{av}$	213,967.7	173	4	210,144.3	1.0182
	$\zeta(5d)$	0.0	Fixed		0.0	
10g	$E_{av}$	216,340.0	175	4	212,474.2	1.0182
	$\zeta(5d)$	0.0	Fixed		0.0	
11g	$E_{av}$	218,091.5	177	4	214,194.4	1.0182
	$\zeta(11g)$	0.0	Fixed		0.0	
12g	$E_{av}$	219,428.0	178	4	215,507.0	1.0182
	$\zeta(12g)$	0.0	Fixed		0.0	
4d <sup>9</sup> 5s <sup>2</sup>	$E_{av}$	122,546.3	196		124,206.8	0.9866
	$\zeta(4d)$	2827.6	53	5	2706.2	1.0449
4d <sup>9</sup> 5p <sup>2</sup>	$E_{av}$	248,495.0	551		246,591.5	1.0077
	$F^2(5p,5p)$	27,409.1	4453		39,408.9	0.6955
	$\zeta(4d)$	2855.5	54	5	2732.9	1.0449
	$\zeta(5p)$	3648.0	138		2988.1	1.2208
	$F^2(4d,5p)$	20,103.9	530		24,204.1	0.8306
	$G^1(4d,5p)$	6453.4	Fixed		7592.2	0.8500
	$G^3(4d,5p)$	5725.3	Fixed		6735.6	0.8500
4d <sup>9</sup> 5s5d *	$E_{av}$	262,301.3	2850		253,437.2	1.0350
4d <sup>9</sup> 5s6s *	$E_{av}$	252,606.4	Fixed		252,606.4	1.0000
	$\sigma^{\#}$	172				
<b>Odd Parity</b>						
5p	$E_{av}$	60,352.9	42	1	59,151.7	1.0203
	$\zeta(5p)$	2671.6	242	2	2505.1	1.0665
6p	$E_{av}$	145,688.0	103	1	142,788.3	1.0203
	$\zeta(6p)$	863.2	78	2	809.4	1.0665
7p	$E_{av}$	178,073.7	125	1	174,529.4	1.0203
	$\zeta(7p)$	396.3	36	2	371.6	1.0665
8p	$E_{av}$	194,213.5	137	1	190,348.0	1.0203
	$\zeta(8p)$	216.2	20	2	202.7	1.0666
9p	$E_{av}$	203,466.4	143	1	199,416.7	1.0203
	$\zeta(9p)$	131.0	12	2	122.8	1.0668
10p	$E_{av}$	209,274.8	147	1	205,109.5	1.0203
	$\zeta(10p)$	85.4	8	2	80.1	1.0662
11p	$E_{av}$	213,160.3	150	1	208,917.6	1.0203
	$\zeta(11p)$	58.8	5	2	55.1	1.0672
12p	$E_{av}$	215,887.1	152	1	211,590.2	1.0203
	$\zeta(12p)$	42.1	4	2	39.5	1.0658
4f	$E_{av}$	162,121.7	202		158,107.9	1.0254
	$\zeta(4f)$	1.2	Fixed		1.2	1.0000
5f	$E_{av}$	185,069.7	206		181,299.2	1.0208
	$\zeta(5f)$	0.8	Fixed		0.8	1.0000
6f	$E_{av}$	191,442.6	406	3	193,937.2	0.9871
	$\zeta(6f)$	0.5	Fixed		0.5	1.0000
7f	$E_{av}$	198,958.4	422	3	201,550.9	0.9871
	$\zeta(7f)$	0.3	Fixed		0.3	1.0000
8f	$E_{av}$	203,826.5	432	3	206,482.5	0.9871
	$\zeta(8f)$	0.2	Fixed		0.2	1.0000
9f	$E_{av}$	207,155.3	439	3	209,854.6	0.9871
	$\zeta(9f)$	0.2	Fixed		0.2	1.0000
10f	$E_{av}$	209,529.7	445	3	212,260.0	0.9871
	$\zeta(10f)$	0.1	Fixed		0.1	1.0000
11f	$E_{av}$	211,278.0	448	3	214,031.1	0.9871
	$\zeta(11f)$	0.1	Fixed		0.1	1.0000
12f	$E_{av}$	212,609.0	451	3	215,379.4	0.9871
	$\zeta(12f)$	0.1	Fixed		0.1	1.0000
6h	$E_{av}$	198,520.8	109	4	194,930.4	1.0184
	$\zeta(6h)$	0.1	Fixed		0.1	1.0000
7h	$E_{av}$	205,935.4	113	4	202,210.9	1.0184
	$\zeta(7h)$	0.1	Fixed		0.1	1.0000

Table 1. Cont.

Configuration	Parameters <sup>a</sup>	LSF	STD <sup>#</sup>	Group <sup>b</sup>	HFR	LSF/HFR
8h	$E_{av}$	210,752.2	116	4	206,940.6	1.0184
	$\zeta(8h)$	0.1	Fixed		0.1	1.0000
9h	$E_{av}$	214,053.7	118	4	210,182.4	1.0184
	$\zeta(9h)$	0.0	Fixed		0.0	
10h	$E_{av}$	216,415.1	119	4	212,501.1	1.0184
	$\zeta(10h)$	0.0	Fixed		0.0	
4d <sup>9</sup> 5s5p	$E_{av}$	179,088.7	71	5	177,339.0	1.0099
	$\zeta(4d)$	2747.9	79		2718.8	1.0107
	$\zeta(5p)$	3591.3	175		2994.7	1.1992
	$F^2(4d,5p)$	196,94.2	839		24,199.1	0.8138
	$G^2(4d,5s)$	12,656.6	1434		13,315.8	0.9505
	$G^1(4d,5p)$	7671.9	563		7655.9	1.0021
	$G^3(4d,5p)$	6794.6	499		6780.4	1.0021
	$G^1(5s,5p)$	33,087.5	270		48,386.8	0.6838
4d <sup>9</sup> 5s6p	$E_{av}$	275,446.9	127	5	272,620.0	1.0104
	$\sigma^{\#}$	216				

<sup>a</sup> All configuration-interaction parameters  $R^k$  for even and odd parity configurations were fixed at 80% of the Hartree–Fock value. <sup>b</sup> Parameters in each numbered group were linked together with their ratio fixed at the Hartree–Fock level. <sup>#</sup>  $\sigma$  and STD are the standard deviations of the fit for the levels and parameters, respectively. \* Only  $E_{av}$  of unobserved interacting configurations are given.

#### 4. Spectrum Analysis

The initial approach of the analysis was to identify In III lines with correct ionization character. A computer code FIND3 [14] was useful in the analysis to search for new levels. A total of 91 levels have been established, of which 24 are new; they are assembled in Table 2 along with least squares fitted values and LS percentage composition. Two hundred fifty-one lines have been classified in In III and they are given in Table 3 along with their transition probabilities. In the present analysis, apart from the one- electron spectrum 4d<sup>10</sup> $n\ell$ , the configurations involving inner-shell excitation, such as 4d<sup>9</sup>5s (5p + 4f), 4d<sup>9</sup>5s<sup>2</sup> and 4d<sup>9</sup>5p<sup>2</sup> have also been studied extensively. The following sections describe them in detail.

Table 2. Optimized energy levels of in III.

LS Compositions <sup>d</sup>									
<i>J</i>	Energy <sup>a</sup> cm <sup>-1</sup>	Unc <sup>b</sup>	$\Delta E_{oe-c}$ cm <sup>-1</sup>	1st Component	2nd Component	3rd Component	No. of Lines <sup>e</sup>	Lev. Ref. f	
Even Parity									
0.5	0.00	0.3	0	99	4d <sup>10</sup> s	<sup>2</sup> S			
2.5	115,572.19	0.25	71	97	4d <sup>9</sup> 5s <sup>2</sup>	<sup>2</sup> D	3	4d <sup>9</sup> 5p <sup>2</sup> ( <sup>1</sup> S) <sup>2</sup> D	B*
1.5	122,419.73	0.22	-74	95	4d <sup>9</sup> 5s <sup>2</sup>	<sup>2</sup> D	3	4d <sup>9</sup> 5p <sup>2</sup> ( <sup>1</sup> S) <sup>2</sup> D	B*
0.5	126,879.89	0.24	0	100	4d <sup>10</sup> 6s	<sup>2</sup> S			B*
1.5	128,458.36	0.23	6	97	4d <sup>10</sup> 5d	<sup>2</sup> D	2	4d <sup>9</sup> 5s <sup>2</sup> <sup>2</sup> D	B*
2.5	128,748.33	0.25	-6	99	4d <sup>10</sup> 5d	<sup>2</sup> D			B*
0.5	169,434.59	0.25	0	100	4d <sup>10</sup> 7s	<sup>2</sup> S			B*
1.5	170,555.76	0.24	-8	100	4d <sup>10</sup> 6d	<sup>2</sup> D			B*
2.5	170,7718.81	0.3	8	100	4d <sup>10</sup> 6d	<sup>2</sup> D			B*
3.5	186,527.40	0.3	0	100	4d <sup>10</sup> 5g	<sup>2</sup> G			B*
4.5	186,528.26	0.3	-1	100	4d <sup>10</sup> 5g	<sup>2</sup> G			B*
0.5	189,374.5	0.3	1	100	4d <sup>10</sup> 8s	<sup>2</sup> S			B*
1.5	190,038.8	0.3	-4	100	4d <sup>10</sup> 7d	<sup>2</sup> D			B*
2.5	190,136.3	0.4	4	100	4d <sup>10</sup> 7d	<sup>2</sup> D			B*
4.5	198,654.0	0.8	0	100	4d <sup>10</sup> 6g	<sup>2</sup> G			B*
3.5	198,654.3	0.4	0	100	4d <sup>10</sup> 6g	<sup>2</sup> G			B*
0.5	200,362.77	0.3	0	100	4d <sup>10</sup> 9s	<sup>2</sup> S			B*
1.5	200,778.32	0.23	-2	100	4d <sup>10</sup> 8d	<sup>2</sup> D			B*
2.5	200,836.01	0.24	2	100	4d <sup>10</sup> 8d	<sup>2</sup> D			B*
3.5	205,966.56	0.3	1	100	4d <sup>10</sup> 7g	<sup>2</sup> G			B*
4.5	205,966.76	0.3	0	100	4d <sup>10</sup> 7g	<sup>2</sup> G			B*
1.5	207,338.8	0.4	38	100	4d <sup>10</sup> 10s	<sup>2</sup> S			B*
2.5	207,379.7	0.4	3	100	4d <sup>10</sup> 9d	<sup>2</sup> D			B*
4.5	210,770.88	0.3	-1	100	4d <sup>10</sup> 8g	<sup>2</sup> G			B*
3.5	210,7713.04	0.3	1	100	4d <sup>10</sup> 8g	<sup>2</sup> G			B*
0.5	211,462.1	0.3	-3	100	4d <sup>10</sup> 11s	<sup>2</sup> S			B*
1.5	(211,708.6)			100	4d <sup>10</sup> 10d	<sup>2</sup> D			B*
2.5	(211,732.5)			100	4d <sup>10</sup> 10d	<sup>2</sup> D			B*
4.5	213,966.18	0.3	-1	100	4d <sup>10</sup> 9g	<sup>2</sup> G			B*
3.5	213,966.94	0.4	1	100	4d <sup>10</sup> 9g	<sup>2</sup> G			B*
0.5	214,497.7	1.4	-33	100	4d <sup>10</sup> 12s	<sup>2</sup> S			B*
1.5	(214,732.2)			100	4d <sup>10</sup> 11d	<sup>2</sup> D			B*
2.5	(214,749.3)			100	4d <sup>10</sup> 11d	<sup>2</sup> D			B*
3.5	(216,339)			100	4d <sup>10</sup> 10g	<sup>2</sup> G			B*
4.5	(216,339.2)			100	4d <sup>10</sup> 10g	<sup>2</sup> G			B*
0.5	(216,744.7)			100	4d <sup>10</sup> 13s	<sup>2</sup> S			B*
1.5	(216,917.2)			100	4d <sup>10</sup> 12d	<sup>2</sup> D			B*

Table 2. Cont.

LS Compositions <sup>d</sup>									
<i>J</i>	Energy <sup>a</sup> cm <sup>-1</sup>	Unc <sup>b</sup>	$\Delta E_{o-c}$ cm <sup>-1</sup>	1st Component	2nd Component	3rd Component	No. of Lines <sup>c</sup>	Lev. Ref. f	
2.5	(216,929.7)			4d <sup>10</sup> 2d	2D				
3.5	(218,090.7)			4d <sup>10</sup> 1g	2G				
4.5	(218,090.8)			4d <sup>10</sup> 1g	2G				
0.5	(218,391.9)			4d <sup>10</sup> 4s	2S				
3.5	(219,427.4)			4d <sup>10</sup> 2g	2G				
4.5	(219,427.4)			4d <sup>10</sup> 2g	2G				
2.5	235,451.0	0.4	248	4d <sup>9</sup> 5p <sup>2</sup> ( <sup>3</sup> P)	4D	11 4d <sup>9</sup> 5p <sup>2</sup> ( <sup>3</sup> P)	2D	TW	
3.5	236,170.2	0.4	-577	4d <sup>9</sup> 5p <sup>2</sup> ( <sup>3</sup> P)	4D	9 4d <sup>9</sup> 5p <sup>2</sup> ( <sup>3</sup> P)	3	TW	
4.5	(236,964.5)			4d <sup>9</sup> 5p <sup>2</sup> (1D)	2G				
1.5	237,145.6	1.3	-104	4d <sup>9</sup> 5p <sup>2</sup> (1D)	2P	19 4d <sup>9</sup> 5s( <sup>3</sup> D)5d <sup>2</sup> G	9 4d <sup>9</sup> 5p <sup>2</sup> ( <sup>3</sup> P)	R+TW	
0.5	237,201.7	2	343	4d <sup>9</sup> 5p <sup>2</sup> (1D)	2S	21 4d <sup>9</sup> 5p <sup>2</sup> (1D)	2S	R*	
1.5	238,830.9	0.4	207	4d <sup>9</sup> 5p <sup>2</sup> ( <sup>3</sup> P)	4D	14 4d <sup>9</sup> 5p <sup>2</sup> ( <sup>3</sup> P)	2P	R*	
2.5	239,739.3	0.4	-71	4d <sup>9</sup> 5p <sup>2</sup> (1D)	2D	11 4d <sup>9</sup> 5s( <sup>3</sup> D)5d <sup>2</sup> D	11 4d <sup>9</sup> 5p <sup>2</sup> ( <sup>3</sup> P)	TW	
3.5	240,891.5	0.5	-191	4d <sup>9</sup> 5p <sup>2</sup> (1D)	2F	20 4d <sup>9</sup> 5p <sup>2</sup> ( <sup>3</sup> P)	2G	TW	
2.5	241,544.42	0.3	73	4d <sup>9</sup> 5p <sup>2</sup> ( <sup>3</sup> P)	2F	19 4d <sup>9</sup> 5p <sup>2</sup> ( <sup>3</sup> P)	4P	TW	
0.5	241,683.8	0.8	-448	4d <sup>9</sup> 5p <sup>2</sup> ( <sup>3</sup> P)	4D	5 4d <sup>9</sup> 5p <sup>2</sup> (1D)	2S	TW	
3.5	(243,413.3)			4d <sup>9</sup> 5p <sup>2</sup> ( <sup>3</sup> P)	4F	25 4d <sup>9</sup> 5p <sup>2</sup> (1D)	2G	TW	
0.5	243,423.3	2	-224	4d <sup>9</sup> 5p <sup>2</sup> (1D)	2P	15 4d <sup>9</sup> 5p <sup>2</sup> (1D)	2S	R*	
4.5	244,559.9	0.4	-49	4d <sup>9</sup> 5p <sup>2</sup> ( <sup>3</sup> P)	4F	6 4d <sup>9</sup> 5p <sup>2</sup> (1D)	2G	TW	
3.5	(245,494.4)			4d <sup>9</sup> 5p <sup>2</sup> (1D)	2F	24 4d <sup>9</sup> 5p <sup>2</sup> (1D)	2G		
1.5	245,704.30	0.5	152	4d <sup>9</sup> 5p <sup>2</sup> ( <sup>3</sup> P)	2D	19 4d <sup>9</sup> 5p <sup>2</sup> ( <sup>3</sup> P)	4F	R*	
1.5	246,474.9	0.4	-11	4d <sup>9</sup> 5p <sup>2</sup> ( <sup>3</sup> P)	4F	12 4d <sup>9</sup> 5p <sup>2</sup> ( <sup>3</sup> P)	4P	R*	
2.5	246,503.2	0.3	64	4d <sup>9</sup> 5p <sup>2</sup> ( <sup>3</sup> P)	4P	16 4d <sup>9</sup> 5p <sup>2</sup> ( <sup>3</sup> P)	4D	R*	
2.5	247,098.2	0.5	-468	4d <sup>9</sup> 5p <sup>2</sup> ( <sup>3</sup> P)	4F	25 4d <sup>9</sup> 5p <sup>2</sup> ( <sup>3</sup> P)	2F	R*	
3.5	(247,109.4)			4d <sup>9</sup> 5s( <sup>3</sup> D)6s	4D				
1.5	247,351.6	0.5	250	4d <sup>9</sup> 5p <sup>2</sup> (1D)	2D	36 4d <sup>9</sup> 5p <sup>2</sup> ( <sup>3</sup> P)	2D	TW	
2.5	(248,375.7)			4d <sup>9</sup> 5s( <sup>3</sup> D)6s	4D				
1.5	(249,769.2)			4d <sup>9</sup> 5s( <sup>3</sup> D)6s	4D	12 4d <sup>9</sup> 5s( <sup>3</sup> D)6s	2D		
2.5	250,202.6	0.7	403	4d <sup>9</sup> 5p <sup>2</sup> ( <sup>3</sup> P)	2D	12 4d <sup>9</sup> 5s( <sup>3</sup> D)6s	2D	R*	
1.5	250,491.4	0.7	-73	4d <sup>9</sup> 5p <sup>2</sup> ( <sup>3</sup> P)	4P	25 4d <sup>9</sup> 5p <sup>2</sup> ( <sup>3</sup> P)	4D	R*	
0.5	251,157.4	0.4	40	4d <sup>9</sup> 5p <sup>2</sup> ( <sup>3</sup> P)	2P	8 4d <sup>9</sup> 5p <sup>2</sup> ( <sup>3</sup> P)	4P	R*	
2.5	251,829.7	0.4	-221	4d <sup>9</sup> 5p <sup>2</sup> (1D)	2F	23 4d <sup>9</sup> 5p <sup>2</sup> ( <sup>3</sup> P)	2D	R*	
2.5	(253,116.3)			4d <sup>9</sup> 5s( <sup>3</sup> D)6s	2D	10 4d <sup>9</sup> 5s( <sup>3</sup> D)6s	4F	R*	
3.5	253,457.6	0.5	556	4d <sup>9</sup> 5p <sup>2</sup> ( <sup>3</sup> P)	2F	38 4d <sup>9</sup> 5p <sup>2</sup> ( <sup>3</sup> P)	2D	TW	
1.5	253,703.7	0.6	162	4d <sup>9</sup> 5p <sup>2</sup> ( <sup>3</sup> P)	2P	37 4d <sup>9</sup> 5p <sup>2</sup> ( <sup>3</sup> P)	3	R*	
0.5	254,006.1	0.4	-58	4d <sup>9</sup> 5p <sup>2</sup> ( <sup>3</sup> P)	4P	14 4d <sup>9</sup> 5p <sup>2</sup> ( <sup>3</sup> P)	4	TW	
<b>Odd Parity</b>									
0.5	57,184.0	0.3	367	4d <sup>10</sup> 5p	2p <sup>o</sup>		22	B*	
1.5	61,527.0	base	731	4d <sup>10</sup> 5p	2p <sup>o</sup>		30	B*	
0.5	144,589.32	0.24	-10	4d <sup>10</sup> 6p	2p <sup>o</sup>		8	B*	

Table 2. Cont.

LS Compositions <sup>d</sup>									
<i>J</i>	Energy <sup>a</sup> cm <sup>-1</sup>	Unc <sup>b</sup>	$\Delta E_{o-c}$ cm <sup>-1</sup>	1st Component	2nd Component	3rd Component	No. of Lines <sup>c</sup>	Lev. Ref. f	
1.5	145,926.21	0.23	46	4d <sup>10</sup> 6p 2p <sup>o</sup>			14	B*	
2.5	161,974.14	0.3	14	4d <sup>10</sup> 4f 2f <sup>o</sup>			7	B*	
3.5	161,982.00	0.3	-13	4d <sup>10</sup> 4f 2f <sup>o</sup>			6	B*	
2.5	163,890.3	0.4	534	4d <sup>9</sup> 5s(3D)5p 4p <sup>o</sup>	8 4d <sup>9</sup> 5s(3D)5p <sup>o</sup> D <sup>o</sup>		5	TW	
3.5	167,308.1	0.4	31	4d <sup>9</sup> 5s(3D)5p 4p <sup>o</sup>	12 4d <sup>9</sup> 5s(3D)5p <sup>o</sup> D <sup>o</sup>	2p <sup>o</sup>	4	TW	
1.5	167,339.24	0.3	-126	4d <sup>9</sup> 5s(3D)5p 4p <sup>o</sup>	10 4d <sup>9</sup> 5s(3D)5p <sup>o</sup> D <sup>o</sup>	2p <sup>o</sup>	6	B*	
2.5	167,465.9	0.4	-214	4d <sup>9</sup> 5s(3D)5p 4p <sup>o</sup>	20 4d <sup>9</sup> 5s(1D)5p <sup>o</sup> F <sup>o</sup>	2f <sup>o</sup>	3	TW	
4.5	168,947.6	0.5	-340	4d <sup>9</sup> 5s(3D)5p 4f <sup>o</sup>	9 4d <sup>9</sup> 5s(3D)5p <sup>o</sup> F <sup>o</sup>		3	TW	
1.5	170,813.7	0.5	-143	4d <sup>9</sup> 5s(3D)5p 4f <sup>o</sup>	7 4d <sup>9</sup> 5s(3D)5p <sup>o</sup> F <sup>o</sup>		4	K+TW	
0.5	171,315.7	1	-96	4d <sup>9</sup> 5s(3D)5p 4p <sup>o</sup>	9 4d <sup>9</sup> 5s(3D)5p <sup>o</sup> D <sup>o</sup>	2p <sup>o</sup>	2	K+TW	
3.5	174,043.59	0.4	-153	4d <sup>9</sup> 5s(3D)5p 4f <sup>o</sup>	9 4d <sup>9</sup> 5s(1D)5p <sup>o</sup> F <sup>o</sup>	4p <sup>o</sup>	6	TW	
2.5	174,496.6	0.5	238	4d <sup>9</sup> 5s(3D)5p 4f <sup>o</sup>	32 4d <sup>9</sup> 5s(1D)5p <sup>o</sup> F <sup>o</sup>	2f <sup>o</sup>	3	TW	
1.5	175,539.35	0.3	201	4d <sup>9</sup> 5s(1D)5p 2D <sup>o</sup>	23 4d <sup>9</sup> 5s(3D)5p <sup>o</sup> D <sup>o</sup>	2D <sup>o</sup>	5	K*	
2.5	176,090.19	0.4	-281	4d <sup>9</sup> 5s(1D)5p 2f <sup>o</sup>	30 4d <sup>9</sup> 5s(3D)5p <sup>o</sup> F <sup>o</sup>	4D <sup>o</sup>	5	TW	
1.5	177,263.38	0.3	-190	4d <sup>9</sup> 5s(1D)5p 2f <sup>o</sup>	2 4d <sup>9</sup> 5s(1D)5p <sup>o</sup> F <sup>o</sup>		4	B*	
1.5	177,867.74	0.23	4d <sup>10</sup> 7p 2p <sup>o</sup>	4 4d <sup>9</sup> 5s(1D)5p <sup>o</sup> F <sup>o</sup>		7	B*		
0.5	178,187.72	0.3	121	4d <sup>9</sup> 5s(3D)5p 4D <sup>o</sup>	11 4d <sup>9</sup> 5s(3D)5p <sup>o</sup> F <sup>o</sup>	2p <sup>o</sup>	6	K*	
1.5	178,616.85	0.3	-213	4d <sup>9</sup> 5s(1D)5p 2p <sup>o</sup>	22 4d <sup>9</sup> 5s(3D)5p <sup>o</sup> D <sup>o</sup>	2p <sup>o</sup>	5	K*	
0.5	179,320.9	0.3	4	4d <sup>9</sup> 5s(1D)5p 2p <sup>o</sup>	18 4d <sup>9</sup> 5s(3D)5p <sup>o</sup> D <sup>o</sup>	4D <sup>o</sup>	2	K*	
3.5	180,060.3	0.6	23	4d <sup>9</sup> 5s(1D)5p 2f <sup>o</sup>	28 4d <sup>9</sup> 5s(3D)5p <sup>o</sup> F <sup>o</sup>	4p <sup>o</sup>	2	TW	
1.5	180,943.95	0.3	216	4d <sup>9</sup> 5s(3D)5p 4D <sup>o</sup>	25 4d <sup>9</sup> 5s(1D)5p <sup>o</sup> D <sup>o</sup>	2p <sup>o</sup>	7	K*	
2.5	182,399.28	0.4	231	4d <sup>9</sup> 5s(1D)5p 2D <sup>o</sup>	28 4d <sup>9</sup> 5s(3D)5p <sup>o</sup> D <sup>o</sup>	2D <sup>o</sup>	5	TW	
3.5	184,895.95	0.3	-11	4d <sup>10</sup> 5f 2f <sup>o</sup>	4 4d <sup>9</sup> 5s(3D)5p <sup>o</sup> F <sup>o</sup>		5	TW	
2.5	185,024.81	0.3	9	4d <sup>10</sup> 5f 2f <sup>o</sup>	4 4d <sup>9</sup> 5s(3D)5p <sup>o</sup> F <sup>o</sup>		5	B*	
3.5	191,104.1	0.9	404	4d <sup>9</sup> 5s(3D)5p 2f <sup>o</sup>	58 4d <sup>10</sup> 6f 2f <sup>o</sup>	2f <sup>o</sup>	6	B*	
2.5	(191,336.8)		98	4d <sup>9</sup> 5s(3D)5p 2f <sup>o</sup>	2 4d <sup>9</sup> 5s(3D)5p <sup>o</sup> F <sup>o</sup>	2f <sup>o</sup>	1	TW	
1.5	191,509.1	0.3	-55	4d <sup>10</sup> 6f 2f <sup>o</sup>	9 4d <sup>10</sup> 8p 2p <sup>o</sup>	2f <sup>o</sup>	3	K*	
3.5	(192,475.5)		42	4d <sup>10</sup> 6f 2f <sup>o</sup>	32 4d <sup>9</sup> 5s(3D)5p <sup>o</sup> F <sup>o</sup>	2f <sup>o</sup>	3	K*	
0.5	193,938.4	0.4	141	4d <sup>10</sup> 6f 2f <sup>o</sup>	3 4d <sup>9</sup> 5s(3D)5p <sup>o</sup> F <sup>o</sup>		1	B*	
1.5	194,333.3	0.3	-223	4d <sup>10</sup> 8p 2p <sup>o</sup>	8 4d <sup>9</sup> 5s(3D)5p <sup>o</sup> F <sup>o</sup>		5	B*	
2.5	194,902.6	0.4	-57	4d <sup>9</sup> 5s(3D)5p 2D <sup>o</sup>	25 4d <sup>9</sup> 5s(3D)5p <sup>o</sup> F <sup>o</sup>	2D <sup>o</sup>	3	B*	
0.5	198,382.2	0.4	464	4d <sup>9</sup> 5s(3D)5p 2f <sup>o</sup>	18 4d <sup>9</sup> 5s(1D)5p <sup>o</sup> F <sup>o</sup>	2f <sup>o</sup>	3	B*	
2.5	(198,489.7)		54	4d <sup>10</sup> 7f 2f <sup>o</sup>	19 4d <sup>9</sup> 5s(3D)5p <sup>o</sup> F <sup>o</sup>	2D <sup>o</sup>	3	B*	
4.5	(198,518.6)		100	4d <sup>10</sup> 6h 2H <sup>o</sup>					
5.5	(198,519.4)		100	4d <sup>10</sup> 6h 2H <sup>o</sup>					
2.5	198,799.3	0.4	-782	4d <sup>9</sup> 5s(3D)5p 2f <sup>o</sup>	45 4d <sup>10</sup> 7f 2f <sup>o</sup>	2f <sup>o</sup>	3	TW	
3.5	(199,029)		99	4d <sup>10</sup> 7f 2f <sup>o</sup>					
1.5	202,135.0	0.5	28	4d <sup>9</sup> 5s(3D)5p 2D <sup>o</sup>	30 4d <sup>9</sup> 5s(1D)5p <sup>o</sup> D <sup>o</sup>	2D <sup>o</sup>	3	B*	
0.5	(203,388.5)		99	4d <sup>10</sup> 9p 2p <sup>o</sup>					
1.5	(203,556.3)		99	4d <sup>10</sup> 9p 2p <sup>o</sup>					

Table 2. Cont.

LS Compositions <sup>d</sup>									
<i>J</i>	Energy <sup>a</sup> cm <sup>-1</sup>	Unc <sup>b</sup>	$\Delta E_{o-c}$ cm <sup>-1</sup>	1st Component	2nd Component	3rd Component	No. of Lines <sup>c</sup>	Lev. Ref. f	
3.5	(203,854.4)			100 4d <sup>10</sup> 8f 2F <sup>o</sup>					
4.5	(203,879.1)			99 4d <sup>10</sup> 8f 2F <sup>o</sup>					
2.5	206,012.3	0.4	79	100 4d <sup>10</sup> 7h 2H <sup>o</sup>			2	B*	
5.5	206,012.78	0.5	79	100 4d <sup>10</sup> 7h 2H <sup>o</sup>			1	B*	
3.5	(207,170.2)			100 4d <sup>10</sup> 9f 2F <sup>o</sup>					
2.5	(207,177.7)			100 4d <sup>10</sup> 9f 2F <sup>o</sup>					
0.5	(209,199.1)			100 4d <sup>10</sup> 10p 2P <sup>o</sup>					
1.5	(209,320.8)			100 4d <sup>10</sup> 10p 2P <sup>o</sup>				B*	
3.5	(209,539)			100 4d <sup>10</sup> 10f 2F <sup>o</sup>					
2.5	(209,542.4)			100 4d <sup>10</sup> 10f 2F <sup>o</sup>					
4.5	210,743.3	0.5	-9	100 4d <sup>10</sup> 8h 2H <sup>o</sup>			2	B*	
5.5	210,743.8	0.7	-6	100 4d <sup>10</sup> 8h 2H <sup>o</sup>			1	B*	
3.5	(211,284.2)			100 4d <sup>10</sup> 11f 2F <sup>o</sup>					
2.5	(211,286.1)			100 4d <sup>10</sup> 11f 2F <sup>o</sup>					
3.5	(212,613.4)			100 4d <sup>10</sup> 12f 2F <sup>o</sup>					
2.5	(212,614.6)			100 4d <sup>10</sup> 12f 2F <sup>o</sup>					
0.5	(213,103.9)			100 4d <sup>10</sup> 11p 2P <sup>o</sup>					
1.5	(213,189.4)			100 4d <sup>10</sup> 11p 2P <sup>o</sup>					
4.5	213,987.3	0.6	-65	100 4d <sup>10</sup> 9h 2H <sup>o</sup>			2	B*	
5.5	213,987.75	0.8	-64	100 4d <sup>10</sup> 9h 2H <sup>o</sup>			1	B*	
0.5	(215,845.4)			100 4d <sup>10</sup> 12p 2P <sup>o</sup>					
1.5	(215,907.2)			100 4d <sup>10</sup> 12p 2P <sup>o</sup>					
4.5	(216,413.2)			100 4d <sup>10</sup> 10h 2H <sup>o</sup>					
5.5	(216,413.4)			100 4d <sup>10</sup> 10h 2H <sup>o</sup>					
1.5	271,244.30		-184	60 4d <sup>9</sup> 5s( <sup>3</sup> D)6 <sup>3</sup> D <sup>o</sup> 4P <sup>o</sup>	18 4d <sup>9</sup> 5s( <sup>3</sup> D)6 <sup>3</sup> D <sup>o</sup>	4d <sup>9</sup> 5s( <sup>1</sup> D)6p 2P <sup>o</sup>		Ki	
0.5	277,535.30		-3	62 4d <sup>9</sup> 5s( <sup>3</sup> D)6p 4P <sup>o</sup>	18 4d <sup>9</sup> 5s( <sup>3</sup> D)6p <sup>2</sup> P <sup>o</sup>	4d <sup>9</sup> 5s( <sup>1</sup> D)6p 2P <sup>o</sup>		Ki	
0.5	278,100.20		-121	73 4d <sup>9</sup> 5s( <sup>3</sup> D)6p 4D <sup>o</sup>	23 4d <sup>9</sup> 5s( <sup>3</sup> D)6p <sup>2</sup> P <sup>o</sup>	4d <sup>9</sup> 5s( <sup>3</sup> D)6p 2D <sup>o</sup>		Ki	
1.5	278,906.10		50	34 4d <sup>9</sup> 5s( <sup>3</sup> D)6p 2P <sup>o</sup>	21 4d <sup>9</sup> 5s( <sup>3</sup> D)6p <sup>2</sup> P <sup>o</sup>	4d <sup>9</sup> 5s( <sup>3</sup> D)6p 2D <sup>o</sup>		Ki	
1.5	279,955.20		258	55 4d <sup>9</sup> 5s( <sup>1</sup> D)6p 2P <sup>o</sup>	21 4d <sup>9</sup> 5s( <sup>1</sup> D)6p <sup>2</sup> P <sup>o</sup>	4d <sup>9</sup> 5s( <sup>1</sup> D)6p 2D <sup>o</sup>		Ki	
1.5	286,407.80		-76	75 4d <sup>9</sup> 5s( <sup>3</sup> D)4f 4P <sup>o</sup>	23 4d <sup>9</sup> 5s( <sup>3</sup> D)4f <sup>4</sup> D <sup>o</sup>	4d <sup>9</sup> 5s( <sup>3</sup> D)4f 4P <sup>o</sup>		Ki	
0.5	288,020.60		-178	34 4d <sup>9</sup> 5s( <sup>3</sup> D)4f 4D <sup>o</sup>	32 4d <sup>9</sup> 5s( <sup>3</sup> D)4f <sup>4</sup> F <sup>o</sup>	4d <sup>9</sup> 5s( <sup>3</sup> D)4f 4P <sup>o</sup>		Ki	
1.5	288,423.30		-303	73 4d <sup>9</sup> 5s( <sup>3</sup> D)4f 4F <sup>o</sup>	17 4d <sup>9</sup> 5s( <sup>3</sup> D)4f <sup>4</sup> F <sup>o</sup>	4d <sup>9</sup> 5s( <sup>3</sup> D)4f 4P <sup>o</sup>		Ki	
0.5	289,472.80		-265	66 4d <sup>9</sup> 5s( <sup>3</sup> D)4f 2P <sup>o</sup>	27 4d <sup>9</sup> 5s( <sup>3</sup> D)4f <sup>2</sup> P <sup>o</sup>	4d <sup>9</sup> 5s( <sup>3</sup> D)4f 4P <sup>o</sup>		Ki	
1.5	290,682.60		117	34 4d <sup>9</sup> 5s( <sup>3</sup> D)4f 2P <sup>o</sup>	28 4d <sup>9</sup> 5s( <sup>3</sup> D)4f <sup>4</sup> F <sup>o</sup>	4d <sup>9</sup> 5s( <sup>3</sup> D)4f 2D <sup>o</sup>		Ki	
1.5	295,198.90		26	31 4d <sup>9</sup> 5s( <sup>3</sup> D)4f 4F <sup>o</sup>	29 4d <sup>9</sup> 5s( <sup>3</sup> D)4f <sup>4</sup> F <sup>o</sup>	4d <sup>9</sup> 5s( <sup>3</sup> D)4f 2D <sup>o</sup>		Ki	
1.5	297,860.10		69	73 4d <sup>9</sup> 5s( <sup>1</sup> D)4f 2P <sup>o</sup>	10 4d <sup>9</sup> 5s( <sup>1</sup> D)4f <sup>2</sup> P <sup>o</sup>	4d <sup>9</sup> 5s( <sup>1</sup> D)4f 4P <sup>o</sup>		Ki	
1.5	297,860.40		246	62 4d <sup>9</sup> 5s( <sup>1</sup> D)4f 2D <sup>o</sup>	24 4d <sup>9</sup> 5s( <sup>1</sup> D)4f <sup>2</sup> P <sup>o</sup>	4d <sup>9</sup> 5s( <sup>1</sup> D)4f 4P <sup>o</sup>		Ki	
0.5	297,860.50		368	66 4d <sup>9</sup> 5s( <sup>1</sup> D)4f 2P <sup>o</sup>	16 4d <sup>9</sup> 5s( <sup>1</sup> D)4f <sup>4</sup> D <sup>o</sup>	4d <sup>9</sup> 5s( <sup>1</sup> D)4f 2P <sup>o</sup>		Ki	
1.5	305,280.50		2	38 4d <sup>9</sup> 5s( <sup>3</sup> D)7p 4P <sup>o</sup>	37 4d <sup>9</sup> 5s( <sup>3</sup> D)7p <sup>4</sup> P <sup>o</sup>	4d <sup>9</sup> 5s( <sup>3</sup> D)7p 4D <sup>o</sup>		Ki	
1.5	312,862.60		244	43 4d <sup>9</sup> 5s( <sup>3</sup> D)5f 2D <sup>o</sup>	27 4d <sup>9</sup> 5s( <sup>3</sup> D)5f <sup>4</sup> P <sup>o</sup>	4d <sup>9</sup> 5s( <sup>3</sup> D)5f 2P <sup>o</sup>		Ki	
0.5	313,888.90		272	59 4d <sup>9</sup> 5s( <sup>3</sup> D)5f 4D <sup>o</sup>	30 4d <sup>9</sup> 5s( <sup>3</sup> D)5f <sup>2</sup> P <sup>o</sup>	4d <sup>9</sup> 5s( <sup>3</sup> D)5f 2P <sup>o</sup>		Ki	



Table 2. Cont.

LS Compositions <sup>d</sup>									
<i>J</i>	Energy <sup>a</sup> cm <sup>-1</sup>	Unc <sup>b</sup>	$\Delta E_{\text{oc}}$ <sup>c</sup> cm <sup>-1</sup>	1st Component	2nd Component	3rd Component	No. of Lines <sup>e</sup>	Lev. Ref. f	
1.5	314,636.90		-317	4d <sup>9</sup> 5s(3D)5f	2p <sup>0</sup> 26	4d <sup>9</sup> 5s(3D)5f <sup>4</sup> f <sup>0</sup>	23	4d <sup>9</sup> 5s(3D)5f	2p <sup>0</sup>
200	321,653.00		116	4d <sup>9</sup> 5s(1D)5f	2p <sup>0</sup> 9	4d <sup>9</sup> 5s(3D)5f <sup>4</sup> f <sup>0</sup>	9	4d <sup>9</sup> 5s(3D)5f	4p <sup>0</sup>
0.5	321,653.40		-352	4d <sup>9</sup> 5s(1D)5f	2p <sup>0</sup> 15	4d <sup>9</sup> 5s(3D)5f <sup>4</sup> f <sup>0</sup>	10	4d <sup>9</sup> 5s(3D)5f	2p <sup>0</sup>
1.5	325,283.70		-311	4d <sup>9</sup> 5s(3D)6f	2D <sup>0</sup> 22	4d <sup>9</sup> 5s(3D)6f <sup>4</sup> f <sup>0</sup>	14	4d <sup>9</sup> 5s(3D)6f	2p <sup>0</sup>
0.5	326,170.10		-153	4d <sup>9</sup> 5s(3D)6f	4D <sup>0</sup> 36	4d <sup>9</sup> 5s(3D)6f <sup>4</sup> f <sup>0</sup>	7	4d <sup>9</sup> 5s(3D)8p	2p <sup>0</sup>
1.5	328,106.90		348	4d <sup>9</sup> 5s(3D)6f	2p <sup>0</sup> 23	4d <sup>9</sup> 5s(3D)6f <sup>4</sup> f <sup>0</sup>	18	4d <sup>9</sup> 5s(1D)6f	2D <sup>0</sup>
1.5	332,461.90		162	4d <sup>9</sup> 5s(3D)6f	2p <sup>0</sup> 23	4d <sup>9</sup> 5s(3D)6f <sup>4</sup> f <sup>0</sup>	19	4d <sup>9</sup> 5s(3D)6f	2p <sup>0</sup>
0.5	333,429.00		42	4d <sup>9</sup> 5s(3D)7f	2D <sup>0</sup> 17	4d <sup>9</sup> 5s(3D)7f <sup>4</sup> f <sup>0</sup>	16	4d <sup>9</sup> 5s(3D)7f	2p <sup>0</sup>
1.5	333,429.80		-63	4d <sup>9</sup> 5s(3D)7f	2p <sup>0</sup> 23	4d <sup>9</sup> 5s(3D)7f <sup>4</sup> f <sup>0</sup>	10	4d <sup>9</sup> 5s(3D)6f	2p <sup>0</sup>

<sup>a</sup> Energy values are optimized from observed wavelengths using the least squares level optimization code LOPT [15]. Values enclosed in parentheses correspond to unobserved energy levels found from the parametric least squares fitting. <sup>b</sup> Uncertainties resulting from the level optimization procedure are given on the level of one standard deviation. They correspond to uncertainties of level separations from 4d<sup>10</sup>5p<sup>2</sup>P<sub>3/2</sub>. To determine uncertainties of excitation energies from the ground level, the given values should be combined in quadrature with the uncertainty of the ground level, 0.3 cm<sup>-1</sup>. If this column is blank, the level value was not included in the level optimization. <sup>c</sup> Differences between observed energies and those calculated in the parametric least squares fitting. <sup>d</sup> Only three leading LS components are given. <sup>e</sup> Number of observed lines determining the level in the optimization procedure LOPT [15]. <sup>f</sup> Reference to the level source as B, K, R, K+TW, R+TW and TW stand for Bhatia [6], Kaufman et al. [7], Ryabtsev et al. [9], previous value [7] has been revised, previous value [9] has been revised, and this work, \* stands for levels from [6,7,9] re-optimized in this work. Ki stands for Kilbane et al. [8] level values, which have not been included in the level optimization.

Table 3. List of classified lines in In III spectrum.

<i>I</i> <sub>obs</sub> <sup>a</sup>	ch <sup>b</sup>	$\lambda_{\text{obs}}$ <sup>c</sup> Å	$\sigma_{\text{obs}}$ <sup>c</sup> cm <sup>-1</sup>	$\lambda_{\text{ritiz}}$ <sup>d</sup> Å	$\Delta\lambda_{\text{critiz}}$ <sup>e</sup> Å	Classification <sup>f</sup>	<i>E</i> <sub>low</sub> <sup>c</sup> cm <sup>-1</sup>	<i>E</i> <sub>upp</sub> <sup>c</sup> cm <sup>-1</sup>	<i>gA</i> <sup>h</sup> s <sup>-1</sup>	#	Lin. Ref <sup>i</sup>
50	494,715(8)	202,137	494,7189(13)	4d <sup>10</sup> 5s	-0.004	(S) <sup>2</sup> S <sub>0,5</sub>	(3D) <sup>2</sup> D <sub>1,5</sub>	0.0	202,135.0	1.42E+08	TW
200	504,080(6)	198,381.2	504,0773(12)	4d <sup>10</sup> 5s	0.003	(S) <sup>2</sup> S <sub>0,5</sub>	(D)P <sub>0,3</sub>	0.0	198,382.2	5.08E+09	TW
50	508,066(6)	196,824.8	508,0730(12)	4d <sup>10</sup> 5p	-0.007	(S) <sup>2</sup> P <sub>0,5</sub>	(3P) <sup>2</sup> P <sub>1,5</sub>	57,184.0	254,006.1	8.17E+08	TW
100	508,846(6)	196,523.1	508,8548(15)	4d <sup>10</sup> 5p	-0.009	(S) <sup>2</sup> P <sub>0,5</sub>	(3P) <sup>2</sup> P <sub>1,5</sub>	57,184.0	253,703.7	4.60E+08	#
20	514,583(8)	194,332	514,5798(11)	4d <sup>10</sup> 5s	0.003	(S) <sup>2</sup> S <sub>0,5</sub>	4d <sup>10</sup> 8p	0.0	194,333.3	3.30E+09	B
750	515,532(6)	193,974.4	515,5346(12)	4d <sup>10</sup> 5p	-0.003	(S) <sup>2</sup> P <sub>0,5</sub>	(3P) <sup>2</sup> P <sub>1,5</sub>	57,184.0	251,157.4	3.94E+09	R
45	519,544(6)	192,476.5	519,5369(11)	4d <sup>10</sup> 5p	0.007	(S) <sup>2</sup> P <sub>1,5</sub>	(3P) <sup>2</sup> P <sub>1,5</sub>	61,527.0	254,006.1	2.39E+08	TW
620	520,357(6)	192,175.8	520,3544(15)	4d <sup>10</sup> 5p	0.003	(S) <sup>2</sup> P <sub>1,5</sub>	(3P) <sup>2</sup> P <sub>1,5</sub>	61,527.0	253,703.7	8.31E+09	R
120	522,166(6)	191,510.0	522,1684(11)	4d <sup>10</sup> 5s	-0.002	(S) <sup>2</sup> S <sub>0,5</sub>	(3D) <sup>2</sup> P <sub>1,5</sub>	0.0	191,509.1	1.07E+10	K
300	525,300(6)	190,367.4	525,2995(14)	4d <sup>10</sup> 5p	0.001	(S) <sup>2</sup> P <sub>0,5</sub>	(3D) <sup>2</sup> D <sub>1,5</sub>	57,184.0	247,551.6	1.85E+10	R
250	525,482(6)	190,301.5	525,4786(12)	4d <sup>10</sup> 5p	0.003	(S) <sup>2</sup> P <sub>1,5</sub>	(1D) <sup>2</sup> F <sub>2,5</sub>	61,527.0	251,829.7	5.20E+09	R

Table 3. Cont.

$J_{obs}^a$	ch <sup>b</sup>	$\lambda_{obs}^c$ Å	$\sigma_{obs}^d$ cm <sup>-1</sup>	$\lambda_{Ritz}^e$ Å	$\Delta\lambda_{O-Ritz}^e$ Å	Classification <sup>f</sup>	$E_{low}^g$ cm <sup>-1</sup>	$E_{upp}^g$ cm <sup>-1</sup>	$gA^h$ s <sup>-1</sup>	Lin. Ref <sup>i</sup>
540		527.348(6)	189.628(1)	527.3416(12)	0.006	4d <sup>10</sup> 5p (S) <sup>2</sup> P <sub>1,5</sub>	61,527.0	251,157.4	3.46E+09	R
230		528.287(6)	188.291(0)	528.2874(12)	0.000	4d <sup>10</sup> 5p (S) <sup>2</sup> P <sub>0,5</sub>	57,184.0	246,474.9	1.15E+06	R
630		529.200(6)	188.964(5)	529.2002(19)	0.000	4d <sup>10</sup> 5p (S) <sup>2</sup> P <sub>1,5</sub>	61,527.0	250,491.4	7.53E+09	R
450		530.000(6)	188.679(2)	530.0102(20)	-0.010	4d <sup>10</sup> 5p (S) <sup>2</sup> P <sub>0,5</sub>	61,527.0	250,202.6	2.73E+10	R
460		530.448(6)	188.519(9)	530.4469(14)	0.001	4d <sup>10</sup> 5p (S) <sup>2</sup> P <sub>0,5</sub>	57,184.0	245,704.3	4.21E+09	R
300		540.613(6)	184.975(2)	540.6101(10)	0.003	4d <sup>10</sup> 5p (S) <sup>2</sup> P <sub>1,5</sub>	61,527.0	246,503.2	4.37E+09	R
200		540.678(6)	184.953(0)	540.6928(11)	-0.015	4d <sup>10</sup> 5p (S) <sup>2</sup> P <sub>1,5</sub>	61,527.0	246,474.9	6.21E+08	R
480		549.764(6)	181.896(2)	549.764(6)	0.000	4d <sup>10</sup> 5p (S) <sup>2</sup> P <sub>1,5</sub>	61,527.0	243,423.3	2.42E+09	R
570		550.518(6)	181.647(1)	550.5186(13)	-0.001	4d <sup>10</sup> 5p (S) <sup>2</sup> P <sub>0,5</sub>	57,184.0	238,830.9	3.66E+09	R
25		552.660(6)	180.943(1)	552.6573(11)	0.003	4d <sup>10</sup> 5p (S) <sup>2</sup> P <sub>0,5</sub>	0.0	180,943.95	4.73E+08	K
15		555.069(6)	180.157(8)	555.0720(24)	-0.003	4d <sup>10</sup> 5p (S) <sup>2</sup> P <sub>1,5</sub>	61,527.0	241,683.8	3.56E+08	TW
20		555.301(6)	180.017(7)	555.301(6)	0.000	4d <sup>10</sup> 5p (S) <sup>2</sup> P <sub>0,5</sub>	57,184.0	237,201.7	4.56E+09	TW
390		555.669(6)	179.963(3)	555.674(4)	-0.005	4d <sup>10</sup> 5p (S) <sup>2</sup> P <sub>0,5</sub>	57,184.0	237,145.6	1.08E+09	R
150		557.662(6)	179.320(1)	557.6595(13)	0.003	4d <sup>10</sup> 5p (S) <sup>2</sup> P <sub>0,5</sub>	0.0	179,320.9	1.47E+09	K
130		559.857(6)	178.617(0)	559.8576(11)	-0.001	4d <sup>10</sup> 5p (S) <sup>2</sup> P <sub>1,5</sub>	0.0	178,616.85	1.27E+10	K
130		561.210(6)	178.186(4)	561.2059(11)	0.004	4d <sup>10</sup> 5p (S) <sup>2</sup> P <sub>0,5</sub>	0.0	178,187.72	5.47E+09	K
200		562.214(6)	177.868(2)	562.2155(11)	-0.001	4 <sup>10</sup> 7p (S) <sup>2</sup> P <sub>1,5</sub>	0.0	177,867.74	5.56E+09	B, TW
160		564.131(6)	177.263(8)	564.1323(11)	-0.001	4 <sup>10</sup> 7p (S) <sup>2</sup> P <sub>0,5</sub>	0.0	177,263.38	3.77E+09	B, TW
480		569.421(6)	175.617(0)	569.416(4)	0.005	4d <sup>10</sup> 5p (S) <sup>2</sup> P <sub>1,5</sub>	61,527.0	237,145.6	1.72E+09	R
80		569.677(6)	175.538(1)	569.6728(12)	0.004	4d <sup>10</sup> 5p (S) <sup>2</sup> P <sub>0,5</sub>	0.0	175,539.35	7.80E+08	K
80		583.723(6)	171.314(1)	583.718(3)	0.005	4d <sup>10</sup> 5p (S) <sup>2</sup> P <sub>0,5</sub>	0.0	171,315.7	9.39E+08	TW
50		585.440(6)	170.811(7)	585.4331(18)	0.007	4d <sup>10</sup> 5p (S) <sup>2</sup> P <sub>0,5</sub>	0.0	170,813.7	2.95E+07	K
100		597.596(6)	167.337(1)	597.5885(13)	0.008	4d <sup>10</sup> 5p (S) <sup>2</sup> P <sub>0,5</sub>	0.0	167,339.24	1.18E+09	B, TW
30		635.672(8)	157.313(8)	635.673(6)	-0.001	4d <sup>10</sup> 12s (S) <sup>2</sup> P <sub>0,5</sub>	57,184.0	214,497.7	3.71E+07	B
32		648.188(8)	154.276(9)	648.1801(15)	0.005	4d <sup>10</sup> 11s (S) <sup>2</sup> P <sub>0,5</sub>	57,184.0	211,462.1	5.21E+07	B
33		653.721(8)	152.970(5)	653.720(6)	0.001	4d <sup>10</sup> 12s (S) <sup>2</sup> P <sub>0,5</sub>	61,527.0	214,497.7	6.79E+07	B
41		665.979(8)	150.154(9)	665.9794(17)	0.000	4d <sup>10</sup> 9d (S) <sup>2</sup> D <sub>1,5</sub>	57,184.0	207,338.8	9.52E+07	B
40		666.963(8)	149.933(4)	666.9552(15)	0.008	4d <sup>10</sup> 11s (S) <sup>2</sup> P <sub>1,5</sub>	61,527.0	211,462.1	9.55E+07	B
40		667.177(8)	149.885(3)	667.1807(15)	-0.004	4d <sup>10</sup> 10s (S) <sup>2</sup> P <sub>0,5</sub>	57,184.0	207,068.43	7.66E+07	B
80		685.273(6)	145.927(2)	685.2779(16)	-0.005	4d <sup>10</sup> 6p (S) <sup>2</sup> P <sub>0,5</sub>	0.0	145,926.21	4.63E+07	B, TW
41		685.612(8)	145.855(1)	685.6232(17)	-0.011	4d <sup>10</sup> 9d (S) <sup>2</sup> D <sub>1,5</sub>	61,527.0	207,379.7	1.68E+08	B
67		685.815(8)	145.811(9)	685.8156(17)	-0.001	4d <sup>10</sup> 9d (S) <sup>2</sup> P <sub>1,5</sub>	61,527.0	207,338.8	1.88E+07	B
48		687.076(8)	145.544(3)	687.0896(15)	-0.014	4d <sup>10</sup> 10s (S) <sup>2</sup> P <sub>1,5</sub>	61,527.0	207,068.43	1.41E+08	B
200		691.610(6)	144.590(2)	691.6140(17)	-0.004	4d <sup>10</sup> 6p (S) <sup>2</sup> P <sub>0,5</sub>	0.0	144,589.32	2.10E+07	B, TW
50		696.399(8)	143.595(8)	696.4064(13)	-0.007	4d <sup>10</sup> 8d (S) <sup>2</sup> D <sub>1,5</sub>	57,184.0	200,778.32	1.79E+08	B
65		698.422(8)	143.179(9)	698.4276(15)	-0.006	4d <sup>10</sup> 9s (S) <sup>2</sup> P <sub>0,5</sub>	57,184.0	200,362.77	1.20E+08	B
68		717.834(8)	139.308(0)	717.8287(12)	0.005	4d <sup>10</sup> 8d (S) <sup>2</sup> P <sub>1,5</sub>	61,527.0	200,836.01	3.09E+08	B
60		718.135(8)	139.249(6)	718.1260(12)	0.009	4d <sup>10</sup> 8d (S) <sup>2</sup> D <sub>1,5</sub>	61,527.0	200,778.32	3.45E+07	B

Table 3. Cont.

$J_{obs}^a$	ch <sup>b</sup>	$\lambda_{obs}, \text{ \AA}$	$\sigma_{obs}, \text{ cm}^{-1}$	$\lambda_{ritz}, \text{ \AA}$	$\Delta\lambda_{ritz}, \text{ e \AA}$	Classification <sup>c</sup>	$E_{low}, \text{ cm}^{-1}$	$E_{upp}, \text{ cm}^{-1}$	$gA^d, \text{ s}^{-1}$	Lin. Ref <sup>e</sup>
70		720.281(8)	138.834(7)	720.2755(15)	0.006	$4d^{10}5p$	$(S^1)P_{1,5}$	200,362.77	2.20E+08	B
15		752.699(6)	132.855(2)	752.7014(21)	-0.002	$4d^{10}5p$	$(S^1)D_{1,5}$	51,527.0	3.91E+08	B, TW
20		756.484(6)	132.190(5)	756.4840(21)	0.000	$4d^{10}5p$	$(S^1)P_{0,5}$	189,374.5	2.04E+08	B, TW
10		777.547(6)	128.609(6)	777.549(3)	-0.002	$4d^{10}5p$	$(S^1)P_{1,5}$	61,527.0	6.60E+08	B, TW
65		778.142(8)	128.511(2)	778.1387(21)	0.003	$4d^{10}5p$	$(S^1)D_{1,5}$	190,038.8	7.34E+07	B
30		782.187(6)	127.846(7)	782.1819(20)	0.005	$4d^{10}5p$	$(S^1)P_{1,5}$	189,374.5	3.73E+08	B, TW
180		882.207(6)	113.352(1)	882.2095(22)	-0.003	$4d^{10}5p$	$(S^1)D_{1,5}$	170,535.76	1.12E+09	B, TW
150		890.870(6)	112.249(8)	890.8639(23)	0.006	$4d^{10}5p$	$(S^1)P_{0,5}$	169,434.59	4.00E+08	B, TW
120		915.824(6)	109.191(3)	915.8196(21)	0.004	$4d^{10}5p$	$(S^1)P_{1,5}$	170,718.81	1.84E+09	B, TW
25		917.355(6)	109.109(1)	917.3573(20)	-0.002	$4d^{10}5p$	$(S^1)D_{1,5}$	170,535.76	2.04E+08	B, TW
120		926.723(8)	107.907(1)	926.7189(21)	0.004	$4d^{10}5p$	$(S^1)P_{1,5}$	61,527.0	7.20E+08	B
200		1153.839(8)	86.667(2)	1153.844(5)	-0.005	$4d^95s5p$	$(^3D^1)P_{1,5}$	167,339.24	3.60E+08	#
200		1162.895(8)	85.992(3)	1162.903(6)	-0.008	$4d^95s5p$	$(^3D^1)F_{2,5}$	253,457.6	3.59E+09	TW
50		1201.523(8)	83.227(7)	1201.532(5)	-0.009	$4d^95s^2$	$(^3D^1)D_{2,5}$	115,572.19	2.25E+09	TW
80		1210.468(8)	826.12(7)	1210.465(5)	0.003	$4d^95s^2$	$(^3D^1)F_{2,5}$	246,530.2	2.49E+09	TW
300	w	1254.458(16)	79.15(7)	1254.465(7)	-0.007	$4d^95s^2$	$(^3D^1)D_{1,5}$	122,419.73	7.59E+09	B, TW
300	w	1260.567(16)	79.329(4)	1260.551(6)	0.016	$4d^95s^2$	$(^3D^1)D_{2,5}$	115,572.19	1.49E+10	TW
200		1263.152	79.167(0)	1263.201(5)	0.000	$4d^95s^2$	$(^3D^1)P_{1,5}$	167,339.24	3.92E+09	TW
100		1263.594	79.139(3)	1263.653(6)	0.000	$4d^95s^2$	$(^3D^1)F_{1,5}$	246,474.9	3.06E+08	TW
15		1285.588(8)	77.785(4)	1285.577(6)	0.011	$4d^95s5p$	$(^3D^1)D_{3,5}$	174,496.6	4.50E+06	#
20		1287.732(8)	77.654(7)	1287.762(5)	-0.010	$4d^95s5p$	$(^3D^1)F_{2,5}$	163,890.3	1.29E+09	TW
150		1294.468(8)	77.251(8)	1294.468(5)	0.000	$4d^95s5p$	$(^3D^1)F_{1,5}$	167,308.1	5.06E+09	TW
250	w	1309.269(16)	76.378(5)	1309.251(6)	0.018	$4d^{10}5s^2$	$(^3D^1)D_{1,5}$	122,419.73	8.07E+09	TW
15		1315.880(8)	75.994(8)	1315.880(8)	0.000	$4d^95s5p$	$(^3D^1)D_{2,5}$	250,491.4	1.81E+09	TW
280	w	1316.430(16)	75.963(0)	1316.440(7)	-0.010	$4d^95s^2$	$(^3D^1)D_{1,5}$	122,419.73	3.01E+09	TW
70		1318.399(8)	75.849(6)	1318.409(5)	-0.010	$4d^95s5p$	$(^3D^1)D_{2,5}$	163,890.3	2.39E+09	TW
60		1318.946(8)	75.818(1)	1318.941(6)	0.005	$4d^95s5p$	$(^3D^1)D_{0,5}$	178,187.72	1.12E+08	TW
100		1320.314(8)	75.739(6)	1320.315(6)	-0.001	$4d^95s5p$	$(^3D^1)F_{2,5}$	176,090.19	251,829.7	#
150		1321.683(8)	75.661(1)	1321.681(7)	0.002	$4d^95s5p$	$(^3D^1)F_{1,5}$	170,813.7	4.82E+09	TW
200		1322.526(8)	75.612(9)	1322.536(6)	-0.010	$4d^95s5p$	$(^3D^1)F_{4,5}$	168,947.6	244,559.9	TW
250	w	1323.944(16)	75.531(9)	1323.944(16)	0.000	$4d^95s^2$	$(^3D^1)D_{2,5}$	115,572.19	191,104.1	1.75E+10
80		1349.914(8)	74.078(8)	1349.919(6)	-0.005	$4d^95s5p$	$(^3D^1)F_{2,5}$	167,465.9	241,544.42	6.37E+09
60		1357.284(8)	73.676(5)	1357.282(7)	0.002	$4d^{10}5d$	$(S^1)D_{1,5}$	128,458.36	202,135.0	4.03E+09
100		1358.998(8)	73.583(6)	1359.002(7)	-0.004	$4d^95s5p$	$(^3D^1)F_{3,5}$	167,308.1	240,891.5	1.66E+09
200		1362.448(8)	73.397(5)	1362.448(8)	-0.003	$4d^95s5p$	$(^3D^1)F_{4,5}$	180,060.3	253,457.6	1.10E+10
15		1370.424(8)	72.970(1)	1370.432(7)	-0.008	$4d^95s5p$	$(^3D^1)D_{0,5}$	178,187.72	251,157.4	6.79E+08
8	f	1378.569(16)	72.539(0)	1378.539(8)	0.030	$4d^95s5p$	$(^3D^1)P_{0,5}$	178,161.85	251,157.4	4.19E+08
160		1380.066(8)	72.460(3)	1380.079(5)	-0.013	$4d^95s5p$	$(^3D^1)D_{2,5}$	174,043.59	246,530.2	6.43E+09
160		1380.638(8)	72.420(3)	1380.621(6)	0.017	$4d^95s5p$	$(^3D^1)F_{2,5}$	167,308.1	239,739.3	1.06E+09
180		1383.510(8)	72.279(9)	1383.510(6)	0.000	$4d^95s5p$	$(^3D^1)D_{3,5}$	163,890.3	236,170.2	1.06E+10
40	f	1389.976(8)	71.943(7)	1389.972(7)	0.004	$4d^95s5p$	$(^3D^1)F_{4,5}$	168,947.6	240,891.5	4.36E+08
8	f	1390.554(16)	71.913(8)	1390.558(5)	-0.004	$4d^{10}5s^2$	$(^3D^1)D_{1,5}$	122,419.73	194,333.3	1.89E+07
20		1397.429(8)	71.560(0)	1397.415(6)	0.014	$4d^95s5p$	$(^3D^1)D_{2,5}$	163,890.3	235,451.0	2.21E+09

Table 3. Cont.

$J_{obs}^a$	ch <sup>b</sup>	$\lambda_{obs}^c, \text{ \AA}$	$\sigma_{obs}^d, \text{ cm}^{-1}$	$\lambda_{ritz}^e, \text{ \AA}$	$\Delta\lambda_{ritz}^e, \text{ \AA}$	Classification <sup>f</sup>	$E_{low}, \text{ cm}^{-1}$	$E_{upp}, \text{ cm}^{-1}$	$gA^h, \text{ s}^{-1}$	Lin. Ref <sup>i</sup>
200		1398.755(8)	71.492.1	1398.765(7)	-0.010	4d <sup>9</sup> 5s5p	( <sup>3</sup> P) <sup>2</sup> D <sub>3,5</sub>	238.830.9	1.78E+09	TW
10		1399.355(8)	71.461.5	1399.357(7)	-0.002	4d <sup>9</sup> 5s5p	( <sup>1</sup> D) <sup>2</sup> F <sub>2,5</sub>	167.339.24	2.30E+09	TW
100		1401.254(8)	71.364.6	1401.247(7)	0.007	4d <sup>9</sup> 5s5p	( <sup>3</sup> D) <sup>2</sup> F <sub>2,5</sub>	238.830.9	247.551.6	4.84E+09
100		1402.439(8)	71.304.3	1402.438(8)	0.001	4d <sup>9</sup> 5s5p	( <sup>1</sup> D) <sup>2</sup> D <sub>2,5</sub>	182.399.28	253.703.7	6.34E+09
280	w	1403.017(16)	71.275.0	1403.029(6)	-0.012	4d <sup>10</sup> 5d	( <sup>1</sup> S) <sup>2</sup> P <sub>0,5</sub>	57.184.0	128.458.36	4.26E+09
150		1404.342(8)	71.207.7	1404.343(7)	-0.001	4d <sup>9</sup> 5s5p	( <sup>3</sup> D) <sup>2</sup> D <sub>2,5</sub>	174.496.6	3.40E+09	TW
200		1407.302(8)	71.058.0	1407.295(7)	0.007	4d <sup>9</sup> 5s5p	( <sup>1</sup> D) <sup>2</sup> D <sub>2,5</sub>	182.399.28	253.457.6	4.50E+09
120		1408.292(8)	71.008.0	1408.292(7)	0.000	4d <sup>9</sup> 5s5p	( <sup>1</sup> D) <sup>2</sup> F <sub>2,5</sub>	176.090.19	247.998.2	3.16E+09
2	f	1411.028(16)	70.870.3	1411.032(14)	-0.004	4d <sup>9</sup> 5s5p	( <sup>3</sup> D) <sup>2</sup> F <sub>1,5</sub>	170.813.7	241.683.8	3.00E+09
2	f	1413.821(16)	70.730.3	1413.813(9)	0.008	4d <sup>9</sup> 5s5p	( <sup>3</sup> D) <sup>2</sup> F <sub>1,5</sub>	170.813.7	241.544.42	1.55E+09
150		1418.119(8)	70.515.9	1418.112(6)	0.007	4d <sup>9</sup> 5s5p	( <sup>3</sup> D) <sup>2</sup> D <sub>3,5</sub>	174.043.59	244.559.9	5.34E+09
5	f	1420.204(16)	70.412.4	1420.192(7)	0.012	4d <sup>9</sup> 5s5p	( <sup>1</sup> D) <sup>2</sup> F <sub>2,5</sub>	176.090.19	246.503.2	4.82E+08
4	f	1421.105(16)	70.367.8	1421.098(15)	0.007	4d <sup>9</sup> 5s5p	( <sup>3</sup> D) <sup>2</sup> P <sub>0,5</sub>	171.315.7	241.683.8	1.38E+09
6		1421.649(8)	70.340.9	1421.647(6)	0.002	4d <sup>9</sup> 5s5p	( <sup>3</sup> D) <sup>2</sup> F <sub>2,5</sub>	128.458.36	198.799.3	4.94E+09
100		1425.676(8)	70.142.2	1425.673(8)	0.003	4d <sup>9</sup> 5s5p	( <sup>1</sup> D) <sup>2</sup> D <sub>3,5</sub>	180.060.3	250.202.6	4.78E+09
35		1430.130(8)	69.923.7	1430.127(7)	0.003	4d <sup>9</sup> 5s5p	( <sup>3</sup> D) <sup>2</sup> P <sub>0,5</sub>	128.458.36	198.382.2	1.38E+09
280	w	1434.800(16)	69.696.1	1434.805(6)	-0.005	4d <sup>10</sup> 5d	( <sup>1</sup> S) <sup>2</sup> P <sub>0,5</sub>	57.184.0	126.879.89	1.08E+09
35	bl	1439.854(16)	69.451.5	1439.830(4)	0.024	4d <sup>10</sup> 5d	( <sup>1</sup> S) <sup>2</sup> D <sub>2,5</sub>	115.572.19	185.024.81	7.33E+06
100		1440.281(8)	69.430.9	1440.291(7)	-0.010	4d <sup>9</sup> 5s5p	( <sup>1</sup> D) <sup>2</sup> D <sub>2,5</sub>	182.399.28	251.829.7	2.33E+09
200	bl	1442.512(16)	69.323.5	1442.507(5)	0.005	4d <sup>9</sup> 5s5p	( <sup>3</sup> D) <sup>2</sup> F <sub>2,5</sub>	115.572.19	184.895.95	2.52E+08
110		1447.387(8)	69.090.0	1447.401(6)	-0.014	4d <sup>9</sup> 5s5p	( <sup>3</sup> D) <sup>2</sup> D <sub>1,5</sub>	122.419.73	191.509.1	1.09E+08
100		1467.495(8)	68.143.3	1467.504(6)	-0.009	4d <sup>9</sup> 5s5p	( <sup>3</sup> D) <sup>2</sup> F <sub>2,5</sub>	167.339.24	235.451.0	6.54E+09
120		1468.172(8)	68.111.9	1468.175(6)	-0.003	4d <sup>9</sup> 5s5p	( <sup>3</sup> D) <sup>2</sup> D <sub>2,5</sub>	167.339.24	235.451.0	3.47E+09
40	f	1481.468(8)	67.500.6	1481.463(5)	0.005	4d <sup>9</sup> 5s5p	( <sup>1</sup> D) <sup>2</sup> D <sub>3,5</sub>	174.043.59	241.544.42	1.54E+09
8	f	1482.483(16)	67.454.4	1482.505(6)	-0.022	4d <sup>10</sup> 6s	( <sup>1</sup> S) <sup>2</sup> S <sub>0,5</sub>	126.879.89	194.333.3	8.27E+06
300	w	1487.623(23)	67.221.3	1487.595(10)	0.028	4d <sup>10</sup> 6s	( <sup>3</sup> P) <sup>2</sup> F <sub>1,5</sub>	168.947.6	236.170.2	1.06E+10
300	w	1487.623(23)	67.221.3	1487.623(5)	0.000	4d <sup>10</sup> 5d	( <sup>1</sup> S) <sup>2</sup> P <sub>1,5</sub>	61.527.0	128.748.33	8.44E+09
15	f	1491.235(8)	67.058.5	1491.235(8)	0.000	4d <sup>10</sup> 6s	( <sup>1</sup> S) <sup>2</sup> S <sub>0,5</sub>	126.879.89	193.938.4	5.84E+05
5	f	1491.474(16)	67.047.8	1491.473(10)	0.001	4d <sup>9</sup> 5s5p	( <sup>1</sup> D) <sup>2</sup> D <sub>2,5</sub>	174.496.6	241.544.42	2.20E+09
200	w	1494.066(16)	66.931.4	1494.068(5)	-0.002	4d <sup>10</sup> 5d	( <sup>1</sup> S) <sup>2</sup> P <sub>1,5</sub>	61.527.0	128.458.36	7.21E+08
5	f	1495.389(8)	66.872.2	1495.377(6)	0.012	4d <sup>10</sup> 6p	( <sup>1</sup> S) <sup>2</sup> P <sub>0,5</sub>	144.589.32	211.462.1	2.09E+07
20		1505.020(8)	66.444.3	1505.021(7)	-0.001	4d <sup>10</sup> 5d	( <sup>3</sup> D) <sup>2</sup> D <sub>2,5</sub>	128.458.36	194.902.6	6.10E+08
40	*	1511.615(23)	66.154.4	1511.619(11)	-0.004	4d <sup>9</sup> 5s5p	( <sup>3</sup> P) <sup>2</sup> F <sub>2,5</sub>	180.943.95	247.998.2	1.23E+09
40	*	1511.615(23)	66.154.4	1511.618(6)	-0.003	4d <sup>9</sup> 5s5p	( <sup>3</sup> D) <sup>2</sup> D <sub>2,5</sub>	128.748.33	194.902.6	1.91E+08
35		1515.040(8)	66.004.9	1515.035(6)	0.005	4d <sup>9</sup> 5s5p	( <sup>3</sup> D) <sup>2</sup> F <sub>2,5</sub>	175.539.35	241.544.42	2.10E+09
10		1518.024(8)	65.975.9	1518.028(5)	-0.004	4d <sup>10</sup> 6p	( <sup>1</sup> S) <sup>2</sup> P <sub>1,5</sub>	128.458.36	194.333.3	2.33E+07
60		1522.164(8)	65.695.9	1522.169(6)	-0.005	4d <sup>9</sup> 5s5p	( <sup>3</sup> D) <sup>2</sup> D <sub>1,5</sub>	174.043.59	239.739.3	7.16E+08
25		1524.750(8)	65.584.5	1524.740(6)	0.010	4d <sup>10</sup> 6p	( <sup>1</sup> S) <sup>2</sup> D <sub>2,5</sub>	128.748.33	194.333.3	7.42E+07
10		1525.344(8)	65.559.0	1525.338(6)	0.006	4d <sup>9</sup> 5s5p	( <sup>3</sup> P) <sup>2</sup> P <sub>1,5</sub>	180.943.95	246.503.2	1.21E+08

Table 3. Cont.

$J_{obs}^a$	ch <sup>b</sup>	$\lambda_{obs}, \text{ \AA}$	$\sigma_{obs}, \text{ cm}^{-1}$	$\lambda_{ritz}, \text{ \AA}$	$\Delta\lambda_{ritz}, \text{ e \AA}$	Classification <sup>c</sup>	$E_{low}, \text{ cm}^{-1}$	$E_{upp}, \text{ cm}^{-1}$	$gA^d, \text{ s}^{-1}$	Lin. Ref <sup>e</sup>	
14		1525.869(8)	65.536.4	1525.881(6)	-0.012	$4d^{10}6p$	$(^3P^o)P_{1,5}$	145.926.21	211.462.1	3.95E+07	B
100		1526.000(8)	65.530.8	1525.996(7)	-0.004	$4d^95s5p$	$(^3D^o)D_{1,5}$	180.943.95	246.474.9	7.67E+08	TW
40		1527.784(8)	65.454.3	1527.785(6)	-0.001	$4d^95s5p$	$(^1D^o)F_{2,5}$	176.090.19	241.544.42	7.27E+07	TW
52		1529.704(8)	65.372.1	1529.713(5)	-0.009	$4d^95s5p$	$(^3D^o)D_{2,5}$	115.572.19	180.943.95	7.42E+06	#
260	w	1530.169(16)	65.352.3	1530.154(6)	0.015	$4d^{10}6p$	$(^3S^o)P_{1,5}$	61.527.0	126.879.89	1.82E+09	B, TW
180	w	1532.926(16)	65.234.7	1532.902(6)	0.024	$4d^{10}6p$	$(^3D^o)D_{1,5}$	57.184.0	122.419.73	2.79E+09	B, TW
5	f	1534.868(16)	65.152.2	1534.865(10)	0.003	$4d^95s2p$	$(^1D^o)D_{2,5}$	182.399.28	247.551.6	1.00E+08	TW
48		1547.300(8)	64.628.7	1547.288(6)	0.012	$4d^{10}6s$	$(^3D^o)P_{1,5}$	126.879.89	191.509.1	1.64E+07	TW
25		1579.653(8)	63.305.0	1579.654(7)	-0.001	$4d^95s5p$	$(^3D^o)D_{2,5}$	182.399.28	245.704.3	4.09E+07	TW
30		(1593.384)	62.759.5	1593.352(8)	-0.001	$4d^{10}5d$	$(^3D^o)D_{3,5}$	128.748.33	191.509.1	4.16E+06	#
32		(1593.592)	62.751.3	1593.639(8)	-0.001	$4d^{10}6p$	$(^3D^o)P_{0,5}$	144.589.32	207.338.8	8.02E+07	B
78		1597.329(8)	62.604.5	1597.314(4)	0.015	$4d^95s2p$	$(^3D^o)D_{1,5}$	122.419.73	185.024.81	1.92E+08	B
50		1600.535(8)	62.479.1	1600.535(6)	0.000	$4d^{10}6p$	$(^3S^o)P_{0,5}$	144.589.32	207.068.43	3.15E+07	B
60	w	(1605.211)	62.297.1	1605.251(6)	-0.001	$4d^95s2p$	$(^3D^o)P_{1,5}$	115.572.19	177.867.74	7.79E+05	#
10		1609.613(8)	62.126.7	1609.616(7)	-0.003	$4d^95s5p$	$(^3D^o)D_{3,5}$	174.043.59	236.170.2	3.86E+08	TW
400	w	1625.301(16)	61.527.1	1625.303(9)	-0.002	$4d^{10}5s$	$(^3S^o)S_{0,5}$	0.0	61.527.0	3.34E+09	B, TW
60		1627.249(8)	61.453.4	1627.247(8)	0.002	$4d^{10}6p$	$(^3S^o)P_{1,5}$	145.926.21	207.379.7	1.37E+08	B
49		1628.330(8)	61.412.6	1628.331(8)	-0.001	$4d^{10}6p$	$(^3S^o)P_{1,5}$	145.926.21	207.338.8	1.52E+07	B
35		1635.594(8)	61.142.1	1635.591(6)	0.003	$4d^{10}6p$	$(^3S^o)P_{1,5}$	145.926.21	207.068.43	5.93E+07	B
180	w	1642.237(16)	60.892.6	1642.232(6)	0.005	$4d^{10}5p$	$(^3D^o)D_{1,5}$	61.527.0	122.419.73	4.70E+08	B, TW
65		1667.581(8)	59.967.1	1667.579(5)	0.002	$4d^95s2p$	$(^3D^o)D_{2,5}$	115.572.19	175.539.35	2.38E+07	B
60		(1708.662)	58.525.3	1708.694(5)	-0.001	$4d^95s5p$	$(^3D^o)D_{1,5}$	115.572.19	180.943.95	2.48E+06	#
400	w	1748.728(16)	57.184.4	1748.741(11)	-0.013	$4d^{10}5s$	$(^3S^o)P_{0,5}$	0.0	57.184.0	1.38E+09	B, TW
14		1757.432(8)	56.901.2	1757.433(8)	-0.001	$4d^95s2p$	$(^3D^o)D_{1,5}$	122.419.73	179.320.9	6.87E+06	#
68		1767.840(8)	56.566.2	1767.832(5)	0.008	$4d^{10}5d$	$(^3F^o)F_{2,5}$	128.748.36	185.024.81	6.40E+07	B
53		1776.943(8)	56.276.4	1776.941(5)	0.002	$4d^{10}5d$	$(^3S^o)F_{2,5}$	128.748.33	185.024.81	1.31E+07	B
40		1779.457(8)	56.196.9	1779.451(5)	0.006	$4d^95s2p$	$(^3D^o)D_{1,5}$	122.419.73	178.616.85	5.00E+06	B
65		1779.704(8)	56.189.1	1779.708(5)	-0.004	$4d^{10}6p$	$(^3S^o)P_{0,5}$	144.589.32	200.778.32	1.44E+08	B
70		1781.020(8)	56.147.6	1781.019(6)	0.001	$4d^{10}5d$	$(^3S^o)F_{3,5}$	128.748.33	184.895.95	2.40E+08	B
50		1792.962(8)	55.773.63	1792.968(6)	-0.006	$4d^{10}6p$	$(^3S^o)P_{0,5}$	144.589.32	200.362.77	5.11E+07	B
40		1793.146(8)	55.677.91	1793.143(5)	0.003	$4d^95s2p$	$(^3D^o)D_{1,5}$	122.419.73	178.867.74	2.70E+05	B
19		1803.500(8)	55.447.74	1803.491(5)	0.009	$4d^95s2p$	$(^3D^o)D_{1,5}$	122.419.73	177.867.74	9.39E+05	B
60		1821.158(8)	54.910.12	1821.169(5)	-0.011	$4d^{10}6p$	$(^3S^o)P_{1,5}$	145.926.21	200.836.01	2.44E+08	B
41		1823.097(8)	54.851.72	1823.084(5)	0.013	$4d^{10}6p$	$(^3S^o)P_{1,5}$	145.926.21	200.778.32	2.70E+07	B
29		1823.363(8)	54.843.71	1823.365(6)	-0.002	$4d^95s2p$	$(^3D^o)D_{1,5}$	122.419.73	177.263.38	8.19E+06	B
60		1837.300(8)	54.436.40	1837.301(6)	0.005	$4d^{10}6p$	$(^3S^o)P_{1,5}$	145.926.21	200.362.77	9.55E+07	B
80	w	1850.280(16)	54.045.9	1850.303(8)	-0.023	$4d^95s2p$	$(^3D^o)D_{2,5}$	61.527.0	115.572.19	2.28E+08	B, TW
70		1882.547(8)	53.119.52	1882.544(6)	0.003	$4d^95s2p$	$(^3D^o)D_{1,5}$	122.419.73	175.539.35	1.09E+07	B
13		1905.284(8)	52.485.61	1905.285(6)	-0.001	$4d^95s5p$	$(^3D^o)D_{1,5}$	128.748.36	180.943.95	2.37E+05	#

Table 3. Cont.

$J_{obs}^a$	ch <sup>b</sup>	$\lambda_{obs}^c, \text{ \AA}$	$\sigma_{obs}^d, \text{ cm}^{-1}$	$\lambda_{Ritz}^e, \text{ \AA}$	$\Delta\lambda_{Ritz}^e, \text{ \AA}$	Classification <sup>f</sup>	$gA^h, S^{-1}$	$E_{upp}^i, \text{ cm}^{-1}$	$gA^h, S^{-1}$	#	Lin.	Ref <sup>i</sup>	
19		1915.881(8)	521.953(1)	1915.870(6)	0.011	4d <sup>10</sup> 5d	( <sup>3</sup> D) <sup>2</sup> D <sub>3,5</sub>	180.943.95	1.26E+05		B		
50		1923.343(10)	51.992(8)	1923.343(10)	0.000	4d <sup>10</sup> 4f	( <sup>1</sup> S) <sup>2</sup> F <sub>3,5</sub>	128.748.33	2.19E+08	sh	B		
46		1923.654(10)	51.984.4	1923.662(7)	-0.008	4d <sup>10</sup> 4f	( <sup>1</sup> S) <sup>2</sup> F <sub>3,5</sub>	161.974.14	2.19E+08	sh	B		
75		1931.728(8)	51.767.12	1931.731(7)	-0.003	4d <sup>9</sup> 5s <sup>2</sup>	( <sup>3</sup> D) <sup>2</sup> D <sub>3,5</sub>	115.572.19	1.63E+07	#	B		
58		(1932.89)	51.736.00	1932.854(8)	-	4d <sup>10</sup> 6s	( <sup>1</sup> S) <sup>2</sup> S <sub>0,5</sub>	126.879.89	3.74E+06		B		
38		1949.021(8)	51.307.81	1949.020(6)	0.001	4d <sup>10</sup> 6s	( <sup>1</sup> S) <sup>2</sup> S <sub>0,5</sub>	126.879.89	2.11E+06		B		
38		1961.245(8)	50.988.02	1961.252(6)	-0.007	4d <sup>10</sup> 6s	( <sup>1</sup> S) <sup>2</sup> S <sub>0,5</sub>	126.879.89	3.29E+05	#	B		
75		(1965.976)	50.865.32	1966.083(11)	-	4d <sup>9</sup> 5s <sup>2</sup> p	( <sup>3</sup> D) <sup>2</sup> D <sub>3,5</sub>	179.320.9	1.19E+05	#	B		
30		1984.780(8)	50.383.42	1984.777(6)	0.003	4d <sup>10</sup> 6s	( <sup>1</sup> S) <sup>2</sup> D <sub>1,5</sub>	128.458.36	1.38E+05	#	B		
10		1993.680(8)	50.158.50	1993.680(6)	0.000	4d <sup>10</sup> 5d	( <sup>1</sup> S) <sup>2</sup> D <sub>1,5</sub>	128.458.36	4.67E+05	#	B		
66		2004.620(20)	49.868.6	2004.624(8)	-0.004	4d <sup>10</sup> 5d	( <sup>1</sup> S) <sup>2</sup> D <sub>1,5</sub>	128.458.36	3.64E+07	#	B		
36		2010.200(20)	49.730.2	2010.235(8)	-0.035	4d <sup>10</sup> 5d	( <sup>3</sup> D) <sup>2</sup> D <sub>3,5</sub>	178.187.72	2.68E+07	#	B		
63		2023.260(20)	49.409.3	2023.255(7)	0.005	4d <sup>10</sup> 5d	( <sup>1</sup> S) <sup>2</sup> D <sub>1,5</sub>	128.458.36	8.57E+06	#	B		
76		2035.190(20)	49.119.7	2035.201(6)	-0.011	4d <sup>10</sup> 5d	( <sup>1</sup> S) <sup>2</sup> D <sub>1,5</sub>	177.867.74	5.75E+07	#	B		
76		2048.310(20)	48.805.1	2048.313(8)	-0.003	4d <sup>10</sup> 5d	( <sup>1</sup> S) <sup>2</sup> D <sub>1,5</sub>	128.748.33	1.84E+07	#	B		
74		2051.070(20)	48.739.4	2051.092(8)	-0.022	4d <sup>10</sup> 4f	( <sup>1</sup> S) <sup>2</sup> F <sub>2,5</sub>	161.974.14	3.39E+08	#	B		
78		2051.410(20)	48.731.3	2051.423(9)	-0.013	4d <sup>10</sup> 4f	( <sup>1</sup> S) <sup>2</sup> F <sub>2,5</sub>	161.974.14	1.25E+07	#	B		
10		2136.480(20)	46.791.2	2136.488(9)	-0.008	4d <sup>10</sup> 5d	( <sup>1</sup> S) <sup>2</sup> D <sub>2,5</sub>	128.748.33	3.77E+05	#	B		
81		(2154.04)	46.409.8	2154.039(11)	-	4d <sup>9</sup> 5s <sup>2</sup>	( <sup>1</sup> D) <sup>2</sup> D <sub>2,5</sub>	115.572.19	1.48E+08	#	B		
80		2154.400(20)	46.402.0	2154.404(10)	-0.004	4d <sup>10</sup> 5d	( <sup>1</sup> D) <sup>2</sup> D <sub>2,5</sub>	161.974.14	8.14E+06	#	B		
77		2199.550(20)	45.449.7	2199.558(13)	-0.008	4d <sup>10</sup> 6p	( <sup>1</sup> S) <sup>2</sup> P <sub>0,5</sub>	144.589.32	3.15E+08	#	B		
42		(2201.47)	45.410.0	2201.686(19)	-	4d <sup>10</sup> 4f	( <sup>1</sup> S) <sup>2</sup> F <sub>2,5</sub>	161.974.14	2.98E+05	#	B		
10		(2203.54)	45.367.4	2203.671(18)	-	4d <sup>10</sup> 4f	( <sup>1</sup> S) <sup>2</sup> F <sub>2,5</sub>	161.974.14	4.11E+06	#	B		
45		2225.480(20)	44.920.2	2225.512(11)	-0.032	4d <sup>9</sup> 5s <sup>2</sup>	( <sup>1</sup> D) <sup>2</sup> D <sub>1,5</sub>	122.419.73	8.27E+05	#	B		
75		2232.170(20)	44.785.5	2232.188(13)	-0.018	4d <sup>10</sup> 6p	( <sup>1</sup> S) <sup>2</sup> P <sub>0,5</sub>	144.589.32	9.32E+07	#	B		
77		2261.230(20)	44.210.0	2261.227(19)	0.003	4d <sup>10</sup> 6p	( <sup>1</sup> S) <sup>2</sup> P <sub>1,5</sub>	190.136.3	5.25E+08	#	B		
74		2266.230(20)	44.112.5	2266.226(14)	0.004	4d <sup>10</sup> 6p	( <sup>1</sup> S) <sup>2</sup> P <sub>1,5</sub>	145.926.21	5.80E+07	#	B		
78		2272.370(20)	43.993.3	2272.417(9)	-0.047	4d <sup>10</sup> 4f	( <sup>1</sup> S) <sup>2</sup> F <sub>2,5</sub>	161.974.14	205.966.56	5.74E+08	#	B	
80		2272.810(20)	43.984.8	2272.812(13)	-0.002	4d <sup>10</sup> 4f	( <sup>1</sup> S) <sup>2</sup> F <sub>2,5</sub>	161.974.14	205.966.76	7.44E+08	#	B	
81		2300.890(20)	43.448.1	2300.878(14)	0.012	4d <sup>10</sup> 4f	( <sup>1</sup> S) <sup>2</sup> P <sub>1,5</sub>	145.926.21	1.72E+08	#	B		
74		2527.380(20)	39.554.8	2527.403(11)	-0.023	4d <sup>10</sup> 6p	( <sup>1</sup> D) <sup>2</sup> D <sub>1,5</sub>	122.419.73	1.45E+09	#	B		
10		(2572.42)	38.862.3	2572.446(15)	-	4d <sup>10</sup> 4f	( <sup>1</sup> S) <sup>2</sup> F <sub>2,5</sub>	161.974.14	200.836.01	4.91E+05	#	B	
30		(2572.94)	38.854.4	2572.966(17)	-	4d <sup>10</sup> 4f	( <sup>1</sup> S) <sup>2</sup> F <sub>2,5</sub>	161.982.00	9.82E+06	#	B		
22		(2576.15)	38.806.0	2576.270(15)	-	4d <sup>10</sup> 4f	( <sup>1</sup> S) <sup>2</sup> P <sub>0,5</sub>	161.974.14	200.778.32	6.77E+06	#	B	
85		2725.460(20)	36.680.2	2725.462(19)	-0.002	4d <sup>10</sup> 4f	( <sup>1</sup> S) <sup>2</sup> F <sub>2,5</sub>	161.974.14	198.651.3	1.13E+09	#	B	
86	*	2726.07(6)	36.672.0	2726.046(23)	0.02	4d <sup>10</sup> 6g	( <sup>1</sup> S) <sup>2</sup> G <sub>3,5</sub>	161.982.00	198.654.3	4.18E+07	#	B	
86	*	2726.07(6)	36.672.0	2726.07(6)	0.000	4d <sup>10</sup> 4f	( <sup>1</sup> S) <sup>2</sup> F <sub>2,5</sub>	161.982.00	198.654.0	1.46E+09	#	B	
26		(2923.41)	34.196.62	2923.223(3)	-	4d <sup>10</sup> 7p	( <sup>1</sup> S) <sup>2</sup> P <sub>0,5</sub>	177.263.38	211.462.1	8.81E+06	#	B	
80		2982.800(20)	33.515.77	2982.799(14)	0.001	4d <sup>10</sup> 5d	( <sup>1</sup> S) <sup>2</sup> D <sub>1,5</sub>	128.458.36	161.974.14	2.16E+09	#	S	

Table 3. Cont.

$J_{obs}^a$	ch <sup>b</sup>	$\lambda_{obs}^c$ Å	$\sigma_{obs}^d$ cm <sup>-1</sup>	$\lambda_{lit}^e$ Å	$\Delta\lambda_{lit}^f$ e Å	Classification <sup>f</sup>	$E_{low}^g$ cm <sup>-1</sup>	$E_{upp}^g$ cm <sup>-1</sup>	$gA^h$ s <sup>-1</sup>	Lin.	Ref <sup>i</sup>
82		3008.080(20)	33,234.11	3008.120(15)	-0.040	4d <sup>10</sup> 5d	(S) <sup>2</sup> D <sub>3,5</sub>	161,982.00	4.91E+09	S	
77		(3008.76)	33,226.60	3008.832(17)		4d <sup>10</sup> 5d	(S) <sup>2</sup> D <sub>2,5</sub>	128,748.33	2.44E+08	B	
45		(3293.56)	30,353.54	3293.51(3)		4d <sup>10</sup> 6p	(P) <sup>2</sup> D <sub>3,5</sub>	115,572.19	145,926.21	4.41E+06	B
21		3438.970(20)	29,070.14	3438.960(18)	0.010	4d <sup>10</sup> 5f	(S) <sup>2</sup> F <sub>3,5</sub>	184,895.95	213,966.18	2.06E+08	B
37		(3551.03)	28,152.80	3550.84(6)		4d <sup>10</sup> 4f	(S) <sup>2</sup> F <sub>3,5</sub>	161,982.00	190,136.3	1.84E+07	B
28		(3562.35)	28,063.34	3562.18(5)		4d <sup>10</sup> 4f	(S) <sup>2</sup> F <sub>2,5</sub>	161,974.14	190,038.8	1.27E+07	B
30	*	3640.69(10)	27,459.5	3640.69(10)	0.00	4d <sup>10</sup> 5g	(S) <sup>2</sup> G <sub>4,5</sub>	186,528.26	213,987.75	1.37E+08	B
30	*	3640.69(10)	27,459.5	3640.64(8)	0.05	4d <sup>10</sup> 5g	(S) <sup>2</sup> G <sub>4,5</sub>	186,527.40	213,987.3	1.11E+08	B
30	*	3640.69(10)	27,459.5	3640.75(8)	-0.06	4d <sup>10</sup> 5g	(S) <sup>2</sup> G <sub>4,5</sub>	186,528.26	213,987.3	2.53E+06	B
91		3653.010(20)	25,946.38	3653.001(17)	0.009	4d <sup>10</sup> 6p	(S) <sup>2</sup> P <sub>0,5</sub>	144,589.32	170,535.76	1.15E+09	B
65		3872.630(20)	25,814.93	3872.630(20)	0.000	4d <sup>10</sup> 5f	(S) <sup>2</sup> F <sub>3,5</sub>	184,895.95	210,710.88	3.11E+08	B
45		3891.740(20)	25,688.17	3891.731(19)	0.009	4d <sup>10</sup> 5f	(S) <sup>2</sup> F <sub>2,5</sub>	185,024.81	210,713.04	2.42E+08	B
86		(4023.82)	24,844.98	4023.77(3)		4d <sup>10</sup> 6p	(S) <sup>2</sup> P <sub>0,5</sub>	144,589.32	169,434.59	2.29E+08	B
90		4032.320(20)	24,792.61	4032.322(20)	-0.002	4d <sup>10</sup> 6p	(S) <sup>2</sup> P <sub>1,5</sub>	145,926.21	170,718.81	1.81E+09	S
88		4062.510(20)	24,609.59	4062.516(17)	-0.006	4d <sup>10</sup> 6d	(S) <sup>2</sup> D <sub>3,5</sub>	145,926.21	170,535.76	1.97E+08	B
81		4071.640(20)	24,553.20	4071.629(19)	0.011	4d <sup>10</sup> 4f	(S) <sup>2</sup> F <sub>2,5</sub>	161,974.14	186,527.40	2.96E+09	B
92		4072.780(20)	24,546.32	4072.790(19)	-0.010	4d <sup>10</sup> 4f	(S) <sup>2</sup> F <sub>3,5</sub>	161,982.00	186,528.26	1.10E+08	B
40	*	4128.42(10)	24,215.5	4128.42(10)	0.00	4d <sup>10</sup> 5g	(S) <sup>2</sup> G <sub>4,5</sub>	186,528.26	210,743.8	2.43E+08	B
40	*	4128.42(10)	24,215.5	4128.35(8)	0.07	4d <sup>10</sup> 5g	(S) <sup>2</sup> G <sub>3,5</sub>	186,527.40	210,743.3	1.98E+08	B
40	*	4128.42(10)	24,215.5	4128.50(8)	-0.08	4d <sup>10</sup> 5g	(S) <sup>2</sup> G <sub>4,5</sub>	186,528.26	210,743.3	4.50E+06	B
38		(4233.56)	23,614.13	4233.50(6)		4d <sup>10</sup> 6d	(S) <sup>2</sup> D <sub>3,5</sub>	177,263.38	210,743.3	7.87E+06	B
64		(4250.94)	23,517.59	4251.42(4)		4d <sup>10</sup> 7p	(S) <sup>2</sup> P <sub>0,5</sub>	177,263.38	200,778.32	7.93E+07	B
88		4252.600(20)	23,508.41	4252.605(20)	-0.005	4d <sup>10</sup> 6p	(S) <sup>2</sup> P <sub>1,5</sub>	145,926.21	169,434.59	3.93E+08	B
80		(4252.91)	23,506.69	4252.95(4)		4d <sup>10</sup> 5s <sup>2</sup>	(P) <sup>2</sup> D <sub>1,5</sub>	122,419.73	145,926.21	1.51E+07	B
40		(4328.03)	23,098.71	4327.90(5)		4d <sup>10</sup> 7p	(S) <sup>2</sup> P <sub>0,5</sub>	177,263.38	200,362.77	2.32E+07	B
12		4352.620(20)	22,968.21	4352.609(19)	0.011	4d <sup>10</sup> 7p	(S) <sup>2</sup> P <sub>1,5</sub>	177,263.38	200,836.01	1.48E+08	B
2		4363.560(20)	22,910.63	4363.569(19)	-0.009	4d <sup>10</sup> 7p	(S) <sup>2</sup> P <sub>1,5</sub>	177,867.74	200,778.32	1.65E+07	B
50		(4444.56)	22,494.11	4444.18(4)		4d <sup>10</sup> 7p	(S) <sup>2</sup> P <sub>1,5</sub>	177,867.74	200,362.77	4.83E+07	B
22		(4479.97)	22,315.32	4480.24(8)		4d <sup>10</sup> 9d	(S) <sup>2</sup> D <sub>3,5</sub>	185,024.81	207,338.8	5.53E+06	B
87		(4509.78)	22,167.81	4509.42(4)		4d <sup>10</sup> 6p	(S) <sup>2</sup> P <sub>0,5</sub>	122,419.73	144,589.32	6.28E+07	B
73	*	4744.58(6)	21,070.8	4744.62(4)	-0.04	4d <sup>10</sup> 5f	(S) <sup>2</sup> F <sub>3,5</sub>	184,895.95	205,966.56	1.44E+07	B
73	*	4744.58(6)	21,070.8	4744.58(5)	0.00	4d <sup>10</sup> 7g	(S) <sup>2</sup> F <sub>2,5</sub>	184,895.95	205,966.56	5.05E+08	B
63	*	4773.830(20)	20,941.69	4773.815(19)	0.015	4d <sup>10</sup> 5f	(S) <sup>2</sup> F <sub>2,5</sub>	185,024.81	205,966.56	3.93E+08	B
44	*	5130.85(10)	19,484.5	5130.85(10)	0.00	4d <sup>10</sup> 5g	(S) <sup>2</sup> G <sub>4,5</sub>	186,528.26	206,012.78	5.20E+08	B
44	*	5130.85(10)	19,484.5	5130.75(8)	0.10	4d <sup>10</sup> 7h	(S) <sup>2</sup> H <sub>4,5</sub>	186,527.40	206,012.3	4.23E+08	B
44	*	5130.85(10)	19,484.5	5130.98(8)	-0.13	4d <sup>10</sup> 7h	(S) <sup>2</sup> H <sub>4,5</sub>	186,528.26	206,012.3	9.62E+06	B

Table 3. Cont.

$I_{\text{obs}}^a$	ch <sup>b</sup>	$\lambda_{\text{obs}}^c \text{ \AA}$	$\sigma_{\text{obs}}^c \text{ cm}^{-1}$	$\lambda_{\text{Ritz}}^d \text{ \AA}$	$\Delta\lambda_{\text{O-Ritz}}^e \text{ \AA}$	Classification <sup>f</sup>	$E_{\text{low}} \text{ cm}^{-1}$	$E_{\text{upp}} \text{ cm}^{-1}$	$gA^h \text{ s}^{-1}$	Lin. Ref <sup>i</sup>
72		(5248.77)	19,046.78	5248.90(6)	4d <sup>10</sup> 6s	( <sup>1</sup> S) <sup>2</sup> S <sub>0,5</sub>	( <sup>1</sup> S) <sup>2</sup> P <sub>1,5</sub>	145,926.21	4.79E+08	S
70		(5644.96)	17,710.00	5645.14(7)	4d <sup>10</sup> 6s	( <sup>1</sup> S) <sup>2</sup> S <sub>0,5</sub>	( <sup>1</sup> S) <sup>2</sup> P <sub>0,5</sub>	144,589.32	1.96E+08	B
76		(5722.71)	17,469.39	5723.22(7)	4d <sup>10</sup> 5d	( <sup>1</sup> S) <sup>2</sup> D <sub>3,5</sub>	( <sup>1</sup> S) <sup>2</sup> P <sub>1,5</sub>	145,926.21	2.50E+07	B
70		(5819.41)	17,179.11	5819.83(8)	4d <sup>10</sup> 5d	( <sup>1</sup> S) <sup>2</sup> D <sub>3,5</sub>	( <sup>1</sup> S) <sup>2</sup> P <sub>1,5</sub>	145,926.21	3.39E+08	B
40		(6197.72)	16,130.50	6197.54(9)	4d <sup>10</sup> 5d	( <sup>1</sup> S) <sup>2</sup> D <sub>1,5</sub>	( <sup>1</sup> S) <sup>2</sup> P <sub>0,5</sub>	144,589.32	1.02E+08	B
10		(6520.50)	15,332.01	6519.8(5)	4d <sup>10</sup> 6g	( <sup>1</sup> S) <sup>2</sup> G <sub>4,5</sub>	( <sup>1</sup> S) <sup>2</sup> H <sub>5,5</sub>	213,987.75	1.49E+08	B

<sup>a</sup> Observed relative intensities on an arbitrary scale (1–400) for the blackening of the lines on the photographic plates. Response functions of the instruments were not taken into account.  
<sup>b</sup> Character of the observed line encoded as follows: w—wide line; f—faint line; sh—shaded line; \*—intensity shared by two or more transitions. <sup>c</sup> Observed and Ritz wavelengths are given in standard air for wavenumber  $\sigma$  between 5000  $\text{cm}^{-1}$  and 50,000  $\text{cm}^{-1}$  and in vacuum outside of this range. The uncertainty (standard deviation) in the last digit is given in parentheses for both  $\lambda_{\text{obs}}$  and  $\lambda_{\text{Ritz}}$ . ( $\lambda$ ) denotes values not included in the level optimization. <sup>d</sup> Ritz wavelengths and their uncertainties were determined in the least-squares level optimization procedure LOPT [15]. <sup>e</sup> Difference between observed and Ritz wavelength. If this column is blank, the line was excluded from the level optimization because its observed wavelength deviates from the Ritz value by more than our given uncertainty. <sup>f</sup> Classification specifies the lower and upper levels of the transition. <sup>h</sup> Weighted transition probability values ( $g = 2J_{\text{upper}} + 1$  is statistical weight of the upper level). If marked as # then the given  $gA$  values are too unreliable for the transitions whose cancellation factor |CFI| < 0.10 in our calculations with Cowan's code [12]. <sup>i</sup> Reference to the source: B—Bhatia et al. [6]; B, TW—Wavelength from this work; K—Kaufman et al. [7]; R—Ryabsev et al. [9]; S—Skočič et al. [10]; TW—this work.



#### 4.1. The $4d^{10}5s- [4d^{10}np]$ Transition Array

The resonance transitions  $4d^{10}5s-4d^{10}5p$  were first reported by Rao [1], and confirmed by all other workers [2–5]. We observed these two lines in our indium spectra with high intensity. They were the main reference in establishing the In III ionization characteristics. Bhatia [6] reported the levels of  $4d^{10}np$  ( $n = 5-9$ ). We agreed with Bhatia's analysis only up to  $4d^{10}8p$ . The  $4d^{10}5s-4d^{10}9p$  transitions could not be seen in our spectra. The reported level value of  $4d^{10}9p\ ^2P_{3/2,1/2}$  at  $201,180.3\text{ cm}^{-1}$  did not fit in our least squares fitted parametric calculations. Our predicted values were found to be at  $203,388.5\text{ cm}^{-1}$  and  $203,556.3\text{ cm}^{-1}$  for  $^2P_{3/2}$  and  $^2P_{1/2}$ , respectively. A plot of the energy differences between observed and Hartree-Fock (HF) calculated values of  $4d^{10}np$  ( $n = 5-9$ )  $^2P_{3/2}$  series is shown in Figure 2, and it is evident from this figure that the reported value for  $4d^{10}9p$  levels shows an irregular behavior. Therefore, this reported level seems to be doubtful. We did not find any alternative value as  $4d^{10}9p$  transitions were too weak to be observed on our plates.

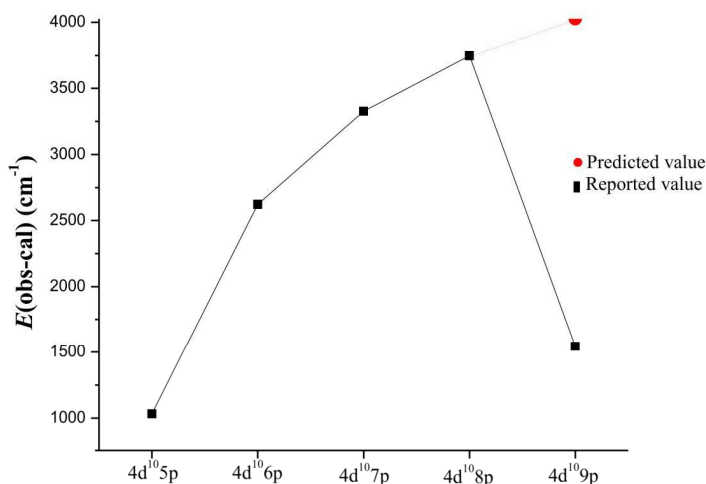
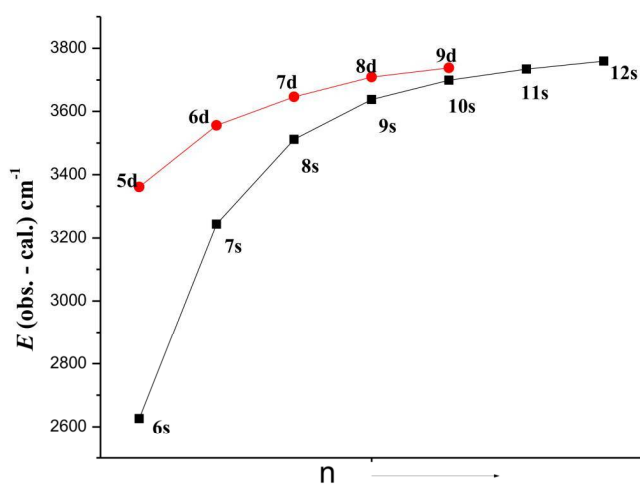


Figure 2. A plot of the observed and calculated energy difference in  $4d^{10}np$  series of In III.

#### 4.2. The $4d^{10}np-[4d^{10}(ns + nd) + 4d^95s^2]$ Transition Array

The second excitation,  $4d^{10}5p-[4d^{10}(6s + 5d) + 4d^95s^2]$  transitions, is also observed to be quite strong. In the  $4d^{10}ns$  series, we observed transitions  $4d^{10}5p-4d^{10}ns$  ( $n = 6-8$ ) and  $4d^{10}6p-4d^{10}ns$  ( $n = 9-12$ ), and, in the  $4d^{10}nd$  series, three transitions are possible between each of the  $4d^{10}np-4d^{10}nd$  configurations out of which two transitions, namely  $^2P_{1/2}-^2D_{3/2}$  and  $^2P_{3/2}-^2D_{5/2}$ , were observed to be quite strong, while the third transition,  $^2P_{3/2}-^2D_{3/2}$ , was predicted to be weak in the series. All these three transitions were observed in  $4d^{10}[5p-nd]$  ( $n = 5-7$ ). Thus, we confirmed the levels of the  $4d^{10}ns$  ( $n = 6-12$ ) and  $4d^{10}nd$  ( $n = 5-7$ ) configurations. The transitions from  $4d^{10}nd$  ( $n = 8, 9$ ) to  $4d^{10}5p$  were not observed on our plates. However, these transitions were reported by Bhatia [6]. We examined these levels and found their scaling factor to be quite regular. Secondly, a similar plot as in Figure 2 with the average energy difference between the calculated and observed values shows a regular behavior for the  $4d^{10}ns$  and  $4d^{10}nd$  series (Figure 3). Although we could not confirm the levels of the  $4d^{10}nd$  ( $n = 8, 9$ ) configurations, on the basis of their regularity, we included them in Table 2 for the sake of completeness.



**Figure 3.** A plot  $E(\text{obs.-cal.})$  for the  $4d^{10}ns$  and  $4d^{10}nd$  series in In III.

The other configuration  $4d^95s^2$  in even parity system has two inverted  $^2D$  levels having the same energy range as the  $4d^{10}5d$   $^2D$  levels. Both  $^2D$  levels of these two configurations interact with each other. As a result of this interaction,  $4d^{10}5p-4d^95s^2$  transitions are observed. Further confirmation of these two levels was made by the observed transitions from the levels of the  $4d^95s5p$  configuration that will be discussed later.

#### 4.3. The $4d^{10}(nf + ng + nh)$ Configurations

The  $4d^{10}5d-4d^{10}4f$  transitions lie beyond our wavelength region of investigation (above 2080 Å); therefore, we could not confirm them experimentally in the present work. However, these levels were well established by Nodwell [4] along with levels of the  $4d^{10}ng$  ( $n = 5-7$ ) series by observing transitions from  $4d^{10}4f$ . The repeated appearance of the  $4d^{10}4f$   $^2F_{5/2,7/2}$  interval in transitions from the  $4d^{10}(5g, 6g \text{ and } 7g)$   $^2G_{7/2,9/2}$  levels confirms the correctness of the  $4d^{10}4f$  levels. The latter were compiled in AEL [5] and were later confirmed by Bhatia [6]. The  $4d^{10}5d-4d^{10}5f$  transitions lie in our wavelength region. We observed a pair of lines from  $4d^{10}5d$   $^2D_{3/2}$  and  $^2D_{5/2}$ , and two transitions from  $4d^95s^2$   $^2D_{5/2,3/2}$ , thus confirming  $4d^{10}5f$   $^2F_{5/2}$ . The other level  $4d^{10}5f$   $^2F_{7/2}$  is also expected to give two transitions, one from  $4d^{10}5d$   $^2D_{5/2}$  and the other from  $4d^95s^2$   $^2D_{5/2}$ ; both were in fact found. Furthermore, the level positions agree well with theoretical prediction of an inverted doublet. The  $4d^{10}6f$   $^2F_{5/2,7/2}$  levels are strongly mixed with the  $4d^95s5p$   $^2F_{5/2,7/2}$  levels. Bhatia [6] reported only the  $4d^{10}6f$   $^2F_{5/2}$  level at  $198,499.3 \text{ cm}^{-1}$ , but our least squares fitted calculation predicted at  $191,337 \text{ cm}^{-1}$ . This large deviation does not seem to be right. Bhatia [6] reported unresolved  $4d^{10}7f$  levels, but we did not find his identified lines on our line list. Therefore, his  $4d^{10}6f$  and  $4d^{10}7f$  levels could not be confirmed.

Neither the  $4d^{10}4f-4d^{10}ng$  ( $n = 5-7$ ) nor  $4d^{10}5g-4d^{10}nh$  ( $n = 7-9$ ) transitions lie in our wavelength region. Therefore, they could not be confirmed in the present work. However, we have compared Bhatia's experimental results [6] with the theoretical calculations for the known spectra in the isoelectronic sequence from Ag I–Sn IV [11], and they appear to be regular. The  $4d^{10}4f-(8g + 9g)$  transitions do lie in our wavelength region, but they are too weak to be verified. However, we have included them in our LSF calculations for the sake of completeness.

#### 4.4. The $4d^9 5s 5p$ Configuration

This configuration arises due to core excitation of the ground level configuration  $4d^{10} 5s$ . A number of levels from this configuration were reported by Bhatia [6]. Kaufman et al. [7] revised three levels of this configuration by observing transitions from the ground level  $4d^{10} 5s \ ^2S_{1/2}$ , thus connecting only  $J = 1/2$  and  $3/2$  levels. The remaining levels of Bhatia (with  $J = 5/2, 7/2$  and  $9/2$ ) still remain to be verified. In the present investigation, we agreed with six levels of Kaufman et al. [7] but revised four levels. The ionization separation on our recorded spectrum in this wavelength region was quite clear, thus new levels could be found with full confidence. The level  $^2P_{1/2}$  reported by Bhatia [6] at  $199,561.2 \text{ cm}^{-1}$  was revised by Kaufman et al. [7] to a new position at  $197,081 \text{ cm}^{-1}$ . The line ( $507.406 \text{ \AA}$ ) used by Kaufman et al. [7] for this transition actually belongs to O III ( $507.391 \text{ \AA}$ ) [11] and the line used by Bhatia was not found on our spectrograms. We found an unclassified In III line with moderate intensity at  $504.080 \text{ \AA}$  that has been assigned to this transition, yielding the level value at  $198,382.2 \text{ cm}^{-1}$  that also fits well in the least squares calculations.

Kaufman et al. [7] had revised another  $J = 1/2$  level of Bhatia [6] and re-designated it as a  $J = 3/2$  level at  $170,888 \text{ cm}^{-1}$  based on Bhatia's line list as they did not observe the corresponding lines. We also could not find the lines associated with this level in our line list. Therefore, this level was rejected. According to our analysis, we found that the lowest  $J = 1/2$  level reported by Kaufman et al. [7] at  $170,812 \text{ cm}^{-1}$  is in fact a  $J = 3/2$  level and the replacement for the lowest  $J = 1/2$  level is found at  $171,315.7 \text{ cm}^{-1}$ . The lowest  $J = 3/2$  level of this configuration reported by Kaufman et al. [7] at  $167,079 \text{ cm}^{-1}$  is in fact based on an In IV line ( $598.526 \text{ \AA}$ ) [16,17]. However, Bhatia [6] had reported this level at  $167,339.1 \text{ cm}^{-1}$ , which was based on a correct In III line at ( $597.589 \text{ \AA}$ ), and we agree with this identification. Moreover, it also gives two transitions from the recently found  $4d^9 5p^2$  configuration [9] that confirm the identification of this level.

The highest  $J = 3/2$  level was not found by Kaufman et al. [7] because calculations predict a weak transition to the ground level. However, Bhatia [6] had reported this level at  $202,132.3 \text{ cm}^{-1}$ . We found two strong lines with correct In III ionization characteristics, which we classified as transitions from  $4d^9 5s^2$  levels to the level in question. Thus, we confirmed Bhatia's level value. Table 4 shows the summary of the  $J = 1/2$  and  $3/2$  levels of the  $4d^9 5s 5p$  configuration given by previous researchers [6,7] and the present analysis.

**Table 4.** Energy level values ( $J = 1/2$  &  $3/2$  Levels) of  $4d^9 5s 5p$  Configuration.

Configuration ( $4d^9 5s 5p$ )	Previous Work		This Work	
	Bhatia [6]	Kaufman et al. [7]		
$(^3D)^4P_{1/2}$	170,888.3	170,812	171,315.7	Revised
$(^1D)^2P_{1/2}$	178,187.5	178,187	178,187.72	Verified
$(^3D)^4D_{1/2}$	179,321.0	179,321	179,320.9	Verified
$(^3D)^2P_{1/2}$	199,561.2	197,081	198,382.2	Revised
$(^3D)^4P_{3/2}$	167,339.1	167,079	167,339.24	Revised
$(^3D)^4F_{3/2}$	170,918.9	170,888	170,813.7	Revised
$(^1D)^2D_{3/2}$	175,538.7	175,538	175,539.35	Verified
$(^1D)^2P_{3/2}$	178,616.5	178,616	178,616.85	Verified
$(^3D)^4D_{3/2}$	180,945.0	180,945	180,943.95	Verified
$(^3D)^2P_{3/2}$	191,509.2	191,508	191,509.1	Verified
$(^3D)^2D_{3/2}$	202,132.3	-	202,134.5	Verified

The remaining 12 levels of this configuration with higher  $J$  values ( $5/2$ – $9/2$ ) were considered next. These levels have only been reported by Bhatia [6] through the transitions from  $4d^9 5s^2$ . We found lines corresponding to transitions from the  $J = 5/2$  level at  $194,902.6 \text{ cm}^{-1}$  and confirmed only this level in Bhatia's list. We were successful in locating 10 remaining levels of  $J = 5/2$  and  $7/2$  from transitions to  $4d^9 5s^2$  and  $4d^9 5p^2$  levels. The level with the highest  $J$  value ( $9/2$ ) does not connect to any other known configuration except  $4d^9 5p^2$ , which was partially known. We extended that configuration to

include  $J = 7/2$  levels. This paved the way for the establishment of the  $J = 9/2$  level. We found three transitions placing the  $J = 9/2$  level at  $168,947.6 \text{ cm}^{-1}$ . All 23 levels of  $4d^9 5s 5p$  configuration are now known experimentally.

#### 4.5. The $4d^9 5s$ ( $nf + np$ ) Configurations

These are the configurations that arise due to the core excitation. The  $4d^9 5s 4f$  configuration has a large energy spread and contains 39 levels. Since the ground configuration contains only the  $^2S_{1/2}$  level, only  $J = 1/2$  and  $3/2$  levels of the  $4d^9 5s 4f$  configuration can decay to the ground configuration. Kilbane et al. [8] have studied the  $4d^9 5s nf$  ( $n = 4-12$ ) and  $4d^9 5s np$  ( $n = 6-11$ ) configurations using a photoabsorption technique. They reported 10 levels of  $4d^9 5s 4f$  and seven levels of  $4d^9 5s 6p$  belonging to  $J = 1/2$  and  $3/2$ . In our spectra, these transitions lie in the shorter wavelength region, where reflectivity of the grating falls considerably in the normal incidence setting. Therefore, these transitions appeared with very weak intensity on our spectrograms. Secondly, a large number of In V [18] and In VI [19] transitions overlap in this region. Therefore, it was very difficult to identify confidently In III lines of this array. Moreover, these levels lie above the ionization limit and consequently have a very small population. Therefore, these levels could not be located in the present work. However, we performed least squares fitted parametric calculations to provide a precise prediction of the remaining levels of the  $4d^9 5s nf$  ( $n = 4-7$ ) and  $4d^9 5s np$  ( $n = 6-7$ ) configurations based on the identification made in reference [8].

#### 4.6. The $4d^9 5p^2$ Configuration

The first attempt to study the low-lying autoionizing configuration  $4d^9 5p^2$  in the sequence In III–Te VI was made by Ryabtsev et al. [9], connecting this configuration with  $4d^{10} 5p$ . It is important to note that all the levels of this configuration lie above the ionization limit. It was difficult to arrange experimental conditions providing for a reasonable population above the ionization limit. Certainly it was advantageous to identify the broad lines due to continuum effect, but only the strongest transitions could be observed. Not many pairs connecting to both  $4d^{10} 5p \ ^2P_{1/2,3/2}$  were found to confirm these levels. However, the lines used to locate these levels have a definite In III characteristic and show continuum broadening effect. Out of 28 levels of  $4d^9 5p^2$ , only 13 levels with  $J = 1/2, 3/2$  and  $5/2$  were reported by Ryabtsev et al. [9]. We should point out that two levels ( $^1D$ )  $^2S_{1/2}$  and ( $^1D$ )  $^2P_{3/2}$  were reported by Ryabtsev et al. [9] with the same energy level values. They were based on the double classification of the same pair of lines ( $555.669 \text{ \AA}$  and  $569.421 \text{ \AA}$ ). We agreed with assignments of these lines to ( $^1D$ )  $^2P_{3/2}$  giving the level value at  $237,145.6 \text{ cm}^{-1}$  as both transitions are predicted to be of the comparable intensity. However, the ( $^1D$ )  $^2S_{1/2}$  level is predicted to have one strong and one weak transition, and we found one unclassified line on our plate at  $555.501 \text{ \AA}$ , which we used to establish this level at  $237,201.7 \text{ cm}^{-1}$ . Several levels have also been confirmed through transitions to the  $4d^9 5s 5p$  configuration. The higher  $J$  values of  $4d^9 5p^2$  configuration ( $J = 7/2$  and  $9/2$ ) could only be established through transitions from  $4d^9 5s 5p$ . We were successful in establishing three  $J = 7/2$  and one  $J = 9/2$  levels. One  $J = 9/2$  and two  $J = 7/2$  levels remain unknown. The study of the  $4d^9 5p^2$  and  $4d^9 5s 5p$  configurations together complemented each other. The other even parity configuration  $4d^9 5s 5d$  lies above the ionization limit and partially overlaps the  $4d^9 5p^2$  configuration. It has also been incorporated in the least squares fitted parametric calculation to interpret the results.

### 5. Optimization of the Energy Levels

The transition wavelengths observed for this spectrum were used to derive the energy level values. For this purpose, a least-squares level optimization code LOPT [15] was used. The essential factors for the level optimization procedure are the correct identification of the spectral lines and estimation of their uncertainties. The wavelength uncertainty is determined by the combined effect of the statistical deviation of the line position measured on the comparator and systematic uncertainty of reference wavelengths used in the fitting. Ryabtsev et al. [9] reported the uncertainty of autoionized

lines to be  $\pm 0.006 \text{ \AA}$ . Our wavelength accuracy for sharp and unblended lines is estimated to be within  $\pm 0.006 \text{ \AA}$  and  $\pm 0.008 \text{ \AA}$  below and above  $900 \text{ \AA}$ . We estimated the uncertainty of Bhatia's lines to be  $\pm 0.008 \text{ \AA}$  for lines below  $2000 \text{ \AA}$  with the comparison of our measurement and Kaufman et al. [7] for sharp and unblended lines. Bhatia mentioned in his paper that the prism lines are not accurate to more than  $0.01 \text{ \AA}$ . However, he gave wavelengths above  $2000 \text{ \AA}$  with only two places after the decimal point implying that the uncertainty is at least  $0.02 \text{ \AA}$  or higher. In our level optimization with Bhatia's lines [6], we noticed several lines showing a deviation around  $0.22 \text{ \AA}$  for the region  $2000\text{--}4000 \text{ \AA}$  from their Ritz values. The deviation increases up to  $0.8 \text{ \AA}$  for the longer-wavelength region  $4000\text{--}6500 \text{ \AA}$ . We, therefore, did not use these lines with large deviation in the level optimization. All of the lines used in the optimization of the level values were given an estimated uncertainty to find the final optimized energy level values with an estimated uncertainty for each level. Since the level  $4d^{10}5p (^1S) ^2P_{3/2}$  connects with the largest number of observed transitions, it was adopted as the base level, hence all the level uncertainties in Table 2 are given with respect to this level. All the given uncertainties are taken to be at the level of one standard deviation.

## 6. Ionization Potential

Since more than one series with three members are known in In III, its ionization potential can be determined with good accuracy. The value of ionization potential of In III given in AEL [5] at  $226,100 \text{ cm}^{-1}$  was derived by Catalan and Rico [20] by comparison of the third spectra from Y to In. Bhatia [6] improved the value of ionization potential by using  $4d^{10}ng$  ( $n = 5\text{--}9$ ) and  $4d^{10}nh$  ( $n = 6\text{--}9$ ) in frames of the polarization theory [21]. He calculated the In III limit at  $226,191 \text{ cm}^{-1}$ ; this value is listed in the NIST Atomic Spectra Database [11]. We have calculated the ionization potential from two series,  $ns$  ( $n = 5\text{--}12$ ) and  $ng$  ( $n = 5\text{--}9$ ) using the Ritz quantum defect extrapolation method with the aid of the RITZPL code [22]. However, the non-penetrating ( $4d^{10}ng$ ) series is certainly expected to give more accurate value. The value of IP obtained using the three-parameter extended Ritz formula [22] for the  $4d^{10}ns$  ( $n = 5\text{--}12$ ) series is  $226,196.58 \text{ cm}^{-1}$ , while the values obtained by fitting the two-parameter extended Ritz formula for the two  $4d^{10}ng$   $^2G_{7/2,9/2}$  ( $n = 5\text{--}9$ ) series are  $226,197.00 \text{ cm}^{-1}$  and  $226,195.08 \text{ cm}^{-1}$ , respectively. The limits calculated by the POLAR code [22] for the  $ng$  ( $n = 5\text{--}9$ )  $^2G_{7/2, 9/2}$  series were found to be  $226,197.28$  and  $226,195.35 \text{ cm}^{-1}$ , respectively. The adopted value is the average of these calculations at  $226,196.3 \text{ cm}^{-1} \pm 1.0 \text{ cm}^{-1}$  ( $28.0448 \pm 0.0001 \text{ eV}$ ) differing by  $5 \text{ cm}^{-1}$  from Bhatia's value.

## 7. Conclusions

A total of 91 energy levels have been established, among which three levels are revised and 21 are new. All of these levels were based on the identification of 218 spectral transitions, 70 being new. The results were interpreted using Cowan's codes and the least square fitted parametric theory. The optimized energy levels and their calculated values are given in Table 2 along with the level uncertainty, *LS*-percentage compositions and number of connecting transitions. All of the classified transitions are given in Table 3 along with their weighted transition probabilities (*gA*) obtained with least squares fitted energy parameters. This table also contains the Ritz wavelengths of all transitions with their uncertainties obtained by using the level optimization code (LOPT).

**Author Contributions:** All authors contributed equally to this work.

**Conflicts of Interest:** The authors declare no conflict of interest.

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Article

# Identification and Plasma Diagnostics Study of Extreme Ultraviolet Transitions in Highly Charged Yttrium

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Academic Editor: Joseph Reader

Received: 17 July 2017; Accepted: 12 September 2017; Published: 18 September 2017

**Abstract:** Extreme ultraviolet spectra of the L-shell ions of highly charged yttrium ( $Y^{26+}$ – $Y^{36+}$ ) were observed in the electron beam ion trap of the National Institute of Standards and Technology using a flat-field grazing-incidence spectrometer in the wavelength range of 4 nm–20 nm. The electron beam energy was systematically varied from 2.3 keV–6.0 keV to selectively produce different ionization stages. Fifty-nine spectral lines corresponding to  $\Delta n = 0$  transitions within the  $n = 2$  and  $n = 3$  shells have been identified using detailed collisional-radiative (CR) modeling of the non-Maxwellian plasma. The uncertainties of the wavelength determinations ranged between 0.0004 nm and 0.0020 nm. Li-like resonance lines,  $2s$ – $2p_{1/2}$  and  $2s$ – $2p_{3/2}$ , and the Na-like D lines,  $3s$ – $3p_{1/2}$  and  $3s$ – $3p_{3/2}$ , have been measured and compared with previous measurements and calculations. Forbidden magnetic dipole (M1) transitions were identified and analyzed for their potential applicability in plasma diagnostics using large-scale CR calculations including approximately 1.5 million transitions. Several line ratios were found to show strong dependence on electron density and, hence, may be implemented in the diagnostics of hot plasmas, in particular in fusion devices.

**Keywords:** highly charged ions; yttrium; spectroscopy; extreme ultraviolet; Li-like; Na-like; magnetic dipole; plasma diagnostics; electron beam ion trap; non-Maxwellian plasma

## 1. Introduction

Multi-electron ions are under intense theoretical study as state-of-the-art calculations rival highly accurate measurements sensitive to higher order terms of quantum electrodynamics (QED) corrections to atomic energy levels [1]. While elements with a high-Z atomic number have these effects amplified, ions in the medium-Z region have special importance because they allow for more accurate experiments and provide constraints to theoretical trends. In the past few years, the electron beam ion trap (EBIT) research program at the National Institute of Standards and Technology (NIST) has reported accurate measurements in the extreme ultraviolet (EUV) region that focus on systematic observations of transitions in L-shell, M-shell and N-shell ions [2–14]. The work reported here extends these results to a range of previously unobserved transitions of a fifth row element, yttrium.

Yttrium was chosen for the current investigation because of its relevance as a possible diagnostic impurity in tokamak fusion plasmas. For instance, together with strontium, zirconium, niobium and molybdenum, yttrium has been injected into the Texas Experimental Tokamak (TEXT) [15,16], the Joint European Torus (JET) tokamak [17] and the Princeton tokamaks [18–20] and has also been

observed in laser-produced linear plasmas [16,21]. L-shell ions of high-Z elements, especially Be-like to Ne-like [22–26], and a few M-shell ions such as Na-like, Mg-like and Al-like [15,16,27–30] were used to diagnose these hot plasmas for decades. The elemental abundance of yttrium in stars also makes it astronomically important. Its relevance in nuclear astrophysics, weak interaction physics and nuclear structure physics has been discussed [31–34].

Among the various transitions in these elements, special interest is devoted to forbidden transitions that originate from long-lived metastable energy levels. The importance of the forbidden transitions in medium-Z and high-Z elements has been demonstrated by different researchers for astrophysical [35] and fusion [18,36] plasmas. For example, charge states near closed shells include potentially useful forbidden transitions such as those between the  $2s^2 2p^5 - 2s 2p^6$  configurations of F-like ions and the magnetic dipole transition  $2s^2 2p^5 \ ^2P_{3/2} - ^2P_{1/2}$  in the same ion. These have been extensively investigated in earlier studies [37–40].

There have been a few EUV measurements of highly charged yttrium over the past couple of decades. Alexander et al. observed the EUV spectra of Y IX–XIII in the wavelength range of 4.5 nm–35 nm using vacuum spark [41]. Ekberg et al. performed a series of measurements for the identification of transitions in Si-like Y XXVI [42], Al-like Y XXVII [43] and Mg-like Y XXVIII [21,28] in the EUV spectra emitted from line-focus laser-produced plasmas as part of the X-ray laser research program. Reader et al. have reported observations of F-like Y XXXI [37], Mg-like Y XXVIII [44] and Na-like Y XXIV [16,45] using laser-produced and tokamak plasmas in a series of systematic spectroscopic studies. Similar experiments for moderate charge states also reported observations of multiply-charged yttrium spectra (Y II–XI); see, e.g., [46–50]. Despite these experiments, the second row isoelectronic sequences of yttrium have largely been unexplored in the EUV region to date.

In this paper, we report the systematic study and identification of atomic spectral lines of the L-shell charge states of yttrium ranging from Li-like to Ne-like ions (Y XXX–Y XXXVII) created and trapped in the NIST EBIT [51,52]. We also present the most pronounced spectral lines of the Na-like, Mg-like and Al-like yttrium charge states, as these can provide benchmark experimental results for precise multi-electron atomic theory calculations. Na-like D1 and D2 lines originate from quasi-hydrogenic ions and have been used as a probe of QED contributions due to their high intensities and the available precise ab initio calculations [6,53–55]. We report the first data for the wavelengths of the Na-like D1 and D2 yttrium lines measured with an EBIT to provide accurate experimental results that complement the previously reported measurements of Reader et al. [45] in laser-produced and tokamak plasmas.

In addition to the spectral analysis, we also discuss the forbidden magnetic dipole (M1) transitions of highly charged yttrium ions that are potentially important for plasma diagnostics. The spectroscopy of forbidden magnetic dipole lines can help deduce important plasma parameters such as the density and temperature of plasmas. These parameters are obtained in practice from intensity ratios of various atomic spectral lines rather than direct measurements, which are difficult or even impossible in fusion, laboratory and astrophysical plasmas [56]. The availability of accurate collisional-radiative models makes this technique a reliable tool for plasma diagnostics [57–59].

M1 transition probabilities strongly depend on the spectroscopic charge  $Z_{sp}$ , and for highly ionized ions, these transitions become prominent. At low electron densities, the radiative decay rates are substantially larger than collisional depopulation from both metastable and allowed excited levels. At higher densities, however, the metastable levels decay both by collision and radiation, whereas allowed transitions still take place mostly by radiative decay. This makes the ratio of the allowed versus forbidden transitions dependent on the electron density.

The following sections describe the experimental method, the theoretical calculations that aided in line identifications, the list of the observed transitions and their uncertainties and a discussion of the diagnostic capabilities of some of the M1 transitions.



## 2. Experiment

The NIST EBIT and a multi-cathode metal vapor vacuum arc ion source (MEVVA) were used to produce highly charged yttrium ions, and the ion spectra were recorded with a custom-made EUV flat field grazing incidence spectrometer [60]. Both the MEVVA and the NIST EBIT are discussed in detail elsewhere [51,61], but we will now briefly review the most important details.

The MEVVA, which produces singly-charged ions by sparking a high voltage across metal cathodes, is located  $\approx 2$  m above the central trapping region of the EBIT. The ions are created at a potential of about 10 kV above ground and are accelerated towards the center of the EBIT through several electrodes at lower voltages. The trapping region, consisting of the drift tubes (upper, middle and lower), is floated on top of the voltage of the cylindrically-shaped shield electrode. To capture the ions in the trap, the shield electrode voltage is very briefly (on the order of  $10^{-3}$  s) switched to a potential of about 9.6 kV, and the middle drift tube voltage is simultaneously raised by an additional 0.4 kV. Then, precisely at the arrival of the ions, the middle drift tube is pulsed down to the shield voltage in order to trap and confine the plasma in the trap. During the entire timing sequence, the lower and upper drift tubes are kept at constant potentials with respect to the shield (0.5 kV and 0.26 kV, respectively) to create axial trapping. Radial confinement is accomplished by a combination of the axial 2.7 T magnetic field and the space charge of the intense electron beam, which is directed through the drift tubes to further ionize the ions. The electron beam energy can then be set as required for the experiment by adjusting the shield electrode voltage. The beam energy in the EBIT is determined by the voltage difference between the electron gun and the middle drift tube, taking into account the space charge of the electron beam in the interaction region [62]. The latter depends on the density of the electron beam and therefore scales with the beam energy and current in addition to the ion cloud neutralization factor, which is generally difficult to quantify. In our experiment, the modeling of the observed spectral line intensities showed that the space charge correction was approximately 150 eV. Electron beam currents were varied between 66 mA and 147 mA during the measurement. To control the charge-state distribution of the yttrium ions, the energy of the electron beam was systematically varied from 2.3 keV–6.0 keV.

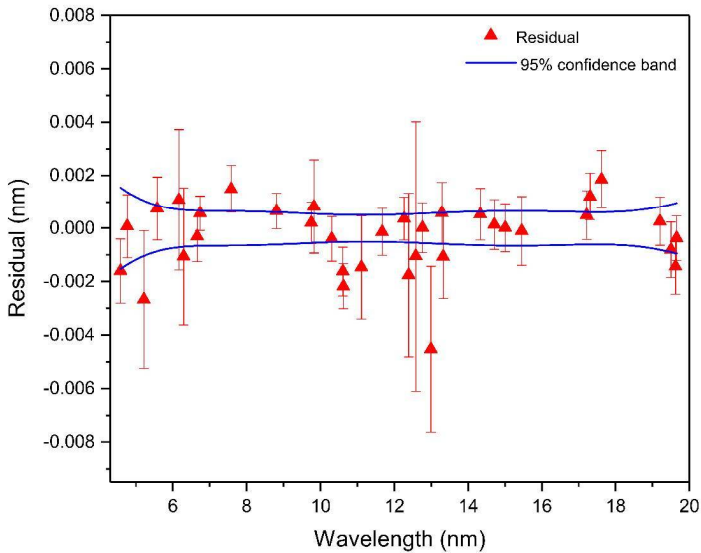
The flat field EUV grazing incidence spectrometer [60] is equipped with a liquid-nitrogen-cooled charged-coupled device (CCD) detector with  $2048 \times 512$  active pixels of  $13.5 \mu\text{m} \times 13.5 \mu\text{m}$  size each. The spectrometer consists of a gold-coated spherical focusing mirror that focuses light radiated from the EBIT plasma onto a slit, followed by a gold-coated concave reflection grating with a groove spacing of approximately  $1200 \text{ lines mm}^{-1}$ . The instrument has a resolving power of  $\lambda/d\lambda \approx 400$ . The 2D images recorded by the CCD were hardware collapsed along the vertical axis, so that the resulting image was a 1D ( $2048 \times 1$ ) spectrum. Ten 60 s frames of yttrium spectra were collected in a set, giving a total acquisition time of 600 s for each energy. The spectra were filtered of cosmic rays using a program that identifies outlier intensities among different frames within the same set. If the intensity of a channel in a certain frame is five or more Poisson standard deviations away from the mean of all of the frames, it is replaced by the average value of the other frames before the frames are summed together to form the overall spectrum.

## 3. Wavelength Calibration

Spectra emitted by yttrium ions were acquired in the approximate wavelength region of 4 nm to 20 nm. Wavelength calibration was performed using highly charged neon lines (Ne V–VIII), xenon lines (Xe XLI–XLII), barium lines (Ba XLIII–XLIV), oxygen lines (O V–VI) and iron lines (Fe XXIII–XXIV) [5,7,11,63,64], as described in this section. Neon and carbon dioxide gases were injected into the EBIT as neutral atoms from the gas injection setup described by Fahy et al. [2], with the injection pressure normally on the order of  $10^{-3}$  Pa. Iron ions were loaded from the MEVVA ion source. Small amounts of barium and xenon ions are always present in the trap as heavy ion contaminants from the electron gun and the ion pumps. In order to prevent long-term accumulation of these ions, the EBIT trap was emptied and reloaded every 10 s.

The calibration lines were fitted using unweighted Gaussian profiles, and the locations of the peaks were noted in terms of the channel (pixel) numbers corresponding to the respective lines. The literature-recommended wavelengths [5,11,64] were plotted as a function of channel number weighted with the uncertainty in these wavelengths. A third order polynomial from the fit was used to convert the uncertainties in channel number to the uncertainties in wavelength. The statistical uncertainties of the calibration lines were then determined from the quadrature sum of these uncertainties with the adopted wavelength uncertainties from the literature.

The final calibration function was a third order polynomial that describes the wavelength versus channel as a fit weighted by the inverse square of the total uncertainties of the lines. The latter was calculated as the quadrature sum of the overall statistical uncertainty and the systematic uncertainty. The systematic uncertainty was estimated to be 0.0006 nm by requiring the reduced chi-square of the fit to be 1 according to the standard statistical procedure [65]. Systematic uncertainty may arise from several factors during the experiment such as small device vibrations or uneven pixel response. The residual of the literature values of the calibration lines with respect to their calibrated wavelength provided an assessment of the quality of the calibration. Including their uncertainties, 95% of the residual should lie within two standard deviation ( $\sigma$ ) of their mean ( $\mu$ ):  $P(\mu - 2\sigma \leq x \leq \mu + 2\sigma) \approx 0.9545$ . Figure 1 shows the calibration data points and 95% confidence band of the fit.



**Figure 1.** Residual of the adopted wavelength of the calibration lines with respect to their calibrated wavelength. The individual uncertainties of the data points are as described in the text. The solid (blue) line corresponds to the 95% confidence band of the calibration fit.

In calculating the overall calibration uncertainty contributing to the total uncertainty at a given wavelength for the identified yttrium lines, we have used the 95% confidence band at the position of the line. The calibration uncertainties reported are equal to the vertical width of the confidence band divided by four (equivalent to one standard deviation). The calibration uncertainty calculated from the 68.3% confidence band corresponding to one standard deviation gives comparable results, as expected.

#### 4. Theoretical Modeling

The spectral modeling for the non-Maxwellian EBIT plasma was performed with the collisional-radiative code NOMAD [66] that has been extensively used in EBIT spectroscopy. The yttrium plasma was assumed

to be in the steady state, optically thin and uniform with electron density of  $10^{11} \text{ cm}^{-3}$ . The electron beam energy distribution was modeled by a Gaussian function with the full width at half maximum of 40 eV.

A detailed collisional-radiative (CR) model would generally require a large amount of atomic data, such as energy levels, wavelengths, transition probabilities and cross-sections. For the present analysis, we make use of the Flexible Atomic Code (FAC) [67], which is based on a fully-relativistic model potential and can consistently generate all required data. In total, our CR model included 13 ionization stages from Si-like to He-like ions of yttrium, about 5000 atomic levels and nearly 1.5 million transitions describing spontaneous radiative decays, electron-impact ionization and excitation, as well as radiative recombination. NOMAD also takes into account the charge exchange of ions with neutral atoms present in the trap, which shifts the ionization balance to lower charge states. Within the model, the density of neutral atoms is a free parameter and adjusted such that the theoretical and experimental spectra closely agree. The neutral densities obtained from the spectra of the current experiment are consistent with previous values under similar EBIT conditions.

Another adjustable parameter (although less important due to the lower sensitivity of the results to its variations) is the space charge correction to the electron beam energy as described in the experimental section. A generally good match between the observed and calculated line intensity ratios was obtained with a 150 eV correction to the values calculated from the applied voltages.

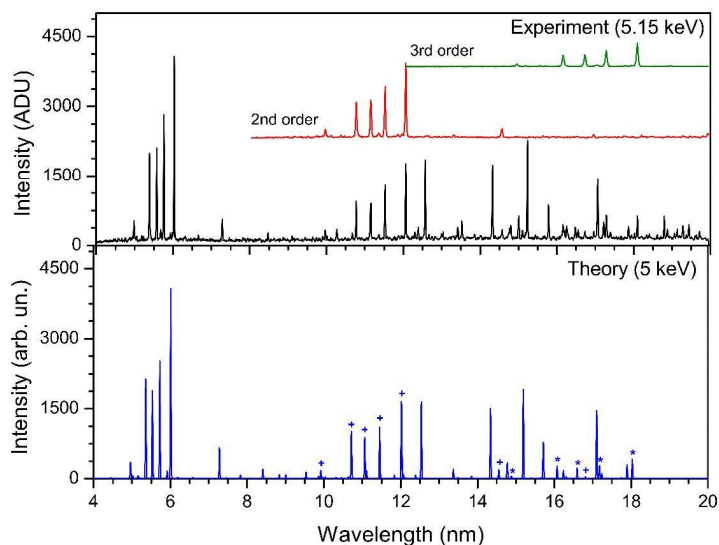
The CR model used these data to build and solve a system of rate equations to determine level populations and line intensities for EBIT plasmas of given electron energies. With this approach, NOMAD was used to simulate the yttrium emission as the electron beam energy was systematically changed during the experiment. The calculated spectra were convoluted with the spectrometer energy resolution and corrected for the efficiency of the grazing incidence instrument to obtain the theoretical result.

## 5. Line Identification

Yttrium spectra were taken as a function of the calibrated wavelength and fitted with unweighted Gaussians to determine the line positions. The uncertainty associated with the identified lines was then calculated from the quadrature sum of the uncertainty of the line fit that corresponds to the statistical uncertainty, the calibration uncertainty, the systematic uncertainty (estimated using the calibration data as discussed above) and uncertainty assigned for a possible small systematic line asymmetry (discussed below), which might be due to line blends or instrument asymmetries. In order to reach the desired ionization stages, the beam energy was systematically varied from 2.3 keV–6.0 keV. By matching theoretical and experimental spectra, we were able to conveniently identify most of the yttrium lines, as shown in Figure 2.

Some of the yttrium lines were also observed in the second and third orders of diffraction, in addition to the first order. Second order and third order yttrium spectra were plotted simultaneously as a visual aid to better identify the observed lines. They were obtained by dividing the line intensities of the first order experimental spectra by 2.5 and eight and multiplying the wavelength by two and three, respectively. Since we observed the same yttrium lines at several different beam energies, our reported wavelengths are the weighted averages of the positions of these lines using the formula for the best combined estimate of  $N$  measurements of the same quantity,  $x_{CE} = \frac{\sum w_i \times x_i}{\sum w_i}$ ,  $x_i$  being the line position at different energies. The weight  $w_i$  is given by  $w_i = \frac{1}{s_i^2}$ , where  $s_i$  is the total uncertainty corresponding to each measurement. A few lines were blended with unresolved features, making it difficult to precisely determine their positions. In such cases, the spectra at energies that gave the cleanest and strongest signals were solely used. As a test for unanticipated systematics, the difference in the individual wavelengths at different energies with their weighted average was calculated. This difference was binned to get a histogram that represents a normal distribution about their mean, which should be zero. The distribution was fitted with a Gaussian function, and the mean value of 0.0003 nm was assigned to be the uncertainty due to unknown line asymmetries. As mentioned earlier, this uncertainty was added in quadrature to the rest of the uncertainties to get the total line uncertainty.

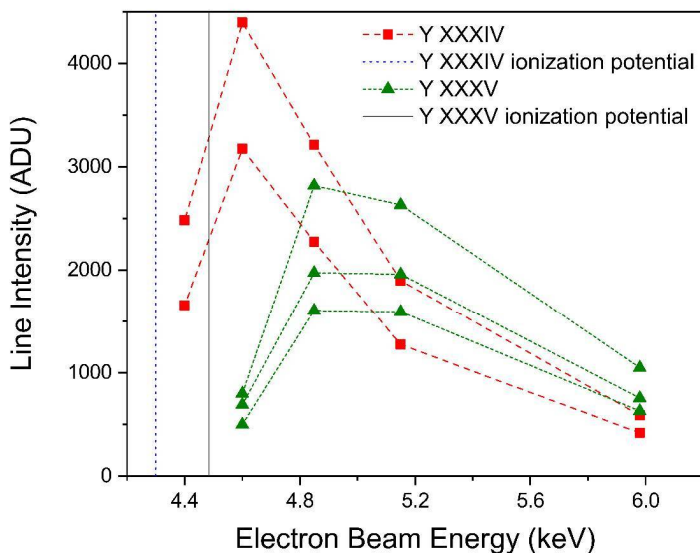
For the lines that we observed in second and third order, the wavelengths and the corresponding uncertainties were divided by two and three, respectively, and the weighted average was calculated accordingly. The total uncertainty for each of the identified lines was computed using the error propagation method  $s = \sqrt{\frac{1}{\sum \frac{1}{s_i^2}}}$ .



**Figure 2.** Comparison of the experimental spectrum (**top**) of yttrium with the theoretical spectrum (**bottom**). The intensity is given in analog to digital units (ADU) for the measured spectra. The second and third order spectra for the experimental data are also shown (red and green insets, respectively). The theoretical spectrum includes the second (+) and third (\*) order spectra and is calculated at an energy of 5 keV for the electron beam energy of 5.15 keV, to account for the space-charge correction in the experiment.

The most prominent observed lines were unambiguously identified through comparison with theory. For instance, the Be-like lines  $2s^2 \ ^1S_0-2s2p \ ^1P_1$  and  $2s^2 \ ^1S_0-2s2p \ ^3P_1$  were identified at 6.0322(5) nm and 15.2336(7) nm experimentally compared to the calculated values of 6.0098 nm and 15.1907 nm. The measured wavelengths of the Li-like, B-like, C-like and N-like yttrium lines are within 1.3% of our theoretical values, sufficient for line identification purposes. We note that for electron beam energies below 3.75 keV, where M-shell yttrium ion charge states become prominent, a more accurate relativistic many-body perturbation theory (RMBPT) calculation had to be invoked to match theoretical and experimental data. These calculations were performed by Safronova et al. [68] for the lines of the Ne-like, Na-like, Mg-like and Al-like charge states of yttrium lines.

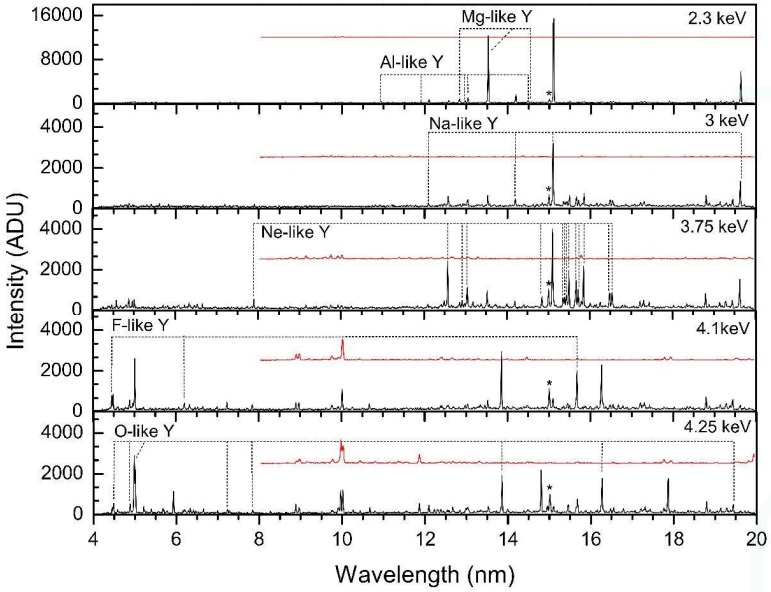
In order to help with the identification of lines that were close in wavelength, we considered the evolution of charge states with electron beam energy by plotting the line intensities as a function of the beam energy. The ionization energies of the different charge states determine the minimum beam energy required for the emergence of a particular charge state. For instance, the ionization energy of Y XXXIV is 4.299 keV [64]; hence, a beam energy of 4.299 keV or higher is required to observe spectral lines from Be-like Y XXXV. This gives an idea of the range of charge states one is supposed to observe at a particular beam energy. In addition, lines emitted from the same ionization state usually depend in a similar way on the beam energy. These qualitative dependencies aided the line identification as illustrated in Figure 3. In order to verify these qualitative assumptions, we have used our detailed CR model calculations to make a final assignment based on the line intensity dependences.



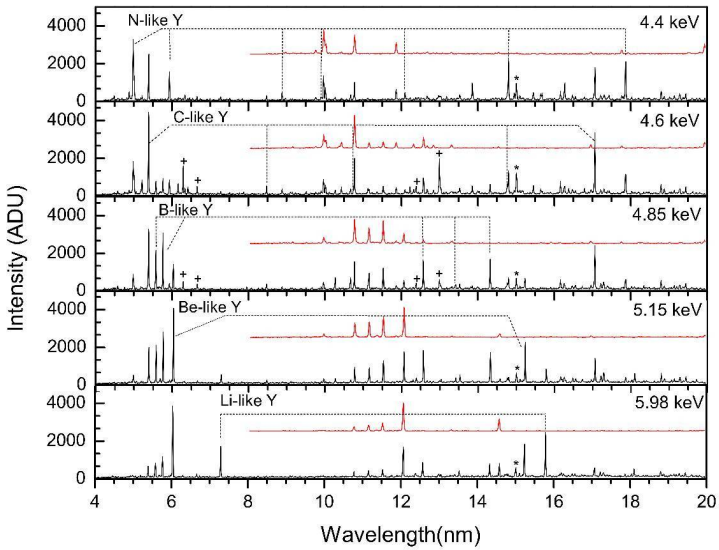
**Figure 3.** Line intensity plotted as a function of electron beam energy for three Y XXXV lines (green triangles) and two Y XXXIV lines (red squares). The solid (black) and dotted (blue) vertical lines depict the ionization potential of Y XXXV and Y XXXIV, respectively.

## 6. Results and Discussions

Table 1 presents the yttrium lines identified in our experiment for the charge state range between Y XXVII and Y XXXVII. We focused on lines that originate from  $\Delta n = 0$  transitions within the  $n = 2$  and  $n = 3$  principal quantum number states. Most of the lines are electric dipole (E1) transitions, while a few lines are magnetic dipole (M1) transitions. All M1 lines correspond to transitions within the  $2s^2 2p^m$  ground state configurations of different charge states ( $m = 1, 2, 3, 4, 5$ ), with the exception of the line at 16.4817(7) nm, which originates from within the excited configuration  $2p^5 3s$  of Ne-like yttrium ion. The energy levels within the ground configuration are close and result in longer wavelength forbidden lines, while the energy levels contributing to the allowed (E1) transitions are further separated and give rise to shorter wavelength lines. Level notations are taken from FAC and are given in  $jj$ -coupling. The plus sign stands for the  $j$  value of  $l + 1/2$ , and the minus sign represents the  $j$  value of  $l - 1/2$ , where  $l$  is the orbital angular momentum. As an example, the line at 5.9329(4) nm connects the  $2s^2 2p^3$  upper level with a total angular momentum of  $J = 5/2$  to the  $2s 2p^4$  of  $J = 3/2$ . It should be noted that in FAC, the subshells that couple to zero angular momentum are omitted in the notation. As an illustration of this, the  $2p^5$  configuration is noted as  $2p_+^3$  when both electrons on the  $2p_-$  subshell are present and couple to zero joint angular momentum. Yttrium spectra recorded at different energies are shown in Figures 4 and 5, with the identified lines labeled by their isoelectronic sequence.



**Figure 4.** Yttrium spectra at beam energies from 2.30 keV–4.25 keV. The black and red (shifted) spectra correspond to the first and second order Y spectra, respectively. The \* marks the impurity coming from oxygen at 15.0099(5) nm.



**Figure 5.** Yttrium spectra at beam energies from 4.40 keV–5.98 keV. The black and red (shifted) spectra correspond to the first and second order Y spectra, respectively. The + marks the Na-like and Mg-like xenon impurities at beam energies of 4.6 keV and 4.85 keV and the \* marks the impurity coming from oxygen at 15.0099(5) nm.

**Table 1.** The table below presents the list of the yttrium lines identified  $Y^{26+} \rightarrow Y^{36+}$ . Previous measurements and calculations are reported as well. Isoelectronic sequence is abbreviated as  $Seq_i$ , configuration is abbreviated as  $Config_i$ , and the level number is abbreviated as  $No_i$ .

Ion Charge	Seq.	Type	Lower Level			Upper Level			Experimental Wavelength (nm)			Theoretical Wavelength (nm)																															
			No.	Config.	Term <sub>j</sub>	No.	Config.	Term <sub>j</sub>	This Work	Previous Work	This Work	Previous Work	This Work	Previous Work																													
36	Li	E1	1	2s	2s <sub>+</sub>	2	2p	2p <sub>+</sub>	7.2874(6)	7.2771	7.2893 [69]	7.2887(1) [70]	7.2892 [71]	7.2890(1) [72]	7.2888 [73]																												
																36	Li	E1	1	2s	2s <sub>+</sub>	3	2p	2p <sub>-</sub>	15.7862(9)	15.7139	15.7868(5) [70]	15.7865 [71]	15.7874(4) [72]	15.7867 [73]													
																															35	Be	E1	1	2s <sup>2</sup>	(2s <sub>+</sub> <sup>2</sup> ) <sub>0</sub>	6	2s2p	(2s <sub>+</sub> , 2p <sub>-</sub> ) <sub>1</sub>	6.0322(5)	6.0098	6.0337(20) f [24]	6.0283 [74]
34	B	E1	1	2p	2p <sub>-</sub>	7	2s2p <sup>2</sup>	((2s <sub>+</sub> , 2p <sub>-</sub> ) <sub>1</sub> , 2p <sub>+</sub> ) <sub>1/2</sub>	5.5768(6)	5.5310	5.5771 f [25]																																
												34	B	E1	1	2p	2p <sub>-</sub>	6	2s2p <sup>2</sup>	((2s <sub>+</sub> , 2p <sub>-</sub> ) <sub>1</sub> , 2p <sub>+</sub> ) <sub>3/2</sub>	5.7623(6)	5.7254	5.7629 f [25]																				
34	B	E1	1	2p	2p <sub>-</sub>	3	2s2p <sup>2</sup>	2s <sub>+</sub>	12.5372	12.5372																																	
											34	B	E1	2	2p	2p <sub>+</sub>	5	2s2p <sup>2</sup>	((2s <sub>+</sub> , 2p <sub>-</sub> ) <sub>1</sub> , 2p <sub>+</sub> ) <sub>5/2</sub>	13.4185(8)	13.3700																						
34	B	M1	1	2p	2p <sub>-</sub>	2	2p	2p <sub>+</sub>	14.3334(5)	14.3363	14.321 [75]	14.322 f [25]																															
													33	C	E1	1	2p <sup>2</sup>	(2p <sub>-</sub> <sup>2</sup> ) <sub>0</sub>	7	2s2p <sup>3</sup>	(2s <sub>+</sub> , 2p <sub>+</sub> ) <sub>1</sub>	5.3878(5)	5.3571																				
33	C	E1	3	2p <sup>2</sup>	(2p <sub>-</sub> , 2p <sub>+</sub> ) <sub>2</sub>	7	2s2p <sup>3</sup>	(2s <sub>+</sub> , 2p <sub>+</sub> ) <sub>1</sub>	8.4792(19) <sup>b</sup>	8.4071																																	
											33	C	E1	2	2p <sup>2</sup>	(2p <sub>-</sub> , 2p <sub>+</sub> ) <sub>1</sub>	5	2s2p <sup>3</sup>	(2s <sub>+</sub> , 2p <sub>+</sub> ) <sub>2</sub>	11.1236(9) <sup>b</sup>	11.1132																						
33	C	M1	1	2p <sup>2</sup>	(2p <sub>-</sub> <sup>2</sup> ) <sub>0</sub>	3	2p <sup>2</sup>	(2p <sub>-</sub> , 2p <sub>+</sub> ) <sub>2</sub>	14.7700(10)	14.7668																																	
											33	C	M1	1	2p <sup>2</sup>	(2p <sub>-</sub> <sup>2</sup> ) <sub>0</sub>	2	2p <sup>2</sup>	(2p <sub>-</sub> , 2p <sub>+</sub> ) <sub>1</sub>	17.0632(7)	17.0625 [76]																						
32	N	E1	1	2p <sup>3</sup>	2p <sub>+</sub>	8	2s2p <sup>4</sup>	(2s <sub>+</sub> , (2p <sub>+</sub> <sup>2</sup> ) <sub>2</sub> ) <sub>3/2</sub>	4.9858(6)	4.9593	17.0558 [76]																																

Table 1. Cont.

Ion Charge	Seq.	Type	Lower Level			Upper Level			Experimental Wavelength (nm)			Theoretical Wavelength (nm)		
			No.	Config.	Term <sub>j</sub>	No.	Config.	Term <sub>j</sub>	This Work	Previous Work	This Work	Previous Work	This Work	Previous Work
32	N	E1	1	2p <sup>3</sup>	2p <sub>+</sub>	6	2s2p <sup>4</sup>	(2s <sub>+</sub> , (2p <sub>+</sub> <sup>2</sup> ) <sub>2</sub> ) <sub>5/2</sub>	5.929(4)		5.9151			
32	N	E1	2	2p <sup>3</sup>	(2p <sub>-</sub> , (2p <sub>+</sub> <sup>2</sup> ) <sub>2</sub> ) <sub>3/2</sub>	6	2s2p <sup>4</sup>	(2s <sub>+</sub> , (2p <sub>+</sub> <sup>2</sup> ) <sub>2</sub> ) <sub>5/2</sub>	8.8622(7)		8.8358			
32	N	E1	3	2p <sup>3</sup>	(2p <sub>-</sub> , (2p <sub>+</sub> <sup>2</sup> ) <sub>2</sub> ) <sub>5/2</sub>	6	2s2p <sup>4</sup>	(2s <sub>+</sub> , (2p <sub>+</sub> <sup>2</sup> ) <sub>2</sub> ) <sub>5/2</sub>	9.9054(10)		9.8612			
32	N	M1	1	2p <sup>3</sup>	2p <sub>+</sub>	4	2p <sup>3</sup>	(2p <sub>-</sub> , (2p <sub>+</sub> <sup>2</sup> ) <sub>0</sub> ) <sub>1/2</sub>	12.0926(6)		12.0717			
32	N	M1	1	2p <sup>3</sup>	2p <sub>+</sub>	3	2p <sup>3</sup>	(2p <sub>-</sub> , (2p <sub>+</sub> <sup>2</sup> ) <sub>2</sub> ) <sub>5/2</sub>	14.8036(5)		14.7819			
32	N	M1	1	2p <sup>3</sup>	2p <sub>+</sub>	2	2p <sup>3</sup>	(2p <sub>-</sub> , (2p <sub>+</sub> <sup>2</sup> ) <sub>2</sub> ) <sub>3/2</sub>	17.8665(6)		17.8947			
31	O	E1	1	2p <sup>4</sup>	(2p <sub>+</sub> <sup>2</sup> ) <sub>2</sub>	7	2s2p <sup>5</sup>	(2s <sub>+</sub> , (2p <sub>+</sub> <sup>2</sup> ) <sub>3/2</sub> ) <sub>1</sub>	4.4854(8)	4.4857(15) [77]	4.4567			
31	O	E1	2	2p <sup>4</sup>	(2p <sub>+</sub> <sup>2</sup> ) <sub>0</sub>	7	2s2p <sup>5</sup>	(2s <sub>+</sub> , (2p <sub>+</sub> <sup>2</sup> ) <sub>3/2</sub> ) <sub>1</sub>	4.8871(12)	4.8882(15) [77]	4.8569			
31	O	E1	1	2p <sup>4</sup>	(2p <sub>+</sub> <sup>2</sup> ) <sub>2</sub>	6	2s2p <sup>5</sup>	(2s <sub>+</sub> , (2p <sub>+</sub> <sup>2</sup> ) <sub>3/2</sub> ) <sub>2</sub>	5.0103(5)	5.0085(15) [77]	4.9828			
31	O	E1	3	2p <sup>4</sup>	(2p <sub>-</sub> , (2p <sub>+</sub> <sup>2</sup> ) <sub>3/2</sub> ) <sub>1</sub>	6	2s2p <sup>5</sup>	(2s <sub>+</sub> , (2p <sub>+</sub> <sup>2</sup> ) <sub>3/2</sub> ) <sub>2</sub>	7.2352(8)	7.2356(15) [77]	7.1754			
31	O	E1	4	2p <sup>4</sup>	(2p <sub>-</sub> , (2p <sub>+</sub> <sup>2</sup> ) <sub>3/2</sub> ) <sub>2</sub>	6	2s2p <sup>5</sup>	(2s <sub>+</sub> , (2p <sub>+</sub> <sup>2</sup> ) <sub>3/2</sub> ) <sub>2</sub>	7.8430(8)		7.7848			
31	O	M1	1	2p <sup>4</sup>	(2p <sub>+</sub> <sup>2</sup> ) <sub>2</sub>	4	2p <sup>4</sup>	(2p <sub>-</sub> , (2p <sub>+</sub> <sup>2</sup> ) <sub>3/2</sub> ) <sub>2</sub>	13.8581(6)		13.8442	13.89(2) [77]		
31	O	M1	1	2p <sup>4</sup>	(2p <sub>+</sub> <sup>2</sup> ) <sub>2</sub>	3	2p <sup>4</sup>	(2p <sub>-</sub> , (2p <sub>+</sub> <sup>2</sup> ) <sub>3/2</sub> ) <sub>1</sub>	16.2725(9)		16.307	16.28(2) [77]		
31	O	E1	16	2p <sup>3</sup> 3p	(2p <sub>+</sub> , 3p <sub>+</sub> ) <sub>3</sub>	32	2p <sup>3</sup> 3d	(2p <sub>+</sub> , 3d <sub>+</sub> ) <sub>4</sub>	19.4383(8)		19.4639			
30	F	E1	1	2p <sup>5</sup>	(2p <sub>+</sub> <sup>3</sup> ) <sub>3/2</sub>	3	2s	2s <sub>+</sub>	4.4500(7)	4.4496(15) [37]	4.417	4.4083 [26] 4.4486 <sup>f</sup> [26] 4.4492 [39]		
30	F	E1	2	2p <sup>5</sup>	2p <sub>-</sub>	3	2s	2s <sub>+</sub>	6.2115(14) <sup>b</sup>	6.2107(15) [37]	6.1454	6.1299 [26] 6.2109 <sup>f</sup> [26]		
30	F	M1	1	2p <sup>5</sup>	(2p <sub>+</sub> <sup>3</sup> ) <sub>3/2</sub>	2	2p <sup>5</sup>	2p <sub>-</sub>	15.6801(11)		15.7043	15.681(12) <sup>f</sup> [37] 15.654(5) <sup>f</sup> [78] 15.678 <sup>f</sup> [26] 15.678(12) [79] 15.71 [38] 15.6826 [39] 15.685 <sup>f</sup> [80]		



Table 1. Cont.

Ion Charge	Seq.	Type	Lower Level			Upper Level			Experimental Wavelength (nm)			Theoretical Wavelength (nm)		
			No.	Config.	Term <sub>j</sub>	No.	Config.	Term <sub>j</sub>	This Work	Previous Work	This Work	Previous Work	This Work	Previous Work
29	Ne	E1	3	2p <sup>5</sup> 3s	((2p <sup>3</sup> <sub>+</sub> ) <sub>3/2</sub> , 3s <sub>+</sub> ) <sub>1</sub>	20	2p <sup>5</sup> 3p	(2p <sub>-</sub> , 3p <sub>-</sub> ) <sub>0</sub>	7.8983(8)		7.9003 <sup>a</sup>	7.914 <sup>f</sup> [81]		
29	Ne	E1	3	2p <sup>5</sup> 3s	((2p <sup>3</sup> <sub>+</sub> ) <sub>3/2</sub> , 3s <sub>+</sub> ) <sub>1</sub>	11	2p <sup>5</sup> 3p	((2p <sup>3</sup> <sub>+</sub> ) <sub>3/2</sub> , 3p <sub>+</sub> ) <sub>0</sub>	12.5743(7)		12.5696 <sup>a</sup>	12.576 <sup>f</sup> [81]		
29	Ne	E1	12	2p <sup>5</sup> 3p	(2p <sub>-</sub> , 3p <sub>-</sub> ) <sub>1</sub>	24	2p <sup>5</sup> 3d	(2p <sub>-</sub> , 3d <sub>-</sub> ) <sub>2</sub>	12.9238(8)		12.9267 <sup>a</sup>			
29	Ne	E1	5	2p <sup>5</sup> 3p	((2p <sup>3</sup> <sub>+</sub> ) <sub>3/2</sub> , 3p <sub>-</sub> ) <sub>2</sub>	15	2p <sup>5</sup> 3d	((2p <sup>3</sup> <sub>+</sub> ) <sub>3/2</sub> , 3d <sub>-</sub> ) <sub>3</sub>	13.0471(8)		13.0550 <sup>a</sup>			
29	Ne	E1	2	2p <sup>5</sup> 3s	((2p <sup>3</sup> <sub>+</sub> ) <sub>3/2</sub> , 3s <sub>+</sub> ) <sub>2</sub>	10	2p <sup>5</sup> 3p	((2p <sup>3</sup> <sub>+</sub> ) <sub>3/2</sub> , 3p <sub>+</sub> ) <sub>2</sub>	14.8480(7)		14.8389 <sup>a</sup>			
29	Ne	E1	10	2p <sup>5</sup> 3p	((2p <sup>3</sup> <sub>+</sub> ) <sub>3/2</sub> , 3p <sub>+</sub> ) <sub>2</sub>	22	2p <sup>5</sup> 3d	((2p <sup>3</sup> <sub>+</sub> ) <sub>3/2</sub> , 3d <sub>+</sub> ) <sub>3</sub>	15.3559(10)		15.3587 <sup>a</sup>			
29	Ne	E1	19	2p <sup>5</sup> 3p	(2p <sub>-</sub> , 3p <sub>+</sub> ) <sub>2</sub>	26	2p <sup>5</sup> 3d	(2p <sub>-</sub> , 3d <sub>+</sub> ) <sub>3</sub>	15.3945(10)		15.3972 <sup>a</sup>			
29	Ne	E1	18	2p <sup>5</sup> 3p	(2p <sub>-</sub> , 3p <sub>+</sub> ) <sub>1</sub>	25	2p <sup>5</sup> 3d	(2p <sub>-</sub> , 3d <sub>+</sub> ) <sub>2</sub>	15.4387(10)		15.4444 <sup>a</sup>			
29	Ne	E1	3	2p <sup>5</sup> 3s	((2p <sup>3</sup> <sub>+</sub> ) <sub>3/2</sub> , 3s <sub>+</sub> ) <sub>1</sub>	10	2p <sup>5</sup> 3p	((2p <sup>3</sup> <sub>+</sub> ) <sub>3/2</sub> , 3p <sub>+</sub> ) <sub>2</sub>	15.4902(18) <sup>b</sup>	15.497(15) [82] 15.50 [83]	15.4882 <sup>a</sup>	15.503 <sup>f</sup> [81] 15.50 [84]		
29	Ne	E1	9	2p <sup>5</sup> 3s	(2p <sub>-</sub> , 3s <sub>+</sub> ) <sub>1</sub>	20	2p <sup>5</sup> 3p	(2p <sub>-</sub> , 3p <sub>-</sub> ) <sub>0</sub>	15.5024(8) <sup>b</sup>		15.4904 <sup>a</sup>	15.498 <sup>f</sup> [81]		
29	Ne	E1	6	2p <sup>5</sup> 3p	((2p <sup>3</sup> <sub>+</sub> ) <sub>3/2</sub> , 3p <sub>+</sub> ) <sub>3</sub>	17	2p <sup>5</sup> 3d	((2p <sup>3</sup> <sub>+</sub> ) <sub>3/2</sub> , 3d <sub>+</sub> ) <sub>4</sub>	15.6711(10)		15.6769 <sup>a</sup>			
29	Ne	E1	9	2p <sup>5</sup> 3s	(2p <sub>-</sub> , 3s <sub>+</sub> ) <sub>1</sub>	19	2p <sup>5</sup> 3p	(2p <sub>-</sub> , 3p <sub>+</sub> ) <sub>2</sub>	15.7208(7)	15.714(15) [82] 15.71 [83]	15.7085 <sup>a</sup>	15.723 <sup>f</sup> [81] 15.71 [84]		
29	Ne	E1	2	2p <sup>5</sup> 3s	((2p <sup>3</sup> <sub>+</sub> ) <sub>3/2</sub> , 3s <sub>+</sub> ) <sub>2</sub>	6	2p <sup>5</sup> 3p	((2p <sup>3</sup> <sub>+</sub> ) <sub>3/2</sub> , 3p <sub>+</sub> ) <sub>3</sub>	15.8537(7)		15.8455 <sup>a</sup>			
29	Ne	M1	3	2p <sup>5</sup> 3s	((2p <sup>3</sup> <sub>+</sub> ) <sub>3/2</sub> , 3s <sub>+</sub> ) <sub>1</sub>	8	2p <sup>5</sup> 3s	(2p <sub>-</sub> , 3s <sub>+</sub> ) <sub>0</sub>	16.4817(7)		16.4843 <sup>a</sup>			
29	Ne	E1	3	2p <sup>5</sup> 3s	((2p <sup>3</sup> <sub>+</sub> ) <sub>3/2</sub> , 3s <sub>+</sub> ) <sub>1</sub>	7	2p <sup>5</sup> 3p	((2p <sup>3</sup> <sub>+</sub> ) <sub>3/2</sub> , 3p <sub>+</sub> ) <sub>1</sub>	16.5411(8)		16.5488 <sup>a</sup>	16.542 <sup>f</sup> [81] 16.463 [85] 16.484 [85]		
28	Na	E1	2	3p	3p <sub>-</sub>	4	3d	3d <sub>-</sub>	12.0979(8)		12.1353	12.09248 [86] 12.0993(7) <sup>f</sup> [45]		
28	Na	E1	3	3p	3p <sub>+</sub>	5	3d	3d <sub>+</sub>	14.1938(7)		14.2458	14.1873 [86] 14.1959(7) <sup>f</sup> [45]		

Table 1. *Cont.*

Ion Charge	Seq.	Type	Lower Level			Upper Level			Experimental Wavelength (nm)		Theoretical Wavelength (nm)		
			No.	Config.	Term/ Term <sub>j</sub>	No.	Config.	Term/ Term <sub>j</sub>	This Work	Previous Work	This Work	Previous Work	
28	Na	E1	1	3s <sup>2</sup>	3s <sub>+</sub>	3p <sub>+</sub>	3	3p	3p <sub>+</sub>	15.1037(5)	15.1035(10) [16]	15.0542	15.1038 [55]
													15.10402(40) [7]
													15.1033 / [29]
28	Na	E1	1	3s <sup>2</sup>	3s <sub>+</sub>	3p <sub>-</sub>	2	3p	3p <sub>-</sub>	19.6212(7)	19.6215(10) [16]	19.5175	15.1038(7) / [45]
													15.0658 [86]
													19.6199 [55]
27	Mg	E1	5	3s3p	(3s <sub>+</sub> ,3p <sub>+</sub> ) <sub>1</sub>	(3s <sub>+</sub> ,3d <sub>+</sub> ) <sub>2</sub>	14	3s3d	12.8333(9)	12.8352(10) [21]	12.7875	12.8349(5) [15]	
												12.8301(15) [44]	
												13.5279(10) [21]	
27	Mg	E1	1	3s <sup>2</sup>	(3s <sub>+</sub> ) <sub>0</sub>	(3s <sub>+</sub> ,3p <sub>+</sub> ) <sub>1</sub>	5	3s3p	13.5276(6)	13.5283(5) [15]	13.4437	13.5276 [87]	
												13.5216(15) [44]	
												13.5213 [88]	
27	Mg	E1	3	3s3p	(3s <sub>+</sub> ,3p <sub>-</sub> ) <sub>1</sub>	(3p <sub>-</sub> ,3p <sub>+</sub> ) <sub>2</sub>	7	3p <sup>2</sup>	14.5650(20) <sup>b</sup>	14.5603(10) [21]	14.528	19.6199 [55]	
												10.9391(20) [30]	
												10.9413(10) [43]	
26	Al	E1	1	3p	3p <sub>-</sub>	(3s <sub>+</sub> ,(3p <sub>+</sub> ) <sub>3/2</sub> )	10	3s3p <sup>2</sup>	10.9388(15) <sup>w,b</sup>	10.9388(15) [30]	10.8578	11.9131(20) [30]	
												11.9110(10) [43]	
												11.9072(12) <sup>w,b</sup>	
26	Al	E1	2	3p	3p <sub>+</sub>	3d <sub>-</sub>	11	3s3d	11.9072(12) <sup>w,b</sup>	11.9110(10) [43]	11.8248	12.9729(20) [30]	
												12.9745(10) [43]	
												12.9717(11) <sup>w</sup>	
26	Al	E1	2	3p	3p <sub>+</sub>	(3s <sub>+</sub> ,(3p <sub>+</sub> ) <sub>2,3</sub> )	10	3s3p <sup>2</sup>	12.9717(11) <sup>w</sup>	13.0416(20) [30]	12.852	13.0417(10) [43]	
												13.0416(20) [30]	
												13.0417(10) [43]	
26	Al	E1	1	3p	3p <sub>-</sub>	((3s <sub>+</sub> ,3p <sub>-</sub> ) <sub>1</sub> ),3p <sub>+</sub> <sub>1/2</sub>	8	3s3p <sup>2</sup>	13.0401(8)	13.0416(20) [30]	12.9265	14.4914(20) [30]	
												14.4910(10) [43]	
												14.4883(8) <sup>w</sup>	
26	Al	E1	1	3p	3p <sub>-</sub>	((3s <sub>+</sub> ,3p <sub>-</sub> ) <sub>1</sub> ),3p <sub>+</sub> <sub>3/2</sub>	6	3s3p <sup>2</sup>	14.4883(8) <sup>w</sup>	14.4910(10) [43]	14.4675		

<sup>a</sup> Wavelength from Saitonova et al.'s calculation [68]; <sup>b</sup> blended with other line feature; <sup>w</sup> weak lines; and <sup>f</sup> fitted values.

A total of 59 spectral lines were identified in this work from the Li-like to the Al-like isoelectronic sequences. Of these lines, 38 are new and 21 correspond to previously measured transitions in O-like, F-like, Na-like, Mg-like and Al-like charge states [15,16,21,24–26,29,30,37,43–45,77]. The previously measured transitions are also listed in Table 1 together with their currently measured wavelengths. We observed an O VI line at 15.0099(5) nm in all of the spectra due to impurities in the trap. At 4.60 keV and 4.85 keV drift tube voltages, we also observed impurity lines due to xenon, including a Xe XLII line at 15.0116(7) nm blended with the above-mentioned O VI line. Mg-like Xe XLIII lines were observed at 6.2903(6) nm and 12.9969(9) nm wavelengths, and two Na-like Xe XLIV lines were found at 6.6628(7) nm and 12.3939(7) nm. These lines are listed in the NIST Atomic Spectra Database [7,64] at 6.288(3) nm, 12.993(3) nm, 6.6628(5) nm and 12.394(1) nm, respectively.

Two Li-like yttrium lines were identified at 7.2874(6) nm/170.134(15) eV and 15.7862(9) nm/78.5395(44) eV, corresponding to the  $(2s_+) - (2p_+)$  and  $(2s_+) - (2p_-)$  electric dipole transitions, respectively. The Li-like isoelectronic sequence has been extensively studied both theoretically and experimentally due to its simple electronic structure. Highly accurate ab initio calculations agree with precise experimental results at the high-Z end of the isoelectronic sequence [1,89]. Although recent results are sensitive to higher order QED terms, further developments are expected, especially in the moderately high-Z region where experiments can provide accurate data due to the wavelength range available to grazing incidence EUV spectrometers. Our current relative uncertainty of  $57 \times 10^{-6}$  for the wavelength of the  $(2s_+) - (2p_-)$  transition shows good agreement with previous high precision calculations [70–72]; however, the  $(2s_+) - (2p_+)$  theoretical results [70,72] are slightly outside our relative uncertainty of  $82 \times 10^{-6}$  as shown in Figure 6. Upon close examination, a small feature of unidentified origin was found in the low wavelength wings of both Li-like lines. They were taken into account with the inclusion of a second small Gaussian peak in the fits. The reported results and uncertainties reflect the inclusion of these features, and we therefore believe that they are not responsible for the slight disagreement between the theoretical values and our results for the  $(2s_+) - (2p_+)$  line.

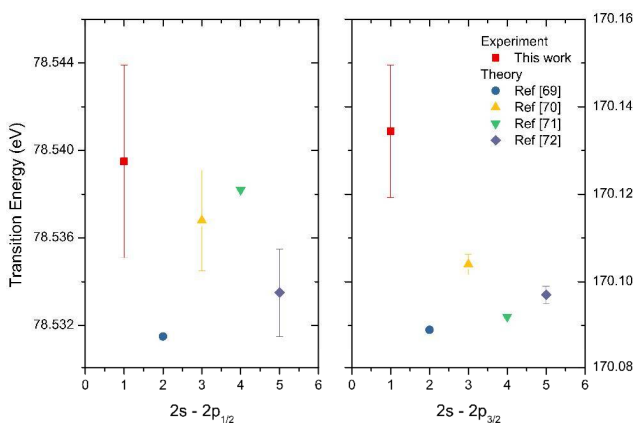


Figure 6. Comparison of measured and calculated Li-like yttrium lines.

The two electric dipole Be-like yttrium lines in the measured spectra at 6.0322(5) nm and 15.2336(7) nm correspond to the transitions of  $(2s_+^2)_0 - (2s_+, 2p_+)_1$  and  $(2s_+^2)_0 - (2s_+, 2p_-)_1$ , respectively. Be-like ions are quasi two-electron systems. Therefore, calculations at the level of the precision of the measurement are difficult. Denne et al. [24] predicted these wavelengths in yttrium by fitting the difference between the theoretical and experimental wave numbers and then extrapolating to attain the fine-structure separation. Their predictions of 6.0337(20) nm and 15.2345(20) nm had uncertainties

much larger than our measurements. Thus, we provide a considerable increase in the accuracy of the wavelengths.

A similar approach was used by Mrynas et al. [25] for the predictions of the wavelengths of B-like yttrium  $(2p_-)-(2s_+, 2p_-)_1, 2p_+)_1, 2p_-)-(2s_+, 2p_-)_1, 2p_+)_3/2$  and  $(2p_-)-(2p_+)$  lines. The obtained respective values were 5.5771 nm, 5.7629 nm and 14.322 nm, but no uncertainties were provided for the fitted wavelength predictions. These results are in a generally good agreement with our observed values of 5.5768(6) nm, 5.7623(6) nm and 14.3234(5) nm. Beyond these three transitions, two additional lines have been identified for B-like yttrium, as shown in Table 1. Out of the five reported transitions, four are E1, and one is an M1 transition.

With an increasing number of electrons, the electronic structure of open shell ions becomes more difficult for theory. However, the experimental wavelength determinations are as accurate as for their simpler structure counterparts. Accurate wavelength results in these ions can provide guidance for further theoretical work for the better understanding of the electron-electron interactions in these systems. Here, we report E1 and M1 transitions for both C-like and N-like yttrium ions.

Behring et al. [77] observed O-like yttrium transitions by irradiating a solid yttrium target with 24 frequency-tripled laser beams. We identified six E1 transitions and two M1 transitions in the same system and provide wavelength values for these in Table 1. The observations of Behring et al. are consistent with our measurements with the exception of the M1 transition  $(2p_+^2)_2-(2p_-, (2p_+^3)_{3/2})_2$ . Our measurement of 13.8581(6) nm for this M1 line is at a shorter wavelength than their predicted wavelength of 13.89(2) nm. The M1 transition at 16.2725(9) nm agrees with their predicted wavelength of 16.28(2) nm [77].

Wavelengths of F-like yttrium lines were measured by Reader et al. [37] using laser produced plasmas. The  $(2p_+^3)_{3/2}-(2s_+)$  and  $(2p_-)-(2s_+)$  transitions in these ions were measured to be 4.4496(15) nm and 6.2107(15) nm, respectively. Our results for the same transitions indicated 4.4500(7) nm and 6.2115(14) nm wavelengths and are in good agreement with the previously observed values. Calculations by Feldman et al. [26] reported values of 4.4083 nm and 6.1299 nm that are further away from these measurements than our FAC calculated wavelengths values of 4.417 nm and 6.1454 nm.

The M1 transition  $(2p_+^3)_{3/2}-(2p_-)$  in F-like Y is interesting due to its potential for plasma diagnostics [37,38]. Reader et al. [37] predicted the wavelength by comparing the observed fine-structure intervals with Dirac-Fock calculations and obtained 15.681(12) nm. This is in agreement with our measured value of 15.6801(11) nm.

The ground state of Ne-like ions is a closed shell. However, the low lying excited states have interesting features that have been exploited in many experiments and observations [90]. The level structure has been investigated for use in the diagnosis of astrophysical and laboratory plasmas [91,92] and has been used in soft X-ray laser schemes [93]. We report fourteen E1 and one M1 transitions in Ne-like Y. The Ne-like yttrium lines were identified using the theoretical values from highly accurate RMBPT calculations [68].

In our spectra, we were able to identify four E1 transitions of Na-like yttrium ions. The two most prominent ones are the well-known Na-like  $D_1 (3s_+)-(3p_+)$  and  $D_2 (3s_+)-(3p_-)$  lines. Our measured wavelength values of 15.1037(5) nm and 19.6212(7) nm, respectively, lie within the uncertainty of the 15.1035(10) nm and 19.6215(10) nm measurements by Reader et al. in tokamak plasmas and laser-produced plasmas [16]. Seely et al. [29] reported calculated values of 15.0961 nm and 15.0310 nm for the  $D_1$  line and 19.6047 nm and 19.4851 nm for the  $D_2$  line with and without QED corrections, respectively. This illustrates the importance of QED corrections at this level of experimental accuracy. Their fitted values of 15.1033 nm and 19.6219 nm for these transitions are within our experimental uncertainty. Our measured wavelengths also agree well with Blundell's calculated values of 15.10402(40) nm and 19.6209(7) nm for the  $D_1$  and  $D_2$  lines [7]. Gillaspay et al. [7] have pointed out that the accuracy of the measurements in medium-Z to high-Z systems is sensitive to the finite

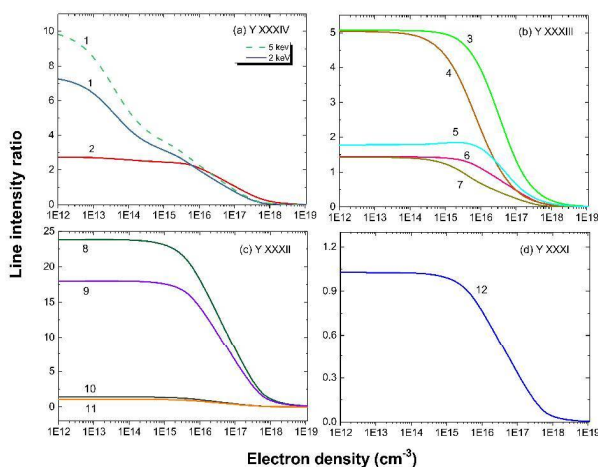
nuclear size correction in the otherwise calculable QED terms. This illustrates the importance of these transitions in studies at the interface of atomic and nuclear physics.

Our goal in these studies was the identification of lines in the L-shell ion states of yttrium in the EUV region. The few M-shell charge states we report here appeared at the low energy end of our systematic scans. The highest isoelectronic sequences investigated here were those for Mg and Al. In Mg-like yttrium, we report the observation of three E1 lines that have been previously measured by Ekberg et al. [21], Sugar et al. [15] and Reader et al. [44]. Similarly, the five Al-like yttrium E1 lines that we identified were previously measured by Ekberg et al. [43] and Sugar et al. [30]. The slight disagreement with some of the previous measurements might be due to weak lines and blends with other line features.

### 7. Diagnostically Important M1 Transitions

Among the 59 identified yttrium lines listed in Table 1, 10 lines are due to forbidden M1 transitions. States that decay via M1 transitions have a different dependence on collisional depopulation from states with E1 transitions. Thus, the corresponding intensity ratios of M1 to E1 lines are sensitive to the electron densities and temperatures, thereby making them potential candidates for plasma diagnostics. To analyze the feasibility of this, calculations with the CR modeling code NOMAD were performed for Maxwellian electron energy distribution plasmas with electron densities ranging from  $10^{12} \text{ cm}^{-3}$ – $10^{20} \text{ cm}^{-3}$  and temperatures from 1500 eV–6000 eV, which provide the largest abundance of the ions.

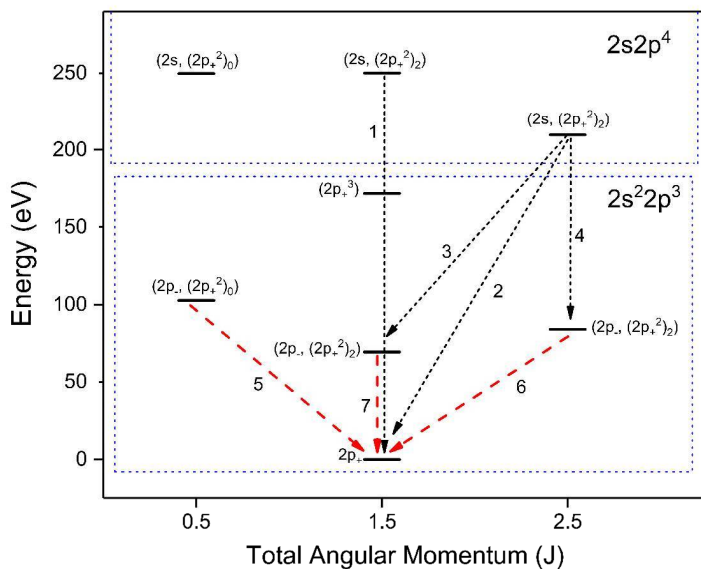
The most sensitive intensity ratios for the spectral lines of  $\text{Y}^{30+}$ – $\text{Y}^{33+}$  ions are presented in Figure 7. The figure provides examples for sensitivity to the electron density ( $n_e$ ) in the range of  $10^{12} \text{ cm}^{-3}$ – $10^{19} \text{ cm}^{-3}$ . At low densities, radiative rates for both forbidden and allowed transitions are much stronger than the collisional rates, and therefore, no dependence on electron density arises. However, at higher densities, collisional quenching dominates radiative decay for forbidden lines, and the line intensity ratios become sensitive to  $n_e$ .



**Figure 7.** Density-sensitive line ratios for (a) C-like Y XXXIV, (b) N-like Y XXXIII, (c) O-like Y XXXII and (d) F-like Y XXXI. The number labels correspond to the line ratios: (1) 17.0632(7) nm/11.1236(9) nm at 5-keV electron energy (dash) and 2-keV electron energy (solid), (2) 17.0632(7) nm/8.4792(19) nm, (3) 17.8665(6) nm/9.9054(10) nm, (4) 14.8036(5) nm/9.9054(10) nm, (5) 12.0926(6) nm/9.9054(10) nm, (6) 17.8665(6) nm/8.8822(7) nm, (7) 14.8036(5) nm/8.8822(7) nm, (8) 13.8581(6) nm/19.4383(8) nm, (9) 16.2725(9) nm/19.4383(8) nm, (10) 16.2725(9) nm/7.2352(8) nm, (11) 13.8581(6) nm/7.2352(8) nm and (12) 15.6801(11) nm/6.21115(14) nm.

The five C-like yttrium lines listed in Table 1 include an M1 transition at a 17.0632(7) nm wavelength. The ratio of this M1 line to the E1 line at 8.4792(19) nm varies by a factor of 45 or less in the electron density range of  $10^{15} \text{ cm}^{-3}$ – $10^{18} \text{ cm}^{-3}$ . The line intensity ratio  $I(17.0632(7))/I(11.1236(9))$  varies by more than two orders of magnitude for the same range of electron density. This line ratio also shows dependence on the electron temperature at lower densities as illustrated in Figure 7a. The line ratio of the M1 line at 17.0632(7) nm to another line at the FAC wavelength of 12.3869 nm shows a similar dependence on electron density and temperature because both of the E1 transitions at 11.1236(9) nm and 12.3869 nm arise from the same upper level decaying to the second and third energy levels, respectively. The line at 12.3869 nm, which is about half of the intensity of line at 11.1236(9) nm, could not be resolved due to strong blend with a Na-like Xe line at 12.3939(7) nm. However, at other plasma conditions with no Xe, this line should be easily resolved.

Among the seven identified N-like yttrium lines, four of the lines arise from E1 transitions, and three arise from M1 transitions. The ratios of the M1/E1 intensity show a dependence on  $n_e$  between  $10^{15} \text{ cm}^{-3}$  and  $10^{18} \text{ cm}^{-3}$  of a maximum of two orders of magnitude. According to our FAC calculations, the transition probability of the M1 line at 14.8036(5) nm is  $6.75 \times 10^5 \text{ s}^{-1}$  compared to the transition probability of  $3.9 \times 10^6 \text{ s}^{-1}$  for the M1 line at 12.0926(6) nm and  $3.7 \times 10^6 \text{ s}^{-1}$  for the M1 line at 17.8665(6) nm. This explains why the ratios  $I(14.8036(5))/I(9.9054(10))$  and  $I(14.8036(5))/I(8.8822(7))$  start decreasing at densities of  $10^{15} \text{ cm}^{-3}$ , whereas the intensity ratios of the M1 line at 12.0926(6) nm to the E1 lines and the M1 line at 17.8665(6) nm to the E1 lines only start to fall off at densities of  $10^{16} \text{ cm}^{-3}$  and higher. These transitions are illustrated in the Grotrian diagram shown in Figure 8.



**Figure 8.** Partial Grotrian diagram of the ground state and first lowest excited configurations of N-like yttrium. The number labels in increasing order from 1–7 correspond to the lines at 4.9858(6) nm, 5.9329(4) nm, 8.8822(7) nm, 9.9054(10) nm, 12.0926(6) nm, 14.8036(5) nm and 17.8665(6) nm, respectively. Only three of the energy levels for the  $2s2p^4$  configuration are shown. The dashed red lines correspond to magnetic dipole (M1) transitions, and the dotted black lines correspond to electric dipole (E1) transitions.

A closer look at the the density dependence of M1/E1 ratios in N-like ions gives an insight into the population scheme of allowed and metastable upper levels. For instance, let us take the population

and depopulation channels of the metastable level in the ground state configuration  $2p^3$  that is the upper level of the 17.8665(6) nm M1 transition and a  $2s2p^4$  excited state level that is the origin of three E1 transitions (5.9329(4) nm, 8.8822(7) nm and 9.9054(10) nm wavelengths). At a temperature of 1500 eV, the metastable level  $2p^3$  at a lower density of  $10^{12}$  cm $^{-3}$  is depopulated by radiative decay with 99.96% probability. At a higher density of  $10^{16}$  cm $^{-3}$ , the depopulation is 73% by collisional excitation to higher levels, 3% by collisional deexcitation to a lower ground state level, and only a 21% probability remains for radiative decay. At an even more elevated electron density of  $10^{18}$  cm $^{-3}$ , the level is depopulated mostly by collisional excitation with nearly 94% probability, leaving 4% to collisional deexcitation, 1% to radiative recombination and a negligible probability (0.27%) to radiation. The  $2s2p^4$  excited level is depopulated 100% by radiative decay at  $10^{12}$  cm $^{-3}$  and  $10^{16}$  cm $^{-3}$ , and the probability only slightly lowers to 99.6% at  $10^{18}$  cm $^{-3}$ . This means that the ratio of the intensity of the  $2s2p^4$  E1 transitions to that of the  $2p^3$  M1 transition shows a strong variation with the electron density.

Out of the eight O-like yttrium lines, we observed two that originate from M1 transitions at 13.8581(6) nm and 16.2725(9) nm. The intensity ratios between the M1 and E1 transitions vary by more than an order of magnitude in the density ranges we investigated. For instance, the intensity ratio  $I(13.8581(6))/I(19.4383(8))$  changes by a factor of 67 for densities ranging from  $10^{15}$  cm $^{-3}$ – $10^{18}$  cm $^{-3}$ .

For the one M1 and two E1 lines in F-like Y, an order of magnitude variation is seen for the intensity ratio of M1 line at 15.6801(11) nm to the E1 line at 6.2115(14) nm.

## 8. Conclusions

New and previously-measured EUV lines in L-shell ions along with transitions in a few M-shell ions of highly charged yttrium were observed. The measurements were performed with an electron beam ion trap, and spectral lines were recorded in the wavelength region of 4 nm–20 nm. The experimental uncertainties were combinations of statistical and systematic uncertainties that included sources with calibration origins and uncertainties from unresolved blends. The total uncertainties ranged between 0.0004 nm and 0.0020 nm. Line identifications were inferred from comparisons with spectra simulated from the collisional-radiative model NOMAD based on a non-Maxwellian distribution designed for EBIT-like environments. For Ne-like Y ions, a better agreement between theory and experiment was found using relativistic many-body perturbation theory (RMBPT) [68]. Several of the identified forbidden M1 transitions were found to be potentially useful for density diagnostics of laboratory, fusion and astrophysical plasmas.

**Acknowledgments:** This work was funded by the Measurement Science and Engineering (MSE) Research Grant Programs of the Department of Commerce at the National Institute of Standards and Technology (NIST). We would like to thank the Department of Physics and Astronomy at Clemson University for their support. We are grateful to M. Safronova for providing the theory for Ne-like Y ions. J.M.D. acknowledges support from a National Research Council Associateship award at NIST.

**Author Contributions:** E.T. and J.D.G. contributed to the design and construction of the apparatus. R.S., E.T., Y.R. and J.M.D. conceived of and designed the experiments. R.S., J.M.D., E.T. and J.D.G. performed the experiments. Y.R. performed the calculations. R.S. analyzed the data. All authors contributed to writing the paper.

**Conflicts of Interest:** The authors declare no conflict of interest.

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Article

# Spectrum of Singly Charged Uranium (U II) : Theoretical Interpretation of Energy Levels, Partition Function and Classified Ultraviolet Lines

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Academic Editor: Joseph Reader

Received: 23 March 2017; Accepted: 16 June 2017; Published: 26 June 2017

**Abstract:** In an attempt to improve U II analysis, the lowest configurations of both parities have been interpreted by means of the Racah-Slater parametric method, using Cowan codes. In the odd parity, including the ground state, 253 levels of the interacting configurations  $5f^37s^2 + 5f^36d7s + 5f^36d^2 + 5f^47p + 5f^5$  are interpreted by 24 free parameters and 64 constrained ones, with a root mean square (*rms*) deviation of  $60 \text{ cm}^{-1}$ . In the even parity, the four known configurations  $5f^47s, 5f^46d, 5f^26d^27s, 5f^26d7s^2$  and the unknown  $5f^26d^3$  form a basis for interpreting 125 levels with a *rms* deviation of  $84 \text{ cm}^{-1}$ . Due to perturbations, the theoretical description of the higher configurations  $5f^37s7p + 5f^36d7p$  remains unsatisfactory. The known and predicted levels of U II are used for a determination of the partition function. The parametric study led us to a re-investigation of high resolution ultraviolet spectrum of uranium recorded at the Meudon Observatory in the late eighties, of which the analysis was unachieved. In the course of the present study, a number of 451 lines of U II has been classified in the region  $2344 - 2955 \text{ \AA}$ . One new level has been established as  $5f^36d7p \text{ } ^4I^6K(J = 5.5)$  at  $39113.98 \pm 0.1 \text{ cm}^{-1}$ .

**Keywords:** uranium; actinide ions; emission spectrum; energy levels; energy parameters; partition function

## 1. Introduction

The spectroscopy of uranium is of interest in many respects. Being the element with the highest atomic number ( $Z = 92$ ) naturally available, the nuclear decay of  $^{238}\text{U}$  provides a tool for the evaluation of the age of the Universe [1]. In the astrophysical plasma models, the ionized uranium (U II) transition at  $3859.572 \text{ \AA}$  ( $5f^36d7s \text{ } ^6L_{11/2} - 5f^36d7p \text{ } ^6M_{13/2}$ ) is used for the diagnostics. Not only are specific radiative data for this transition needed, but so are partition functions that depend on energy levels relative to the ground level  $5f^37s^2 \text{ } ^4I_{9/2}$ . Therefore a comprehensive picture of the level scheme in ionized uranium is desired. For U II, as for other complex spectra of heavy elements, the interpretation of the observed emission lines does not allow a complete determination of the energy level scheme. Nevertheless, by application of the Racah-Slater parametric method, the energy parameters adjusted against known experimental energy values  $E_{exp}$  should lead to improved predictions of energies  $E_{th}$  for the levels left undetermined. The relevance of the methods that were used with success in lower- $Z$  elements [2] was confirmed in the cases of several higher- $Z$  elements, including thorium [3,4],

despite the fact that the non-relativistic perturbative model was primarily unsatisfactory for these heavy systems. Due to the limited computer capacities in the early times, the previous calculations on U II [5,6] had to neglect configuration interaction (CI) effects or to use truncated bases of configurations. Therefore, the necessary limitation of core configurations  $5f^3$  and  $5f^4$  to their lowest  $LS$  terms impaired the calculated energies and wave functions for the  $5f^3l''$  and  $5f^4l$  levels, consequence of the large spin-orbit interactions and the intermediate coupling conditions.

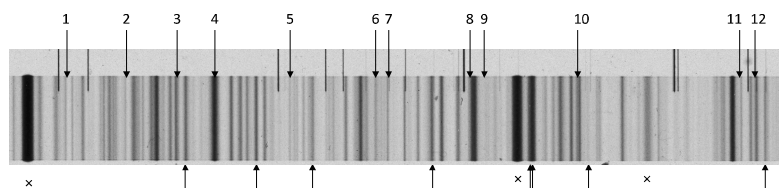
The critical compilation of energy levels and spectra of actinides published in 1992 by Blaise and Wyart [3] provided preliminary tables of energy levels of both parities in U II. The compilation of U II was based on emission data from Steinhaus et al. [7] and on new FTS measurements by Palmer et al. [8]. In particular, energy values of the lowest levels of configurations involving  $5f, 6d, 7s, 7p$  electrons were reported, thus updating the previous estimates by Brewer [9]. The list of experimental energy levels in U II was further extended by Blaise et al. [6]. Although the earlier calculations [5,6] usefully supported the search for energy levels, it is worth taking advantage of the present possibilities of Cowan codes [10,11] implemented on modern computers for improving the interpretation of the level scheme in U II, and more generally in actinides. This is the main purpose of the present work.

On the experimental side, a set of uranium emission spectra in the ultraviolet range (1000–3000 Å) recorded in the late eighties at the Meudon Observatory was available at the beginning of the present work. The original aim of these recordings, involving one of the present authors (JFW), was to support the critical compilation of the U III spectrum in Blaise and Wyart [3] by supplementing the Fourier Transform measurements [12] in the range (2000 Å–4 μ) with data in the shorter wavelength range. However the spectrograms had been only partly measured and had never been completely analyzed, leaving most of the experimental material unpublished. Only improvements for U III were reported in an EGAS conference [13] and in the compilation [3]. The analysis of the unknown spectrum of U IV was also planned but never initiated. With the recent publication of IR data on uranium [14], these unused ultraviolet data represent an opportunity for a new step in a comprehensive description of ionized uranium emission spectra.

## 2. Available Experimental Data

The available experimental spectra in the wavelength range 1000–3000 Å were emitted by a vacuum triggered spark source with uranium electrode and recorded on photographic plates using the high-resolution 10.7 m normal incidence vacuum ultraviolet spectrograph of the Meudon Observatory. The spectrograph is equipped with a 3600 lines/mm holographic concave grating, leading to a linear dispersion of 0.26 Å/mm on the plates. At the time of the experiment, only partial measurement of the plates was carried out on a semi-automatic comparator (microdensitometer). Wavelength calibration was insured by external reference lines in a superimposed spectrum from a iron Penning discharge source. In addition to U III lines, the spectrograms contain known lines from U V [15] and U VI [16], and a number of unidentified lines. Among the last ones, many likely belong to the unknown U IV spectrum. Although the discharge conditions were favorable for producing more than doubly charged ions, many sharp lines were present at the long wavelength end, which we presumed to belong to U II. In the present work, more complete measurements have been resumed for the wavelength range 2250–2955 Å, by digitizing the spectral plates using a flatbed scanner. The plates were scanned simultaneously with a precision ruler with markings every 1 mm, allowing interpolation between markings for correction of possible distortions, as described in [17]. Then the positions of lines were determined by superimposing two symmetrical profiles of the line displayed by a “homemade” software that mimics the rotating prism set-up of the comparator [18]. For wavelength calibration, internal standards were preferred. These were chosen among the U III wavelengths from Fourier Transform Spectrometry (FTS) [12] and the U II Ritz wavelengths calculated from level energies determined by FTS [6]. For the wavelength range shorter than 2350 Å, some U V wavelengths [15] were used. The uncertainty of the wavelength measurements varies between  $\pm 0.001$  and  $\pm 0.003$  Å.

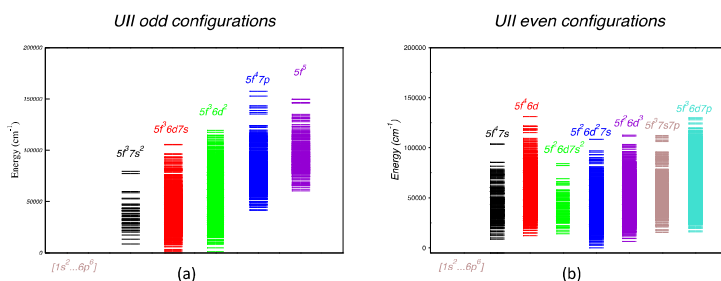
Figure 1 shows a section of the triggered spark spectrum between 2863–2875 Å. The shape of the lines, from relatively sharp (for U II) to hazy (for U IV) may be attributed to Doppler broadening as higher charged ions are produced in hotter part of the sparks. Identified U II lines are numbered. The numbers and corresponding wavelengths can be found in Table 9.



**Figure 1.** Section of a vacuum triggered spark spectrum (2863–2875 Å). Downward arrows: the U II lines identified in the present work, their numbers and corresponding wavelengths can be found in Table 9; Upward arrows: U III lines from [12]; x: Unidentified lines, likely from U IV. The superimposed iron spectrum is visible above the uranium spectrum but not used in the present work.

### 3. Theoretical Interpretation of the Energy Levels

Figure 2 shows a diagram of U II configurations of both parities included in the present study. The energy levels spread as predicted by ab initio calculations in the Relativistic Hartree-Fock mode (Cf text below).



**Figure 2.** Energy levels of U II belonging to the configurations included in the present study as predicted by ab initio HFR calculations. (a) Odd parity configurations. (b) Even parity configurations.

We started our work from the energy values tabulated in the final publication on U II [6]. Table 1 recalls the account of various observables available in [6] used for checking the validity of theoretical calculations. The lowest levels of configurations with 5*f*, 6*d*, 7*s* and 7*p* electrons, as determined in [6], may be supplemented by predictions for unknown configurations given in [3] according to Brewer’s work [9]. This guided our choice of the bases of interacting electronic configurations.

**Table 1.** Summary of experimental data available for the parametric interpretation of U II levels.  $N_{tot}$ : total number of levels;  $N_{ZE}$ : number of levels with Landé factor measured by Zeeman effect,  $N_{IS}$ : number of levels with measured isotope shift;  $N_{ident}$ : number of levels with empirical identification. The number of classified lines per level was not given in [6].

	Odd Parity Levels	Even Parity Levels
$N_{tot}$	354	809
$N_{ZE}$	137	355
$N_{IS}$	114	401
$N_{ident}$	109	113

### 3.1. Odd Parity Levels

The present work benefited from the similarities between lanthanides and actinides elements. In the periodic table of elements, neodymium occupies the same position in the lanthanide row as does uranium in the actinide row. Similarities between the two spectra do exist, although configurations built on the  $5f^3$  core are much lower relative to the core  $5f^4$  in U II than are those built on  $4f^3$  relative to  $4f^4$  in Nd II.

In Nd II, the basis set of overlapping odd configurations  $4f^3 5d 6s + 4f^3 5d^2 + 4f^3 6s^2 + 4f^4 6p + 4f^5$  was adopted for the parametric interpretation of 596 energy levels of these configurations [19,20] by means of the Cowan's codes [10,11]. It had been proven to be adequate by a *root mean square (rms)* deviation as small as  $53 \text{ cm}^{-1}$ . Since in U II the corresponding configurations (with principal quantum numbers increased by one) are also the lowest ones in the parity, we used the same basis set for resuming the calculation of odd parity levels, including the lowest odd parity levels listed in [6]. However, in the case of U II, the  $5f^5$  configuration is unknown but is involved by electrostatic interaction with the  $5f^3 6d^2$  configuration. The next higher unknown configuration  $5f^2 6d 7s 7p$  was not included in the basis. Since its lowest level is expected at  $38000 \pm 5000 \text{ cm}^{-1}$  above the ground state, according to Brewer's estimates [9], it should not overlap the other odd levels included in the calculation, although CI repulsion effects could be present.

In the first step of the calculation, the RCN and RCN2 codes were used in the Relativistic Hartree-Fock (HFR) mode. The electrostatic and spin-orbit radial integrals were then scaled with factors obtained as averages from earlier actinide calculations [4] and helped for generating the set of parameters for the first diagonalization by the RCG code. Appropriate corrections on the average energy  $E_{av}$  parameters were made for establishing a fair correspondence between calculated and experimental energies and Landé factors [6] for the low levels of  $f^3 ds$ ,  $f^3 d^2$  and  $f^3 s^2$ . Then the iterative Least Squares Fit (LSF) of the energy parameters was performed by means of the RCE code, minimizing the *rms* deviation  $\Delta E = \sqrt{\sum_i (E_i^{exp} - E_i^{th})^2 / (N_i - N_p)}$ , where  $N_i$  and  $N_p$  are respectively the number of experimental energies and the number of free parameters, with a few dozens of experimental energies to start. Constraints on the parameters were applied for preventing uncontrolled divergence problems. Step by step, the number of levels in the fit was increased up to 253 with a final *rms* deviation of  $60 \text{ cm}^{-1}$ . Final values for 22 free parameters and 64 constrained ones are reported in Table 2. The electrostatic and spin-orbit integrals are listed with their fitted values and their HFR values from which the scaling factors  $SF(P) = P_{fit} / P_{HFR}$  are derived. In addition to the explicit CI effects, second order CI effects of distant configurations have been taken into account by using effective parameters. These are  $\alpha$ ,  $\beta$  and  $\gamma$  for the  $5f^n$  core configurations and Slater forbidden parameters for  $5f^n nl$  (enabled by a specific option of the RCG code). Their initial values were chosen semi-empirically by comparison with earlier works [4].

The comparison of experimental and calculated levels is given in Table 3, which is ordered by increasing theoretical energies  $E_{th}$ . One may notice that leading *LS* components of eigenfunctions often represent a small part of the total wave functions. As an example, the eigenfunction of the level at  $E_{exp} = 8379.697 \text{ cm}^{-1}$  has three leading components representing respectively only 14, 11 and 10 percent of the total wavefunction. However, the calculation seems correct, as shown by the small deviations for both energies and Landé factors:  $E_{exp} - E_{th} = 22 \text{ cm}^{-1}$  and  $g_{exp} - g_{th} = 0.002$ . At higher energies, in the bulk of calculated levels, it occurs that leading *LS* components become as small as 3% only. Considering that the configuration sharing is more meaningful than tiny term components, we have summed the squared amplitudes in the wave functions separately for the 5 configurations. The dominant configuration and its percentage are respectively reported in the last two columns of the table.

Below  $20,000 \text{ cm}^{-1}$ , it was possible to establish a reliable correspondence between experimental and theoretical energies for the LSF procedure, which was generally supported by agreement between  $g_{th}$  and  $g_{exp}$  Landé factors, when available [6]. However, a few exceptions have been observed. As an example, the two  $J = 7.5$  levels at  $8394.362$  and  $8521.922 \text{ cm}^{-1}$  were previously [6] assigned respectively

as  $f^3d^2\ ^6M_{15/2}$  and  $f^3ds\ ^6K_{15/2}$ , based on the empirical identification of Landé factors and isotope shifts. In the present work, the initial HFR step predicted these two levels in an inverted order of energies at respectively 8536 and 8438  $\text{cm}^{-1}$ , with strongly mixed eigenfunctions. Furthermore, the LSF following this inverted order led to smaller deviations, although physically unsatisfactory. Therefore this order has been adopted in Table 3. Above 20,000  $\text{cm}^{-1}$  Landé factors are missing for a majority of levels and the quantum number  $J$  is reported as ambiguous for some of them. Since the correspondence between calculated and experimental energies becomes uncertain as energy increases, identifications above 25,726  $\text{cm}^{-1}$  are not reported here.

At an intermediate step of the parametric fitting, the previously assigned  $J$  value,  $J = 11/2$ , of the level  $E_{exp} = 13,695.737\ \text{cm}^{-1}$  raised questions. It was found that on one hand, no other level with  $J = 11/2$  was predicted between the two experimental levels at 13,270.612 and 13,961.850  $\text{cm}^{-1}$ , and on the other hand, one  $J = 9/2$  level was missing between  $E_{exp} = 13,450.490$  and 14,265.976  $\text{cm}^{-1}$ . The possibility for correcting the  $J$ -value for  $E_{exp} = 13,695.737$  was thus examined. Indeed, while a  $J = 11/2$  attribution can be justified by only one unique transition with a  $J = 13/2$  even level, a  $J = 9/2$  value is supported by 16 lines of [7] and by two unidentified lines from the infrared line list of [14] that fit transitions with  $J = 7/2$  even levels. Table 4 collects the transitions supporting the present assignation of a  $J = 9/2$  for this level. Similar ambiguity for some other levels led us to be cautious and to avoid inclusion of too many  $E_{exp}$  values in the LSF fitting process with no other reason but a small  $\Delta E$  value.

**Table 2.** Fitted parameters (in  $\text{cm}^{-1}$ ) for odd parity configurations of U II compared with HFR radial integrals. The scaling factors  $SF(P) = P_{fit}/P_{HFR}$  (dimensionless) are replaced by  $\Delta E = E_{fit} - E_{HFR}$  for  $E_{av}$  average energies (in  $\text{cm}^{-1}$ ). Constraints on some parameters are in the second column under ‘Cstr.’ (denoted ‘f’ for fixed parameters or ‘m’, which link parameters of the same ‘m’ to vary in a constant ratio). The HFR values of  $E_{av}$  parameters are relative to the ground state configuration  $5f^37s^2$  taken as zero value.

Param. $P$	Cstr.	$5f^37s^2$				$5f^36d7s$				$5f^36d^2$			
		$P_{fit}$	Unc.	$P_{HFR}$	$\Delta E/SF$	$P_{fit}$	Unc.	$P_{HFR}$	$\Delta E/SF$	$P_{fit}$	Unc.	$P_{HFR}$	$\Delta E/SF$
$E_{av}$		22711	54	0	22711	30141	35	4716	25425	41875	29	15459	26916
$F^2(ff)$	r1	47923	244	70159	0.683	47163	241	69047	0.683	46426	237	67969	0.683
$F^4(ff)$	r2	31974	437	45448	0.704	31411	429	44648	0.704	30868	422	43877	0.704
$F^6(ff)$	r3	21971	563	33210	0.662	21568	552	32601	0.662	21180	542	32015	0.662
$\alpha$	r4	36.3	1			36.3	1			36.3	1		
$\beta$	f	−600				−600				−600			
$\gamma$	f	1500				1500				1500			
$F^2(dd)$										23885	401	33922	0.704
$F^4(dd)$										12305	782	22307	0.551
$\alpha_d^2$	f									10			
$\zeta_f$	r5	1732.4	4	1868.5	0.927	1705.7	4	1839.8	0.927	1681.2	4	1813.4	0.927
$\zeta_d$	r6					1531.8	14	1793.1	0.854	1410.4	13	1650.9	0.854
$F^1(fd)$	r7					880	202			880	202		
$F^2(fd)$	r8					19605	205	28026	0.700	18724	196	26766	0.700
$F^4(fd)$	r9					13940	363	15151	0.920	13251	345	14404	0.920
$G^1(fd)$	r10					11304	81	18156	0.623	10995	78	17660	0.623
$G^2(fd)$	r11					833	295			833	295		
$G^3(fd)$	r12					11699	227	13054	0.896	11236	218	12535	0.896
$G^4(fd)$	r13					2858	355			2858	355		
$G^5(fd)$	r14					8054	353	9682	0.832	7696	337	9250	0.832
$G^3(fs)$						2583	88	4198	0.615				
$G^2(ds)$						13609	247	21081	0.646				



Table 2. Cont.

Param. <i>P</i>	Cstr.	$5f^47p$				$5f^5$				
		$P_{fit}$	Unc.	$P_{HFR}$	$\Delta E/SF$	$P_{fit}$	Unc.	$P_{HFR}$	$\Delta E/SF$	
$E_{av}$		60158	196	42943	17215	f	61000		58456	2544
$F^2(ff)$	r1	43973	224	64376	0.683	f	38003		55478	0.686
$F^4(ff)$	r2	29072	397	41323	0.704	f	24513		35118	0.691
$F^6(ff)$	r3	19894	509	30071	0.662	f	17151		25410	0.675
$\alpha$	r4	37.7	1				36.5	1		
$\beta$	f	-600					-600			
$\gamma$	f	1500					1500			
$\zeta_f$	r5	1550.4	4	1672.2	0.927		1333.5	3	1437.9	0.927
$\zeta_p$	f	3325.8	209	3293.7	1.01					
$F^1(fp)$	f	100								
$F^2(fp)$	f	7215		8016	0.900					
$G^2(fp)$	f	2058		2058	1.000					
$G^4(fp)$	f	1800		1800	1.000					
Configuration Interaction										
$5f^37s^2 - 5f^36d7s$										
$R^2(fs,fd)$	r15	-6614	71	-10104	0.65					
$R^3(fs,df)$	r15	-1442	15	-2204	0.65					
$5f^3s^2 - 5f^3d^2$										
$R^2(ss,dd)$	r15	14670	157	22412	0.65					
$5f^37s^2 - 5f^5$										
$R^3(ss,ff)$	r15	4516	48	6900	0.65					
$5f^36d7s - 5f^36d^2$										
$R^2(fs,fd)$	r15	-6605	71	-9955	0.65					
$R^3(fs,df)$	r15	-1500	16	-2284	0.65					
$R^2(ds,dd)$	r15	-16091	172	-24584	0.65					
$5f^36d7s - 5f^47p$										
$R^1(ds,fp)$	r15	-9384	101	-14337	0.65					
$R^3(ds,pf)$	r15	-2805	30	-4286	0.65					
$5f^36d7s - 5f^5$										
$R^3(ds,ff)$	r15	-3507	38	-5357	0.65					
$5f^36d^2 - 5f^47p$										
$R^1(dd,fp)$	r15	5580	60	8526	0.66					
$R^3(dd,fp)$	r15	2490	27	3805	0.66					
$5f^36d^2 - 5f^5$										
$R^1(dd,ff)$	r15	15269	164	23326	0.66					
$R^3(dd,ff)$	r15	10171	109	15537	0.66					
$R^5(dd,ff)$	r15	7325	78	11191	0.66					
$5f^47p - 5f^5$										
$R^2(fp,ff)$	r15	-2887	31	-4410	0.66					
$R^4(fp,ff)$	r15	-2501	27	-3821	0.66					

**Table 3.** Energy levels of U II, odd parity. Comparison of experimental energies and Landé factors with values calculated from the parameter set of Table 2.  $\Delta E = E^{exp} - E^{th}$ . The percentage of the leading term (notations from Cowan codes) and its configuration are specified by columns 7–9. The dominant configuration and its percentage are reported in the last two columns.

<i>J</i>	$E^{exp}$ ( $\text{cm}^{-1}$ )	$E^{th}$ ( $\text{cm}^{-1}$ )	$\Delta E$ ( $\text{cm}^{-1}$ )	$g_L^{th}$	$g_L^{exp}$	% 1 <sup>st</sup> comp	Conf	Term	Main conf	%
4.5	0.000	−56.8	56	0.756	0.765	77	f3s2	(4I)4I	f3s2	91.7
5.5	289.041	224.4	64	0.656	0.655	77	f3ds	(4I)6L	f3ds	99.9
4.5	914.765	930.2	−15	0.604	0.605	71	f3ds	(4I)6K	f3ds	96.2
6.5	1749.123	1715.5	33	0.864	0.865	45	f3ds	(4I)6L	f3ds	93.8
5.5	2294.696	2320.7	−26	0.868	0.865	47	f3ds	(4I)6K	f3ds	97.5
5.5	4420.871	4406.4	14	0.971	0.97	89	f3s2	(4I)4I	f3s2	93.6
6.5	4585.434	4577.9	7	0.793	0.785	28	f3d2	(4I)6M	f3d2	51.8
2.5	4706.273	4674.8	31	0.477	0.480	33	f3ds	(4I)6H	f3ds	96.8
7.5	5259.653	5247.0	12	1.007	1.015	68	f3ds	(4I)6L	f3ds	97.6
3.5	5401.503	5352.6	48	0.767	0.690	26	f3ds	(4I)6I	f3ds	98.0
6.5	5526.750	5549.1	−22	1.019	1.020	70	f3ds	(4I)6K	f3ds	98.3
3.5	5667.331	5695.5	−28	0.657	0.735	51	f3ds	(4I)6I	f3ds	96.9
5.5	5790.641	5827.3	−36	0.851	0.860	39	f3ds	(4I)6K	f3ds	95.5
6.5	6283.431	6392.9	−109	0.785	0.790	39	f3d2	(4I)6M	f3ds	54.5
4.5	6445.035	6471.2	−26	0.835	0.840	43	f3ds	(4I)6I	f3ds	97.6
0.5		6999.4		2.398		20	f3ds	(4F)4Pa	f3ds	97.8
1.5	7017.172	7096.0	−78	0.612	0.620	58	f3s2	(4F)4F	f3s2	90.8
4.5	7166.632	7259.7	−93	0.945	0.940	20	f3ds	(4I)6H	f3ds	94.9
5.5	7598.353	7626.3	−27	0.971	0.980	18	f3ds	(4I)4Ia	f3ds	98.0
3.5	7547.374	7629.2	−81	0.802	0.790	21	f3ds	(4I)4Ha	f3ds	84.8
6.5	8276.733	8248.0	28	1.093	1.090	84	f3s2	(4I)4I	f3s2	89.9
4.5	8379.697	8357.5	22	0.841	0.840	14	f3ds	(4I)6I	f3ds	76.1
1.5	8400.125	8426.1	−25	0.086	0.150	68	f3ds	(4I)6G	f3ds	97.7
2.5	8430.185	8432.6	−2	0.719	0.720	38	f3ds	(4I)6G	f3ds	94.3
7.5	8394.362	8437.9	−43	1.052	0.960	55	f3ds	(4I)6K	f3ds	74.2
5.5	8510.866	8446.9	63	0.854	0.860	11	f3ds	(4I)4Kb	f3ds	78.7
7.5	8521.922	8535.6	−13	0.968	1.060	41	f3d2	(4I)6M	f3d2	57.1
6.5	8755.640	8767.9	−12	1.042	1.040	14	f3ds	(4I)4Lb	f3ds	92.2
8.5	8853.748	8815.5	38	1.105	1.105	83	f3ds	(4I)6L	f3ds	98.6
3.5	9075.732	9020.5	55	0.873	0.870	15	f3ds	(4I)6H	f3ds	68.6
2.5	9344.625	9250.9	93	0.751	0.79	25	f3s2	(4G)4G	f3s2	47.1
4.5	9241.971	9254.9	−12	1.023	1.015	12	f3ds	(4I)6H	f3ds	77.6
5.5	9553.187	9584.8	−31	1.053	1.060	56	f3ds	(4I)6I	f3ds	96.4
6.5	9626.113	9637.3	−11	0.946	0.950	39	f3ds	(4I)4Kb	f3ds	83.9
4.5	9690.665	9707.7	−17	0.991	0.995	10	f3s2	(2H)2H2	f3ds	60.9
1.5	9881.618	9911.4	−29	0.272		51	f3ds	(4F)6G	f3ds	98.3
3.5	9933.226	9916.5	16	0.823	0.82	27	f3ds	(4I)4Hb	f3ds	88.1
4.5	9882.726	9967.6	−84	0.878	0.875	16	f3s2	(4I)4Ib	f3ds	43.9
2.5	10285.072	10178.1	106	0.454	0.42	35	f3ds	(4F)6H	f3ds	93.1
7.5	10198.312	10250.6	−52	0.968	0.960	44	f3ds	(4I)4Lb	f3ds	79.5
2.5	10366.253	10437.7	−71	0.922		58	f3s2	(4F)4F	f3s2	68.1
3.5	10444.432	10437.7	6	0.878	0.865	12	f3ds	(4F)4Hb	f3ds	74.7
1.5	-	10643.1		1.731		30	f3ds	(4F)6D	f3ds	97.8
5.5	10740.958	10688.6	52	0.690	0.685	68	f3d2	(4I)6L	f3d2	84.1
2.5	10732.087	10867.1	−135	0.953		29	f3ds	(4F)6G	f3ds	92.0
2.5	11350.714	11227.9	122	1.254		17	f3ds	(4F)6D	f3ds	95.3
1.5	-	11230.7		1.617		58	f3s2	(4S)4S	f3s2	91.6
3.5	11363.537	11289.2	74	1.033		13	f3d2	(4I)6Ia	f3ds	69.2
8.5	11382.321	11330.6	51	1.179	1.185	75	f3ds	(4I)6K	f3ds	96.4
4.5	11544.672	11426.0	118	0.673	0.690	45	f3d2	(4I)6Ka	f3d2	61.1
3.5	-	11571.9		0.994		23	f3s2	(4F)4F	f3s2	52.5
7.5	11708.483	11664.6	43	1.175	1.175	77	f3s2	(4I)4I	f3s2	92.2

Table 3. Cont.

$J$	$E^{exp}$ ( $\text{cm}^{-1}$ )	$E^{th}$ ( $\text{cm}^{-1}$ )	$\Delta E$ ( $\text{cm}^{-1}$ )	$g_L^{th}$	$g_L^{exp}$	% 1 <sup>st</sup> comp	Conf	Term	Main conf	%
3.5	11707.835	11743.7	-35	0.781	0.705	37	f3ds	(4G)6I	f3ds	60.0
5.5	11784.953	11809.2	-24	1.097		36	f3ds	(4I)6H	f3ds	97.0
6.5	11813.450	11833.5	-20	1.008	1.09	26	f3ds	(4I)6I	f3ds	81.0
6.5	11787.315	11841.2	-53	1.030	0.940	37	f3ds	(4I)6I	f3ds	83.9
4.5	11797.343	11854.3	-56	1.005		16	f3ds	(4I)6G	f3ds	96.3
0.5	-	11902.1		1.361		22	f3ds	(4F)2P	f3ds	95.6
2.5	12112.402	12095.7	16	0.957		10	f3ds	(4F)6G	f3ds	94.6
4.5	12055.788	12117.5	-61	0.976		18	f3ds	(4C)6I	f3ds	93.8
8.5	12033.378	12121.2	-87	1.014	1.005	78	f3d2	(4I)6M	f3d2	90.9
3.5	12092.319	12161.5	-69	0.823		22	f3ds	(4F)6H	f3ds	86.6
9.5	12350.555	12255.1	95	1.176	1.200	89	f3ds	(4I)6L	f3ds	99.0
1.5	-	12392.5		0.562		19	f3ds	(4G)4Fa	f3ds	90.4
5.5	12530.613	12519.6	10	0.987	1.000	12	f3d2	(4I)6Ka	f3ds	74.9
6.5	12629.355	12578.1	51	1.044	1.095	23	f3d2	(4I)6L	f3ds	65.8
3.5	12627.826	12582.6	45	0.965		24	f3s2	(4G)4G	f3ds	49.3
7.5	12660.559	12591.2	69	1.072	1.015	8	f3ds	(4I)4Lb	f3ds	88.1
5.5	12638.060	12690.0	-51	0.997		14	f3ds	(4I)4Ib	f3ds	78.1
2.5	-	12691.9		0.713		33	f3s2	(4G)4G	f3ds	47.4
4.5	12687.308	12718.0	-30	0.916		13	f3d2	(4I)6Ia	f3d2	49.9
1.5	-	12891.3		0.905		8	f3ds	(4F)4Db	f3ds	78.5
7.5	13015.838	12958.6	57	1.070	1.125	30	f3ds	(4I)4Kb	f3ds	96.0
3.5	13183.793	13117.1	66	0.982		22	f3ds	(4F)6G	f3ds	70.5
2.5	-	13125.8		0.997		20	f3ds	(4F)6G	f3ds	83.5
5.5	13089.590	13133.0	-43	0.941	0.940	34	f3d2	(4I)6Ka	f3d2	53.3
4.5	13275.365	13247.5	27	0.956		15	f3ds	(4I)6H	f3ds	78.9
5.5	13270.612	13272.1	-1	1.134		20	f3ds	(4I)6G	f3ds	92.7
6.5	13344.198	13275.1	69	0.905	0.910	35	f3d2	(4I)6L	f3d2	60.6
3.5	13450.362	13423.3	27	0.979		19	f3ds	(4I)6G	f3ds	80.0
4.5	13450.490	13449.0	1	1.014		15	f3ds	(4C)6I	f3ds	69.0
7.5	13503.319	13524.3	-20	1.101	1.13	19	f3ds	(4I)6I	f3ds	87.2
4.5	13695.737	13683.4	12	1.058		21	f3ds	(4F)6H	f3ds	85.3
3.5	13733.500	13730.8	2	0.934		22	f3ds	(4F)6G	f3ds	64.9
2.5	-	13751.0		0.638		17	f3d2	(4I)6Ha	f3ds	61.8
0.5	-	13817.0		0.009		51	f3ds	(4F)6F	f3ds	94.3
6.5	13975.278	13932.4	42	1.021		19	f3ds	(4I)2K	f3ds	81.3
2.5	13967.812	13944.8	23	0.734		18	f3ds	(4I)4Ga	f3ds	87.9
5.5	13961.850	13980.2	-18	0.972		14	f3ds	(4I)4Ib	f3ds	63.9
3.5	14107.329	14042.4	64	0.829		16	f3ds	(4F)4Hb	f3ds	84.4
9.5	-	14049.9		1.232		72	f3ds	(4I)6K	f3ds	97.9
1.5	-	14142.4		1.176		34	f3ds	(4F)6F	f3ds	88.8
8.5	14177.723	14148.0	29	1.072	1.085	60	f3ds	(4I)4Lb	f3ds	86.1
4.5	14265.976	14230.0	35	1.110		17	f3ds	(4I)4Hb	f3ds	81.3
4.5	14366.889	14399.2	-32	1.078		8	f3ds	(4I)6H	f3ds	90.1
1.5	-	14477.7		1.043		14	f3ds	(4S)6D	f3ds	65.8
6.5	-	14496.9		1.142		16	f3ds	(4I)4Ia	f3ds	96.8
6.5	14599.600	14557.6	42	0.934		17	f3d2	(4I)6L	f3d2	61.8
4.5	14654.181	14628.3	25	1.057		12	f3ds	(4F)6G	f3ds	75.8
2.5	-	14660.8		0.777		17	f3ds	(4F)4Gb	f3ds	71.4
7.5	14724.776	14738.1	-13	1.170	1.170	34	f3ds	(4I)6I	f3ds	96.5
5.5	14709.266	14771.1	-61	0.925	0.920	10	f3ds	(4I)4Ka	f3ds	49.4
3.5	14900.134	14873.4	26	1.010		7	f3ds	(4G)6G	f3ds	84.7
0.5	-	14905.3		1.636		32	f3ds	(4S)6D	f3ds	92.3
4.5	-	14981.0		1.177		44	f3s2	(4F)4F	f3s2	71.3
6.5	14991.377	14993.8	-2	1.180		17	f3ds	(4F)6H	f3ds	88.6
2.5	-	15013.4		1.198		13	f3ds	(4F)6P	f3ds	89.2

Table 3. Cont.

<i>J</i>	$E^{exp}$ ( $cm^{-1}$ )	$E^{th}$ ( $cm^{-1}$ )	$\Delta E$ ( $cm^{-1}$ )	$g_L^{th}$	$g_L^{exp}$	% 1 <sup>st</sup> comp	Conf	Term	Main conf	%
3.5	15147.878	15080.0	67	0.989		9	f3ds	(4F)4Gb	f3ds	79.0
1.5	-	15205.3		1.007		10	f3ds	(4G)6G	f3ds	66.4
5.5	15234.383	15205.3	29	1.058		7	f3ds	(4F)6H	f3ds	78.7
2.5	-	15280.5		1.147		33	f3ds	(4F)6F	f3ds	71.8
1.5	-	15308.6		1.985		55	f3ds	(4F)6P	f3ds	93.4
5.5	15330.434	15334.3	-3	1.123		14	f3ds	(4I)6G	f3ds	82.6
4.5	15413.346	15397.6	15	0.984		14	f3ds	(4G)6I	f3ds	52.3
0.5	-	15411.9		0.611		25	f3ds	(4S)4Db	f3ds	81.9
3.5	15587.280	15423.3	164	1.031		9	f3ds	(4I)4Ga	f3ds	63.2
5.5	15430.900	15483.0	-52	1.073		16	f3s2	(2H)2H2	f3ds	54.4
9.5	15534.868	15604.8	-69	1.093	1.095	89	f3d2	(4I)6M	f3ds	97.5
7.5	15692.655	15633.9	58	1.005		62	f3d2	(4I)6L	f3d2	92.4
10.5	-	15655.2		1.230		91	f3ds	(4I)6L	f3ds	99.7
8.5	15767.762	15683.0	84	1.200		36	f3ds	(4I)6I	f3ds	96.2
3.5	-	15689.4		1.136		11	f3ds	(4F)6P	f3ds	82.3
6.5	15717.452	15736.5	-19	1.026	1.04	35	f3d2	(4I)6Ka	f3d2	69.0
5.5	15863.755	15811.3	52	1.027		14	f3d2	(4I)6Ia	f3d2	51.9
4.5	15916.166	15879.5	36	0.971		28	f3d2	(4I)6Kb	f3ds	55.2
2.5	-	15883.4		0.628		10	f3d2	(4I)6Ha	f3d2	49.2
6.5	15884.560	15900.5	-15	1.072	1.150	12	f3ds	(4I)4Ka	f3ds	72.3
7.5	16156.487	16066.8	89	1.150		19	f3ds	(4I)6H	f3ds	82.9
2.5	16213.945	16073.4	140	1.010		7	f3ds	(4G)2F	f3ds	84.5
0.5	-	16099.2	0	2.345		32	f3ds	(4F)6D	f3ds	93.9
4.5	16063.244	16101.2	-37	0.889		21	f3d2	(4I)6Kb	f3ds	44.9
5.5	16003.163	16120.1	-116	1.091		20	f3ds	(4G)6I	f3ds	75.8
3.5	-	16140.4		1.052		15	f3ds	(4C)6H	f3ds	75.0
1.5	-	16176.8		1.130		9	f3ds	(4F)4Pa	f3ds	85.5
2.5	16336.514	16281.8	54	1.161		7	f3ds	(4F)6P	f3ds	74.4
3.5	16239.757	16285.9	-46	1.230		14	f3ds	(4F)6P	f3ds	83.5
4.5	16338.719	16290.5	48	1.040		6	f3ds	(4I)4Ia	f3ds	87.9
8.5	-	16419.3		1.098		22	f3ds	(4I)4La	f3ds	78.7
3.5	16376.820	16443.1	-66	1.048		9	f3ds	(4I)4Gb	f3ds	63.7
6.5	16532.589	16466.5	66	1.043		14	f3ds	(4I)2I	f3ds	77.6
1.5	-	16471.3		1.008		12	f3ds	(4F)2D	f3ds	86.2
2.5	16473.747	16481.7	-7	0.952		13	f3ds	(4F)6F	f3ds	65.1
5.5	16397.828	16490.5	-92	1.045		13	f3s2	(2H)2H2	f3ds	51.3
1.5	-	16528.6		0.844		10	f3s2	(4D)4D	f3ds	49.5
4.5	16514.265	16528.9	-14	0.986		16	f3s2	(4C)4G	f3ds	51.5
6.5	16618.369	16650.2	-31	0.987		60	f3s2	(2K)2K	f3s2	68.2
2.5	-	16660.2		1.339		22	f3ds	(4F)6P	f3ds	80.3
3.5	16672.399	16723.4	-51	1.019		7	f3ds	(4C)6G	f3ds	69.2
7.5	16690.212	16731.2	-40	0.986		14	f3ds	(2K)4M	f3ds	51.9
4.5	16819.694	16758.4	61	1.033		11	f3ds	(4F)6G	f3ds	68.2
5.5	16699.409	16782.6	-83	1.114		16	f3ds	(4I)6H	f3ds	78.5
2.5	16838.258	16808.1	30	0.982		10	f3ds	(4C)6H	f3ds	83.1
0.5	-	16830.2		0.230		14	f3d2	(4I)6F	f3d2	71.1
2.5	-	16867.1		1.060		8	f3ds	(4C)6H	f3ds	58.8
3.5	16857.015	16868.5	-11	0.838		10	f3d2	(4F)6I	f3ds	54.8
5.5	16758.024	16899.5	-141	1.026		12	f3ds	(4I)4Ka	f3ds	65.5
8.5	16982.510	16958.9	23	1.143		22	f3ds	(4I)4Kb	f3ds	91.3
4.5	-	16964.3		1.026		11	f3ds	(4F)4Hb	f3ds	64.7
6.5	16990.271	17005.7	-15	1.118		12	f3ds	(4I)4Ib	f3ds	59.7
1.5	-	17006.8		0.859		9	f3d2	(4I)6F	f3ds	55.0
2.5	17008.229	17102.2	-94	1.154		10	f3ds	(4F)6D	f3ds	84.7
3.5	-	17117.2		0.920		8	f3ds	(4C)4Hb	f3ds	60.7

Table 3. Cont.

$J$	$E^{exp}$ ( $\text{cm}^{-1}$ )	$E^{th}$ ( $\text{cm}^{-1}$ )	$\Delta E$ ( $\text{cm}^{-1}$ )	$g_L^{th}$	$g_L^{exp}$	% 1 <sup>st</sup> comp	Conf	Term	Main conf	%
5.5	17205.372	17170.4	34	1.120		28	f3ds	(4F)6G	f3ds	76.8
1.5	-	17192.9		0.957		17	f3ds	(4F)2P	f3ds	82.7
0.5	-	17217.5		0.499		30	f3s2	(2P)2P	f3s2	53.9
4.5	17200.903	17280.6	-79	0.979	0.970	10	f3ds	(4C)4Ib	f3d2	50.5
7.5	17259.216	17301.3	-42	1.118		12	f3ds	(4I)4Ib	f3ds	79.9
2.5	-	17320.0		0.619		18	f3ds	(4C)6H	f3ds	48.2
3.5	17381.930	17363.1	18	1.184		17	f3ds	(4F)6D	f3ds	84.2
1.5	-	17364.5		0.679		7	f3ds	(4F)4Fa	f3ds	77.1
4.5	17388.631	17392.7	-4	1.010		13	f3ds	(4I)4Hb	f3ds	65.2
6.5	17461.883	17423.5	38	1.155		18	f3ds	(4I)6G	f3ds	84.6
3.5	-	17481.4		1.163		15	f3ds	(4S)6D	f3ds	67.6
7.5	17556.776	17523.7	33	1.055		11	f3d2	(4I)6L	f3ds	68.6
1.5	-	17579.4		0.960		15	f3d2	(4I)6F	f3ds	57.4
2.5	17621.175	17607.3	13	0.941		5	f3d2	(4I)6Hb	f3ds	57.1
3.5	17560.922	17619.6	-58	0.991		10	f3ds	(4G)4Gb	f3ds	72.9
5.5	17755.028	17785.9	-30	1.050		11	f3ds	(2H)4K2	f3ds	84.0
6.5	17775.960	17808.2	-32	1.046		15	f3d2	(4I)6Ka	f3d2	57.7
0.5	-	17812.2		0.076		13	f3d2	(4I)6F	f3ds	51.0
3.5	17823.434	17820.9	2	0.950		12	f3d2	(4F)6I	f3d2	51.4
2.5	-	17857.4		0.987		5	f3s2	(4D)4D	f3d2	44.1
5.5	17922.769	17934.8	-12	0.973		11	f3d2	(4I)4Ka	f3d2	65.0
6.5	17888.312	17935.3	-47	1.157		21	f3ds	(4F)6H	f3ds	90.7
3.5	-	17959.5		0.963		12	f3d2	(4I)6Ha	f3ds	48.7
4.5	18009.838	17965.3	44	1.119		12	f3ds	(4F)6F	f3ds	71.6
9.5	-	17995.9		1.146		68	f3ds	(4I)4Lb	f3ds	81.7
8.5	18032.564	18015.8	16	1.044		25	f3d2	(4I)6L	f3d2	92.4
3.5	18041.437	18095.3	-53	0.913		9	f3d2	(4F)6I	f3ds	51.0
2.5	18178.854	18128.3	50	1.074		5	f3s2	(4D)4D	f3ds	54.7
5.5	18102.958	18150.0	-47	1.117		7	f3ds	(4F)6F	f3ds	79.1
4.5	-	18182.7		1.081		8	f3d2	(4I)6Ha	f3ds	70.3
3.5	-	18232.9		0.974		7	f3d2	(4I)6Ha	f3d2	40.4
3.5	18291.412	18326.3	-34	0.893		19	f3d2	(4I)6Ib	f3d2	63.0
1.5	-	18385.9		0.921		8	f3ds	(4F)6F	f3ds	59.8
4.5	-	18424.3		1.061		8	f3ds	(4F)4Ib	f3ds	68.1
0.5	-	18436.4		0.102		30	f3ds	(4G)6F	f3ds	59.7
1.5	-	18451.3		0.966		10	f3ds	(4S)6D	f3ds	54.7
2.5	18594.848	18459.0	135	0.995		4	f3d2	(4I)6Ha	f3d2	49.9
7.5	-	18486.3		1.112		7	f3ds	(4I)4Ia	f3ds	50.0
4.5	18526.283	18503.5	22	0.990		10	f3d2	(4I)6Ia	f3d2	54.0
3.5	-	18505.9		0.955		6	f3d2	(4I)6Ia	f3ds	50.6
7.5	18539.154	18523.8	15	1.098		10	f3ds	(4I)4Ia	f3ds	50.6
6.5	18451.979	18576.6	-124	1.116		40	f3ds	(4G)6I	f3ds	89.1
0.5	-	18623.1		1.461		35	f3ds	(4F)4Pb	f3ds	79.0
1.5	-	18664.9		1.001		11	f3ds	(4F)4Pb	f3ds	57.2
2.5	18852.922	18728.5	124	1.145		5	f3ds	(4S)6D	f3ds	72.2
5.5	18754.949	18740.0	14	1.013		12	f3d2	(4I)6Kb	f3d2	60.4
6.5	18788.827	18792.5	-3	1.042		14	f3d2	(4I)4La	f3d2	67.4
8.5	-	18796.5		1.153		29	f3ds	(2H)4K2	f3ds	90.2
3.5	18796.998	18857.5	-60	0.841		15	f3d2	(4I)6Hb	f3d2	61.4
5.5	18892.289	18858.6	33	0.969		24	f3d2	(4I)6Kb	f3d2	61.0
2.5	-	18913.1		1.008		5	f3d2	(4F)6Ga	f3ds	60.9
7.5	19017.870	18939.8	78	1.161		16	f3ds	(4I)4Ka	f3ds	81.9
10.5	-	18945.7		1.157		92	f3d2	(4I)6M	f3d2	100.
0.5	-	18964.1		0.717		10	f3ds	(4F)4Db	f3ds	72.7
4.5	19004.689	18967.7	36	1.024		5	f3ds	(4F)4Gb	f3ds	65.0
2.5	-	19032.8		0.700		14	f3d2	(4I)6Hb	f3ds	52.2

Table 3. Cont.

<i>J</i>	$E^{exp}$ ( $\text{cm}^{-1}$ )	$E^{th}$ ( $\text{cm}^{-1}$ )	$\Delta E$ ( $\text{cm}^{-1}$ )	$g_L^{th}$	$g_L^{exp}$	% 1 <sup>st</sup> comp	Conf	Term	Main conf	%
1.5	-	19059.2		1.033		16	f3ds	(4G)6F	f3ds	59.4
1.5	-	19112.9		1.073		13	f3ds	(4F)4Fb	f3ds	76.4
4.5	19147.489	19141.1	6	1.179		16	f3ds	(4F)6F	f3ds	70.5
5.5	19129.394	19157.3	-27	1.019		11	f3ds	(4I)4Gb	f3ds	62.9
8.5	19242.364	19215.9	26	1.042		48	f3d2	(4I)6L	f3d2	89.0
4.5	19237.394	19219.6	17	1.174		12	f3s2	(4G)4G	f3ds	66.2
6.5	19276.989	19249.2	27	1.166		8	f3ds	(4I)6G	f3ds	67.6
0.5	-	19274.8		0.018		13	f3ds	(4F)4Da	f3ds	62.7
4.5	19375.292	19300.7	74	1.031		11	f3d2	(4G)6K	f3ds	58.0
3.5	19316.823	19365.5	-48	1.211		16	f3ds	(4F)6P	f3ds	78.0
1.5	-	19372.2		0.983		12	f3d2	(4I)6G	f3ds	49.7
5.5	19473.367	19473.3		0.982		13	f3d2	(4I)6Kb	f3d2	64.7
3.5	-	19490.5		1.086		11	f3ds	(4F)4Fb	f3d2	50.5
7.5	19510.817	19551.1	-40	1.045		8	f3ds	(2K)4K	f3ds	71.7
7.5	-	19592.9		1.049		23	f3s2	(2K)2K	f3s2	47.0
4.5	19627.056	19598.3	28	1.093		9	f3d2	(4G)6K	f3ds	64.9
3.5	19570.868	19600.8	-29	1.017		5	f3ds	(4S)4Db	f3d2	56.0
2.5	19469.535	19630.2	-160	1.085		9	f3ds	(4G)6F	f3ds	68.6
1.5	-	19743.7		0.654		26	f3d2	(4I)6G	f3d2	48.0
7.5	19748.316	19758.5	-10	1.078		20	f3d2	(4I)6Ka	f3d2	46.6
2.5	-	19760.1		1.182		9	f3s2	(2D)2D1	f3ds	59.1
6.5	19694.329	19779.6	-85	1.023		9	f3ds	(2K)4K	f3ds	61.3
5.5	19733.338	19797.2	-63	1.079		13	f3ds	(4G)6H	f3ds	68.9
4.5	19869.609	19841.7	27	1.053		7	f3d2	(4I)6Hb	f3d2	52.8
3.5	-	19846.5		0.967		7	f3ds	(4S)4Db	f3ds	68.2
9.5	-	19865.8		1.141		23	f3ds	(4I)4La	f3ds	81.4
6.5	-	19922.7		1.035		15	f3d2	(4I)6Kb	f3d2	56.3
4.5	20018.685	19953.9	64	0.910		28	f3d2	(4G)6K	f3d2	52.5
5.5	-	19960.6		1.063		16	f3ds	(2K)4K	f3ds	79.3
2.5	-	20001.7		0.970		10	f3d2	(4I)6G	f3d2	51.3
1.5	-	20038.3		0.807		8	f3d2	(4I)6G	f3ds	50.0
3.5	20084.775	20039.4	45	0.978		6	f3ds	(4F)4Gb	f3d2	45.1
0.5	-	20067.8		1.423		16	f3ds	(4G)6D	f3ds	58.5
6.5	20055.098	20097.5	-42	1.129		19	f3ds	(4F)6G	f3ds	66.5
5.5	-	20103.3		1.080		11	f3ds	(4G)6G	f3ds	73.9
3.5	20263.434	20107.4	156	1.038		11	f3d2	(4F)6H	f3d2	54.8
7.5	20148.474	20124.4	24	0.985		18	f3d2	(4I)4Ma	f3d2	51.4
8.5	-	20130.9		1.093		26	f3d2	(4I)6Ka	f3d2	83.3
4.5	20033.114	20149.0	-115	1.128		13	f3d2	(4I)6Ha	f3ds	47.2
2.5	-	20196.5		1.138		8	f3ds	(4G)6F	f3ds	49.0
1.5	-	20202.8		1.050		10	f3ds	(4D)6F	f3ds	67.7
6.5	-	20217.0		1.067		9	f3d2	(4I)4Lb	f3ds	66.3
5.5	-	20249.0		1.138		16	f3s2	(2H)2H1	f3ds	47.4
0.5	-	20290.5		0.067		17	f3ds	(4G)6F	f3ds	58.5
4.5	20340.780	20306.0	34	1.083		13	f3d2	(4F)6I	f3d2	51.7
2.5	-	20356.6		1.013		16	f3s2	(2D)2D1	f3ds	59.5
4.5	-	20458.9		0.949		7	f3ds	(2H)4I2	f3ds	52.5
6.5	-	20499.6		1.108		23	f3ds	(4I)4Hb	f3ds	86.7
3.5	20514.235	20526.7	-12	1.030		9	f3ds	(4G)6H	f3ds	68.5
4.5	20500.810	20528.4	-27	1.006		8	f3d2	(4F)6I	f3ds	61.3
2.5	-	20537.7		1.034		6	f3ds	(2G)4G1	f3ds	54.5
5.5	-	20541.7		1.078		9	f3ds	(4G)4Ib	f3ds	51.7
3.5	-	20595.8		1.055		7	f3ds	(4F)6F	f3ds	58.1
1.5	-	20632.0		1.171		7	f3ds	(4G)6F	f3ds	64.4
5.5	-	20634.6		1.069		8	f3ds	(2H)4I2	f3ds	67.9
4.5	-	20658.4		1.023		11	f3d2	(4I)6Hb	f3ds	49.6

Table 3. Cont.

$J$	$E^{exp}$ ( $\text{cm}^{-1}$ )	$E^{th}$ ( $\text{cm}^{-1}$ )	$\Delta E$ ( $\text{cm}^{-1}$ )	$g_L^{th}$	$g_L^{exp}$	% 1 <sup>st</sup> comp	Conf	Term	Main conf	%
7.5	-	20663.4		1.098		21	f3ds	(4G)6I	f3ds	71.6
8.5	-	20670.8		1.068		14	f3ds	(2K)4M	f3d2	50.5
2.5	-	20704.1		1.122		19	f3ds	(4G)6F	f3ds	65.7
7.5	-	20771.0		1.031		11	f3d2	(4I)4Ma	f3ds	52.3
6.5	-	20779.4		1.008		10	f3ds	(2K)4L	f3ds	61.0
3.5	-	20780.2		1.054		7	f3d2	(4F)6H	f3d2	52.7
0.5	-	20796.7		1.267		16	f3ds	(4G)6D	f3ds	65.5
4.5	20899.429	20808.9	90	1.065		8	f3ds	(4G)6G	f3ds	61.3
2.5	-	20851.8		0.970		26	f3s2	(2D)2D1	f3s2	33.0
5.5	-	20951.3		1.110		15	f3d2	(4I)6Ib	f3d2	55.1
1.5	-	20961.9		0.786		8	f3ds	(2P)4F	f3ds	58.5
3.5	20890.426	20965.3	-74	1.130		9	f3ds	(4F)4Fb	f3ds	50.1
5.5	-	21022.3		1.084		7	f3ds	(2H> 2I2	f3ds	59.9
7.5	20946.239	21023.1	-76	1.008		23	f3d2	(4I)4Mb	f3d2	79.4
4.5	21103.432	21118.7	-15	1.078		7	f3d2	(4F)6H	f3ds	50.6
1.5	-	21159.6		0.906		11	f3ds	(4G)6F	f3ds	54.0
3.5	21107.881	21165.2	-57	0.870		14	f3d2	(4G)6I	f3d2	49.3
7.5	-	21215.3		1.111		13	f3ds	(4F)6H	f3ds	84.4
4.5	-	21232.1		1.062		14	f3ds	(4G)4Hb	f3ds	55.3
6.5	-	21247.7		1.005		6	f3ds	(2H)2K2	f3d2	52.8
2.5	-	21256.4		1.004		6	f3d2	(4I)6G	f3d2	51.8
1.5	-	21288.7		1.046		5	f3ds	(4S)6D	f3ds	71.5
4.5	21387.040	21309.6	77	0.940		9	f3d2	(4G)6I	f3d2	74.1
5.5	-	21309.5		1.129		13	f3ds	(4F)6F	f3ds	62.0
2.5	-	21350.9		1.045		10	f3ds	(4G)6F	f3ds	57.4
0.5	-	21372.9		1.981		13	f3ds	(4D)6D	f3ds	64.7
3.5	-	21415.6		1.018		9	f3ds	(4F)2G	f3ds	70.7
5.5	-	21494.8		1.104		4	f3ds	(4F)6G	f3ds	66.0
1.5	-	21502.1		0.977		6	f3ds	(4G)4Fb	f3ds	64.9
8.5	-	21531.9		1.072		12	f3ds	(2K)4M	f3d2	58.7
2.5	-	21553.7		1.045		7	f3ds	(4D)6F	f3ds	65.9
8.5	-	21582.8		1.058		24	f3ds	(4I)4Kb	f3ds	78.3
6.5	21645.939	21597.3	48	1.152		12	f3d2	(4I)6Ha	f3ds	51.0
0.5	-	21604.6		0.518		11	f3s2	(2P)2P	f3ds	44.8
9.5	-	21618.8		1.159		73	f3d2	(4I)6L	f3d2	99.9
3.5	-	21651.4		1.144		11	f3ds	(4G)4Gb	f3ds	67.0
4.5	-	21656.8		1.177		21	f3ds	(2H)4F2	f3ds	82.7
5.5	-	21662.8		1.075		6	f3d2	(4I)6Hb	f3d2	65.7
2.5	-	21718.6		1.114		7	f3d2	(4F)6Ga	f3ds	51.7
0.5	-	21721.7		0.048		14	f3d2	(4S)6F	f3d2	58.4
4.5	21793.334	21750.4	42	1.067		10	f3d2	(4F)6Ga	f3d2	65.1
7.5	-	21768.7		1.100		9	f3ds	(2H)2K2	f3ds	92.0
6.5	-	21803.0		1.117		7	f3ds	(4I)4Ha	f3ds	75.2
5.5	-	21819.9		1.081		7	f3d2	(4I)6Ha	f3ds	51.0
4.5	-	21821.1		1.070		7	f3d2	(4G)6I	f3ds	52.6
3.5	-	21855.1		1.096		6	f3ds	(2H> 2F2	f3ds	63.9
6.5	21858.433	21863.2	-4	1.015		31	f3d2	(4I)6Kb	f3d2	80.9
2.5	-	21873.3		1.090		7	f3ds	(4F)4Pb	f3ds	70.7
5.5	-	21886.1		1.088		7	f3ds	(4F)4Gb	f3ds	53.7
2.5	-	21942.1		1.178		8	f3d2	(4F)6P	f3d2	70.4
1.5	-	21944.2		0.872		8	f3d2	(4S)6F	f3ds	44.7
4.5	-	21981.2		1.074		8	f3d2	(4F)6H	f3ds	65.1
3.5	-	22046.5		1.089		6	f3d2	(4F)6Ga	f3ds	61.1
1.5	-	22059.7		1.278		11	f3ds	(4G)6D	f3ds	58.5
2.5	-	22070.4		0.903		6	f3ds	(4G)4Gb	f3ds	60.4
5.5	-	22089.4		1.062		24	f3s2	(2I)2I	f3d2	33.5

Table 3. Cont.

$J$	$E^{exp}$ ( $\text{cm}^{-1}$ )	$E^{th}$ ( $\text{cm}^{-1}$ )	$\Delta E$ ( $\text{cm}^{-1}$ )	$g_L^{th}$	$g_L^{exp}$	% 1 <sup>st</sup> comp	Conf	Term	Main conf	%
5.5	-	22123.0		1.023		14	f3d2	(4G)6K	f3d2	62.3
1.5	-	22127.9		1.207		88	f3d2	(4I)6M	f3d2	100.
8.5	-	22150.9		1.120		16	f3ds	(4I)6I	f3ds	84.2
3.5	-	22152.9		1.206		18	f3ds	(4G)6F	f3ds	74.8
3.5	-	22197.0		1.101		8	f3d2	(4I)6F	f3d2	59.6
4.5	22230.453	22197.0	33	1.114		7	f3s2	(2G)2G1	f3d2	41.3
6.5	-	22225.0		1.093		4	f3ds	(4G)6G	f3d2	51.3
2.5	-	22226.7		1.125		8	f3ds	(2H)4F2	f3ds	70.4
4.5	-	22262.3		0.943		8	f3d2	(4G)6I	f3ds	49.9
1.5	-	22269.6		1.121		6	f3ds	(4D)6D	f3d2	50.6
6.5	-	22273.6		1.086		10	f3ds	(4F)4Hb	f3ds	64.9
4.5	22305.305	22289.0	16	1.090		15	f3ds	(4I)2G	f3ds	55.5
7.5	-	22300.7		1.062		15	f3ds	(4I)4Ib	f3ds	58.6
3.5	-	22350.7		0.985		9	f3d2	(4I)4Hc	f3d2	61.8
4.5	-	22398.8		1.054		8	f3s2	(2G)2G1	f3ds	42.7
1.5	-	22425.5		1.053		9	f3ds	(4F)4Fb	f3ds	62.9
3.5	-	22449.8		1.049		7	f3ds	(4G)6G	f3d2	50.1
5.5	-	22470.4		1.019		17	f3d2	(4G)6K	f3d2	78.5
5.5	22567.167	22555.9	11	1.080		11	f3d2	(4G)6K	f3d2	50.3
7.5	-	22582.5		1.220		23	f3ds	(4G)6H	f3ds	68.3
2.5	-	22589.1		0.927		6	f3d2	(4I)4Gb	f3d2	58.8
4.5	-	22604.6		1.115		5	f3ds	(4I)4Ga	f3ds	49.4
0.5	-	22620.1		0.894		11	f3ds	(4D)6D	f3ds	60.9
3.5	-	22645.0		1.020		5	f3ds	(4I)4Ga	f3ds	51.8
6.5	-	22692.1		1.223		23	f3ds	(4G)6G	f3ds	80.8
2.5	-	22693.8		1.021		6	f3ds	(2D)4F2	f3ds	61.9
5.5	-	22708.2		1.185		6	f3ds	(4G)6G	f3ds	53.5
3.5	-	22729.6		1.131		7	f3ds	(4D)6D	f3ds	58.6
5.5	22813.792	22788.4	25	1.049		6	f3ds	(2K)4I	f3ds	52.7
3.5	-	22793.4		1.215		8	f3s2	(4D)4D	f3ds	68.0
7.5	-	22819.3		1.048		12	f3d2	(4I)6Kb	f3d2	64.3
6.5	-	22820.8		1.050		7	f3ds	(4G)4Ib	f3ds	55.7
0.5	-	22833.5		1.834		20	f3ds	(2D)2S1	f3ds	80.9
1.5	-	22833.8		1.287		9	f3d2	(4F)6P	f3d2	59.8
5.5	-	22851.9		1.043		7	f3d2	(4F)6I	f3d2	61.3
3.5	-	22857.0		1.182		7	f3s2	(4D)4D	f3ds	58.4
8.5	-	22888.2		1.135		34	f3d2	(4I)6Ka	f3d2	82.6
1.5	-	22942.6		1.091		7	f3ds	(4G)6D	f3ds	72.5
3.5	-	22963.0		1.051		8	f3ds	(2H> 2F2	f3ds	64.5
2.5	-	22972.1		1.012		5	f3ds	(4G)4Fb	f3ds	62.2
1.5	-	22991.6		0.806		8	f3d2	(4F)6Ga	f3ds	51.1
4.5	-	23006.5		1.047		3	f3d2	(4I)6Ib	f3d2	46.1
2.5	-	23031.6		1.181		4	f3ds	(2H> 2F2	f3ds	53.7
2.5	-	23062.2		1.204		14	f3ds	(4G)6D	f3ds	66.3
4.5	23106.350	23094.0	12	1.023		7	f3d2	(4G)6I	f3d2	63.8
6.5	23013.222	23100.7	-87	1.066		9	f3ds	(4G)6H	f3d2	53.5
8.5	-	23125.4		1.173		34	f3ds	(4G)6I	f3ds	84.5
5.5	23043.896	23135.7	-91	1.111		11	f3s2	(4G)4G	f3ds	49.8
0.5	-	23170.1		0.636		11	f3d2	(4F)6Fa	f3d2	53.0
5.5	-	23170.0		1.131		9	f3ds	(2H)4G2	f3ds	76.9
1.5	-	23225.8		1.043		5	f3ds	(2D)4P1	f3ds	54.4
3.5	-	23259.0		1.082		6	f3d2	(4F)6Fb	f3d2	51.4
7.5	23371.611	23282.8	88	1.047		26	f3d2	(4I)6Kb	f3d2	82.3
2.5	-	23293.3		0.964		5	f3d2	(4F)6Fa	f3ds	48.9
9.5	-	23318.7		1.196		47	f3d2	(4I)6Ka	f3d2	99.9



Table 3. Cont.

$J$	$E^{exp}$ ( $\text{cm}^{-1}$ )	$E^{th}$ ( $\text{cm}^{-1}$ )	$\Delta E$ ( $\text{cm}^{-1}$ )	$g_L^{th}$	$g_L^{exp}$	% 1 <sup>st</sup> comp	Conf	Term	Main conf	%
6.5	-	23329.5		1.092		7	f3d2	(4F)6H	f3d2	69.3
2.5	-	23330.0		1.174		6	f3ds	(2D)4P1	f3ds	73.2
1.5	-	23364.1		1.369		14	f3d2	(4F)6P	f3d2	49.4
0.5	-	23375.3		1.338		23	f3ds	(2D)2S1	f3ds	78.6
4.5	-	23397.0		1.097		11	f3ds	(4F)4Fb	f3ds	60.5
3.5	-	23461.6		1.152		6	f3d2	(4F)6P	f3d2	54.8
4.5	-	23474.8		1.020		13	f3d2	(4I)6G	f3d2	69.7
8.5	-	23507.1		1.032		28	f3d2	(4I)4Ma	f3d2	79.9
6.5	-	23534.5		1.060		5	f3ds	(2K)4L	f3ds	53.0
2.5	-	23557.4		1.091		6	f3d2	(4I)6F	f3d2	45.6
5.5	23528.305	23572.0	-43	1.079		6	f3d2	(4F)6H	f3d2	59.3
3.5	-	23585.2		1.047		4	f3ds	(2H)4G2	f3ds	54.3
5.5	-	23594.8		1.146		9	f3ds	(2H)4H2	f3ds	56.3
3.5	-	23601.2		1.214		9	f3ds	(4G)6D	f3ds	51.7
1.5	-	23648.2		0.829		9	f3ds	(2D)4F1	f3ds	62.1
7.5	-	23651.9		1.084		15	f3ds	(2H)4K2	f3ds	75.8
5.5	-	23671.9		1.137		6	f3d2	(4F)6Ga	f3d2	58.2
0.5	-	23688.3		0.487		15	f3d2	(4F)6Fa	f3ds	49.3
4.5	-	23706.2		1.100		8	f3d2	(4I)6G	f3d2	58.8
3.5	-	23726.6		1.131		3	f3ds	(4D)6F	f3ds	56.0
9.5	-	23730.0		1.088		41	f3ds	(2K)4M	f3ds	99.9
6.5	-	23735.2		1.093		8	f3d2	(4F)6I	f3ds	62.3
4.5	-	23760.6		1.112		10	f3d2	(4I)6F	f3d2	51.8
0.5	-	23774.7		0.513		14	f3s2	(4D)4D	f3ds	46.4
2.5	-	23811.4		0.973		9	f3d2	(4S)6F	f3d2	64.0
1.5	-	23813.8		0.906		15	f3d2	(4F)6Fa	f3d2	47.4
5.5	-	23814.8		1.095		5	f3s2	(4G)4G	f3d2	65.2
6.5	-	23819.7		1.094		5	f3ds	(4G)4Ib	f3d2	51.7
7.5	-	23823.9		1.037		21	f3d2	(4I)4Mb	f3d2	89.3
2.5	-	23844.1		1.166		5	f3ds	(2D)4P1	f3ds	62.3
6.5	-	23916.1		1.130		11	f3d2	(4I)6Ib	f3d2	65.2
2.5	-	23926.4		1.092		6	f3ds	(4F)4Ga	f3ds	75.7
1.5	-	23940.0		0.948		6	f3ds	(4D)6G	f3ds	65.3
3.5	-	23945.5		1.031		4	f3d2	(4G)6I	f3d2	52.2
4.5	23924.333	23956.4	-32	1.100		5	f3ds	(2K)4I	f3ds	70.9
0.5	-	23978.6		1.410		10	f3d2	(4S)6F	f3d2	66.6
8.5	-	23985.8		0.995		13	f3d2	(4I)4N	f3d2	54.4
5.5	-	24014.6		1.150		11	f3d2	(4F)6H	f3ds	49.7
5.5	-	24061.4		1.115		8	f3ds	(4G)6F	f3ds	70.7
7.5	-	24091.8		1.123		10	f3d2	(4I)6Ha	f3d2	64.6
4.5	-	24098.6		1.129		7	f3d2	(4I)6G	f3ds	50.5
1.5	-	24104.3		0.872		10	f3d2	(4F)6Gb	f3ds	43.9
5.5	-	24163.8		1.111		8	f3ds	(4G)4Gb	f3ds	54.0
3.5	-	24199.1		0.952		6	f3d2	(4I)4Hc	f3d2	62.1
0.5	-	24202.1		0.767		9	f3ds	(2D)4P1	f3ds	61.4
2.5	-	24214.8		1.139		5	f3ds	(4F)4Db	f3ds	62.7
3.5	-	24215.6		1.249		8	f3ds	(4G)6F	f3ds	48.6
4.5	-	24232.9		1.084		11	f3d2	(4F)6Ga	f3d2	58.8
6.5	-	24278.4		1.060		7	f3d2	(4G)6K	f3d2	64.9
9.5	-	24314.3		1.013		50	f3d2	(4I)4N	f3d2	99.9
2.5	-	24319.2		0.969		8	f3d2	(4G)6Ha	f3d2	57.6
2.5	-	24359.1		1.202		6	f3d2	(4F)6P	f3ds	48.6
1.5	-	24369.2		1.084		6	f3ds	(2D)4P1	f3ds	53.5
4.5	-	24377.2		1.100		4	f3ds	(4F)2H	f3d2	63.1
5.5	-	24383.2		1.098		7	f3ds	(2K)4I	f3ds	65.1
6.5	-	24388.0		1.063		10	f3ds	(2K)4K	f3ds	57.9

Table 3. Cont.

<i>J</i>	$E^{exp}$ ( $\text{cm}^{-1}$ )	$E^{th}$ ( $\text{cm}^{-1}$ )	$\Delta E$ ( $\text{cm}^{-1}$ )	$g_L^{th}$	$g_L^{exp}$	% 1 <sup>st</sup> comp	Conf	Term	Main conf	%
3.5	-	24403.0		1.168		8	f3ds	(4D)6G	f3ds	51.2
10.5	-	24433.6		1.209		71	f3d2	(4I)6L	f3d2	99.9
7.5	-	24441.5		1.077		12	f3ds	(2K)4K	f3ds	53.7
1.5	-	24488.1		0.673		20	f3d2	(4F)6Gb	f3d2	57.1
1.5	-	24505.5		1.121		5	f3ds	(2D)4P1	f3ds	65.9
4.5	24446.491	24505.8	-59	1.070		4	f3d2	(4I)2Ha	f3d2	47.6
3.5	-	24548.7		1.089		5	f3ds	(4D)4Gb	f3ds	53.8
2.5	-	24570.0		1.060		6	f3d2	(4I)4Ga	f3d2	59.3
1.5	-	24602.0		1.162		9	f3ds	(4D)6D	f3ds	63.0
8.5	-	24605.5		1.069		19	f3d2	(4I)4Mb	f3d2	58.0
4.5	-	24707.3		0.959		4	f3d2	(4I)4Ib	f3ds	46.1
5.5	24771.463	24720.3	51	1.096		7	f3d2	(4C)6I	f3ds	58.6
6.5	-	24735.1		1.056		36	f3d2	(4G)6K	f3d2	91.9
2.5	-	24740.2		1.161		11	f3ds	(4G)4Db	f3d2	49.4
7.5	-	24754.0		1.125		8	f3d2	(4I)6Ha	f3d2	52.1
3.5	-	24790.7		1.124		4	f3ds	(4I)6D	f3d2	55.0
6.5	-	24812.7		1.058		7	f3ds	(4G)4Hb	f3d2	53.6
0.5	-	24840.6		0.546		9	f3d2	(4I)6F	f3d2	55.9
7.5	-	24851.5		1.093		10	f3ds	(2K)4L	f3ds	53.1
3.5	-	24861.8		1.247		9	f3ds	(4G)6D	f3ds	60.8
2.5	-	24877.5		1.259		6	f3ds	(4D)6D	f3ds	53.9
1.5	-	24889.3		0.985		3	f3d2	(4F)6Fa	f3d2	54.6
5.5	-	24920.7		1.094		5	f3ds	(4G)6F	f3d2	58.8
4.5	24888.132	24945.0	-56	1.161		9	f3ds	(4G)6F	f3ds	50.8
2.5	-	24964.3		1.135		5	f3ds	(2P)4F	f3ds	52.9
6.5	-	24986.3		1.073		5	f3d2	(4G)6K	f3ds	50.2
4.5	24984.711	25008.7	-23	1.023		3	f3ds	(2H)4I1	f3ds	57.1
8.5	-	25008.2		1.077		14	f3d2	(4I)6Ia	f3d2	52.8
7.5	-	25019.1		1.182		11	f3d2	(4F)6H	f3d2	78.6
3.5	-	25045.7		1.077		4	f3ds	(2P)2Fa	f3d2	54.7
5.5	25111.924	25063.7	48	1.170		6	f3ds	(4F)4Gb	f3ds	56.2
3.5	-	25082.7		1.126		5	f3ds	(4G)6G	f3d2	49.5
1.5	-	25084.7		1.215		11	f3d2	(4F)6Da	f3d2	56.5
6.5	-	25130.0		1.110		10	f3ds	(4G)6H	f3ds	50.0
4.5	-	25154.2		1.173		7	f3ds	(2H> 2G2	f3ds	51.7
2.5	-	25158.7		1.017		8	f3ds	(2H)2F2	f3d2	49.9
2.5	-	25179.5		1.213		5	f3d2	(4F)6Fa	f3d2	51.9
1.5	-	25219.2		0.913		7	f3d2	(4I)4Fb	f3ds	51.9
4.5	-	25236.5		1.036		9	f3s2	(2H)2H1	f3ds	48.1
5.5	25245.183	25237.4	7	1.021		25	f3d2	(4C)6I	f3d2	71.9
8.5	-	25302.6		1.037		23	f3d2	(4I)4Mb	f3d2	54.4
2.5	-	25320.0		1.094		8	f3d2	(4S)6F	f3d2	49.8
4.5	-	25325.8		1.152		6	f3ds	(4F)4Fb	f3ds	58.6
6.5	-	25376.5		1.091		8	f3s2	(2I)2I	f3d2	68.6
0.5	-	25379.7		1.245		11	f3ds	(4D)6D	f3ds	67.7
3.5	-	25396.3		1.018		5	f3ds	(4F)2G	f3d2	47.5
6.5	-	25411.7		1.092		9	f3s2	(2I)2I	f3d2	50.4
3.5	-	25453.7		1.070		4	f3d2	(4I)2G	f3d2	47.5
4.5	25439.103	25463.6	-24	1.076		5	f3d2	(4S)6F	f3d2	58.6
5.5	25423.490	25476.5	-53	0.977		7	f3ds	(2I)4K	f3d2	54.5
1.5	-	25482.2		1.014		8	f3ds	(2D)4S1	f3ds	53.0
3.5	-	25516.3		1.045		4	f3d2	(4G)6I	f3d2	56.6
0.5	-	25521.6		0.983		6	f3ds	(2D> 2P1	f3ds	53.1
5.5	25514.656	25537.8	-23	1.082		10	f3ds	(4G)2I	f3ds	49.4
4.5	-	25545.5		1.169		12	f3d2	(4S)6F	f3d2	58.7
6.5	-	25558.5		1.096		7	f3ds	(4G)4Ia	f3ds	63.1

Table 3. Cont.

$J$	$E^{exp}$ ( $\text{cm}^{-1}$ )	$E^{th}$ ( $\text{cm}^{-1}$ )	$\Delta E$ ( $\text{cm}^{-1}$ )	$g_L^{th}$	$g_L^{exp}$	% 1 <sup>st</sup> comp	Conf	Term	Main conf	%
2.5	-	25582.3		1.134		9	f3d2	(4F)6Fa	f3ds	53.6
2.5	-	25603.8		0.986		6	f3ds	(4D)4Fb	f3d2	48.7
6.5	-	25647.8		1.088		42	f3s2	(2I)2I	f2s2	44.7
4.5	-	25665.7		1.137		4	f3ds	(4G)6F	f3d2	57.5
1.5	-	25666.4		1.063		7	f3ds	(4D)6G	f3d2	49.1
7.5	-	25671.0		1.079		7	f3ds	(2L)4M	f3ds	67.3
5.5	25726.260	25729.7	-3	1.101		4	f3d2	(4I)6G	f3ds	60.1
1.5	-	25754.9		1.030		6	f3d2	(4F)6Gb	f3d2	64.2

Table 4. Transitions of the U II odd parity level at 13695.737  $\text{cm}^{-1}$  with  $J = 4.5$  to even levels of  $J = 3.5$ .

$w_{Ritz}^I$ in Air ( $\text{\AA}$ )	$w_{Ritz}$ ( $\text{cm}^{-1}$ )	$w_{exp}$ ( $\text{cm}^{-1}$ )	$E_{even}$ ( $\text{cm}^{-1}$ )	$J$	$E_{odd}$ ( $\text{cm}^{-1}$ )	$J$	Int	Ref
14539.464	6875.953	6875.950	20571.690	3.5	13695.737	4.5	18.15	[14]
13112.082	7624.469	7624.468	21320.206	3.5	13695.737	4.5	9.22	[14]
4566.3396	21893.243	21893.239	35588.980	3.5	13695.737	4.5	142	[7]
4452.1493	22454.758	22454.757	36150.495	3.5	13695.737	4.5	112	[7]
4354.3144	22959.274	22959.276	36655.011	3.5	13695.737	4.5	135	[7]
4343.3456	23017.256	23017.274	36712.993	3.5	13695.737	4.5	139	[7]
4299.6016	23251.430	23251.429	36947.167	3.5	13695.737	4.5	131	[7]
4103.8897	24360.253	24360.293	38055.990	3.5	13695.737	4.5	236	[7]
4058.3724	24633.463	24633.459	38329.200	3.5	13695.737	4.5	269	[7]
4036.9830	24763.977	24763.973	38459.714	3.5	13695.737	4.5	138	[7]
4026.7550	24826.878	24826.899	38522.615	3.5	13695.737	4.5	151	[7]
3990.6927	25051.223	25051.233	38746.960	3.5	13695.737	4.5	126	[7]
3965.9476	25207.524	25207.546	38903.261	3.5	13695.737	4.5	133	[7]
3891.9441	25686.821	25686.815	39382.558	3.5	13695.737	4.5	171	[7]
3765.4517	26549.697	26549.706	40245.434	3.5	13695.737	4.5	166	[7]
3734.8311	26767.359	26767.361	40463.096	3.5	13695.737	4.5	157	[7]
3728.6081	26812.033	26812.083	40507.770	3.5	13695.737	4.5	141	[7]
3697.7707	27035.628	27035.603	40731.365	3.5	13695.737	4.5	217	[7]

### 3.2. Even Parity Levels

Similarly to the odd parity study, the RCN and RCN2 codes were used in the Relativistic Hartree-Fock (HFR) mode. Considering the large CI interaction integrals within the group  $5f^2(6d+7s)^3$ , the previously undetermined configuration  $5f^26d^3$  was added to the four lowest configurations  $5f^47s$ ,  $5f^46d$ ,  $5f^26d^27s$ ,  $5f^26d7s^2$ . Appropriate scaling of Slater and spin-orbit integrals and corrections on the average energy parameters were applied for preparing the initial input data of the RCG code and of the LSF in the RCE code. In the final cycle of optimization, 125 levels and 22 free parameters led to a *rms* deviation of  $84 \text{ cm}^{-1}$ , i.e., which is less satisfactory than in the odd parity. One of these levels, given at  $E_{exp} = 22917.453 \text{ cm}^{-1}$  without any label in [6] has been identified as the lowest level of the  $5f^26d^3$  configuration, slightly above the error bars of Brewer’s predictions [9]. It is seen that the scaling factors of fitted parameters reported in Table 5 are not very different from those obtained in the opposite parity (Table 2). With regard to the unachieved status of the parametric interpretation in the even parity, only the dominant configuration and the first component of the eigenfunctions are given in Table 6, together with the energies and Landé factors calculated in the final LSF.

Attempts to interpret  $5f^37s7p + 5f^36d7p$  with the same method of parametric fitting could not go beyond the optimization of the average energy  $E_{av}$  and spin-orbit  $\zeta_{5f}$  parameters. In Table 7 energy parameters adopted for  $5f^37s7p + 5f^36d7p$  are reported and they lead to the calculated energies in Table 8. The empirical attribution of  $E_{exp}$  levels to configurations derived from isotope shifts and transition intensities in [6] are not fully supported by the present calculations. There were more

$5f^37s7p$  labels in Table 2 of [6] than predicted from the present work (Cf Table 8). The quantitative evaluation of the CI effects within the whole group  $5f^4(7s + 6d) + 5f^2(6d + 7s)^3 + 5f^37s7p + 5f^36d7p$  has been attempted but has failed.

**Table 5.** Fitted parameters (in  $\text{cm}^{-1}$ ) for even parity configurations of U II with  $5f^2$  and  $5f^4$  cores compared with HFR radial integrals. The scaling factors are  $SF(P) = P_{fit}/P_{HFR}$  (dimensionless). They are replaced by  $\Delta E = E_{fit} - E_{HFR}$  for  $E_{av}$  average energies (in  $\text{cm}^{-1}$ ). Constraints on some parameters are in the ‘Cstr’ columns (denoted ‘f’ for fixed parameters or ‘rn’, which link parameters of the same ‘m’ to vary in a constant ratio). The HFR values of  $E_{av}$  parameters are relative to the lowest odd configuration  $5f^37s^2$  taken as zero value.

		$5f^47s$					$5f^46d$				
Param. $P$	$P_{fit}$	Cstr.	Unc.	$P_{HFR}$	$\Delta E/SF$	$P_{fit}$	Cstr.	Unc.	$P_{HFR}$	$\Delta E/SF$	
$E_{av}$	32165		112	15872	16293	46815		153	29044	17771	
$F^2(ff)$	42100	r1	471	63821	0.660	41167	r1	461	62408	0.660	
$F^4(ff)$	25599	r2	810	40934	0.625	24977	r2	790	39939	0.625	
$F^6(ff)$	18480	r3	814	29779	0.621	18016	r3	794	29030	0.621	
$\alpha$	19.5	r4	2			19.5	r4	2			
$\beta$	−600	f				−600	f				
$\gamma$	1600	f				1600	f				
$\zeta_f$	1557	r5	9	1661	0.938	1529	r5	9	1631	0.938	
$\zeta_d$						1145	r6	19	1369	0.836	
$F^1(fd)$						509	f				
$F^2(fd)$						20390	r8	520	24906	0.819	
$F^4(fd)$						14468	r9	776	13477	1.074	
$G^1(fd)$						11163	r10	248	18109	0.616	
$G^2(fd)$						1524	f	197			
$G^3(fd)$						13293	r11	511	12342	1.077	
$G^4(fd)$						2691	f				
$G^5(fd)$						7527	r12	923	8963	0.840	
$G^3(fs)$	2132		113	4561	0.467						
		$5f^26d7s^2$					$5f^26d^27s$				
Param. $P$	$P_{fit}$	Cstr.	Unc.	$P_{HFR}$	$\Delta E/SF$	$P_{fit}$	Cstr.	Unc.	$P_{HFR}$	$\Delta E/SF$	
$E_{av}$	39115		305	11841	27274	43050		208	12973	30077	
$F^2(ff)$	49005	r1	548	74289	0.660	48413	r1	542	73381	0.660	
$F^4(ff)$	30284	r2	958	48424	0.625	29870	r2	945	47763	0.625	
$F^6(ff)$	22025	r3	971	35490	0.621	21710	r3	957	34984	0.621	
$\alpha$	19.5	r4	2			19.5	r4	2			
$\beta$	−600	f				−600	f				
$\gamma$	1600	f				1600	f				
$F^2(dd)$						23302	r13	1546	37756	0.617	
$F^4(dd)$						14997	r16	3057	25080	0.598	
$\alpha(dd)$						10	f				
$\zeta_f$	1908	r5	11	2036	0.937	1884	r5	11	2010	0.937	
$\zeta_d$	1889	r6	32	2259	0.931	1760	r6		2104	0.837	
$F^1(fd)$	509	f				509	f				
$F^2(fd)$	25399	r8	647	31025	0.819	24437	r8	623	29850	0.819	
$F^4(fd)$	18040	r9	968	16803	1.074	17283	r9	927	16099	1.074	
$G^1(fd)$	11285	r10	250	18306	0.616	11030	r10	245	17892	0.616	
$G^2(fd)$	1524	f				1524	f				
$G^3(fd)$	14821	r11	570	13760	1.077	14324	r11	551	13299	1.077	
$G^4(fd)$	2691	f				2691	f				
$G^5(fd)$	8727	r12	1071	10389	0.840	8394	r12	1030	9996	0.840	
$G^3(fs)$	1578	f		2450	0.644	1885	r6	100	4033	0.467	
$G^2(ds)$						12984		597	20874	0.622	

Table 5. Cont.

$5f^26d^3$					
Param. $P$	$P_{fit}$	Cstr.	Unc.	$P_{HFR}$	$\Delta E/SF$
$E_{av}$	52093	401	20882	31211	
$F^2(ff)$	47830	r1	535	74289	0.660
$F^4(ff)$	29460	r2	932	44131	0.625
$F^6(ff)$	21410	r3	943	34500	0.621
$\alpha$	19.5	r4	2		
$\beta$	-600	f			
$\gamma$	1600	f			
$F^2(dd)$	22416	r13	1488	36319	0.617
$F^4(dd)$	14359	r16	2926	24013	0.598
$\alpha(dd)$	10	f			
$\zeta_f$	1860	r5	11	1986	0.937
$\zeta_d$	1635	r6	27	1956	0.836
$F^1(fd)$	509	f			
$F^2(fd)$	25399	r8	647	31025	0.819
$F^4(fd)$	18040	r9	968	16803	1.074
$G^1(fd)$	11285	r10	250	18306	0.616
$G^2(fd)$	1524	f			
$G^3(fd)$	13799	r11	570	12811	1.077
$G^4(fd)$	2691	f			
$G^5(fd)$	8050	r12	988	9587	0.840
Configuration Interaction					
$5f^47s - 5f^46d$					
$R^2(fs, fd)$	-6216	r14	357	-10574	0.588
$R^3(fs, df)$	-1875	r14	108	-3189	0.588
$5f^47s - 5f^26d7s^2$					
$R^3(ff, ds)$	-2310	r14	133	-3930	0.588
$5f^47s - 5f^26d^27s$					
$R^1(ff, dd)$	10962	r15	214	23117	0.474
$R^3(ff, dd)$	7708	r15	150	16225	0.474
$R^5(ff, dd)$	5672	r15	111	11961	0.474
$5f^46d - 5f^26d7s^2$					
$R^3(ff, ss)$	3556	r14	204	6050	0.588
$5f^46d - 5f^26d^27s$					
$R^3(ff, ds)$	-2385	r14	137	-4056	0.588
$5f^46d - 5f^26d^3$					
$R^1(ff, dd)$	10762	r15	210	22694	0.474
$R^3(ff, dd)$	7466	r15	146	15745	0.474
$R^5(ff, dd)$	5465	r15	107	11525	0.474
$5f^26d7s^2 - 5f^26d^27s$					
$R^2(fs, fd)$	-5657	r14	324	-9621	0.588
$R^3(fs, df)$	-908	r14	52	-1545	0.588
$R^2(ds, dd)$	-14874	r14	853	-25302	0.588
$5f^26d7s^2 - 5f^26d^3$					
$R^2(ss, dd)$	13119	r14	752	22316	0.588
$5f^26d^27s - 5f^26d^3$					
$R^2(fs, fd)$	-5558	r14	319	-9454	0.588
$R^4(fs, df)$	-938	r14	54	-1596	0.588
$R^2(ds, dd)$	-14638	r14	840	-24900	0.588

**Table 6.** Energy levels of U II, even parity with  $5f^2$  and  $5f^4$  parent configurations. Comparison of experimental energies and Landé factors with values calculated from the parameter set of Table 5.  $\Delta E = E^{exp} - E^{th}$ . The percentage, the configuration and the *LS* name of the leading component in the corresponding configuration are given in the last three columns.

<i>J</i>	$E^{exp}$ ( $cm^{-1}$ )	$E^{th}$ ( $cm^{-1}$ )	$\Delta E$ ( $cm^{-1}$ )	$g_L^{th}$	$g_L^{exp}$	% 1 <sup>st</sup> comp	Conf	Term
3.5	4663.803	4647	16	0.500	0.490	71	f4s	(5I)6I
4.5	5716.449	5564	152	0.830	0.830	40	f4s	(5I)6I
5.5	8347.690	8327	19	1.030	1.040	62	f4s	(5I)6I
4.5	8423.418	8423		0.797	0.790	41	f4s	(5I)4I
6.5	10740.265	10772	-31	1.142	1.145	72	f4s	(5I)6I
1.5	10987.204	10954	32	0.690	0.645	24	f4s	(5F)6F
2.5	11252.337	11138	114	1.175		22	f4s	(5F)6F
5.5	11389.469	11419	-30	0.961	0.970	59	f4s	(5I)4I
0.5		12254		-0.516		70	f4s	(5F)6F
5.5	12513.881	12493	19	0.676	0.680	61	f4s	(5I)6L
3.5	12804.950	12821	-16	0.922		12	f4s	(3G)4G2
7.5	12862.155	12880	-17	1.206	1.22	69	f4s	(5I)6I
4.5	13023.114	12905	118	1.134		11	f4s	(3G)4G2
1.5	13006.990	13044	-37	0.701		34	f4s	(5F)6F
5.5	13783.030	13733	49	0.695	0.685	56	f2d2s	(3H)6L
2.5	13758.142	13807	-49	0.931		30	f4s	(5G)6G
6.5	13865.969	13875	-9	1.068	1.10	61	f4s	(5I)4I
3.5	14018.821	13979	39	1.260		46	f4s	(5F)6F
1.5		14204		0.370		34	f4s	(5F)4F
2.5	14239.503	14439	-199	1.517		34	f4s	(5S)6S
8.5	14796.725	14742	54	1.245		61	f4s	(5I)6I
3.5	14767.466	14759	8	1.044		30	f4s	(5G)6G
2.5	14848.575	14955	-107	1.004		26	f4s	(5F)4F
2.5	15087.785	15088		0.951		23	f4s	(5G)4G
6.5	15392.416	15353	38	0.871	0.880	72	f4d	(5I)6L
3.5	15679.555	15734	-55	0.589	0.615	20	f2d2s	(3H)6Ia
3.5	15812.498	15857	-44	0.588	0.590	17	f2d2s	(5I)6I
1.5	15888.905	15870	18	1.529		42	f4s	(5S)4S
7.5	15992.765	15937	55	1.129	1.20	53	f4s	(5I)4I
6.5	15962.320	15959	3	0.903	0.900	46	f2d2s	(3H)6L
4.5	16211.704	16356	-145	0.663	0.615	53	f4d	(5I)6K
5.5	16379.878	16364	14	1.283		24	f4s	(5F)6F
4.5	16804.920	16546	259	0.759	0.845	19	f2d2s	(3H)6K
4.5	16656.412	16711	-55	1.318		52	f4s	(5F)6F
5.5	16706.303	16913	-207	0.788	0.790	36	f4s	(3K)4K2
4.5	17225.885	17216	9	0.991		14	f4s	(3H)6K
5.5	17434.363	17438	-4	0.795	0.800	20	f2ds2	(3K)4K2
6.5	17380.868	17463	-82	0.973		31	f4s	(3K)4K2
4.5	17392.211	17604	-212	0.860	0.785	16	f2d2s	(3H)6K
3.5		17683		1.115		49	f4s	(5F)4F
2.5		18060		0.680		17	f4d	(5I)4G
7.5	18136.366	18062	73	1.004	1.005	76	f4d	(5I)6L
4.5	18084.435	18154	-69	0.971		19	f4d	(5G)6G
4.5	18200.092	18334	-134	0.836	0.780	27	f2ds2	(3H)4I
3.5		18599		0.980		25	f4s	(5G)4G
4.5	18536.705	18600	-63	0.967		26	f4d	(5I)6I
2.5		18675		0.575		10	f4d	(5I)6H
5.5	18827.008	18694	133	0.908	0.945	36	f2d2s	(3H)6K
7.5	18656.355	18699	-42	1.053		21	f4s	(3L)4L
0.5		18737		2.635		39	f4s	(5D)6D
6.5	18617.807	18791	-173	0.908		42	f4s	(3L)4L
5.5	18654.316	18850	-196	0.874	0.880	70	f4d	(5I)6K
2.5		19047		0.751		12	f4s	(3G)4G2

Table 6. Cont.

<i>J</i>	$E^{exp}$ ( $cm^{-1}$ )	$E^{th}$ ( $cm^{-1}$ )	$\Delta E$ ( $cm^{-1}$ )	$g_L^{th}$	$g_L^{exp}$	% 1 <sup>st</sup> comp	Conf	Term
5.5	19097.594	19096	1	1.330		42	f4s	(5F)6F
2.5		19134		0.933		10	f4s	(5F)6F
1.5		19159		0.448		17	f2d2s	(3F)6Ga
3.5		19246		1.001		13	f4s	(3G)4G2
2.5	19395.168	19330	64	0.779		7	f2d2s	(3H)6Ha
2.5		19354		1.001		10	f4s	(3H)6Ha
1.5		19412		0.996		17	f4s	(5F)6F
3.5	19517.729	19546	-28	0.821	0.815	15	f4d	(5I)6I
7.5	19743.511	19756	-12	1.017	1.000	67	f2d2s	(3H)6L
1.5		19796		0.191		48	f4d	(5I)6G
2.5		19863		0.909		12	f2d2s	(3H)6Ha
5.5	19840.514	19899	-58	0.947		8	f4d	(5I)6K
6.5	19977.100	19935	41	0.969	0.960	32	f2d2s	(3H)6L
3.5	19971.328	19977	-5	0.857	0.860	11	f4d	(5I)4H
8.5	20230.479	20127	102	1.099		20	f4s	(5I)6I
5.5	20353.992	20310	43	1.029	1.015	29	f2d2s	(3H)6Ia
4.5		20365		1.208		50	f4s	(5F)4F
7.5	20425.567	20445	-20	0.975		32	f4s	(3M)4M
3.5	20571.690	20474	97	0.947	0.935	8	f4d	(3H)6Ha
0.5		20496		1.065		26	f4s	(3P)4P2
1.5		20530		1.274		20	f4s	(5D)6D
8.5	20739.844	20612	127	1.095	1.11	74	f4d	(5I)6L
2.5	20678.779	20672	6	1.066		8	f4s	(1D)2D3
4.5	20635.272	20721	-86	0.914	0.945	13	f2d2s	(3H)6Ia
6.5	20702.037	20789	-87	1.034	0.990	40	f4d	(5I)6K
1.5		20828		1.079		12	f4s	(3P)4P2
6.5	20934.186	20858	76	1.265		45	f4s	(5G)6G
3.5	20961.720	20901	60	0.877	0.855	11	f4d	(5I)6H
2.5		20917		0.750		14	f4d	(5I)6H
5.5	20742.878	20940	-197	1.012		29	f4d	(5I)6I
5.5	20932.139	21050	-118	1.173		25	f4s	(5G)6G
1.5		21053		1.534		31	f4s	(5D)6D
4.5	21154.557	21066	88	1.061	1.010	13	f4d	(5I)4H
4.5	21053.528	21089	-35	1.215		21	f4s	(3F)4F4
3.5	21207.738	21190	17	1.303	1.150	19	f4s	(5D)6D
3.5	21320.206	21514	-194	0.822	0.835	14	f4d	(3H)6Ia
5.5	21691.517	21532	159	0.961	0.975	15	f2d2s	(3H)4I
4.5	21555.275	21619	-63	0.915	1.025	9	f2d2s	(3H)4Ic
6.5	21710.768	21641	68	0.917	0.915	31	f2d2s	(3H)4Lb
3.5		21650		1.062		9	f4s	(3F)2F4
2.5		21719		0.862		15	f4d	(5F)6G
4.5		21720		1.001		26	f4s	(5G)4G
1.5		21728		0.478		12	f4s	(3F)4F3
0.5		21778		0.852		34	f4s	(5D)4D
0.5		21942		1.493		33	f4s	(3P)4P2
2.5		21953		1.186		15	f4s	(3D)2D1
3.5	21860.051	21954	-94	0.718	0.67	16	f2d2s	(3H)6Ia
3.5	22158.070	22053	104	0.910		11	f4d	(5I)6H
5.5	22157.162	22058	98	1.171		39	f4s	(5G)4G
6.5	21975.590	22058	-82	1.030	1.03	29	f4d	(5I)6K
2.5		22142		1.003		8	f4s	(3F)4F3
1.5		22153		0.300		25	f4d	(5F)6G
4.5	22165.179	22197	-32	1.007	0.895	12	f4d	(5F)6H
3.5	22250.398	22216	34	0.863	0.885	12	f2d2s	(3F)6I
4.5	22429.865	22303	126	0.874	0.935	13	f4s	(3I)4I1
5.5	22389.574	22326	62	0.992	1.040	6	f2d2s	(3H)6K

Table 6. Cont.

<i>J</i>	$E^{exp}$ ( $cm^{-1}$ )	$E^{th}$ ( $cm^{-1}$ )	$\Delta E$ ( $cm^{-1}$ )	$g_L^{th}$	$g_L^{exp}$	% 1 <sup>st</sup> comp	Conf	Term
6.5	22615.319	22534	80	0.986	0.995	28	f2d2s	(3H)4K
0.5		22613		1.207		14	f2ds2	(3F)2P
5.5	22764.904	22625	139	1.030	0.980	17	f4s	(1H)2H1
4.5	22642.478	22634	8	0.936	0.875	8	f2d2s	(3I)4I1
2.5		22696		1.168		14	f2d2s	(5D)6D
3.5	22815.123	22740	74	0.786		26	f2ds2	(3F)4H
7.5		22776		1.032		40	f4d	(5I)6K
3.5	22960.667	22891	69	0.997	0.945	9	f2d2s	(3H)6Ha
4.5	22868.033	22902	-34	0.943	0.980	9	f2d2s	(5I)6H
5.5	22917.453	22942	-25	0.759	0.860	38	f2d3	(3H)6L
6.5	23107.566	22945	161	1.120	1.060	29	f2d2s	(3H)6Ia
2.5	23029.458	23039	-9	0.988		17	f4d	(5I)6G
9.5		23076		1.160		71	f4d	(5I)6L
1.5		23104		1.446		15	f2d2s	(3H)6D
5.5	23241.365	23121	119	0.968	0.96	17	ds2	(3H)4I *
2.5		23148		1.070		13	f2d2s	(5D)6D
4.5	23241.033	23168	72	0.959	1.050	6	f2d2s	(5I)6I
3.5	23257.613	23205	52	0.597		21	f4d	(5G)6I
6.5	23234.820	23223	11	1.024	1.090	29	f4d	(5I)6I
2.5	23353.601	23264	89	0.779		20	f2d2s	(3H)6Ha
7.5	23262.359	23350	-87	1.102	1.070	24	f2d2s	(3H)6K
3.5		23412		0.960		13	f4d	(5I)6G
0.5		23428		2.116		14	f2d2s	(3H)6D
8.5		23441		1.107		73	f2d2s	(3H)6L
6.5		23492		1.202		24	f4s	(3H)4H3
4.5		23501		1.073		12	f4s	(3G)4G2
5.5		23628		1.033		11	f4d	(5I)4H
3.5		23644		0.849		11	f2d2s	(3H)6Ib
1.5	23673.649	23648	25	1.276		25	f4d	(5D)4D
6.5	23635.919	23712	-77	0.986	0.920	18	f2d2s	(3H)4Lb
2.5	23700.946	23739	-38	0.868		17	f2d2s	(3F)6H
5.5		23792		0.923		22	f2ds2	(3H)4I
4.5	23817.508	23802	15	0.958	0.870	11	f2d2s	(3H)6K
0.5		23827		1.989		9	f4d	(5S)6D
2.5	23905.877	23828	77	1.085		9	f4d	(3F)6H
3.5	23803.252	23831	-27	0.991		7	f4d	(3F)4G
7.5	24071.418	23927	143	1.023		41	f4s	(3L)4L
1.5		23943		0.969		7	f2d2s	(3H)6Ga
4.5		23962		0.947		8	f2d2s	(3H)6K
3.5	23895.471	24064	-169	0.969	0.735	10	f4s	(3G)2G2
6.5	24159.696	24072	86	0.922	0.965	31	f4s	(3L)4L
8.5		24074		1.069		42	f4s	(3L)4L
5.5	24010.467	24077	-66	0.934	0.975	18	f4d	(5I)4K
7.5	24247.529	24122	124	1.113		22	f4d	(5I)6I
4.5	24220.675	24158	62	1.094		7	f4d	(5F)6G
5.5		24168		0.989		7	f2d2s	(3H)2H3
2.5		24213		1.052		11	f4d	(5F)6F
3.5	24209.303	24243	-34	1.086		12	f2d2s	(3F)6Ga
1.5		24292		0.768		17	f2d2s	(5F)6F
2.5		24299		1.004		17	f4d	(5F)6G
6.5		24375		1.024		9	f4d	(5I)4K
7.5	24423.656	24381	42	0.995		38	f4d	(3L)2L
5.5		24432		1.037		12	f4s	(5G)4G
4.5		24440		1.016		12	f2d2s	(3F)6I
3.5		24491		1.262		17	f4s	(5D)6D
1.5		24501		0.628		15	f2d2s	(3H)6Ga
4.5		24593		1.023		13	f4d	(3H)6K



Table 6. Cont.

$J$	$E^{\text{exp}}$ ( $\text{cm}^{-1}$ )	$E^{\text{th}}$ ( $\text{cm}^{-1}$ )	$\Delta E$ ( $\text{cm}^{-1}$ )	$g_L^{\text{th}}$	$g_L^{\text{exp}}$	% 1 <sup>st</sup> comp	Conf	Term
0.5		24650		0.273		29	f2d2s	(3F)6Fa
7.5		24675		0.974		17	f4d	(3K)4M2
8.5		24686		1.084		30	f4d	(5I)6K
0.5		24712		-0.082		43	f4d	(5F)6F
3.5	24709.449	24720	-10	0.943		16	f2d2s	(3H)6Ib
5.5		24722		1.007		11	f4d	(5I)6H
1.5		24746		1.386		15	f4d	(5F)6D
4.5	24684.135	24802	-117	0.981	0.935	7	f2d2s	(3H)6K
2.5		24840		0.805		12	f2d2s	(3F)4G
9.5		24845		1.114		46	f4s	(3L)4L
5.5	24857.570	24893	-35	1.068		7	f2d2s	(3H)4Ga
4.5		24928		0.975		11	f2d2s	(3H)6K
3.5	24862.698	24946	-83	0.993		10	f2d2s	(3H)6Ib
6.5		24977		1.111		18	f4s	(3I)4I1
4.5		24981		1.159		16	f4s	(3F)4F2
2.5		24984		0.830		8	f2d2s	(3H)4Gc
8.5	25053.005	25075	-22	1.063		43	f4s	(3M)4M
3.5		25132		1.140		9	f4d	(3F)4F3
2.5		25247		0.917		7	f4s	(3F)2F3
6.5		25248		1.000		14	f2d2s	(3H)6L
3.5		25294		1.056		8	f4d	(5I)6G
5.5	25356.972	25334	22	0.997	1.020	9	f4d	(3H)4Kb
4.5		25343		1.003		9	f2d2s	(3H)4H
3.5		25346		1.020		10	f4d	(3H)6Ha
4.5		25424		0.904		23	f2d2s	(3H)6Ib
1.5		25434		0.868		7	f4d	(5F)6F
8.5		25458		1.157		22	f4d	(5I)6I
0.5		25477		1.513		12	f4d	(5G)4D
7.5	25399.465	25518	-119	0.986		32	f4s	(3M)4M
3.5		25532		0.989		9	f4s	(3F)2F2
4.5		25537		0.950		7	f2d2s	(3H)4I
1.5	25582.631	25561	21	1.305		14	f4d	(5S)6D
2.5		25564		0.793		9	f4d	(5G)6H
8.5		25575		1.040		44	f4s	(3M)2M
2.5		25628		0.942		7	f2d2s	(3H)6Ga
5.5	25626.941	25635	-8	1.038		8	f4s	(5I)6H
3.5		25637		1.038		8	f2d2s	(5F)6F
10.5		25657		1.215		72	f4d	(5I)6L
1.5		25669		0.638		15	f2d2s	(3H)4F
6.5		25714		1.088		14	f4d	(3H)6L
7.5	25667.906	25733	-65	1.164	1.100	29	f4s	(3I)4I1
5.5		25746		0.978		20	f2d2s	(3H)4Kb
2.5		25748		1.061		6	f2d2s	(3F)6Ga
3.5		25784		1.051		13	f2d2s	(3H)6Ga
7.5		25784		1.078		15	f2d2s	(3H)6L
2.5		25875		1.115		9	f4d	(5F)6F
6.5		25892		0.998		20	f2d2s	(3H)6L
5.5		25894		1.083		22	f2d2s	(3H)6Ha
1.5		25981		0.913		21	f2d2s	(3F)6Fa
0.5		26012		1.555		14	f4d	(5S)6D
4.5		26038		1.116		7	f2d2s	(5F)6G
6.5		26058		1.176		12	f4d	(5I)6G
2.5		26094		1.261		16	f4s	(3P)4P2
0.5		26143		0.461		29	f4s	(3D)4D1
5.5	26158.897	26164	-5	1.010		18	f2d2s	(3F)6I
1.5		26166		1.167		18	f4s	(3P)4P2
3.5		26246		0.996		7	f2d2s	(3H)4Hb

Table 6. Cont.

$J$	$E^{\text{exp}}$ ( $\text{cm}^{-1}$ )	$E^{\text{th}}$ ( $\text{cm}^{-1}$ )	$\Delta E$ ( $\text{cm}^{-1}$ )	$g_L^{\text{th}}$	$g_L^{\text{exp}}$	% 1 <sup>st</sup> comp	Conf	Term
5.5		26321		1.134		8	f4d	(3G)4G2
4.5		26343		1.008		9	f2d2s	(3H)6Ib
2.5		26364		1.209		16	f4s	(5D)4D
6.5		26375		1.035		18	f4s	(3I)2I1
8.5		26386		1.162		13	f2d2s	(3H)4Ka
1.5		26397		1.140		12	f4s	(3P)2P2
3.5		26446		1.063		4	f4d	(3H)4H2
4.5		26457		1.042		7	f4d	(5F)6G
2.5		26470		0.912		5	f4s	(3H)6D
7.5	26527.106	26493	33	1.095	1.075	17	f4d	(3H)4Lb
1.5		26521		1.308		10	f4d	(5F)6P
5.5		26544		1.093		9	f2d2s	(3H)4Kb
4.5		26569		1.066		7	f4d	(5D)6D
3.5		26623		1.160		6	f4d	(5S)6D
5.5	26628.496	26633	-5	1.065	1.155	19	f4d	(3H)6K
9.5		26641		1.176		41	f4d	(5I)6K
0.5		26642		0.493		8	f2d2s	(5G)6F
8.5		26703		1.050		30	f4d	(5I)6K
4.5		26717		1.094		7	f4s	(1G)2G4
0.5		26793		0.457		14	f4d	(5F)4D
2.5		26801		1.049		18	f2d2s	(3F)6Fa
3.5		26811		0.980		7	f2.d	(3H)4Hh
6.5		26842		1.015		12	f4d	(3H)4I
4.5		26856		1.076		6	f2d2s	(3G)2G2
5.5	26989.437	26863	125	1.103	1.095	13	f4d	(3H)6K
7.5		26868		1.061		34	f4s	(3H)6K
5.5		26903		1.059		12	f4d	(3H)6K
1.5		26918		0.766		6	f2d2s	(5F)6G
3.5		26919		1.111		14	f4s	(3F)4F4
7.5	26931.699	26961	-29	1.058		18	f4d	(5I)4L
2.5		26966		1.098		4	f2d2s	(3H)6D
3.5		26974		1.143		5	f4d	(5D)4D
4.5		26984		1.056		9	f4d	(5F)6F
5.5		27019		1.135		9	f4d	(5I)6G
6.5		27037		0.995		14	f2d2s	(3H)4Ka
1.5		27069		0.490		17	f2d2s	(3F)6Gb
2.5		27161		1.031		5	f4d	(5F)6G
6.5		27170		1.006		6	f4d	(3H)4Ka
4.5		27177		1.117		9	f4d	(5S)6D
3.5		27192		0.990		5	f4d	(5D)4D
4.5		27287		1.014		13	f2d2s	(3F)6H
5.5		27295		1.094		6	f4d	(5I)6G
3.5		27356		1.029		5	f2d2s	(3H)4H2
1.5		27358		1.067		9	f2d2s	(3H)6F
3.5		27382		1.005		4	f2d2s	(3F)6H
2.5		27385		0.982		7	f4d	(5S)6D
4.5		27390		1.060		5	f2d2s	(3G)2G2
2.5		27434		0.998		9	f4d	(3F)2F4
6.5		27439		1.033		17	f2d2s	(3H)4I
4.5		27484		1.089		9	f2d2s	(3F)4H

Table 6. Cont.

<i>J</i>	$E^{exp}$ ( $cm^{-1}$ )	$E^{th}$ ( $cm^{-1}$ )	$\Delta E$ ( $cm^{-1}$ )	$g_L^{th}$	$g_L^{exp}$	% 1 <sup>st</sup> comp	Conf	Term
6.5		27508		1.098		9	f2d2s	(3H)6Ia
1.5		27520		0.933		6	f4d	(3F)6P
9.5		27553		1.178		89	f2d2s	(3H)6L
0.5		27574		1.729		17	f2d2s	(3F)4P
7.5		27597		1.181		15	f4d	(5I)6H
5.5		27618		1.033		9	f2d2s	(3H)6Ib
3.5		27629		1.046		6	f4d	(5F)6D
4.5		27659		0.944		9	f2d2s	(3H)6Ib
2.5		27661		0.922		7	f2d2s	(3H)6Hb
3.5		27737		0.930		9	f2d2s	(3H)4Hb
7.5	27695.597	27788	-92	1.073	1.090	9	f4d	(3H)4Lb

\*: The level at 23241.365  $cm^{-1}$  has a leading component belonging to the  $5f^26d7s^2$  configuration but the dominant configuration is  $5f^26d^27s$ .

**Table 7.** Adopted parameters (in  $cm^{-1}$ ) for even parity configurations  $5f^37s7p$  and  $5f^36d7p$  of U II compared with HFR radial integrals. The scaling factors are  $SF(P) = P_{fit}/P_{HFR}$ . Constraints on some parameters (denoted 'rn' in the 'Unc' columns of standard errors) link parameters of the same 'm' to vary in a constant ratio. The HFR values of  $E_{av}$  parameters are relative to the lowest even configuration  $5f^47s$  taken as zero value.

Param. <i>P</i>	$5f^37s7p$					$5f^36d7p$				
	$P_{fit}$	Cstr.	Unc.	$P_{HFR}$	$\Delta E/SF$	$P_{fit}$	Cstr.	Unc.	$P_{HFR}$	$\Delta E/SF$
$E_{av}$	54614		598	10338	44276	61291		312	17718	43573
$F^2(ff)$	48327	f		70448	0.686	47577	f		69355	0.686
$F^4(ff)$	45655	f		45655	0.691	31003	f		44867	0.691
$F^6(ff)$	22523	f		33367	0.675	22117	f		32766	0.675
$\alpha$	36.5	f				36.5	f			
$\beta$	-600	f				-600	f			
$\gamma$	1500	f				1500	f			
$\zeta_f$	1809	r1	102	1875	0.965	1781	r1	100	1846	0.965
$\zeta_d$						1624	f		1902	0.854
$\zeta_p$	5118	f		4490	1.14	4232	f		3713	1.14
$F^2(fp)$	7201	f		9001	0.80	6461	f		8077	0.80
$F^2(fd)$						20160	f		29007	0.695
$F^4(fd)$						15386	f		15765	0.976
$F^2(dp)$						13971	f		17464	0.80
$G^1(fd)$						11676	f		18742	0.623
$G^3(fd)$						12558	f		13562	0.926
$G^5(fd)$						8692	f		10084	0.862
$G^2(fp)$	2205	f		2205		1552	f		1939	0.8
$G^4(fp)$	1978	f		1978		1382	f		1727	0.8
$G^3(fs)$	2618	f		4328	0.605					
$G^1(dp)$						6543	f		10904	0.6
$G^3(dp)$						4812	f		8019	0.6
$G^1(sp)$	23515	f		26415	0.89					
Configuration Interaction										
$5f^37s7p - 5f^36d7p$										
$R^2(fs, fd)$	-6710	f	-10167	0.66						
$R^3(fs, df)$	-1442	f	-2185	0.66						
$R^2(sp, dp)$	-11708	f	-17742	0.66						
$R^1(sp, pd)$	-10971	f	-16622	0.66						

**Table 8.** Energy levels for even parity configurations  $5f^37s7p$  and  $5f^36d7p$  of U II.  $\Delta E = E^{exp} - E^{th}$ . The percentage, the configuration and the *LS* name of the leading component in the corresponding configuration are given in the last three columns.

<i>J</i>	$E^{exp}$ ( $cm^{-1}$ )	$E^{th}$ ( $cm^{-1}$ )	$\Delta E$ ( $cm^{-1}$ )	$g_L^{th}$	$g_L^{exp}$	% <i>1<sup>st</sup> comp</i>	<i>Conf</i>	<i>Term</i>
4.5	23315.092	22981	333	0.649	0.875	56	$5f^37s7p$	(4I)6I
5.5	24608.168	24608		0.874	0.910	30	$5f^37s7p$	(4I)6I
3.5	24342.199	24688	−345	0.577	0.760	53	$5f^37s7p$	(4I)6I
4.5	25437.162	25193	243	0.887	0.930	15	$5f^37s7p$	(4I)6I
6.5	26191.312	25937	253	0.753	0.890	49	$5f^36d7p$	(4I)6M
5.5		26810		0.733		33	$5f^36d7p$	(4I)6La
5.5		27873		0.834		25	$5f^37s7p$	(4I)6K
4.5		28301		0.729		30	$5f^36d7p$	(4I)4If
5.5	28154.447	28532	−378	0.862	0.890	18	$5f^37s7p$	(4I)6Lb
6.5		28989		1.033		48	$5f^37s7p$	(4I)6K
5.5		29614		0.970		18	$5f^37s7p$	(4I)6K
4.5		29689		0.865		42	$5f^37s7p$	(4I)6I
2.5		30187		0.362		65	$5f^37s7p$	(4I)6H
3.5		30321		0.723		31	$5f^37s7p$	(4I)6H
1.5		30387		0.375		46	$5f^37s7p$	(4F)6G
7.5	30341.673	30527	−185	0.910	1.010	59	$5f^36d7p$	(4I)6M
4.5		30725		0.874		19	$5f^37s7p$	(4I)6H
2.5		31004		0.787		8	$5f^36d7p$	(4I)4Ga
6.5		31106		0.919		36	$5f^36d7p$	(4I)6La
5.5		31210		0.965		15	$5f^37s7p$	(4I)4Ka
3.5		31231		0.705		14	$5f^36d7p$	(4I)6Ia
6.5		31719		1.005		21	$5f^37s7p$	(4I)6I
0.5		31781		0.118		28	$5f^37s7p$	(4F)6F
1.5		32017		1.030		12	$5f^37s7p$	(4F)6F
2.5		32113		0.862		34	$5f^37s7p$	(4F)6G
6.5	32535.021	32250	283	0.940	0.990	29	$5f^36d7p$	(4I)6Lb
5.5		32326		0.930		35	$5f^36d7p$	(4I)6Kb
6.5		32464		1.093		21	$5f^37s7p$	(4I)6H
4.5		32642		0.693		40	$5f^36d7p$	(4I)6Ka
6.5		32856		0.840		27	$5f^36d7p$	(4I)4Ld
7.5		32894		1.139		47	$5f^37s7p$	(4I)6K
3.5		33045		0.673		31	$5f^36d7p$	(4I)4Hf
5.5		33215		0.799		25	$5f^36d7p$	(4I)6Lb
4.5		33289		0.888		11	$5f^37s7p$	(2H)4I2
0.5		33509		0.499		12	$5f^36d7p$	(4F)6F
4.5		33651		0.809		21	$5f^36d7p$	(4I)6Kb
6.5		33806		1.036		21	$5f^37s7p$	(4I)4Ka
2.5		33859		1.057		10	$5f^37s7p$	(4F)6G
5.5		33985		1.026		22	$5f^37s7p$	(4I)4Ia
5.5	34207.000	34347		0.837		15	$5f^36d7p$	(4I)6La
3.5		34351		0.951		22	$5f^37s7p$	(4F)6G
6.5		34409		0.936		11	$5f^36d7p$	(4I)4Lc
5.5		34427		1.048		12	$5f^37s7p$	(4I)6I
2.5		34433		0.540		26	$5f^37s7p$	(4C)6H
1.5		34435		0.866		14	$5f^37s7p$	(4C)6G
3.5		34466		0.698		25	$5f^36d7p$	(4I)6I
4.5		34496		0.920		11	$5f^36d7p$	(4I)6Ia
7.5		34524		0.959		17	$5f^36d7p$	(4I)4Mb
4.5		34560		0.990		14	$5f^37s7p$	(4I)6H
3.5		34761		0.935		17	$5f^37s7p$	(4F)6G
1.5		34812		1.605		42	$5f^37s7p$	(4S)6P
8.5	34632.367	34911	−279	1.024	1.085	60	$5f^36d7p$	(4I)6M

Table 8. Cont.

<i>J</i>	$E^{exp}$ ( $cm^{-1}$ )	$E^{th}$ ( $cm^{-1}$ )	$\Delta E$ ( $cm^{-1}$ )	$g_L^{th}$	$g_L^{exp}$	% 1 <sup>st</sup> comp	Conf	Term
2.5		35093		0.837		17	$5f^3 7s 7p$	(4F)4Ga
3.5		35149		0.908		9	$5f^3 7s 7p$	(4I)6H
7.5		35301		1.085		17	$5f^3 6d 7p$	(4I)6I
4.5		35338		0.895		10	$5f^3 6d 7p$	(4I)6K
2.5		35498		1.074		17	$5f^3 7s 7p$	(4F)6F
6.5		35514		0.990		31	$5f^3 6d 7p$	(4I)6Kb
7.5		35529		1.051		27	$5f^3 6d 7p$	(4I)6La
3.5		35552		0.873		12	$5f^3 6d 7p$	(4I)6H
3.5		35666		0.834		6	$5f^3 6d 7p$	(4I)6H
4.5		35696		0.811		13	$5f^3 6d 7p$	(4I)6H
5.5		35744		0.966		19	$5f^3 7s 7p$	(4I)2I
4.5		35780		0.867		11	$5f^3 6d 7p$	(4I)4Ia
5.5		35804		0.901		14	$5f^3 6d 7p$	(4I)4Ke
6.5		35809		1.064		30	$5f^3 7s 7p$	(4I)2K
7.5		35892		1.196		34	$5f^3 7s 7p$	(4I)6H
3.5		35906		1.009		9	$5f^3 6d 7p$	(4F)6G
5.5		35985		0.961		13	$5f^3 6d 7p$	(4I)6Ka
1.5		36046		0.867		14	$5f^3 7s 7p$	(4F)6F
3.5		36064		1.089		10	$5f^3 7s 7p$	(4F)6D
4.5		36137		0.865		10	$5f^3 6d 7p$	(4I)6Ib
2.5		36149		1.444		33	$5f^3 7s 7p$	(4S)6P
8.5		36364		1.210		31	$5f^3 7s 7p$	(4I)6I
7.5		36389		1.059		29	$5f^3 6d 7p$	(4I)6Ib
6.5		36410		1.019		14	$5f^3 6d 7p$	(4I)6I
2.5		36417		0.607		17	$5f^3 6d 7p$	(4F)6Ha
1.5		36462		1.200		14	$5f^3 7s 7p$	(4S)2P
5.5		36516		0.934		39	$5f^3 6d 7p$	(4I)6Ka
0.5		36680		1.812		15	$5f^3 6d 7p$	(4S)4Pa
3.5		36721		0.935		9	$5f^3 7s 7p$	(4F)6I
4.5		36849		0.904		18	$5f^3 6d 7p$	(4I)4Hf
2.5		36946		1.020		5	$5f^3 6d 7p$	(4F)4Fa
4.5		37004		1.163		34	$5f^3 7s 7p$	(4F)6G
3.5		37008		0.949		10	$5f^3 6d 7p$	(4I)6Ia
1.5		37053		0.995		12	$5f^3 6d 7p$	(4I)6Ga
0.5		37112		2.063		27	$5f^3 7s 7p$	(4F)6D
2.5		37313		0.864		6	$5f^3 6d 7p$	(4I)6Ga
3.5		37369		0.935		16	$5f^3 7s 7p$	(4C)6H
2.5		37477		0.897		13	$5f^3 6d 7p$	(4C)6H
1.5		37537		0.695		14	$5f^3 6d 7p$	(4F)4Ff
7.5		37620		1.065		13	$5f^3 7s 7p$	(4I)4Ka
6.5		37789		1.127		26	$5f^3 7s 7p$	(4I)4Ha
3.5		37822		0.986		8	$5f^3 7s 7p$	(4F)4Ca
1.5		37855		1.172		15	$5f^3 6d 7p$	(4F)6F
5.5		37879		0.929		11	$5f^3 6d 7p$	(4I)6Kb
7.5		37917		0.996		18	$5f^3 6d 7p$	(4I)4Mb
2.5		37960		0.861		9	$5f^3 6d 7p$	(4C)6H
8.5	37308.326	37991	-683	1.062	1.070	18	$5f^3 6d 7p$	(4I)6M
4.5		38040		0.895		18	$5f^3 6d 7p$	(4I)6I
3.5		38063		0.821		10	$5f^3 6d 7p$	(4F)6I
1.5		38080		0.578		23	$5f^3 6d 7p$	(4C)6G
6.5		38156		0.931		15	$5f^3 6d 7p$	(4I)4Ld
5.5		38183		0.896		13	$5f^3 6d 7p$	(4I)6K
4.5		38205		0.863		12	$5f^3 6d 7p$	(4I)6I
2.5		38217		0.816		9	$5f^3 6d 7p$	(4I)6Hb
0.5		38228		2.117		26	$5f^3 7s 7p$	(4F)6D

Table 8. Cont.

<i>J</i>	$E^{exp}$ ( $cm^{-1}$ )	$E^{th}$ ( $cm^{-1}$ )	$\Delta E$ ( $cm^{-1}$ )	$g_L^{th}$	$g_L^{exp}$	% 1 <sup>st</sup> comp	Conf	Term
3.5		38436		0.941		9	$5f^3 6d7p$	(4F)4Hd
2.5		38452		0.879		17	$5f^3 7s7p$	(4G)2F
7.5		38497		1.029		25	$5f^3 6d7p$	(4I)4Lc
2.5		38554		0.760		11	$5f^3 6d7p$	(4I)6Gb
4.5		38630		1.028		10	$5f^3 6d7p$	(4G)6H
6.5		38721		0.974		15	$5f^3 6d7p$	(4I)6Kb
1.5		38794		1.134		8	$5f^3 6d7p$	(4F)6D
5.5		38809		0.916		22	$5f^3 6d7p$	(4I)6K
8.5		38835		1.187		29	$5f^3 7s7p$	(4I)6K
2.5		38916		1.074		12	$5f^3 6d7p$	(4F)6F
4.5		38931		1.064		7	$5f^3 6d7p$	(4I)6I
4.5		38975		0.830		20	$5f^3 6d7p$	(4G)6K
3.5		38993		0.936		8	$5f^3 7s7p$	(4I)4Ha
2.5		39000		0.891		14	$5f^3 7s7p$	(4G)6G
1.5		39006		0.407		30	$5f^3 6d7p$	(4I)6Gb
9.5	39809.365	39050	758	1.111	1.105	48	$5f^3 6d7p$	(4I)6M
5.5		39065		1.092		5	$5f^3 6d7p$	(4I)6Kb
6.5		39122		1.038		14	$5f^3 6d7p$	(4I)6Ka
4.5		39161		1.136		14	$5f^3 6d7p$	(4F)6D

### 3.3. Partition Function

To get an idea of how semi-empirical parametric calculations could influence the value of the partition function  $Q(T) = \sum_i (2J_i + 1) \exp(-E_i/k_B T)$  ( $k_B$ : Boltzmann constant), we made an estimation of the partition function of U II for a typical stellar temperature. The temperature chosen is 4825 K ( $k_B T = 3353.54 \text{ cm}^{-1}$ ), which is the temperature quoted by Cayrel et al. [1] for a metal-poor star showing the U II line at 3859.57 Å in its spectrum.

Since experimental levels are incompletely determined, a partition function calculated with only known experimental energies would be underestimated. Therefore we calculated the partition function with all the available experimental energies supplemented by the final least squares fitted energies when experimental ones are missing. In the expression of the partition function we included all the levels below  $46\,000 \text{ cm}^{-1}$  of both parities. The result is:  $Q_{exp/LSF}(T) = 122.99$ , which is the best value possible in the present case. When the partition function is calculated with the same number of levels, but with all the fitted energies, the result is:  $Q_{LSF}(T) = 120.99$ , which agrees with  $Q_{exp/LSF}(T)$  within 2%. When *ab initio* HFR energy values are used, we have  $Q_{HFR}(T) = 89.19$ , which is 26% smaller. Consequently, in absence of complete experimental level energies, the energies calculated from fitted parameters provide a realistic estimation of the partition function.

### 3.4. Transition Probabilities

The parametric calculations provide  $gA$  values for transition probabilities ( $g$ : upper level statistical weight;  $A$ : Einstein coefficient of spontaneous emission) between calculated levels. Extensive comparison with experimental transition probabilities is not possible because of the scarcity of measurements. Furthermore, because of the strongly mixed wave functions, weak transitions are sensitive to small changes of energy parameters and may not be reliable for comparison. Nevertheless, it is interesting to consider the line at 3859.6 Å, which is strong and used as cosmochronometer [1]. Chen and Borzileri [21] measured the  $gA$  value for this line and found  $2.8 \times 10^8 \text{ s}^{-1}$ , to be compared with previous measurement  $1.1 \times 10^8 \text{ s}^{-1}$  by Corliss [22]. Nilsson et al. [23] derived branching ratios from relative intensities measured in FTS spectra and combined with radiative lifetime of the upper level at  $26191 \text{ cm}^{-1}$  to find a  $g_{if}$  value of 0.856 for the oscillator strength weighted by the lower level degeneracy. The corresponding  $gA$  value (Equation (1) of [23]) is  $3.8 \times 10^8 \text{ s}^{-1}$  in agreement with the

value of  $3.5 \times 10^8 \text{ s}^{-1}$  calculated by Kurucz [24]. Our calculations lead to  $gA = 1.53 \times 10^9 \text{ s}^{-1}$ , four times larger, but they confirm the order of magnitude. However, the parametric study for the high even levels of  $5f^37s7p + 5f^36d7p$  is still unachieved, since treated without all the interacting even configurations. Its results should be taken with caution.

#### 4. Classified Lines of U II in the Ultraviolet

On our spectrograms described in Section 2, some lines were relatively sharp and were likely emitted by singly charged uranium ions. For identification of U II lines, we searched experimental wave numbers matching the Ritz wave numbers calculated from the energy differences of known U II energy levels reported in [6], even when the level was not assigned with quantum numbers. The maximum uncertainty of the wavelength measurements is estimated to be  $\pm 0.003 \text{ \AA}$ . Thus the corresponding uncertainty on wave numbers should be less than  $\pm 0.05 \text{ cm}^{-1}$ . To take into account any possible perturbations in the spark spectrum, we chose a tolerance of  $\pm 0.1 \text{ cm}^{-1}$  for a criterion of identification. Indeed, according to [14], the level energies in [6], therefore the Ritz wave numbers, have negligible uncertainties of about  $\pm 0.01 \text{ cm}^{-1}$ . Table 9 lists the 451 lines between 2344 and 2955 Å identified as U II transitions, with calculated Ritz wavelengths, experimental wavelengths, deviations exp-Ritz and line intensities, together with the corresponding upper and lower levels. One line has triple identification and 24 lines have double identification. These concern mostly lines with two deviations of opposite signs. Otherwise, the line with the smallest deviation is retained. No  $gA$  values were available here for confirmation of identifications since the even levels involved in these transitions have only experimental energy values but no quantum numbers assigned except the  $J$  values.

Search of new levels of  $5f^36d7p$  close to the predicted energies of Table 8 was attempted using the possible U II lines left unidentified. Unfortunately, only one chain of transitions supported by calculated transition probabilities could be found leading to a level  $5f^36d7p (^4I)^6K$  with  $J = 5.5$  at  $39113.98 \pm 0.1 \text{ cm}^{-1}$ . Table 10 lists the six transitions that establish this level.

**Table 9.** Ultraviolet transitions of U II emitted from a vacuum spark source.  $wl_{Ritz}$ : Ritz wavelength calculated with experimental energies from [6];  $wl_{exp}$ : experimental wavelength;  $\Delta wl = wl_{exp} - wl_{Ritz}$ ;  $w_{n_{exp}}$ : experimental wavenumbers;  $\Delta wn = wn_{exp} - (E_{even} - E_{odd})$ .

$wl_{Ritz}$ in Air (Å)	$wl_{exp}$ in Air (Å)	Int	Note	$w_{n_{exp}}$ ( $\text{cm}^{-1}$ )	$\Delta wl$ (Å)	$\Delta wn$ ( $\text{cm}^{-1}$ )	$E_{odd}$ ( $\text{cm}^{-1}$ )	$J_{odd}$	$E_{even}$ ( $\text{cm}^{-1}$ )	Jeven
2343.5696	2343.5707	49		42656.867	0.0012	-0.021	0.000	4.5	42656.888	5.5
2348.8952	2348.8968	73		42560.149	0.0016	-0.029	289.041	5.5	42849.219	5.5
2390.9748	2390.9742	10		41811.216	-0.0006	0.011	0.000	4.5	41811.205	5.5
2401.1302	2401.1330	125		41634.329	0.0029	-0.050	289.041	5.5	41923.420	6.5
2423.7052	2423.7102	52		41246.529	0.0051	-0.086	0.000	4.5	41246.615	4.5
2427.0021	2427.0022	43		41190.593	0.0001	-0.001	914.765	4.5	42105.359	5.5
2448.0954	2448.0942	97		40835.731	-0.0012	0.020	289.041	5.5	41124.752	6.5
2448.9324	2448.9265	7		40821.854	-0.0059	0.099	0.000	4.5	40821.755	4.5
2471.0901	2471.0868	55		40455.794	-0.0033	0.054	2294.696	5.5	42750.436	6.5
2477.1835	2477.1824	30		40356.253	-0.0010	0.017	1749.123	6.5	42105.359	5.5
2478.6816	2478.6852	37	as	40331.791	0.0036	-0.059	914.765	4.5	41246.615	4.5
2481.1377	2481.1412	24		40291.868	0.0034	-0.056	289.041	5.5	40580.965	5.5
2484.0042	2484.0095	16		40245.347	0.0054	-0.087	0.000	4.5	40245.434	3.5
2484.6702	2484.6667	41		40234.703	-0.0035	0.057	0.000	4.5	40234.646	5.5
2490.2907	2490.2899	9		40143.856	-0.0009	0.014	914.765	4.5	41058.607	5.5
2491.4292	2491.4330	8		40125.442	0.0037	-0.060	1749.123	6.5	41874.625	6.5
2506.8037	2506.8012	25		39879.462	-0.0025	0.039	914.765	4.5	40794.188	4.5
2512.5746	2512.5784	13		39787.777	0.0038	-0.060	0.000	4.5	39787.837	5.5
2514.7696	2514.7686	19	LA	39753.125	-0.0010	0.016	4420.871	5.5	44173.980	6.5
2518.9755	2518.9760	37		39686.730	0.0005	-0.008	0.000	4.5	39686.738	5.5
2533.2401	2533.2370	42		39463.326	-0.0031	0.049	0.000	4.5	39463.277	5.5
2537.6966	2537.6954	163		39393.998	-0.0012	0.018	289.041	5.5	39683.021	5.5
2538.4329	2538.4355	85		39382.517	0.0026	-0.041	0.000	4.5	39382.558	3.5
2538.7351	2538.7384	33		39377.819	0.0033	-0.051	289.041	5.5	39666.911	4.5
2539.1756	2539.1760	96	as	39371.032	0.0004	-0.006	289.041	5.5	39660.079	6.5
2540.7030	2540.7065	39	c	39347.316	0.0034	-0.053	1749.123	6.5	41096.492	6.5
2541.3669	2541.3655	39	c	39337.112	-0.0014	0.022	0.000	4.5	39337.090	4.5
2554.3761	2554.3725	134	as	39136.819	-0.0035	0.054	1749.123	6.5	40885.888	6.5

Table 9. Cont.

$wl_{Ritz}$ in Air (Å)	$wl_{exp}$ in Air (Å)	Int	Note	$wn_{exp}$ ( $cm^{-1}$ )	$\Delta wl$ (Å)	$\Delta wn$ ( $cm^{-1}$ )	$E_{odd}$ ( $cm^{-1}$ )	$J_{odd}$	Even ( $cm^{-1}$ )	Jeven
2556.1928	2556.1946	82	LA	39108.922	0.0018	-0.028	0.000	4.5	39108.950	5.5
2560.1798	2560.1743	20		39048.133	-0.0055	0.084	289.041	5.5	39337.090	4.5
2560.3421	2560.3457	29		39045.519	0.0037	-0.056	0.000	4.5	39045.575	4.5
2561.7992	2561.7934	46		39023.455	-0.0058	0.089	914.765	4.5	39938.131	5.5
2565.4072	2565.4130	104	LA	38968.400	0.0058	-0.088	0.000	4.5	38968.488	5.5
2567.2954	2567.2987	174	as	38939.778	0.0032	-0.049	2294.696	5.5	41234.523	6.5
2567.9515	2567.9578	11		38929.783	0.0063	-0.095	0.000	4.5	38929.878	4.5
2568.9777	2568.9783	26	LA,as	38914.318	0.0006	-0.009	5259.653	7.5	44173.980	6.5
2569.7085	2569.7095	45	LA	38903.246	0.0010	-0.015	0.000	4.5	38903.261	3.5
2575.2266	2575.2291	23	LA	38819.872	0.0025	-0.037	289.041	5.5	39108.950	5.5
2577.3205	2577.3219	20		38788.354	0.0015	-0.022	0.000	4.5	38788.376	4.5
2578.7860	2578.7797	155		38766.427	-0.0063	0.095	1749.123	6.5	40515.455	5.5
2579.5692	2579.5681	29		38754.579	-0.0011	0.017	0.000	4.5	38754.562	4.5
2584.4158	2584.4163	42	LA	38681.882	0.0005	-0.008	0.000	4.5	38681.890	3.5
2584.9012	2584.9028	10	c	38674.602	0.0016	-0.024	0.000	4.5	38674.626	4.5
2586.1972	2586.1965	44		38655.256	-0.0007	0.010	4420.871	5.5	43076.117	4.5
2591.2483	2591.2450	107	as	38579.949	-0.0034	0.050	0.000	4.5	38579.899	4.5
2592.5704	2592.5690	60		38560.247	-0.0014	0.021	0.000	4.5	38560.226	3.5
2593.5699	2593.5698	30		38545.372	-0.0001	0.002	0.000	4.5	38545.370	5.5
2601.4681	2601.4695	72		38428.328	0.0014	-0.020	4420.871	5.5	42849.219	5.5
2604.2985	2604.2993	48	p	38386.572	0.0008	-0.012	0.000	4.5	38386.584	3.5
2606.7253	2606.7266	63		38350.837	0.0013	-0.019	0.000	4.5	38350.856	4.5
2607.3014	2607.3069	65		38342.302	0.0055	-0.081	289.041	5.5	38631.424	5.5
2608.1733	2608.1800	28	p	38329.466	0.0067	-0.099	4420.871	5.5	42750.436	6.5
2609.2426	2609.2457	23		38313.811	0.0031	-0.046	0.000	4.5	38313.857	5.5
2609.8933	2609.8900	253		38304.353	-0.0033	0.049	914.765	4.5	39219.069	5.5
2612.4565	2612.4555	11		38266.741	-0.0010	0.015	0.000	4.5	38266.726	4.5
2613.9584	2613.9578	11		38244.748	-0.0005	0.008	0.000	4.5	38244.740	3.5
2615.9468	2615.9422	24		38215.737	-0.0046	0.067	0.000	4.5	38215.670	4.5
2616.0690	2616.0679	35		38213.901	-0.0012	0.017	0.000	4.5	38213.884	5.5
2620.8611	2620.8670	19		38143.931	0.0059	-0.086	914.765	4.5	39058.782	5.5
2621.4511	2621.4463	21		38135.502	-0.0048	0.070	1749.123	6.5	39884.555	6.5
2623.5499	2623.5514	17		38104.907	0.0015	-0.022	4420.871	5.5	42525.800	5.5
2624.9155	2624.9101	24		38085.183	-0.0054	0.078	4420.871	5.5	42505.976	6.5
2625.2536	2625.2508	21		38080.241	-0.0028	0.041	0.000	4.5	38080.200	5.5
2628.9275	2628.9276	41		38026.982	0.0001	-0.002	0.000	4.5	38026.984	4.5
2632.6555	2632.6570	32		37973.118	0.0015	-0.021	0.000	4.5	37973.139	5.5
2632.9771	2632.9786	42		37968.480	0.0015	-0.021	0.000	4.5	37968.501	4.5
2634.3223	2634.3286	35		37949.022	0.0063	-0.091	2294.696	5.5	40243.809	6.5
2635.1207	2635.1213	26		37937.607	0.0006	-0.008	1749.123	6.5	39686.738	5.5
2635.3792	2635.3781	69	as	37933.914	-0.0011	0.016	1749.123	6.5	39683.021	5.5
2635.5278	2635.5306	102		37931.719	0.0028	-0.041	0.000	4.5	37931.760	4.5
2637.6935	2637.6967	15		37900.569	0.0032	-0.046	4420.871	5.5	42321.486	6.5
2639.5742	2639.5720	20	p	37873.643	-0.0022	0.032	914.765	4.5	38788.376	4.5
2639.8350	2639.8351	26	p	37869.868	0.0001	-0.001	0.000	4.5	37869.869	5.5
2641.5456	2641.5488	20		37845.305	0.0031	-0.045	0.000	4.5	37845.350	3.5
2641.9333	2641.9291	8	p	37839.856	-0.0041	0.059	914.765	4.5	38754.562	4.5
2644.1238	2644.1281	20		37808.391	0.0043	-0.062	0.000	4.5	37808.453	5.5
2645.4716	2645.4749	78	LA	37789.143	0.0033	-0.047	0.000	4.5	37789.190	4.5
2648.7844	2648.7857	9		37741.914	0.0013	-0.018	0.000	4.5	37741.932	4.5
2649.0644	2649.0686	68		37737.884	0.0041	-0.059	289.041	5.5	38026.984	4.5
2650.7354	2650.7392	2		37714.100	0.0038	-0.054	1749.123	6.5	39463.277	5.5
2652.1885	2652.1883	29		37693.494	-0.0003	0.004	1749.123	6.5	39442.613	7.5
2652.8221	2652.8233	83		37684.471	0.0012	-0.017	4420.871	5.5	42105.359	5.5
2656.5889	2656.5910	172		37631.029	0.0021	-0.030	914.765	4.5	38545.824	3.5
2660.1401	2660.1369	20		37580.873	-0.0032	0.045	289.041	5.5	37869.869	5.5
2662.8483	2662.8539	21		37542.527	0.0057	-0.080	4420.871	5.5	41963.478	4.5
2663.2920	2663.2908	4		37536.369	-0.0012	0.017	5526.750	6.5	43063.102	6.5
2664.1581	2664.1519	11	p	37524.237	-0.0062	0.088	4420.871	5.5	41945.020	6.5
2664.4580	2664.4578	23	p	37519.928	-0.0002	0.003	4585.434	6.5	42105.359	5.5
2665.6926	2665.6909	36		37502.572	-0.0016	0.023	4420.871	5.5	41923.420	6.5
2665.8632	2665.8615	6	LA	37500.173	-0.0017	0.024	289.041	5.5	37789.190	4.5
2666.5295	2666.5315	14		37490.754	0.0021	-0.029	5259.653	7.5	42750.436	6.5
2667.8790	2667.8833	25	b,	37471.758	0.0043	-0.061	914.765	4.5	38386.584	3.5
2668.0123	2668.0134	7		37469.931	0.0011	-0.015	1749.123	6.5	39219.069	5.5
2669.1658	2669.1602	28		37453.832	-0.0056	0.078	4420.871	5.5	41874.625	6.5
2669.2273	2669.2230	28		37452.951	-0.0043	0.060	289.041	5.5	37741.932	4.5
2670.5030	2670.5089	49		37434.916	0.0059	-0.083	2294.696	5.5	39729.695	6.5
2672.2712	2672.2736	11		37410.195	0.0024	-0.034	289.041	5.5	37699.270	5.5
2672.4852	2672.4830	182		37407.265	-0.0022	0.031	5259.653	7.5	42666.887	7.5



Table 9. Cont.

$wl_{Ritz}$ in Air (Å)	$wl_{exp}$ in Air (Å)	Int	Note	$wl_{exp}$ ( $cm^{-1}$ )	$\Delta wl$ (Å)	$\Delta wn$ ( $cm^{-1}$ )	$E_{odd}$ ( $cm^{-1}$ )	$J_{odd}$	Even ( $cm^{-1}$ )	Jeven
2672.7077	2672.7030	72		37404.185	-0.0047	0.066	0.000	4.5	37404.119	5.5
2675.1142	2675.1087	37		37370.552	-0.0054	0.076	289.041	5.5	37659.517	4.5
2675.8767	2675.8790	35	LA	37359.794	0.0024	-0.033	1749.123	6.5	39108.950	5.5
2676.4154	2676.4115	187	LA	37352.362	-0.0039	0.055	6283.431	6.5	43635.738	6.5
2676.6836	2676.6849	11		37348.546	0.0014	-0.019	1749.123	6.5	39097.688	6.5
2677.4419	2677.4355	23	p	37338.076	-0.0065	0.090	4585.434	6.5	41923.420	6.5
2678.7931	2678.7924	72	p	37319.163	-0.0007	0.010	4585.434	6.5	41904.587	5.5
2683.2766	2683.2723	55		37256.861	-0.0043	0.060	1749.123	6.5	39005.924	5.5
2683.4216	2683.4147	4	c	37254.884	-0.0070	0.097	289.041	5.5	37543.828	4.5
2683.4719	2683.4724	12	c	37254.083	0.0004	-0.006	289.041	5.5	37543.130	5.5
2684.0314	2684.0318	24	as	37246.318	0.0004	-0.005	5259.653	7.5	42505.976	6.5
2685.9761	2685.9705	10	LA,p	37219.443	-0.0056	0.078	1749.123	6.5	38968.488	5.5
2689.1080	2689.1152	13	D	37175.918	0.0072	-0.099	0.000	4.5	37176.017	4.5
2689.1195	2689.1152	13	D	37175.918	-0.0043	0.059	289.041	5.5	37464.900	6.5
2689.6460	2689.6496	8		37168.531	0.0036	-0.050	2294.696	5.5	39463.277	5.5
2691.0334	2691.0336	219	p	37149.415	0.0003	-0.004	4420.871	5.5	41570.290	5.5
2693.7311	2693.7346	55	as	37112.170	0.0036	-0.049	914.765	4.5	38026.984	4.5
2697.3932	2697.3884	20		37061.899	-0.0048	0.066	5259.653	7.5	42321.486	6.5
2697.9173	2697.9129	24	p	37054.694	-0.0044	0.060	1749.123	6.5	38803.757	7.5
2698.4845	2698.4782	148		37046.932	-0.0063	0.087	4585.434	6.5	41632.279	6.5
2700.2512	2700.2548	12	as	37022.562	0.0036	-0.049	4420.871	5.5	41443.482	6.5
2705.7866	2705.7917	13		36946.806	0.0051	-0.070	1749.123	6.5	38695.999	5.5
2706.9739	2706.9728	63		36930.686	-0.0012	0.016	8276.733	6.5	45207.403	7.5
2708.9821	2708.9885	66		36903.206	0.0064	-0.087	4585.434	6.5	41488.727	5.5
2709.5050	2709.5064	30	LA,p	36896.153	0.0013	-0.018	4420.871	5.5	41317.042	5.5
2709.5564	2709.5498	77		36895.562	-0.0066	0.090	0.000	4.5	36895.472	4.5
2711.1029	2711.0998	13	LA,as	36874.468	-0.0032	0.043	914.765	4.5	37789.190	4.5
2711.7043	2711.7061	7		36866.223	0.0018	-0.024	5790.641	5.5	42656.888	5.5
2711.7820	2711.7807	22	b	36865.209	-0.0013	0.018	0.000	4.5	36865.191	5.5
2712.0582	2712.0588	8		36861.429	0.0005	-0.007	4420.871	5.5	41282.307	6.5
2714.5822	2714.5861	7		36827.115	0.0038	-0.052	914.765	4.5	37741.932	4.5
2715.5344	2715.5334	5		36814.267	-0.0010	0.013	2294.696	5.5	39108.950	5.5
2716.4220	2716.4269	9		36802.158	0.0049	-0.067	289.041	5.5	37091.266	4.5
2716.8633	2716.8693	9		36796.166	0.0060	-0.081	1749.123	6.5	38545.370	5.5
2718.0425	2718.0410	39		36780.304	-0.0015	0.020	1749.123	6.5	38529.407	7.5
2718.0444	2718.0410	39		36780.304	-0.0035	0.047	5259.653	7.5	42039.910	7.5
2719.3675	2719.3687	21		36762.350	0.0013	-0.017	1749.123	6.5	38511.490	5.5
2723.1625	2723.1671	139		36711.073	0.0046	-0.062	1749.123	6.5	38460.258	6.5
2725.0668	2725.0738	4	D,c	36685.386	0.0071	-0.095	8521.922	7.5	45207.403	7.5
2725.0752	2725.0738	4	D,c	36685.386	-0.0014	0.019	5259.653	7.5	41945.020	6.5
2725.2686	2725.2662	137	as	36682.796	-0.0024	0.032	6283.431	6.5	42966.195	7.5
2726.6810	2726.6841	27		36663.725	0.0031	-0.042	5259.653	7.5	41923.420	6.5
2727.7730	2727.7792	77	as	36649.007	0.0061	-0.082	4585.434	6.5	41234.523	6.5
2728.4664	2728.4701	7		36639.726	0.0037	-0.050	289.041	5.5	36928.817	4.5
2728.6183	2728.6233	8		36637.669	0.0050	-0.067	4420.871	5.5	41058.607	5.5
2733.9627	2733.9667	45		36566.071	0.0040	-0.054	289.041	5.5	36855.166	4.5
2734.0667	2734.0715	7		36564.670	0.0048	-0.064	1749.123	6.5	38313.857	5.5
2734.2730	2734.2762	285		36561.932	0.0032	-0.043	5401.503	3.5	41963.478	4.5
2735.5783	2735.5728	22	p	36544.602	-0.0055	0.073	4420.871	5.5	40965.400	6.5
2738.9799	2738.9848	35		36499.079	0.0049	-0.065	2294.696	5.5	38793.840	6.5
2739.3900	2739.3921	20	D	36493.652	0.0021	-0.028	2294.696	5.5	38788.376	4.5
2739.3906	2739.3921	20	D,LA	36493.652	0.0015	-0.020	289.041	5.5	36782.713	6.5
2740.6331	2740.6355	6		36477.099	0.0024	-0.032	289.041	5.5	36766.172	5.5
2740.8273	2740.8282	18		36474.534	0.0010	-0.013	289.041	5.5	36763.588	4.5
2740.9305	2740.9325	9		36473.146	0.0020	-0.027	4585.434	6.5	41058.607	5.5
2741.7458	2741.7506	24		36462.264	0.0047	-0.063	914.765	4.5	37377.092	4.5
2742.0571	2742.0563	15		36458.198	-0.0008	0.010	5259.653	7.5	41717.841	7.5
2744.4027	2744.3996	25		36427.069	-0.0032	0.042	914.765	4.5	37341.792	4.5
2745.0627	2745.0659	7		36418.227	0.0032	-0.043	5526.750	6.5	41945.020	6.5
2746.1590	2746.1557	12		36403.775	-0.0033	0.044	1749.123	6.5	38152.854	7.5
2746.6917	2746.6870	179		36396.733	-0.0048	0.063	5526.750	6.5	41923.420	6.5
2747.3598	2747.3547	23		36387.891	-0.0051	0.067	0.000	4.5	36387.824	3.5
2748.4450	2748.4475	7		36373.424	0.0025	-0.033	6283.431	6.5	42656.888	5.5
2748.5078	2748.5044	17		36372.671	-0.0034	0.045	5259.653	7.5	41632.279	6.5
2749.9421	2749.9398	37		36353.685	-0.0023	0.030	8853.748	8.5	45207.403	7.5
2750.3794	2750.3750	15		36347.933	-0.0044	0.058	5526.750	6.5	41874.625	6.5
2750.5536	2750.5520	7		36345.594	-0.0017	0.022	8276.733	6.5	44622.305	7.5

Table 9. Cont.

$wl_{Ritz}$ in Air (Å)	$wl_{exp}$ in Air (Å)	Int	Note	$wl_{exp}$ ( $cm^{-1}$ )	$\Delta wl$ (Å)	$\Delta wl_{int}$ ( $cm^{-1}$ )	$F_{odd}$ ( $cm^{-1}$ )	$J_{odd}$	Even ( $cm^{-1}$ )	Jeven
2751.2231	2751.2161	21		36336.820	-0.0070	0.092	2294.696	5.5	38631.424	5.5
2752.4357	2752.4349	13		36320.730	-0.0008	0.011	1749.123	6.5	38069.842	5.5
2754.1493	2754.1480	80		36298.143	-0.0013	0.017	914.765	4.5	37212.891	3.5
2756.8379	2756.8307	22		36262.821	-0.0072	0.095	289.041	5.5	36551.767	5.5
2756.9499	2756.9462	9	c	36261.301	-0.0037	0.049	914.765	4.5	37176.017	4.5
2757.5498	2757.5455	32		36253.420	-0.0043	0.056	0.000	4.5	36253.364	5.5
2758.9517	2758.9473	10	as	36235.000	-0.0043	0.057	914.765	4.5	37149.708	4.5
2759.7839	2759.7817	24		36224.045	-0.0022	0.029	1749.123	6.5	37973.139	5.5
2762.7151	2762.7167	12		36185.566	0.0017	-0.022	1749.123	6.5	37934.711	7.5
2762.8494	2762.8471	18		36183.858	-0.0022	0.029	5259.653	7.5	41443.482	6.5
2762.8797	2762.8769	38		36183.468	-0.0028	0.037	0.000	4.5	36183.431	5.5
2763.4090	2763.4131	29		36176.447	0.0041	-0.054	914.765	4.5	37091.266	4.5
2763.6889	2763.6843	14		36172.897	-0.0046	0.060	5790.641	5.5	41963.478	4.5
2764.2397	2764.2400	20	D	36165.625	0.0003	-0.004	5526.750	6.5	41692.379	5.5
2764.2449	2764.2400	20	D	36165.625	-0.0048	0.063	2294.696	5.5	38460.258	6.5
2764.6629	2764.6561	56		36160.182	-0.0067	0.088	4420.871	5.5	40580.965	5.5
2765.3970	2765.3989	49		36150.470	0.0019	-0.025	0.000	4.5	36150.495	3.5
2766.7528	2766.7518	13		36132.792	-0.0010	0.013	5790.641	5.5	41923.420	5.5
2766.8721	2766.8729	28	as	36131.211	0.0008	-0.010	0.000	4.5	36131.221	6.5
2767.6745	2767.6669	314		36120.845	-0.0076	0.099	1749.123	6.5	37869.869	5.5
2768.8587	2768.8516	37		36105.395	-0.0071	0.093	1749.123	6.5	37854.425	5.5
2770.0418	2770.0399	34		36089.906	-0.0019	0.025	0.000	4.5	36089.881	3.5
2770.7417	2770.7376	65		36080.819	-0.0041	0.054	6445.035	4.5	42525.800	5.5
2772.1759	2772.1743	9		36062.120	-0.0016	0.021	4420.871	5.5	40482.970	5.5
2772.3887	2772.3910	9		36059.300	0.0023	-0.030	1749.123	6.5	37808.453	5.5
2772.6325	2772.6313	38		36056.175	-0.0012	0.015	2294.696	5.5	38350.856	4.5
2773.6033	2773.6039	29		36043.532	0.0006	-0.008	5526.750	6.5	41570.290	5.5
2775.0145	2775.0118	6		36025.245	-0.0027	0.035	5526.750	6.5	41551.960	5.5
2775.2114	2775.2079	7		36022.699	-0.0035	0.045	5259.653	7.5	41282.307	6.5
2775.3724	2775.3675	5		36020.628	-0.0049	0.064	5790.641	5.5	41811.205	5.5
2775.8213	2775.8148	11		36014.828	-0.0066	0.085	4420.871	5.5	40435.614	6.5
2776.8169	2776.8205	7		36001.784	0.0036	-0.047	1749.123	6.5	37750.954	5.5
2778.4471	2778.4532	12	p	35980.629	0.0060	-0.078	914.765	4.5	36895.472	4.5
2779.4472	2779.4478	2	D	35967.757	0.0006	-0.008	1749.123	6.5	37716.888	7.5
2779.4508	2779.4478	2	D	35967.757	-0.0029	0.038	1749.123	6.5	37716.842	6.5
2780.0321	2780.0339	11	LA	35960.175	0.0018	-0.023	0.000	4.5	35960.198	4.5
2781.0310	2781.0317	9		35947.273	0.0007	-0.009	289.041	5.5	36236.323	4.5
2781.5634	2781.5684	21		35940.336	0.0050	-0.065	914.765	4.5	36855.166	4.5
2782.0684	2782.0730	5		35933.818	0.0046	-0.059	44357.295	4.5	8423.418	4.5
2783.2065	2783.2076	12		35919.174	0.0011	-0.014	2294.696	5.5	38213.884	5.5
2783.2899	2783.2969	3		35918.021	0.0070	-0.090	0.000	4.5	35918.111	5.5
2783.3968	2783.4034	41	?	35916.647	0.0066	-0.085	5526.750	6.5	41443.482	6.5
2784.4497	2784.4498	16		35903.149	0.0001	-0.001	5526.750	6.5	41429.900	6.5
2784.5592	2784.5533	95	b	35901.815	-0.0060	0.077	5790.641	5.5	41692.379	5.5
2784.6660	2784.6669	11		35900.350	0.0009	-0.011	289.041	5.5	36189.402	5.5
2784.9076	2784.9081	4		35897.241	0.0005	-0.006	8276.733	6.5	44173.980	6.5
2788.5251	2788.5246	11		35850.685	-0.0005	0.007	0.000	4.5	35850.678	5.5
2789.2284	2789.2236	79		35841.700	-0.0048	0.062	5790.641	5.5	41632.279	6.5
2791.2531	2791.2572	3		35815.592	0.0041	-0.052	5259.653	7.5	41075.297	8.5
2793.9333	2793.9363	47		35781.248	0.0030	-0.039	289.041	5.5	36070.328	4.5
2794.0612	2794.0576	8	D,as	35779.695	-0.0036	0.046	5790.641	5.5	41570.290	5.5
2794.0636	2794.0576	8	D,as	35779.695	-0.0060	0.077	8394.362	7.5	44173.980	6.5
2794.9276	2794.9215	37		35768.636	-0.0062	0.079	8853.748	8.5	44622.305	7.5
2795.2282	2795.2335	41		35764.643	0.0053	-0.068	914.765	4.5	36679.476	3.5
2796.2329	2796.2312	5		35751.882	-0.0017	0.022	0.000	4.5	35751.860	5.5
2797.1416	2797.1451	19		35740.201	0.0035	-0.045	914.765	4.5	36655.011	3.5
2800.1004	2800.0975	38		35702.521	-0.0029	0.037	5526.750	6.5	41229.234	7.5
2803.8298	2803.8262	40		35655.042	-0.0036	0.046	1749.123	6.5	37404.119	5.5
2805.2406	2805.2421	14	D	35637.045	0.0015	-0.019	2294.696	5.5	37931.760	4.5
2805.2455	2805.2421	14	D	35637.045	-0.0034	0.043	914.765	4.5	36551.767	5.5
2806.4938	2806.4936	11		35621.158	-0.0002	0.002	6283.431	6.5	41904.587	5.5
2807.1192	2807.1167	69	as	35613.251	-0.0025	0.032	289.041	5.5	35902.260	4.5
2809.0118	2809.0131	34		35589.208	0.0013	-0.017	1749.123	6.5	37338.348	7.5
2809.6382	2809.6426	29		35581.234	0.0044	-0.056	9626.113	6.5	45207.403	7.5
2809.9856	2809.9791	15	p	35576.974	-0.0066	0.083	289.041	5.5	35865.932	4.5
2813.0414	2813.0421	17		35538.240	0.0007	-0.009	4706.273	2.5	40244.522	1.5
2813.5474	2813.5491	7		35531.835	0.0017	-0.022	5526.750	6.5	41058.607	5.5
2814.7037	2814.7027	5		35517.273	-0.0010	0.013	4420.871	5.5	39938.131	5.5
2817.9580	2817.9578	37		35476.246	-0.0002	0.002	914.765	4.5	36391.009	3.5

Table 9. Cont.

$wl_{Ritz}$ in Air (Å)	$wl_{exp}$ in Air (Å)	Int	Note	$wl_{exp}$ (cm <sup>-1</sup> )	$\Delta wl$ (Å)	$\Delta wn$ (cm <sup>-1</sup> )	$E_{odd}$ (cm <sup>-1</sup> )	$J_{odd}$	Even (cm <sup>-1</sup> )	$J_{even}$
2819.0247	2819.0286	7		35462.770	0.0039	-0.049	289.041	5.5	35751.860	5.5
2819.2845	2819.2778	8		35459.636	-0.0067	0.084	6445.035	4.5	41904.587	5.5
2820.2640	2820.2637	6		35447.240	-0.0003	0.004	2294.696	5.5	37741.932	4.5
2820.5036	2820.4993	13	as	35444.279	-0.0043	0.054	4585.434	6.5	40029.659	6.5
2821.1209	2821.1202	103		35436.482	-0.0006	0.008	914.765	4.5	36351.239	3.5
2826.2615	2826.2551	73	as	35372.099	-0.0064	0.080	0.000	4.5	35372.019	5.5
2826.6653	2826.6723	15		35366.879	0.0070	-0.087	4420.871	5.5	39787.837	5.5
2826.7289	2826.7250	25		35366.219	-0.0039	0.049	6445.035	4.5	41811.205	5.5
2828.9347	2828.9339	37		35338.608	-0.0007	0.009	914.765	4.5	36253.364	5.5
2829.2940	2829.2865	132		35334.205	-0.0075	0.094	5790.641	5.5	41124.752	6.5
2829.3965	2829.4002	53	p	35332.784	0.0038	-0.047	1749.123	6.5	37081.954	7.5
2830.0727	2830.0759	10		35324.349	0.0032	-0.040	0.000	4.5	35324.389	5.5
2831.5587	2831.5603	26	p	35305.831	0.0016	-0.020	5790.641	5.5	41096.492	6.5
2832.0616	2832.0605	44		35299.599	-0.0011	0.014	5259.653	7.5	40559.238	8.5
2832.0988	2832.0965	14		35299.150	-0.0023	0.029	4585.434	6.5	39884.555	6.5
2833.8199	2833.8173	29		35277.715	-0.0026	0.032	2294.696	5.5	37572.379	6.5
2834.0646	2834.0590	57	as	35274.707	-0.0056	0.070	914.765	4.5	36189.402	5.5
2834.5444	2834.5520	13		35268.572	0.0076	-0.094	914.765	4.5	36183.431	5.5
2834.5554	2834.5520	13		35268.572	-0.0035	0.043	6283.431	6.5	41551.960	5.5
2835.5690	2835.5682	10		35255.932	-0.0008	0.010	289.041	5.5	35544.963	4.5
2836.9143	2836.9164	19		35239.182	0.0021	-0.026	4420.871	5.5	39660.079	6.5
2837.1943	2837.1947	18		35235.725	0.0004	-0.005	914.765	4.5	36150.495	3.5
2837.3302	2837.3253	27		35234.103	-0.0049	0.061	0.000	4.5	35234.042	5.5
2839.7944	2839.8005	27		35203.393	0.0061	-0.075	914.765	4.5	36118.233	4.5
2839.8803	2839.8864	34	D	35202.328	0.0061	-0.075	4585.434	6.5	39787.837	5.5
2839.8925	2839.8864	34	D	35202.328	-0.0061	0.076	289.041	5.5	35491.293	5.5
2840.4603	2840.4659	16		35195.146	0.0056	-0.069	1749.123	6.5	36944.338	5.5
2842.4803	2842.4828	54		35170.173	0.0025	-0.031	2294.696	5.5	37464.900	6.5
2842.8541	2842.8515	26		35165.612	-0.0027	0.033	40882.028	5.5	5716.449	4.5
2845.5385	2845.5356	6		35132.445	-0.0028	0.035	1749.123	6.5	36881.533	6.5
2845.9556	2845.9514	9	as	35127.312	-0.0042	0.052	914.765	4.5	36042.025	4.5
2846.1491	2846.1474	11	D	35124.893	-0.0017	0.021	8510.866	5.5	43635.738	6.5
2846.1497	2846.1474	11	D	35124.893	-0.0023	0.028	8276.733	6.5	43401.598	7.5
2846.3700	2846.3683	16		35122.167	-0.0017	0.021	7166.632	4.5	42288.778	5.5
2849.9862	2849.9799	7		35077.659	-0.0063	0.077	5259.653	7.5	40337.235	8.5
2852.7458	2852.7524	9		35043.573	0.0065	-0.080	5526.750	6.5	40407.403	6.5
2853.4221	2853.4200	348		35035.374	-0.0021	0.026	289.041	5.5	35324.389	5.5
2853.5636	2853.5639	12	LA,D	35033.607	0.0003	-0.004	6283.431	6.5	41317.042	5.5
2853.5653	2853.5639	12	LA,D	35033.607	-0.0014	0.017	1749.123	6.5	36782.713	6.5
2854.9132	2854.9129	4		35017.053	-0.0003	0.004	1749.123	6.5	36766.172	5.5
2855.7135	2855.7198	135		35007.158	0.0064	-0.078	8394.362	7.5	43401.598	7.5
2856.0308	2856.0297	182		35003.360	-0.0011	0.014	914.765	4.5	35918.111	5.5
2856.2831	2856.2829	67		35000.257	-0.0002	0.003	2294.696	5.5	37294.950	6.5
2856.6147	2856.6188	13	as	34996.141	0.0042	-0.051	9626.113	6.5	44622.305	7.5
2857.2259	2857.2328	3		34988.621	0.0069	-0.084	5526.750	6.5	40515.455	5.5
2858.9077	2858.9146	124		34968.038	0.0069	-0.085	0.000	4.5	34968.123	5.5
2859.8812	2859.8868	30		34956.151	0.0056	-0.069	5526.750	6.5	40482.970	5.5
2860.4656	2860.4578	141	p	34949.178	-0.0079	0.096	0.000	4.5	34949.082	3.5
2860.7997	2860.8038	48		34944.950	0.0042	-0.051	289.041	5.5	35234.042	5.5
2862.2375	2862.2426	37		34927.384	0.0052	-0.063	7598.353	5.5	42525.800	5.5
2862.4075	2862.4069	69		34925.379	-0.0006	0.007	289.041	5.5	35214.413	4.5
2862.6160	2862.6160	53	LA	34922.828	0.0000	0.000	4585.434	6.5	39508.262	7.5
2863.5279	2863.5306	29	#1	34911.674	0.0027	-0.033	5259.653	7.5	40171.360	8.5
2863.8629	2863.8701	4	c	34907.535	0.0072	-0.088	7598.353	5.5	42505.976	6.5
2864.4082	2864.4097	34	#2	34900.960	0.0015	-0.018	2294.696	5.5	37195.674	6.5
2865.1378	2865.1415	113	#3	34892.046	0.0036	-0.044	4420.871	5.5	39312.961	6.5
2865.6808	2865.6847	558	#4, LA	34885.431	0.0039	-0.048	0.000	4.5	34885.479	5.5
2866.1576	2866.1603	85		34879.643	0.0027	-0.033	8521.922	7.5	43401.598	7.5
2866.7879	2866.7887	24	#5	34871.997	0.0008	-0.010	6445.035	4.5	41317.042	5.5
2868.0074	2868.0134	63	#6	34857.106	0.0060	-0.073	4585.434	6.5	39442.613	7.5
2868.1857	2868.1865	47	#7	34855.003	0.0007	-0.009	2294.696	5.5	37149.708	4.5
2869.3858	2869.3803	62	#8, p	34840.505	-0.0054	0.066	5667.331	3.5	40507.770	3.5
2869.6612	2869.6595	22	#9	34837.116	-0.0017	0.021	914.765	4.5	35751.860	5.5
2870.9740	2870.9721	116	#10	34821.188	-0.0019	0.023	289.041	5.5	35110.206	4.5
2872.5019	2872.5038	25	c	34802.620	0.0020	-0.024	1749.123	6.5	36551.767	5.5
2872.5897	2872.5899	2		34801.577	0.0002	-0.003	6445.035	4.5	41246.615	4.5
2873.0033	2873.0085	44		34796.507	0.0052	-0.063	2294.696	5.5	37091.266	4.5
2873.2953	2873.2939	50	#11	34793.050	-0.0014	0.017	5526.750	6.5	40319.783	5.5
2873.5191	2873.5141	146	#12	34790.384	-0.0050	0.060	5790.641	5.5	40580.965	5.5
2874.0820	2874.0812	86		34783.519	-0.0007	0.009	1749.123	6.5	36532.633	7.5
2874.4694	2874.4633	21		34778.896	-0.0061	0.074	0.000	4.5	34778.822	5.5

Table 9. Cont.

$w_{Ritz}$ in Air (Å)	$w_{exp}$ in Air (Å)	Int	Note	$w_{exp}$ (cm <sup>-1</sup> )	$\Delta w$ (Å)	$\Delta w_{int}$ (cm <sup>-1</sup> )	$F_{odd}$ (cm <sup>-1</sup> )	J <sub>odd</sub>	Even (cm <sup>-1</sup> )	J <sub>even</sub>
2874.7708	2874.7635	148		34775.264	-0.0073	0.088	6283.431	6.5	41058.607	5.5
2875.1857	2875.1898	89	T <sub>p</sub>	34770.108	0.0041	-0.049	289.041	5.5	35059.198	6.5
2875.1866	2875.1898	89	T <sub>p</sub>	34770.108	0.0031	-0.038	8510.866	5.5	43281.012	5.5
2875.1952	2875.1898	89	T <sub>p</sub>	34770.108	-0.0055	0.066	914.765	4.5	35684.807	5.5
2876.5188	2876.5190	55		34754.041	0.0002	-0.003	1749.123	6.5	36503.167	5.5
2877.5677	2877.5722	41	LA	34741.325	0.0045	-0.054	0.000	4.5	34741.379	4.5
2877.7302	2877.7226	194		34739.509	-0.0075	0.091	2294.696	5.5	37034.114	5.5
2878.9404	2878.9408	30		34724.810	0.0003	-0.004	5790.641	5.5	40515.455	5.5
2879.0798	2879.0806	118		34723.123	0.0008	-0.010	7598.353	5.5	42321.486	6.5
2879.9719	2879.9729	15	P	34712.365	0.0010	-0.012	43060.067	5.5	8347.690	5.5
2881.7318	2881.7380	18		34691.103	0.0062	-0.075	2294.696	5.5	36985.874	6.5
2881.7944	2881.7925	23		34690.447	-0.0018	0.022	7598.353	5.5	42288.778	5.5
2881.8744	2881.8796	16		34689.399	0.0052	-0.063	8276.733	6.5	42966.195	7.5
2881.9893	2881.9962	28	as	34687.995	0.0070	-0.084	4420.871	5.5	39108.950	5.5
2882.5843	2882.5784	127		34680.989	-0.0059	0.071	0.000	4.5	34680.918	4.5
2882.7370	2882.7381	233		34679.068	0.0012	-0.014	289.041	5.5	34968.123	5.5
2882.9252	2882.9279	165		34676.785	0.0027	-0.032	4420.871	5.5	39097.688	6.5
2885.1866	2885.1884	45		34649.620	0.0018	-0.022	2294.696	5.5	36944.338	5.5
2885.3330	2885.3323	10	c	34647.893	-0.0007	0.009	5667.331	3.5	40315.215	3.5
2885.5754	2885.5836	7		34644.875	0.0082	-0.098	5790.641	5.5	40435.614	6.5
2885.6088	2885.6149	33		34644.499	0.0062	-0.074	7166.632	4.5	41811.205	5.5
2886.0312	2886.0284	32		34639.535	-0.0027	0.033	914.765	4.5	35554.267	3.5
2886.1638	2886.1640	29		34637.908	0.0002	-0.003	4420.871	5.5	39058.782	5.5
2886.4456	2886.4514	28	LA	34634.459	0.0058	-0.070	289.041	5.5	34923.570	6.5
2886.4796	2886.4792	37	D	34634.126	-0.0004	0.005	2294.696	5.5	36928.817	4.5
2886.4824	2886.4792	37	D	34634.126	-0.0033	0.039	0.000	4.5	34634.087	4.5
2886.9223	2886.9234	53		34628.796	0.0012	-0.014	7166.632	4.5	41795.442	3.5
2887.0060	2887.0111	7		34627.745	0.0051	-0.061	40344.255	5.5	5716.449	4.5
2887.2481	2887.2529	165		34624.845	0.0048	-0.057	5259.653	7.5	39884.555	6.5
2887.5908	2887.5910	70	LA	34620.790	0.0003	-0.003	9553.187	5.5	44173.980	6.5
2888.2558	2888.2565	96	LA	34612.813	0.0008	-0.009	0.000	4.5	34612.822	4.5
2888.7371	2888.7399	83		34607.021	0.0028	-0.034	4420.871	5.5	39027.926	6.5
2889.1209	2889.1232	39		34602.430	0.0023	-0.027	6283.431	6.5	40885.888	6.5
2889.2613	2889.2607	29		34600.783	-0.0006	0.007	2294.696	5.5	36895.472	4.5
2889.6236	2889.6258	198	LA	34596.412	0.0022	-0.026	289.041	5.5	34885.479	5.5
2890.4257	2890.4214	43		34586.889	-0.0043	0.052	2294.696	5.5	36881.533	6.5
2891.6259	2891.6265	6	as	34572.478	0.0007	-0.008	8276.733	6.5	42849.219	5.5
2891.6805	2891.6847	19		34571.783	0.0042	-0.050	8394.362	7.5	42966.195	7.5
2891.7924	2891.7926	66	D	34570.493	0.0002	-0.002	2294.696	5.5	36865.191	5.5
2891.8001	2891.7926	66	D	34570.493	-0.0075	0.090	42918.093	5.5	8347.690	5.5
2894.8391	2894.8403	45		34534.101	0.0012	-0.014	1749.123	6.5	36283.238	5.5
2895.5407	2895.5443	47		34525.704	0.0036	-0.043	7166.632	4.5	41692.379	5.5
2895.6254	2895.6257	34		34524.734	0.0003	-0.004	1749.123	6.5	36273.861	6.5
2895.7279	2895.7315	4		34523.472	0.0037	-0.044	4585.434	6.5	39108.950	5.5
2896.0761	2896.0695	46		34519.443	-0.0065	0.078	5526.750	6.5	40046.115	5.5
2896.6728	2896.6710	717	as,IV	34512.275	-0.0018	0.021	4585.434	6.5	39097.688	6.5
2897.4573	2897.4562	47		34502.923	-0.0012	0.014	5526.750	6.5	40029.659	6.5
2898.1286	2898.1254	144	as	34494.955	-0.0032	0.038	5259.653	7.5	39754.570	8.5
2898.3689	2898.3677	51		34492.072	-0.0013	0.015	289.041	5.5	34781.098	4.5
2898.5602	2898.5686	146		34489.681	0.0084	-0.100	289.041	5.5	34778.822	5.5
2898.7085	2898.7080	30		34488.022	-0.0004	0.005	2294.696	5.5	36782.713	6.5
2898.9194	2898.9231	174		34485.463	0.0037	-0.044	42833.197	5.5	8347.690	5.5
2899.9121	2899.9080	19		34473.751	-0.0040	0.048	8276.733	6.5	42750.436	6.5
2899.9419	2899.9443	21		34473.320	0.0024	-0.028	4585.434	6.5	39058.782	5.5
2900.2638	2900.2714	46	D <sub>c</sub>	34469.432	0.0076	-0.090	8379.697	4.5	42849.219	5.5
2900.2656	2900.2714	46	D <sub>c</sub>	34469.432	0.0058	-0.069	5259.653	7.5	39729.154	7.5
2900.3168	2900.3173	23	c	34468.886	0.0005	-0.006	2294.696	5.5	36763.588	4.5
2900.7128	2900.7164	27	P	34464.144	0.0036	-0.043	4706.273	2.5	39170.460	2.5
2902.3902	2902.3976	39	p	34444.185	0.0074	-0.088	8521.922	7.5	42966.195	7.5
2902.4127	2902.4100	29	P	34444.037	-0.0027	0.032	5790.641	5.5	40234.646	5.5
2902.8069	2902.8073	19	LA	34439.323	0.0004	-0.005	0.000	4.5	34439.328	5.5
2903.7855	2903.7816	121		34427.768	-0.0039	0.046	42775.412	5.5	8347.690	5.5
2904.5041	2904.5065	63	LA	34419.176	0.0024	-0.028	289.041	5.5	34708.245	6.5
2905.8166	2905.8110	46		34403.724	-0.0056	0.066	7166.632	4.5	41570.290	5.5
2906.0896	2906.0976	81		34400.331	0.0080	-0.095	5259.653	7.5	39660.079	6.5
2906.9576	2906.9550	70		34390.184	-0.0025	0.030	8276.733	6.5	42666.887	7.5
2907.0539	2907.0554	41		34388.997	0.0014	-0.017	289.041	5.5	34678.055	6.5
2908.0936	2908.0988	14		34376.658	0.0052	-0.062	6445.035	4.5	40821.755	4.5
2908.4109	2908.4115	89		34372.962	0.0006	-0.007	4420.871	5.5	38793.840	6.5
2909.0748	2909.0674	24		34365.212	-0.0074	0.087	7598.353	5.5	41963.478	4.5

Table 9. Cont.

$wl_{Ritz}$ in Air (Å)	$wl_{exp}$ in Air (Å)	Int	Note	$wl_{exp}$ ( $cm^{-1}$ )	$\Delta wl$ (Å)	$\Delta wv$ ( $cm^{-1}$ )	$E_{odd}$ ( $cm^{-1}$ )	$J_{odd}$	$E_{even}$ ( $cm^{-1}$ )	$J_{even}$
2909.6946	2909.6885	63		34357.877	-0.0061	0.072	5526.750	6.5	39884.555	6.5
2910.4278	2910.4339	63		34349.081	0.0061	-0.072	6445.035	4.5	40794.188	4.5
2910.5243	2910.5222	10		34348.039	-0.0021	0.025	5259.653	7.5	39607.667	6.5
2910.6385	2910.6395	32		34346.655	0.0010	-0.012	7598.353	5.5	41945.020	6.5
2911.7385	2911.7334	17		34333.752	-0.0052	0.061	4420.871	5.5	38754.562	4.5
2912.5792	2912.5779	40	LA	34323.796	-0.0013	0.015	289.041	5.5	34612.822	4.5
2913.9646	2913.9679	26		34307.424	0.0032	-0.038	8755.640	6.5	43063.102	6.5
2914.2520	2914.2493	70	D	34304.111	-0.0027	0.032	289.041	5.5	34593.120	5.5
2914.2561	2914.2493	70	D	34304.111	-0.0068	0.080	45044.296	7.5	10740.265	6.5
2914.6285	2914.6235	106		34299.707	-0.0050	0.059	914.765	4.5	35214.413	4.5
2914.7246	2914.7324	82	p	34298.425	0.0078	-0.092	0.000	4.5	34298.517	5.5
2915.4993	2915.4945	97	as	34289.459	-0.0048	0.056	8394.362	7.5	42683.765	8.5
2915.5822	2915.5801	38		34288.453	-0.0021	0.025	1749.123	6.5	36037.551	7.5
2916.7057	2916.7052	57	D	34275.226	-0.0005	0.006	5526.750	6.5	39801.970	6.5
2916.7136	2916.7052	57	D	34275.226	-0.0083	0.098	4420.871	5.5	38695.999	5.5
2916.9351	2916.9366	37		34272.507	0.0015	-0.018	8394.362	7.5	42666.887	7.5
2917.5409	2917.5390	207		34265.431	-0.0020	0.023	5401.503	3.5	39666.911	4.5
2917.9089	2917.9034	26		34261.152	-0.0055	0.065	5526.750	6.5	39787.837	5.5
2938.9919	2938.9908	114		34015.338	-0.0010	0.012	1749.123	6.5	35764.449	7.5
2940.0800	2940.0783	18	p	34002.757	-0.0017	0.020	1749.123	6.5	35751.860	5.5
2940.2834	2940.2880	274	p	34000.331	0.0047	-0.054	9075.732	3.5	43076.117	4.5
2940.4294	2940.4290	46		33998.701	-0.0004	0.005	5401.503	3.5	39400.199	4.5
2941.3079	2941.3068	30		33988.555	-0.0011	0.013	2294.696	5.5	36283.238	5.5
2941.6963	2941.6897	32		33984.131	-0.0067	0.077	8521.922	7.5	42505.976	6.5
2941.9164	2941.9176	213	LA	33981.498	0.0012	-0.014	5526.750	6.5	39508.262	7.5
2942.1196	2942.1204	74		33979.156	0.0008	-0.009	2294.696	5.5	36273.861	6.5
2942.4224	2942.4278	7	D	33975.606	0.0054	-0.062	10198.312	7.5	44173.980	6.5
2942.4268	2942.4278	7	D,LA	33975.606	0.0010	-0.011	4706.273	2.5	38681.890	3.5
2942.7456	2942.7519	100		33971.864	0.0063	-0.073	7598.353	5.5	41570.290	5.5
2942.8515	2942.8516	49	LA	33970.713	0.0001	-0.001	914.765	4.5	34885.479	5.5
2943.8954	2943.8964	160		33958.656	0.0010	-0.012	2294.696	5.5	36253.364	5.5
2944.3342	2944.3300	12	as	33953.655	-0.0042	0.048	7598.353	5.5	41551.960	5.5
2944.5416	2944.5456	34		33951.169	0.0040	-0.046	6283.431	6.5	40234.646	5.5
2945.5252	2945.5297	7		33939.830	0.0045	-0.052	5259.653	7.5	39199.535	7.5
2945.5971	2945.5947	10		33939.081	-0.0023	0.027	5790.641	5.5	39729.695	6.5
2945.8164	2945.8129	13		33936.567	-0.0035	0.040	5526.750	6.5	39463.277	5.5
2945.8896	2945.8919	96	D,LA	33935.658	0.0023	-0.026	1749.123	6.5	35684.807	5.5
2945.8980	2945.8919	96	D	33935.658	-0.0062	0.071	5401.503	3.5	39337.090	4.5
2946.2771	2946.2831	13		33931.152	0.0060	-0.069	4585.434	6.5	38516.655	6.5
2946.6046	2946.6073	32	p	33927.418	0.0027	-0.031	5526.750	6.5	39454.199	6.5
2946.6329	2946.6252	42	p	33927.212	-0.0076	0.088	8394.362	7.5	42321.486	6.5
2947.5118	2947.5119	51		33917.006	0.0001	-0.001	2294.696	5.5	36211.703	6.5
2948.0897	2948.0907	161		33910.347	0.0010	-0.012	289.041	5.5	34199.400	5.5
2949.4511	2949.4501	79	p	33894.718	-0.0010	0.012	2294.696	5.5	36189.402	5.5
2949.6008	2949.6057	38	as	33892.930	0.0049	-0.056	4420.871	5.5	38313.857	5.5
2949.6888	2949.6890	33		33891.973	0.0002	-0.002	7166.632	4.5	41058.607	5.5
2949.8281	2949.8363	23		33890.280	0.0082	-0.094	7598.353	5.5	41488.727	5.5
2949.9708	2949.9735	14		33888.704	0.0027	-0.031	2294.696	5.5	36183.431	5.5
2950.5021	2950.5005	15		33882.651	-0.0017	0.019	4585.434	6.5	38468.066	7.5
2950.5656	2950.5655	26		33881.905	-0.0002	0.002	1749.123	6.5	35631.026	7.5
2951.0563	2951.0646	84	D	33876.174	0.0084	-0.096	5790.641	5.5	39666.911	4.5
2951.0724	2951.0646	84	D	33876.174	-0.0078	0.089	0.000	4.5	33876.085	5.5
2951.9221	2951.9153	23	p	33866.412	-0.0069	0.079	914.765	4.5	34781.098	4.5
2953.0016	2953.0029	105		33853.938	0.0013	-0.015	4706.273	2.5	38560.226	3.5
2953.5797	2953.5870	60		33847.243	0.0073	-0.084	5667.331	3.5	39514.658	2.5
2953.7715	2953.7756	188	p	33845.082	0.0041	-0.047	7598.353	5.5	41443.482	6.5
2954.5230	2954.5233	326	p	33836.521	0.0003	-0.004	2294.696	5.5	36131.221	5.5
2954.6867	2954.6825	143		33834.698	-0.0042	0.048	5259.653	7.5	39094.303	7.5

LA: line already assigned as U II transition in [7], as: asymmetrical line, c: complex line shape, p: line resolved on the plate, but perturbed by a close line, b: broad line, ?: line given by [12] as U III without classification, IV : this line could be blended with a strong U IV line, D: line with double identification, T: line with triple identification, #n: line number in Figure 1.

**Table 10.** Transitions establishing the newly determined even parity level  $5f^3 6d7p$  ( $^4I$ ) $^6K$  ( $J = 5.5$ ) of the  $U^+$  ion at  $39113.98 \pm 0.1 \text{ cm}^{-1}$ . In  $\log(g_I/f)$ ,  $f$  is the absorption oscillator strength and  $g_I$ , the statistical weight of the lower level.  $gA$  is the upper level statistical weight  $g$  multiplied by the Einstein coefficient of spontaneous emission.  $CF$  is the cancellation factor defined by Equation (14.107), p432 in [10].

$E_{th}$ ( $\text{cm}^{-1}$ )	$J$	Odd Level	$wn_{th}$ ( $\text{cm}^{-1}$ )	$\log(g_I/f)$	$gA$ ( $\text{s}^{-1}$ )	$CF$	$E_{exp}$ ( $\text{cm}^{-1}$ )	$wn_{exp}$ ( $\text{cm}^{-1}$ )	$\lambda_{exp}$ in Air ( $\text{\AA}$ )	$Int_{exp}$ (arb.)
−56.8	4.5	$5f^3 7s^2$ (4I) 4I	38865.8	0.263	1.847E+09	0.63	0.000	39114.382	2555.8378	545
224.4	5.5	$5f^3 6d7s$ (4I) 6L	38584.6	−1.518	3.014E+07	0.03	289.041	38824.783	2574.9033	4
1715.5	6.5	$5f^3 6d7s$ (4I) 6L	37093.5	0.181	1.391E+09	−0.27	1749.123	37364.867	2675.5157	228
2320.7	5.5	$5f^3 6d7s$ (4I) 6K	36488.3	−0.252	4.974E+08	−0.21	2294.696	36819.292	2715.1628	36
4406.4	5.5	$5f^3 7s^2$ (4I) 4I	34402.6	−0.877	1.048E+08	0.20	4420.871	34692.797	2881.5973	14
4577.9	6.5	$5f^3 6d7s$ (4I) 6L	34231.1	−0.160	5.404E+08	−0.16	4585.434	34528.617	2895.3001	33

## 5. Conclusions

The lowest energy levels of the singly ionized uranium are interpreted following the Racah-Slater parametric method by means of Cowan codes. In the odd parity, the number of interpreted levels is about ten times larger than the number of free parameters. The relatively small *rms* deviation of the energies and the deviations between  $g_L^{th}$  and  $g_L^{exp}$  Landé factors for many levels show that the present model is robust. Some experimental level energies, although supported by the high accuracy of the observed FTS wave numbers, could not be attributed unambiguously to a theoretical level energy. The limitations of the present theoretical description are even more obvious in the even parity with larger *rms* deviations on the energies for both groups of configurations studied. After 70 years of investigations, the spectrum of U II still deserves further experimental studies for removing uncertain interpretations. The main difficulties are due to the ambiguities on the  $J$  values of levels, the determination of which would need a more complete study of Zeeman effect. Furthermore, the description of the strongly mixed CI wave functions could only be confirmed by the value of the Landé factor. By remembering the sentence *Levels without known  $g$  values are less certain because of the possibilities of fortuitous coincidences* written in [6], we do consider that the present calculations are satisfactory in spite of the uninterpreted levels. A theoretical interpretation of the core configurations  $5f^4$  and  $5f^3(6d + 7s)$  of U III is presently under way for a better knowledge of appropriate scaling factors of the *HFR* radial integrals to be used in U II. An estimate of the partition function shows that level energies from parametric fit are preferable for its calculation. On the experimental side, a list of 451 ultraviolet spectral lines from high resolution vacuum spark spectra identified as U II transitions is reported, as well as six other transitions establishing a new energy level in the even parity configuration  $5f^3 6d7p$ .

**Acknowledgments:** The photographic spectrograms were recorded between 1986 and 1988 with technical assistance of Françoise Launay and Maurice Benharrour. Christophe Blaess is acknowledged for digitizing the spectrograms. The financial support of the French CNRS – PNPS national program is acknowledged. This work is part of the Plas@Par LabEx project managed by the ANR (ANR-11-IDEX-0004-02). AM and MS wish to acknowledge supports from Université Mouloud Mammeri, Tizi-Ouzou, Algeria and from the project CNEPRU D00520110032, Algeria.

**Author Contributions:** These authors contributed equally to this work.

**Conflicts of Interest:** The authors declare no conflict of interest.

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Article

# The Role of the Hyperfine Structure for the Determination of Improved Level Energies of Ta II, Pr II and La II

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Academic Editor: Joseph Reader

Received: 19 January 2017; Accepted: 21 February 2017; Published: 28 February 2017

**Abstract:** For the determination of improved energy levels of ionic spectra of elements with large values of nuclear magnetic dipole moment (and eventually large values of nuclear quadrupole moments), it is necessary to determine the center of gravity of spectral lines from resolved hyperfine structure patterns appearing in highly resolved spectra. This is demonstrated on spectral lines of Ta II, Pr II and La II. Blend situations (different transitions with accidentally nearly the same wave number difference between the combining levels) must also be considered.

**Keywords:** energy levels; Ta II; Pr II; La II

## 1. Introduction

The laser spectroscopy group at Graz University of Technology has been concerned since 1990 with investigations of the hyperfine (hf) structure of several elements. The spectra of tantalum, praseodymium and lanthanum were investigated most intensely. As a source of free atoms, a hollow cathode lamp was used in which a low-pressure plasma of the treated element was generated by cathode sputtering. For starting the discharge, a noble gas (argon or neon) at a typical pressure of 0.5 mbar was used. This source of free atoms and ions was investigated by tunable laser light (band width ca. 1 MHz) by scanning the laser frequency across the selected wavelength range. Either laser-induced fluorescence light or the change of the discharge impedance (optogalvanic detection) was observed. Details of the experimental arrangement can be found in various publications, e.g., [1–3].

In this paper, spectra of Ta, Pr and La are treated. These elements have in their natural abundance either only one dominant isotope (Ta, La, see Table 1) or are isotopically pure (Pr). Their nuclear magnetic dipole moment  $\mu$  is large enough to cause hyperfine splitting of the spectral lines larger than the Doppler width in the spectra. Thus, in most cases, the observed hf structure can be used as valuable help for the classification of the spectral lines. The isotope composition and nuclear moments can be found in Table 1. For Pr and La, the quadrupole moment is quite small and can be neglected for most of the energy levels.



**Table 1.** Isotope composition and nuclear moments of the investigated elements (natural abundance). In the spectra of Ta and La, we observed only the dominant isotopes  $^{181}\text{Ta}$  and  $^{139}\text{La}$ .

Element	Z	Isotope	Natural Abundance %	Lifetime (Years)	Nuclear Spin Quantum Number I	Magnetic Moment $\mu$ ( $\mu_N$ )	Electric Quadrupole Moment Q ( $10^{-28} \text{ m}^2$ )
Ta	73	180	0.012	$1.2 \times 10^{15}$	9	+4.825(11)	+4.95(2)
Ta	73	181	99.998	stable	7/2	+2.3705(7)	+3.28(6)
Pr	59	141	100	stable	5/2	+4.2754(5)	-0.059(4)
La	57	138	0.09	$1.05 \times 10^{11}$	5	+3.713646(7)	+0.45(2)
La	57	139	99.91	stable	7/2	+2.7830455(9)	+0.20(1)

\* Based on uncorrected proton moment, 2.79277564 nm. Values of  $\mu$  and Q from [4].

While at the early stage of the investigations, the hf constants of already known energy levels were determined, and it turned out later that the list of energy levels given in literature [5,6] is far from being complete. Thus, the focus was directed to the finding of new energy levels in order to explain spectral lines that could not be classified as transitions between known energy levels. An overview of how previously unknown energy levels can be found is given in Ref. [7].

In order to get accurate start wavelengths for laser spectroscopic investigations, spectra with high resolution and high wavelength precision are needed. These requirements can be fulfilled by means of Fourier-transform (FT) spectroscopy. Several co-operations led to the availability of spectra of Ta [8], Pr [9], and La [10]. In these spectra, much more lines can be found than listed in commonly used wavelength tables [11]. The spectra were taken with a resolution between 0.03 and 0.05  $\text{cm}^{-1}$  and carefully wavelength calibrated using Ar II lines [12].

For strong lines which were classified and for which the hf constants of the combining levels were known, one finds that the center of gravity (cg) wavelengths determined from the FT spectra usually differ from wavelengths calculated from the known level energies. The conversion from wave numbers to standard air wavelengths and back was performed using the formula given by Reeder and Peck [13] for the refractive index of air.

Thus, exploiting the low uncertainty of the cg wavelengths determined from the FT spectra, improved level energies were determined. This was made step by step, beginning with the upper levels combining with the ground level. From these upper levels, transitions to lower levels were searched and energies of low-lying levels were corrected, and so on. Finally, the level energies were determined by a global fit procedure.

Since each spectrum contains several tenths of thousands of spectral lines, and since the treated elements have several hundreds or thousands energy levels, one can imagine that this procedure is very time-consuming. Thus, first the spectra of the first ions, Ta II, Pr II and La II, were used to perform a final determination of level energies. For most of the levels, an uncertainty of the level energy below 0.01  $\text{cm}^{-1}$  was achieved.

For the determination of the hf constants of the levels involved in an investigated transition (hf resolved spectra either from an FT spectrum or a laser spectroscopic scan), we used a software called "Fitter" which was very helpful [14].

It is clear that a suitable computer program is needed to manage such huge numbers of lines and the extended FT spectra. Thus, a program called "Elements" was developed (for descriptions, see Refs. [7,15]). One can select a certain wavelength and then go from one line to the next. The corresponding part of the FT spectrum is automatically shown. For classified lines, the combining levels and the hf pattern is shown in graphical form. For unclassified lines, classification suggestions (transitions between known energy levels within a selected wave number deviation) are also shown. A part of the FT spectrum can be copied easily to a simulation window where it can be compared with such a suggestion, for which the hf pattern is graphically shown. If no agreement between the pattern from the FT spectrum and any suggestion can be found, one has to assume that a previously unknown energy level is involved in the structure.

In the following sections, peculiarities of the investigated spectra are discussed in more details.

2. Ta II

Energy levels of Ta II are listed in the famous tables of Moore [5]. The given data are based mainly on works of Kiess [16], who published separately a collection of Ta II energy levels including the classified lines. Concerning the hf structure, a relatively low number of publications can be found. In 1952, Brown and Tamboulian [17] determined for the first time the nuclear moments of <sup>181</sup>Ta investigating the hf structure of 7 Ta II lines. In 1987, Engleman Jr. [18] determined the hf constants of several Ta II levels and improved the energy values, but the results were presented only at a symposium but never published. Eriksson et al. [19] investigated in 2002 the Ta II spectrum with respect to applications in astrophysics. Laser spectroscopic determinations of the hf constants of Ta II were performed by Messnarz and Guthöhrlein [20,21] at approximately the same time. During work on his thesis, Messnarz discovered some new energy levels of Ta II and could correct some incorrect classifications. Zilio and Pickering [22] investigated an FT spectrum of Ta II and published hf constants of several levels.

The FT spectrum taken by J. Pickering at Imperial College London and spectra taken at the Kitt Peak Observatory by Engleman Jr. were used later in Graz [8,23,24]. In these papers, the discovery of new energy levels of Ta I and the determination of hf constants of already known Ta I levels are reported. The papers are part of a series of works published in *Zeitschrift für Physik*, the succeeding *European Journal of Physics* and later in *Physica Scripta*, entitled “Investigation of the hyperfine structure of Ta I lines, Part I to X”. As can be seen from the list of authors, a strong collaboration between the group in Graz and the group of G. H. Guthöhrlein in Hamburg took place.

In the early stage of the investigations, it was very helpful to have a tool for distinguishing Ta I and Ta II spectral lines. This could be done with the help of photographic spectra, taken with a classical spectrograph, using for one trace of the spectrum a direct current (DC) hollow cathode lamp and, for a second trace, a discharge with pulsed excitation. In the pulsed discharge, the ionic lines are much more intense, allowing a clear distinguishing between Ta I and Ta II lines. One example of such spectra—in comparison with the FT spectra—is given in Ref. [25]. Another example where two spectral lines, one belonging to Ta I and the second to Ta II, are located side by side (Figure 1).

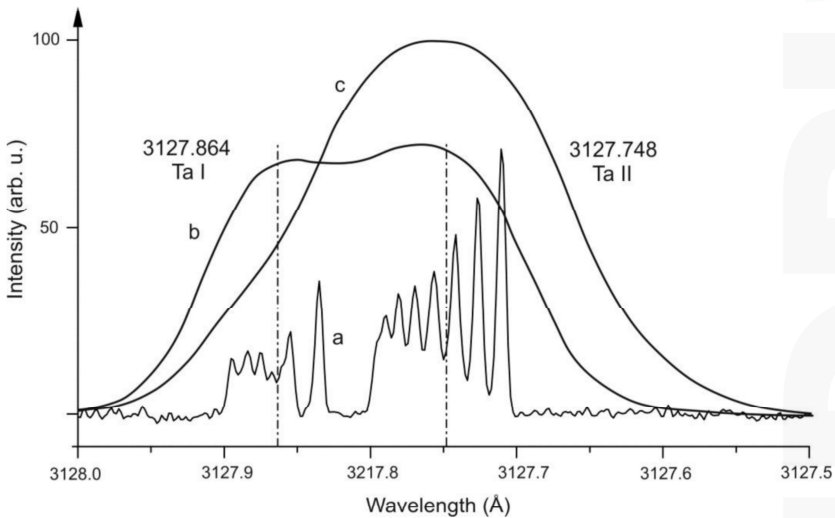
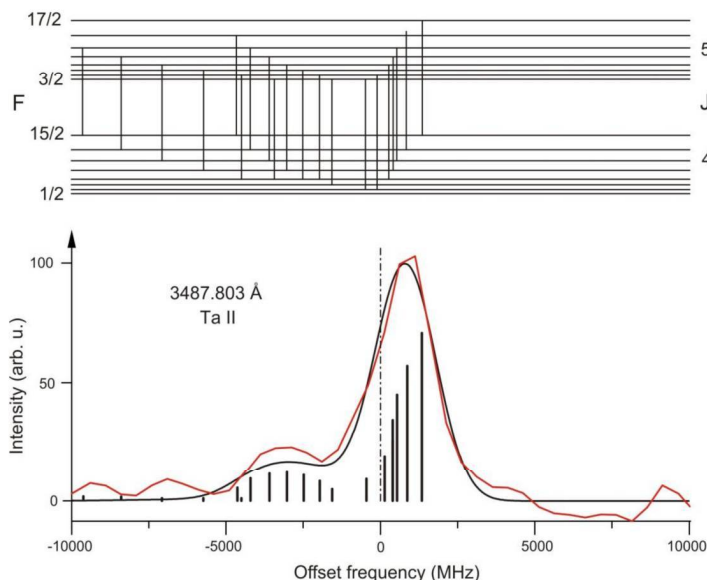


Figure 1. Comparison of a part of a highly resolved Fourier-transform (FT) spectrum with photographic spectra. For a description, see text.

In Figure 1, trace a shows the FT spectrum, full width at half maximum (FWHM) ca. 2.2 GHz. The light source was a hollow cathode lamp, operated by DC. The hf patterns of the lines are well resolved. The cg positions are marked with vertical dash-dotted lines. Traces b and c show photographic spectra, digitized from a photo plate generated by means of an Ebert-mounted grating spectrograph, focal length 2 m, 7th order (dispersion 0.72 Å/mm). The resolution is ca. 25 GHz (0.08 Å). In trace b, a hollow cathode lamp operated by DC was used, while, in trace c, the discharge was pulsed. This pulsed operation enhanced significantly the intensity of the ionic line compared to the atomic one. Thus, this spectral line on the photo plate causes difficulties in finding the cg wavelengths, since width and line center position strongly depend on the ratio of the intensities of the two lines and thus from the discharge conditions. Nevertheless, the two different photographic spectra made it easy to identify the structure at 3127.748 Å as an ionic line. The classification of the lines (and also of the lines in the subsequent figures) is given in Table A1 (see Appendix A).

In the FT spectra from Kitt Peak Observatory, an electrodeless microwave discharge was used as the light source. In these spectra, one can find a large number of unclassified lines. Some of them showed well resolved hf patterns. Analyzing these lines, a previously unknown system of high lying even parity ionic states with energies above 72,000 cm<sup>-1</sup> could be found, while the highest previously known even level is located at 40,900 cm<sup>-1</sup>. First, results were published (together with the description of the classification program “Elements”) in 2002 [15], all new energy levels in Ref. [26].

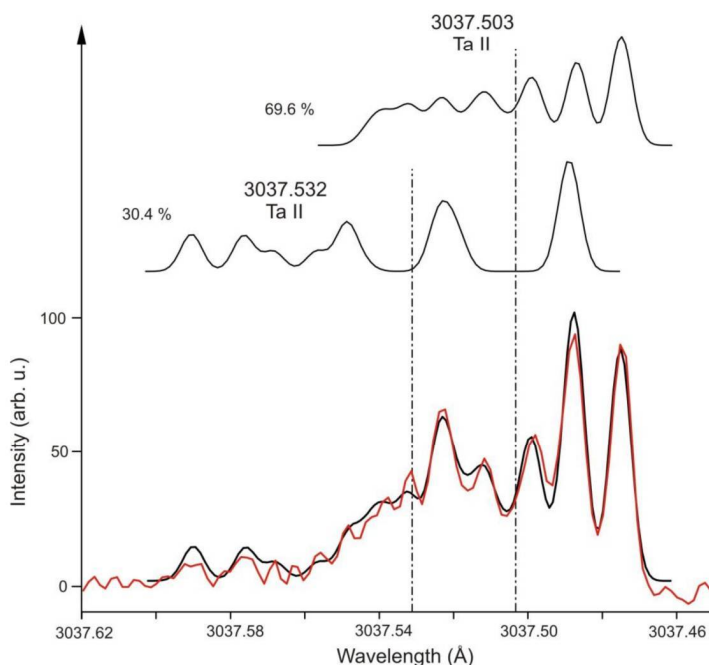
For finding accurate cg wavelengths of lines, it is very important to take into account their hf pattern. Figure 2 shows an example where, in the FT spectrum, practically only a single peak is visible. However, treating the peak wavelength as cg is not correct. Components with small intensities, but located far from the highest peak, shift the cg wavelength to the middle of the low-frequency wing of the peak.



**Figure 2.** Example of a Ta II spectral line where the center of gravity (cg) wavelength is different from the single large peak appearing in the FT spectrum. Red line: FT spectrum, black line: simulation, full width at half maximum (FWHM) 2.2 GHz. Shown is also the hyperfine (hf) level scheme, the transitions and the components (theoretical intensity ratios). The components on the left side of the high peak (built by overlapping hf components for which  $\Delta F = \Delta J$ ) are only barely visible in the FT spectrum. The cg is shifted against the peak by 0.8 GHz (0.05 Å). The cg wavelength is marked by a vertical line (chain-dotted).

During the procedure of line classification and cg wavelength determination, one is quite often confronted with blend situations. As an example, Figure 3 shows a blend situation of two Ta II lines. With known hf constants of the four involved energy levels, it is possible to decompose the observed structure into two overlapping lines and to determine their cg wavelengths (in this case differing by 0.029 Å).

In the Ta FT spectra, ranging from 2120 Å to 46,000 Å, one can find a number of 12,200 spectral lines, from which as many lines as possible were classified. Around 1000 of them are Ar I or Ar II lines, which can be used for wavelength calibration. Ca. 3000 lines belong to the Ta II spectrum. Despite of all efforts, roughly 2000 lines are still not classified.

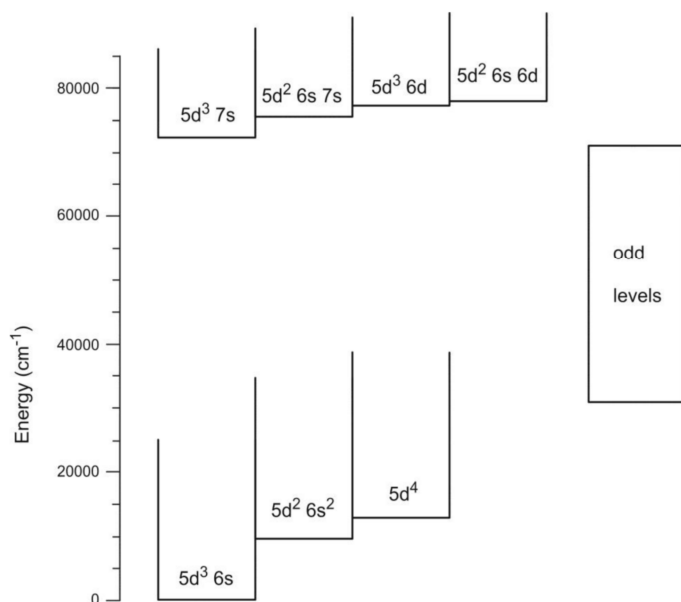


**Figure 3.** A blend situation of two Ta II lines. Red line: FT spectrum, black line: simulation, FWHM 2.2 GHz. In the upper part, normalized hf spectra of both lines are shown. Both profiles, added with the percentage given in the figure, gave the simulated sum profile, which describes the observed structure quite well. Thus, both cg wavelengths can be determined with high accuracy from the FT spectrum.

A systematic investigation of Ta II lines in the FT spectra available in Graz was performed in the PhD work of Uddin [27]. The determination of the hf constants of Ta II levels, either from laser spectroscopic records of Ta II lines or from the hf patterns of Ta II lines in the FT spectrum, made it possible to determine quite accurate values of cg wavelengths. From the classified Ta II lines, lines with good signal-to-noise ratio (SNR) were selected in order to re-calculate the level energies. Using the obtained vacuum wave numbers, a transition matrix was built up, and, in a global least squares fit, values for the level energies were calculated, together with their statistical uncertainties. The result was published recently [25].

The even parity system of Ta II was investigated theoretically—based on the results given in ref. [25]—by Stachowska et al. [28] performing a semi-empirical analysis, which confirmed also the new high lying levels above  $72,000\text{ cm}^{-1}$  (Figure 4). For this analysis, an important point was to exclude energy levels given in literature but in reality not existing. This is sometimes very difficult,

especially if it could not be verified under which assumptions (which lines) the corresponding level was introduced.



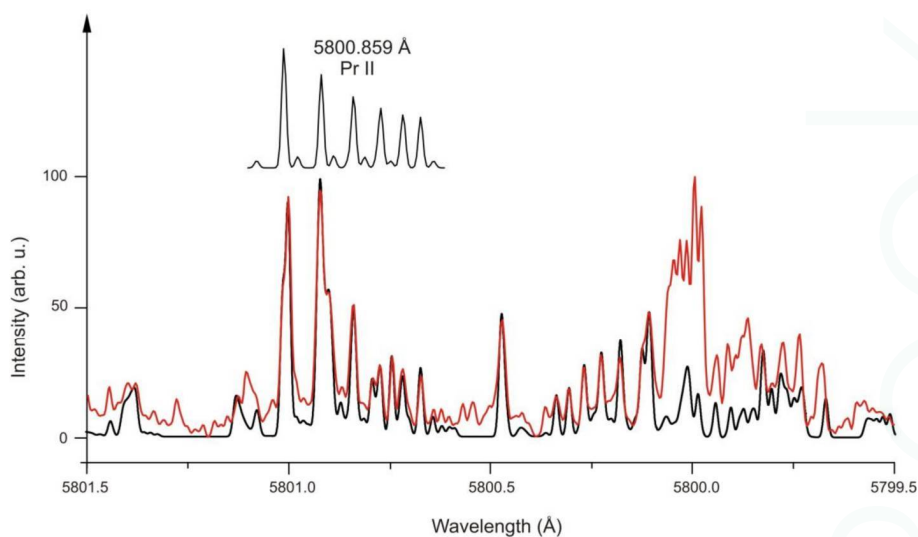
**Figure 4.** Simplified level scheme of Ta II. The theoretical analysis showed that the new even parity energy levels above  $72,000 \text{ cm}^{-1}$  belong to the configurations shown in the picture.

### 3. Pr II

First investigations of the hf structure of Pr II lines were performed in 1929 by White [29]. In 1941, Rosen et al. [30] investigated Zeeman patterns of Pr II lines and determined Landé factors and J values of 74 energy levels. Further progress in finding fine structure levels was made by Blaise et al. [31] in 1973. All available data on Pr energy levels (and of all other atoms of the lanthanide group) were collected by Martin et al. in 1978 [6]. The work of Blaise was continued by Ginibre [32–35], who achieved remarkable progress in the classification of Pr I and Pr II lines. She discovered a large number of previously unknown energy levels and determined their hf constants. In 2001, Ivarsson et al. [36] improved the wavelength accuracy of some Pr II lines of astrophysical relevance. Investigations of the hf structure and search for new energy levels were performed also by the groups in Hamburg [37] and Graz. First results were published in a common paper [38], but still many of the results achieved in Hamburg are still not published.

The available FT spectra of Pr ( $3260\text{--}9880 \text{ \AA}$ ) were taken by members of the group in Graz using an FT spectrometer in Hannover (group of Prof. Tiemann) and a hollow cathode lamp brought from Graz to Hannover. A first analysis of the spectra revealed more than 9000 previously unknown spectral lines of Pr I and Pr II, from which ca. 1200 could be classified as transitions between already known energy levels. During this first examination, 24 previously unknown energy levels were also discovered [9]. Later, these FT spectra were very helpful for laser spectroscopic investigations since the excitation wavelength could be set precisely to interesting peaks in the FT spectrum.

In between the list of spectral lines in the FT spectrum ca. 30,000 lines are contained, among them only 200 Ar lines and 650 Pr II lines. All other lines belong to the spectrum of neutral Pr (Pr I). In some spectral regions, the number of lines is so big that nearly no wavelength can be found at which the Pr plasma does not emit light. For example, the region around  $5800 \text{ \AA}$  is shown in Figure 5.



**Figure 5.** Part of an FT spectrum of Pr, using a direct current (DC) hollow cathode as light source (red line). As can be seen, there is nearly no wavelength at which the Pr plasma emits no light. The black curve shows a simulation taking into account all classified lines (FWHM 1.2 GHz). As can be seen (especially around 5800.0 Å), there are some quite dominant structures that are still not interpreted as transitions between known energy levels. Among the spectral lines, there is also one Pr II line (hf pattern shown in the upper part of the figure).

An overview concerning the already published newly discovered Pr I energy levels can be found in Ref. [39] and references therein.

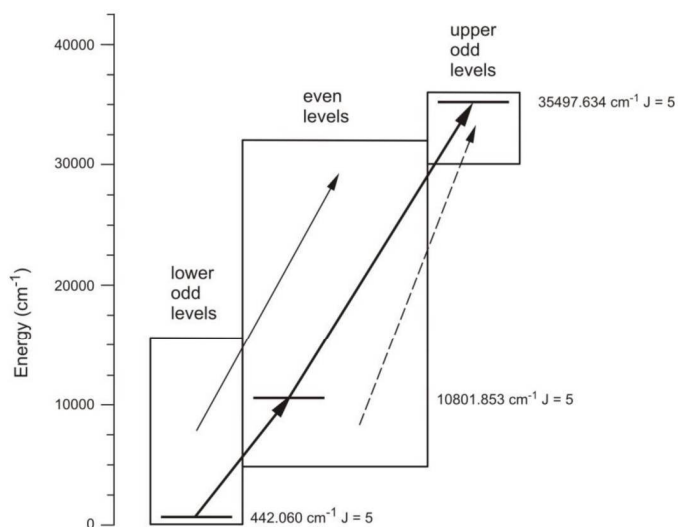
In contrary to Ta II, even and odd levels of Pr II are not separated by a large energy difference. Thus, for the determination of improved energy values, one first has to build up two transition matrixes separately. These two could then be connected by only one line, 4048.132. Even though this line had a low SNR of only 6, it must be used. A simplified level scheme is shown in Figure 6.

The FT spectra were also used to improve the accuracy of Pr II level energies. As can be seen from Figure 5, it may sometimes be tricky to find Pr II lines among the manifold of Pr I lines. Fortunately, in the blue and near infrared region, the identification becomes easier. Nevertheless, blend situations are quite frequently observed. As an example, in Figure 7, a blend of three lines is shown. In a more noisy spectrum or a spectrum with less resolution, one would notice only the dominant peak of the Pr I line at 5161.717 Å. Decomposing the observed pattern also allows for a precise determination of the cg wavelength of the involved Pr II line.

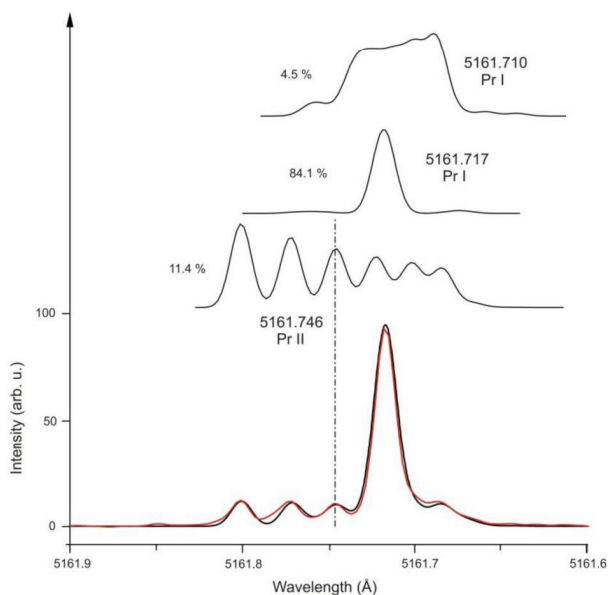
In Figure 8, a blend of two Pr II lines having nearly the same cg wavelength is shown. The wavelength difference is only 0.0025 Å (0.454 GHz or 0.015 cm<sup>-1</sup>). The observed structure is well reproduced by adding the profiles of the two Pr II lines.

The wavelength of selected Pr II lines were determined carefully and a global fit of the level energies was performed. The results are published in Ref. [40].

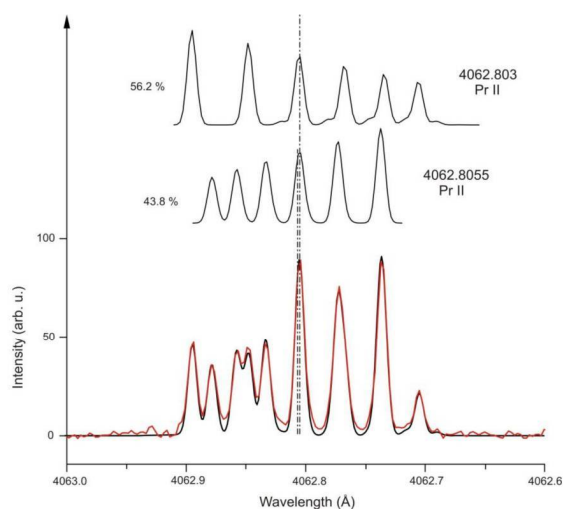
Beside laser spectroscopic experiments, in which the plasma of a hollow cathode discharge was used as source of free Pr atoms, highly precise investigations of the hyperfine structure of Pr II lines were also made using collinear laser-ion beam spectroscopy (CLIBS) [41]. Such experiments were also performed earlier by Rivest et al. [42]. During the last time, CLIBS investigations were performed in the presence of a magnetic field in order to re-determine the Landé g<sub>J</sub>-factors of the involved levels [43,44].



**Figure 6.** Simplified level scheme of Pr II. All transitions from lower odd levels to high-lying even levels are symbolized by the thin full arrow, all from the even levels to the upper odd levels by the dashed arrow. Only one ladder (bold arrows) could be found, which allowed for combining the two sub-systems of transitions.



**Figure 7.** Blend of a Pr II line and two Pr I lines. Red line: FT spectrum, black line: simulation, FWHM 1.6 GHz). Knowing the hf constants of the involved levels, the cg wavelengths of all lines can be determined. In a less resolved spectrum, only the strong peak of the Pr I line at 5161.717 Å would be noticeable.



**Figure 8.** A blend situation of two Pr II lines with nearly the same cg wavelength. Red line: FT spectrum, black line: simulation, FWHM 1.6 GHz. In the upper part, normalized hf spectra of both lines are shown. Both profiles, added with the percentage given in the figure, gave the simulated sum profile (black), which describes the observed structure quite well. Thus, both cg wavelengths can be determined with high accuracy from the FT spectrum.

#### 4. La II

Energy levels of La are also listed in Ref. [6]. Precise values of the hf structure constants of low lying metastable levels were obtained by a CLIBS technique by Höhle et al. [45] in 1982. These and other data were the basis of a theoretical interpretation of the hf structure of La II by Bauche et al. [46]. Later, CLIBS methods were also used by Li [47], Li [48], and Liang [49]. Some hf constants were determined by Lawler et al. [50] using an FT spectrum. Laser spectroscopic investigations of La II lines were made by Furmann et al. [51,52].

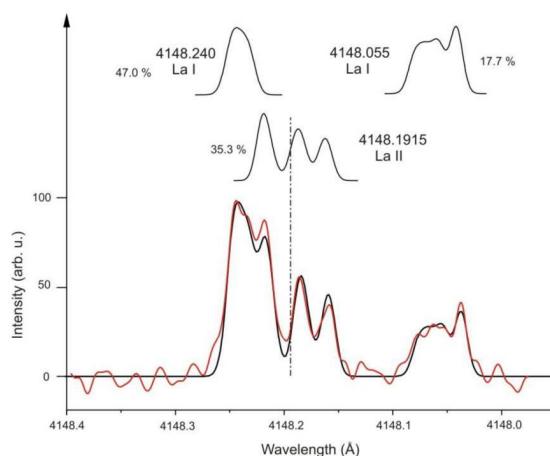
The FT spectra available in Graz (3225–16,600 Å) were taken in the group of Ferber (Laser Centre, University of Latvia, Riga, Latvia) with support of Kröger (Hochschule für Technik und Wirtschaft, Berlin, Germany). The near infrared part was analyzed in co-operation with the group of Basar (Physics Department, Istanbul University, Istanbul, Turkey). This was the first investigation of a La spectrum at wavelengths higher than 10,600 Å (investigated spectral range 8330–16,600 Å) [10]. The spectra were calibrated carefully using Ar II spectral lines. This allowed, together with the knowledge of the hf constants of the involved levels, a precise determination of transition wavelengths. From these values, improved energy values were determined. The results are submitted for publication [53]. Laser spectroscopy was performed in Graz mainly on atomic lines of La. These investigations are supported from the theoretical side by the group of Dembczyński (Institute of Materials Research and Quantum Engineering, Poznań University of Technology, Poznań, Poland).

As in the case of Pr, in the La spectrum blend situations are also observed quite frequently, despite the fact that the number of lines appearing in the spectra is lower (ca. 10,500). Figure 9 shows a typical blend situation.

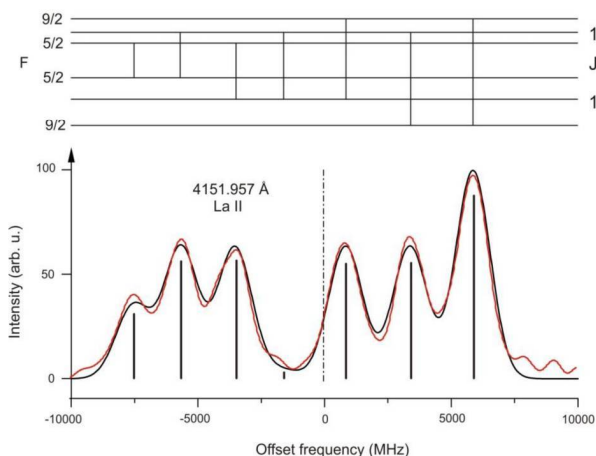
Figure 10 shows an example for a La II line with widely split hf components. The line at 4151.957 Å is split into two groups of components. Since all components are well resolved, at such line, an independent determination of the hf constants of both combining levels is possible.

Additionally, Zeeman patterns of La II lines were investigated using a hollow cathode discharge in the presence of a magnetic field [54].





**Figure 9.** Blend of a La II and a La I line. Close to the blended lines another La I line appears. Red line: FT spectrum, black line: simulation, FWHM 2.4 GHz. Despite the fact that the signal-to noise ratio (SNR) is small (only 16 for the highest peak), the transitions can be clearly identified and their cg wavelength can be determined with good accuracy.



**Figure 10.** Example of a La II spectral line. Red line: FT spectrum, black line: simulation, FWHM 1.6 GHz. Also shown is the hf level scheme, the transitions and the components (theoretical intensity ratios).

### 5. Conclusions

Improved level energies of Ta II, Pr II, and La II were published. This paper is concerned with some peculiarities that had to be taken into account for an improvement of the energy values.

**Acknowledgments:** The author would like to thank all persons who contributed to the work described in the present article. Special thanks are devoted to G.H. Guthöhrlein, Universität der Bundeswehr Hamburg (Germany), for a very fruitful co-operation for more than 25 years. The work was theoretically supported by the group of J. Dembczyński, University of Technology, Poznań (Poland). Special thanks are devoted to W. Ernst, the present head (since 2002) of the Institute of Experimental Physics, Graz University of Technology, Graz, Austria, for allowing me to keep a room and a laser spectroscopy lab after my retirement (2014).

**Conflicts of Interest:** The author declares no conflict of interest.

Appendix A

Table A1. Classification of the lines shown in the figures and data of the involved energy levels. Cols.: columns, Sp.: spectrum, tw: this work.

Fig. No.	Sp.	Line		Upper level						Lower level						References to Cols.			
		Wavelength (Å)	SNR	J	P	A (MHz)	B(MHz)	Energy (cm <sup>-1</sup> )	J	P	A (MHz)	B(MHz)	Energy (cm <sup>-1</sup> )	J	P	A (MHz)	B(MHz)	5,10	8,9
1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17			
1	Ta II	3127.748	86	41708.994	5	o	914(5)	350(100)	9746.376	4	e	303(10)	1680(300)	[25]	[25]	[25]			
1	Ta I	3127.864	30	31961.442	5/2	o	1243(3)	740(10)	0	3/2	e	509.084(1)	-1012.238(8)	[18]	tw	[55]			
2	Ta II	3487.803	21	54048.682	5	o	650(10)	1200(200)	25385.546	4	e	730(20)	0(200)	[25]	[25]	[25]			
3	Ta II	3037.503	39	39743.636	4	o	955(5)	-1200(100)	6831.437	3	e	360(10)	970(200)	[25]	[25]	[25]			
3	Ta II	3037.532	17	46387.287	2	o	1802(15)	-130(50)	13475.416	1	e	-480(4)	724(20)	[25]	[25]	[21]			
5	Pr II	5800.859	16	17676.112	5	e	805	-	442.060	5	o	1910.3(21)	-	[40]	[34]	[42]			
7	Pr I	5161.710	15	33932.700	13/2	o	737(1)	-	14564.673	13/2	e	577(2)	-	[38]	[38]	[37]			
7	Pr I	5161.717	280	29899.954	17/2	o	529(1)	-	10531.951	17/2	e	546(3)	-	[38]	[38]	[38]			
7	Pr II	5161.746	38	23261.402	5	e	581.9(3)	-19(5)	3893.46	6	o	902.1	-	[40]	[41]	[34]			
8	Pr II	4062.803	55	28009.828	7	e	556.5(7)	-34(25)	3403.226	6	o	-146.5(4)	-	[40]	[41]	[42]			
8	Pr II	4062.8055	34	27604.990	6	e	597.0(5)	1(32)	2998.412	7	o	1435.2(16)	-	[40]	[41]	[42]			
9	La I	4148.055	6	33820.316	1/2	o	-232.7(60)	-	9719.429	3/2	e	-655.138	-33.249	tw	[56]	[57]			
9	La II	4148.1915	12	51524.005	2	e	-220(3)	-	27423.911	1	o	886.9(15)	-18.9(48)	[53]	[53]	[49]			
9	La I	4148.240	16	38903.885	5/2	e	181(3)	-	14804.067	5/2	o	335.01(74)	23.64(95)	[58]	[58]	[59]			
10	La II	4151.957	24	25973.360	1	o	547.3(30)	27(7)	1895.128	1	e	-1128.1(0.9)	49.8(65)	[53]	[52]	[45]			

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Article

# Hyperfine Structure and Isotope Shifts in Dy II

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Academic Editor: Joseph Reader

Received: 8 December 2016; Accepted: 13 January 2017; Published: 20 January 2017

**Abstract:** Using fast-ion-beam laser-fluorescence spectroscopy (FIBLAS), we have measured the hyperfine structure (hfs) of 14 levels and an additional four transitions in Dy II and the isotope shifts (IS) of 12 transitions in the wavelength range of 422–460 nm. These are the first precision measurements of this kind in Dy II. Along with hfs and IS, new undocumented transitions were discovered within 3 GHz of the targeted transitions. These atomic data are essential for astrophysical studies of chemical abundances, allowing correction for saturation and the effects of blended lines. Lanthanide abundances are important in diffusion modeling of stellar interiors, and in the mechanisms and history of nucleosynthesis in the universe. Hfs and IS also play an important role in the classification of energy levels, and provide a benchmark for theoretical atomic structure calculations.

**Keywords:** laser spectroscopy; ionized atoms; hyperfine structure; isotope shifts

## 1. Introduction

Accurate elemental abundances in stars and the interstellar medium are essential for understanding stellar formation, evolution, and structure. Deriving abundances from stellar spectra requires accurate atomic data: tabulated spectra of several ionization states (usually I–III), oscillator strengths, hyperfine structure (hfs), and isotope shifts (IS). Even though hfs and IS are too small to be resolved in most astrophysical spectra because of Doppler and rotational broadening, they contribute to the overall profile of a spectral line; extracting the elemental abundance from a line often requires a knowledge of the hfs to correct for saturation [1], and ignoring the underlying structure arising from hfs and IS can lead to errors as large as two to three orders of magnitude [2]. In addition, there can be errors in the determination of rotational, microturbulent and macroturbulent velocities from Fourier analysis of line profiles, and unknown shifts in wavelengths of saturated lines [3]. The lanthanides are particularly important because they provide a contiguous sequence of observable elements in which patterns of abundance may be observed and related to nucleosynthesis and chemical fractionation [4]. In this paper, we present new measurements of hfs and IS in Dy II, one of the lanthanide elements that is used to understand these processes.

The main mechanisms of neutron capture by which elements beyond  $^{56}\text{Fe}$  are formed are the *r*-process and *s*-process, named by whether the rate of neutron capture is rapid or slow compared to the rate of  $\beta$ -decay [5]. The *s*-process is believed to take place in thermally pulsing asymptotic giant branch (AGB) stars [6], whereas the *r*-process requires the high neutron density characteristic of supernovas. Comparison of the elemental composition of a star with theoretical *r*- or *s*-process models gives information about the nature of these processes and about the environment in which the star formed. The observed ratio of the abundances of a pair of unstable and stable *r*-process elements, e.g.,  $[\text{Th}]/[\text{Eu}]$ , can yield the age of the star when compared with the theoretical production ratio [7]. There are several recent studies of abundances in very metal-poor stars, which are believed to have

formed from the debris of the very first generation of initially metal-free massive stars (Population III). These studies shed light on the earliest nucleosynthesis of heavy elements in the universe and how they were incorporated into later stars [8,9]. CH stars, which are deficient in Fe and enhanced in C and s-process elements, obtained their heavy elements by mass transfer from now-unseen white dwarf binary companions when the latter were in the AGB stage of evolution. Thus the composition of CH stars reveals information about AGB synthesis of s-process elements [10].

Accurate abundance information is also required in the study of diffusion processes within stars, where chemical fractionation occurs due to a combination of gravity, convection and radiation pressure. The chemically peculiar (CP) stars exhibit typically large lanthanide abundance excesses relative to solar and meteoritic values, and the abundance pattern expected from nucleosynthesis may be greatly perturbed [4]. One of the most exciting recent developments in stellar astrophysics has been the rapid expansion of the field of asteroseismology [11], in which the observation of natural, resonant oscillations provides information about stellar interiors and evolution. These observations can be photometric or velocity measurements from Doppler shifts. In the latter case, it is essential to be able to model spectral line shapes accurately, requiring good atomic data.

Extensive spectroscopy of Dy II has been done principally by Conway and Worden [12], Wyart [13–15], and more recently by Nave and Griesmann [16], who pointed out the complexity of lanthanide spectra due to the large number of terms arising from the unfilled  $4f$  shell and the fact that  $4f$ ,  $5d$ , and  $6s$  electrons all have similar binding energies. The NIST Atomic Spectra Database [17] lists 576 levels of which a significant number are only partly classified as to principal configuration and term, and configuration mixing is common. One of the tools that has been used to aid in level classification is IS, since the ‘field shift’ part of the IS (the dominant contribution in heavy atoms) depends on the electron density at the nucleus and therefore is a function of the electronic states involved in a transition. Early measurements of IS were carried out by Pacheva and Abadjieva [18]. Aufmuth [19] measured IS for Dy isotopes 162–164 in 29 lines of Dy II in order to check the mixing of three configurations calculated by Wyart [13–15]. Ahmad et al. [20] measured the IS of 62 spectral lines, three of which overlap with our measurements. The only previous report of hfs is by Murakawa and Kamei [21].

## 2. Experimental Setup

The FIBLAS method [22] we use is very well suited to the measurement of the detailed structure within an atomic transition because of the high spectral resolution (full-width-half-maximum linewidths of  $\sim 100$  MHz), the high wavelength selectivity of a narrow-band laser, and the ability to mass-select the targeted ions in the fast beam. The transition linewidths are a combination of the natural width (here 20–70 MHz), and Doppler broadening from the ion source, significantly narrowed for fast ions by ‘kinematic compression’ [23]. The hfs and IS of an optical transition are often completely resolved, a goal difficult to achieve in other techniques, such as Fourier transform spectroscopy.

In our apparatus, Dy<sup>+</sup> ions are created using a Penning sputter ion source, engineered by us to yield a small energy spread of a few eV in the extracted beam [24,25]. Another important feature is the large population of metastable ions in the beam with energies up to  $\sim 22,000$  cm<sup>-1</sup>, greatly enhancing the number of transitions we can observe. The use of sputtering rather than thermal evaporation makes the source universal for any solid conducting element in the periodic table; this is a great advantage for the lanthanides and many other refractory metals of astrophysical importance. A discharge in the Ne support gas is easily struck at anode-cathode potentials of several hundred volts, with the discharge current regulated at 60 mA. Our experience with lanthanides is that there is an initial period of conditioning (up to 2 h), during which the potential drops to  $\sim 200$ – $300$  V, and the extracted ion current, as measured in a downstream Faraday cup, rises sharply to  $\sim 200$  nA. We attribute this behavior to sputter-cleaning of the surfaces of the lanthanide cathode and anticathode to remove oxide layers, which form easily in air.

After initial acceleration to energies of 10–12 keV, the ion beam is focused by an einzel lens, steered, and mass-selected using a Wien filter. Removal of the large  $\text{Ne}^+$  current from the beam reduces space-charge spreading and significantly lowers the collision-induced background fluorescence. The mass resolution of the Wien filter was selected by adjustment of its electric field to reject the Ne ions, while transmitting nearly equally the seven stable isotopes of Dy (see Table 1) to allow IS measurement. The mass-selected beam is then horizontally deflected by  $5^\circ$  to make it collinear with the laser beam. After further focusing and steering, the ions are accelerated by 478 eV into a ‘Doppler tuning’ region; this energy boost ensures the laser-induced fluorescence (LIF) is mainly confined to this region, from which it is transmitted out of the vacuum chamber by an array of optical fibers to a photomultiplier equipped with a short-pass filter. The filter allows rejection of the scattered laser light while transmitting most of the LIF, since the lower (metastable) energy states of the laser-induced transitions we observed ranged from  $\sim 4300 \text{ cm}^{-1}$  to  $22,000 \text{ cm}^{-1}$ .

**Table 1.** Properties of the Dy isotopes.  $I$ ,  $\mu$ , and  $Q$  are the nuclear spin, magnetic dipole moment, and electric quadrupole moment, respectively.

Isotope	Mass (u) <sup>a</sup>	Abundance (%) <sup>b</sup>	$I$ <sup>c</sup>	$\mu$ (nm) <sup>c</sup>	$Q$ (b) <sup>c</sup>
$^{156}\text{Dy}$	155.924278	0.06	0		
$^{158}\text{Dy}$	157.924405	0.10	0		
$^{160}\text{Dy}$	159.925194	2.34	0		
$^{161}\text{Dy}$	160.926930	18.91	5/2	−0.480 (3)	+2.51 (2)
$^{162}\text{Dy}$	161.926795	25.51	0		
$^{163}\text{Dy}$	162.928728	24.90	5/2	+0.673 (4)	+2.318 (6)
$^{164}\text{Dy}$	163.929171	28.18	0		

<sup>a</sup> Reference [26]; <sup>b</sup> Reference [27]; <sup>c</sup> Reference [28].

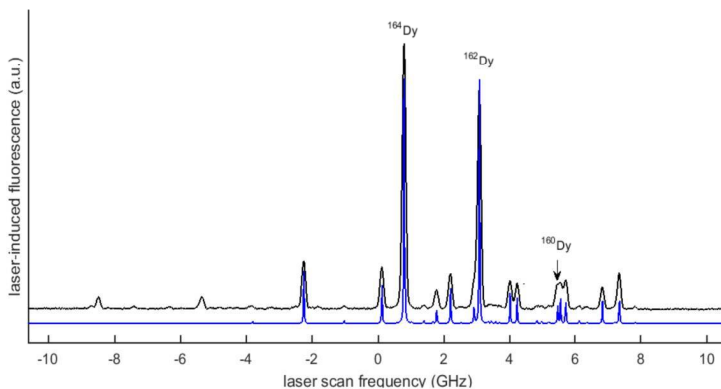
The laser system is a single-mode ring dye laser operating with Stilbene 420 dye, whose usable output range is  $\sim 420 \text{ nm}$  to  $460 \text{ nm}$ . It is pumped with the all-lines UV output of an Ar-ion laser, and is frequency stabilized to a few MHz. The dye laser wavelength is monitored to  $\sim 1$  part in  $10^7$  by a traveling-mirror Michelson interferometer [29] using a polarization-stabilized HeNe laser as a reference. The laser beam is loosely focused to a waist located approximately in the Doppler-tuning region. Before starting the laser scan across the hfs/IS components of a transition, the laser frequency is manually tuned to the absorption line of  $^{162}\text{Dy}$ , which is the even isotope (i.e., without hfs) closest to the mean mass of the stable isotopes. The overlap of the laser and ion beams is optimized by adjusting steering and focusing of the ion beam. This results in a scan where the peak intensities of the even isotopes approximately match their standard abundances, facilitating subsequent analysis of the spectrum. During the scan, a computer steps the laser frequency over the entire spectrum of the line ( $<20 \text{ GHz}$ ) in intervals of  $\sim 1/10$ th of a linewidth with a dwell time of typically 250 ms. The computer simultaneously records the LIF signal along with the ion beam current, laser beam power, and a calibration signal that corrects for the nonlinearity ( $\sim 2\%$ ) of the laser scan. This calibration signal is obtained using a set of markers generated by a plane-parallel Fabry-Perot interferometer with a free spectral range of 665.980 MHz, which is used to convert channel number into laser frequency difference.

Because the Dy II hfs is complicated by the existence of an unusually large electric quadrupole interaction, we introduced some redundancy to the data in order to allow checks on the robustness of the analysis. This was done by taking spectra with the laser beam both parallel (P) and antiparallel (A) to the ion beam, and by changing the ion-beam energy. Both of these measures change the large Doppler shift for each isotope, resulting in significant changes in the appearance of the measured spectrum. This can result in a P (or A) spectrum that is much less congested than its counterpart, greatly facilitating the analysis (see below).



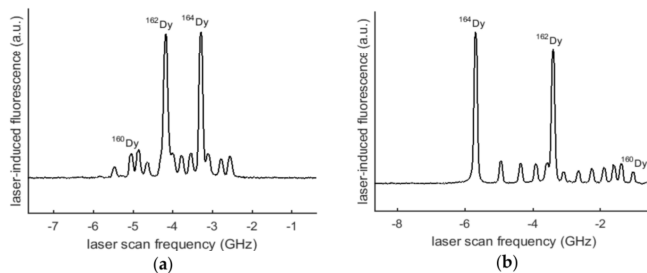
### 3. Data and Analysis

A typical spectrum with fully resolved hfs and IS is shown in Figure 1, in which the ‘stick figure’ below the data shows the fitted peak locations. At the left of the figure, a number of peaks belonging to another, weaker transition can be seen. The spectra in which such blends occurred are noted in the IS table below by asterisks. The relative intensities of the extra transitions ranged from 1% to 15%, except in the case of the 443.100 nm line, for which two nearly equal-intensity transitions were seen, precluding analysis. The peaks corresponding to  $^{156}\text{Dy}$  and  $^{158}\text{Dy}$  were too small to be seen above the noise in our spectra and were not included in the analysis.



**Figure 1.** Laser-induced fluorescence spectrum of the transition  $4f^{10}(^5I_6)6s_{1/2} (6, ^1/2)_{13/2} - 4f^{10}(^5I)6p^{\circ}_{13/2}$  at 438.430 nm in Dy II. The laser beam and ion beam were in parallel geometry. The observed spectrum (upper curve) is a single scan of 1024 channels at a dwell time of 400 ms per channel. The photomultiplier signal current for the  $^{164}\text{Dy}$  peak was  $\sim 80$  nA on a background of  $\sim 10$  nA due to collisionally-induced light. The observed FWHM linewidth was 98.8 MHz, which includes the 10.6 MHz natural width. The lower ‘stick figure’ (blue online) shows the positions and amplitudes of the fitted components, and has been displaced vertically for clarity. The hfs components of  $^{161}\text{Dy}$  and  $^{163}\text{Dy}$  are not individually annotated. It is important to understand that the separations between peaks of different isotopes arise from a combination of IS and relative Doppler shift. Note that the components of a second, partially blended, transition are visible on the left side.

Figure 2a,b show another transition observed in both P and A modes to demonstrate the ‘decongestion’ that occurs in one of these modes.



**Figure 2.** Laser-induced fluorescence spectrum of the transition  $4f^9(^6H^{\circ})5d(^7I^{\circ})6s^8I_{17/2}^{\circ} - 4f^9(^6H^{\circ})5d(^7H^{\circ})6p_{15/2}$  at 436.135 nm in Dy II, showing the advantage of viewing the same transition in two different laser beam/ion beam geometries: (a) Anti-parallel; (b) Parallel.

It is important to note that in the large separation  $\Delta\nu_\ell$  any pair of peaks corresponding to two different isotopes shown in these spectra is predominantly a *differential Doppler shift* arising from the slightly different velocity of each isotope. In the A (P) mode, driving a transition whose rest-frame frequency is  $\nu_0$  requires a laser frequency  $\nu_\ell$  given by

$$\nu_\ell = \nu_0 \left( \frac{1 \mp \beta}{1 \pm \beta} \right)^{1/2} \quad (1)$$

where  $\beta = (2eV/Mc^2)^{1/2}$  for a singly-charged ion of mass  $M$  accelerated from rest through a potential difference  $V$ . Thus, the ion-rest-frame peak separation  $\Delta\nu_0$  (which is the IS within a sign) for a pair of masses  $M$  and  $M'$  is related to  $\Delta\nu_\ell$  by

$$\Delta\nu_\ell = \Delta\nu_0 \left( \frac{1 \mp \beta'}{1 \pm \beta'} \right)^{1/2} + \nu_0 \left[ \left( \frac{1 \mp \beta'}{1 \pm \beta'} \right)^{1/2} - \left( \frac{1 \mp \beta}{1 \pm \beta} \right)^{1/2} \right] \quad (2)$$

(This formula may also be applied to the separation of a pair of hf peaks of the same mass by setting  $\beta' = \beta$ .) Creating the model spectrum to be fit to the data thus requires knowledge of the kinetic energy of the fast ions, which depends on the potential in the ion source, the extraction voltage, and the potential in the Doppler-tuning region. It is possible to determine the beam energy directly by measuring the Doppler-shifted wavenumber of a given spectral line in both A and P modes; a simple calculation with Equation (1) yields the velocity of the isotope corresponding to that spectral line as well as the transition wavenumber in the ion rest frame. Such measurements have shown that the beam energy is, within ~1 eV, just the sum of the anode-cathode potential difference  $V_{ac}$  (the power-supply potential difference  $V_{supply}$  minus the 58.5 V drop across a 1 k $\Omega$  stabilizing ballast resistor) and the 10 kV or 12 kV extraction voltage, minus the potential in the central region of the Doppler-tuning region (–478 V), determined from its applied voltage using a numerical solution of Laplace’s equation. This implies that the plasma region in which the ions are created is at the potential of the anode. In order to account for the Doppler shifts in a spectrum, we thus needed to monitor only  $V_{supply}$  during the few minutes of a scan. Typically,  $V_{supply}$  varied by <1 V in the current-regulated plasma, and only such scans were used as data.

The model used in the least-squares fit makes use of the standard formula [30] for the hyperfine contribution to the energy of a level with a nuclear spin  $I$ , an electronic angular momentum  $J$ , and a total angular momentum  $F$ , containing magnetic-dipole and electric-quadrupole terms, with parameters  $A$  and  $B$ , respectively:

$$\nu_{\text{hfs}}(F) = \frac{1}{2}AK + \frac{1}{2}B \frac{3K(K+1) - 4I(I+1)J(J+1)}{2I(2I-1)2J(2J-1)} \quad (3)$$

where  $K = F(F+1) - I(I+1) - J(J+1)$ . The amplitudes of the model peaks are constrained by the standard abundances of the isotopes, and, also, for the odd isotopes displaying hfs, by standard angular momentum recoupling coefficients:

$$a(F, F') \propto (2I+1)^{-1}(2F+1)(2F'+1) \left\{ \begin{matrix} F' & F & 1 \\ J & J' & I \end{matrix} \right\}^2 \quad (4)$$

where the primes (non-primes) indicate the upper (lower) level of a transition. A further constraint was the use of known ratios (see Table 1) of the nuclear magnetic moments and electric quadrupole moments of the odd isotopes  $^{161}\text{Dy}$  and  $^{163}\text{Dy}$ , so that the hfs of only one isotope needed to be fit. We are thus neglecting the hyperfine anomaly, which is expected to be small compared to our measurement uncertainty. The experimental lineshapes combine natural broadening with asymmetric Doppler broadening, arising mainly from the unknown potential distribution in the source plasma; we interpret the ‘tail’ of slower-energy ions as those created in the ‘cathode fall’ region. In the course

of data analysis, we observed that an asymmetric Lorentzian profile improved the consistency of the data. We note that the peak frequency differences determining the IS and hfs constants are insensitive to the detailed lineshape model used.

In addition to the four observable IS (measured with  $^{164}\text{Dy}$  as the reference) and four hfs constants for a given transition, other adjustable parameters in the fit included the overall frequency offset, overall amplitude, background, linewidth, asymmetry, and laser power (to account for saturation). The large electric quadrupole contribution to the hfs created splittings very different from the standard ‘flag’ pattern obtained when the magnetic dipole interaction dominates. Without the help of pattern recognition, it was necessary to use trial and error along with global fitting algorithms, searching across up to six parameters to find a fit. Another issue was that the pattern of a spectrum was dependent mainly on the differences  $B'-B$  and  $A'-A$ , with only subtle changes in the fit spectrum resulting from varying the individual values of the constants. Thus, as an intermediate measure, the search space could be reduced by fixing the constants associated with either the lower or upper energy level. A very important factor in breaking these parameter correlations is the ability to measure the relatively weak satellite peaks ( $\Delta F \neq \Delta J$ ) in the hyperfine spectra, since the frequencies of these peaks depend algebraically on the four hfs constants rather differently than for the principal peaks ( $\Delta F = \Delta J$ ). We also dealt with these correlations experimentally by repeating measurements of most transitions at different beam energies (10 keV and 12 keV) and different relative beam orientations (A and P modes). In four cases, the satellite peaks were not visible, with the result that the associated hfs constants were not individually well-determined, but are rather to be regarded as a set of ‘effective’ parameters that reproduce the principal peaks of the observed spectrum very well so as to be of practical use in modeling astrophysical spectra.

The resulting hfs constants for six lower and eight upper levels are given in Table 2, while Table 3 lists the effective hfs parameters for the four transitions referred to above. For the levels listed in Table 2, we were able to use several transitions to determine the hfs constants in each case, providing important ‘cross-checks’; however, the levels in Table 3 were only accessible using the transitions listed.

**Table 2.** Hyperfine structure constants of levels of  $^{161}\text{Dy}$  II and  $^{163}\text{Dy}$  II derived from transitions where satellite peaks are well fit.  $A$  and  $B$  are the magnetic dipole and electric quadrupole constants, respectively.  $J$  is the total angular momentum. Energies of odd-parity levels are italicized.

Configuration <sup>a</sup>	Term <sup>a</sup>	$J$ <sup>a</sup>	Energy <sup>a</sup> ( $\text{cm}^{-1}$ )	$A$ ( $^{161}\text{Dy}$ ) (MHz)	$B$ ( $^{161}\text{Dy}$ ) (MHz)	$A$ ( $^{163}\text{Dy}$ ) (MHz)	$B$ ( $^{163}\text{Dy}$ ) (MHz)
$4f^{10}(\overset{5}{I}_7)6s_{1/2}$	(7, 1/2)	15/2	4341.104	-251.89 (94)	1045 (48)	352.6 (1.3)	1104 (46)
$4f^{10}(\overset{1}{I}_6)6s_{1/2}$	(6, 1/2)	13/2	7485.117	93.22 (16)	-883.4 (7.1)	-130.48 (22)	-933.1 (7.5)
$4f^{10}(\overset{3}{F}_5)6s_{1/2}$	(5, 1/2)	11/2	13,338.27	-272.49 (23)	-818 (10)	381.44 (32)	-864 (11)
<i><math>4f^9(^6\text{H}^\circ)5d(\overset{7}{K}^\circ)6s</math></i>	$^8\text{K}^\circ$	19/2	17,606.65	-144.40 (30)	4081 (17)	202.13 (41)	4310 (18)
<i><math>4f^9(^6\text{H}^\circ)5d(\overset{7}{K}^\circ)6s</math></i>	$^6\text{K}^\circ$	19/2	19,571.75	-69.51 (35)	3861 (24)	97.29 (49)	4078 (25)
<i><math>4f^9(^6\text{H}^\circ)5d(\overset{3}{F})</math></i>	$^\circ$	11/2	20,517.39	-96.98 (37)	2076 (17)	135.76 (52)	2193 (18)
<i><math>4f^9(^6\text{H}^\circ)5d(\overset{3}{P})</math></i>	$^\circ$	15/2	27,435.132	-97.23 (12)	252.8 (7.1)	136.10 (17)	267.1 (7.5)
<i><math>4f^9(^6\text{H}^\circ)5d(\overset{3}{F})</math></i>	$^\circ$	13/2	28,019.70	-114.76 (56)	1104 (37)	159.67 (78)	1166 (39)
<i><math>4f^{10}(\overset{5}{I})6p</math></i>	$^\circ$	13/2	30,287.36	278.44 (18)	-973.9 (7.3)	-389.76 (25)	-1028.6 (7.7)
<i><math>4f^{10}(\overset{5}{I})6p</math></i>	$^\circ$	9/2	36,466.34	-110.97 (24)	801 (14)	155.34 (33)	846 (15)
<i><math>4f^9(^6\text{H}^\circ)6s6p(\overset{3}{P}^\circ)</math></i>	$^\circ$	17/2	40,455.73	-165.08 (32)	3851 (17)	231.08 (44)	4067 (18)
<i><math>4f^9(^6\text{H}^\circ)5d(\overset{7}{H}^\circ)6p</math></i>	$^\circ$	17/2	41,583.90	-102.69 (31)	1826 (18)	143.75 (43)	1929 (19)
<i><math>4f^9(^6\text{H}^\circ)5d(\overset{7}{H}^\circ)6p</math></i>	$^\circ$	13/2	42,289.33	-96.92 (45)	2773 (38)	135.67 (63)	2929 (40)
<i><math>4f^9(^6\text{H}^\circ)5d(\overset{7}{H}^\circ)6p</math></i>	$^\circ$	19/2	42,478.98	-113.16 (42)	3099 (24)	158.40 (59)	3273 (26)

<sup>a</sup> Reference [17].

Table 4 presents the IS for 12 transitions, using the standard sign convention that  $IS \equiv \nu_{M'} - \nu_M$  where  $M' > M$ . The uncertainties in the data arise from the curve-fitting procedure, the residual non-linearity of the laser scan, and small drifts in  $V_{ac}$ . Equation (2) can be used to calculate the sensitivity of the measured separation  $\Delta\nu_\ell$  of two spectral peaks to the accuracy of the ion-beam energy eV, and to drifts in that energy during a scan. If the drift is zero,  $d(\Delta\nu_\ell)/dV$  is completely negligible for two hyperfine (hf) peaks of the same mass, and is  $\sim 0.15$  MHz/V for peaks of the isotope pair (160, 164).

Since we know  $V$  to  $\sim 1$  V, this effect is negligible compared to fitting errors. If the drift is non-zero, the sensitivity for any pair of peaks is  $\sim 12$  MHz/V for typical values of  $\nu_0$  and the beam energy. For the hf spectrum of a given isotope, the effect of a drift is taken into account by the fitting error since the many hf peaks are fit with only four hf parameters. For the same reason any residual non-linearity in the frequency scale is also subsumed in the fitting error. However, drift in  $V$  can contribute an error to the IS data, just as non-linearity can. Accordingly, we have added a contribution to the error budget of the IS of 10 MHz to account for both of these effects. We present evidence (see below) that this estimate is conservative.

**Table 3.** Hyperfine structure constants of transitions of  $^{161}\text{Dy II}$  and  $^{163}\text{Dy II}$  where satellite peaks are not well fit.  $A$  and  $B$  are the magnetic dipole and electric quadrupole constants, respectively.  $J$  is the total angular momentum. Energies of odd-parity levels are italicized.

$\lambda_{\text{air}}^a$ (nm)	Configuration <sup>b</sup>	Term <sup>b</sup>	$J^b$	Energy <sup>b</sup> ( $\text{cm}^{-1}$ )	$A$ ( $^{161}\text{Dy}$ ) (MHz)	$B$ ( $^{161}\text{Dy}$ ) (MHz)	$A$ ( $^{163}\text{Dy}$ ) (MHz)	$B$ ( $^{163}\text{Dy}$ ) (MHz)
424.846	$4f^9(^6\text{H}^\circ)5d(^7\text{H}^\circ)6s$	$^8\text{H}^\circ$	11/2	<i>14,347.205</i>	-63.33 (91)	1905 (37)	88.7 (1.3)	2012 (39)
	$4f^9(^6\text{H}^\circ)6s6p(^3\text{P}^\circ)$		13/2	37,878.55	-26.0 (1.4)	1552 (31)	36.4 (2.0)	1639 (32)
436.135	$4f^9(^6\text{H}^\circ)5d(^7\text{F}^\circ)6s$	$^8\text{F}^\circ$	17/2	<i>14,895.06</i>	-94.86 (79)	2106 (60)	132.8 (1.1)	2224 (64)
	$4f^9(^6\text{H}^\circ)5d(^7\text{H}^\circ)6p$		15/2	37,817.31	-65.15 (91)	1598 (59)	91.2 (1.3)	1688 (62)
451.851	$4f^9(^6\text{H}^\circ)5d(^2\text{F}^\circ)$	$^8\text{K}^\circ$	21/2	<i>22,031.98</i>	11.69 (73)	-1613 (50)	-16.4 (1.0)	-1704 (53)
	$4f^9(^6\text{H}^\circ)5d(^7\text{F}^\circ)6p$	$^8\text{K}^\circ$	21/2	44,156.98	-7.72 (73)	-503 (50)	10.8 (1.0)	-531 (53)
457.385	$4f^9(^6\text{H}^\circ)5d(^2\text{F}^\circ)$	$^8\text{K}^\circ$	17/2	<i>20,884.42</i>	68.32 (87)	-1358 (63)	-95.6 (1.2)	-1434 (66)
	$4f^9(^6\text{H}^\circ)5d(^7\text{H}^\circ)6p$		17/2	42,741.69	44.11 (88)	-1206 (63)	-61.7 (1.2)	-1274 (66)

<sup>a</sup> Reference [31]. <sup>b</sup> Reference [17].

**Table 4.** Isotope shifts in Dy II, denoted by mass pairs:  $(M, M')$ . The signs are determined by the convention that  $IS \equiv \nu_{M'} - \nu_M$  where  $M' > M$ .  $J_{\text{lo}}$ ,  $E_{\text{lo}}$  and  $J_{\text{up}}$ ,  $E_{\text{up}}$  are the total angular momentum and energy of the lower and upper levels of a transition, respectively.

$\lambda_{\text{air}}^a$ (nm)	$J_{\text{lo}}^a$	$E_{\text{lo}}^a$ ( $\text{cm}^{-1}$ )	$J_{\text{up}}^a$	$E_{\text{up}}^a$ ( $\text{cm}^{-1}$ )	(160, 164) (MHz)	(161, 164) (MHz)	(162, 164) (MHz)	(163, 164) (MHz)
422.203 *	15/2	4341.10	13/2	28,019.70	-610 (11)	-427 (10)	-306 (10)	-129 (10)
424.846 *	11/2	14,347.21	13/2	37,878.55	-960 (11)	-842 (11)	-456 (11)	-326 (10)
432.253 *	11/2	13,338.27	9/2	36,466.34	-1760 (11)	-1453 (10)	-857 (10)	-533 (10)
432.891	15/2	4341.10	15/2	27,435.12	-1204 (10)	-945 (10)	-591 (10)	-331 (10)
436.135 *	17/2	14,895.06	15/2	37,817.31	-1429 (10)	-1237 (11)	-694 (10)	-463 (11)
436.421	19/2	19,571.75	19/2	42,478.98	-1812 (10)	-1550 (10)	-870 (10)	-581 (10)
437.531	19/2	17,606.65	17/2	40,455.73	-108 (10)	-74 (10)	-52 (10)	-23 (10)
438.430 *	13/2	7485.12	13/2	30,287.36	-1457 (11)	-1175 (10)	-707 (10)	-408 (10)
451.851 *	21/2	22,031.98	21/2	44,156.98	-363 (10)	-334 (11)	-173 (10)	-133 (10)
454.167	19/2	19,571.75	17/2	41,583.90	-1759 (10)	-1506 (11)	-847 (10)	-565 (10)
457.385	17/2	20,884.42	17/2	42,741.69	-790 (11)	-700 (11)	-378 (10)	-272 (10)
459.178	11/2	20,517.39	13/2	42,289.33	-709 (11)	-628 (10)	-339 (10)	-244 (10)

<sup>a</sup> Reference [31]. \* These transitions contained unidentified blends whose relative intensities were  $<15\%$ . A spectrum at 443.100 nm contained a blend of two transitions of comparable relative intensity and could not be analyzed.

#### 4. Discussion and Conclusions

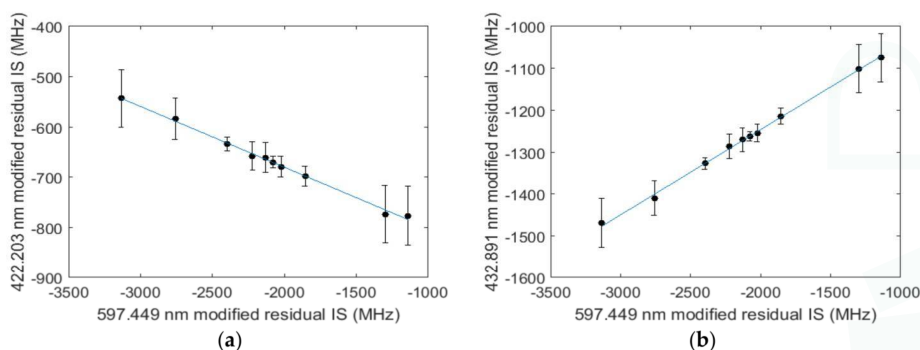
We have measured hfs parameters in 14 levels of Dy II, and effective hfs parameters in a further four transitions. There is no previous hfs data for these levels for comparison, but the very large magnitude of the electric quadrupole constants is consistent with measurements in Dy I [32]. Comparison with hfs measurements in isoelectronic  $^{159}\text{Tb I}$  is not useful as the electron configurations of the levels studied [33] are different from those in the present work, and also because the magnetic dipole and electric quadrupole moments are quite different from those of  $^{161}\text{Dy}$  and  $^{163}\text{Dy}$ .

Of the 12 transition ISs we measured, we can compare three with the data of Ahmad et al. [20] made with a Fabry-Perot spectrometer viewing a hollow-cathode discharge. As shown in Table 5, the agreement is excellent, and our results are more precise by an order of magnitude. None of the transitions measured by Aufmuth [19] overlap with our data.

**Table 5.** Comparison of IS measurements with previous work.

$\lambda_{\text{air}}$ (nm)	Mass Pair	IS (MHz)	
		This Work	Ahmad [20]
432.891	(160, 164)	−1204 (10)	−1268 (90)
436.421	(160, 164)	−1812 (10)	−1820 (90)
437.531	(160, 164)	−108 (10)	~0 (90)

Another check on our IS values is through the conventional King plot analysis [29] (Chapter 6). As a reference transition in the King plots, we used the 597.4 nm transition in Dy I, for which ISs have been measured [34,35] at a high accuracy (~2 MHz). Both fits were excellent straight lines (see Figure 3). That linearity reflects almost entirely the quality of *our* data since the errors we have ascribed to our IS measurements are about five times greater than those for the reference transition. This suggests that the uncertainty of 10 MHz that we have attached to our IS measurements to account for source-voltage drift and residual nonlinearity is conservative.



**Figure 3.** King plots of modified residual IS (see text) of pairs of transitions in Dy II and Dy I. The mass pair (160, 164) has been chosen as the reference, and points have been plotted for all unique pairs of isotopes. The straight line (blue online) is a linear least-squares fit. Note that the error bars in the horizontal direction are smaller than the data symbols. (a) King plot for the 422.201 nm vs. 597.449 nm transitions; (b) King plot for the 432.891 nm vs. 597.449 nm transitions.

**Acknowledgments:** We thank the Natural Sciences and Engineering Research Council of Canada for financial support. We thank Timothy J. Scholl for extremely helpful assistance with the laser system.

**Author Contributions:** All authors contributed equally to acquiring and analyzing data and writing the manuscript.

**Conflicts of Interest:** The authors declare no conflict of interest.

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Article

# Combining Multiconfiguration and Perturbation Methods: Perturbative Estimates of Core–Core Electron Correlation Contributions to Excitation Energies in Mg-Like Iron

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Academic Editor: Joseph Reader

Received: 25 November 2016; Accepted: 6 January 2017; Published: 12 January 2017

**Abstract:** Large configuration interaction (CI) calculations can be performed if part of the interaction is treated perturbatively. To evaluate the combined CI and perturbative method, we compute excitation energies for the  $3l3l'$ ,  $3l4l'$  and  $3s5l$  states in Mg-like iron. Starting from a CI calculation including valence and core–valence correlation effects, it is found that the perturbative inclusion of core–core electron correlation halves the mean relative differences between calculated and observed excitation energies. The effect of the core–core electron correlation is largest for the more excited states. The final relative differences between calculated and observed excitation energies is 0.023%, which is small enough for the calculated energies to be of direct use in line identifications in astrophysical and laboratory spectra.

**Keywords:** excitation energies; multiconfiguration Dirac–Hartree–Fock; configuration interaction

## 1. Introduction

Transitions from highly charged ions are observed in the spectra of astrophysical sources as well as in Tokamak and laser-produced plasmas, and they are routinely used for diagnostic purposes [1]. Often, transitions between configurations in the same complex are used, but transitions from higher lying configurations are also important (see, e.g., [2] for a discussion of the higher lying states in the case of Mg-like iron). Transition energies are available from experiments for many ions and collected in various data bases [3], but large amounts of data are still lacking. Although experimental work is aided by a new generation of light sources such as EBITs [4], spectral identifications are still a difficult and time-consuming task. A way forward is provided by theoretical transition energies that support line identification and render consistency checks for experimental level designations.

Much work has been done to improve both multiconfiguration methods and perturbative methods, each with their strengths and weaknesses, in order to provide theoretical transition energies of spectroscopic accuracy, i.e., transition energies with uncertainties of the same order as the ones obtained from experiments and observations using Chandra, Hinode or other space based missions in the X-ray and EUV spectral ranges [5–8]. Further advancements for complex systems with several



electrons outside a closed atomic core calls for a combination of multiconfiguration and perturbative methods [9] and also for methods based on new principles [10,11].

In this paper, we describe how the multiconfiguration Dirac–Hartree–Fock (MCDHF) and relativistic configuration interaction (CI) methods can be modified to include perturbative corrections that account for core–core electron correlation. Taking Mg-like iron as an example, we show how the corrections improve excitation energies for the more highly excited states.

## 2. Relativistic Multiconfiguration Methods

### 2.1. Multiconfiguration Dirac–Hartree–Fock and Configuration Interaction

In the MCDHF method [12,13], as implemented in the GRASP2K program package [14], the wave function  $\Psi(\gamma P J M_J)$  for a state labeled  $\gamma P J M_J$ , where  $J$  and  $M_J$  are the angular quantum numbers and  $P$  is the parity, is expanded in antisymmetrized and coupled configuration state functions (CSFs)

$$\Psi(\gamma P J M_J) = \sum_{j=1}^M c_j \Phi(\gamma_j P J M_J). \quad (1)$$

The labels  $\{\gamma_j\}$  denote other appropriate information of the configuration state functions, such as orbital occupancy and coupling scheme. The CSFs are built from products of one-electron orbitals, having the general form

$$\psi_{n\kappa,m}(\mathbf{r}) = \frac{1}{r} \begin{pmatrix} P_{n\kappa}(r) \chi_{\kappa,m}(\theta, \varphi) \\ i Q_{n\kappa}(r) \chi_{-\kappa,m}(\theta, \varphi) \end{pmatrix}, \quad (2)$$

where  $\chi_{\pm\kappa,m}(\theta, \varphi)$  are 2-component spin-orbit functions. The radial functions  $\{P_{n\kappa}(r), Q_{n\kappa}(r)\}$  are numerically represented on a grid.

Wave functions for a number of targeted states are determined simultaneously in the extended optimal level (EOL) scheme. Given initial estimates of the radial functions, the energies  $E$  and expansion coefficients  $\mathbf{c} = (c_1, \dots, c_M)^t$  for the targeted states are obtained as solutions to the configuration interaction (CI) problem

$$\mathbf{H}\mathbf{c} = E\mathbf{c}, \quad (3)$$

where  $\mathbf{H}$  is the CI matrix of dimension  $M \times M$  with elements

$$H_{ij} = \langle \Phi(\gamma_i P J M_J) | H | \Phi(\gamma_j P J M_J) \rangle. \quad (4)$$

In relativistic calculations, the Hamiltonian  $H$  is often taken as the Dirac–Coulomb Hamiltonian. Once the expansion coefficients have been determined, the radial functions are improved by solving a set of differential equations results from applying the variational principle on a weighted energy functional of the targeted states together with additional terms needed to preserve orthonormality of the orbitals. The CI problem and the solution of the differential equations are iterated until the radial orbitals and the energy are converged to a specified tolerance.

The MCDHF calculations are often followed by CI calculations where terms representing the transverse photon interaction are added to the Dirac–Coulomb Hamiltonian and the vacuum polarization effects are taken into account by including the Uehling potential. Electron self-energies are calculated with the screened hydrogenic formula [12,15]. Due to the relative simplicity of the CI method, often much larger expansions are included in the final CI calculations compared to the MCDHF calculations.

## 2.2. Large Expansions and Perturbative Corrections

The number of CSFs in the wave function expansions depend on the shell structure of the ionic system as well as the model for electron correlation (to be discussed in Section 3). For accurate calculations, a large number of CSFs are required, leading to very large matrices. To handle these large matrices, the CSFs can a priori be divided into two groups. The first group,  $P$ , with  $m$  elements ( $m \ll M$ ) contains CSFs that account for the major parts of the wave functions. The second group,  $Q$ , with  $M - m$  elements contains CSFs that represent minor corrections. Allowing interaction between CSFs in group  $P$ , interaction between CSFs in group  $P$  and  $Q$  and diagonal interactions between CSFs in  $Q$  gives a matrix

$$\begin{pmatrix} H^{(PP)} & H^{(PQ)} \\ H^{(QP)} & H^{(QQ)} \end{pmatrix}, \quad (5)$$

where  $H_{ij}^{(QQ)} = \delta_{ij}E_i^Q$ . The restriction of  $H^{(QQ)}$  to diagonal elements results in a huge reduction in the total number of matrix elements and corresponding computational time. The assumptions of the approximation and the connections to the method of deflation in numerical analysis are discussed in [13]. This form of the CI matrix, which has been available in the non-relativistic and relativistic multiconfiguration codes for a long time [16,17], yields energies that are similar to the ones obtained by applying second-order perturbation theory (PT) corrections to the energies of the smaller  $m \times m$  matrix. The method is therefore referred to here as CI combined with second-order Brillouin–Wigner perturbation theory [18]. Note, however, that the CI method with restrictions on the interactions gives, in contrast to ordinary perturbative methods, wave functions that can be directly used to evaluate expectation values such as transition rates.

## 3. Calculations

Calculations were performed for states belonging to the  $3s^2$ ,  $3p^2$ ,  $3s3d$ ,  $3d^2$ ,  $3s4s$ ,  $3s4d$ ,  $3p4p$ ,  $3p4f$ ,  $3d4s$ ,  $3d4d$ ,  $3s5s$ ,  $3s5d$ ,  $3s5g$  even configurations and the  $3s3p$ ,  $3p3d$ ,  $3s4p$ ,  $3p4s$ ,  $3s4f$ ,  $3p4d$ ,  $3d4p$ ,  $3d4f$ ,  $3s5p$ ,  $3s5f$  odd configurations of Mg-like iron. For  $3d4f$ , only states below the  $3p5s$  configuration were included. The above configurations define the multireference (MR) for the even and odd parities, respectively. Following the procedure in [19], an initial MCDHF calculation for all even and odd reference states was done in the EOL scheme. The initial calculation was followed by separate calculations in the EOL scheme for the even and odd parity states. The MCDHF calculations for the even states were based on CSF expansions obtained by allowing single (S) and double (D) substitutions of orbitals in the even MR configurations to an increasing active set of orbitals. In a similar way, the calculations for the odd states were based on CSF expansions obtained by allowing single (S) and double (D) substitutions of orbitals in the odd MR configurations to an increasing active set of orbitals. To prevent the CSF expansions from growing unmanageably large and in order to obtain orbitals that are spatially localized in the valence and core–valence region, at most, single substitutions were allowed from the  $2s^22p^6$  core. The  $1s^2$  shell was always closed. The active sets of orbitals for the even and odd parity states were extended by layers to include orbitals with quantum numbers up to  $n = 8$  and  $l = 6$ , at which point the excitation energies are well converged.

To investigate the effects of electron correlation, three sets of CI calculations were done. In the first set of CI calculations, one calculation was done for the even states and one calculation for the odd states, the SD substitutions were only allowed from the valence shells of the MR, and the CSFs account for valence–valence correlation. In the second set of calculations, SD substitutions were such that there was at most one substitution from the  $2s^22p^6$  core, and the CSFs account for valence–valence and core–valence correlation. In the final set of calculations, all SD substitutions were allowed, and the CSFs account for valence–valence, core–valence and core–core correlation. When all substitutions are allowed, the number of CSFs grows very large. For this reason, we apply CI with second-order perturbation corrections. The CSFs describing valence–valence and core–valence effects (SD substitutions with at most one substitution from the  $2s^22p^6$  core) were included in group  $P$ ,

whereas the CSFs accounting for core–core correlation (D substitutions from  $2s^22p^6$ ) were included in group Q and treated in second-order perturbation theory. The number of CSFs for the different CI calculations are given in Table 1.

**Table 1.** Number of CSFs for the even and odd parity expansions for the different sets of CI calculations. VV are the expansions accounting for valence–valence correlation, VV+CV are the expansions accounting for valence–valence and core–valence correlation and VV+CV+CC are the expansions accounting for valence–valence, core–valence and core–core correlation.

	VV	VV+CV	VV+CV+CC
even	2738	644,342	5,624,158
odd	2728	630,502	6,214,393

#### 4. Results

The excitation energies from the different CI calculations, along with observed energies from the NIST database [3], are displayed in Table 2. From the table, we see that states belonging to  $3l3l'$ , with the exception of  $3s3p\ ^3P_{0,1,2}$ , are too high for the valence–valence correlation calculation. The states belonging to  $3l4l'$  and  $3s5l$ , on the other hand, are too low. When including also the core–valence correlation, the states belonging to  $3l3l'$  go down in energy and approach the observed excitation energies. The states belonging to  $3l4l'$  and  $3s5l$  go up and are now too high. Including also the core–core correlation results in a rather small energy change for the states belonging to  $3l3l'$ . The main effect of the core–core correlation is to lower the energies of the states belonging to  $3l4l'$  and  $3s5l$ , bringing them in very good agreement with observations. The labeling of levels is normally done by looking at the quantum designation of the leading component in the CSF expansion [20]. There are two levels (67 and 69) with  $3p4d\ ^3D_3$  as the leading component in the corresponding CSF expansion. To distinguish these levels, we added subscripts A and B to the labels of the dominant component. In a similar way, subscripts A and B were added to distinguish levels 78 and 80, both with  $3p4f\ ^3F_3$  as the leading component.

Table 2 indicates that there are a few states that are either misidentified or assigned with a label that is inconsistent with the labels of the current calculation. The observed energy for  $3p4f\ ^3D_2$  (level 84) is  $2417\text{ cm}^{-1}$  too low compared to the calculated value and the observed energy for  $3s5s\ ^3S_1$  (level 92) is  $33,948\text{ cm}^{-1}$  too high. There seem to be no other computed energy levels that match the observed energies. The observed energy for  $3s5p\ ^1P_1^o$  (level 100) is  $3733\text{ cm}^{-1}$  too low. The observed energy matches the computed energy of  $3s5p\ ^3P_1^o$  (level 97), and, thus, it seems like an inconsistency in the labeling. Finally,  $3s5f\ ^1F_3^o$  (level 117) is  $101,545\text{ cm}^{-1}$  too high and there is no other computed energy level that matches. Removing the energy outliers above, the mean relative energy differences are, respectively, 0.217%, 0.051%, 0.023% for the valence, the valence and core–valence and the valence, core–valence and core–core calculations. The energy differences are mainly due to higher-order electron correlation effects that have not been accounted for in the calculations. At the same time, one should bear in mind that the observed excitation energies are also associated with uncertainties as reflected in the limited number of valid digits displayed in the NIST tables.

In Table 3, the excitation energies obtained by including core–core correlation in the CI calculations are compared with energies from calculations by Landi [2] using the FAC code and with energies by Aggarwal et al. [21] using CIV3 in the Breit–Pauli approximation. The uncertainties of the excitation energies for the latter calculations are substantially larger. The calculations by Landi support the conclusion that some of the levels in the NIST database are misidentified. One may note that Landi gives levels 78 and 80 the labels  $3p4f\ ^3F_3$  and  $3p4f\ ^1F_3$ , respectively, whereas Aggarwal et al. reverse the labels. This illustrates that labeling is dependent on the calculation and that the labeling process is far from straightforward [20].

**Table 2.** Comparison of calculated and observed excitation energies in Mg-like iron (Fe XV).  $E_{VV}$  are energies from CI calculations that account for valence–valence correlation.  $E_{VV+CV}$  are energies from CI calculations that account for valence–valence and core–valence electron correlation.  $E_{VV+CV+CC}$  are energies that account for valence–valence and core–valence electron correlation and where core–core electron correlation effects have been included perturbatively.  $E_{NIST}$  are observed energies from the NIST database ([3]).  $\Delta E$  are energy differences with respect to  $E_{NIST}$ . All energies are in  $\text{cm}^{-1}$ .

No.	Level	$E_{VV}$	$\Delta E$	$E_{VV+CV}$	$\Delta E$	$E_{VV+CV+CC}$	$\Delta E$	$E_{NIST}$
1	$3s^2\ ^1S_0$	0	0	0	0	0	0	0
2	$3s3p\ ^3P_0^o$	233,087	−755	233,828	−14	233,928	86	233,842
3	$3s3p\ ^3P_1^o$	238,936	−724	239,668	8	239,741	81	239,660
4	$3s3p\ ^3P_2^o$	253,017	−803	253,829	9	253,773	−47	253,820
5	$3s3p\ ^1P_1^o$	354,941	3030	352,169	258	352,091	180	351,911
6	$3p^2\ ^3P_0$	556,594	2070	554,643	119	554,895	371	554,524
7	$3p^2\ ^1D_2$	559,900	300	559,834	234	559,661	61	559,600
8	$3p^2\ ^3P_1$	566,524	1922	564,663	61	564,674	72	56,4602
9	$3p^2\ ^3P_2$	583,327	1524	581,933	130	581,870	67	581,803
10	$3p^2\ ^1S_0$	662,999	3372	660,269	642	660,229	602	659,627
11	$3s3d\ ^3D_1$	680,522	1750	678,954	182	678,329	−443	678,772
12	$3s3d\ ^3D_2$	681,520	1735	679,986	201	679,381	−404	679,785
13	$3s3d\ ^3D_3$	683,080	1664	681,603	187	680,952	−464	681,416
14	$3s3d\ ^1D_2$	766,690	4597	762,729	636	762,176	83	762,093
15	$3p3d\ ^3F_2^o$	929,158	917	928,565	324	928,086	−155	928,241
16	$3p3d\ ^3F_3^o$	938,885	759	938,469	343	938,068	−58	938,126
17	$3p3d\ ^1D_2^o$	950,226	1713	948,768	255	948,383	−130	948,513
18	$3p3d\ ^3F_4^o$	950,300	642	949,990	332	949,451	−207	949,658
19	$3p3d\ ^3D_1^o$	986,221	3353	983,077	209	982,740	−128	982,868
20	$3p3d\ ^3P_2^o$	986,499	2985	983,765	251	983,350	−164	983,514
21	$3p3d\ ^3D_3^o$	998,324	3472	995,088	236	994,712	−140	994,852
22	$3p3d\ ^3P_1^o$	998,597	2708	996,218	329	995,835	−54	995,889
23	$3p3d\ ^3P_0^o$	999,166	2923	996,547	304	996,127	−116	996,243
24	$3p3d\ ^3D_2^o$	999,755	3132	996,892	269	996,449	−174	996,623
25	$3p3d\ ^1F_3^o$	1,066,906	4391	1,063,163	648	1,062,704	189	1,062,515
26	$3p3d\ ^1P_1^o$	1,078,913	4026	1,075,795	908	1,075,306	419	1,074,887
27	$3d^2\ ^3F_2$	1,373,374	3043	1,370,858	527	1,369,758	−573	1,370,331
28	$3d^2\ ^3F_3$	1,374,983	2948	1,372,527	492	1,371,407	−628	1,372,035
29	$3d^2\ ^3F_4$	1,376,965	2909	1,374,580	524	1,373,475	−581	1,374,056
30	$3d^2\ ^1D_2$	1,405,702	3110	1,403,474	882	1,402,237	−355	1,402,592
31	$3d^2\ ^3P_0$	1,409,066		1,406,328		1,405,381		
32	$3d^2\ ^3P_1$	1,409,639		1,406,926		1,405,672		
33	$3d^2\ ^1G_4$	1,409,702	2644	1,407,974	916	1,406,831	−227	1,407,058
34	$3d^2\ ^3P_2$	1,411,053	3280	1,408,467	694	1,407,210	−563	1,407,773
35	$3d^2\ ^1S_0$	1,489,913	2859	1,488,993	1939	1,487,460	406	1,487,054
36	$3s4s\ ^3S_1$	1,761,471	−2229	1,764,876	1176	17,63,699	−1	1,763,700
37	$3s4s\ ^1S_0$	1,785,265	−1735	1,788,455	1455	1,787,322	322	1,787,000
38	$3s4p\ ^3P_0^o$	1,880,014		1,883,187		1,882,236		
39	$3s4p\ ^3P_1^o$	1,880,440		1,883,595		1,882,588		
40	$3s4p\ ^3P_2^o$	1,887,508		1,890,703		1,889,632		
41	$3s4p\ ^1P_1^o$	1,887,879	−2098	1,891,051	1081	1,890,042	72	1,889,970
42	$3s4d\ ^3D_1$	2,029,659	−1651	2,032,907	1597	2,031,683	373	2,031,310
43	$3s4d\ ^3D_2$	2,030,413	−1607	2,033,653	1633	2,032,413	393	2,032,020

Table 2. Cont.

No.	Level	$E_{VV}$	$\Delta E$	$E_{VV+CV}$	$\Delta E$	$E_{VV+CV+CC}$	$\Delta E$	$E_{NIST}$
44	3s4d $^3D_3$	2,031,636	-1544	2,034,880	1700	2,033,623	443	2,033,180
45	3s4d $^1D_2$	2,032,991	-2289	2,036,318	1038	2,035,053	-227	2,035,280
46	3p4s $^3P_0^o$	2,051,314		2,053,909		2,053,031		
47	3p4s $^3P_1^o$	2,054,922		2,057,446		2,056,493		
48	3p4s $^3P_2^o$	2,071,700		2,074,376		2,073,372		
49	3p4s $^1P_1^o$	2,085,097		2,087,237		2,086,235		
50	3s4f $^3F_2^o$	2,105,597	-2923	2,109,821	1301	2,108,281	-239	2,108,520
51	3s4f $^3F_3^o$	2,105,804	-2816	2,110,029	1409	2,108,503	-117	2,108,620
52	3s4f $^3F_4^o$	2,106,098	-2782	2,110,327	1447	2,108,798	-82	2,108,880
53	3s4f $^1F_3^o$	2,120,519	-2631	2,124,654	1504	2,123,180	30	2,123,150
54	3p4p $^1P_1$	2,152,851		2,155,266		2,154,244		
55	3p4p $^3D_1$	2,167,018		2,169,386		2,168,341		
56	3p4p $^3D_2$	2,168,756		2,171,070		2,170,006		
57	3p4p $^3P_0$	2,173,624		2,175,566		2,174,583		
58	3p4p $^3P_1$	2,181,779		2,183,914		2,182,831		
59	3p4p $^3D_3$	2,184,022		2,186,457		2,185,350		
60	3p4p $^3P_2$	2,189,341		2,191,385		2,190,270		
61	3p4p $^3S_1$	2,192,119		2,194,460		2,193,367		
62	3p4p $^1D_2$	2,206,894		2,208,893		2,207,746		
63	3p4p $^1S_0$	2,235,724		2,237,406		2,236,314		
64	3p4d $^3D_1^o$	2,311,660		2,314,071		2,313,090		
65	3p4d $^1D_2^o$	2,311,989		2,314,331		2,313,312		
66	3p4d $^3D_2^o$	2,312,449		2,314,882		2,313,865		
67	3p4d $^3D_{3A}^o$	2,313,908		2,316,401		2,315,387		
68	3p4d $^3F_2^o$	2,329,261		2,331,722		2,330,678		
69	3p4d $^3D_{3B}^o$	2,330,539		2,333,084		2,332,039		
70	3p4d $^3F_4^o$	2,337,384		2,339,922		2,338,857		
71	3p4d $^1F_3^o$	2,337,651		2,340,302		2,339,278		
72	3p4d $^3P_0^o$	2,341,803		2,344,120		2,343,033		
73	3p4d $^3P_1^o$	2,342,778		2,345,091		2,344,049		
74	3p4d $^3P_0^o$	2,346,915		2,349,198		2,348,199		
75	3p4d $^1P_1^o$	2,350,169		2,352,543		2,351,513		
76	3p4f $^3G_3$	2,377,507	-2653	2,381,283	1123	2,379,714	-446	2,380,160
77	3p4f $^3G_4$	2,384,217	-2483	2,387,976	1276	2,386,434	-266	2,386,700
78	3p4f $^3F_{3A}$	2,384,435		2,388,118		2,386,537		
79	3p4f $^3F_2$	2,388,049	-2051	2,391,670	1570	2,390,091	-9	2,390,100
80	3p4f $^3F_{3B}$	2,397,860		2,401,630		2,400,029		
81	3p4f $^3G_5$	2,399,542	-2558	2,403,453	1353	2,401,876	-224	2,402,100
82	3p4f $^3F_4$	2,400,524	-1576	2,404,286	2186	2,402,697	597	2,402,100
83	3p4f $^3D_3$	2,411,680	-1320	2,415,368	2368	2,413,758	758	2,413,000
84	3p4f $^3D_2$	2,414,633	333	2,418,319	4019	2,416,717	2417	2,414,300
85	3p4f $^3D_1$	2,417,852	-2248	2,421,557	1457	2,419,975	-125	2,420,100
86	3p4f $^1G_4$	2,426,828	-1872	2,430,497	1797	2,429,063	363	2,428,700
87	3p4f $^1D_2$	2,433,430	-2570	2,437,039	1039	2,435,534	-466	2,436,000
88	3d4s $^3D_1$	2,458,614		2,460,640		2,458,997		
89	3d4s $^3D_2$	2,459,450		2,461,503		2,459,846		
90	3d4s $^3D_3$	2,461,283		2,463,415		2,461,742		
91	3d4s $^1D_2$	2,468,780		2,470,737		2,469,163		
92	3s5s $^3S_1$	2,507,700	-37,100	2,512,036	-32,764	2,510,852	-33,948	2,544,800

Table 2. Cont.

No.	Level	$E_{VV}$	$\Delta E$	$E_{VV+CV}$	$\Delta E$	$E_{VV+CV+CC}$	$\Delta E$	$E_{NIST}$
93	3s5s $^1S_0$	2,516,613		2,520,681		2,519,752		
94	3d4p $^1D_2^o$	2,561,358		2,563,408		2,561,899		
95	3d4p $^3D_1^o$	2,564,069		2,567,301		2,565,949		
96	3s5p $^3P_0^o$	2,564,472		2,568,582		2,567,624		
97	3s5p $^3P_1^o$	2,565,848		2,568,791		2,567,639		
98	3d4p $^3D_2^o$	2,567,134		2,569,092		2,567,703		
99	3d4p $^3D_3^o$	2,568,154		2,571,175		2,569,693		
100	3s5p $^1P_1^o$	2,568,200	1200	2,571,834	4834	2,570,733	3733	2,567,000
101	3s5p $^3P_2^o$	2,569,213		2,572,157		2,570,743		
102	3d4p $^3F_2^o$	2,570,296		2,572,316		2,571,126		
103	3d4p $^3F_3^o$	2,573,116		2,575,101		2,573,592		
104	3d4p $^3F_4^o$	2,576,139		2,578,374		2,576,829		
105	3d4p $^3P_1^o$	2,583,286		2,585,242		2,583,862		
106	3d4p $^3P_2^o$	2,583,400		2,585,407		2,583,960		
107	3d4p $^3P_0^o$	2,583,734		2,585,658		2,584,322		
108	3d4p $^1F_3^o$	2,592,868		2,594,519		2,593,236		
109	3d4p $^1P_1^o$	2,603,279		2,605,145		2,604,533		
110	3s5d $^3D_1$	2,637,190	-2910	2,641,400	1300	2,640,247	147	2,640,100
111	3s5d $^3D_2$	2,637,419	-2481	2,641,630	1730	2,640,442	542	2,639,900
112	3s5d $^3D_3$	2,637,852	-2448	2,642,072	1772	2,640,870	570	2,640,300
113	3s5d $^1D_2$	2,639,773		2,643,981		2,642,888		
114	3s5f $^3F_2^o$	2,672,676	-3724	2,677,360	960	2,675,889	-511	2,676,400
115	3s5f $^3F_3^o$	2,672,770	-3630	2,677,455	1055	2,675,988	-412	2,676,400
116	3s5f $^3F_4^o$	2,672,907	-3693	2,677,594	994	2,676,123	-477	2,676,600
117	3s5f $^1F_3^o$	2,678,041	-104,659	2,682,597	-100,103	2,681,155	-101,545	2,782,700
118	3s5g $^3G_3$	2,682,487		2,687,368		2,685,680		
119	3s5g $^3G_4$	2,682,654		2,687,556		2,685,877		
120	3s5g $^3G_5$	2,682,855		2,687,777		2,686,099		
121	3s5g $^1G_4$	2,685,580		2,690,506		2,688,841		
122	3d4d $^1F_3$	2,699,116		2,701,602		2,699,874		
123	3d4d $^3D_1$	2,703,542		2,705,972		2,704,354		
124	3d4d $^3D_2$	2,704,742		2,707,218		2,705,580		
125	3d4d $^3D_3$	2,706,116		2,708,636		2,706,964		
126	3d4d $^3G_3$	2,707,934		2,710,522		2,708,828		
127	3d4d $^1P_1$	2,709,315		2,711,813		2,710,163		
128	3d4d $^3G_4$	2,709,360		2,711,928		2,710,264		
129	3d4d $^3G_5$	2,711,220		2,713,878		2,712,174		
130	3d4d $^3S_1$	2,720,698		2,723,175		2,721,783		
131	3d4d $^3F_2$	2,726,309		2,728,092		2,726,350		
132	3d4d $^3F_3$	2,727,568		2,729,398		2,727,634		
133	3d4d $^3F_4$	2,729,029		2,730,908		2,729,156		
134	3d4d $^1D_2$	2,741,839		2,743,862		2,742,627		
135	3d4d $^3P_0$	2,744,213		2,746,022		2,744,706		
136	3d4d $^3P_1$	2,744,807		2,746,626		2,745,163		
137	3d4d $^3P_2$	2,745,935		2,747,809		2,746,300		
138	3d4d $^1G_4$	2,748,985		2,751,121		2,749,474		
139	3d4f $^3H_4^o$	2,765,833		2,770,098		2,768,443		
140	3d4f $^1G_4^o$	2,767,533		2,771,821		2,770,030		
141	3d4f $^3H_5^o$	2,767,692		2,771,943		2,770,434		
142	3d4d $^1S_0$	2,775,538		2,779,275		2,777,362		

Table 2. Cont.

No.	Level	$E_{VV}$	$\Delta E$	$E_{VV+CV}$	$\Delta E$	$E_{VV+CV+CC}$	$\Delta E$	$E_{NIST}$
143	$3d4f\ ^3F_2^o$	2,776,151		2,779,298		2,778,011		
144	$3d4f\ ^3F_3^o$	2,776,264		2,779,933		2,778,867		
145	$3d4f\ ^3F_4^o$	2,776,981		2,780,796		2,780,729		
146	$3d4f\ ^1D_2^o$	2,786,768		2,790,305		2,788,248		

Table 3. Comparison of calculated and observed excitation energies in Mg-like iron (Fe XV).  $E_{VV+CV+CC}$  are energies that account for valence–valence and core–valence electron correlation and where core–core electron correlation effects have been included perturbatively.  $E_{FAC}$  are energies by Landi [2] using the FAC code.  $E_{CIV3}$  are energies by Aggarwal et al. [21] using the CIV3 code.  $E_{NIST}$  are observed energies from the NIST database ([3]).  $\Delta E$  are energy differences with respect to  $E_{NIST}$ . All energies are in  $\text{cm}^{-1}$ .

No.	Level	$E_{VV+CV+VV}$	$\Delta E$	$E_{FAC}$	$\Delta E$	$E_{CIV3}$	$\Delta E$	$E_{NIST}$
1	$3s^2\ ^1S_0$	0	0	0	0	0	0	0
2	$3s3p\ ^3P_0^o$	233,928	86	233,068	−774	235,013	1171	233,842
3	$3s3p\ ^3P_1^o$	239,741	81	238,900	−760	240,511	851	239,660
4	$3s3p\ ^3P_2^o$	253,773	−47	252,917	−903	253,548	−272	253,820
5	$3s3p\ ^1P_1^o$	352,091	180	356,126	4215	356,262	4351	351,911
6	$3p^2\ ^3P_0$	554,895	371	556,994	2470	560,275	5751	554,524
7	$3p^2\ ^1D_2$	559,661	61	560,266	666	563,216	3616	559,600
8	$3p^2\ ^3P_1$	564,674	72	566,832	2230	569,295	4693	564,602
9	$3p^2\ ^3P_2$	581,870	67	583,564	1761	584,856	3053	581,803
10	$3p^2\ ^1S_0$	660,229	602	665,768	6141	665,260	5633	659,627
11	$3s3d\ ^3D_1$	678,329	−443	680,146	1374	687,680	8908	678,772
12	$3s3d\ ^3D_2$	679,381	−404	681,129	1344	688,733	8948	679,785
13	$3s3d\ ^3D_3$	680,952	−464	682,667	1251	690,401	8985	681,416
14	$3s3d\ ^1D_2$	762,176	83	769,369	7276	774,295	12,202	762,093
15	$3p3d\ ^3F_2^o$	928,086	−155	928,786	545	938,265	10,024	928,241
16	$3p3d\ ^3F_3^o$	938,068	−58	938,555	429	947,307	9181	938,126
17	$3p3d\ ^1D_2^o$	948,383	−130	949,447	934	958,402	9889	948,513
18	$3p3d\ ^3F_4^o$	949,451	−207	949,927	269	957,820	8162	949,658
19	$3p3d\ ^3D_1^o$	982,740	−128	986,082	3214	995,526	12,658	982,868
20	$3p3d\ ^3P_2^o$	983,350	−164	986,407	2893	995,767	12,253	983,514
21	$3p3d\ ^3D_3^o$	994,712	−140	997,944	3092	1,007,026	12,174	994,852
22	$3p3d\ ^3P_0^o$	995,835	−54	998,762	2873	1,006,708	10,819	995,889
23	$3p3d\ ^3P_1^o$	996,127	−116	999,173	2930	1,007,366	11,123	996,243
24	$3p3d\ ^3D_2^o$	996,449	−174	999,578	2955	1,008,124	11,501	996,623
25	$3p3d\ ^1F_3^o$	1,062,704	189	1,070,794	8279	1,077,456	14,941	1,062,515
26	$3p3d\ ^1P_1^o$	1,075,306	419	1,083,826	8939	1,089,691	14,804	1,074,887
27	$3d^2\ ^3F_2$	1,369,758	−573	1,372,400	2069	1,388,111	17,780	1,370,331
28	$3d^2\ ^3F_3$	1,371,407	−628	1,373,988	1953	1,389,834	17,799	1,372,035
29	$3d^2\ ^3F_4$	1,373,475	−581	1,375,938	1882	1,391,941	17,885	1,374,056
30	$3d^2\ ^1D_2$	1,402,237	−355	1,407,428	4836	1,421,702	19,110	1,402,592
31	$3d^2\ ^3P_0$	1,405,381		1,409,507		1,424,577		
32	$3d^2\ ^3P_1$	1,405,672		1,410,109		1,425,246		
33	$3d^2\ ^1G_4$	1,406,831	−227	1,412,127	5069	1,425,872	18,814	1,407,058
34	$3d^2\ ^3P_2$	1,407,210	−563	1,411,643	3870	1,426,815	19,042	1,407,773
35	$3d^2\ ^1S_0$	1,487,460	406	1,498,668	11,614	1,508,954	21,900	1,487,054
36	$3s4s\ ^3S_1$	1,763,699	−1	1,760,910	−2790	1,764,005	305	1,763,700

Table 3. Cont.

No.	Level	$E_{VV+CV+VV}$	$\Delta E$	$E_{FAC}$	$\Delta E$	$E_{CIV3}$	$\Delta E$	$E_{NIST}$
37	3s4s $^1S_0$	1,787,322	322	1,786,052	-948	1,787,950	950	1,787,000
38	3s4p $^3P_0^o$	1,882,236		1,880,319		1,883,685		
39	3s4p $^3P_1^o$	1,882,588		1,880,746		1,884,091		
40	3s4p $^3P_2^o$	1,889,632		1,887,756		1,890,313		
41	3s4p $^1P_1^o$	1,890,042	72	1,888,124	-1846	1,890,631	661	1,889,970
42	3s4d $^3D_1$	2,031,683	373	2,029,563	-1747	2,034,124	2814	2,031,310
43	3s4d $^3D_2$	2,032,413	393	2,030,328	-1692	2,034,848	2828	2,0320,20
44	3s4d $^3D_3$	2,033,623	443	2,031,544	-1636	2,036,055	2875	2,033,180
45	3s4d $^1D_2$	2,035,053	-227	2,033,212	-2068	2,037,569	2289	2,035,280
46	3p4s $^3P_0^o$	2,053,031		2,051,778		2,055,797		
47	3p4s $^3P_1^o$	2,056,493		2,055,514		2,059,308		
48	3p4s $^3P_2^o$	2,073,372		2,072,083		2,074,452		
49	3p4s $^1P_1^o$	2,086,235		2,086,607		2,088,795		
50	3s4f $^3F_2^o$	2,108,281	-239	2,107,228	-1292	2,110,073	1553	2,108,520
51	3s4f $^3F_3^o$	2,108,503	-117	2,107,423	-1197	2,110,281	1661	2,108,620
52	3s4f $^3F_4^o$	2,108,798	-82	2,107,701	-1179	2,110,567	1687	2,108,880
53	3s4f $^1F_3^o$	2,123,180	30	2,124,054	904	2,125,886	2736	2,123,150
54	3p4p $^1P_1$	2,154,244		2,167,343		2,158,599		
55	3p4p $^3D_1$	2,168,341		2,153,046		2,171,635		
56	3p4p $^3D_2$	2,170,006		2,169,173		2,173,578		
57	3p4p $^3P_0$	2,174,583		2,175,103		2,178,812		
58	3p4p $^3P_1$	2,182,831		2,182,790		2,185,901		
59	3p4p $^3D_3$	2,185,350		2,184,242		2,187,229		
60	3p4p $^3P_2$	2,190,270		2,190,674		2,193,265		
61	3p4p $^3S_1$	2,193,367		2,192,597		2,195,756		
62	3p4p $^1D_2$	2,207,746		2,209,221		2,211,163		
63	3p4p $^1S_0$	2,236,314		2,239,314		2,241,187		
64	3p4d $^3D_1^o$	2,313,090		2,311,999		2,318,014		
65	3p4d $^1D_2^o$	2,313,312		2,312,326		2,318,179		
66	3p4d $^3D_2^o$	2,313,865		2,312,835		2,318,826		
67	3p4d $^3D_{3,A}^o$	2,315,387		23,144,663		2,320,538		
68	3p4d $^3F_2^o$	2,330,678		2,329,647		2,334,178		
69	3p4d $^3D_{3,B}^o$	2,332,039		2,331,0213		2,335,726		
70	3p4d $^3F_4^o$	2,338,857		2,338,064		2,342,277		
71	3p4d $^1F_3^o$	2,339,278		2,338,703		2,343,517		
72	3p4d $^3P_2^o$	2,343,033		2,342,598		2,347,544		
73	3p4d $^3P_1^o$	2,344,049		2,343,850		2,348,795		
74	3p4d $^3P_0^o$	2,348,199		2,347,823		2,352,406		
75	3p4d $^1P_1^o$	2,351,513		2,351,661		2,356,773		
76	3p4f $^3G_3$	2,379,714	-446	2,379,430	-730	2,384,306	4146	2,380,160
77	3p4f $^3G_4$	2,386,434	-266	2,386,688	-12	2,391,198	4498	2,386,700
78	3p4f $^3F_{3A}$	2,386,537		2,386,430		2,390,473		
79	3p4f $^3F_2$	2,390,091	-9	2,390,112	12	2,393,842	3742	2,390,100
80	3p4f $^3F_{3B}$	2,400,029		2,399,796		2,402,786		
81	3p4f $^3G_5$	2,401,876	-224	2,401,746	-354	2,405,617	3517	2,402,100
82	3p4f $^3F_4$	2,402,697	597	2,402,507	407	2,405,496	3396	2,402,100
83	3p4f $^3D_3$	2,413,758	758	2,414,120	1120	2,417,151	4151	2,413,000
84	3p4f $^3D_2$	2,416,717	2417	2,417,276	2976	2,420,124	5824	2,414,300
85	3p4f $^3D_1$	2,419,975	-125	2,420,512	412	2,423,219	3119	2,420,100
86	3p4f $^1G_4$	2,429,063	363	2,432,908	4208	2,435,828	7128	2,428,700



Table 3. Cont.

No.	Level	$E_{VV+CV+VV}$	$\Delta E$	$E_{FAC}$	$\Delta E$	$E_{CIV3}$	$\Delta E$	$E_{NIST}$
87	3p4f $^1D_2$	2,435,534	-466	2,438,982	2982	2,440,239	4239	2,436,000
88	3d4s $^3D_1$	2,458,997		2,458,814		2,468,047		
89	3d4s $^3D_2$	2,459,846		2,459,675		2,468,969		
90	3d4s $^3D_3$	2,461,742		2,461,461		2,470,911		
91	3d4s $^1D_2$	2,469,163		2,470,364		2,479,437		
92	3s5s $^3S_1$	2,510,852	-33,948	2,507,572	-37,228			2,544,800
93	3s5s $^1S_0$	2,519,752		2,517,043				
94	3d4p $^1D_2^o$	2,561,899		2,561,169		2,571,814		
95	3d4p $^3D_1^o$	2,565,949		2,566,041		2,576,851		
96	3s5p $^3P_0^o$	2,567,624		2,564,597				
97	3s5p $^3P_1^o$	2,567,639		2,564,254				
98	3d4p $^3D_2^o$	2,567,703		2,567,341		2,577,905		
99	3d4p $^3D_3^o$	2,569,693		2,569,518		2,583,117		
100	3s5p $^1P_1^o$	2,570,733	3733	2,568,358	1358			2,567,000
101	3s5p $^3P_2^o$	2,570,743		2,568,240				
102	3d4p $^3F_2^o$	2,571,126		2,570,526		2,580,319		
103	3d4p $^3F_3^o$	2,573,592		2,573,370		2,579,847		
104	3d4p $^3F_4^o$	2,576,829		2,576,531		2,586,036		
105	3d4p $^3P_1^o$	2,583,862		2,584,287		2,593,158		
106	3d4p $^3P_2^o$	2,583,960		2,584,326		2,593,586		
107	3d4p $^3P_0^o$	2,584,322		2,584,699		2,593,641		
108	3d4p $^1F_3^o$	2,593,236		2,596,425		2,604,571		
109	3d4p $^1P_1^o$	2,604,533		2,607,817		2,610,870		
110	3s5d $^3D_1$	2,640,247	147	2,637,143	-2957			2,640,100
111	3s5d $^3D_2$	2,640,442	542	2,637,376	-2524			2,639,900
112	3s5d $^3D_3$	2,640,870	570	2,637,804	-2496			2,640,300
113	3s5d $^1D_2$	2,642,888		2,640,084	0			
114	3s5f $^3F_2^o$	2,675,889	-511	2,673,354	-3046			2,676,400
115	3s5f $^3F_3^o$	2,675,988	-412	2,673,444	-2956			2,676,400
116	3s5f $^3F_4^o$	2,676,123	-477	2,673,575	-3025			2,676,600
117	3s5f $^1F_3^o$	2,681,155	-101,545	2,679,558	-103,142			2,782,700
118	3s5g $^3G_3$	2,685,680		2,683,089				
119	3s5g $^3G_4$	2,685,877		2,683,272				
120	3s5g $^3G_5$	2,686,099		2,683,494				
121	3s5g $^1G_4$	2,688,841		2,686,809				
122	3d4d $^1F_3$	2,699,874		2,697,717		2,710,391		
123	3d4d $^3D_1$	2,704,354		2,702,464		2,714,967		
124	3d4d $^3D_2$	2,705,580		2,703,625		2,716,229		
125	3d4d $^3D_3$	2,706,964		2,705,001		2,717,578		
126	3d4d $^3G_3$	2,708,828		2,707,726		2,717,919		
127	3d4d $^1P_1$	2,710,163		2,708,170		2,721,079		
128	3d4d $^3G_4$	2,710,264		2,709,064		2,719,345		
129	3d4d $^3G_5$	2,712,174		2,710,955		2,721,463		
130	3d4d $^3S_1$	2,721,783		2,720,286		2,732,634		
131	3d4d $^3F_2$	2,726,350		2,726,401		2,738,407		
132	3d4d $^3F_3$	2,727,634		2,727,604		2,739,745		
133	3d4d $^3F_4$	2,729,156		2,729,075		2,741,293		
134	3d4d $^1D_2$	2,742,627		2,743,889		2,755,547		
135	3d4d $^3P_0$	2,744,706		2,745,181		2,757,907		
136	3d4d $^3P_1$	2,745,163		2,745,727		2,758,477		

Table 3. Cont.

No.	Level	$E_{VV+CV+VV}$	$\Delta E$	$E_{FAC}$	$\Delta E$	$E_{CIV3}$	$\Delta E$	$E_{NIST}$
137	$3d4d\ ^3P_2$	2,746,300		2,747,024		2,759,619		
138	$3d4d\ ^1G_4$	2,749,474		2,752,675		2,761,254		
139	$3d4f\ ^3F_4^o$	2,768,443		2,766,350		2,778,483		
140	$3d4f\ ^1G_4^o$	2,770,030		2,768,154		2,780,096		
141	$3d4f\ ^3F_5^o$	2,770,434		2,768,448		2,780,831		
142	$3d4d\ ^1S_0$	2,777,362		2,781,322		2,792,233		
143	$3d4f\ ^3F_2^o$	2,778,011		2,775,995		2,787,305		
144	$3d4f\ ^3F_3^o$	2,778,867		2,776,790		2,787,964		
145	$3d4f\ ^3F_4^o$	2,780,729		2,777,446		2,788,842		
146	$3d4f\ ^1D_2^o$	2,788,248		2,787,354		2,798,312		

## 5. Conclusions

CI with restrictions on the interactions (CI combined with second-order Brillouin–Wigner perturbation theory) makes it possible to handle large CSF expansions. The calculations including core–core correlation take around 20 h with 10 nodes on a cluster and bring the computed and observed excitation energies into very good agreement. To improve the computed excitation energies, the orbital set would need to be further extended leading to even larger matrices. The combined CI and perturbation method can be applied to include core–valence correlation in systems with many valence electrons and calculations. Calculations including valence–valence correlation and where core–valence correlation is treated perturbatively are in progress for P-, S-, and Cl-like systems.

**Acknowledgments:** Per Jönsson gratefully acknowledges support from the Swedish Research Council under contract 2015-04842.

**Author Contributions:** All authors contributed equally to the work.

**Conflicts of Interest:** The authors declare no conflicts of interest.

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Article

# JJ2LSJ Transformation and Unique Labeling for Energy Levels

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Academic Editor: Joseph Reader

Received: 21 December 2016; Accepted: 19 January 2017; Published: 27 January 2017

**Abstract:** The JJ2LSJ program, which is important not only for the GRASP2K package but for the atom theory in general, is presented. The program performs the transformation of atomic state functions (ASFs) from a *jj*-coupled CSF basis into an *LSJ*-coupled CSF basis. In addition, the program implements a procedure that assigns a unique label to all energy levels. Examples of how to use the JJ2LSJ program are given. Several cases are presented where there is a unique labeling problem.

**Keywords:** energy levels; *LSJ*-coupling; *jj*-coupling; JJ2LSJ transformation; unique label

## 1. Introduction

In principle, any valid coupling scheme can be used to represent the wave function in atomic structure calculations. Levels of an energy spectrum are identified and labeled with the help of sets of quantum numbers describing the coupling scheme used for the wave function. However, these quantum numbers are exact only for the cases of pure coupling. In a calculations of energy spectra one has to start with the coupling scheme closest to reality [1]. The most frequently used coupling schemes in atomic theory are the *LSJ* and *jj*. In atomic spectroscopy, the standard *LSJ* notation of the levels is frequently applied for classifying the low-lying level structures of atoms or ions.

Calculations may be performed in the relativistic (*jj*-coupling) scheme in order to get more accurate data that include relativistic effects. Thus, after a multiconfiguration Dirac-Hartree-Fock (MCDHF) or relativistic configuration interaction (RCI) [2] calculation the transformation to *LSJ*-coupling is needed. The JJ2LSJ code in GRASP2K [3] does this by applying a unitary transformation to the relativistic configuration state function (CSF) basis set which preserves orthonormality. The unitary transformation selected is the coupling transformation that changes the order of coupling from *jj* to *LSJ*, a transformation that does not involve the radial factor, only the spin-angular factor.

An energy level is normally assigned the label of the leading CSF in the wave function expansion. For many systems, two or more wave functions have the same leading CSFs giving rise to non-unique labels for the energy levels. We have such a situation for Si-like ions [4] and some other systems [5]. The new JJ2LSJ program implements a procedure that resolves these problems, assigning a unique label to all energy levels.

## 2. Theory

### 2.1. Transformation from *jj*- to *LSJ*-Coupling

Each nonrelativistic *nl*-orbital (except for *ns*) is associated with two relativistic orbitals  $l_{\pm} \equiv j = l \pm 1/2$ . In the transformation of the spin-angular factor  $|l^w \alpha LS\rangle$  into a *jj*-coupled angular basis, two subshell states, one with  $l_- \equiv j = l - 1/2$  and another one with  $l_+ \equiv j = l + 1/2$ , may occur in the expansion. This shell-splitting

$$|l^w \alpha \nu LS\rangle \longrightarrow (|l_-^{w_1} \nu_1 J_1\rangle, |l_+^{w_2} \nu_2 J_2\rangle), \quad (1)$$

obviously conserves the number of electrons, provided ( $w = w_1 + w_2$ ), with  $w_1(\max) = 2l$  and  $w_2(\max) = 2(l + 1)$ . Making use of this notation, the transformation between the subshell states in *LSJ*- and *jj*-coupling can be written as

$$|l^w \alpha \nu LSJ\rangle = \sum_{\nu_1 J_1 \nu_2 J_2 w_1} |(l_-^{w_1} \nu_1 J_1, l_+^{(w-w_1)} \nu_2 J_2) J\rangle \langle (l_-^{w_1} \nu_1 J_1, l_+^{(w-w_1)} \nu_2 J_2) J | l^w \alpha \nu LSJ\rangle, \quad (2)$$

$$|(l_-^{w_1} \nu_1 J_1, l_+^{(w-w_1)} \nu_2 J_2) J\rangle = \sum_{\alpha \nu LS} |l^w \alpha \nu LSJ\rangle \langle l^w \alpha \nu LSJ | (l_-^{w_1} \nu_1 J_1, l_+^{(w-w_1)} \nu_2 J_2) J\rangle, \quad (3)$$

which, in both cases, includes a summation over all the quantum numbers (except of *n*,  $l_-$ , and  $l_+$ ). Here,  $|(l_-^{w_1} \nu_1 J_1, l_+^{w_2} \nu_2 J_2) J\rangle$  is a coupled angular state with well-defined total angular momentum *J* which is built from the corresponding *jj*-coupled subshell states with  $j_1 = l_- = l - \frac{1}{2}$ ,  $j_2 = l_+ = l + \frac{1}{2}$  and the total subshell angular momenta  $J_1$  and  $J_2$ , respectively.

An explicit expression for the coupling transformation coefficients

$$\langle (l_-^{w_1} \nu_1 J_1, l_+^{(w-w_1)} \nu_2 J_2) J | l^w \alpha \nu LSJ\rangle = \langle l^w \alpha \nu LSJ | (l_-^{w_1} \nu_1 J_1, l_+^{(w-w_1)} \nu_2 J_2) J\rangle \quad (4)$$

in (2) and (3) can be obtained only if we take the construction of the subshell states of *w* equivalent electrons from their corresponding *parent states* with  $w - 1$  electrons into account. In general, however, the *recursive* definition of the subshell states, out of their parent states, also leads to a recursive generation of the transformation matrices (4). These transformation coefficients can be chosen *real*: they occur very frequently as the *building blocks* in the transformation of all symmetry functions. The expressions and values of these coefficients are published in [6,7].

These transformation matrices, which are applied internally by the program JJ2LSJ, are consistent with the definition of the coefficients of fractional parentage [8,9] and with the phase system used in the [10]. So the program presented in the paper supports transformation from *jj*- to *LSJ*-coupling if ASF (which needs transformation) was created using the approach [7–10]. Otherwise the program may perform the transformation incorrectly.

### 2.2. Unique Labeling

An energy level is often given the label of the leading CSF in the wave function expansion. But it sometimes happens that two wave functions have the same largest CSF in *LSJ*- or *jj*-coupling, and then classification in energy spectra is not unique. The simplest way to have a unique identification of an energy level would be use a position number (POS) and symmetry *J*. But to get the energy spectra with unique labels in *LSJ*-coupling we should re-classify levels. For that purpose JJ2LSJ transformation with the unique labeling option can be used. To obtain unique labels the algorithm proposed in [11,12] is used: for a given set of wave functions with the same *J* and parity, the CSF with largest expansion coefficient is used as the label for the function containing this largest component. Once a label is assigned, the corresponding CSF is removed from consideration in the determination of the next label. In such a way we will get energy levels with unique labels. In this process, cases where

one CSF is dominant (defines more than 50 % of the wave function composition) that CSF will give the label for the corresponding energy level, but when the composition is spread over a number of CSFs, and none particularly large, the label is defined by the algorithm. Thus labeling is done by blocks of levels, each of the same  $J$  and parity. The first step is to order the levels by energy and assign the POS (position) identifier with the lowest having POS = 1, the second POS = 2, etc. and then proceed with determining the label.

In the Section 4 we will present a few examples where wave functions have the same dominant term and where the unique labeling algorithm is needed.

### 3. The JJ2LSJ Program

JJ2LSJ program is intended to perform the transformation of ASFs from a  $jj$ -coupled CSF basis into an  $LSJ$ -coupled CSF basis. This program is written in FORTRAN90 and is included in the GRASP2K package [3]. It uses the same libraries as other programs in GRASP2K. The program is based on the earlier published LSJ program [13], but modified for speed up. The new program transforms only the most important components of large expansions. In addition, the new program provides an option to choose unique labeling versus labeling by the leading CSF in the wave function expansion.

For running the JJ2LSJ program we need several input files generated with the GRASP2K package: the CSFs list file (name.c) and the mixing coefficients file after MCDHF (name.m) or after RCI calculations (name.cm). The example below shows the execution of the JJ2LSJ program for the odd states of Si-like Sr (Sr XXV) ion, built on a CSF basis containing orbitals with principal quantum numbers up to  $n = 7$  and expansion coefficients from RCI calculations. In the following example, the unique labeling option is chosen and the program is run in default mode. It should be remembered that the contribution to the wave function composition from a particular CSF is the square of the expansion coefficient. Thus a CSF with an expansion coefficient of 0.10 contributes 1% to the wave function composition.

```
>>jj2lsj

jj2lsj: Transformation of ASFs from a jj-coupled CSF basis
      into an LSJ-coupled CSF basis (Fortran 95 version)
      (C) Copyright by G. Gaigalas and Ch. F. Fischer,
      (2017).

Input files: name.c, name.(c)m
Output files: name.lsj.lbl,
      (optional) name.lsj.c, name.lsj.j,
      name.uni.lsj.lbl, name.uni.lsj.sum

Name of state
>>odd7
Loading Configuration Symmetry List File ...
There are 49 relativistic subshells;
There are 4420742 relativistic CSFs;
... load complete;

Mixing coefficients from a CI calc.?
>>y
Do you need a unique labeling? (y/n)
>>y
nelec =      14
ncftot =    4420742
nw      =      49
nblock =      5

block   ncf   nev   2j+1   parity
  1  190132     2     1     -1
  2   703411     7     3     -1
  3 1095473     8     5     -1
```

4 1276414 4 7 -1  
 5 1155312 1 9 -1

Default settings? (y/n)

>>y

Maximum % of omitted composition is 1.000

Below 5.0E-03 the eigenvector component is to be neglected for calculating

Below 1.0E-03 the eigenvector composition is to be neglected for printing

Under investigation is the block: 1 The number of eigenvectors: 2  
 The number of CSF (in jj-coupling): 190132 The number of CSF (in LS-coupling): 184  
 Weights of major contributors to ASF in jj-coupling:

Level	J	Parity	CSF contributions											
1	0	-	0.89670 of	2	0.08762 of	1	0.00642 of	7	0.00250 of	13				
			0.00204 of	9										
Total sum over weight (in jj) is: 0.99907840477285059														

Definition of leading CSF:

2)	2s ( 2)	2p-( 2)	2p ( 4)	3s ( 1)	3p-( 1)	3p ( 2)				
				1/2	1/2					
					1/2		0			

Weights of major contributors to ASF in LS-coupling:

Level	J	Parity	CSF contributions											
1	0	-	0.89670 of	2	0.08762 of	1	0.00821 of	4	0.00441 of	11				
Total sum over weight (in LSJ) is: 0.99862429376844597														

Definition of leading CSF:

1)	2s ( 2)	2p ( 6)	3s ( 2)	3p ( 1)	3d ( 1)					
	1S0	1S0	1S0	2P1	2D1	1S	1S	2P	3P	0
2)	2s ( 2)	2p ( 6)	3s ( 1)	3p ( 3)						
	1S0	1S0	2S1	2P1	1S	2S	3P	0		
4)	2s ( 2)	2p ( 6)	3s ( 1)	3p ( 1)	3d ( 2)					
	1S0	1S0	2S1	2P1	1S0	1S	2S	3P	3P	0
11)	2s ( 2)	2p ( 6)	3p ( 3)	3d ( 1)						
	1S0	1S0	2P1	2D1	1S	2P	3P	0		

The new level is under investigation.

Weights of major contributors to ASF in jj-coupling:

Level	J	Parity	CSF contributions											
2	0	-	0.88679 of	1	0.08724 of	2	0.00640 of	4	0.00505 of	13				
			0.00354 of	10										
Total sum over weight (in jj) is: 0.99887286591520896														

Definition of leading CSF:

1)	2s ( 2)	2p-( 2)	2p ( 4)	3s ( 2)	3p ( 1)	3d-( 1)				
					3/2	3/2				
						3/2	0			

Weights of major contributors to ASF in LS-coupling:

Level	J	Parity	CSF contributions							
2	0	-	0.88679 of	1	0.08724 of	2	0.00852 of	11	0.00670 of	3
			0.00537 of	8	0.00251 of	6				
Total sum over weight (in LSJ) is: 0.99726815958280934										

Definition of leading CSF:

1)	2s( 2)	2p( 6)	3s( 2)	3p( 1)	3d( 1)						
	1S0	1S0	1S0	2P1	2D1	1S	1S	2P	3P	0	
2)	2s( 2)	2p( 6)	3s( 1)	3p( 3)							
	1S0	1S0	2S1	2P1	1S	2S	3P	0			
3)	2s( 2)	2p( 6)	3s( 1)	3p( 1)	3d( 2)						
	1S0	1S0	2S1	2P1	3P2	1S	2S	1P	3P	0	
6)	2s( 2)	2p( 6)	3s( 1)	3p( 1)	3d( 2)						
	1S0	1S0	2S1	2P1	3P2	1S	2S	3P	3P	0	
8)	2s( 2)	2p( 6)	3s( 1)	3p( 1)	3d( 2)						
	1S0	1S0	2S1	2P1	1D2	1S	2S	3P	3P	0	
11)	2s( 2)	2p( 6)	3p( 3)	3d( 1)							
	1S0	1S0	2P1	2D1	1S	2P	3P	0			

jj2lsj: Execution complete.

The program, in default mode, produces the name .lsj .lbl file in which, for each ASF, the position, J, parity, total energy (in hartrees), and percentage of the wave function compositions are provided, followed by a list of expansion coefficients, their squares (compositions), and the CSF in LSJ-coupling. The example for odd7. lsj .lbl is given below. The label of the ASF is given by the the notation of the first line. So the level with total energy -2794.938367562 is labeled 2s(2) .2p(6) .3s(2) .3p\_2P .3d\_3F.

Output file odd7.lsj.lbl

```
-----
```

Pos	J	Parity	Energy Total	Comp. of ASF
1	0	-	-2795.294072330	99.862%
			0.94694267	0.89670042 2s(2) .2p(6) .3s_2S .3p(3)2P1_3P
			-0.29599906	0.08761544 2s(2) .2p(6) .3s(2) .3p_2P .3d_3P
			-0.09062556	0.00821299 2s(2) .2p(6) .3s_2S .3p_3P .3d(2)1S0_3P
			-0.06641103	0.00441042 2s(2) .2p(6) .3p(3)2P1_2P .3d_3P
2	0	-	-2793.959522946	99.727%
			-0.94169405	0.88678769 2s(2) .2p(6) .3s(2) .3p_2P .3d_3P
			0.29537085	0.08724394 2s(2) .2p(6) .3s_2S .3p(3)2P1_3P
			-0.09229288	0.00851798 2s(2) .2p(6) .3p(3)2P1_2P .3d_3P
			0.08186357	0.00670164 2s(2) .2p(6) .3s_2S .3p_1P .3d(2)3P2_3P
			-0.07330494	0.00537361 2s(2) .2p(6) .3s_2S .3p_3P .3d(2)1D2_3P
			-0.05007114	0.00250712 2s(2) .2p(6) .3s_2S .3p_3P .3d(2)3P2_3P
.....				
4	2	-	-2794.938367562	99.746%
			0.61826021	0.38224569 2s(2) .2p(6) .3s(2) .3p_2P .3d_3F
			0.54278368	0.29461412 2s(2) .2p(6) .3s_2S .3p(3)2P1_3P
			0.37809496	0.14295580 2s(2) .2p(6) .3s(2) .3p_2P .3d_1D
			0.29469334	0.08684416 2s(2) .2p(6) .3s_2S .3p(3)2D3_3D
			0.17060037	0.02910449 2s(2) .2p(6) .3s(2) .3p_2P .3d_3P
			-0.16453825	0.02707283 2s(2) .2p(6) .3s_2S .3p(3)4S3_5S
			0.12507106	0.01564277 2s(2) .2p(6) .3s_2S .3p(3)2D3_1D
			-0.06574377	0.00432224 2s(2) .2p(6) .3s(2) .3p_2P .3d_3D
			0.06041988	0.00365056 2s(2) .2p(6) .3p(3)2P1_2P .3d_3F



```

0.05069300  0.00256978  2s(2).2p(6).3s_2S.3p_3P.3d(2)1S0_3P
0.03868154  0.00149626  2s(2).2p(6).3p(3)2P1_2P.3d_3P
0.03576268  0.00127897  2s(2).2p(6).3p(3)2P1_2P.3d_1D
-0.03187628  0.00101610  2s(2).2p(6).3s_2S.3p_1P.3d(2)3F2_3F

```

When the unique labeling option is chosen, the name .uni.lsj.lbl and name .uni.lsj.sum files are produced. The format and information in the name .uni.lsj.lbl is the same as in name .lsj.lbl, but all the levels have unique labels. Please note that the third level, with total energy -2794.938367562, and a smaller largest component, was relabeled as 2s(2).2p(6).3s\_2S.3p(3)2P1\_3P since the <sup>3</sup>F label had already been assigned.

Output file odd7.uni.lsj.lbl

Pos	J	Parity	Energy Total	Comp. of ASF
1	0	-	-2795.294072330	99.862%
			0.94694267	0.89670042 2s(2).2p(6).3s_2S.3p(3)2P1_3P
			-0.29599906	0.08761544 2s(2).2p(6).3s(2).3p_2P.3d_3P
			-0.09062556	0.00821299 2s(2).2p(6).3s_2S.3p_3P.3d(2)1S0_3P
			-0.06641103	0.00441042 2s(2).2p(6).3p(3)2P1_2P.3d_3P
2	0	-	-2793.959522946	99.727%
			-0.94169405	0.88678769 2s(2).2p(6).3s(2).3p_2P.3d_3P
			0.29537085	0.08724394 2s(2).2p(6).3s_2S.3p(3)2P1_3P
			-0.09229288	0.00851798 2s(2).2p(6).3p(3)2P1_2P.3d_3P
			0.08186357	0.00670164 2s(2).2p(6).3s_2S.3p_1P.3d(2)3P2_3P
			-0.07330494	0.00537361 2s(2).2p(6).3s_2S.3p_3P.3d(2)1D2_3P
			-0.05007114	0.00250712 2s(2).2p(6).3s_2S.3p_3P.3d(2)3P2_3P
4	2	-	-2794.938367562	99.746%
			0.54278368	0.29461412 2s(2).2p(6).3s_2S.3p(3)2P1_3P
			0.61826021	0.38224569 2s(2).2p(6).3s(2).3p_2P.3d_3F
			0.37809496	0.14295580 2s(2).2p(6).3s(2).3p_2P.3d_1D
			0.29469334	0.08684416 2s(2).2p(6).3s_2S.3p(3)2D3_3D
			0.17060037	0.02910449 2s(2).2p(6).3s(2).3p_2P.3d_3P
			-0.16453825	0.02707283 2s(2).2p(6).3s_2S.3p(3)4S3_5S
			0.12507106	0.01564277 2s(2).2p(6).3s_2S.3p(3)2D3_1D
			-0.06574377	0.00432224 2s(2).2p(6).3s(2).3p_2P.3d_3D
			0.06041988	0.00365056 2s(2).2p(6).3p(3)2P1_2P.3d_3F
			0.05069300	0.00256978 2s(2).2p(6).3s_2S.3p_3P.3d(2)1S0_3P
			0.03868154	0.00149626 2s(2).2p(6).3p(3)2P1_2P.3d_3P
			0.03576268	0.00127897 2s(2).2p(6).3p(3)2P1_2P.3d_1D
			-0.03187628	0.00101610 2s(2).2p(6).3s_2S.3p_1P.3d(2)3F2_3F

Below is the odd7.uni.lsj.sum file that provides the information - J, position, composition, serial number, and identification - for each ASF, where the serial number is the number of CSFs used in determining the composition. If the serial number of the composition is equal 1 the level is identified with the largest expansion coefficient, if 2, ..., etc., as in example below for levels with J = 2 Pos = 4 and Pos = 8, the levels are relabeled.

Output file odd7.uni.lsj.sum

```
-----
      Composition  Serial No.      Coupling
              of compos.
J =      0
-----
Pos  1  0.896700420  1  2s(2).2p(6).3s_2S.3p(3)2P1_3P
Pos  2  0.886787690  1  2s(2).2p(6).3s(2).3p_2P.3d_3P
-----
```

```
.....
      Composition  Serial No.      Coupling
              of compos.
J =      2
-----
Pos  1  0.816598140  1  2s(2).2p(6).3s_2S.3p(3)4S3_5S
Pos  2  0.623434900  1  2s(2).2p(6).3s_2S.3p(3)2D3_3D
Pos  6  0.495079260  1  2s(2).2p(6).3s(2).3p_2P.3d_3P
Pos  5  0.477147080  1  2s(2).2p(6).3s(2).3p_2P.3d_3F
Pos  7  0.400735720  1  2s(2).2p(6).3s(2).3p_2P.3d_3D
Pos  4  0.294614120  2  2s(2).2p(6).3s_2S.3p(3)2P1_3P
Pos  3  0.283483530  1  2s(2).2p(6).3s_2S.3p(3)2D3_1D
Pos  8  0.137996860  3  2s(2).2p(6).3s(2).3p_2P.3d_1D
-----
```

The program can also be used in non-default mode. The typical run proceeds as follows:

```
Default settings? (y/n)
>>n
All levels (Y/N)
>>y
Maximum % of omitted composition
>>0.5
What is the value below which an eigenvector component is to be neglected
in the determination of the LSJ expansion: should be smaller than: 0.00500
>>0.003
What is the value below which an eigenvector composition is to be neglected
for printing?
>>0.0005
Do you need the output file *.lsj.c? (y/n)
>>y
Do you need the output file *.lsj.j? (y/n)
>>y
```

The non-default mode is useful in several cases:

(1) The present code allows the user, through the first parameter (0.5), to select the maximum percentage of the ASF composition that can be omitted. Given this information and with the help of the second parameter (0.003), it is easy to derive the largest small coefficient in the CSF expansion that may be included. However, with many components of about the same size, smaller values may be needed to meet the original objective. In this implementation, the user specifies the CSFs that can be omitted. The remaining CSFs define the basis that is to be transformed. By transforming this basis in decreasing order of importance, the desired percentage of the wave function can be transformed. A third parameter (0.0005) controls the printing of expansion coefficients in the *LSJ* basis and their contribution to the composition of the wave function. The default is to transform at least 99% of the wave function composition and print components in *LSJ* that contribute more than 0.1% to the composition. The cut-off for the *jj*-expansion has the value of 0.005, whereas the cut-off for printing is 0.001.

(2) In particular, the user may request a complete transformation, with a resulting list of CSFs in *LSJ*-coupling in name.lsj.c and their expansion coefficients in name.lsj.j. The two files have the same format as in ATSP2K [14]. Complete expansions are feasible only for small expansions. In this case the first and second parameter should be 0.

(3) The non-default option should be used if we choose a unique labeling option, but the program will not give the unique identification for all levels. In this case we need to transform a larger amount of ASF with larger number of expansion coefficients. It can be done with help of the first and second parameter.

4. Results

In the recent calculations of energy spectra for Sr XXV [4] two pairs of odd levels with  $J = 2$  had the same label and were separated by adding subscripts 'a' and 'b'. In the NIST database [15] for two ( $3s\ 3p^3\ (^2P) \ ^3P_2^o$  and the  $3s^2\ 3p\ 3d\ (^3F_2^o)$ ) of these levels there is no data and the  $3s^2\ 3p\ 3d\ ^1D_2^o$  level is not identified.

Running the JJ2LSJ program for Sr XXV levels 13 and 25 are relabeled in the Table 1. Table 1 gives also the labels from [4]. As we see level 13 had the same label as level 14, and 25 was labeled as 17. In Table 1 also the compositions in *LSJ*-coupling are given. In the Table 2 transition data of E1, M1, M2 transitions for relabeled levels are presented.

**Table 1.** Energy levels in  $\text{cm}^{-1}$  and *LSJ*-composition for Si-like Sr. In the original data levels 13 and 14 had the same label and subscripts 'a' and 'b' were introduced to separate the levels. Using the JJ2LSJ program levels 13 and 14 are now assigned unique labels.

No.	Level [4]	Level (Relabeled)	<i>LSJ</i> -Composition	$n = 7$
1	$3s^2\ 3p^2\ (^3P) \ ^3P_0$	$3s^2\ 3p^2\ (^3P) \ ^3P_0$	$0.82 + 0.16\ 3s^2\ 3p^2\ (^1S) \ ^1S$	0
2	$3s^2\ 3p^2\ (^3P) \ ^3P_1$	$3s^2\ 3p^2\ (^3P) \ ^3P_1$	0.98	92 950
3	$3s^2\ 3p^2\ (^3P) \ ^3P_2$	$3s^2\ 3p^2\ (^3P) \ ^3P_2$	$0.54 + 0.44\ 3s^2\ 3p^2\ (^1D) \ ^1D$	122 240
4	$3s^2\ 3p^2\ (^1D) \ ^1D_2$	$3s^2\ 3p^2\ (^1D) \ ^1D_2$	$0.54 + 0.44\ 3s^2\ 3p^2\ (^3P) \ ^3P$	239 120
5	$3s^2\ 3p^2\ (^1S) \ ^1S_0$	$3s^2\ 3p^2\ (^1S) \ ^1S_0$	$0.81 + 0.16\ 3s^2\ 3p^2\ (^3P) \ ^3P$	313 384
6	$3s\ 3p^3\ (^4S) \ ^5S_2^o$	$3s\ 3p^3\ (^4S) \ ^5S_2^o$	$0.82 + 0.14\ 3s\ 3p^3\ (^2P) \ ^3P^o + 0.02\ 3s\ 3p^3\ (^3D) \ ^3D^o$	537 112
7	$3s\ 3p^3\ (^3D) \ ^3D_1^o$	$3s\ 3p^3\ (^3D) \ ^3D_1^o$	$0.64 + 0.17\ 3s\ 3p^3\ (^2P) \ ^3P^o + 0.09\ 3s^2\ 3p\ 3d\ ^3D^o$	648 560
8	$3s\ 3p^3\ (^3D) \ ^3D_2^o$	$3s\ 3p^3\ (^3D) \ ^3D_2^o$	$0.62 + 0.14\ 3s\ 3p^3\ (^2P) \ ^3P^o + 0.11\ 3s\ 3p^3\ (^4S) \ ^5S^o$	665 804
9	$3s\ 3p^3\ (^3D) \ ^3D_3^o$	$3s\ 3p^3\ (^3D) \ ^3D_3^o$	$0.88 + 0.10\ 3s^2\ 3p\ 3d\ ^3D^o$	700 704
10	$3s\ 3p^3\ (^2P) \ ^3P_0^o$	$3s\ 3p^3\ (^2P) \ ^3P_0^o$	$0.90 + 0.09\ 3s^2\ 3p\ 3d\ ^3P^o$	767 747
11	$3s\ 3p^3\ (^2D) \ ^1D_2^o$	$3s\ 3p^3\ (^2D) \ ^1D_2^o$	$0.28 + 0.23\ 3s^2\ 3p\ 3d\ ^1D^o + 0.17\ 3s\ 3p^3\ (^2P) \ ^3P^o$	772 281
12	$3s\ 3p^3\ (^2P) \ ^3P_1^o$	$3s\ 3p^3\ (^2P) \ ^3P_1^o$	$0.66 + 0.16\ 3s\ 3p^3\ (^3D) \ ^3D^o + 0.07\ 3s^2\ 3p\ 3d\ ^3P^o$	779 904
13	$3s^2\ 3p\ 3d\ ^3F_2^o_a$	$3s\ 3p^3\ (^2P) \ ^3P_2^o$	$0.29 + 0.38\ 3s^2\ 3p\ 3d\ ^3F^o + 0.14\ 3s^2\ 3p\ 3d\ ^1D^o$	845 815
14	$3s^2\ 3p\ 3d\ ^3F_2^o_b$	$3s^2\ 3p\ 3d\ ^3F_2^o$	$0.48 + 0.21\ 3s\ 3p^3\ (^3D) \ ^1D^o + 0.13\ 3s\ 3p^3\ (^2P) \ ^3P^o$	882 783
15	$3s\ 3p^3\ (^4S) \ ^3S_1^o$	$3s\ 3p^3\ (^4S) \ ^3S_1^o$	$0.55 + 0.32\ 3s\ 3p^3\ (^2P) \ ^1P^o + 0.04\ 3s\ 3p^3\ (^3P) \ ^3P^o$	884 118
16	$3s^2\ 3p\ 3d\ ^3F_3^o$	$3s^2\ 3p\ 3d\ ^3F_3^o$	$0.89 + 0.04\ 3s^2\ 3p\ 3d\ ^3D^o + 0.03\ 3s^2\ 3p\ 3d\ ^1F^o$	906 676
17	$3s^2\ 3p\ 3d\ ^3P_2^o_a$	$3s^2\ 3p\ 3d\ ^3P_2^o$	$0.50 + 0.20\ 3s^2\ 3p\ 3d\ ^3D^o + 0.16\ 3s\ 3p^3\ (^3D) \ ^1D^o$	967 289
18	$3s^2\ 3p\ 3d\ ^3D_1^o$	$3s^2\ 3p\ 3d\ ^3D_1^o$	$0.42 + 0.26\ 3s^2\ 3p\ 3d\ ^3P^o + 0.16\ 3s^2\ 3p\ 3d\ ^1P^o$	971 435
19	$3s^2\ 3p\ 3d\ ^3F_4^o$	$3s^2\ 3p\ 3d\ ^3F_4^o$	0.98	989 440
20	$3s\ 3p^3\ (^2P) \ ^1P_1^o$	$3s\ 3p^3\ (^2P) \ ^1P_1^o$	$0.42 + 0.31\ 3s\ 3p^3\ (^4S) \ ^3S^o + 0.17\ 3s^2\ 3p\ 3d\ ^3D^o$	1 007 850
21	$3s^2\ 3p\ 3d\ ^3D_2^o$	$3s^2\ 3p\ 3d\ ^3D_2^o$	$0.40 + 0.28\ 3s^2\ 3p\ 3d\ ^1D^o + 0.19\ 3s\ 3p^3\ (^3D) \ ^1D^o$	1 052 275
22	$3s^2\ 3p\ 3d\ ^3P_0^o$	$3s^2\ 3p\ 3d\ ^3P_0^o$	$0.89 + 0.09\ 3s\ 3p^3\ (^2P) \ ^3P^o$	1 060 646
23	$3s^2\ 3p\ 3d\ ^3D_3^o$	$3s^2\ 3p\ 3d\ ^3D_3^o$	$0.72 + 0.10\ 3s^2\ 3p\ 3d\ ^1F^o + 0.08\ 3s\ 3p^3\ (^3D) \ ^3D^o$	1 064 175
24	$3s^2\ 3p\ 3d\ ^3P_1^o$	$3s^2\ 3p\ 3d\ ^3P_1^o$	$0.58 + 0.18\ 3s^2\ 3p\ 3d\ ^3D^o + 0.09\ 3s\ 3p^3\ (^2P) \ ^3P^o$	1 075 683
25	$3s^2\ 3p\ 3d\ ^3P_2^o_b$	$3s^2\ 3p\ 3d\ ^1D_2^o$	$0.14 + 0.37\ 3s^2\ 3p\ 3d\ ^3P^o + 0.23\ 3s^2\ 3p\ 3d\ ^3D^o$	1 091 772
26	$3s^2\ 3p\ 3d\ ^1F_3^o$	$3s^2\ 3p\ 3d\ ^1F_3^o$	$0.84 + 0.11\ 3s^2\ 3p\ 3d\ ^3D^o$	1 147 847
27	$3s^2\ 3p\ 3d\ ^1P_1^o$	$3s^2\ 3p\ 3d\ ^1P_1^o$	$0.73 + 0.12\ 3s\ 3p^3\ (^2P) \ ^1P^o + 0.07\ 3s^2\ 3p\ 3d\ ^3D^o$	1 184 571

Table 2. Transition data for Si-like Sr where each level has been assigned a unique label.

Upper	Lower	EM	$\Delta E$ (cm <sup>-1</sup> )	$\lambda$ (Å)	A (s <sup>-1</sup> )	gf	dT
3s3p <sup>3</sup> ( <sup>2</sup> P) <sup>3</sup> P <sub>2</sub> <sup>o</sup>	3s <sup>2</sup> 3p <sup>2</sup> ( <sup>3</sup> P) <sup>3</sup> P <sub>0</sub>	M2	845815	118.23	9.680E+00	1.014E-10	
3s3p <sup>3</sup> ( <sup>2</sup> P) <sup>3</sup> P <sub>2</sub> <sup>o</sup>	3s <sup>2</sup> 3p <sup>2</sup> ( <sup>3</sup> P) <sup>3</sup> P <sub>1</sub>	E1	752864	132.83	1.712E+07	2.264E-04	0.014
3s3p <sup>3</sup> ( <sup>2</sup> P) <sup>3</sup> P <sub>2</sub> <sup>o</sup>	3s <sup>2</sup> 3p <sup>2</sup> ( <sup>3</sup> P) <sup>3</sup> P <sub>1</sub>	M2	752864	132.83	4.646E+00	6.144E-11	
3s3p <sup>3</sup> ( <sup>2</sup> P) <sup>3</sup> P <sub>2</sub> <sup>o</sup>	3s <sup>2</sup> 3p <sup>2</sup> ( <sup>3</sup> P) <sup>3</sup> P <sub>2</sub>	M2	723575	138.20	1.952E+01	2.795E-10	
3s3p <sup>3</sup> ( <sup>2</sup> P) <sup>3</sup> P <sub>2</sub> <sup>o</sup>	3s <sup>2</sup> 3p <sup>2</sup> ( <sup>3</sup> P) <sup>3</sup> P <sub>2</sub>	E1	723575	138.20	4.775E+09	6.837E-02	0.015
3s3p <sup>3</sup> ( <sup>2</sup> P) <sup>3</sup> P <sub>2</sub> <sup>o</sup>	3s <sup>2</sup> 3p <sup>2</sup> ( <sup>1</sup> D) <sup>1</sup> D <sub>2</sub>	E1	606694	164.83	1.828E+09	3.723E-02	0.021
3s3p <sup>3</sup> ( <sup>2</sup> P) <sup>3</sup> P <sub>2</sub> <sup>o</sup>	3s <sup>2</sup> 3p <sup>2</sup> ( <sup>1</sup> D) <sup>1</sup> D <sub>2</sub>	M2	606694	164.83	1.179E+02	2.402E-09	
3s3p <sup>3</sup> ( <sup>2</sup> P) <sup>3</sup> P <sub>2</sub> <sup>o</sup>	3s <sup>2</sup> 3p <sup>2</sup> ( <sup>1</sup> S) <sup>1</sup> S <sub>0</sub>	M2	532430	187.82	3.162E+01	8.361E-10	
3s <sup>2</sup> 3p3d <sup>1</sup> P <sub>1</sub> <sup>o</sup>	3s3p <sup>3</sup> ( <sup>2</sup> P) <sup>3</sup> P <sub>2</sub> <sup>o</sup>	M1	338756	295.20	2.315E+03	9.072E-08	
3s3p <sup>3</sup> ( <sup>2</sup> P) <sup>3</sup> P <sub>2</sub> <sup>o</sup>	3s3p <sup>3</sup> ( <sup>4</sup> S) <sup>5</sup> S <sub>0</sub> <sup>o</sup>	M1	308702	323.94	1.150E+04	9.043E-07	
3s <sup>2</sup> 3p3d <sup>1</sup> F <sub>3</sub> <sup>o</sup>	3s3p <sup>3</sup> ( <sup>2</sup> P) <sup>3</sup> P <sub>2</sub> <sup>o</sup>	M1	302032	331.09	2.777E+03	3.195E-07	
3s <sup>2</sup> 3p3d <sup>3</sup> D <sub>2</sub> <sup>o</sup>	3s3p <sup>3</sup> ( <sup>2</sup> P) <sup>3</sup> P <sub>2</sub> <sup>o</sup>	M1	245957	406.57	3.507E+03	4.346E-07	
3s <sup>2</sup> 3p3d <sup>3</sup> P <sub>1</sub> <sup>o</sup>	3s3p <sup>3</sup> ( <sup>2</sup> P) <sup>3</sup> P <sub>2</sub> <sup>o</sup>	M1	229868	435.03	1.962E+03	1.670E-07	
3s <sup>2</sup> 3p3d <sup>3</sup> D <sub>3</sub> <sup>o</sup>	3s3p <sup>3</sup> ( <sup>2</sup> P) <sup>3</sup> P <sub>2</sub> <sup>o</sup>	M1	218360	457.96	6.377E+03	1.403E-06	
3s <sup>2</sup> 3p3d <sup>3</sup> D <sub>2</sub> <sup>o</sup>	3s3p <sup>3</sup> ( <sup>2</sup> P) <sup>3</sup> P <sub>2</sub> <sup>o</sup>	M1	206460	484.35	2.293E+03	4.032E-07	
3s3p <sup>3</sup> ( <sup>2</sup> P) <sup>3</sup> P <sub>2</sub> <sup>o</sup>	3s3p <sup>3</sup> ( <sup>2</sup> D) <sup>3</sup> D <sub>1</sub> <sup>o</sup>	M1	197254	506.96	1.069E+03	2.060E-07	
3s3p <sup>3</sup> ( <sup>2</sup> P) <sup>3</sup> P <sub>2</sub> <sup>o</sup>	3s3p <sup>3</sup> ( <sup>2</sup> D) <sup>3</sup> D <sub>2</sub> <sup>o</sup>	M1	180010	555.52	1.380E+04	3.193E-06	
3s3p <sup>3</sup> ( <sup>2</sup> P) <sup>1</sup> P <sub>1</sub> <sup>o</sup>	3s3p <sup>3</sup> ( <sup>2</sup> P) <sup>3</sup> P <sub>2</sub> <sup>o</sup>	M1	162035	617.15	1.312E+03	2.248E-07	
3s3p <sup>3</sup> ( <sup>2</sup> P) <sup>3</sup> P <sub>2</sub> <sup>o</sup>	3s3p <sup>3</sup> ( <sup>2</sup> D) <sup>3</sup> D <sub>3</sub> <sup>o</sup>	M1	145110	689.13	5.267E+03	1.875E-06	
3s <sup>2</sup> 3p3d <sup>3</sup> D <sub>1</sub> <sup>o</sup>	3s3p <sup>3</sup> ( <sup>2</sup> P) <sup>3</sup> P <sub>2</sub> <sup>o</sup>	M1	125620	796.05	3.721E+02	1.061E-07	
3s <sup>2</sup> 3p3d <sup>3</sup> P <sub>2</sub> <sup>o</sup>	3s3p <sup>3</sup> ( <sup>2</sup> P) <sup>3</sup> P <sub>2</sub> <sup>o</sup>	M1	121474	823.22	1.112E+02	5.648E-08	
3s3p <sup>3</sup> ( <sup>2</sup> P) <sup>3</sup> P <sub>2</sub> <sup>o</sup>	3s3p <sup>3</sup> ( <sup>2</sup> D) <sup>1</sup> D <sub>2</sub> <sup>o</sup>	M1	73533	1359.92	3.568E+03	4.947E-06	
3s3p <sup>3</sup> ( <sup>2</sup> P) <sup>3</sup> P <sub>2</sub> <sup>o</sup>	3s3p <sup>3</sup> ( <sup>2</sup> P) <sup>3</sup> P <sub>1</sub> <sup>o</sup>	M1	65910	1517.20	1.725E+03	2.976E-06	
3s <sup>2</sup> 3p3d <sup>3</sup> F <sub>3</sub> <sup>o</sup>	3s3p <sup>3</sup> ( <sup>2</sup> P) <sup>3</sup> P <sub>2</sub> <sup>o</sup>	M1	60861	1643.09	2.184E+03	6.189E-06	
3s3p <sup>3</sup> ( <sup>4</sup> S) <sup>3</sup> S <sub>1</sub> <sup>o</sup>	3s3p <sup>3</sup> ( <sup>2</sup> P) <sup>3</sup> P <sub>2</sub> <sup>o</sup>	M1	38303	2610.71	6.515E+00	1.997E-08	
3s <sup>2</sup> 3p3d <sup>3</sup> F <sub>2</sub> <sup>o</sup>	3s3p <sup>3</sup> ( <sup>2</sup> P) <sup>3</sup> P <sub>2</sub> <sup>o</sup>	M1	36968	2705.00	5.987E+02	3.284E-06	
3s <sup>2</sup> 3p3d <sup>1</sup> D <sub>2</sub> <sup>o</sup>	3s <sup>2</sup> 3p <sup>2</sup> ( <sup>3</sup> P) <sup>3</sup> P <sub>0</sub>	M2	1091772	91.59	9.719E+00	6.112E-11	
3s <sup>2</sup> 3p3d <sup>1</sup> D <sub>2</sub> <sup>o</sup>	3s <sup>2</sup> 3p <sup>2</sup> ( <sup>3</sup> P) <sup>3</sup> P <sub>1</sub>	M2	998822	100.12	2.608E+00	1.960E-11	
3s <sup>2</sup> 3p3d <sup>1</sup> D <sub>2</sub> <sup>o</sup>	3s <sup>2</sup> 3p <sup>2</sup> ( <sup>3</sup> P) <sup>3</sup> P <sub>1</sub>	E1	998822	100.12	5.171E+09	3.886E-02	0.002
3s <sup>2</sup> 3p3d <sup>1</sup> D <sub>2</sub> <sup>o</sup>	3s <sup>2</sup> 3p <sup>2</sup> ( <sup>3</sup> P) <sup>3</sup> P <sub>2</sub>	E1	969532	103.14	8.118E+09	6.474E-02	0.012
3s <sup>2</sup> 3p3d <sup>1</sup> D <sub>2</sub> <sup>o</sup>	3s <sup>2</sup> 3p <sup>2</sup> ( <sup>3</sup> P) <sup>3</sup> P <sub>2</sub>	M2	969532	103.14	1.596E+02	1.273E-09	
3s <sup>2</sup> 3p3d <sup>1</sup> D <sub>2</sub> <sup>o</sup>	3s <sup>2</sup> 3p <sup>2</sup> ( <sup>1</sup> D) <sup>1</sup> D <sub>2</sub>	M2	852652	117.28	5.942E+01	6.127E-10	
3s <sup>2</sup> 3p3d <sup>1</sup> D <sub>2</sub> <sup>o</sup>	3s <sup>2</sup> 3p <sup>2</sup> ( <sup>1</sup> D) <sup>1</sup> D <sub>2</sub>	E1	852652	117.28	1.036E+11	1.068E+00	0.003
3s <sup>2</sup> 3p3d <sup>1</sup> D <sub>2</sub> <sup>o</sup>	3s <sup>2</sup> 3p <sup>2</sup> ( <sup>1</sup> S) <sup>1</sup> S <sub>0</sub>	M2	778388	128.47	6.258E+01	7.742E-10	
3s <sup>2</sup> 3p3d <sup>1</sup> D <sub>2</sub> <sup>o</sup>	3s3p <sup>3</sup> ( <sup>4</sup> S) <sup>5</sup> S <sub>0</sub> <sup>o</sup>	M1	554660	180.29	4.087E+03	9.957E-08	
3s <sup>2</sup> 3p3d <sup>1</sup> D <sub>2</sub> <sup>o</sup>	3s3p <sup>3</sup> ( <sup>2</sup> D) <sup>3</sup> D <sub>1</sub> <sup>o</sup>	M1	443212	225.63	1.341E+02	5.116E-09	
3s <sup>2</sup> 3p3d <sup>1</sup> D <sub>2</sub> <sup>o</sup>	3s3p <sup>3</sup> ( <sup>2</sup> D) <sup>3</sup> D <sub>2</sub> <sup>o</sup>	M1	425968	234.76	6.591E+03	2.723E-07	
3s <sup>2</sup> 3p3d <sup>1</sup> D <sub>2</sub> <sup>o</sup>	3s3p <sup>3</sup> ( <sup>2</sup> D) <sup>3</sup> D <sub>3</sub> <sup>o</sup>	M1	391068	255.71	2.693E+03	1.320E-07	
3s <sup>2</sup> 3p3d <sup>1</sup> D <sub>2</sub> <sup>o</sup>	3s3p <sup>3</sup> ( <sup>2</sup> D) <sup>1</sup> D <sub>2</sub> <sup>o</sup>	M1	319491	313.00	4.115E+01	3.022E-09	
3s <sup>2</sup> 3p3d <sup>1</sup> D <sub>2</sub> <sup>o</sup>	3s3p <sup>3</sup> ( <sup>2</sup> P) <sup>3</sup> P <sub>1</sub> <sup>o</sup>	M1	311868	320.65	2.231E+03	1.719E-07	
3s <sup>2</sup> 3p3d <sup>1</sup> D <sub>2</sub> <sup>o</sup>	3s <sup>2</sup> 3p3d <sup>3</sup> F <sub>3</sub> <sup>o</sup>	M1	208989	478.49	1.141E+03	1.958E-07	
3s <sup>2</sup> 3p3d <sup>1</sup> D <sub>2</sub> <sup>o</sup>	3s3p <sup>3</sup> ( <sup>4</sup> S) <sup>3</sup> S <sub>1</sub> <sup>o</sup>	M1	207654	481.57	1.285E+02	2.234E-08	
3s <sup>2</sup> 3p3d <sup>1</sup> D <sub>2</sub> <sup>o</sup>	3s <sup>2</sup> 3p3d <sup>3</sup> F <sub>3</sub> <sup>o</sup>	M1	185096	540.26	3.272E+03	7.160E-07	
3s <sup>2</sup> 3p3d <sup>1</sup> D <sub>2</sub> <sup>o</sup>	3s <sup>2</sup> 3p3d <sup>3</sup> P <sub>2</sub> <sup>o</sup>	M1	124483	803.32	1.272E+04	6.151E-06	
3s <sup>2</sup> 3p3d <sup>1</sup> D <sub>2</sub> <sup>o</sup>	3s <sup>2</sup> 3p3d <sup>3</sup> P <sub>2</sub> <sup>o</sup>	M1	124483	803.32	1.272E+04	6.151E-06	
3s <sup>2</sup> 3p3d <sup>1</sup> D <sub>2</sub> <sup>o</sup>	3s <sup>2</sup> 3p3d <sup>3</sup> D <sub>1</sub> <sup>o</sup>	M1	120337	831.00	5.753E+02	2.978E-07	
3s <sup>2</sup> 3p3d <sup>1</sup> P <sub>1</sub> <sup>o</sup>	3s <sup>2</sup> 3p3d <sup>1</sup> D <sub>2</sub> <sup>o</sup>	M1	92798	1077.60	2.314E+02	1.208E-07	
3s <sup>2</sup> 3p3d <sup>1</sup> D <sub>2</sub> <sup>o</sup>	3s3p <sup>3</sup> ( <sup>2</sup> P) <sup>1</sup> P <sub>1</sub> <sup>o</sup>	M1	83922	1191.58	7.850E+02	8.355E-07	
3s <sup>2</sup> 3p3d <sup>1</sup> F <sub>3</sub> <sup>o</sup>	3s <sup>2</sup> 3p3d <sup>1</sup> D <sub>2</sub> <sup>o</sup>	M1	56074	1783.34	1.104E+02	3.686E-07	
3s <sup>2</sup> 3p3d <sup>1</sup> D <sub>2</sub> <sup>o</sup>	3s <sup>2</sup> 3p3d <sup>3</sup> D <sub>2</sub> <sup>o</sup>	M1	39497	2531.81	3.077E+01	1.478E-07	
3s <sup>2</sup> 3p3d <sup>1</sup> D <sub>2</sub> <sup>o</sup>	3s <sup>2</sup> 3p3d <sup>3</sup> D <sub>3</sub> <sup>o</sup>	M1	27597	3623.57	1.171E+02	1.153E-06	
3s <sup>2</sup> 3p3d <sup>1</sup> D <sub>2</sub> <sup>o</sup>	3s <sup>2</sup> 3p3d <sup>3</sup> P <sub>1</sub> <sup>o</sup>	M1	16089	6215.18	4.670E+01	1.352E-06	

Another example for which problems with unique labels occur is P-like W. Calculations using the MCDHF and RCI methods show that there are many levels with the same labels [16].

Table 3 presents the part of energy spectra with unique labels and *LSJ*-composition. The levels which were relabeled are marked with grey color.

**Table 3.** *LSJ*-composition and energy levels in  $\text{cm}^{-1}$  for P-like W from relativistic configuration interaction (RCI) calculations. Levels that are assigned new labels using the JJ2LSJ program are marked with grey background.

No.	Level	<i>LSJ</i> -Composition	<i>E</i> (RCI)
1	$3s^2 3p^3 (\frac{3}{2}D) ^2 D_{3/2}^\circ$	0.27 + 0.48 $3s^2 3p^3 (\frac{3}{2}P) ^2 P^\circ$ + 0.25 $3s^2 3p^3 (\frac{4}{3}S) ^4 S^\circ$	0
2	$3s^2 3p^2 (\frac{3}{2}P) ^3 P 3d ^4 F_{3/2}$	0.34 + 0.31 $3s^2 3p^2 (\frac{1}{2}S) ^1 S 3d ^2 D$ + 0.11 $3s^2 3p^2 (\frac{3}{2}P) ^3 P 3d ^4 D$	1 853 012
3	$3s^2 3p^2 (\frac{1}{2}D) ^1 D 3d ^2 F_{5/2}$	0.002 + 0.30 $3s^2 3p^2 (\frac{1}{2}S) ^1 S 3d ^2 D$ + 0.20 $3s^2 3p^2 (\frac{3}{2}P) ^3 P 3d ^4 D$	2 613 799
4	$3s^2 3p^3 (\frac{4}{3}S) ^4 S_{3/2}^\circ$	0.55 + 0.44 $3s^2 3p^3 (\frac{3}{2}D) ^2 D^\circ$	2 752 643
5	$3s^2 3p^3 (\frac{3}{2}D) ^2 D_{5/2}^\circ$	0.99	2 847 490
6	$3s^2 3p^3 (\frac{3}{2}P) ^2 P_{1/2}^\circ$	0.99	2 971 667
7	$3s 3p^4 (\frac{3}{2}P) ^4 P_{5/2}$	0.66 + 0.27 $3s 3p^4 (\frac{1}{2}D) ^2 D$ + 0.02 $3s^2 3p^2 (\frac{1}{2}D) ^1 D 3d ^2 D$	4 157 536
8	$3s 3p^4 (\frac{1}{2}D) ^2 D_{3/2}$	0.24 + 0.33 $3s 3p^4 (\frac{3}{2}P) ^2 P$ + 0.11 $3s 3p^4 (\frac{3}{2}P) ^4 P$	4 398 405
9	$3s 3p^4 (\frac{4}{3}S) ^2 S_{1/2}$	0.54 + 0.24 $3s 3p^4 (\frac{3}{2}P) ^4 P$ + 0.07 $3s 3p^4 (\frac{3}{2}P) ^2 P$	4 413 592
10	$3s^2 3p^2 (\frac{3}{2}P) ^3 P 3d ^4 F_{5/2}$	0.47 + 0.29 $3s^2 3p^2 (\frac{1}{2}D) ^1 D 3d ^2 F$ + 0.16 $3s^2 3p^2 (\frac{3}{2}P) ^3 P 3d ^2 F$	4 584 963
11	$3s^2 3p^2 (\frac{3}{2}P) ^3 P 3d ^4 D_{1/2}$	0.80 + 0.13 $3s^2 3p^2 (\frac{3}{2}P) ^3 P 3d ^2 P$ + 0.04 $3s^2 3p^2 (\frac{3}{2}P) ^3 P 3d ^4 P$	4 611 635
12	$3s^2 3p^2 (\frac{3}{2}P) ^3 P 3d ^4 D_{3/2}$	0.28 + 0.33 $3s^2 3p^2 (\frac{3}{2}P) ^3 P 3d ^4 F$ + 0.12 $3s^2 3p^2 (\frac{3}{2}P) ^3 P 3d ^2 P$	4 613 253
13	$3s^2 3p^2 (\frac{1}{2}D) ^1 D 3d ^2 G_{7/2}$	0.52 + 0.18 $3s^2 3p^2 (\frac{3}{2}P) ^3 P 3d ^4 F$ + 0.14 $3s^2 3p^2 (\frac{3}{2}P) ^3 P 3d ^2 F$	4 683 926
14	$3s^2 3p^2 (\frac{3}{2}P) ^3 P 3d ^2 D_{5/2}$	0.30 + 0.24 $3s^2 3p^2 (\frac{1}{2}D) ^1 D 3d ^2 F$ + 0.12 $3s^2 3p^2 (\frac{3}{2}P) ^3 P 3d ^4 P$	4 922 718
15	$3s^2 3p^2 (\frac{1}{2}D) ^1 D 3d ^2 P_{1/2}$	0.35 + 0.31 $3s^2 3p^2 (\frac{3}{2}P) ^3 P 3d ^4 P$ + 0.18 $3s^2 3p^2 (\frac{1}{2}D) ^1 D 3d ^2 S$	5 004 842
16	$3s^2 3p^2 (\frac{1}{2}D) ^1 D 3d ^2 D_{3/2}$	0.27 + 0.22 $3s^2 3p^2 (\frac{3}{2}P) ^3 P 3d ^4 P$ + 0.15 $3s^2 3p^2 (\frac{1}{2}D) ^1 D 3d ^2 P$	5 009 796
17	$3s^2 3p^2 (\frac{3}{2}P) ^3 P 3d ^4 D_{7/2}$	0.47 + 0.37 $3s^2 3p^2 (\frac{3}{2}P) ^3 P 3d ^4 F$ + 0.07 $3s^2 3p^2 (\frac{3}{2}P) ^3 P 3d ^2 F$	5 242 340
18	$3s^2 3p^2 (\frac{3}{2}P) ^3 P 3d ^2 P_{3/2}$	0.25 + 0.23 $3s^2 3p^2 (\frac{3}{2}P) ^3 P 3d ^4 P$ + 0.20 $3s^2 3p^2 (\frac{1}{2}D) ^1 D 3d ^2 P$	5 342 886
19	$3s^2 3p^2 (\frac{1}{2}D) ^1 D 3d ^2 G_{9/2}$	0.62 + 0.37 $3s^2 3p^2 (\frac{3}{2}P) ^3 P 3d ^4 F$	5 346 296
20	$3s^2 3p^2 (\frac{3}{2}P) ^3 P 3d ^2 F_{5/2}$	0.33 + 0.25 $3s^2 3p^2 (\frac{1}{2}D) ^1 D 3d ^2 D$ + 0.22 $3s^2 3p^2 (\frac{3}{2}P) ^3 P 3d ^4 D$	5 371 289
21	$3s^2 3p^2 (\frac{3}{2}P) ^3 P 3d ^4 P_{5/2}$	0.35 + 0.27 $3s^2 3p^2 (\frac{1}{2}D) ^1 D 3d ^2 D$ + 0.14 $3s^2 3p^2 (\frac{3}{2}P) ^3 P 3d ^2 D$	5 534 143
22	$3s^2 3p^2 (\frac{1}{2}D) ^1 D 3d ^2 F_{7/2}$	0.44 + 0.18 $3s^2 3p^2 (\frac{3}{2}P) ^3 P 3d ^2 F$ + 0.17 $3s^2 3p^2 (\frac{3}{2}P) ^3 P 3d ^4 F$	5 544 364
23	$3s^2 3p^2 (\frac{3}{2}P) ^3 P 3d ^2 D_{3/2}$	0.46 + 0.22 $3s^2 3p^2 (\frac{1}{2}D) ^1 D 3d ^2 P$ + 0.14 $3s^2 3p^2 (\frac{1}{2}D) ^1 D 3d ^2 D$	5 614 260
24	$3s^2 3p^2 (\frac{1}{2}D) ^1 D 3d ^2 S_{1/2}$	0.36 + 0.31 $3s^2 3p^2 (\frac{3}{2}P) ^3 P 3d ^2 P$ + 0.23 $3s^2 3p^2 (\frac{1}{2}D) ^1 D 3d ^2 P$	5 645 215
25	$3s^2 3p^3 (\frac{3}{2}P) ^2 P_{3/2}^\circ$	0.51 + 0.28 $3s^2 3p^3 (\frac{3}{2}D) ^2 D^\circ$ + 0.20 $3s^2 3p^3 (\frac{4}{3}S) ^4 S^\circ$	5 738 961
26	$3s 3p^3 (\frac{4}{3}S) ^5 S 3d ^6 D_{5/2}^\circ$	0.19 + 0.20 $3s^2 3p^2 (\frac{3}{2}P) ^3 P 3d ^4 F^\circ$ + 0.11 $3s 3p^3 (\frac{3}{2}P) ^3 P 3d ^4 F^\circ$	5 975 676
27	$3s 3p^3 (\frac{3}{2}P) ^3 P 3d ^4 D_{3/2}^\circ$	0.20 + 0.23 $3s 3p^3 (\frac{4}{3}S) ^5 S 3d ^6 D^\circ$ + 0.14 $3s 3p^3 (\frac{3}{2}P) ^3 P 3d ^4 P^\circ$	5 993 157
28	$3s 3p^3 (\frac{3}{2}D) ^3 D 3d ^4 P_{1/2}^\circ$	0.06 + 0.39 $3s 3p^3 (\frac{3}{2}P) ^3 P 3d ^4 P^\circ$ + 0.29 $3s 3p^3 (\frac{4}{3}S) ^5 S 3d ^6 D^\circ$	6 011 091
29	$3s 3p^3 (\frac{3}{2}P) ^3 P 3d ^4 F_{7/2}^\circ$	0.23 + 0.17 $3s 3p^3 (\frac{3}{2}P) ^3 P 3d ^2 F^\circ$ + 0.16 $3s 3p^3 (\frac{4}{3}S) ^5 S 3d ^6 D^\circ$	6 061 088
30	$3s 3p^3 (\frac{3}{2}D) ^3 D 3d ^4 F_{3/2}^\circ$	0.12 + 0.20 $3s 3p^3 (\frac{3}{2}P) ^1 P 3d ^2 D^\circ$ + 0.11 $3s 3p^3 (\frac{3}{2}P) ^3 P 3d ^4 P^\circ$	6 210 048
31	$3s 3p^3 (\frac{3}{2}D) ^3 D 3d ^4 G_{5/2}^\circ$	0.20 + 0.21 $3s 3p^3 (\frac{3}{2}P) ^1 P 3d ^2 F^\circ$ + 0.11 $3s^2 3p 3d^2 (\frac{3}{2}F) ^4 G^\circ$	6 299 645
32	$3s 3p^3 (\frac{3}{2}D) ^3 D 3d ^4 D_{1/2}^\circ$	0.11 + 0.25 $3s 3p^3 (\frac{3}{2}P) ^1 P 3d ^2 P^\circ$ + 0.17 $3s 3p^3 (\frac{4}{3}S) ^3 S 3d ^4 D^\circ$	6 335 321
33	$3s^2 3p 3d^2 (\frac{3}{2}F) ^4 G_{5/2}^\circ$	0.42 + 0.15 $3s^2 3p 3d^2 (\frac{1}{2}D) ^2 F^\circ$ + 0.13 $3s^2 3p 3d^2 (\frac{3}{2}F) ^2 F^\circ$	6 551 091
34	$3s 3p^3 (\frac{3}{2}D) ^3 D 3d ^4 G_{9/2}^\circ$	0.10 + 0.47 $3s 3p^3 (\frac{3}{2}P) ^3 P 3d ^4 F^\circ$ + 0.30 $3s 3p^3 (\frac{4}{3}S) ^5 S 3d ^6 D^\circ$	6 636 519
35	$3s 3p^3 (\frac{3}{2}D) ^1 D 3d ^2 D_{5/2}^\circ$	0.05 + 0.20 $3s 3p^3 (\frac{3}{2}P) ^3 P 3d ^4 P^\circ$ + 0.16 $3s 3p^3 (\frac{3}{2}P) ^3 P 3d ^2 D^\circ$	6 771 988
36	$3s 3p^3 (\frac{4}{3}S) ^5 S 3d ^6 D_{7/2}^\circ$	0.14 + 0.23 $3s 3p^3 (\frac{3}{2}P) ^3 P 3d ^2 F^\circ$ + 0.19 $3s 3p^3 (\frac{3}{2}P) ^3 P 3d ^4 D^\circ$	6 832 810
37	$3s 3p^3 (\frac{3}{2}D) ^3 D 3d ^2 D_{3/2}^\circ$	0.07 + 0.19 $3s 3p^3 (\frac{3}{2}P) ^3 P 3d ^2 D^\circ$ + 0.17 $3s 3p^3 (\frac{4}{3}S) ^5 S 3d ^4 D^\circ$	6 845 169
38	$3s^2 3p 3d^2 (\frac{3}{2}P) ^4 D_{1/2}^\circ$	0.36 + 0.26 $3s^2 3p 3d^2 (\frac{1}{2}S) ^2 P^\circ$ + 0.12 $3s^2 3p 3d^2 (\frac{3}{2}P) ^2 P^\circ$	6 891 509
39	$3s^2 3p 3d^2 (\frac{3}{2}F) ^4 F_{3/2}^\circ$	0.30 + 0.25 $3s^2 3p 3d^2 (\frac{3}{2}F) ^2 D^\circ$ + 0.07 $3s^2 3p 3d^2 (\frac{3}{2}F) ^4 D^\circ$	6 929 835
40	$3s 3p^3 (\frac{3}{2}P) ^1 P 3d ^2 F_{7/2}^\circ$	0.25 + 0.16 $3s 3p^3 (\frac{4}{3}S) ^3 S 3d ^4 D^\circ$ + 0.11 $3s 3p^3 (\frac{3}{2}D) ^3 D 3d ^4 G^\circ$	6 971 178
41	$3s 3p^4 (\frac{3}{2}P) ^4 P_{3/2}$	0.70 + 0.16 $3s 3p^4 (\frac{1}{2}D) ^2 D$ + 0.03 $3s^2 3p^2 (\frac{3}{2}P) ^3 P 3d ^4 D$	6 998 090
42	$3s 3p^3 (\frac{3}{2}P) ^3 P 3d ^2 P_{1/2}^\circ$	0.36 + 0.27 $3s 3p^3 (\frac{4}{3}S) ^5 S 3d ^4 D^\circ$ + 0.07 $3s 3p^3 (\frac{3}{2}P) ^3 P 3d ^4 D^\circ$	7 042 278
43	$3s 3p^3 (\frac{3}{2}P) ^1 P 3d ^2 D_{5/2}^\circ$	0.17 + 0.12 $3s 3p^3 (\frac{3}{2}P) ^3 P 3d ^2 F^\circ$ + 0.09 $3s 3p^3 (\frac{3}{2}D) ^3 D 3d ^4 F^\circ$	7 084 012
44	$3s 3p^3 (\frac{3}{2}P) ^1 P 3d ^2 P_{3/2}^\circ$	0.18 + 0.13 $3s 3p^3 (\frac{3}{2}D) ^3 D 3d ^4 P^\circ$ + 0.11 $3s 3p^3 (\frac{4}{3}S) ^5 S 3d ^2 D^\circ$	7 100 823
45	$3s 3p^4 (\frac{1}{2}D) ^2 D_{5/2}$	0.63 + 0.24 $3s 3p^4 (\frac{3}{2}P) ^4 P$ + 0.04 $3s^2 3p^2 (\frac{3}{2}P) ^3 P 3d ^4 D$	7 144 999
46	$3s^2 3p 3d^2 (\frac{3}{2}F) ^4 G_{7/2}^\circ$	0.55 + 0.14 $3s^2 3p 3d^2 (\frac{3}{2}F) ^2 G^\circ$ + 0.13 $3s^2 3p 3d^2 (\frac{3}{2}F) ^4 F^\circ$	7 224 945

## 5. Conclusions

In this paper, a new version of the JJ2LSJ program, consistent with the approach described in [7–10], is presented. The program performs the transformation of ASFs from a *jj*-to *LSJ*-coupling and provides the option to assign all level unique labels. Examples of the program use and explanations of possible options are given. In the paper, a few cases (Si-like Sr and P-like W) where the problem with unique labeling in energy spectra occur, are discussed and new labels are assigned.

The program is freely distributed. It may be obtained from the corresponding author.

**Acknowledgments:** Computations were performed on resources at the High Performance Computing Center “HPC Sauletekis” in Vilnius University Faculty of Physics.

**Author Contributions:** Gediminas Gaigalas developed the theory and created algorithms, performed programming work. Charlotte Froese Fischer created algorithms, performed programming work. Pavel Rynkun and Per Jonsson performed the calculations, tested the program. All authors wrote the paper.

**Conflicts of Interest:** The authors declare no conflict of interest.

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Article

# Core Effects on Transition Energies for $3d^k$ Configurations in Tungsten Ions

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Academic Editor: Joseph Reader

Received: 20 December 2016; Accepted: 26 January 2017; Published: 8 February 2017

**Abstract:** All energy levels of the  $3d^k$ ,  $k = 1, 2, \dots, 8, 9$ , configurations for tungsten ions, computed using the GRASP2K fully relativistic code based on the variational multiconfiguration Dirac–Hartree–Fock method, are reported. Included in the calculations are valence correlation where all  $3s, 3p, 3d$  orbitals are considered to be valence orbitals, as well as core–valence and core–core effects from the  $2s, 2p$  subshells. Results are compared with other recent theory and with levels obtained from the wavelengths of lines observed in the experimental spectra. It is shown that the core correlation effects considerably reduce the disagreement with levels linked directly to observed wavelengths, but may differ significantly from the NIST levels, where an unknown shift of the levels could not be determined from experimental wavelengths. For low values of  $k$ , levels were in good agreement with relativistic many-body perturbation levels, but for  $2 < k < 8$ , the present results were in better agreement with observation.

**Keywords:** core correlation effects; energy levels; multiconfiguration Dirac–Hartree–Fock; tungsten ions

## 1. Introduction

Because of their importance for the ITER project [1], spectra of tungsten ions have recently received much attention over a wide range of wavelengths. Of special interest are the NIST EBIT experiments reported by Ralchenko et al. [2], who studied tungsten ions with the ground states  $3d, 3d^2, \dots, 3d^8$ , and  $3d^9$ . Detailed collisional–radiative modelling was undertaken to identify the measured spectral lines. For the modelling they relied on energy levels, radiative transition probabilities, and electron–impact collisional cross-sections obtained using the relativistic Flexible Atomic Code (FAC) [3]. They found that many of the strong lines arose from magnetic dipole (M1) transitions. These lines were located in a narrow range of wavelengths, mostly well isolated with line ratios that could infer plasma properties, and were sensitive to electron densities. All these features make the M1 lines useful for plasma diagnostics. The measured observed wavelengths for M1 transitions and the FAC energy levels were analyzed by Kramida [4] for spectra for these ions, and form the basis for the energy levels included in the Atomic Spectra Database (ASD) [5].

At the same time, highly charged ions are of special interest for theory in that both correlation and relativistic effects are interrelated, and additional quantum electrodynamic (QED) corrections are needed for accurate results. Quinet [6] reports an extensive summary of a large variety of theoretical energy levels and forbidden transitions for all levels of  $3d^k$  ground configurations, and compared their energy levels with the NIST energies. Included among the various methods were results that he obtained using the GRASP code developed by Norrington [7]. Most of the correlation included in the calculation was valence correlation restricted to the  $n = 3$  complex. More recently, Guo et al. [8] computed energy levels, wavelengths, and transition probabilities for the same configurations for a number of ions, including tungsten. The theoretical basis for their work was the relativistic many-body perturbation theory (RMBPT) as described in [9], but small corrections for finite nuclear size, nuclear recoil, vacuum polarization, and self-energy correction were also included using standard procedures such as those in GRASP2K [10]. All basis orbitals were determined from the same central field, and all three types of correlation—valence–valence (VV), core–valence (CV), and core–core (CC)—where the core consists of the the full  $1s, 2s, 2p$  core were included. Statistically, their energy levels were in much better agreement with NIST values than those of Quinet [6].

The purpose of the present work was to evaluate the accuracy of energy levels obtained from variational multiconfiguration Dirac–Hartree–Fock methods as implemented in the GRASP2K code [10]. Included are all three correlation types as in the RMBPT calculation—except for the  $1s^2$  core, that will be assumed to be inactive.

## 2. Multiconfiguration Dirac–Hartree–Fock (MCDHF) and Configuration Interaction Methods

In the MCDHF method [11,12], as implemented in the GRASP2K program package [10], the wave function  $\Psi(\gamma PJM_J)$  for a state labeled  $\gamma PJM_J$ , where  $J$  and  $M_J$  are the angular quantum numbers and  $P$  is the parity, is expanded in antisymmetrized and coupled configuration state functions (CSFs)

$$\Psi(\gamma PJM_J) = \sum_{j=1}^M c_j \Phi(\gamma_j PJM_J). \quad (1)$$

The labels  $\{\gamma_j\}$  denote other appropriate information about the CSFs, such as orbital occupancy and coupling of the subshells. The CSFs are built from products of one-electron orbitals, having the general form

$$\psi_{n\kappa,m}(\mathbf{r}) = \frac{1}{r} \begin{pmatrix} P_{n\kappa}(r)\chi_{\kappa,m}(\theta, \varphi) \\ iQ_{n\kappa}(r)\chi_{-\kappa,m}(\theta, \varphi) \end{pmatrix}, \quad (2)$$

where  $\chi_{\pm\kappa,m}(\theta, \varphi)$  are two-component spin–orbit functions. The radial functions  $\{P_{n\kappa}(r), Q_{n\kappa}(r)\}$  are represented numerically on a grid.

Wave functions for a number of targeted states are determined simultaneously in the extended optimal level (EOL) scheme. Given initial estimates of the radial functions, the energies  $E$  and expansion coefficients  $\mathbf{c} = (c_1, \dots, c_M)^t$  for the targeted states are obtained as solutions to the configuration interaction (CI) problem

$$\mathbf{H}\mathbf{c} = E\mathbf{c}, \quad (3)$$

where  $\mathbf{H}$  is the CI matrix of dimension  $M \times M$  with elements

$$H_{ij} = \langle \Phi(\gamma_i PJM_J) | H | \Phi(\gamma_j PJM_J) \rangle. \quad (4)$$

Radial functions are solutions of systems of differential equations that define a stationary state of an energy functional for a wave function expansion.



Two types of expansions may be used. In the past, both usually were the same, but for large calculations, there are advantages to relaxing this restraint. The first is the expansion that determines the radial functions using the RMCDHF program of the GRASP2K package. For occupied orbitals, optimized radial functions can be obtained by applying the variational principal of an energy expression. However, when correlation orbitals are to be determined, the most effective orbitals are those that are in the same region of space as the occupied orbitals for a given type of correlation, as has been shown in partitioned configuration interaction (PCFI) studies [13]. In this work, we consider two regions: the  $3s, 3p, 3d$  region for valence–valence (VV) correlation and the  $2s, 2p$  region for core–valence (CV) and core–core (CC) correlations.

The second is an expansion for the relativistic configuration interaction (RCI) program that determines the wavefunction and its associated energy for a given Hamiltonian and based on a given orbital basis. In the present work, the Hamiltonian for RCI was the Dirac–Coulomb Hamiltonian (DC) plus the transverse photon interaction (DCB), the vacuum polarization effects as accounted for by the Uehling potential, and electron self-energies as calculated with the screened hydrogenic formula [12,14], namely the DCBQ Hamiltonian. The RCI program is relatively simple to parallelize efficiently [15,16] using message passing. As a result, much larger expansions are possible for RCI calculations than RMCDHF ones that build the orbital basis. Present calculations were done with forty-eight (48) processors for the larger cases.

The computational procedure was essentially the same for all ions. The first step was to perform Dirac–Hartree–Fock (DHF) calculations (in the EOL approximation) for all states associated with the  $3s^2 3p^6 3d^k$  configuration. This calculation determined the  $1s, 2s, 2p$  orbitals for all subsequent calculations. Then, sequentially, orbital sets of increasing size, with maximum principal quantum numbers  $n = 3, 4, 5$ , were determined from expansions that defined valence–valence correlation expansions. The latter were obtained from single- and double-excitations from the valence shells to those of the orbital set. Since the  $3d$  shell is unfilled, excitations such as  $3s^2 \rightarrow 3d^2$  are allowed and increase the generalized occupation number for the  $3d$  orbitals but decrease those of  $3s$ . Variational methods determined the new orbitals introduced at each stage using the Dirac–Coulomb Hamiltonian. The  $n = 6$  orbitals were targeted for core correlation effects. They were obtained from calculations that included CV correlation from the  $n = 2$  shell where one orbital from the active core (either  $2s$  or  $2p$ ) and one  $3s, 3p$ , or  $3d$  orbital were excited, as well as CC, where two  $n = 2$  orbitals were excited. At the same time, excitations from  $3s, 3p$  subshells were limited to single excitations for  $3s$  or  $3p$ , thereby contracting the  $n = 6$  orbitals to overlap more strongly with the  $n = 2$  orbitals and reducing the size of the expansions. For the configurations  $3d^k$ ,  $k = 3, 4, 5, 6, 7$ , the expansions were still exceedingly large and additional restrictions on interactions were imposed that define the energy functional. First, what might be considered a zero-order approximation was obtained that consisted of the CSFs of the  $n = 5$  VV expansion that accounted for 99.9 percent of the normalized expansion. All other terms of the  $n = 6$  expansions were treated as first-order corrections. In deriving the energy expression that determines the radial factors of the  $n = 6$  orbitals, it was assumed that the interaction between CSFs of the first-order corrections could be neglected. This procedure optimizes the interaction of the  $n = 6$  orbitals with the zero-order wave function, and has the effect of contracting the core–valence orbitals.

Each of these four orbital sets were then used in relativistic configuration interaction (RCI) calculations that included VV, CV, and CC correlation effects (excluding the  $1s$  shell) for the three Hamiltonians—DC, DCB, and DCBQ. Again, for the cases where  $k = 3, 4, 5, 6, 7$ , the RCI calculations were performed under the assumption that interactions between CSF of the first-order correction could be ignored.

Table 1 summarizes the size of various expansions for the different  $3d^k$  configurations, whereas Table 2 shows how the mean radii of the  $n = 6$  orbitals are contracted relative to the valence correlation orbitals. Note that the size increases rapidly as the number of electrons (or holes) increases from one to five, as well as the number of  $l$  values and levels. The number of CSFs defining 99.9% of the wave

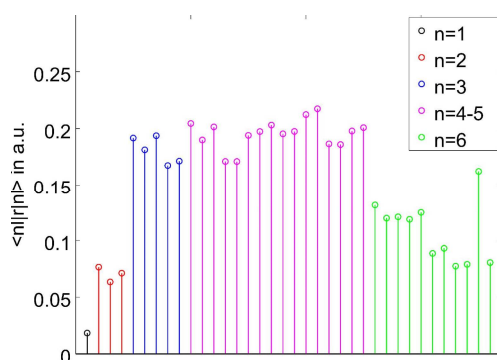
function composition is relatively small. Increasing this percentage to 99.99% would include some higher order corrections. As for mean radii, it should be noted the the  $3d$  orbitals (in non-relativistic notation) have a mean radius closer to the core than either  $3s$  or  $3p$ . Listed in Table 2 are typical values for the  $3d^5$  configuration. The mean radii are also depicted graphically in Figure 1. Correlation increases the generalized orbital occupation number of the  $3d$  orbitals, but decreases those of all other occupied orbitals. The  $n = 4$  and  $n = 5$  orbitals have mean radii similar to those of the valence orbitals, whereas the  $n = 6$  orbitals that are used to represent CC and CV correlation have mean radii either similar to  $n = 2$  orbitals or between  $n = 2$  and  $n = 3$ , as in CV correlation.

**Table 1.** Table showing the size ( $M$ ) of the  $n = 6$  relativistic configuration interaction (RCI) expansions and the size of the zero-order space ( $m$ ) for the different tungsten ions.

$J$	$M$	$m$	$J$	$M$	$m$
$3d$			$3d^9$		
3/2	103 104	-	3/2	152 230	-
5/2	130 021	-	5/2	193 718	-
$3d^2$			$3d^8$		
0	109 376	-	0	138 241	-
1	306 873	-	1	388 664	-
2	453 546	-	2	576 194	-
3	526 871	-	3	672 708	-
4	529 065	-	4	679 881	-
$3d^3$			$3d^7$		
1/2	508 854	514	1/2	584 675	734
3/2	934 941	1 056	3/2	1 075 476	1 564
5/2	1 217 067	1 062	5/2	1 402 693	1 563
7/2	1 328 694	668	7/2	1 535 467	1 020
9/2	1 281 840	737	9/2	1 486 446	1 055
11/2	2216460	277	11/2	1 300 160	353
$3d^4$			$3d^6$		
0	433 540	925	0	462 613	1 113
1	1 228 917	1 070	1	1 311 786	1 244
2	1 840 515	1 688	2	1 965 798	2 071
3	2 187 525	1 375	3	2 338 660	1 738
4	2 261 243	1 624	4	2 420 366	1 921
5	2 095 354	632	5	2 246 438	761
6	1 771 535	572	6	1 902 774	659
$3d^5$					
1/2	1 022 700	1 119			
3/2	1 888 910	1 688			
5/2	2 480 422	2 352			
7/2	2 741 429	1 857			
9/2	2 687 207	1 306			
11/2	2 387 571	910			
13/2	1 943 915	329			

**Table 2.** Mean radii in a.u. of orbitals for the  $3d^5$  configuration and their generalized occupation number  $w$ .

$nl$	$\langle nl r nl\rangle$	$w$
1s	1.83433D-02	2.00000
2s	7.64525D-02	1.99992
2p <sub>-</sub>	6.33222D-02	1.99986
2p	7.10859D-02	3.99969
3s	1.91692D-01	1.99940
3p <sub>-</sub>	1.81324D-01	1.99853
3p	1.93743D-01	3.99577
3d <sub>-</sub>	1.67488D-01	2.00137
3d	1.71346D-01	3.00266
4s	2.04509D-01	1.24D-04
4p <sub>-</sub>	1.89988D-01	1.45D-04
4p	2.01490D-01	2.94D-04
4d <sub>-</sub>	1.71036D-01	1.73D-04
4d	1.70979D-01	2.82D-04
4f <sub>-</sub>	1.94058D-01	5.94D-04
4f	1.97398D-01	8.24D-04
5s	2.03090D-01	1.93D-05
5p <sub>-</sub>	1.95387D-01	2.23D-05
5p	1.97508D-01	4.08D-05
5d <sub>-</sub>	2.12303D-01	2.88D-05
5d	2.17420D-01	4.47D-05
5f <sub>-</sub>	1.86560D-01	1.30D-05
5f	1.85984D-01	2.01D-05
5g <sub>-</sub>	1.97882D-01	3.38D-05
5g	2.00859D-01	5.11D-05
6s	1.31230D-01	6.77D-06
6p <sub>-</sub>	1.19574D-01	8.04D-06
6p	1.20726D-01	1.40D-05
6d <sub>-</sub>	1.18546D-01	1.71D-05
6d	1.24725D-01	2.58D-05
6f <sub>-</sub>	8.84520D-02	7.35D-06
6f	9.29611D-02	1.10D-05
6g <sub>-</sub>	7.72823D-02	2.26D-06
6g	7.88248D-02	3.31D-06
6h <sub>-</sub>	1.62256D-01	2.42D-06
6h	8.04121D-02	7.65D-07



**Figure 1.** Plot of the mean radii of orbitals of the  $3d^5$  configuration in the order listed in Table 2.

### 3. Results and Their Comparison

Table 3 reports some of the results for all levels of the  $3d^k$  configurations of tungsten ions from RCI calculations for the DCBQ Hamiltonian. The classification of energy levels are presented in the  $LSJ$ - and  $jj$ -couplings. A set of three quantum numbers  $L$ ,  $S$ , and seniority  $\nu$  allows a one-to-one classification of  $3d^k$  ( $k = 3, 4, 5, 6, 7$ ) energy levels in  $LSJ$ -coupling. These quantum numbers are presented in Table 3 as  $(^{2S+1})L^\nu$ . The  $n = 5$  results include only VV correlation, whereas  $n = 6$  include all three correlation effects. The next column is the energy levels as reported by NIST [5]. Included here are the different types of results. Energies with no square brackets are directly related to observed wavelengths—often these are in the lower portion of the spectrum. Then, there are levels that may be linked to an observed wavelength but the shift of the energy levels relative to the ground state is not known from experiment. These levels include a  $+x$  or  $+y$  in the table. Thus, the difference between two levels with the same  $+x$  is known accurately, but not the levels themselves. Taking these factors into account, it is clear that the inclusion of core effects has reduced the discrepancy with NIST values by about a factor of 1/2. In the next column, the values found by Quinet [6] are generally like the VV results. From a general theoretical point of view, the the RMBPT results of Guo et al. [8] should be the most accurate. In the case of  $3d^2$ , RMBPT results have also been reported by Safronova and Safronova [17], and are reported in the last column. These results are not as accurate as those of Guo et al. In these tables, all energies are reported in the units of  $1000 \text{ cm}^{-1}$ .

**Table 3.** Energy level results for  $3d, 3d^2, \dots, 3d^8, 3d^9$  ground configuration of tungsten ions. Shown is a unique label in  $LSJ$ - and  $jj$ -notation, the  $J$  value, the present  $n = 5$  result for valence–valence (VV) correlation, and  $n = 6$  result for all three types of correlation, the Atomic Spectra Database (ASD) value [5], the Quinet value [6], the Guo et al. RMBPT<sub>g</sub> value [8], and the Safronova & Safronova RMBPT<sub>s</sub> value [17]. All energy levels are reported in  $1000 \text{ cm}^{-1}$ .

$LSJ$ -	Label $jj$ -Couplings		$J$	Present Work		ASD	GRASP	RMBPT <sub>g</sub>	RMBPT <sub>s</sub>
				$n = 5$	$n = 6$				
W <sup>55+</sup> (K-like)									
$3d^2\ ^2D$	$3d_-$	(3/2,0)	3/2	0.00	0.00	0.00	0.00	0.00	
$3d^2\ ^2D$	$3d_+$	(0,5/2)	5/2	625.23	626.17	626.49	624.7	626.56	
W <sup>54+</sup> (Ca-like)									
$3d^2\ ^3F$	$3d_-^2$	(2,0)	2	0.00	0.00	0.00	0.00	0.00	0.00
$3d^2\ ^3P$	$3d_-^2$	(0,0)	0	186.42	186.23	[188]	186.9	184.86	187.11
$3d^2\ ^3F$	$3d_-3d_+$	(3/2,5/2)	3	584.05	584.75	585.48	583.5	585.80	582.85
$3d^2\ ^3P$	$3d_-3d_+$	(3/2,5/2)	2	667.45	667.96	668.49	667.6	668.00	666.21
$3d^2\ ^3P$	$3d_-3d_+$	(3/2,5/2)	1	706.35	706.75	709.46+x	707.1	706.78	705.41
$3d^2\ ^1G$	$3d_-3d_+$	(3/2,5/2)	4	695.68	696.10	[697]	697.1	696.74	693.81
$3d^2\ ^3F$	$3d_+^2$	(0,4)	4	1234.31	1235.57	[1234]	1234.1	1237.00	1231.64
$3d^2\ ^3P$	$3d_+^2$	(0,2)	2	1298.91	1300.18	[1299]	1298.6	1300.28	1296.73
$3d^2\ ^1S$	$3d_+^2$	(0,0)	0	1492.04	1493.71	[1493]	1491.0	1491.18	1491.54
W <sup>53+</sup> (Sc-like)									
$3d^3\ ^4F^3$	$3d_-^3$	(3/2,0)	3/2	0.00	0.00	0.00	0.00	0.00	
$3d^3\ ^4F^3$	$3d_-^2\ 3d_+$	(2,5/2)	5/2	528.39	529.07	530.03	528.2	530.51	
$3d^3\ ^4P^3$	$3d_-^2\ 3d_+$	(2,5/2)	3/2	579.43	579.99	580.86	579.9	580.86	
$3d^3\ ^2G^3$	$3d_-^2\ 3d_+$	(2,5/2)	7/2	610.41	610.86	[610]	611.7	611.86	
$3d^3\ ^4P^3$	$3d_-^2\ 3d_+$	(2,5/2)	1/2	622.72	623.22	623.95	623.6	623.53	
$3d^3\ ^2H^3$	$3d_-^2\ 3d_+$	(2,5/2)	9/2	609.94	610.32	[610]+x	612.0	611.62	
$3d^3\ ^2D^1$	$3d_-^2\ 3d_+$	(0,5/2)	5/2	811.84	812.07	812.22	814.2	811.77	
$3d^3\ ^4F^3$	$3d_-3d_+^2$	(3/2,4)	7/2	1127.31	1128.60	[1126]	1127.1	1130.58	
$3d^3\ ^4F^3$	$3d_-3d_+^2$	(3/2,4)	9/2	1164.81	1165.99	[1164]	1165.7	1168.15	

Table 3. Cont.

LSJ-	Label <i>jj</i> -Couplings		<i>J</i>	Present Work		ASD	GRASP	RMBPT <sub>g</sub>	RMBPT <sub>s</sub>
				<i>n</i> = 5	<i>n</i> = 6				
3d <sup>3</sup> 4p <sup>3</sup>	3d <sub>-</sub> 3d <sub>+</sub> <sup>2</sup> <sub>+</sub>	(3/2,2)	3/2	1206.41	1207.73	[1206]	1206.2	1208.34	
3d <sup>3</sup> 2p <sup>3</sup>	3d <sub>-</sub> 3d <sub>+</sub> <sup>2</sup> <sub>-</sub>	(3/2,2)	1/2	1230.34	1231.58	[1230]	1230.5	1232.08	
3d <sup>3</sup> 2D <sup>3</sup>	3d <sub>-</sub> 3d <sub>+</sub> <sup>2</sup> <sub>+</sub>	(3/2,4)	5/2	1243.67	1244.61	[1244]	1245.0	1245.39	
3d <sup>3</sup> 2H <sup>3</sup>	3d <sub>-</sub> 3d <sub>+</sub> <sup>2</sup> <sub>+</sub>	(3/2,4)	11/2	1242.38	1243.30	1243.51+x	1245.2	1245.42	
3d <sup>3</sup> 2F <sup>3</sup>	3d <sub>-</sub> 3d <sub>+</sub> <sup>2</sup> <sub>-</sub>	(3/2,2)	5/2	1314.58	1315.54	[1315]	1316.4	1315.84	
3d <sup>3</sup> 2F <sup>3</sup>	3d <sub>-</sub> 3d <sub>+</sub> <sup>2</sup> <sub>+</sub>	(3/2,2)	7/2	1318.68	1319.55	[1320]	1321.5	1320.10	
3d <sup>3</sup> 2D <sup>1</sup>	3d <sub>-</sub> 3d <sub>+</sub> <sup>2</sup> <sub>+</sub>	(3/2,0)	3/2	1479.96	1481.26	[1482]	1481.3	1479.89	
3d <sup>3</sup> 2G <sup>3</sup>	3d <sub>+</sub> <sup>3</sup>	(0,9/2)	9/2	1762.93	1764.86		1762.9	1767.02	
3d <sup>3</sup> 2P <sup>3</sup>	3d <sub>+</sub> <sup>3</sup>	(0,3/2)	3/2	1876.44	1878.32		1877.0	1878.54	
3d <sup>3</sup> 2D <sup>1</sup>	3d <sub>+</sub> <sup>3</sup>	(0,5/2)	5/2	1958.00	1960.12		1957.9	1959.56	
W <sup>52+</sup> (Ti-like)									
3d <sup>4</sup> 3p <sup>2</sup>	3d <sup>4</sup>	(0,0)	0	0.00	0.00	0.00	0.00	0.00	
3d <sup>4</sup> 5D <sup>4</sup>	3d <sub>-</sub> 3d <sub>+</sub>	(3/2,5/2)	1	515.87	516.51	517.63	516.0	518.08	
3d <sup>4</sup> 3H <sup>4</sup>	3d <sub>-</sub> 3d <sub>+</sub>	(3/2,5/2)	4	613.24	613.54	[613]+y	615.6	614.79	
3d <sup>4</sup> 5D <sup>4</sup>	3d <sub>-</sub> 3d <sub>+</sub>	(3/2,5/2)	2	637.98	638.39	[638]+x	639.9	639.34	
3d <sup>4</sup> 3F <sup>2</sup>	3d <sub>-</sub> 3d <sub>+</sub>	(3/2,5/2)	3	665.84	666.09	665.5621+x	668.6	667.04	
3d <sup>4</sup> 5D <sup>4</sup>	3d <sub>-</sub> 3d <sub>+</sub> <sup>2</sup> <sub>-</sub>	(2,2)	0	1101.86	1103.18	[1100]	1101.6	1104.66	
3d <sup>4</sup> 5D <sup>4</sup>	3d <sub>-</sub> 3d <sub>+</sub> <sup>2</sup> <sub>+</sub>	(2,4)	2	1106.82	1107.98	1109.69	1107.6	1110.02	
3d <sup>4</sup> 3H <sup>4</sup>	3d <sub>-</sub> 3d <sub>+</sub> <sup>2</sup> <sub>+</sub>	(2,4)	4	1125.54	1126.59	1127.27+y	1127.3	1129.11	
3d <sup>4</sup> 5D <sup>4</sup>	3d <sub>-</sub> 3d <sub>+</sub> <sup>2</sup> <sub>-</sub>	(2,4)	3	1142.02	1143.02	[1141]	1144.0	1145.19	
3d <sup>4</sup> 3H <sup>4</sup>	3d <sub>-</sub> 3d <sub>+</sub> <sup>2</sup> <sub>+</sub>	(2,4)	5	1172.24	1173.06	1173.35+y	1175.7	1175.60	
3d <sup>4</sup> 3D <sup>4</sup>	3d <sub>-</sub> 3d <sub>+</sub> <sup>2</sup> <sub>+</sub>	(2,2)	1	1213.52	1214.54	[1213]	1215.4	1215.64	
3d <sup>4</sup> 1F <sup>4</sup>	3d <sub>-</sub> 3d <sub>+</sub> <sup>2</sup> <sub>-</sub>	(2,4)	6	1195.60	1196.31	[1195]	1200.00	1199.02	
3d <sup>4</sup> 3F <sup>4</sup>	3d <sub>-</sub> 3d <sub>+</sub> <sup>2</sup> <sub>+</sub>	(2,2)	3	1239.13	1239.92	[1240]	1242.5	1240.99	
3d <sup>4</sup> 3G <sup>4</sup>	3d <sub>-</sub> 3d <sub>+</sub> <sup>2</sup> <sub>-</sub>	(2,2)	4	1242.41	1243.17	[1243]	1245.7	1244.47	
3d <sup>4</sup> 3F <sup>4</sup>	3d <sub>-</sub> 3d <sub>+</sub> <sup>2</sup> <sub>+</sub>	(2,2)	2	1257.75	1258.62	[1258]	1260.6	1259.43	
3d <sup>4</sup> 3F <sup>2</sup>	3d <sub>-</sub> 3d <sub>+</sub> <sup>2</sup> <sub>-</sub>	(2,0)	2	1359.28	1360.44	[1361]	1361.1	1360.35	
3d <sup>4</sup> 3F <sup>2</sup>	3d <sub>-</sub> 3d <sub>+</sub> <sup>2</sup> <sub>+</sub>	(0,4)	4	1403.66	1404.22	1403.95+x	1408.6	1405.11	
3d <sup>4</sup> 1D <sup>2</sup>	3d <sub>-</sub> 3d <sub>+</sub> <sup>2</sup> <sub>-</sub>	(0,2)	2	1505.68	1506.35	[1509]	1510.3	1505.82	
3d <sup>4</sup> 3P <sup>4</sup>	3d <sub>-</sub> 3d <sub>+</sub> <sup>2</sup> <sub>+</sub>	(0,0)	0	1633.13	1634.15	[1637]	1636.5	1632.74	
3d <sup>4</sup> 5D <sup>4</sup>	3d <sub>-</sub> 3d <sub>+</sub> <sup>3</sup>	(3/2,9/2)	4	1714.26	1715.10		1715.3	1718.50	
3d <sup>4</sup> 3F <sup>4</sup>	3d <sub>-</sub> 3d <sub>+</sub> <sup>3</sup>	(3/2,9/2)	3	1725.24	1727.04		1725.9	1729.15	
3d <sup>4</sup> 3D <sup>4</sup>	3d <sub>-</sub> 3d <sub>+</sub> <sup>3</sup>	(3/2,3/2)	1	1766.70	1768.58		1767.1	1769.70	
3d <sup>4</sup> 3G <sup>4</sup>	3d <sub>-</sub> 3d <sub>+</sub> <sup>3</sup>	(3/2,9/2)	5	1773.76	1775.28		1776.4	1777.84	
3d <sup>4</sup> 3H <sup>4</sup>	3d <sub>-</sub> 3d <sub>+</sub> <sup>3</sup>	(3/2,9/2)	6	1778.76	1780.21		1782.4	1783.28	
3d <sup>4</sup> 3F <sup>4</sup>	3d <sub>-</sub> 3d <sub>+</sub> <sup>3</sup>	(3/2,3/2)	2	1841.18	1842.98		1842.9	1843.90	
3d <sup>4</sup> 3D <sup>4</sup>	3d <sub>-</sub> 3d <sub>+</sub> <sup>3</sup>	(3/2,3/2)	3	1857.70	1859.24		1860.2	1860.18	
3d <sup>4</sup> 1S <sup>4</sup>	3d <sub>-</sub> 3d <sub>+</sub> <sup>3</sup>	(3/2,3/2)	0	1922.88	1924.06		1925.8	1923.37	
3d <sup>4</sup> 3P <sup>2</sup>	3d <sub>-</sub> 3d <sub>+</sub> <sup>3</sup>	(3/2,5/2)	1	1983.87	1985.44		1987.2	1985.44	
3d <sup>4</sup> 3F <sup>2</sup>	3d <sub>-</sub> 3d <sub>+</sub> <sup>3</sup>	(3/2,5/2)	3	1979.96	1981.50		1983.6	1981.91	
3d <sup>4</sup> 1G <sup>2</sup>	3d <sub>-</sub> 3d <sub>+</sub> <sup>3</sup>	(3/2,5/2)	4	1985.00	1986.57		1988.7	1987.02	
3d <sup>4</sup> 1D <sup>4</sup>	3d <sub>-</sub> 3d <sub>+</sub> <sup>3</sup>	(3/2,5/2)	2	2018.63	2020.04		2022.8	2019.68	
3d <sup>4</sup> 3F <sup>2</sup>	3d <sub>+</sub> <sup>4</sup>	(0,4)	4	2376.23	2378.86		2376.1	2380.51	
3d <sup>4</sup> 1D <sup>2</sup>	3d <sub>+</sub> <sup>4</sup>	(0,2)	2	2460.51	2463.08		2461.4	2463.56	
3d <sup>4</sup> 3P <sup>2</sup>	3d <sub>+</sub> <sup>4</sup>	(0,0)	0	2662.74	2665.52		2663.5	2663.60	
W <sup>51+</sup> (V-like)									
3d <sup>5</sup> 4p <sup>3</sup>	3d <sub>-</sub> 3d <sub>+</sub>	(0,5/2)	5/2	0.00	0.00	0.00	0.00	0.00	
3d <sup>5</sup> 6S <sup>5</sup>	3d <sub>-</sub> 3d <sub>+</sub> <sup>2</sup> <sub>-</sub>	(3/2,4)	5/2	469.71	470.75	71.63	469.1	472.03	

Table 3. Cont.

LSJ-	Label <i>jj</i> -Couplings	<i>J</i>	Present Work		ASD	GRASP	RMBPT <sub>g</sub>	RMBPT <sub>s</sub>
			<i>n</i> = 5	<i>n</i> = 6				
3d <sup>5</sup> 4G <sup>5</sup>	3d <sub>-</sub> 3d <sub>+</sub> <sup>2</sup> <sub>+</sub> (3/2,4)	7/2	564.98	565.80	66.25	566.2	566.41	
3d <sup>5</sup> 4D <sup>5</sup>	3d <sub>-</sub> 3d <sub>+</sub> <sup>2</sup> <sub>-</sub> (3/2,2)	3/2	579.61	580.50	80.89	579.8	580.44	
3d <sup>5</sup> 2H <sup>3</sup>	3d <sub>-</sub> 3d <sub>+</sub> <sup>2</sup> <sub>+</sub> (3/2,4)	11/2	576.03	576.78	[577] <sub>+x</sub>	578.5	577.80	
3d <sup>5</sup> 2G <sup>5</sup>	3d <sub>-</sub> 3d <sub>+</sub> <sup>2</sup> <sub>-</sub> (3/2,4)	9/2	620.92	621.61	[623]	623.7	622.20	
3d <sup>5</sup> 4D <sup>5</sup>	3d <sub>-</sub> 3d <sub>+</sub> <sup>2</sup> <sub>-</sub> (3/2,2)	5/2	650.71	651.45	[652]	652.8	651.27	
3d <sup>5</sup> 4P <sup>3</sup>	3d <sub>-</sub> 3d <sub>+</sub> <sup>2</sup> <sub>+</sub> (3/2,2)	1/2	679.60	680.38	[681]	680.8	679.83	
3d <sup>5</sup> 2F <sup>5</sup>	3d <sub>-</sub> 3d <sub>+</sub> <sup>2</sup> <sub>-</sub> (3/2,2)	7/2	687.73	688.28	88.18	690.9	687.90	
3d <sup>5</sup> 2D <sup>1</sup>	3d <sub>-</sub> 3d <sub>+</sub> <sup>2</sup> <sub>-</sub> (3/2,0)	3/2	823.99	824.95	[827]	825.5	823.60	
3d <sup>5</sup> 6S <sup>5</sup>	3d <sub>-</sub> 3d <sub>+</sub> <sup>3</sup> <sub>+</sub> (2,9/2)	5/2	1025.98	1027.97	[1015]	1024.9	1029.11	
3d <sup>5</sup> 4D <sup>5</sup>	3d <sub>-</sub> 3d <sub>+</sub> <sup>3</sup> <sub>-</sub> (2,9/2)	7/2	1096.84	1098.61	[1097]	1097.9	1099.59	
3d <sup>5</sup> 4G <sup>5</sup>	3d <sub>-</sub> 3d <sub>+</sub> <sup>3</sup> <sub>+</sub> (2,9/2)	11/2	1100.79	1102.51	1103.43	1103.0	1104.04	
3d <sup>5</sup> 4G <sup>5</sup>	3d <sub>-</sub> 3d <sub>+</sub> <sup>3</sup> <sub>-</sub> (2,9/2)	9/2	1116.98	1118.70	[1118]	1118.8	1119.70	
3d <sup>5</sup> 4D <sup>5</sup>	3d <sub>-</sub> 3d <sub>+</sub> <sup>3</sup> <sub>-</sub> (2,3/2)	1/2	1155.66	1157.40		1156.6	1157.55	
3d <sup>5</sup> 4P <sup>3</sup>	3d <sub>-</sub> 3d <sub>+</sub> <sup>3</sup> <sub>+</sub> (2,5/2)	3/2	1164.73	1166.79		1163.6	1166.64	
3d <sup>5</sup> 2I <sup>5</sup>	3d <sub>-</sub> 3d <sub>+</sub> <sup>3</sup> <sub>+</sub> (2,9/2)	13/2	1142.15	1143.78	[1143]	1145.6	1145.272	
3d <sup>5</sup> 2F <sup>5</sup>	3d <sub>-</sub> 3d <sub>+</sub> <sup>3</sup> <sub>-</sub> (2,3/2)	5/2	1174.89	1176.61		1176.3	1176.63	
3d <sup>5</sup> 2H <sup>3</sup>	3d <sub>-</sub> 3d <sub>+</sub> <sup>3</sup> <sub>-</sub> (2,5/2)	9/2	1217.34	1219.21		1218.4	1219.39	
3d <sup>5</sup> 2G <sup>5</sup>	3d <sub>-</sub> 3d <sub>+</sub> <sup>3</sup> <sub>+</sub> (2,3/2)	7/2	1237.88	1239.44		1240.9	1239.13	
3d <sup>5</sup> 4F <sup>3</sup>	3d <sub>-</sub> 3d <sub>+</sub> <sup>3</sup> <sub>-</sub> (2,5/2)	5/2	1254.59	1256.46		1255.8	1256.02	
3d <sup>5</sup> 2D <sup>5</sup>	3d <sub>-</sub> 3d <sub>+</sub> <sup>3</sup> <sub>-</sub> (2,3/2)	3/2	1259.49	1260.94		1262.1	1259.77	
3d <sup>5</sup> 4P <sup>3</sup>	3d <sub>-</sub> 3d <sub>+</sub> <sup>3</sup> <sub>+</sub> (2,5/2)	1/2	1308.19	1309.93		1309.8	1308.63	
3d <sup>5</sup> 2G <sup>3</sup>	3d <sub>-</sub> 3d <sub>+</sub> <sup>3</sup> <sub>-</sub> (2,5/2)	7/2	1307.82	1309.62		1309.9	1308.84	
3d <sup>5</sup> 2G <sup>3</sup>	3d <sub>-</sub> 3d <sub>+</sub> <sup>3</sup> <sub>+</sub> (0,9/2)	9/2	1379.66	1381.18		1383.8	1380.57	
3d <sup>5</sup> 2P <sup>3</sup>	3d <sub>-</sub> 3d <sub>+</sub> <sup>3</sup> <sub>-</sub> (0,3/2)	3/2	1504.94	1506.22		1510.4	1504.14	
3d <sup>5</sup> 2D <sup>1</sup>	3d <sub>-</sub> 3d <sub>+</sub> <sup>3</sup> <sub>-</sub> (0,5/2)	5/2	1533.17	1534.71		1537.4	1532.74	
3d <sup>5</sup> 4P <sup>3</sup>	3d <sub>-</sub> 3d <sub>+</sub> <sup>4</sup> <sub>+</sub> (3/2,4)	5/2	1660.92	1663.98		1658.7	1664.07	
3d <sup>5</sup> 4F <sup>3</sup>	3d <sub>-</sub> 3d <sub>+</sub> <sup>4</sup> <sub>-</sub> (3/2,4)	7/2	1733.68	1736.62		1733.1	1736.60	
3d <sup>5</sup> 4D <sup>5</sup>	3d <sub>-</sub> 3d <sub>+</sub> <sup>4</sup> <sub>-</sub> (3/2,2)	3/2	1759.25	1762.30		1758.1	1761.85	
3d <sup>5</sup> 2H <sup>3</sup>	3d <sub>-</sub> 3d <sub>+</sub> <sup>4</sup> <sub>+</sub> (3/2,4)	11/2	1746.45	1749.34		1747.2	1749.91	
3d <sup>5</sup> 2G <sup>5</sup>	3d <sub>-</sub> 3d <sub>+</sub> <sup>4</sup> <sub>-</sub> (3/2,4)	9/2	1806.21	1808.95		1807.7	1808.86	
3d <sup>5</sup> 2D <sup>3</sup>	3d <sub>-</sub> 3d <sub>+</sub> <sup>4</sup> <sub>-</sub> (3/2,2)	5/2	1843.82	1846.49		1844.6	1845.21	
3d <sup>5</sup> 2G <sup>3</sup>	3d <sub>-</sub> 3d <sub>+</sub> <sup>4</sup> <sub>+</sub> (3/2,2)	7/2	1871.70	1874.38		1874.1	1873.74	
3d <sup>5</sup> 2P <sup>3</sup>	3d <sub>-</sub> 3d <sub>+</sub> <sup>4</sup> <sub>-</sub> (3/2,2)	1/2	1933.91	1936.39		1937.0	1934.46	
3d <sup>5</sup> 2D <sup>1</sup>	3d <sub>-</sub> 3d <sub>+</sub> <sup>4</sup> <sub>-</sub> (3/2,0)	3/2	2063.04	2065.78		2065.5	2062.96	
3d <sup>5</sup> 2D <sup>1</sup>	3d <sub>-</sub> 3d <sub>+</sub> <sup>5</sup> <sub>+</sub> (0,5/2)	5/2	2362.48	2366.70		2359.4	2365.33	
W <sup>50+</sup> (Cr-like)								
3d <sup>6</sup> 5D <sup>4</sup>	3d <sub>-</sub> 3d <sub>+</sub> <sup>2</sup> <sub>+</sub> (0,4)	4	0.00	0.00	0.00	0.00	0.00	
3d <sup>6</sup> 3D <sup>4</sup>	3d <sub>-</sub> 3d <sub>+</sub> <sup>2</sup> <sub>-</sub> (0,2)	2	62.74	62.71	62.38	62.6	61.56	
3d <sup>6</sup> 3P <sup>2</sup>	3d <sub>-</sub> 3d <sub>+</sub> <sup>2</sup> <sub>+</sub> (0,0)	0	207.31	207.66	[208] <sub>+x</sub>	205.9	205.74	
3d <sup>6</sup> 5D <sup>4</sup>	3d <sub>-</sub> 3d <sub>+</sub> <sup>3</sup> <sub>+</sub> (3/2,9/2)	3	506.28	507.09	508.03	505.2	507.80	
3d <sup>6</sup> 5D <sup>4</sup>	3d <sub>-</sub> 3d <sub>+</sub> <sup>3</sup> <sub>-</sub> (3/2,9/2)	4	518.36	519.02	519.78	518.0	519.83	
3d <sup>6</sup> 5D <sup>4</sup>	3d <sub>-</sub> 3d <sub>+</sub> <sup>3</sup> <sub>+</sub> (3/2,3/2)	1	545.62	546.54	[545]	543.8	546.53	
3d <sup>6</sup> 3G <sup>4</sup>	3d <sub>-</sub> 3d <sub>+</sub> <sup>3</sup> <sub>-</sub> (3/2,9/2)	5	582.70	583.09	583.67	584.2	583.74	
3d <sup>6</sup> 3H <sup>4</sup>	3d <sub>-</sub> 3d <sub>+</sub> <sup>3</sup> <sub>-</sub> (3/2,9/2)	6	582.40	582.70	[583]	584.3	583.61	
3d <sup>6</sup> 3F <sup>4</sup>	3d <sub>-</sub> 3d <sub>+</sub> <sup>3</sup> <sub>+</sub> (3/2,3/2)	2	637.99	638.51	[639]	638.1	637.59	
3d <sup>6</sup> 3D <sup>4</sup>	3d <sub>-</sub> 3d <sub>+</sub> <sup>3</sup> <sub>-</sub> (3/2,3/2)	3	649.76	650.29	650.91	650.6	649.82	
3d <sup>6</sup> 3P <sup>4</sup>	3d <sub>-</sub> 3d <sub>+</sub> <sup>3</sup> <sub>-</sub> (3/2,3/2)	0	725.01	725.35	[729]	727.9	723.98	
3d <sup>6</sup> 3P <sup>2</sup>	3d <sub>-</sub> 3d <sub>+</sub> <sup>3</sup> <sub>+</sub> (3/2,5/2)	1	767.07	767.54	768.98 <sub>+x</sub>	769.3	766.38	

Table 3. Cont.

LSJ-	Label <i>jj</i> -Couplings	<i>J</i>	Present Work		ASD	GRASP	RMBPT <sub>g</sub>	RMBPT <sub>s</sub>
			<i>n</i> = 5	<i>n</i> = 6				
3d <sup>6</sup> 3D <sup>4</sup>	3d <sup>3</sup> 3d <sup>3</sup> <sub>+</sub> (3/2,5/2)	2	766.25	766.84	766.95	767.6	765.69	
3d <sup>6</sup> 1G <sup>2</sup>	3d <sup>3</sup> 3d <sup>3</sup> <sub>+</sub> (3/2,5/2)	4	760.65	761.12	761.21	762.5	760.28	
3d <sup>6</sup> 3F <sup>2</sup>	3d <sup>3</sup> 3d <sup>3</sup> <sub>+</sub> (3/2,5/2)	3	782.18	782.54	782.53	785.0	781.26	
3d <sup>6</sup> 5D <sup>4</sup>	3d <sup>2</sup> 3d <sup>4</sup> <sub>+</sub> (2,4)	2	1058.57	1060.19		1055.6	1060.64	
3d <sup>6</sup> 5D <sup>4</sup>	3d <sup>2</sup> 3d <sup>4</sup> <sub>+</sub> (2,2)	0	1083.07	1084.88		1079.6	1085.16	
3d <sup>6</sup> 3H <sup>4</sup>	3d <sup>2</sup> 3d <sup>4</sup> <sub>+</sub> (2,4)	4	1108.16	1109.55		1106.9	1110.13	
3d <sup>6</sup> 5D <sup>4</sup>	3d <sup>2</sup> 3d <sup>4</sup> <sub>+</sub> (2,4)	3	1135.23	1136.57		1134.6	1136.84	
3d <sup>6</sup> 3H <sup>4</sup>	3d <sup>2</sup> 3d <sup>4</sup> <sub>+</sub> (2,4)	5	1142.11	1143.32		1142.4	1144.11	
3d <sup>6</sup> 1I <sup>4</sup>	3d <sup>2</sup> 3d <sup>4</sup> <sub>+</sub> (2,4)	6	1169.18	1170.23		1170.5	1171.16	
3d <sup>6</sup> 3F <sup>4</sup>	3d <sup>2</sup> 3d <sup>4</sup> <sub>+</sub> (2,2)	3	1196.79	1198.08		1197.0	1198.01	
3d <sup>6</sup> 3D <sup>4</sup>	3d <sup>2</sup> 3d <sup>4</sup> <sub>+</sub> (2,2)	1	1217.26	1218.50		1217.8	1217.79	
3d <sup>6</sup> 1G <sup>4</sup>	3d <sup>2</sup> 3d <sup>4</sup> <sub>+</sub> (2,2)	4	1232.82	1233.95		1234.1	1233.73	
3d <sup>6</sup> 3F <sup>4</sup>	3d <sup>2</sup> 3d <sup>4</sup> <sub>+</sub> (2,2)	2	1243.66	1244.79		1244.0	1243.75	
3d <sup>6</sup> 3F <sup>2</sup>	3d <sup>2</sup> 3d <sup>4</sup> <sub>+</sub> (2,0)	2	1336.95	1338.38		1336.9	1336.97	
3d <sup>6</sup> 3F <sup>2</sup>	3d <sup>2</sup> 3d <sup>4</sup> <sub>+</sub> (0,4)	4	1374.79	1375.77		1376.9	1375.03	
3d <sup>6</sup> 1D <sup>2</sup>	3d <sup>2</sup> 3d <sup>4</sup> <sub>+</sub> (0,2)	2	1518.97	1519.86		1523.2	1517.58	
3d <sup>6</sup> 1S <sup>0</sup>	3d <sup>2</sup> 3d <sup>4</sup> <sub>+</sub> (0,0)	0	1660.58	1661.58		1664.9	1658.28	
3d <sup>6</sup> 3P <sup>2</sup>	3d <sub>-</sub> 3d <sup>5</sup> <sub>+</sub> (3/2,5/2)	1	1663.26	1665.83		1657.7	1665.57	
3d <sup>6</sup> 1G <sup>2</sup>	3d <sub>-</sub> 3d <sup>5</sup> <sub>+</sub> (3/2,5/2)	4	1764.33	1766.52		1762.0	1766.29	
3d <sup>6</sup> 3P <sup>2</sup>	3d <sub>-</sub> 3d <sup>5</sup> <sub>+</sub> (3/2,5/2)	2	1813.76	1815.87		1811.7	1814.75	
3d <sup>6</sup> 3F <sup>2</sup>	3d <sub>-</sub> 3d <sup>5</sup> <sub>+</sub> (3/2,5/2)	3	1831.23	1833.30		1830.3	1832.64	
3d <sup>6</sup> 3P <sup>2</sup>	3d <sup>6</sup> <sub>+</sub> (0,0)	0	2321.86	2325.36		2314.1	2323.82	
W <sup>49+</sup> (Mn-like)								
3d <sup>7</sup> 4F <sup>3</sup>	3d <sup>4</sup> 3d <sup>3</sup> <sub>+</sub> (0,9/2)	9/2	0.00	0.00	0.00	0.00	0.00	
3d <sup>7</sup> 2P <sup>3</sup>	3d <sup>4</sup> 3d <sup>3</sup> <sub>+</sub> (0,3/2)	3/2	101.71	101.64	[103]+x	102.1	100.13	
3d <sup>7</sup> 2D <sup>1</sup>	3d <sup>4</sup> 3d <sup>3</sup> <sub>+</sub> (0,5/2)	5/2	158.95	159.10	158.75	158.7	157.62	
3d <sup>7</sup> 4F <sup>3</sup>	3d <sup>3</sup> 3d <sup>4</sup> <sub>+</sub> (3/2,4)	7/2	527.98	528.88	529.66	526.1	529.08	
3d <sup>7</sup> 4F <sup>3</sup>	3d <sup>3</sup> 3d <sup>4</sup> <sub>+</sub> (3/2,4)	9/2	583.50	584.16	584.59	583.1	584.18	
3d <sup>7</sup> 4P <sup>3</sup>	3d <sup>3</sup> 3d <sup>4</sup> <sub>+</sub> (3/2,2)	3/2	607.96	608.87	[608]	606.6	608.30	
3d <sup>7</sup> 4P <sup>3</sup>	3d <sup>3</sup> 3d <sup>4</sup> <sub>+</sub> (3/2,4)	5/2	624.97	625.72	628.02+x	624.9	625.41	
3d <sup>7</sup> 4P <sup>3</sup>	3d <sup>3</sup> 3d <sup>4</sup> <sub>+</sub> (3/2,2)	1/2	635.89	636.62	638.62+x	635.1	635.45	
3d <sup>7</sup> 2H <sup>3</sup>	3d <sup>3</sup> 3d <sup>4</sup> <sub>+</sub> (3/2,4)	11/2	650.16	650.58	650.70	651.8	650.55	
3d <sup>7</sup> 2F <sup>3</sup>	3d <sup>3</sup> 3d <sup>4</sup> <sub>+</sub> (3/2,2)	7/2	705.20	705.71	705.92	706.4	704.86	
3d <sup>7</sup> 2F <sup>3</sup>	3d <sup>3</sup> 3d <sup>4</sup> <sub>+</sub> (3/2,2)	5/2	742.86	743.30	[747]	745.4	742.07	
3d <sup>7</sup> 2D <sup>1</sup>	3d <sup>3</sup> 3d <sup>4</sup> <sub>+</sub> (3/2,0)	3/2	888.41	889.03	[893]	890.8	886.67	
3d <sup>7</sup> 4F <sup>3</sup>	3d <sup>2</sup> 3d <sup>5</sup> <sub>+</sub> (2,5/2)	5/2	1115.46	1117.19		1112.0	1116.93	
3d <sup>7</sup> 4P <sup>3</sup>	3d <sup>2</sup> 3d <sup>5</sup> <sub>+</sub> (2,5/2)	3/2	1147.62	1149.25		1145.1	1148.65	
3d <sup>7</sup> 2P <sup>3</sup>	3d <sup>2</sup> 3d <sup>5</sup> <sub>+</sub> (2,5/2)	1/2	1192.13	1193.65		1189.9	1192.53	
3d <sup>7</sup> 2H <sup>3</sup>	3d <sup>2</sup> 3d <sup>5</sup> <sub>+</sub> (2,5/2)	9/2	1185.68	1187.07		1184.9	1186.89	
3d <sup>7</sup> 2F <sup>3</sup>	3d <sup>2</sup> 3d <sup>5</sup> <sub>+</sub> (2,5/2)	7/2	1210.79	1212.16		1210.3	1211.44	
3d <sup>7</sup> 2D <sup>1</sup>	3d <sup>2</sup> 3d <sup>5</sup> <sub>+</sub> (0,5/2)	5/2	1410.07	1411.30		1411.0	1409.49	
3d <sup>7</sup> 2D <sup>1</sup>	3d <sub>-</sub> 3d <sup>6</sup> <sub>+</sub> (3/2,0)	3/2	1751.87	1754.44		1746.4	1753.15	
W <sup>48+</sup> (Fe-like)								
3d <sup>8</sup> 3F	3d <sup>4</sup> 3d <sup>4</sup> <sub>+</sub> (0,4)	4	0.00	0.00	0.00	0.00	0.00	
3d <sup>8</sup> 1D	3d <sup>4</sup> 3d <sup>4</sup> <sub>+</sub> (0,2)	2	72.15	72.12	[73.4]+x	72.8	71.26	
3d <sup>8</sup> 3P	3d <sup>4</sup> 3d <sup>4</sup> <sub>+</sub> (0,0)	0	229.94	230.10	[233]	230.7	228.17	
3d <sup>8</sup> 3F	3d <sup>3</sup> 3d <sup>5</sup> <sub>+</sub> (3/2,5/2)	3	525.18	526.07	526.65	523.2	526.13	
3d <sup>8</sup> 3P	3d <sup>3</sup> 3d <sup>5</sup> <sub>+</sub> (3/2,5/2)	2	600.38	601.15	603.12+x	599.7	600.69	

Table 3. Cont.

LSJ-	Label jj-Couplings	J	Present Work		ASD	GRASP	RMBPT <sub>g</sub>	RMBPT <sub>s</sub>
			n = 5	n = 6				
3d <sup>8</sup> 3P	3d <sup>3</sup> 3d <sup>5</sup> <sub>+</sub> (3/2,5/2)	1	642.01	642.71	644.76+x	642.7	642.14	
3d <sup>8</sup> 1G	3d <sup>3</sup> 3d <sup>5</sup> <sub>+</sub> (3/2,5/2)	4	643.89	644.43	644.70	645.0	644.03	
3d <sup>8</sup> 3F	3d <sup>2</sup> 3d <sup>6</sup> <sub>+</sub> (2,2)	2	1106.91	1108.59	[1106]	1103.6	1108.17	
3d <sup>8</sup> 1S	3d <sup>2</sup> 3d <sup>6</sup> <sub>+</sub> (0,0)	0	1304.16	1305.75	[1306]	1301.7	1304.07	
W <sup>47+</sup> (Co-like)								
3d <sup>9</sup> 2D	3d <sup>4</sup> 3d <sup>5</sup> <sub>+</sub> (0,5/2)	5/2	0.00	0.00	0.00	0.00	0.00	
3d <sup>9</sup> 2D	3d <sup>3</sup> 3d <sup>6</sup> <sub>+</sub> (3/2,0)	3/2	537.21	538.04	538.59	535.6	538.05	

The uncertainties of NIST energy levels not based on observed wavelengths are estimated as being less than 5000 cm<sup>-1</sup>, or 5.00 in our table. In order to better understand the importance of various effects in Table 4, we report the NIST energy levels that are based on observation and differences of various theories for only those levels where NIST values are accurate, although there may be an unknown shift.

Table 4. Difference from NIST energy levels derived from observation. Shown is the LS label, the J value, the present n = 5 result for VV correlation, and n = 6 result for all three types of correlation, the ASD value [5], the Quinet value [6], the Guo et al. RMBPT<sub>g</sub> value [8], and the Safranov & Safranov RMBPT<sub>s</sub> value [17]. All energy levels are reported in 1000 cm<sup>-1</sup>.

Label	J	Present Work		ASD	GRASP	RMBPT <sub>g</sub>	RMBPT <sub>s</sub>
		n = 5	n = 6				
W <sup>55+</sup> (K-like)							
3d 2D	3/2	0.00	0.00	0.00	0.00	0.00	
3d 2D	5/2	1.25	0.32	626.49	2.49	-0.07	
W <sup>54+</sup> (Ca-like)							
3d <sup>2</sup> 3F	2	0.00	0.00	0.00	0.00	0.00	0.00
3d <sup>2</sup> 3F	3	1.43	0.73	585.48	1.98	-0.32	2.63
3d <sup>2</sup> 3P	2	1.04	0.53	668.49	0.89	0.49	2.28
3d <sup>2</sup> 3P	1	3.11	2.71	709.46+x	2.36	2.68	4.05
W <sup>53+</sup> (Sc-like)							
3d <sup>3</sup> 4F <sup>3</sup>	3/2	0.00	0.00	0.00	0.00	0.00	
3d <sup>3</sup> 4F <sup>3</sup>	5/2	1.64	0.96	530.03	1.83	-0.48	
3d <sup>3</sup> 4P <sup>3</sup>	3/2	1.43	0.87	580.86	0.96	0.0	
3d <sup>3</sup> 4P <sup>3</sup>	1/2	1.23	0.73	623.95	0.35	0.42	
3d <sup>3</sup> 2D <sup>1</sup>	5/2	0.38	0.15	812.22	-1.98	0.45	
3d <sup>3</sup> 2H <sup>3</sup>	11/2	1.13	0.21	1234.51+x	-1.69	0.45	
W <sup>52+</sup> (Ti-like)							
3d <sup>4</sup> 3P <sup>2</sup>	0	0.00	0.00	0.00	0.00	0.00	
3d <sup>4</sup> 5D <sup>4</sup>	1	1.76	1.12	517.63	1.63	-0.45	
3d <sup>4</sup> 3F <sup>2</sup>	3	-0.28	-0.53	665.5621+x	-3.04	-1.48	
3d <sup>4</sup> 5D <sup>4</sup>	2	2.87	1.71	1109.69	2.09	-0.33	
3d <sup>4</sup> 3H <sup>4</sup>	4	1.73	0.68	1127.27+y	-0.03	-1.84	
3d <sup>4</sup> 3H <sup>4</sup>	5	1.11	0.29	1173.35+y	-2.35	-22.25	
3d <sup>4</sup> 3F <sup>2</sup>	4	0.29	-0.27	1403.95+x	-4.65	-1.16	



Table 4. Cont.

Label	J	Present Work		ASD	GRASP	RMBPT <sub>g</sub>	RMBPT <sub>s</sub>
		n = 5	n = 6				
<b>W<sup>51+</sup> (V-like)</b>							
3d <sup>5</sup> 4p <sup>3</sup>	5/2	0.00	0.00	0.00	0.00	0.00	
3d <sup>5</sup> 6s <sup>5</sup>	5/2	1.92	0.88	471.63	2.53	−0.40	
3d <sup>5</sup> 4G <sup>5</sup>	7/2	1.27	0.45	566.25	0.05	−0.16	
3d <sup>5</sup> 4D <sup>5</sup>	3/2	1.28	0.39	580.89	1.09	0.45	
3d <sup>5</sup> 2F <sup>5</sup>	7/2	0.45	−0.10	688.18	−2.72	0.28	
3d <sup>5</sup> 4G <sup>5</sup>	11/2	2.64	0.92	1103.43	0.43	−0.61	
<b>W<sup>50+</sup> (Cr-like)</b>							
3d <sup>6</sup> 5D <sup>4</sup>	4	0.00	0.00	0.00	0.00	0.00	
3d <sup>6</sup> 3D <sup>4</sup>	2	−0.36	−0.29	62.38	−0.22	0.82	
3d <sup>6</sup> 5D <sup>4</sup>	3	1.75	1.04	508.03	2.83	0.23	
3d <sup>6</sup> 5D <sup>4</sup>	4	1.41	0.74	519.78	1.78	0.05	
3d <sup>6</sup> 3G <sup>4</sup>	5	0.97	0.44	583.67	−0.53	−0.07	
3d <sup>6</sup> 3D <sup>4</sup>	3	1.15	0.56	650.91	0.31	1.09	
3d <sup>6</sup> 3p <sup>2</sup>	1	1.91	1.44	768.98+x	−0.32	2.60	
3d <sup>6</sup> 3D <sup>4</sup>	2	0.70	0.11	766.95	−0.65	1.26	
3d <sup>6</sup> 1G <sup>2</sup>	4	0.56	−0.04	761.21	−1.29	0.93	
3d <sup>6</sup> 3F <sup>2</sup>	3	0.35	−0.08	782.53	−2.47	1.27	
<b>W<sup>49+</sup> (Mn-like)</b>							
3d <sup>7</sup> 4F <sup>3</sup>	9/2	0.00	0.00	0.00	0.00	0.00	
3d <sup>7</sup> 2D <sup>1</sup>	5/2	−0.20	−0.35	158.75	0.05	1.13	
3d <sup>7</sup> 4F <sup>3</sup>	7/2	1.68	0.78	529.66	3.56	0.58	
3d <sup>7</sup> 4F <sup>3</sup>	9/2	1.09	0.43	584.59	1.49	0.41	
3d <sup>7</sup> 4p <sup>3</sup>	5/2	3.05	2.30	628.02+x	3.12	2.61	
3d <sup>7</sup> 4p <sup>3</sup>	1/2	2.73	2.00	638.62+x	3.52	3.17	
3d <sup>7</sup> 2H <sup>3</sup>	11/2	0.54	0.12	650.70	−1.10	0.15	
3d <sup>7</sup> 2F <sup>3</sup>	7/2	0.72	0.21	705.92	−0.48	1.06	
<b>W<sup>48+</sup> (Fe-like)</b>							
3d <sup>8</sup> 3F	4	0.00			0.00	0.00	0.00
3d <sup>8</sup> 3F	3	1.47	0.58	526.65	3.45	0.52	
3d <sup>8</sup> 3P	2	2.74	1.97	603.12+x	3.42	2.43	
3d <sup>8</sup> 3P	1	2.73	2.05	644.76+x	2.06	2.62	
<b>W<sup>47+</sup> (Co-like)</b>							
3d <sup>9</sup> 2D	5/2	0.00	0.00	0.00	0.00	0.00	
3d <sup>9</sup> 2D	3/2	1.38	0.55	538.59	2.99	0.54	

Table 4 shows clearly that the uncertainties of the present  $n = 6$  results are smaller by about a factor of a half when no shifts are indicated in the NIST value. For these levels, the  $n = 6$  results statistically differ less than the Quinet values that are similar to the less accurate  $n = 5$  values. The most accurate results for  $3d$  and  $3d^9$  are the RMCDFH<sub>g</sub> results, although for  $3d^9$ , the  $n = 6$  are almost of the same accuracy. RMBPT<sub>g</sub> is the more accurate for  $3d^2$ , with  $n = 6$  almost the same. For  $3d^8$ , the two lower levels, RMBPT<sub>g</sub> is the more accurate, whereas  $n = 6$  is the more accurate for the two upper levels. A similar pattern seems to hold for other spectra. An interesting case is  $3d^7 4p$   $J = 5/2$  and  $1/2$ , where both levels have an unknown shift. An exact theoretical value and an exact NIST value (except for the shift) would have the same difference for the two levels. In the present case, the

$n = 6$  differences are more similar than the  $\text{RMCDHF}_g$  differences. In fact, from this table, we can conclude that any NIST value for which the theoretical difference from NIST for both methods is more than 1.00 has a noticeable error. Thus, for example, the  $^3P_1$  level of  $3d^8$  with an energy level of  $644.70 \text{ Kcm}^{-1}$  suggests that the NIST values is not accurate to two decimal places.

The errors in different theoretical results are shown in Figure 2. Note the similarity in accuracy of the present  $n = 6$  results and values reported by Guo et al. [8].

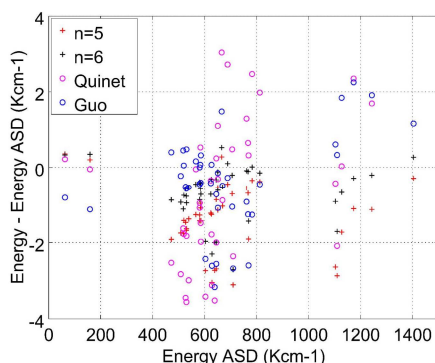


Figure 2. Plot comparing the accuracy of different theoretical methods.

The accuracy of theoretical energy levels are best evaluated by comparing theoretical wavelengths with wavelengths of observed lines in the spectrum. In Table 5, all wavelengths for M1 transitions between the  $3d^k$  levels for the present  $n = 5, 6$  results are compared with experimental results and other theory, when available. This table clearly shows the improvement in accuracy of  $n = 6$  calculations over  $n = 5$ , as well as the GRASP results reported by Quinet [6], and in many cases the very close agreement with Guo et al. [8]. Two exceptions are the  $3d^7 \ ^4F^3 - 3d^7 \ ^2F^3$  ( $J = 9/2$  to  $J = 7/2$ ) transition, for which the observed wavelength is  $14.166(3) \text{ nm}$ , the present  $n = 6$  is  $14.170 \text{ nm}$ , and the Guo et al. value is  $14.187 \text{ nm}$ . Similarly, the  $3d^8 \ ^3F - 3d^8 \ ^1G$  ( $J = 4$  to  $J = 4$ ) transition has an observed wavelength of  $15.511(3) \text{ nm}$ , whereas the present value is  $15.518 \text{ nm}$  and the Guo et al. value is  $15.463 \text{ nm}$ .

Table 5. Wavelengths from theory for observed M1 transitions compared with observed wavelengths (in nm). Included are some long wavelengths for transitions between close-lying levels.

Label and $J$ for Lower	Label and $J$ for Upper	Present Work		Expt (Ref. [2])	GRASP	RMBPT <sub>g</sub>	RCI <sub>g</sub>
		$n = 5$	$n = 6$				
$W^{55+}$ (K-like)							
$3d \ ^2D$	$3/2 \ 3d \ ^2D$	15.994	15.970	15.962(3)	16.008	15.960	16.035
$W^{54+}$ (Ca-like)							
$3d^2 \ ^3F$	$2 \ 3d^2 \ ^3F$	17.122	17.101	17.080(3)	17.138	17.071	17.218
$3d^2 \ ^3F$	$2 \ 3d^2 \ ^3P$	14.982	14.971	14.959(3)	14.980	14.970	14.924
$3d^2 \ ^3F$	$2 \ 3d^2 \ ^3P$	14.157	14.149				
$3d^2 \ ^3F$	$2 \ 3d^2 \ ^3P$	7.699	7.691				
$3d^2 \ ^3P$	$0 \ 3d^2 \ ^3P$	19.233	19.211	19.177(3)	19.222	19.160	19.422
$3d^2 \ ^3F$	$3 \ 3d^2 \ ^3P$	119.908	120.168				
$3d^2 \ ^3F$	$3 \ 3d^2 \ ^1G$	89.580	89.805				
$3d^2 \ ^3F$	$3 \ 3d^2 \ ^3F$	15.378	15.365				
$3d^2 \ ^3F$	$3 \ 3d^2 \ ^3P$	13.989	13.977				

Table 5. Cont.

Label and J for Lower		Label and J for Upper		Present Work		Expt (Ref. [2])	GRASP	RMBPT <sub>g</sub>	RCI <sub>g</sub>
				n = 5	n = 6				
3d <sup>2</sup> 3P	2	3d <sup>2</sup> 3P	1	257.054	257.793				
3d <sup>2</sup> 3P	2	3d <sup>2</sup> 3P	2	15.836	15.817				
3d <sup>2</sup> 3P	1	3d <sup>2</sup> 3P	2	16.876	16.851				
3d <sup>2</sup> 3P	1	3d <sup>2</sup> 1S	0	12.728	12.707				
3d <sup>2</sup> 1G	4	3d <sup>2</sup> 3F	4	18.566	18.537				
W <sup>53+</sup> (Sc-like)									
3d <sup>3</sup> 4F <sup>3</sup>	3/2	3d <sup>3</sup> 4F <sup>3</sup>	5/2	18.925	18.901	18.867(3)	18.933	18.850	19.120
3d <sup>3</sup> 4F <sup>3</sup>	3/2	3d <sup>3</sup> 4P <sup>3</sup>	3/2	17.258	17.242	17.216(3)	17.243	17.216	17.315
3d <sup>3</sup> 4F <sup>3</sup>	3/2	3d <sup>3</sup> 4P <sup>3</sup>	1/2	16.059	16.046	16.027(3)	16.035	16.038	16.038
3d <sup>3</sup> 4F <sup>3</sup>	3/2	3d <sup>3</sup> 2D <sup>1</sup>	5/2	12.318	12.314	12.312(3)	12.282	12.319	12.225
3d <sup>3</sup> 4F <sup>3</sup>	3/2	3d <sup>3</sup> 4P <sup>3</sup>	3/2	8.289	8.280				
3d <sup>3</sup> 4F <sup>3</sup>	3/2	3d <sup>3</sup> 2P <sup>3</sup>	1/2	8.128	8.120				
3d <sup>3</sup> 4F <sup>3</sup>	3/2	3d <sup>3</sup> 2D <sup>3</sup>	5/2	8.041	8.035				
3d <sup>3</sup> 4F <sup>3</sup>	3/2	3d <sup>3</sup> 2F <sup>3</sup>	5/2	7.607	7.601				
3d <sup>3</sup> 4F <sup>3</sup>	3/2	3d <sup>3</sup> 2D <sup>1</sup>	3/2	6.757	6.751				
3d <sup>3</sup> 4F <sup>3</sup>	3/2	3d <sup>3</sup> 2P <sup>3</sup>	3/2	5.329	5.324				
3d <sup>3</sup> 4F <sup>3</sup>	3/2	3d <sup>3</sup> 2D <sup>1</sup>	5/2	5.107	5.102				
3d <sup>3</sup> 4F <sup>3</sup>	5/2	3d <sup>3</sup> 4P <sup>3</sup>	3/2	195.953	196.390				
3d <sup>3</sup> 4F <sup>3</sup>	5/2	3d <sup>3</sup> 2G <sup>3</sup>	7/2	121.923	122.264				
3d <sup>3</sup> 4F <sup>3</sup>	5/2	3d <sup>3</sup> 2D <sup>1</sup>	5/2	35.279	35.336				
3d <sup>3</sup> 4F <sup>3</sup>	5/2	3d <sup>3</sup> 4F <sup>3</sup>	7/2	16.697	16.680				
3d <sup>3</sup> 4F <sup>3</sup>	5/2	3d <sup>3</sup> 4P <sup>3</sup>	3/2	14.749	14.735				
3d <sup>3</sup> 4F <sup>3</sup>	5/2	3d <sup>3</sup> 2D <sup>3</sup>	5/2	13.981	13.975				
3d <sup>3</sup> 4F <sup>3</sup>	5/2	3d <sup>3</sup> 2F <sup>3</sup>	5/2	12.720	12.715				
3d <sup>3</sup> 4F <sup>3</sup>	5/2	3d <sup>3</sup> 2F <sup>3</sup>	7/2	12.654	12.651				
3d <sup>3</sup> 4F <sup>3</sup>	5/2	3d <sup>3</sup> 2D <sup>1</sup>	3/2	10.509	10.502				
3d <sup>3</sup> 4F <sup>3</sup>	5/2	3d <sup>3</sup> 2P <sup>3</sup>	3/2	7.418	7.412				
3d <sup>3</sup> 4F <sup>3</sup>	5/2	3d <sup>3</sup> 2D <sup>1</sup>	5/2	6.995	6.988				
3d <sup>3</sup> 4P <sup>3</sup>	3/2	3d <sup>3</sup> 4P <sup>3</sup>	1/2	230.965	231.304				
3d <sup>3</sup> 4P <sup>3</sup>	3/2	3d <sup>3</sup> 2D <sup>1</sup>	5/2	43.026	43.089				
3d <sup>3</sup> 4P <sup>3</sup>	3/2	3d <sup>3</sup> 4P <sup>3</sup>	3/2	15.949	15.930				
3d <sup>3</sup> 4P <sup>3</sup>	3/2	3d <sup>3</sup> 2P <sup>3</sup>	1/2	15.364	15.347				
3d <sup>3</sup> 4P <sup>3</sup>	3/2	3d <sup>3</sup> 2D <sup>3</sup>	5/2	15.055	15.046				
3d <sup>3</sup> 4P <sup>3</sup>	3/2	3d <sup>3</sup> 2F <sup>3</sup>	5/2	13.603	13.595				
3d <sup>3</sup> 4P <sup>3</sup>	3/2	3d <sup>3</sup> 2D <sup>1</sup>	3/2	11.105	11.095				
3d <sup>3</sup> 4P <sup>3</sup>	3/2	3d <sup>3</sup> 2P <sup>3</sup>	3/2	7.710	7.702				
3d <sup>3</sup> 4P <sup>3</sup>	3/2	3d <sup>3</sup> 2D <sup>1</sup>	5/2	7.254	7.246				
3d <sup>3</sup> 2H <sup>3</sup>	9/2	3d <sup>3</sup> 2G <sup>3</sup>	7/2	21322.871	18591.162				
3d <sup>3</sup> 2H <sup>3</sup>	9/2	3d <sup>3</sup> 4F <sup>3</sup>	7/2	19.329	19.295				
3d <sup>3</sup> 2H <sup>3</sup>	9/2	3d <sup>3</sup> 4F <sup>3</sup>	9/2	18.022	17.996				
3d <sup>3</sup> 2H <sup>3</sup>	9/2	3d <sup>3</sup> 2H <sup>3</sup>	11/2	15.812	15.798	15.785(3)	15.792	15.778	15.876
3d <sup>3</sup> 2H <sup>3</sup>	9/2	3d <sup>3</sup> 2F <sup>3</sup>	7/2	14.110	14.100				
3d <sup>3</sup> 2H <sup>3</sup>	9/2	3d <sup>3</sup> 2G <sup>3</sup>	9/2	8.673	8.661				
3d <sup>3</sup> 2G <sup>3</sup>	7/2	3d <sup>3</sup> 2D <sup>1</sup>	5/2	49.645	49.700				
3d <sup>3</sup> 2G <sup>3</sup>	7/2	3d <sup>3</sup> 4F <sup>3</sup>	7/2	19.346	19.315				
3d <sup>3</sup> 2G <sup>3</sup>	7/2	3d <sup>3</sup> 4F <sup>3</sup>	9/2	18.037	18.014				
3d <sup>3</sup> 2G <sup>3</sup>	7/2	3d <sup>3</sup> 2D <sup>3</sup>	5/2	15.791	15.779				
3d <sup>3</sup> 2G <sup>3</sup>	7/2	3d <sup>3</sup> 2F <sup>3</sup>	5/2	14.201	14.191				

Table 5. Cont.

Label and J for Lower		Label and J for Upper		Present Work		Expt (Ref. [2])	GRASP	RMBPT <sub>g</sub>	RCI <sub>g</sub>
				n = 5	n = 6				
3d <sup>3</sup> 2G <sup>3</sup>	7/2	3d <sup>3</sup> 2F <sup>3</sup>	7/2	14.119	14.110				
3d <sup>3</sup> 2G <sup>3</sup>	7/2	3d <sup>3</sup> 2G <sup>3</sup>	9/2	8.677	8.665				
3d <sup>3</sup> 2G <sup>3</sup>	7/2	3d <sup>3</sup> 2D <sup>1</sup>	5/2	7.421	7.411				
3d <sup>3</sup> 4P <sup>3</sup>	1/2	3d <sup>3</sup> 4P <sup>3</sup>	3/2	17.132	17.108				
3d <sup>3</sup> 4P <sup>3</sup>	1/2	3d <sup>3</sup> 2P <sup>3</sup>	1/2	16.459	16.438				
3d <sup>3</sup> 4P <sup>3</sup>	1/2	3d <sup>3</sup> 2D <sup>1</sup>	3/2	11.665	11.654				
3d <sup>3</sup> 4P <sup>3</sup>	1/2	3d <sup>3</sup> 2P <sup>3</sup>	3/2	7.976	7.968				
3d <sup>3</sup> 2D <sup>1</sup>	5/2	3d <sup>3</sup> 4F <sup>3</sup>	7/2	31.700	31.592				
3d <sup>3</sup> 2D <sup>1</sup>	5/2	3d <sup>3</sup> 4P <sup>3</sup>	3/2	25.344	25.274				
3d <sup>3</sup> 2D <sup>1</sup>	5/2	3d <sup>3</sup> 2D <sup>3</sup>	5/2	23.157	23.119				
3d <sup>3</sup> 2D <sup>1</sup>	5/2	3d <sup>3</sup> 2F <sup>3</sup>	5/2	19.891	19.862				
3d <sup>3</sup> 2D <sup>1</sup>	5/2	3d <sup>3</sup> 2F <sup>3</sup>	7/2	19.730	19.705				
3d <sup>3</sup> 2D <sup>1</sup>	5/2	3d <sup>3</sup> 2D <sup>1</sup>	3/2	14.968	14.943				
3d <sup>3</sup> 2D <sup>1</sup>	5/2	3d <sup>3</sup> 2P <sup>3</sup>	3/2	9.393	9.379				
3d <sup>3</sup> 2D <sup>1</sup>	5/2	3d <sup>3</sup> 2D <sup>1</sup>	5/2	8.725	8.710				
3d <sup>3</sup> 4F <sup>3</sup>	7/2	3d <sup>3</sup> 4F <sup>3</sup>	9/2	266.613	267.448				
3d <sup>3</sup> 4F <sup>3</sup>	7/2	3d <sup>3</sup> 2D <sup>3</sup>	5/2	85.937	86.197				
3d <sup>3</sup> 4F <sup>3</sup>	7/2	3d <sup>3</sup> 2F <sup>3</sup>	5/2	53.397	53.492				
3d <sup>3</sup> 4F <sup>3</sup>	7/2	3d <sup>3</sup> 2F <sup>3</sup>	7/2	52.253	52.370				
3d <sup>3</sup> 4F <sup>3</sup>	7/2	3d <sup>3</sup> 2G <sup>3</sup>	9/2	15.733	15.717				
3d <sup>3</sup> 4F <sup>3</sup>	7/2	3d <sup>3</sup> 2D <sup>1</sup>	5/2	12.038	12.026				
3d <sup>3</sup> 4F <sup>3</sup>	9/2	3d <sup>3</sup> 2H <sup>3</sup>	11/2	128.917	129.345				
3d <sup>3</sup> 4F <sup>3</sup>	9/2	3d <sup>3</sup> 2F <sup>3</sup>	7/2	64.991	65.122				
3d <sup>3</sup> 4F <sup>3</sup>	9/2	3d <sup>3</sup> 2G <sup>3</sup>	9/2	16.719	16.698				
3d <sup>3</sup> 4P <sup>3</sup>	3/2	3d <sup>3</sup> 2P <sup>3</sup>	1/2	418.463	419.226				
3d <sup>3</sup> 4P <sup>3</sup>	3/2	3d <sup>3</sup> 2D <sup>3</sup>	5/2	268.399	271.110				
3d <sup>3</sup> 4P <sup>3</sup>	3/2	3d <sup>3</sup> 2F <sup>3</sup>	5/2	92.445	92.751				
3d <sup>3</sup> 4P <sup>3</sup>	3/2	3d <sup>3</sup> 2D <sup>1</sup>	3/2	36.557	36.559				
3d <sup>3</sup> 4P <sup>3</sup>	3/2	3d <sup>3</sup> 2P <sup>3</sup>	3/2	14.925	14.912				
3d <sup>3</sup> 4P <sup>3</sup>	3/2	3d <sup>3</sup> 2D <sup>1</sup>	5/2	13.305	13.291				
3d <sup>3</sup> 2P <sup>3</sup>	1/2	3d <sup>3</sup> 2D <sup>1</sup>	3/2	40.056	40.051				
3d <sup>3</sup> 2P <sup>3</sup>	1/2	3d <sup>3</sup> 2P <sup>3</sup>	3/2	15.477	15.462				
3d <sup>3</sup> 2H <sup>3</sup>	11/2	3d <sup>3</sup> 2G <sup>3</sup>	9/2	19.211	19.173				
3d <sup>3</sup> 2D <sup>3</sup>	5/2	3d <sup>3</sup> 2F <sup>3</sup>	5/2	141.016	140.984				
3d <sup>3</sup> 2D <sup>3</sup>	5/2	3d <sup>3</sup> 2F <sup>3</sup>	7/2	133.312	133.450				
3d <sup>3</sup> 2D <sup>3</sup>	5/2	3d <sup>3</sup> 2D <sup>1</sup>	3/2	42.321	42.257				
3d <sup>3</sup> 2D <sup>3</sup>	5/2	3d <sup>3</sup> 2P <sup>3</sup>	3/2	15.804	15.780				
3d <sup>3</sup> 2D <sup>3</sup>	5/2	3d <sup>3</sup> 2D <sup>1</sup>	5/2	13.999	13.976				
3d <sup>3</sup> 2F <sup>3</sup>	5/2	3d <sup>3</sup> 2F <sup>3</sup>	7/2	2440.155	2497.085				
3d <sup>3</sup> 2F <sup>3</sup>	5/2	3d <sup>3</sup> 2D <sup>1</sup>	3/2	60.469	60.343				
3d <sup>3</sup> 2F <sup>3</sup>	5/2	3d <sup>3</sup> 2P <sup>3</sup>	3/2	17.798	17.769				
3d <sup>3</sup> 2F <sup>3</sup>	5/2	3d <sup>3</sup> 2D <sup>1</sup>	5/2	15.542	15.514				
3d <sup>3</sup> 2F <sup>3</sup>	7/2	3d <sup>3</sup> 2G <sup>3</sup>	9/2	22.510	22.456				
3d <sup>3</sup> 2F <sup>3</sup>	7/2	3d <sup>3</sup> 2D <sup>1</sup>	5/2	15.642	15.611				
3d <sup>3</sup> 2D <sup>1</sup>	3/2	3d <sup>3</sup> 2P <sup>3</sup>	3/2	25.222	25.185				
3d <sup>3</sup> 2D <sup>1</sup>	3/2	3d <sup>3</sup> 2D <sup>1</sup>	5/2	20.919	20.883				
3d <sup>3</sup> 2P <sup>3</sup>	3/2	3d <sup>3</sup> 2D <sup>1</sup>	5/2	122.606	122.246				

Table 5. Cont.

Label and J for Lower	Label and J for Upper	Present Work		Expt (Ref. [2])	GRASP	RMBPT <sub>g</sub>	RCI <sub>g</sub>	
		n = 5	n = 6					
W <sup>52+</sup> (Ti-like)								
3d <sup>4</sup> 3P <sup>2</sup>	0 3d <sup>4</sup> 5D <sup>4</sup>	1	19.385	19.361	19.319(3)	19.379	19.302	19.605
3d <sup>4</sup> 3P <sup>2</sup>	0 3d <sup>4</sup> 3D <sup>4</sup>	1	8.241	8.234				
3d <sup>4</sup> 3P <sup>2</sup>	0 3d <sup>4</sup> 3D <sup>4</sup>	1	5.660	5.654				
3d <sup>4</sup> 3P <sup>2</sup>	0 3d <sup>4</sup> 3P <sup>2</sup>	1	5.041	5.037				
3d <sup>4</sup> 5D <sup>4</sup>	1 3d <sup>4</sup> 5D <sup>4</sup>	2	81.888	82.053				
3d <sup>4</sup> 5D <sup>4</sup>	1 3d <sup>4</sup> 5D <sup>4</sup>	0	17.065	17.045				
3d <sup>4</sup> 5D <sup>4</sup>	1 3d <sup>4</sup> 5D <sup>4</sup>	2	16.922	16.907	16.890(3)	16.903	16.894	16.958
3d <sup>4</sup> 5D <sup>4</sup>	1 3d <sup>4</sup> 3D <sup>4</sup>	1	14.334	14.326				
3d <sup>4</sup> 5D <sup>4</sup>	1 3d <sup>4</sup> 3F <sup>4</sup>	2	13.479	13.475				
3d <sup>4</sup> 5D <sup>4</sup>	1 3d <sup>4</sup> 3F <sup>2</sup>	2	11.857	11.849				
3d <sup>4</sup> 5D <sup>4</sup>	1 3d <sup>4</sup> 1D <sup>2</sup>	2	10.103	10.103				
3d <sup>4</sup> 5D <sup>4</sup>	1 3d <sup>4</sup> 3P <sup>4</sup>	0	8.950	8.947				
3d <sup>4</sup> 5D <sup>4</sup>	1 3d <sup>4</sup> 3D <sup>4</sup>	1	7.995	7.987				
3d <sup>4</sup> 5D <sup>4</sup>	1 3d <sup>4</sup> 3F <sup>4</sup>	2	7.545	7.539				
3d <sup>4</sup> 5D <sup>4</sup>	1 3d <sup>4</sup> 1S <sup>4</sup>	0	7.107	7.105				
3d <sup>4</sup> 5D <sup>4</sup>	1 3d <sup>4</sup> 3P <sup>2</sup>	1	6.812	6.808				
3d <sup>4</sup> 5D <sup>4</sup>	1 3d <sup>4</sup> 1D <sup>4</sup>	2	6.654	6.651				
3d <sup>4</sup> 5D <sup>4</sup>	1 3d <sup>4</sup> 1D <sup>2</sup>	2	5.142	5.137				
3d <sup>4</sup> 5D <sup>4</sup>	1 3d <sup>4</sup> 3P <sup>2</sup>	0	4.658	4.653				
3d <sup>4</sup> 3H <sup>4</sup>	4 3d <sup>4</sup> 3F <sup>2</sup>	3	190.114	190.262				
3d <sup>4</sup> 3H <sup>4</sup>	4 3d <sup>4</sup> 3H <sup>4</sup>	4	19.520	19.491	19.445(3)	19.543	19.443	19.696
3d <sup>4</sup> 3H <sup>4</sup>	4 3d <sup>4</sup> 5D <sup>4</sup>	3	18.912	18.886				
3d <sup>4</sup> 3H <sup>4</sup>	4 3d <sup>4</sup> 3H <sup>4</sup>	5	17.889	17.872	17.846(3)	17.855	17.831	18.065
3d <sup>4</sup> 3H <sup>4</sup>	4 3d <sup>4</sup> 3F <sup>4</sup>	3	15.977	15.965				
3d <sup>4</sup> 3H <sup>4</sup>	4 3d <sup>4</sup> 3G <sup>4</sup>	4	15.894	15.882				
3d <sup>4</sup> 3H <sup>4</sup>	4 3d <sup>4</sup> 3F <sup>2</sup>	4	12.652	12.647				
3d <sup>4</sup> 3H <sup>4</sup>	4 3d <sup>4</sup> 5D <sup>4</sup>	4	9.083	9.071				
3d <sup>4</sup> 3H <sup>4</sup>	4 3d <sup>4</sup> 3F <sup>4</sup>	3	8.993	8.981				
3d <sup>4</sup> 3H <sup>4</sup>	4 3d <sup>4</sup> 3G <sup>4</sup>	5	8.617	8.608				
3d <sup>4</sup> 3H <sup>4</sup>	4 3d <sup>4</sup> 3D <sup>4</sup>	3	8.036	8.028				
3d <sup>4</sup> 3H <sup>4</sup>	4 3d <sup>4</sup> 3F <sup>2</sup>	3	7.317	7.310				
3d <sup>4</sup> 3H <sup>4</sup>	4 3d <sup>4</sup> 1G <sup>2</sup>	4	7.290	7.283				
3d <sup>4</sup> 3H <sup>4</sup>	4 3d <sup>4</sup> 3F <sup>2</sup>	4	5.672	5.665				
3d <sup>4</sup> 5D <sup>4</sup>	2 3d <sup>4</sup> 3F <sup>2</sup>	3	358.990	360.907				
3d <sup>4</sup> 5D <sup>4</sup>	2 3d <sup>4</sup> 5D <sup>4</sup>	2	21.329	21.295				
3d <sup>4</sup> 5D <sup>4</sup>	2 3d <sup>4</sup> 5D <sup>4</sup>	3	19.840	19.816				
3d <sup>4</sup> 5D <sup>4</sup>	2 3d <sup>4</sup> 3D <sup>4</sup>	1	17.375	17.356				
3d <sup>4</sup> 5D <sup>4</sup>	2 3d <sup>4</sup> 3F <sup>4</sup>	3	16.635	16.624				
3d <sup>4</sup> 5D <sup>4</sup>	2 3d <sup>4</sup> 3F <sup>4</sup>	2	16.135	16.123				
3d <sup>4</sup> 5D <sup>4</sup>	2 3d <sup>4</sup> 3F <sup>2</sup>	2	13.864	13.849				
3d <sup>4</sup> 5D <sup>4</sup>	2 3d <sup>4</sup> 1D <sup>2</sup>	2	11.525	11.521				
3d <sup>4</sup> 5D <sup>4</sup>	2 3d <sup>4</sup> 3F <sup>4</sup>	3	9.197	9.186				
3d <sup>4</sup> 5D <sup>4</sup>	2 3d <sup>4</sup> 3D <sup>4</sup>	1	8.860	8.848				
3d <sup>4</sup> 5D <sup>4</sup>	2 3d <sup>4</sup> 3F <sup>4</sup>	2	8.311	8.302				
3d <sup>4</sup> 5D <sup>4</sup>	2 3d <sup>4</sup> 3D <sup>4</sup>	3	8.199	8.191				
3d <sup>4</sup> 5D <sup>4</sup>	2 3d <sup>4</sup> 3F <sup>2</sup>	3	7.452	7.445				
3d <sup>4</sup> 5D <sup>4</sup>	2 3d <sup>4</sup> 3P <sup>2</sup>	1	7.430	7.424				
3d <sup>4</sup> 5D <sup>4</sup>	2 3d <sup>4</sup> 1D <sup>4</sup>	2	7.243	7.238				

Table 5. Cont.

Label and J for Lower		Label and J for Upper		Present Work		Expt (Ref. [2])	GRASP	RMBPT <sub>g</sub>	RCI <sub>g</sub>
				n = 5	n = 6				
3d <sup>4</sup> 5D <sup>4</sup>	2	3d <sup>4</sup> 1D <sup>2</sup>	2	5.487	5.480				
3d <sup>4</sup> 3F <sup>2</sup>	3	3d <sup>4</sup> 5D <sup>4</sup>	2	22.677	22.630				
3d <sup>4</sup> 3F <sup>2</sup>	3	3d <sup>4</sup> 3H <sup>4</sup>	4	21.753	21.716				
3d <sup>4</sup> 3F <sup>2</sup>	3	3d <sup>4</sup> 5D <sup>4</sup>	3	21.001	20.968				
3d <sup>4</sup> 3F <sup>2</sup>	3	3d <sup>4</sup> 3F <sup>4</sup>	3	17.443	17.427				
3d <sup>4</sup> 3F <sup>2</sup>	3	3d <sup>4</sup> 3G <sup>4</sup>	4	17.344	17.329				
3d <sup>4</sup> 3F <sup>2</sup>	3	3d <sup>4</sup> 3F <sup>4</sup>	2	16.895	16.877				
3d <sup>4</sup> 3F <sup>2</sup>	3	3d <sup>4</sup> 3F <sup>2</sup>	2	14.421	14.402				
3d <sup>4</sup> 3F <sup>2</sup>	3	3d <sup>4</sup> 3F <sup>2</sup>	4	13.554	13.548	13.543(3)	13.513	13.549	13.495
3d <sup>4</sup> 3F <sup>2</sup>	3	3d <sup>4</sup> 1D <sup>2</sup>	2	11.907	11.901				
3d <sup>4</sup> 3F <sup>2</sup>	3	3d <sup>4</sup> 5D <sup>4</sup>	4	9.538	9.525				
3d <sup>4</sup> 3F <sup>2</sup>	3	3d <sup>4</sup> 3F <sup>4</sup>	3	9.439	9.426				
3d <sup>4</sup> 3F <sup>2</sup>	3	3d <sup>4</sup> 3F <sup>4</sup>	2	8.508	8.497				
3d <sup>4</sup> 3F <sup>2</sup>	3	3d <sup>4</sup> 3D <sup>4</sup>	3	8.390	8.381				
3d <sup>4</sup> 3F <sup>2</sup>	3	3d <sup>4</sup> 3F <sup>2</sup>	3	7.610	7.602				
3d <sup>4</sup> 3F <sup>2</sup>	3	3d <sup>4</sup> 1G <sup>2</sup>	4	7.581	7.573				
3d <sup>4</sup> 3F <sup>2</sup>	3	3d <sup>4</sup> 1D <sup>4</sup>	2	7.392	7.386				
3d <sup>4</sup> 3F <sup>2</sup>	3	3d <sup>4</sup> 3F <sup>2</sup>	4	5.847	5.839				
3d <sup>4</sup> 3F <sup>2</sup>	3	3d <sup>4</sup> 1D <sup>2</sup>	2	5.572	5.565				
3d <sup>4</sup> 5D <sup>4</sup>	0	3d <sup>4</sup> 3D <sup>4</sup>	1	89.555	89.798				
3d <sup>4</sup> 5D <sup>4</sup>	0	3d <sup>4</sup> 3D <sup>4</sup>	1	15.041	15.028				
3d <sup>4</sup> 5D <sup>4</sup>	0	3d <sup>4</sup> 3P <sup>2</sup>	1	11.338	11.334				
3d <sup>4</sup> 5D <sup>4</sup>	2	3d <sup>4</sup> 5D <sup>4</sup>	3	284.116	285.346				
3d <sup>4</sup> 5D <sup>4</sup>	2	3d <sup>4</sup> 3D <sup>4</sup>	1	93.723	93.840				
3d <sup>4</sup> 5D <sup>4</sup>	2	3d <sup>4</sup> 3F <sup>4</sup>	3	75.583	75.791				
3d <sup>4</sup> 5D <sup>4</sup>	2	3d <sup>4</sup> 3F <sup>4</sup>	2	66.257	66.382				
3d <sup>4</sup> 5D <sup>4</sup>	2	3d <sup>4</sup> 3F <sup>2</sup>	2	39.611	39.610				
3d <sup>4</sup> 5D <sup>4</sup>	2	3d <sup>4</sup> 1D <sup>2</sup>	2	25.072	25.102				
3d <sup>4</sup> 5D <sup>4</sup>	2	3d <sup>4</sup> 3F <sup>4</sup>	3	16.170	16.153				
3d <sup>4</sup> 5D <sup>4</sup>	2	3d <sup>4</sup> 3D <sup>4</sup>	1	15.154	15.138				
3d <sup>4</sup> 5D <sup>4</sup>	2	3d <sup>4</sup> 3F <sup>4</sup>	2	13.617	13.605				
3d <sup>4</sup> 5D <sup>4</sup>	2	3d <sup>4</sup> 3D <sup>4</sup>	3	13.318	13.311				
3d <sup>4</sup> 5D <sup>4</sup>	2	3d <sup>4</sup> 3F <sup>2</sup>	3	11.453	11.448				
3d <sup>4</sup> 5D <sup>4</sup>	2	3d <sup>4</sup> 3P <sup>2</sup>	1	11.402	11.396				
3d <sup>4</sup> 5D <sup>4</sup>	2	3d <sup>4</sup> 1D <sup>4</sup>	2	10.967	10.964				
3d <sup>4</sup> 5D <sup>4</sup>	2	3d <sup>4</sup> 1D <sup>2</sup>	2	7.387	7.380				
3d <sup>4</sup> 3H <sup>4</sup>	4	3d <sup>4</sup> 5D <sup>4</sup>	3	606.876	608.761				
3d <sup>4</sup> 3H <sup>4</sup>	4	3d <sup>4</sup> 3H <sup>4</sup>	5	214.114	215.206				
3d <sup>4</sup> 3H <sup>4</sup>	4	3d <sup>4</sup> 3F <sup>4</sup>	3	88.039	88.243				
3d <sup>4</sup> 3H <sup>4</sup>	4	3d <sup>4</sup> 3G <sup>4</sup>	4	85.561	85.781				
3d <sup>4</sup> 3H <sup>4</sup>	4	3d <sup>4</sup> 3F <sup>2</sup>	4	35.956	36.020				
3d <sup>4</sup> 3H <sup>4</sup>	4	3d <sup>4</sup> 5D <sup>4</sup>	4	16.986	16.966				
3d <sup>4</sup> 3H <sup>4</sup>	4	3d <sup>4</sup> 3F <sup>4</sup>	3	16.675	16.654				
3d <sup>4</sup> 3H <sup>4</sup>	4	3d <sup>4</sup> 3G <sup>4</sup>	5	15.427	15.416				
3d <sup>4</sup> 3H <sup>4</sup>	4	3d <sup>4</sup> 3D <sup>4</sup>	3	13.658	13.649				
3d <sup>4</sup> 3H <sup>4</sup>	4	3d <sup>4</sup> 3F <sup>2</sup>	3	11.704	11.697				
3d <sup>4</sup> 3H <sup>4</sup>	4	3d <sup>4</sup> 1G <sup>2</sup>	4	11.635	11.628				
3d <sup>4</sup> 3H <sup>4</sup>	4	3d <sup>4</sup> 3F <sup>2</sup>	4	7.996	7.986				
3d <sup>4</sup> 5D <sup>4</sup>	3	3d <sup>4</sup> 3F <sup>4</sup>	3	102.978	103.203				

Table 5. Cont.

Label and J for Lower	Label and J for Upper		Present Work		Expt (Ref. [2])	GRASP	RMBPT <sub>g</sub>	RCI <sub>g</sub>
			n = 5	n = 6				
3d <sup>4</sup> 5D <sup>4</sup>	3 3d <sup>4</sup> 3G <sup>4</sup>	4	99.604	99.852				
3d <sup>4</sup> 5D <sup>4</sup>	3 3d <sup>4</sup> 3F <sup>4</sup>	2	86.407	86.507				
3d <sup>4</sup> 5D <sup>4</sup>	3 3d <sup>4</sup> 3F <sup>2</sup>	2	46.028	45.995				
3d <sup>4</sup> 5D <sup>4</sup>	3 3d <sup>4</sup> 3F <sup>2</sup>	4	38.221	38.285				
3d <sup>4</sup> 5D <sup>4</sup>	3 3d <sup>4</sup> 1D <sup>2</sup>	2	27.498	27.524				
3d <sup>4</sup> 5D <sup>4</sup>	3 3d <sup>4</sup> 5D <sup>4</sup>	4	17.475	17.453				
3d <sup>4</sup> 5D <sup>4</sup>	3 3d <sup>4</sup> 3F <sup>4</sup>	3	17.146	17.123				
3d <sup>4</sup> 5D <sup>4</sup>	3 3d <sup>4</sup> 3F <sup>4</sup>	2	14.303	14.287				
3d <sup>4</sup> 5D <sup>4</sup>	3 3d <sup>4</sup> 3D <sup>4</sup>	3	13.973	13.962				
3d <sup>4</sup> 5D <sup>4</sup>	3 3d <sup>4</sup> 3F <sup>2</sup>	3	11.934	11.926				
3d <sup>4</sup> 5D <sup>4</sup>	3 3d <sup>4</sup> 1G <sup>2</sup>	4	11.863	11.855				
3d <sup>4</sup> 5D <sup>4</sup>	3 3d <sup>4</sup> 1D <sup>4</sup>	2	11.408	11.402				
3d <sup>4</sup> 5D <sup>4</sup>	3 3d <sup>4</sup> 3F <sup>2</sup>	4	8.102	8.092				
3d <sup>4</sup> 5D <sup>4</sup>	3 3d <sup>4</sup> 1D <sup>2</sup>	2	7.584	7.575				
3d <sup>4</sup> 3H <sup>4</sup>	5 3d <sup>4</sup> 1J <sup>4</sup>	6	428.184	430.120				
3d <sup>4</sup> 3H <sup>4</sup>	5 3d <sup>4</sup> 3G <sup>4</sup>	4	142.509	142.637				
3d <sup>4</sup> 3H <sup>4</sup>	5 3d <sup>4</sup> 3F <sup>2</sup>	4	43.213	43.261				
3d <sup>4</sup> 3H <sup>4</sup>	5 3d <sup>4</sup> 5D <sup>4</sup>	4	18.450	18.418				
3d <sup>4</sup> 3H <sup>4</sup>	5 3d <sup>4</sup> 3G <sup>4</sup>	5	16.625	16.605				
3d <sup>4</sup> 3H <sup>4</sup>	5 3d <sup>4</sup> 3H <sup>4</sup>	6	16.488	16.470				
3d <sup>4</sup> 3H <sup>4</sup>	5 3d <sup>4</sup> 1G <sup>2</sup>	4	12.304	12.292				
3d <sup>4</sup> 3H <sup>4</sup>	5 3d <sup>4</sup> 3F <sup>2</sup>	4	8.306	8.293				
3d <sup>4</sup> 1I <sup>4</sup>	6 3d <sup>4</sup> 3G <sup>4</sup>	5	17.296	17.272				
3d <sup>4</sup> 1I <sup>4</sup>	6 3d <sup>4</sup> 3H <sup>4</sup>	6	17.148	17.126				
3d <sup>4</sup> 3D <sup>4</sup>	1 3d <sup>4</sup> 3F <sup>4</sup>	2	226.092	226.868				
3d <sup>4</sup> 3D <sup>4</sup>	1 3d <sup>4</sup> 3F <sup>2</sup>	2	68.606	68.541				
3d <sup>4</sup> 3D <sup>4</sup>	1 3d <sup>4</sup> 1D <sup>2</sup>	2	34.228	34.269				
3d <sup>4</sup> 3D <sup>4</sup>	1 3d <sup>4</sup> 3P <sup>4</sup>	0	23.832	23.832				
3d <sup>4</sup> 3D <sup>4</sup>	1 3d <sup>4</sup> 3D <sup>4</sup>	1	18.077	18.049				
3d <sup>4</sup> 3D <sup>4</sup>	1 3d <sup>4</sup> 3F <sup>4</sup>	2	15.932	15.912				
3d <sup>4</sup> 3D <sup>4</sup>	1 3d <sup>4</sup> 1S <sup>4</sup>	0	14.097	14.094				
3d <sup>4</sup> 3D <sup>4</sup>	1 3d <sup>4</sup> 3P <sup>2</sup>	1	12.981	12.972				
3d <sup>4</sup> 3D <sup>4</sup>	1 3d <sup>4</sup> 1D <sup>4</sup>	2	12.421	12.415				
3d <sup>4</sup> 3D <sup>4</sup>	1 3d <sup>4</sup> 1D <sup>2</sup>	2	8.019	8.009				
3d <sup>4</sup> 3D <sup>4</sup>	1 3d <sup>4</sup> 3P <sup>2</sup>	0	6.900	6.892				
3d <sup>4</sup> 3F <sup>4</sup>	3 3d <sup>4</sup> 3G <sup>4</sup>	4	3040.724	3074.775				
3d <sup>4</sup> 3F <sup>4</sup>	3 3d <sup>4</sup> 3F <sup>4</sup>	2	536.990	534.715				
3d <sup>4</sup> 3F <sup>4</sup>	3 3d <sup>4</sup> 3F <sup>2</sup>	2	83.228	82.973				
3d <sup>4</sup> 3F <sup>4</sup>	3 3d <sup>4</sup> 3F <sup>2</sup>	4	60.779	60.864				
3d <sup>4</sup> 3F <sup>4</sup>	3 3d <sup>4</sup> 1D <sup>2</sup>	2	37.516	37.533				
3d <sup>4</sup> 3F <sup>4</sup>	3 3d <sup>4</sup> 5D <sup>4</sup>	4	21.047	21.005				
3d <sup>4</sup> 3F <sup>4</sup>	3 3d <sup>4</sup> 3F <sup>4</sup>	3	20.571	20.529				
3d <sup>4</sup> 3F <sup>4</sup>	3 3d <sup>4</sup> 3F <sup>4</sup>	2	16.610	16.582				
3d <sup>4</sup> 3F <sup>4</sup>	3 3d <sup>4</sup> 3D <sup>4</sup>	3	16.166	16.147				
3d <sup>4</sup> 3F <sup>4</sup>	3 3d <sup>4</sup> 3F <sup>2</sup>	3	13.498	13.485				
3d <sup>4</sup> 3F <sup>4</sup>	3 3d <sup>4</sup> 1G <sup>2</sup>	4	13.407	13.393				
3d <sup>4</sup> 3F <sup>4</sup>	3 3d <sup>4</sup> 1D <sup>4</sup>	2	12.829	12.819				
3d <sup>4</sup> 3F <sup>4</sup>	3 3d <sup>4</sup> 3F <sup>2</sup>	4	8.794	8.780				
3d <sup>4</sup> 3F <sup>4</sup>	3 3d <sup>4</sup> 1D <sup>2</sup>	2	8.187	8.176				

Table 5. Cont.

Label and J for Lower		Label and J for Upper		Present Work		Expt (Ref. [2])	GRASP	RMBPT <sub>g</sub>	RCI <sub>g</sub>
				n = 5	n = 6				
3d <sup>4</sup> 3G <sup>4</sup>	4	3d <sup>4</sup> 3F <sup>2</sup>	4	62.019	62.093				
3d <sup>4</sup> 3G <sup>4</sup>	4	3d <sup>4</sup> 5D <sup>4</sup>	4	21.194	21.149				
3d <sup>4</sup> 3G <sup>4</sup>	4	3d <sup>4</sup> 3F <sup>4</sup>	3	20.711	20.667				
3d <sup>4</sup> 3G <sup>4</sup>	4	3d <sup>4</sup> 3G <sup>4</sup>	5	18.820	18.793				
3d <sup>4</sup> 3G <sup>4</sup>	4	3d <sup>4</sup> 3D <sup>4</sup>	3	16.253	16.232				
3d <sup>4</sup> 3G <sup>4</sup>	4	3d <sup>4</sup> 3F <sup>2</sup>	3	13.559	13.544				
3d <sup>4</sup> 3G <sup>4</sup>	4	3d <sup>4</sup> 1G <sup>2</sup>	4	13.466	13.452				
3d <sup>4</sup> 3G <sup>4</sup>	4	3d <sup>4</sup> 3F <sup>2</sup>	4	8.820	8.805				
3d <sup>4</sup> 3F <sup>4</sup>	2	3d <sup>4</sup> 3F <sup>2</sup>	2	98.494	98.213				
3d <sup>4</sup> 3F <sup>4</sup>	2	3d <sup>4</sup> 1D <sup>2</sup>	2	40.334	40.367				
3d <sup>4</sup> 3F <sup>4</sup>	2	3d <sup>4</sup> 3F <sup>4</sup>	3	21.391	21.348				
3d <sup>4</sup> 3F <sup>4</sup>	2	3d <sup>4</sup> 3D <sup>4</sup>	1	19.648	19.609				
3d <sup>4</sup> 3F <sup>4</sup>	2	3d <sup>4</sup> 3F <sup>4</sup>	2	17.140	17.113				
3d <sup>4</sup> 3F <sup>4</sup>	2	3d <sup>4</sup> 3D <sup>4</sup>	3	16.668	16.649				
3d <sup>4</sup> 3F <sup>4</sup>	2	3d <sup>4</sup> 3F <sup>2</sup>	3	13.846	13.834				
3d <sup>4</sup> 3F <sup>4</sup>	2	3d <sup>4</sup> 3p <sup>2</sup>	1	13.772	13.759				
3d <sup>4</sup> 3F <sup>4</sup>	2	3d <sup>4</sup> 1D <sup>4</sup>	2	13.143	13.133				
3d <sup>4</sup> 3F <sup>4</sup>	2	3d <sup>4</sup> 1D <sup>2</sup>	2	8.314	8.302				
3d <sup>4</sup> 3F <sup>2</sup>	2	3d <sup>4</sup> 1D <sup>2</sup>	2	68.306	68.536				
3d <sup>4</sup> 3F <sup>2</sup>	2	3d <sup>4</sup> 3F <sup>4</sup>	3	27.325	27.278				
3d <sup>4</sup> 3F <sup>2</sup>	2	3d <sup>4</sup> 3D <sup>4</sup>	1	24.544	24.501				
3d <sup>4</sup> 3F <sup>2</sup>	2	3d <sup>4</sup> 3F <sup>4</sup>	2	20.751	20.724				
3d <sup>4</sup> 3F <sup>2</sup>	2	3d <sup>4</sup> 3D <sup>4</sup>	3	20.063	20.048				
3d <sup>4</sup> 3F <sup>2</sup>	2	3d <sup>4</sup> 3F <sup>2</sup>	3	16.111	16.102				
3d <sup>4</sup> 3F <sup>2</sup>	2	3d <sup>4</sup> 3p <sup>2</sup>	1	16.011	16.000				
3d <sup>4</sup> 3F <sup>2</sup>	2	3d <sup>4</sup> 1D <sup>4</sup>	2	15.166	15.161				
3d <sup>4</sup> 3F <sup>2</sup>	2	3d <sup>4</sup> 1D <sup>2</sup>	2	9.081	9.069				
3d <sup>4</sup> 3F <sup>2</sup>	4	3d <sup>4</sup> 5D <sup>4</sup>	4	32.196	32.074				
3d <sup>4</sup> 3F <sup>2</sup>	4	3d <sup>4</sup> 3F <sup>4</sup>	3	31.096	30.977				
3d <sup>4</sup> 3F <sup>2</sup>	4	3d <sup>4</sup> 3G <sup>4</sup>	5	27.020	26.950				
3d <sup>4</sup> 3F <sup>2</sup>	4	3d <sup>4</sup> 3D <sup>4</sup>	3	22.024	21.977				
3d <sup>4</sup> 3F <sup>2</sup>	4	3d <sup>4</sup> 3F <sup>2</sup>	3	17.352	17.323				
3d <sup>4</sup> 3F <sup>2</sup>	4	3d <sup>4</sup> 1G <sup>2</sup>	4	17.201	17.172				
3d <sup>4</sup> 3F <sup>2</sup>	4	3d <sup>4</sup> 3F <sup>2</sup>	4	10.282	10.260				
3d <sup>4</sup> 1D <sup>2</sup>	2	3d <sup>4</sup> 3F <sup>4</sup>	3	45.544	45.312				
3d <sup>4</sup> 1D <sup>2</sup>	2	3d <sup>4</sup> 3D <sup>4</sup>	1	38.310	38.133				
3d <sup>4</sup> 1D <sup>2</sup>	2	3d <sup>4</sup> 3F <sup>4</sup>	2	29.806	29.706				
3d <sup>4</sup> 1D <sup>2</sup>	2	3d <sup>4</sup> 3D <sup>4</sup>	3	28.407	28.337				
3d <sup>4</sup> 1D <sup>2</sup>	2	3d <sup>4</sup> 3F <sup>2</sup>	3	21.085	21.046				
3d <sup>4</sup> 1D <sup>2</sup>	2	3d <sup>4</sup> 3p <sup>2</sup>	1	20.912	20.873				
3d <sup>4</sup> 1D <sup>2</sup>	2	3d <sup>4</sup> 1D <sup>4</sup>	2	19.495	19.467				
3d <sup>4</sup> 1D <sup>2</sup>	2	3d <sup>4</sup> 1D <sup>2</sup>	2	10.473	10.452				
3d <sup>4</sup> 3P <sup>4</sup>	0	3d <sup>4</sup> 3D <sup>4</sup>	1	74.865	74.385				
3d <sup>4</sup> 3P <sup>4</sup>	0	3d <sup>4</sup> 3p <sup>2</sup>	1	28.511	28.466				
3d <sup>4</sup> 5D <sup>4</sup>	4	3d <sup>4</sup> 3F <sup>4</sup>	3	910.088	905.530				
3d <sup>4</sup> 5D <sup>4</sup>	4	3d <sup>4</sup> 3G <sup>4</sup>	5	168.067	168.682				
3d <sup>4</sup> 5D <sup>4</sup>	4	3d <sup>4</sup> 3D <sup>4</sup>	3	69.712	69.810				
3d <sup>4</sup> 5D <sup>4</sup>	4	3d <sup>4</sup> 3F <sup>2</sup>	3	37.636	37.665				
3d <sup>4</sup> 5D <sup>4</sup>	4	3d <sup>4</sup> 1G <sup>2</sup>	4	36.935	36.959				



Table 5. Cont.

Label and J for Lower	Label and J for Upper	Present Work		Expt (Ref. [2])	GRASP	RMBPT <sub>g</sub>	RCI <sub>g</sub>		
		n = 5	n = 6						
3d <sup>4</sup> 5D <sup>4</sup>	4	3d <sup>4</sup> 3F <sup>2</sup>	4	15.106	15.086				
3d <sup>4</sup> 3F <sup>4</sup>	3	3d <sup>4</sup> 3F <sup>4</sup>	2	86.253	86.253				
3d <sup>4</sup> 3F <sup>4</sup>	3	3d <sup>4</sup> 3D <sup>4</sup>	3	75.495	75.642				
3d <sup>4</sup> 3F <sup>4</sup>	3	3d <sup>4</sup> 3F <sup>2</sup>	3	39.260	39.300				
3d <sup>4</sup> 3F <sup>4</sup>	3	3d <sup>4</sup> 1G <sup>2</sup>	4	38.498	38.532				
3d <sup>4</sup> 3F <sup>4</sup>	3	3d <sup>4</sup> 1D <sup>4</sup>	2	34.085	34.130				
3d <sup>4</sup> 3F <sup>4</sup>	3	3d <sup>4</sup> 3F <sup>2</sup>	4	15.361	15.342				
3d <sup>4</sup> 3F <sup>4</sup>	3	3d <sup>4</sup> 1D <sup>2</sup>	2	13.600	13.586				
3d <sup>4</sup> 3D <sup>4</sup>	1	3d <sup>4</sup> 3F <sup>4</sup>	2	134.268	134.420				
3d <sup>4</sup> 3D <sup>4</sup>	1	3d <sup>4</sup> 1S <sup>4</sup>	0	64.031	64.317				
3d <sup>4</sup> 3D <sup>4</sup>	1	3d <sup>4</sup> 3P <sup>2</sup>	1	46.049	46.113				
3d <sup>4</sup> 3D <sup>4</sup>	1	3d <sup>4</sup> 1D <sup>4</sup>	2	39.694	39.769				
3d <sup>4</sup> 3D <sup>4</sup>	1	3d <sup>4</sup> 1D <sup>2</sup>	2	14.413	14.399				
3d <sup>4</sup> 3D <sup>4</sup>	1	3d <sup>4</sup> 3P <sup>2</sup>	0	11.160	11.149				
3d <sup>4</sup> 3G <sup>4</sup>	5	3d <sup>4</sup> 3H <sup>4</sup>	6	1997.212	2027.160				
3d <sup>4</sup> 3G <sup>4</sup>	5	3d <sup>4</sup> 1G <sup>2</sup>	4	47.338	47.329				
3d <sup>4</sup> 3G <sup>4</sup>	5	3d <sup>4</sup> 3F <sup>2</sup>	4	16.598	16.568				
3d <sup>4</sup> 3F <sup>4</sup>	2	3d <sup>4</sup> 3D <sup>4</sup>	3	605.307	614.828				
3d <sup>4</sup> 3F <sup>4</sup>	2	3d <sup>4</sup> 3F <sup>2</sup>	3	72.059	72.193				
3d <sup>4</sup> 3F <sup>4</sup>	2	3d <sup>4</sup> 3P <sup>2</sup>	1	70.085	70.193				
3d <sup>4</sup> 3F <sup>4</sup>	2	3d <sup>4</sup> 1D <sup>4</sup>	2	56.355	56.479				
3d <sup>4</sup> 3F <sup>4</sup>	2	3d <sup>4</sup> 1D <sup>2</sup>	2	16.146	16.126				
3d <sup>4</sup> 3D <sup>4</sup>	3	3d <sup>4</sup> 3F <sup>2</sup>	3	81.796	81.797				
3d <sup>4</sup> 3D <sup>4</sup>	3	3d <sup>4</sup> 1G <sup>2</sup>	4	78.556	78.539				
3d <sup>4</sup> 3D <sup>4</sup>	3	3d <sup>4</sup> 1D <sup>4</sup>	2	62.140	62.192				
3d <sup>4</sup> 3D <sup>4</sup>	3	3d <sup>4</sup> 3F <sup>2</sup>	4	19.285	19.245				
3d <sup>4</sup> 3D <sup>4</sup>	3	3d <sup>4</sup> 1D <sup>2</sup>	2	16.589	16.561				
3d <sup>4</sup> 1S <sup>4</sup>	0	3d <sup>4</sup> 3P <sup>2</sup>	1	163.968	162.926				
3d <sup>4</sup> 3F <sup>2</sup>	3	3d <sup>4</sup> 1G <sup>2</sup>	4	1982.892	1971.659				
3d <sup>4</sup> 3F <sup>2</sup>	3	3d <sup>4</sup> 1D <sup>4</sup>	2	258.586	259.474				
3d <sup>4</sup> 3F <sup>2</sup>	3	3d <sup>4</sup> 3F <sup>2</sup>	4	25.235	25.166				
3d <sup>4</sup> 3F <sup>2</sup>	3	3d <sup>4</sup> 1D <sup>2</sup>	2	20.809	20.765				
3d <sup>4</sup> 3P <sup>2</sup>	1	3d <sup>4</sup> 1D <sup>4</sup>	2	287.662	289.068				
3d <sup>4</sup> 3P <sup>2</sup>	1	3d <sup>4</sup> 1D <sup>2</sup>	2	20.980	20.936				
3d <sup>4</sup> 3P <sup>2</sup>	1	3d <sup>4</sup> 3P <sup>2</sup>	0	14.730	14.704				
3d <sup>4</sup> 1G <sup>2</sup>	4	3d <sup>4</sup> 3F <sup>2</sup>	4	25.560	25.491				
3d <sup>4</sup> 1D <sup>4</sup>	2	3d <sup>4</sup> 1D <sup>2</sup>	2	22.630	22.571				
W <sup>51+</sup> (V-like)									
3d <sup>5</sup> 4P <sup>3</sup>	5/2	3d <sup>5</sup> 6S <sup>5</sup>	5/2	21.290	21.243	21.203(3)	21.317	21.185	21.492
3d <sup>5</sup> 4P <sup>3</sup>	5/2	3d <sup>5</sup> 4G <sup>5</sup>	7/2	17.700	17.674	17.660(3)	17.660	17.655	17.826
3d <sup>5</sup> 4P <sup>3</sup>	5/2	3d <sup>5</sup> 4D <sup>5</sup>	3/2	17.253	17.227	17.215(3)	17.247	17.228	17.249
3d <sup>5</sup> 4P <sup>3</sup>	5/2	3d <sup>5</sup> 4D <sup>5</sup>	5/2	15.368	15.350				
3d <sup>5</sup> 4P <sup>3</sup>	5/2	3d <sup>5</sup> 2F <sup>5</sup>	7/2	14.541	14.529	14.531(3)	14.475	14.537	14.513
3d <sup>5</sup> 4P <sup>3</sup>	5/2	3d <sup>5</sup> 2D <sup>1</sup>	3/2	12.136	12.122				
3d <sup>5</sup> 4P <sup>3</sup>	5/2	3d <sup>5</sup> 6S <sup>5</sup>	5/2	9.747	9.728				
3d <sup>5</sup> 4P <sup>3</sup>	5/2	3d <sup>5</sup> 4D <sup>5</sup>	7/2	9.117	9.102				
3d <sup>5</sup> 4P <sup>3</sup>	5/2	3d <sup>5</sup> 4P <sup>3</sup>	3/2	8.586	8.571				
3d <sup>5</sup> 4P <sup>3</sup>	5/2	3d <sup>5</sup> 2F <sup>5</sup>	5/2	8.511	8.499				

Table 5. Cont.

Label and J for Lower		Label and J for Upper		Present Work		Expt (Ref. [2])	GRASP	RMBPT <sub>g</sub>	RCI <sub>g</sub>
				n = 5	n = 6				
3d <sup>5</sup> 4p <sup>3</sup>	5/2	3d <sup>5</sup> 2G <sup>5</sup>	7/2	8.078	8.068				
3d <sup>5</sup> 4p <sup>3</sup>	5/2	3d <sup>5</sup> 4F <sup>3</sup>	5/2	7.971	7.959				
3d <sup>5</sup> 4p <sup>3</sup>	5/2	3d <sup>5</sup> 2D <sup>5</sup>	3/2	7.940	7.931				
3d <sup>5</sup> 4p <sup>3</sup>	5/2	3d <sup>5</sup> 2G <sup>3</sup>	7/2	7.646	7.636				
3d <sup>5</sup> 4p <sup>3</sup>	5/2	3d <sup>5</sup> 2P <sup>3</sup>	3/2	6.645	6.639				
3d <sup>5</sup> 4p <sup>3</sup>	5/2	3d <sup>5</sup> 2D <sup>1</sup>	5/2	6.522	6.516				
3d <sup>5</sup> 4p <sup>3</sup>	5/2	3d <sup>5</sup> 4P <sup>3</sup>	5/2	6.021	6.010				
3d <sup>5</sup> 4p <sup>3</sup>	5/2	3d <sup>5</sup> 4F <sup>3</sup>	7/2	5.768	5.758				
3d <sup>5</sup> 4p <sup>3</sup>	5/2	3d <sup>5</sup> 4D <sup>5</sup>	3/2	5.684	5.674				
3d <sup>5</sup> 4p <sup>3</sup>	5/2	3d <sup>5</sup> 2D <sup>3</sup>	5/2	5.424	5.416				
3d <sup>5</sup> 4p <sup>3</sup>	5/2	3d <sup>5</sup> 2G <sup>3</sup>	7/2	5.343	5.335				
3d <sup>5</sup> 4p <sup>3</sup>	5/2	3d <sup>5</sup> 2D <sup>1</sup>	3/2	4.847	4.841				
3d <sup>5</sup> 4p <sup>3</sup>	5/2	3d <sup>5</sup> 2D <sup>1</sup>	5/2	4.233	4.225				
3d <sup>5</sup> 6S <sup>5</sup>	5/2	3d <sup>5</sup> 4G <sup>5</sup>	7/2	104.969	105.214				
3d <sup>5</sup> 6S <sup>5</sup>	5/2	3d <sup>5</sup> 4D <sup>5</sup>	3/2	90.995	91.119				
3d <sup>5</sup> 6S <sup>5</sup>	5/2	3d <sup>5</sup> 4D <sup>5</sup>	5/2	55.250	55.341				
3d <sup>5</sup> 6S <sup>5</sup>	5/2	3d <sup>5</sup> 2F <sup>5</sup>	7/2	45.868	45.971				
3d <sup>5</sup> 6S <sup>5</sup>	5/2	3d <sup>5</sup> 2D <sup>1</sup>	3/2	28.226	28.233				
3d <sup>5</sup> 6S <sup>5</sup>	5/2	3d <sup>5</sup> 6S <sup>5</sup>	5/2	17.977	17.946				
3d <sup>5</sup> 6S <sup>5</sup>	5/2	3d <sup>5</sup> 4D <sup>5</sup>	7/2	15.946	15.927				
3d <sup>5</sup> 6S <sup>5</sup>	5/2	3d <sup>5</sup> 4P <sup>3</sup>	3/2	14.388	14.367				
3d <sup>5</sup> 6S <sup>5</sup>	5/2	3d <sup>5</sup> 2F <sup>5</sup>	5/2	14.181	14.167				
3d <sup>5</sup> 6S <sup>5</sup>	5/2	3d <sup>5</sup> 2G <sup>5</sup>	7/2	13.018	13.009				
3d <sup>5</sup> 6S <sup>5</sup>	5/2	3d <sup>5</sup> 4F <sup>3</sup>	5/2	12.741	12.727				
3d <sup>5</sup> 6S <sup>5</sup>	5/2	3d <sup>5</sup> 2D <sup>5</sup>	3/2	12.662	12.655				
3d <sup>5</sup> 6S <sup>5</sup>	5/2	3d <sup>5</sup> 2G <sup>3</sup>	7/2	11.932	11.921				
3d <sup>5</sup> 6S <sup>5</sup>	5/2	3d <sup>5</sup> 2P <sup>3</sup>	3/2	9.660	9.657				
3d <sup>5</sup> 6S <sup>5</sup>	5/2	3d <sup>5</sup> 2D <sup>1</sup>	5/2	9.403	9.399				
3d <sup>5</sup> 6S <sup>5</sup>	5/2	3d <sup>5</sup> 4P <sup>3</sup>	5/2	8.395	8.381				
3d <sup>5</sup> 6S <sup>5</sup>	5/2	3d <sup>5</sup> 4F <sup>3</sup>	7/2	7.912	7.900				
3d <sup>5</sup> 6S <sup>5</sup>	5/2	3d <sup>5</sup> 4D <sup>5</sup>	3/2	7.755	7.743				
3d <sup>5</sup> 6S <sup>5</sup>	5/2	3d <sup>5</sup> 2D <sup>3</sup>	5/2	7.277	7.269				
3d <sup>5</sup> 6S <sup>5</sup>	5/2	3d <sup>5</sup> 2G <sup>3</sup>	7/2	7.133	7.124				
3d <sup>5</sup> 6S <sup>5</sup>	5/2	3d <sup>5</sup> 2D <sup>1</sup>	3/2	6.276	6.269				
3d <sup>5</sup> 6S <sup>5</sup>	5/2	3d <sup>5</sup> 2D <sup>1</sup>	5/2	5.283	5.274				
3d <sup>5</sup> 4G <sup>5</sup>	7/2	3d <sup>5</sup> 2G <sup>5</sup>	9/2	178.750	179.156				
3d <sup>5</sup> 4G <sup>5</sup>	7/2	3d <sup>5</sup> 4D <sup>5</sup>	5/2	116.648	116.752				
3d <sup>5</sup> 4G <sup>5</sup>	7/2	3d <sup>5</sup> 2F <sup>5</sup>	7/2	81.465	81.645				
3d <sup>5</sup> 4G <sup>5</sup>	7/2	3d <sup>5</sup> 6S <sup>5</sup>	5/2	21.692	21.637				
3d <sup>5</sup> 4G <sup>5</sup>	7/2	3d <sup>5</sup> 4D <sup>5</sup>	7/2	18.802	18.768				
3d <sup>5</sup> 4G <sup>5</sup>	7/2	3d <sup>5</sup> 4G <sup>5</sup>	9/2	18.116	18.086				
3d <sup>5</sup> 4G <sup>5</sup>	7/2	3d <sup>5</sup> 2F <sup>5</sup>	5/2	16.396	16.372				
3d <sup>5</sup> 4G <sup>5</sup>	7/2	3d <sup>5</sup> 2H <sup>3</sup>	9/2	15.329	15.304				
3d <sup>5</sup> 4G <sup>5</sup>	7/2	3d <sup>5</sup> 2G <sup>5</sup>	7/2	14.861	14.845				
3d <sup>5</sup> 4G <sup>5</sup>	7/2	3d <sup>5</sup> 4F <sup>3</sup>	5/2	14.501	14.479				
3d <sup>5</sup> 4G <sup>5</sup>	7/2	3d <sup>5</sup> 2G <sup>3</sup>	7/2	13.462	13.444				
3d <sup>5</sup> 4G <sup>5</sup>	7/2	3d <sup>5</sup> 2G <sup>3</sup>	9/2	12.275	12.264				
3d <sup>5</sup> 4G <sup>5</sup>	7/2	3d <sup>5</sup> 2D <sup>1</sup>	5/2	10.329	10.321				
3d <sup>5</sup> 4G <sup>5</sup>	7/2	3d <sup>5</sup> 4P <sup>3</sup>	5/2	9.125	9.106				

Table 5. Cont.

Label and J for Lower		Label and J for Upper		Present Work		Expt (Ref. [2])	GRASP	RMBPT <sub>g</sub>	RCI <sub>g</sub>
				n = 5	n = 6				
3d <sup>5</sup> 4G <sup>5</sup>	7/2	3d <sup>5</sup> 4F <sup>3</sup>	7/2	8.557	8.541				
3d <sup>5</sup> 4G <sup>5</sup>	7/2	3d <sup>5</sup> 2G <sup>5</sup>	9/2	8.057	8.044				
3d <sup>5</sup> 4G <sup>5</sup>	7/2	3d <sup>5</sup> 2D <sup>3</sup>	5/2	7.820	7.808				
3d <sup>5</sup> 4G <sup>5</sup>	7/2	3d <sup>5</sup> 2G <sup>3</sup>	7/2	7.653	7.642				
3d <sup>5</sup> 4G <sup>5</sup>	7/2	3d <sup>5</sup> 2D <sup>1</sup>	5/2	5.563	5.553				
3d <sup>5</sup> 2H <sup>3</sup>	11/2	3d <sup>5</sup> 2G <sup>5</sup>	9/2	222.726	223.030				
3d <sup>5</sup> 2H <sup>3</sup>	11/2	3d <sup>5</sup> 4G <sup>5</sup>	11/2	19.056	19.021	18.996(3)	19.064	19.002	19.185
3d <sup>5</sup> 2H <sup>3</sup>	11/2	3d <sup>5</sup> 4G <sup>5</sup>	9/2	18.486	18.453				
3d <sup>5</sup> 2H <sup>3</sup>	11/2	3d <sup>5</sup> 2I <sup>5</sup>	13/2	17.664	17.637				
3d <sup>5</sup> 2H <sup>3</sup>	11/2	3d <sup>5</sup> 2H <sup>3</sup>	9/2	15.593	15.566				
3d <sup>5</sup> 2H <sup>3</sup>	11/2	3d <sup>5</sup> 2G <sup>3</sup>	9/2	12.443	12.432				
3d <sup>5</sup> 2H <sup>3</sup>	11/2	3d <sup>5</sup> 2H <sup>3</sup>	11/2	8.544	8.528				
3d <sup>5</sup> 2H <sup>3</sup>	11/2	3d <sup>5</sup> 2G <sup>5</sup>	9/2	8.129	8.116				
3d <sup>5</sup> 4D <sup>5</sup>	3/2	3d <sup>5</sup> 4D <sup>5</sup>	5/2	140.653	140.944				
3d <sup>5</sup> 4D <sup>5</sup>	3/2	3d <sup>5</sup> 4P <sup>3</sup>	1/2	100.009	100.120				
3d <sup>5</sup> 4D <sup>5</sup>	3/2	3d <sup>5</sup> 2D <sup>1</sup>	3/2	40.920	40.907				
3d <sup>5</sup> 4D <sup>5</sup>	3/2	3d <sup>5</sup> 6S <sup>5</sup>	5/2	22.403	22.348				
3d <sup>5</sup> 4D <sup>5</sup>	3/2	3d <sup>5</sup> 4D <sup>5</sup>	1/2	17.360	17.334				
3d <sup>5</sup> 4D <sup>5</sup>	3/2	3d <sup>5</sup> 4P <sup>3</sup>	3/2	17.091	17.056				
3d <sup>5</sup> 4D <sup>5</sup>	3/2	3d <sup>5</sup> 2F <sup>5</sup>	5/2	16.799	16.775				
3d <sup>5</sup> 4D <sup>5</sup>	3/2	3d <sup>5</sup> 4F <sup>3</sup>	5/2	14.815	14.794				
3d <sup>5</sup> 4D <sup>5</sup>	3/2	3d <sup>5</sup> 2D <sup>5</sup>	3/2	14.708	14.696				
3d <sup>5</sup> 4D <sup>5</sup>	3/2	3d <sup>5</sup> 4P <sup>3</sup>	1/2	13.725	13.709				
3d <sup>5</sup> 4D <sup>5</sup>	3/2	3d <sup>5</sup> 2P <sup>3</sup>	3/2	10.807	10.802				
3d <sup>5</sup> 4D <sup>5</sup>	3/2	3d <sup>5</sup> 2D <sup>1</sup>	5/2	10.487	10.480				
3d <sup>5</sup> 4D <sup>5</sup>	3/2	3d <sup>5</sup> 4P <sup>3</sup>	5/2	9.248	9.230				
3d <sup>5</sup> 4D <sup>5</sup>	3/2	3d <sup>5</sup> 4D <sup>5</sup>	3/2	8.477	8.462				
3d <sup>5</sup> 4D <sup>5</sup>	3/2	3d <sup>5</sup> 2D <sup>3</sup>	5/2	7.910	7.899				
3d <sup>5</sup> 4D <sup>5</sup>	3/2	3d <sup>5</sup> 2P <sup>3</sup>	1/2	7.384	7.375				
3d <sup>5</sup> 4D <sup>5</sup>	3/2	3d <sup>5</sup> 2D <sup>1</sup>	3/2	6.741	6.733				
3d <sup>5</sup> 4D <sup>5</sup>	3/2	3d <sup>5</sup> 2D <sup>1</sup>	5/2	5.609	5.598				
3d <sup>5</sup> 2G <sup>5</sup>	9/2	3d <sup>5</sup> 2F <sup>5</sup>	7/2	149.683	150.005				
3d <sup>5</sup> 2G <sup>5</sup>	9/2	3d <sup>5</sup> 4D <sup>5</sup>	7/2	21.012	20.964				
3d <sup>5</sup> 2G <sup>5</sup>	9/2	3d <sup>5</sup> 4G <sup>5</sup>	11/2	20.839	20.795				
3d <sup>5</sup> 2G <sup>5</sup>	9/2	3d <sup>5</sup> 4G <sup>5</sup>	9/2	20.159	20.117				
3d <sup>5</sup> 2G <sup>5</sup>	9/2	3d <sup>5</sup> 2H <sup>3</sup>	9/2	16.767	16.734				
3d <sup>5</sup> 2G <sup>5</sup>	9/2	3d <sup>5</sup> 2G <sup>5</sup>	7/2	16.209	16.186				
3d <sup>5</sup> 2G <sup>5</sup>	9/2	3d <sup>5</sup> 2G <sup>3</sup>	7/2	14.558	14.535				
3d <sup>5</sup> 2G <sup>5</sup>	9/2	3d <sup>5</sup> 2G <sup>3</sup>	9/2	13.180	13.165				
3d <sup>5</sup> 2G <sup>5</sup>	9/2	3d <sup>5</sup> 4F <sup>3</sup>	7/2	8.987	8.969				
3d <sup>5</sup> 2G <sup>5</sup>	9/2	3d <sup>5</sup> 2H <sup>3</sup>	11/2	8.885	8.867				
3d <sup>5</sup> 2G <sup>5</sup>	9/2	3d <sup>5</sup> 2G <sup>5</sup>	9/2	8.437	8.422				
3d <sup>5</sup> 2G <sup>5</sup>	9/2	3d <sup>5</sup> 2G <sup>3</sup>	7/2	7.995	7.982				
3d <sup>5</sup> 4D <sup>5</sup>	5/2	3d <sup>5</sup> 2F <sup>5</sup>	7/2	270.094	271.516				
3d <sup>5</sup> 4D <sup>5</sup>	5/2	3d <sup>5</sup> 2D <sup>1</sup>	3/2	57.709	57.636				
3d <sup>5</sup> 4D <sup>5</sup>	5/2	3d <sup>5</sup> 6S <sup>5</sup>	5/2	26.647	26.559				
3d <sup>5</sup> 4D <sup>5</sup>	5/2	3d <sup>5</sup> 4D <sup>5</sup>	7/2	22.415	22.363				
3d <sup>5</sup> 4D <sup>5</sup>	5/2	3d <sup>5</sup> 4P <sup>3</sup>	3/2	19.454	19.404				
3d <sup>5</sup> 4D <sup>5</sup>	5/2	3d <sup>5</sup> 2F <sup>5</sup>	5/2	19.077	19.042				

Table 5. Cont.

Label and J for Lower		Label and J for Upper		Present Work		Expt (Ref. [2])	GRASP	RMBPT <sub>g</sub>	RCI <sub>g</sub>
				n = 5	n = 6				
3d <sup>5</sup> 4D <sup>5</sup>	5/2	3d <sup>5</sup> 2G <sup>5</sup>	7/2	17.031	17.007				
3d <sup>5</sup> 4D <sup>5</sup>	5/2	3d <sup>5</sup> 4F <sup>3</sup>	5/2	16.560	16.529				
3d <sup>5</sup> 4D <sup>5</sup>	5/2	3d <sup>5</sup> 2D <sup>5</sup>	3/2	16.426	16.407				
3d <sup>5</sup> 4D <sup>5</sup>	5/2	3d <sup>5</sup> 2G <sup>3</sup>	7/2	15.218	15.194				
3d <sup>5</sup> 4D <sup>5</sup>	5/2	3d <sup>5</sup> 2P <sup>3</sup>	3/2	11.706	11.699				
3d <sup>5</sup> 4D <sup>5</sup>	5/2	3d <sup>5</sup> 2D <sup>1</sup>	5/2	11.332	11.322				
3d <sup>5</sup> 4D <sup>5</sup>	5/2	3d <sup>5</sup> 4P <sup>3</sup>	5/2	9.899	9.876				
3d <sup>5</sup> 4D <sup>5</sup>	5/2	3d <sup>5</sup> 4F <sup>3</sup>	7/2	9.234	9.215				
3d <sup>5</sup> 4D <sup>5</sup>	5/2	3d <sup>5</sup> 4D <sup>5</sup>	3/2	9.021	9.002				
3d <sup>5</sup> 4D <sup>5</sup>	5/2	3d <sup>5</sup> 2D <sup>3</sup>	5/2	8.381	8.368				
3d <sup>5</sup> 4D <sup>5</sup>	5/2	3d <sup>5</sup> 2G <sup>3</sup>	7/2	8.190	8.177				
3d <sup>5</sup> 4D <sup>5</sup>	5/2	3d <sup>5</sup> 2D <sup>1</sup>	3/2	7.080	7.070				
3d <sup>5</sup> 4D <sup>5</sup>	5/2	3d <sup>5</sup> 2D <sup>1</sup>	5/2	5.842	5.830				
3d <sup>5</sup> 4P <sup>3</sup>	1/2	3d <sup>5</sup> 2D <sup>1</sup>	3/2	69.257	69.169				
3d <sup>5</sup> 4P <sup>3</sup>	1/2	3d <sup>5</sup> 4D <sup>5</sup>	1/2	21.006	20.963				
3d <sup>5</sup> 4P <sup>3</sup>	1/2	3d <sup>5</sup> 4P <sup>3</sup>	3/2	20.613	20.559				
3d <sup>5</sup> 4P <sup>3</sup>	1/2	3d <sup>5</sup> 2D <sup>5</sup>	3/2	17.245	17.225				
3d <sup>5</sup> 4P <sup>3</sup>	1/2	3d <sup>5</sup> 4P <sup>3</sup>	1/2	15.909	15.884				
3d <sup>5</sup> 4P <sup>3</sup>	1/2	3d <sup>5</sup> 2P <sup>3</sup>	3/2	12.116	12.109				
3d <sup>5</sup> 4P <sup>3</sup>	1/2	3d <sup>5</sup> 4D <sup>5</sup>	3/2	9.262	9.243				
3d <sup>5</sup> 4P <sup>3</sup>	1/2	3d <sup>5</sup> 2P <sup>3</sup>	1/2	7.973	7.962				
3d <sup>5</sup> 4P <sup>3</sup>	1/2	3d <sup>5</sup> 2D <sup>1</sup>	3/2	7.228	7.218				
3d <sup>5</sup> 2F <sup>5</sup>	7/2	3d <sup>5</sup> 6G <sup>5</sup>	5/2	29.564	29.438				
3d <sup>5</sup> 2F <sup>5</sup>	7/2	3d <sup>5</sup> 4D <sup>5</sup>	7/2	24.443	24.370				
3d <sup>5</sup> 2F <sup>5</sup>	7/2	3d <sup>5</sup> 4G <sup>5</sup>	9/2	23.296	23.233				
3d <sup>5</sup> 2F <sup>5</sup>	7/2	3d <sup>5</sup> 2F <sup>5</sup>	5/2	20.527	20.478				
3d <sup>5</sup> 2F <sup>5</sup>	7/2	3d <sup>5</sup> 2H <sup>3</sup>	9/2	18.882	18.835				
3d <sup>5</sup> 2F <sup>5</sup>	7/2	3d <sup>5</sup> 2G <sup>5</sup>	7/2	18.177	18.143				
3d <sup>5</sup> 2F <sup>5</sup>	7/2	3d <sup>5</sup> 4F <sup>3</sup>	5/2	17.641	17.600				
3d <sup>5</sup> 2F <sup>5</sup>	7/2	3d <sup>5</sup> 2G <sup>3</sup>	7/2	16.127	16.094				
3d <sup>5</sup> 2F <sup>5</sup>	7/2	3d <sup>5</sup> 2G <sup>3</sup>	9/2	14.452	14.432				
3d <sup>5</sup> 2F <sup>5</sup>	7/2	3d <sup>5</sup> 2D <sup>1</sup>	5/2	11.828	11.814				
3d <sup>5</sup> 2F <sup>5</sup>	7/2	3d <sup>5</sup> 4P <sup>3</sup>	5/2	10.275	10.249				
3d <sup>5</sup> 2F <sup>5</sup>	7/2	3d <sup>5</sup> 4F <sup>3</sup>	7/2	9.561	9.539				
3d <sup>5</sup> 2F <sup>5</sup>	7/2	3d <sup>5</sup> 2G <sup>5</sup>	9/2	8.941	8.923				
3d <sup>5</sup> 2F <sup>5</sup>	7/2	3d <sup>5</sup> 2D <sup>3</sup>	5/2	8.650	8.634				
3d <sup>5</sup> 2F <sup>5</sup>	7/2	3d <sup>5</sup> 2G <sup>3</sup>	7/2	8.446	8.431				
3d <sup>5</sup> 2F <sup>5</sup>	7/2	3d <sup>5</sup> 2D <sup>1</sup>	5/2	5.971	5.958				
3d <sup>5</sup> 2D <sup>1</sup>	3/2	3d <sup>5</sup> 6G <sup>5</sup>	5/2	49.507	49.256				
3d <sup>5</sup> 2D <sup>1</sup>	3/2	3d <sup>5</sup> 4D <sup>5</sup>	1/2	30.151	30.080				
3d <sup>5</sup> 2D <sup>1</sup>	3/2	3d <sup>5</sup> 4P <sup>3</sup>	3/2	29.348	29.253				
3d <sup>5</sup> 2D <sup>1</sup>	3/2	3d <sup>5</sup> 2F <sup>5</sup>	5/2	28.498	28.437				
3d <sup>5</sup> 2D <sup>1</sup>	3/2	3d <sup>5</sup> 4F <sup>3</sup>	5/2	23.224	23.175				
3d <sup>5</sup> 2D <sup>1</sup>	3/2	3d <sup>5</sup> 2D <sup>5</sup>	3/2	22.962	22.936				
3d <sup>5</sup> 2D <sup>1</sup>	3/2	3d <sup>5</sup> 4P <sup>3</sup>	1/2	20.653	20.619				
3d <sup>5</sup> 2D <sup>1</sup>	3/2	3d <sup>5</sup> 2P <sup>3</sup>	3/2	14.685	14.678				
3d <sup>5</sup> 2D <sup>1</sup>	3/2	3d <sup>5</sup> 2D <sup>1</sup>	5/2	14.101	14.089				
3d <sup>5</sup> 2D <sup>1</sup>	3/2	3d <sup>5</sup> 4P <sup>3</sup>	5/2	11.948	11.919				
3d <sup>5</sup> 2D <sup>1</sup>	3/2	3d <sup>5</sup> 4D <sup>5</sup>	3/2	10.692	10.668				

Table 5. Cont.

Label and J for Lower		Label and J for Upper		Present Work		Expt (Ref. [2])	GRASP	RMBPT <sub>g</sub>	RCI <sub>g</sub>
				n = 5	n = 6				
3d <sup>5</sup> 2D <sup>1</sup>	3/2	3d <sup>5</sup> 2D <sup>3</sup>	5/2	9.806	9.789				
3d <sup>5</sup> 2D <sup>1</sup>	3/2	3d <sup>5</sup> 2P <sup>3</sup>	1/2	9.010	8.997				
3d <sup>5</sup> 2D <sup>1</sup>	3/2	3d <sup>5</sup> 2D <sup>1</sup>	3/2	8.071	8.059				
3d <sup>5</sup> 2D <sup>1</sup>	3/2	3d <sup>5</sup> 2D <sup>1</sup>	5/2	6.500	6.486				
3d <sup>5</sup> 6S <sup>5</sup>	5/2	3d <sup>5</sup> 4D <sup>5</sup>	7/2	141.121	141.559				
3d <sup>5</sup> 6S <sup>5</sup>	5/2	3d <sup>5</sup> 4P <sup>3</sup>	3/2	72.074	72.035				
3d <sup>5</sup> 6S <sup>5</sup>	5/2	3d <sup>5</sup> 2F <sup>5</sup>	5/2	67.156	67.278				
3d <sup>5</sup> 6S <sup>5</sup>	5/2	3d <sup>5</sup> 2G <sup>5</sup>	7/2	47.192	47.288				
3d <sup>5</sup> 6S <sup>5</sup>	5/2	3d <sup>5</sup> 4F <sup>3</sup>	5/2	43.743	43.766				
3d <sup>5</sup> 6S <sup>5</sup>	5/2	3d <sup>5</sup> 2D <sup>5</sup>	3/2	42.824	42.924				
3d <sup>5</sup> 6S <sup>5</sup>	5/2	3d <sup>5</sup> 2G <sup>3</sup>	7/2	35.481	35.505				
3d <sup>5</sup> 6S <sup>5</sup>	5/2	3d <sup>5</sup> 2P <sup>3</sup>	3/2	20.879	20.910				
3d <sup>5</sup> 6S <sup>5</sup>	5/2	3d <sup>5</sup> 2D <sup>1</sup>	5/2	19.717	19.734				
3d <sup>5</sup> 6S <sup>5</sup>	5/2	3d <sup>5</sup> 4P <sup>3</sup>	5/2	15.749	15.723				
3d <sup>5</sup> 6S <sup>5</sup>	5/2	3d <sup>5</sup> 4F <sup>3</sup>	7/2	14.130	14.111				
3d <sup>5</sup> 6S <sup>5</sup>	5/2	3d <sup>5</sup> 4D <sup>5</sup>	3/2	13.638	13.618				
3d <sup>5</sup> 6S <sup>5</sup>	5/2	3d <sup>5</sup> 2D <sup>3</sup>	5/2	12.227	12.217				
3d <sup>5</sup> 6S <sup>5</sup>	5/2	3d <sup>5</sup> 2G <sup>3</sup>	7/2	11.824	11.815				
3d <sup>5</sup> 6S <sup>5</sup>	5/2	3d <sup>5</sup> 2D <sup>1</sup>	3/2	9.643	9.636				
3d <sup>5</sup> 6S <sup>5</sup>	5/2	3d <sup>5</sup> 2D <sup>1</sup>	5/2	7.482	7.470				
3d <sup>5</sup> 4D <sup>5</sup>	7/2	3d <sup>5</sup> 4G <sup>5</sup>	9/2	496.548	497.861				
3d <sup>5</sup> 4D <sup>5</sup>	7/2	3d <sup>5</sup> 2F <sup>5</sup>	5/2	128.131	128.214				
3d <sup>5</sup> 4D <sup>5</sup>	7/2	3d <sup>5</sup> 2H <sup>3</sup>	9/2	82.993	82.924				
3d <sup>5</sup> 4D <sup>5</sup>	7/2	3d <sup>5</sup> 2G <sup>5</sup>	7/2	70.903	71.009				
3d <sup>5</sup> 4D <sup>5</sup>	7/2	3d <sup>5</sup> 4F <sup>3</sup>	5/2	63.393	63.353				
3d <sup>5</sup> 4D <sup>5</sup>	7/2	3d <sup>5</sup> 2G <sup>3</sup>	7/2	47.397	47.392				
3d <sup>5</sup> 4D <sup>5</sup>	7/2	3d <sup>5</sup> 2G <sup>3</sup>	9/2	35.359	35.390				
3d <sup>5</sup> 4D <sup>5</sup>	7/2	3d <sup>5</sup> 2D <sup>1</sup>	5/2	22.919	22.931				
3d <sup>5</sup> 4D <sup>5</sup>	7/2	3d <sup>5</sup> 4P <sup>3</sup>	5/2	17.728	17.688				
3d <sup>5</sup> 4D <sup>5</sup>	7/2	3d <sup>5</sup> 4F <sup>3</sup>	7/2	15.703	15.674				
3d <sup>5</sup> 4D <sup>5</sup>	7/2	3d <sup>5</sup> 2G <sup>5</sup>	9/2	14.097	14.078				
3d <sup>5</sup> 4D <sup>5</sup>	7/2	3d <sup>5</sup> 2D <sup>3</sup>	5/2	13.387	13.371				
3d <sup>5</sup> 4D <sup>5</sup>	7/2	3d <sup>5</sup> 2G <sup>3</sup>	7/2	12.906	12.891				
3d <sup>5</sup> 4D <sup>5</sup>	7/2	3d <sup>5</sup> 2D <sup>1</sup>	5/2	7.901	7.886				
3d <sup>5</sup> 4G <sup>5</sup>	11/2	3d <sup>5</sup> 4G <sup>5</sup>	9/2	617.468	617.572				
3d <sup>5</sup> 4G <sup>5</sup>	11/2	3d <sup>5</sup> 2J <sup>5</sup>	13/2	241.792	242.297				
3d <sup>5</sup> 4G <sup>5</sup>	11/2	3d <sup>5</sup> 2H <sup>3</sup>	9/2	85.801	85.691				
3d <sup>5</sup> 4G <sup>5</sup>	11/2	3d <sup>5</sup> 2G <sup>3</sup>	9/2	35.859	35.885				
3d <sup>5</sup> 4G <sup>5</sup>	11/2	3d <sup>5</sup> 2H <sup>3</sup>	11/2	15.488	15.460				
3d <sup>5</sup> 4G <sup>5</sup>	11/2	3d <sup>5</sup> 2G <sup>5</sup>	9/2	14.176	14.155				
3d <sup>5</sup> 4G <sup>5</sup>	9/2	3d <sup>5</sup> 2H <sup>3</sup>	9/2	99.648	99.496				
3d <sup>5</sup> 4G <sup>5</sup>	9/2	3d <sup>5</sup> 2G <sup>5</sup>	7/2	82.713	82.822				
3d <sup>5</sup> 4G <sup>5</sup>	9/2	3d <sup>5</sup> 2G <sup>3</sup>	7/2	52.399	52.378				
3d <sup>5</sup> 4G <sup>5</sup>	9/2	3d <sup>5</sup> 2G <sup>3</sup>	9/2	38.069	38.098				
3d <sup>5</sup> 4G <sup>5</sup>	9/2	3d <sup>5</sup> 4F <sup>3</sup>	7/2	16.215	16.183				
3d <sup>5</sup> 4G <sup>5</sup>	9/2	3d <sup>5</sup> 2H <sup>3</sup>	11/2	15.887	15.857				
3d <sup>5</sup> 4G <sup>5</sup>	9/2	3d <sup>5</sup> 2G <sup>5</sup>	9/2	14.509	14.487				
3d <sup>5</sup> 4G <sup>5</sup>	9/2	3d <sup>5</sup> 2G <sup>3</sup>	7/2	13.250	13.233				
3d <sup>5</sup> 2J <sup>5</sup>	13/2	3d <sup>5</sup> 2H <sup>3</sup>	11/2	16.548	16.513				

Table 5. Cont.

Label and J for Lower		Label and J for Upper		Present Work		Expt (Ref. [2])	GRASP	RMBPT <sub>g</sub>	RCI <sub>g</sub>
				n = 5	n = 6				
3d <sup>5</sup> 4D <sup>5</sup>	1/2	3d <sup>5</sup> 4P <sup>3</sup>	3/2	1102.758	1064.996				
3d <sup>5</sup> 4D <sup>5</sup>	1/2	3d <sup>5</sup> 2D <sup>5</sup>	3/2	96.307	96.583				
3d <sup>5</sup> 4D <sup>5</sup>	1/2	3d <sup>5</sup> 4P <sup>3</sup>	1/2	65.560	65.562				
3d <sup>5</sup> 4D <sup>5</sup>	1/2	3d <sup>5</sup> 2P <sup>3</sup>	3/2	28.630	28.668				
3d <sup>5</sup> 4D <sup>5</sup>	1/2	3d <sup>5</sup> 4D <sup>5</sup>	3/2	16.568	16.532				
3d <sup>5</sup> 4D <sup>5</sup>	1/2	3d <sup>5</sup> 2P <sup>3</sup>	1/2	12.849	12.837				
3d <sup>5</sup> 4D <sup>5</sup>	1/2	3d <sup>5</sup> 2D <sup>1</sup>	3/2	11.021	11.009				
3d <sup>5</sup> 4P <sup>3</sup>	3/2	3d <sup>5</sup> 2F <sup>5</sup>	5/2	984.197	1018.757				
3d <sup>5</sup> 4P <sup>3</sup>	3/2	3d <sup>5</sup> 4F <sup>3</sup>	5/2	111.284	111.525				
3d <sup>5</sup> 4P <sup>3</sup>	3/2	3d <sup>5</sup> 2D <sup>5</sup>	3/2	105.523	106.216				
3d <sup>5</sup> 4P <sup>3</sup>	3/2	3d <sup>5</sup> 4P <sup>3</sup>	1/2	69.704	69.863				
3d <sup>5</sup> 4P <sup>3</sup>	3/2	3d <sup>5</sup> 2P <sup>3</sup>	3/2	29.393	29.461				
3d <sup>5</sup> 4P <sup>3</sup>	3/2	3d <sup>5</sup> 2D <sup>1</sup>	5/2	27.141	27.180				
3d <sup>5</sup> 4P <sup>3</sup>	3/2	3d <sup>5</sup> 4P <sup>3</sup>	5/2	20.153	20.113				
3d <sup>5</sup> 4P <sup>3</sup>	3/2	3d <sup>5</sup> 4D <sup>5</sup>	3/2	16.820	16.793				
3d <sup>5</sup> 4P <sup>3</sup>	3/2	3d <sup>5</sup> 2D <sup>3</sup>	5/2	14.726	14.712				
3d <sup>5</sup> 4P <sup>3</sup>	3/2	3d <sup>5</sup> 2P <sup>3</sup>	1/2	13.001	12.994				
3d <sup>5</sup> 4P <sup>3</sup>	3/2	3d <sup>5</sup> 2D <sup>1</sup>	3/2	11.132	11.124				
3d <sup>5</sup> 4P <sup>3</sup>	3/2	3d <sup>5</sup> 2D <sup>1</sup>	5/2	8.349	8.334				
3d <sup>5</sup> 2F <sup>5</sup>	5/2	3d <sup>5</sup> 2G <sup>5</sup>	7/2	158.747	159.155				
3d <sup>5</sup> 2F <sup>5</sup>	5/2	3d <sup>5</sup> 4F <sup>3</sup>	5/2	125.471	125.234				
3d <sup>5</sup> 2F <sup>5</sup>	5/2	3d <sup>5</sup> 2D <sup>5</sup>	3/2	118.195	118.578				
3d <sup>5</sup> 2F <sup>5</sup>	5/2	3d <sup>5</sup> 2G <sup>3</sup>	7/2	75.224	75.182				
3d <sup>5</sup> 2F <sup>5</sup>	5/2	3d <sup>5</sup> 2P <sup>3</sup>	3/2	30.298	30.339				
3d <sup>5</sup> 2F <sup>5</sup>	5/2	3d <sup>5</sup> 2D <sup>1</sup>	5/2	27.911	27.925				
3d <sup>5</sup> 2F <sup>5</sup>	5/2	3d <sup>5</sup> 4P <sup>3</sup>	5/2	20.575	20.518				
3d <sup>5</sup> 2F <sup>5</sup>	5/2	3d <sup>5</sup> 4F <sup>3</sup>	7/2	17.896	17.857				
3d <sup>5</sup> 2F <sup>5</sup>	5/2	3d <sup>5</sup> 4D <sup>5</sup>	3/2	17.113	17.074				
3d <sup>5</sup> 2F <sup>5</sup>	5/2	3d <sup>5</sup> 2D <sup>3</sup>	5/2	14.949	14.928				
3d <sup>5</sup> 2F <sup>5</sup>	5/2	3d <sup>5</sup> 2G <sup>3</sup>	7/2	14.351	14.331				
3d <sup>5</sup> 2F <sup>5</sup>	5/2	3d <sup>5</sup> 2D <sup>1</sup>	3/2	11.259	11.246				
3d <sup>5</sup> 2F <sup>5</sup>	5/2	3d <sup>5</sup> 2D <sup>1</sup>	5/2	8.420	8.403				
3d <sup>5</sup> 2H <sup>3</sup>	9/2	3d <sup>5</sup> 2G <sup>5</sup>	7/2	486.710	494.218				
3d <sup>5</sup> 2H <sup>3</sup>	9/2	3d <sup>5</sup> 2G <sup>3</sup>	7/2	110.511	110.603				
3d <sup>5</sup> 2H <sup>3</sup>	9/2	3d <sup>5</sup> 2G <sup>3</sup>	9/2	61.605	61.739				
3d <sup>5</sup> 2H <sup>3</sup>	9/2	3d <sup>5</sup> 4F <sup>3</sup>	7/2	19.367	19.327				
3d <sup>5</sup> 2H <sup>3</sup>	9/2	3d <sup>5</sup> 2H <sup>3</sup>	11/2	18.900	18.863				
3d <sup>5</sup> 2H <sup>3</sup>	9/2	3d <sup>5</sup> 2G <sup>5</sup>	9/2	16.982	16.957				
3d <sup>5</sup> 2H <sup>3</sup>	9/2	3d <sup>5</sup> 2G <sup>3</sup>	7/2	15.282	15.263				
3d <sup>5</sup> 2G <sup>5</sup>	7/2	3d <sup>5</sup> 4F <sup>3</sup>	5/2	598.575	587.600				
3d <sup>5</sup> 2G <sup>5</sup>	7/2	3d <sup>5</sup> 2G <sup>3</sup>	7/2	142.974	142.492				
3d <sup>5</sup> 2G <sup>5</sup>	7/2	3d <sup>5</sup> 2G <sup>3</sup>	9/2	70.533	70.553				
3d <sup>5</sup> 2G <sup>5</sup>	7/2	3d <sup>5</sup> 2D <sup>1</sup>	5/2	33.865	33.867				
3d <sup>5</sup> 2G <sup>5</sup>	7/2	3d <sup>5</sup> 4P <sup>3</sup>	5/2	23.638	23.555				
3d <sup>5</sup> 2G <sup>5</sup>	7/2	3d <sup>5</sup> 4F <sup>3</sup>	7/2	20.170	20.113				
3d <sup>5</sup> 2G <sup>5</sup>	7/2	3d <sup>5</sup> 2G <sup>5</sup>	9/2	17.595	17.559				
3d <sup>5</sup> 2G <sup>5</sup>	7/2	3d <sup>5</sup> 2D <sup>3</sup>	5/2	16.503	16.473				
3d <sup>5</sup> 2G <sup>5</sup>	7/2	3d <sup>5</sup> 2G <sup>3</sup>	7/2	15.777	15.750				
3d <sup>5</sup> 2G <sup>5</sup>	7/2	3d <sup>5</sup> 2D <sup>1</sup>	5/2	8.892	8.871				

Table 5. Cont.

Label and J for Lower		Label and J for Upper		Present Work		Expt (Ref. [2])	GRASP	RMBPT <sub>g</sub>	RCI <sub>g</sub>
				n = 5	n = 6				
3d <sup>5</sup> 4F <sup>3</sup>	5/2	3d <sup>5</sup> 2D <sup>5</sup>	3/2	2038.287	2231.127				
3d <sup>5</sup> 4F <sup>3</sup>	5/2	3d <sup>5</sup> 2G <sup>3</sup>	7/2	187.841	188.108				
3d <sup>5</sup> 4F <sup>3</sup>	5/2	3d <sup>5</sup> 2P <sup>3</sup>	3/2	39.944	40.038				
3d <sup>5</sup> 4F <sup>3</sup>	5/2	3d <sup>5</sup> 2D <sup>1</sup>	5/2	35.896	35.939				
3d <sup>5</sup> 4F <sup>3</sup>	5/2	3d <sup>5</sup> 4P <sup>3</sup>	5/2	24.610	24.539				
3d <sup>5</sup> 4F <sup>3</sup>	5/2	3d <sup>5</sup> 4F <sup>3</sup>	7/2	20.873	20.826				
3d <sup>5</sup> 4F <sup>3</sup>	5/2	3d <sup>5</sup> 4D <sup>5</sup>	3/2	19.815	19.769				
3d <sup>5</sup> 4F <sup>3</sup>	5/2	3d <sup>5</sup> 2D <sup>3</sup>	5/2	16.971	16.948				
3d <sup>5</sup> 4F <sup>3</sup>	5/2	3d <sup>5</sup> 2G <sup>3</sup>	7/2	16.205	16.183				
3d <sup>5</sup> 4F <sup>3</sup>	5/2	3d <sup>5</sup> 2D <sup>1</sup>	3/2	12.369	12.356				
3d <sup>5</sup> 4F <sup>3</sup>	5/2	3d <sup>5</sup> 2D <sup>1</sup>	5/2	9.026	9.007				
3d <sup>5</sup> 2D <sup>5</sup>	3/2	3d <sup>5</sup> 4P <sup>3</sup>	1/2	205.353	204.123				
3d <sup>5</sup> 2D <sup>5</sup>	3/2	3d <sup>5</sup> 2P <sup>3</sup>	3/2	40.742	40.770				
3d <sup>5</sup> 2D <sup>5</sup>	3/2	3d <sup>5</sup> 2D <sup>1</sup>	5/2	36.540	36.527				
3d <sup>5</sup> 2D <sup>5</sup>	3/2	3d <sup>5</sup> 4P <sup>3</sup>	5/2	24.911	24.812				
3d <sup>5</sup> 2D <sup>5</sup>	3/2	3d <sup>5</sup> 4D <sup>5</sup>	3/2	20.010	19.946				
3d <sup>5</sup> 2D <sup>5</sup>	3/2	3d <sup>5</sup> 2D <sup>3</sup>	5/2	17.114	17.078				
3d <sup>5</sup> 2D <sup>5</sup>	3/2	3d <sup>5</sup> 2P <sup>3</sup>	1/2	14.828	14.805				
3d <sup>5</sup> 2D <sup>5</sup>	3/2	3d <sup>5</sup> 2D <sup>1</sup>	3/2	12.445	12.425				
3d <sup>5</sup> 2D <sup>5</sup>	3/2	3d <sup>5</sup> 2D <sup>1</sup>	5/2	9.066	9.044				
3d <sup>5</sup> 2G <sup>3</sup>	7/2	3d <sup>5</sup> 2G <sup>3</sup>	9/2	139.208	139.747				
3d <sup>5</sup> 2G <sup>3</sup>	7/2	3d <sup>5</sup> 2D <sup>1</sup>	5/2	44.377	44.427				
3d <sup>5</sup> 2G <sup>3</sup>	7/2	3d <sup>5</sup> 4P <sup>3</sup>	5/2	28.321	28.220				
3d <sup>5</sup> 2G <sup>3</sup>	7/2	3d <sup>5</sup> 4F <sup>3</sup>	7/2	23.482	23.419				
3d <sup>5</sup> 2G <sup>3</sup>	7/2	3d <sup>5</sup> 2G <sup>5</sup>	9/2	20.065	20.027				
3d <sup>5</sup> 2G <sup>3</sup>	7/2	3d <sup>5</sup> 2D <sup>3</sup>	5/2	18.657	18.626				
3d <sup>5</sup> 2G <sup>3</sup>	7/2	3d <sup>5</sup> 2G <sup>3</sup>	7/2	17.735	17.707				
3d <sup>5</sup> 2G <sup>3</sup>	7/2	3d <sup>5</sup> 2D <sup>1</sup>	5/2	9.482	9.460				
3d <sup>5</sup> 4P <sup>3</sup>	1/2	3d <sup>5</sup> 2P <sup>3</sup>	3/2	50.826	50.945				
3d <sup>5</sup> 4P <sup>3</sup>	1/2	3d <sup>5</sup> 4D <sup>5</sup>	3/2	22.170	22.106				
3d <sup>5</sup> 4P <sup>3</sup>	1/2	3d <sup>5</sup> 2P <sup>3</sup>	1/2	15.982	15.963				
3d <sup>5</sup> 4P <sup>3</sup>	1/2	3d <sup>5</sup> 2D <sup>1</sup>	3/2	13.248	13.230				
3d <sup>5</sup> 2G <sup>3</sup>	9/2	3d <sup>5</sup> 4F <sup>3</sup>	7/2	28.247	28.134				
3d <sup>5</sup> 2G <sup>3</sup>	9/2	3d <sup>5</sup> 2H <sup>3</sup>	11/2	27.264	27.162				
3d <sup>5</sup> 2G <sup>3</sup>	9/2	3d <sup>5</sup> 2G <sup>5</sup>	9/2	23.444	23.377				
3d <sup>5</sup> 2G <sup>3</sup>	9/2	3d <sup>5</sup> 2G <sup>3</sup>	7/2	20.324	20.276				
3d <sup>5</sup> 2P <sup>3</sup>	3/2	3d <sup>5</sup> 2D <sup>1</sup>	5/2	354.267	351.029				
3d <sup>5</sup> 2P <sup>3</sup>	3/2	3d <sup>5</sup> 4P <sup>3</sup>	5/2	64.110	63.389				
3d <sup>5</sup> 2P <sup>3</sup>	3/2	3d <sup>5</sup> 4D <sup>5</sup>	3/2	39.323	39.051				
3d <sup>5</sup> 2P <sup>3</sup>	3/2	3d <sup>5</sup> 2D <sup>3</sup>	5/2	29.510	29.388				
3d <sup>5</sup> 2P <sup>3</sup>	3/2	3d <sup>5</sup> 2P <sup>3</sup>	1/2	23.312	23.247				
3d <sup>5</sup> 2P <sup>3</sup>	3/2	3d <sup>5</sup> 2D <sup>1</sup>	3/2	17.918	17.871				
3d <sup>5</sup> 2P <sup>3</sup>	3/2	3d <sup>5</sup> 2D <sup>1</sup>	5/2	11.661	11.621				
3d <sup>5</sup> 2D <sup>1</sup>	5/2	3d <sup>5</sup> 4P <sup>3</sup>	5/2	78.275	77.359				
3d <sup>5</sup> 2D <sup>1</sup>	5/2	3d <sup>5</sup> 4F <sup>3</sup>	7/2	49.873	49.527				
3d <sup>5</sup> 2D <sup>1</sup>	5/2	3d <sup>5</sup> 4D <sup>5</sup>	3/2	44.232	43.939				
3d <sup>5</sup> 2D <sup>1</sup>	5/2	3d <sup>5</sup> 2D <sup>3</sup>	5/2	32.191	32.073				
3d <sup>5</sup> 2D <sup>1</sup>	5/2	3d <sup>5</sup> 2G <sup>3</sup>	7/2	29.540	29.440				
3d <sup>5</sup> 2D <sup>1</sup>	5/2	3d <sup>5</sup> 2D <sup>1</sup>	3/2	18.873	18.830				

Table 5. Cont.

Label and J for Lower		Label and J for Upper		Present Work		Expt (Ref. [2])	GRASP	RMBPT <sub>g</sub>	RCI <sub>g</sub>
				n = 5	n = 6				
3d <sup>5</sup> 2D <sup>1</sup>	5/2	3d <sup>5</sup> 2D <sup>1</sup>	5/2	12.058	12.019				
3d <sup>5</sup> 4P <sup>3</sup>	5/2	3d <sup>5</sup> 4F <sup>3</sup>	7/2	137.450	137.658				
3d <sup>5</sup> 4P <sup>3</sup>	5/2	3d <sup>5</sup> 4D <sup>5</sup>	3/2	101.706	101.709				
3d <sup>5</sup> 4P <sup>3</sup>	5/2	3d <sup>5</sup> 2D <sup>3</sup>	5/2	54.677	54.789				
3d <sup>5</sup> 4P <sup>3</sup>	5/2	3d <sup>5</sup> 2G <sup>3</sup>	7/2	47.445	47.528				
3d <sup>5</sup> 4P <sup>3</sup>	5/2	3d <sup>5</sup> 2D <sup>1</sup>	3/2	24.869	24.888				
3d <sup>5</sup> 4P <sup>3</sup>	5/2	3d <sup>5</sup> 2D <sup>1</sup>	5/2	14.254	14.230				
3d <sup>5</sup> 4F <sup>3</sup>	7/2	3d <sup>5</sup> 2G <sup>5</sup>	9/2	137.868	138.255				
3d <sup>5</sup> 4F <sup>3</sup>	7/2	3d <sup>5</sup> 2D <sup>3</sup>	5/2	90.796	91.013				
3d <sup>5</sup> 4F <sup>3</sup>	7/2	3d <sup>5</sup> 2G <sup>3</sup>	7/2	72.454	72.591				
3d <sup>5</sup> 4F <sup>3</sup>	7/2	3d <sup>5</sup> 2D <sup>1</sup>	5/2	15.903	15.871				
3d <sup>5</sup> 2H <sup>3</sup>	11/2	3d <sup>5</sup> 2G <sup>5</sup>	9/2	167.319	167.768				
3d <sup>5</sup> 4D <sup>5</sup>	3/2	3d <sup>5</sup> 2D <sup>3</sup>	5/2	118.248	118.767				
3d <sup>5</sup> 4D <sup>5</sup>	3/2	3d <sup>5</sup> 2P <sup>3</sup>	1/2	57.255	57.442				
3d <sup>5</sup> 4D <sup>5</sup>	3/2	3d <sup>5</sup> 2D <sup>1</sup>	3/2	32.917	32.951				
3d <sup>5</sup> 4D <sup>5</sup>	3/2	3d <sup>5</sup> 2D <sup>1</sup>	5/2	16.577	16.545				
3d <sup>5</sup> 2G <sup>5</sup>	9/2	3d <sup>5</sup> 2G <sup>3</sup>	7/2	152.705	152.840				
3d <sup>5</sup> 2D <sup>3</sup>	5/2	3d <sup>5</sup> 2G <sup>3</sup>	7/2	358.662	358.634				
3d <sup>5</sup> 2D <sup>3</sup>	5/2	3d <sup>5</sup> 2D <sup>1</sup>	3/2	45.616	45.602				
3d <sup>5</sup> 2D <sup>3</sup>	5/2	3d <sup>5</sup> 2D <sup>1</sup>	5/2	19.280	19.223				
3d <sup>5</sup> 2G <sup>3</sup>	7/2	3d <sup>5</sup> 2D <sup>1</sup>	5/2	20.376	20.312				
3d <sup>5</sup> 2P <sup>3</sup>	1/2	3d <sup>5</sup> 2D <sup>1</sup>	3/2	77.440	77.283				
3d <sup>5</sup> 2D <sup>1</sup>	3/2	3d <sup>5</sup> 2D <sup>1</sup>	5/2	33.396	33.231				
W <sup>50+</sup> (Cr-like)									
3d <sup>6</sup> 5D <sup>4</sup>	4	3d <sup>6</sup> 5D <sup>4</sup>	3	19.752	19.720	19.684(3)	19.796	19.693	19.835
3d <sup>6</sup> 5D <sup>4</sup>	4	3d <sup>6</sup> 5D <sup>4</sup>	4	19.291	19.267	19.239(3)	19.303	19.237	19.425
3d <sup>6</sup> 5D <sup>4</sup>	4	3d <sup>6</sup> 3G <sup>4</sup>	5	17.162	17.150	17.133(3)	17.118	17.131	17.259
3d <sup>6</sup> 5D <sup>4</sup>	4	3d <sup>6</sup> 3D <sup>4</sup>	3	15.390	15.378	15.363(3)	15.370	15.289	15.316
3d <sup>6</sup> 5D <sup>4</sup>	4	3d <sup>6</sup> 1G <sup>2</sup>	4	13.147	13.139	13.137(3)	13.114	13.153	13.050
3d <sup>6</sup> 5D <sup>4</sup>	4	3d <sup>6</sup> 3F <sup>2</sup>	3	12.785	12.779	12.779(3)	12.739	12.800	12.642
3d <sup>6</sup> 5D <sup>4</sup>	4	3d <sup>6</sup> 3H <sup>4</sup>	4	9.024	9.013				
3d <sup>6</sup> 5D <sup>4</sup>	4	3d <sup>6</sup> 5D <sup>4</sup>	3	8.809	8.798				
3d <sup>6</sup> 5D <sup>4</sup>	4	3d <sup>6</sup> 3H <sup>4</sup>	5	8.756	8.746				
3d <sup>6</sup> 5D <sup>4</sup>	4	3d <sup>6</sup> 3F <sup>4</sup>	3	8.356	8.347				
3d <sup>6</sup> 5D <sup>4</sup>	4	3d <sup>6</sup> 1G <sup>4</sup>	4	8.111	8.104				
3d <sup>6</sup> 5D <sup>4</sup>	4	3d <sup>6</sup> 3F <sup>2</sup>	4	7.274	7.269				
3d <sup>6</sup> 5D <sup>4</sup>	4	3d <sup>6</sup> 1G <sup>2</sup>	4	5.668	5.661				
3d <sup>6</sup> 5D <sup>4</sup>	4	3d <sup>6</sup> 3F <sup>2</sup>	3	5.461	5.455				
3d <sup>6</sup> 3D <sup>4</sup>	2	3d <sup>6</sup> 5D <sup>4</sup>	3	22.546	22.503				
3d <sup>6</sup> 3D <sup>4</sup>	2	3d <sup>6</sup> 5D <sup>4</sup>	1	20.709	20.668				
3d <sup>6</sup> 3D <sup>4</sup>	2	3d <sup>6</sup> 3F <sup>4</sup>	2	17.384	17.367				
3d <sup>6</sup> 3D <sup>4</sup>	2	3d <sup>6</sup> 3D <sup>4</sup>	3	17.035	17.019				
3d <sup>6</sup> 3D <sup>4</sup>	2	3d <sup>6</sup> 3D <sup>4</sup>	2	14.214	14.202	14.193(3)	14.184	14.202	14.170
3d <sup>6</sup> 3D <sup>4</sup>	2	3d <sup>6</sup> 3P <sup>2</sup>	1	14.198	14.188				
3d <sup>6</sup> 3D <sup>4</sup>	2	3d <sup>6</sup> 3F <sup>2</sup>	3	13.900	13.892	13.886(3)	13.843	13.895	13.848
3d <sup>6</sup> 3D <sup>4</sup>	2	3d <sup>6</sup> 5D <sup>4</sup>	2	10.042	10.025				
3d <sup>6</sup> 3D <sup>4</sup>	2	3d <sup>6</sup> 5D <sup>4</sup>	3	9.324	9.312				
3d <sup>6</sup> 3D <sup>4</sup>	2	3d <sup>6</sup> 3F <sup>4</sup>	3	8.818	8.808				



Table 5. Cont.

Label and J for Lower		Label and J for Upper		Present Work		Expt (Ref. [2])	GRASP	RMBPT <sub>g</sub>	RCI <sub>g</sub>
				n = 5	n = 6				
3d <sup>6</sup> 3D <sup>4</sup>	2	3d <sup>6</sup> 3D <sup>4</sup>	1	8.662	8.652				
3d <sup>6</sup> 3D <sup>4</sup>	2	3d <sup>6</sup> 3F <sup>4</sup>	2	8.468	8.460				
3d <sup>6</sup> 3D <sup>4</sup>	2	3d <sup>6</sup> 3F <sup>2</sup>	2	7.848	7.839				
3d <sup>6</sup> 3D <sup>4</sup>	2	3d <sup>6</sup> 1D <sup>2</sup>	2	6.867	6.863				
3d <sup>6</sup> 3D <sup>4</sup>	2	3d <sup>6</sup> 3P <sup>2</sup>	1	6.248	6.238				
3d <sup>6</sup> 3D <sup>4</sup>	2	3d <sup>6</sup> 3P <sup>2</sup>	2	5.711	5.704				
3d <sup>6</sup> 3D <sup>4</sup>	2	3d <sup>6</sup> 3F <sup>2</sup>	3	5.655	5.648				
3d <sup>6</sup> 3P <sup>2</sup>	0	3d <sup>6</sup> 5D <sup>4</sup>	1	29.559	29.509				
3d <sup>6</sup> 3P <sup>2</sup>	0	3d <sup>6</sup> 3P <sup>2</sup>	1	17.865	17.861	17.826(3)	17.750	17.837	17.921
3d <sup>6</sup> 3P <sup>2</sup>	0	3d <sup>6</sup> 3D <sup>4</sup>	1	9.901	9.893				
3d <sup>6</sup> 3P <sup>2</sup>	0	3d <sup>6</sup> 3P <sup>2</sup>	1	6.868	6.858				
3d <sup>6</sup> 5D <sup>4</sup>	3	3d <sup>6</sup> 5D <sup>4</sup>	4	827.797	838.107				
3d <sup>6</sup> 5D <sup>4</sup>	3	3d <sup>6</sup> 3F <sup>4</sup>	2	75.926	76.090				
3d <sup>6</sup> 5D <sup>4</sup>	3	3d <sup>6</sup> 3D <sup>4</sup>	3	69.700	69.830				
3d <sup>6</sup> 5D <sup>4</sup>	3	3d <sup>6</sup> 1G <sup>2</sup>	4	39.314	39.365				
3d <sup>6</sup> 5D <sup>4</sup>	3	3d <sup>6</sup> 3D <sup>4</sup>	2	38.467	38.499				
3d <sup>6</sup> 5D <sup>4</sup>	3	3d <sup>6</sup> 3F <sup>2</sup>	3	36.246	36.304				
3d <sup>6</sup> 5D <sup>4</sup>	3	3d <sup>6</sup> 5D <sup>4</sup>	2	18.107	18.080				
3d <sup>6</sup> 5D <sup>4</sup>	3	3d <sup>6</sup> 3H <sup>4</sup>	4	16.615	16.599				
3d <sup>6</sup> 5D <sup>4</sup>	3	3d <sup>6</sup> 5D <sup>4</sup>	3	15.900	15.886				
3d <sup>6</sup> 5D <sup>4</sup>	3	3d <sup>6</sup> 3F <sup>4</sup>	3	14.482	14.472				
3d <sup>6</sup> 5D <sup>4</sup>	3	3d <sup>6</sup> 1G <sup>4</sup>	4	13.764	13.758				
3d <sup>6</sup> 5D <sup>4</sup>	3	3d <sup>6</sup> 3F <sup>4</sup>	2	13.562	13.556				
3d <sup>6</sup> 5D <sup>4</sup>	3	3d <sup>6</sup> 3F <sup>2</sup>	2	12.038	12.029				
3d <sup>6</sup> 5D <sup>4</sup>	3	3d <sup>6</sup> 3F <sup>2</sup>	4	11.514	11.512				
3d <sup>6</sup> 5D <sup>4</sup>	3	3d <sup>6</sup> 1D <sup>2</sup>	2	9.875	9.874				
3d <sup>6</sup> 5D <sup>4</sup>	3	3d <sup>6</sup> 1G <sup>2</sup>	4	7.949	7.940				
3d <sup>6</sup> 5D <sup>4</sup>	3	3d <sup>6</sup> 3P <sup>2</sup>	2	7.648	7.641				
3d <sup>6</sup> 5D <sup>4</sup>	3	3d <sup>6</sup> 3F <sup>2</sup>	3	7.547	7.540				
3d <sup>6</sup> 5D <sup>4</sup>	4	3d <sup>6</sup> 3G <sup>4</sup>	5	155.438	156.080				
3d <sup>6</sup> 5D <sup>4</sup>	4	3d <sup>6</sup> 3D <sup>4</sup>	3	76.108	76.177				
3d <sup>6</sup> 5D <sup>4</sup>	4	3d <sup>6</sup> 1G <sup>2</sup>	4	41.274	41.305				
3d <sup>6</sup> 5D <sup>4</sup>	4	3d <sup>6</sup> 3F <sup>2</sup>	3	37.905	37.948				
3d <sup>6</sup> 5D <sup>4</sup>	4	3d <sup>6</sup> 3H <sup>4</sup>	4	16.955	16.934				
3d <sup>6</sup> 5D <sup>4</sup>	4	3d <sup>6</sup> 5D <sup>4</sup>	3	16.211	16.193				
3d <sup>6</sup> 5D <sup>4</sup>	4	3d <sup>6</sup> 3H <sup>4</sup>	5	16.032	16.018				
3d <sup>6</sup> 5D <sup>4</sup>	4	3d <sup>6</sup> 3F <sup>4</sup>	3	14.740	14.726				
3d <sup>6</sup> 5D <sup>4</sup>	4	3d <sup>6</sup> 1G <sup>4</sup>	4	13.997	13.987				
3d <sup>6</sup> 5D <sup>4</sup>	4	3d <sup>6</sup> 3F <sup>2</sup>	4	11.676	11.672				
3d <sup>6</sup> 5D <sup>4</sup>	4	3d <sup>6</sup> 1G <sup>2</sup>	4	8.026	8.016				
3d <sup>6</sup> 5D <sup>4</sup>	4	3d <sup>6</sup> 3F <sup>2</sup>	3	7.617	7.609				
3d <sup>6</sup> 5D <sup>4</sup>	1	3d <sup>6</sup> 3F <sup>4</sup>	2	108.263	108.730				
3d <sup>6</sup> 5D <sup>4</sup>	1	3d <sup>6</sup> 3P <sup>4</sup>	0	55.744	55.924				
3d <sup>6</sup> 5D <sup>4</sup>	1	3d <sup>6</sup> 3D <sup>4</sup>	2	45.325	45.393				
3d <sup>6</sup> 5D <sup>4</sup>	1	3d <sup>6</sup> 3P <sup>2</sup>	1	45.157	45.248				
3d <sup>6</sup> 5D <sup>4</sup>	1	3d <sup>6</sup> 5D <sup>4</sup>	2	19.495	19.468				
3d <sup>6</sup> 5D <sup>4</sup>	1	3d <sup>6</sup> 5D <sup>4</sup>	0	18.606	18.576				
3d <sup>6</sup> 5D <sup>4</sup>	1	3d <sup>6</sup> 3D <sup>4</sup>	1	14.889	14.882				
3d <sup>6</sup> 5D <sup>4</sup>	1	3d <sup>6</sup> 3F <sup>4</sup>	2	14.326	14.322				

Table 5. Cont.

Label and <i>J</i> for Lower		Label and <i>J</i> for Upper		Present Work		Expt (Ref. [2])	GRASP	RMBPT <sub>g</sub>	RCI <sub>g</sub>
				<i>n</i> = 5	<i>n</i> = 6				
3d <sup>6</sup> 5D <sup>4</sup>	1	3d <sup>6</sup> 3F <sup>2</sup>	2	12.637	12.629				
3d <sup>6</sup> 5D <sup>4</sup>	1	3d <sup>6</sup> 1D <sup>2</sup>	2	10.274	10.274				
3d <sup>6</sup> 5D <sup>4</sup>	1	3d <sup>6</sup> 1G <sup>0</sup>	0	8.969	8.968				
3d <sup>6</sup> 5D <sup>4</sup>	1	3d <sup>6</sup> 3P <sup>2</sup>	1	8.947	8.934				
3d <sup>6</sup> 5D <sup>4</sup>	1	3d <sup>6</sup> 3P <sup>2</sup>	2	7.886	7.878				
3d <sup>6</sup> 5D <sup>4</sup>	1	3d <sup>6</sup> 3P <sup>2</sup>	0	5.630	5.622				
3d <sup>6</sup> 3H <sup>4</sup>	6	3d <sup>6</sup> 3G <sup>4</sup>	5	33171.897	25414.252				
3d <sup>6</sup> 3H <sup>4</sup>	6	3d <sup>6</sup> 3H <sup>4</sup>	5	17.866	17.837				
3d <sup>6</sup> 3H <sup>4</sup>	6	3d <sup>6</sup> 1J <sup>4</sup>	6	17.042	17.020				
3d <sup>6</sup> 3G <sup>4</sup>	5	3d <sup>6</sup> 1G <sup>2</sup>	4	56.196	56.170				
3d <sup>6</sup> 3G <sup>4</sup>	5	3d <sup>6</sup> 3H <sup>4</sup>	4	19.031	18.995				
3d <sup>6</sup> 3G <sup>4</sup>	5	3d <sup>6</sup> 3H <sup>4</sup>	5	17.876	17.850				
3d <sup>6</sup> 3G <sup>4</sup>	5	3d <sup>6</sup> 1J <sup>4</sup>	6	17.051	17.032				
3d <sup>6</sup> 3G <sup>4</sup>	5	3d <sup>6</sup> 1G <sup>4</sup>	4	15.382	15.364				
3d <sup>6</sup> 3G <sup>4</sup>	5	3d <sup>6</sup> 3F <sup>2</sup>	4	12.625	12.615				
3d <sup>6</sup> 3G <sup>4</sup>	5	3d <sup>6</sup> 1G <sup>2</sup>	4	8.463	8.450				
3d <sup>6</sup> 3F <sup>4</sup>	2	3d <sup>6</sup> 3D <sup>4</sup>	3	850.017	848.731				
3d <sup>6</sup> 3F <sup>4</sup>	2	3d <sup>6</sup> 3D <sup>4</sup>	2	77.967	77.927				
3d <sup>6</sup> 3F <sup>4</sup>	2	3d <sup>6</sup> 3P <sup>2</sup>	1	77.469	77.499				
3d <sup>6</sup> 3F <sup>4</sup>	2	3d <sup>6</sup> 3F <sup>2</sup>	3	69.354	69.431				
3d <sup>6</sup> 3F <sup>4</sup>	2	3d <sup>6</sup> 5D <sup>4</sup>	2	23.777	23.715				
3d <sup>6</sup> 3F <sup>4</sup>	2	3d <sup>6</sup> 5D <sup>4</sup>	3	20.111	20.078				
3d <sup>6</sup> 3F <sup>4</sup>	2	3d <sup>6</sup> 3F <sup>4</sup>	3	17.895	17.871				
3d <sup>6</sup> 3F <sup>4</sup>	2	3d <sup>6</sup> 3D <sup>4</sup>	1	17.263	17.242				
3d <sup>6</sup> 3F <sup>4</sup>	2	3d <sup>6</sup> 3F <sup>4</sup>	2	16.511	16.494				
3d <sup>6</sup> 3F <sup>4</sup>	2	3d <sup>6</sup> 3F <sup>2</sup>	2	14.307	14.288				
3d <sup>6</sup> 3F <sup>4</sup>	2	3d <sup>6</sup> 1D <sup>2</sup>	2	11.351	11.346				
3d <sup>6</sup> 3F <sup>4</sup>	2	3d <sup>6</sup> 3P <sup>2</sup>	1	9.754	9.734				
3d <sup>6</sup> 3F <sup>4</sup>	2	3d <sup>6</sup> 3P <sup>2</sup>	2	8.505	8.494				
3d <sup>6</sup> 3F <sup>4</sup>	2	3d <sup>6</sup> 3F <sup>2</sup>	3	8.381	8.370				
3d <sup>6</sup> 3D <sup>4</sup>	3	3d <sup>6</sup> 1G <sup>2</sup>	4	90.179	90.232				
3d <sup>6</sup> 3D <sup>4</sup>	3	3d <sup>6</sup> 3D <sup>4</sup>	2	85.841	85.805				
3d <sup>6</sup> 3D <sup>4</sup>	3	3d <sup>6</sup> 3F <sup>2</sup>	3	75.516	75.617				
3d <sup>6</sup> 3D <sup>4</sup>	3	3d <sup>6</sup> 5D <sup>4</sup>	2	24.461	24.396				
3d <sup>6</sup> 3D <sup>4</sup>	3	3d <sup>6</sup> 3H <sup>4</sup>	4	21.815	21.774				
3d <sup>6</sup> 3D <sup>4</sup>	3	3d <sup>6</sup> 5D <sup>4</sup>	3	20.598	20.565				
3d <sup>6</sup> 3D <sup>4</sup>	3	3d <sup>6</sup> 3F <sup>4</sup>	3	18.280	18.255				
3d <sup>6</sup> 3D <sup>4</sup>	3	3d <sup>6</sup> 1G <sup>4</sup>	4	17.151	17.133				
3d <sup>6</sup> 3D <sup>4</sup>	3	3d <sup>6</sup> 3F <sup>4</sup>	2	16.838	16.821				
3d <sup>6</sup> 3D <sup>4</sup>	3	3d <sup>6</sup> 3F <sup>2</sup>	2	14.552	14.533				
3d <sup>6</sup> 3D <sup>4</sup>	3	3d <sup>6</sup> 3F <sup>2</sup>	4	13.792	13.784				
3d <sup>6</sup> 3D <sup>4</sup>	3	3d <sup>6</sup> 1D <sup>2</sup>	2	11.505	11.500				
3d <sup>6</sup> 3D <sup>4</sup>	3	3d <sup>6</sup> 1G <sup>2</sup>	4	8.972	8.959				
3d <sup>6</sup> 3D <sup>4</sup>	3	3d <sup>6</sup> 3P <sup>2</sup>	2	8.591	8.579				
3d <sup>6</sup> 3D <sup>4</sup>	3	3d <sup>6</sup> 3F <sup>2</sup>	3	8.464	8.453				
3d <sup>6</sup> 3P <sup>4</sup>	0	3d <sup>6</sup> 3P <sup>2</sup>	1	237.757	237.023				
3d <sup>6</sup> 3P <sup>4</sup>	0	3d <sup>6</sup> 3D <sup>4</sup>	1	20.315	20.278				
3d <sup>6</sup> 3P <sup>4</sup>	0	3d <sup>6</sup> 3P <sup>2</sup>	1	10.658	10.633				
3d <sup>6</sup> 1G <sup>2</sup>	4	3d <sup>6</sup> 3F <sup>2</sup>	3	464.412	466.858				

Table 5. Cont.

Label and J for Lower		Label and J for Upper		Present Work		Expt (Ref. [2])	GRASP	RMBPT <sub>g</sub>	RCI <sub>g</sub>
				n = 5	n = 6				
3d <sup>6</sup> 1G <sup>2</sup>	4	3d <sup>6</sup> 3H <sup>4</sup>	4	28.776	28.700				
3d <sup>6</sup> 1G <sup>2</sup>	4	3d <sup>6</sup> 5D <sup>4</sup>	3	26.696	26.635				
3d <sup>6</sup> 1G <sup>2</sup>	4	3d <sup>6</sup> 3H <sup>4</sup>	5	26.215	26.164				
3d <sup>6</sup> 1G <sup>2</sup>	4	3d <sup>6</sup> 3F <sup>4</sup>	3	22.928	22.886				
3d <sup>6</sup> 1G <sup>2</sup>	4	3d <sup>6</sup> 1G <sup>4</sup>	4	21.178	21.149				
3d <sup>6</sup> 1G <sup>2</sup>	4	3d <sup>6</sup> 3F <sup>2</sup>	4	16.283	16.269				
3d <sup>6</sup> 1G <sup>2</sup>	4	3d <sup>6</sup> 1G <sup>2</sup>	4	9.963	9.946				
3d <sup>6</sup> 1G <sup>2</sup>	4	3d <sup>6</sup> 3F <sup>2</sup>	3	9.341	9.327				
3d <sup>6</sup> 3D <sup>4</sup>	2	3d <sup>6</sup> 3p <sup>2</sup>	1	12130.770	14130.082				
3d <sup>6</sup> 3D <sup>4</sup>	2	3d <sup>6</sup> 3F <sup>2</sup>	3	627.813	636.845				
3d <sup>6</sup> 3D <sup>4</sup>	2	3d <sup>6</sup> 5D <sup>4</sup>	2	34.209	34.088				
3d <sup>6</sup> 3D <sup>4</sup>	2	3d <sup>6</sup> 5D <sup>4</sup>	3	27.101	27.047				
3d <sup>6</sup> 3D <sup>4</sup>	2	3d <sup>6</sup> 3F <sup>4</sup>	3	23.226	23.189				
3d <sup>6</sup> 3D <sup>4</sup>	2	3d <sup>6</sup> 3D <sup>4</sup>	1	22.172	22.140				
3d <sup>6</sup> 3D <sup>4</sup>	2	3d <sup>6</sup> 3F <sup>4</sup>	2	20.946	20.922				
3d <sup>6</sup> 3D <sup>4</sup>	2	3d <sup>6</sup> 3F <sup>2</sup>	2	17.522	17.497				
3d <sup>6</sup> 3D <sup>4</sup>	2	3d <sup>6</sup> 1D <sup>2</sup>	2	13.285	13.280				
3d <sup>6</sup> 3D <sup>4</sup>	2	3d <sup>6</sup> 3p <sup>2</sup>	1	11.148	11.124				
3d <sup>6</sup> 3D <sup>4</sup>	2	3d <sup>6</sup> 3p <sup>2</sup>	2	9.546	9.533				
3d <sup>6</sup> 3D <sup>4</sup>	2	3d <sup>6</sup> 3F <sup>2</sup>	3	9.390	9.377				
3d <sup>6</sup> 3p <sup>2</sup>	1	3d <sup>6</sup> 5D <sup>4</sup>	2	34.306	34.171				
3d <sup>6</sup> 3p <sup>2</sup>	1	3d <sup>6</sup> 5D <sup>4</sup>	0	31.646	31.512				
3d <sup>6</sup> 3p <sup>2</sup>	1	3d <sup>6</sup> 3D <sup>4</sup>	1	22.213	22.175				
3d <sup>6</sup> 3p <sup>2</sup>	1	3d <sup>6</sup> 3F <sup>4</sup>	2	20.982	20.954				
3d <sup>6</sup> 3p <sup>2</sup>	1	3d <sup>6</sup> 3F <sup>2</sup>	2	17.548	17.518				
3d <sup>6</sup> 3p <sup>2</sup>	1	3d <sup>6</sup> 1D <sup>2</sup>	2	13.300	13.292				
3d <sup>6</sup> 3p <sup>2</sup>	1	3d <sup>6</sup> 1S <sup>0</sup>	0	11.192	11.185				
3d <sup>6</sup> 3p <sup>2</sup>	1	3d <sup>6</sup> 3p <sup>2</sup>	1	11.158	11.132				
3d <sup>6</sup> 3p <sup>2</sup>	1	3d <sup>6</sup> 3p <sup>2</sup>	2	9.554	9.539				
3d <sup>6</sup> 3p <sup>2</sup>	1	3d <sup>6</sup> 3p <sup>2</sup>	0	6.432	6.419				
3d <sup>6</sup> 3F <sup>2</sup>	3	3d <sup>6</sup> 5D <sup>4</sup>	2	36.181	36.016				
3d <sup>6</sup> 3F <sup>2</sup>	3	3d <sup>6</sup> 3H <sup>4</sup>	4	30.677	30.580				
3d <sup>6</sup> 3F <sup>2</sup>	3	3d <sup>6</sup> 5D <sup>4</sup>	3	28.324	28.246				
3d <sup>6</sup> 3F <sup>2</sup>	3	3d <sup>6</sup> 3F <sup>4</sup>	3	24.119	24.065				
3d <sup>6</sup> 3F <sup>2</sup>	3	3d <sup>6</sup> 1G <sup>4</sup>	4	22.190	22.153				
3d <sup>6</sup> 3F <sup>2</sup>	3	3d <sup>6</sup> 3F <sup>4</sup>	2	21.669	21.633				
3d <sup>6</sup> 3F <sup>2</sup>	3	3d <sup>6</sup> 3F <sup>2</sup>	2	18.025	17.991				
3d <sup>6</sup> 3F <sup>2</sup>	3	3d <sup>6</sup> 3F <sup>2</sup>	4	16.875	16.857				
3d <sup>6</sup> 3F <sup>2</sup>	3	3d <sup>6</sup> 1D <sup>2</sup>	2	13.572	13.563				
3d <sup>6</sup> 3F <sup>2</sup>	3	3d <sup>6</sup> 1G <sup>2</sup>	4	10.182	10.163				
3d <sup>6</sup> 3F <sup>2</sup>	3	3d <sup>6</sup> 3p <sup>2</sup>	2	9.694	9.677				
3d <sup>6</sup> 3F <sup>2</sup>	3	3d <sup>6</sup> 3F <sup>2</sup>	3	9.532	9.517				
3d <sup>6</sup> 5D <sup>4</sup>	2	3d <sup>6</sup> 5D <sup>4</sup>	3	130.436	130.930				
3d <sup>6</sup> 5D <sup>4</sup>	2	3d <sup>6</sup> 3F <sup>4</sup>	3	72.345	72.524				
3d <sup>6</sup> 5D <sup>4</sup>	2	3d <sup>6</sup> 3D <sup>4</sup>	1	63.013	63.168				
3d <sup>6</sup> 5D <sup>4</sup>	2	3d <sup>6</sup> 3F <sup>4</sup>	2	54.026	54.171				
3d <sup>6</sup> 5D <sup>4</sup>	2	3d <sup>6</sup> 3F <sup>2</sup>	2	35.921	35.947				
3d <sup>6</sup> 5D <sup>4</sup>	2	3d <sup>6</sup> 1D <sup>2</sup>	2	21.720	21.755				
3d <sup>6</sup> 5D <sup>4</sup>	2	3d <sup>6</sup> 3p <sup>2</sup>	1	16.537	16.511				

Table 5. Cont.

Label and J for Lower		Label and J for Upper		Present Work		Expt (Ref. [2])	GRASP	RMBPT <sub>g</sub>	RCI <sub>g</sub>
				n = 5	n = 6				
3d <sup>6</sup> 5D <sup>4</sup>	2	3d <sup>6</sup> 3P <sup>2</sup>	2	13.242	13.233				
3d <sup>6</sup> 5D <sup>4</sup>	2	3d <sup>6</sup> 3F <sup>2</sup>	3	12.942	12.935				
3d <sup>6</sup> 5D <sup>4</sup>	0	3d <sup>6</sup> 3D <sup>4</sup>	1	74.520	74.840				
3d <sup>6</sup> 5D <sup>4</sup>	0	3d <sup>6</sup> 3P <sup>2</sup>	1	17.236	17.213				
3d <sup>6</sup> 3H <sup>4</sup>	4	3d <sup>6</sup> 5D <sup>4</sup>	3	369.368	370.105				
3d <sup>6</sup> 3H <sup>4</sup>	4	3d <sup>6</sup> 3H <sup>4</sup>	5	294.589	296.075				
3d <sup>6</sup> 3H <sup>4</sup>	4	3d <sup>6</sup> 3F <sup>4</sup>	3	112.825	112.959				
3d <sup>6</sup> 3H <sup>4</sup>	4	3d <sup>6</sup> 1G <sup>4</sup>	4	80.216	80.382				
3d <sup>6</sup> 3H <sup>4</sup>	4	3d <sup>6</sup> 3F <sup>2</sup>	4	37.506	37.563				
3d <sup>6</sup> 3H <sup>4</sup>	4	3d <sup>6</sup> 1G <sup>2</sup>	4	15.240	15.221				
3d <sup>6</sup> 3H <sup>4</sup>	4	3d <sup>6</sup> 3F <sup>2</sup>	3	13.830	13.817				
3d <sup>6</sup> 5D <sup>4</sup>	3	3d <sup>6</sup> 3F <sup>4</sup>	3	162.444	162.579				
3d <sup>6</sup> 5D <sup>4</sup>	3	3d <sup>6</sup> 1G <sup>4</sup>	4	102.469	102.683				
3d <sup>6</sup> 5D <sup>4</sup>	3	3d <sup>6</sup> 3F <sup>4</sup>	2	92.227	92.402				
3d <sup>6</sup> 5D <sup>4</sup>	3	3d <sup>6</sup> 3F <sup>2</sup>	2	49.574	49.552				
3d <sup>6</sup> 5D <sup>4</sup>	3	3d <sup>6</sup> 3F <sup>2</sup>	4	41.744	41.805				
3d <sup>6</sup> 5D <sup>4</sup>	3	3d <sup>6</sup> 1D <sup>2</sup>	2	26.059	26.090				
3d <sup>6</sup> 5D <sup>4</sup>	3	3d <sup>6</sup> 1G <sup>2</sup>	4	15.896	15.874				
3d <sup>6</sup> 5D <sup>4</sup>	3	3d <sup>6</sup> 3P <sup>2</sup>	2	14.738	14.721				
3d <sup>6</sup> 5D <sup>4</sup>	3	3d <sup>6</sup> 3F <sup>2</sup>	3	14.368	14.353				
3d <sup>6</sup> 3H <sup>4</sup>	5	3d <sup>6</sup> 1J <sup>4</sup>	6	369.318	371.637				
3d <sup>6</sup> 3H <sup>4</sup>	5	3d <sup>6</sup> 1G <sup>4</sup>	4	110.232	110.337				
3d <sup>6</sup> 3H <sup>4</sup>	5	3d <sup>6</sup> 3F <sup>2</sup>	4	42.977	43.021				
3d <sup>6</sup> 3H <sup>4</sup>	5	3d <sup>6</sup> 1G <sup>2</sup>	4	16.071	16.046				
3d <sup>6</sup> 3F <sup>4</sup>	3	3d <sup>6</sup> 1G <sup>4</sup>	4	277.541	278.717				
3d <sup>6</sup> 3F <sup>4</sup>	3	3d <sup>6</sup> 3F <sup>4</sup>	2	213.361	214.066				
3d <sup>6</sup> 3F <sup>4</sup>	3	3d <sup>6</sup> 3F <sup>2</sup>	2	71.346	71.275				
3d <sup>6</sup> 3F <sup>4</sup>	3	3d <sup>6</sup> 3F <sup>2</sup>	4	56.181	56.276				
3d <sup>6</sup> 3F <sup>4</sup>	3	3d <sup>6</sup> 1D <sup>2</sup>	2	31.039	31.076				
3d <sup>6</sup> 3F <sup>4</sup>	3	3d <sup>6</sup> 1G <sup>2</sup>	4	17.620	17.592				
3d <sup>6</sup> 3F <sup>4</sup>	3	3d <sup>6</sup> 3P <sup>2</sup>	2	16.208	16.187				
3d <sup>6</sup> 3F <sup>4</sup>	3	3d <sup>6</sup> 3F <sup>2</sup>	3	15.762	15.743				
3d <sup>6</sup> 3D <sup>4</sup>	1	3d <sup>6</sup> 3F <sup>4</sup>	2	378.830	380.349				
3d <sup>6</sup> 3D <sup>4</sup>	1	3d <sup>6</sup> 3F <sup>2</sup>	2	83.550	83.418				
3d <sup>6</sup> 3D <sup>4</sup>	1	3d <sup>6</sup> 1D <sup>2</sup>	2	33.145	33.182				
3d <sup>6</sup> 3D <sup>4</sup>	1	3d <sup>6</sup> 1S <sup>0</sup>	0	22.557	22.569				
3d <sup>6</sup> 3D <sup>4</sup>	1	3d <sup>6</sup> 3P <sup>2</sup>	1	22.422	22.355				
3d <sup>6</sup> 3D <sup>4</sup>	1	3d <sup>6</sup> 3P <sup>2</sup>	2	16.764	16.740				
3d <sup>6</sup> 3D <sup>4</sup>	1	3d <sup>6</sup> 3P <sup>2</sup>	0	9.053	9.035				
3d <sup>6</sup> 1G <sup>4</sup>	4	3d <sup>6</sup> 3F <sup>2</sup>	4	70.440	70.514				
3d <sup>6</sup> 1G <sup>4</sup>	4	3d <sup>6</sup> 1G <sup>2</sup>	4	18.815	18.777				
3d <sup>6</sup> 1G <sup>4</sup>	4	3d <sup>6</sup> 3F <sup>2</sup>	3	16.711	16.685				
3d <sup>6</sup> 3F <sup>4</sup>	2	3d <sup>6</sup> 3F <sup>2</sup>	2	107.190	106.853				
3d <sup>6</sup> 3F <sup>4</sup>	2	3d <sup>6</sup> 1D <sup>2</sup>	2	36.323	36.354				
3d <sup>6</sup> 3F <sup>4</sup>	2	3d <sup>6</sup> 3P <sup>2</sup>	1	23.832	23.751				
3d <sup>6</sup> 3F <sup>4</sup>	2	3d <sup>6</sup> 3P <sup>2</sup>	2	17.541	17.511				
3d <sup>6</sup> 3F <sup>4</sup>	2	3d <sup>6</sup> 3F <sup>2</sup>	3	17.019	16.992				
3d <sup>6</sup> 3F <sup>2</sup>	2	3d <sup>6</sup> 1D <sup>2</sup>	2	54.939	55.101				
3d <sup>6</sup> 3F <sup>2</sup>	2	3d <sup>6</sup> 3P <sup>2</sup>	1	30.646	30.539				

Table 5. Cont.

Label and J for Lower		Label and J for Upper		Present Work		Expt (Ref. [2])	GRASP	RMBPT <sub>g</sub>	RCI <sub>g</sub>
				n = 5	n = 6				
3d <sup>6</sup> 3F <sup>2</sup>	2	3d <sup>6</sup> 3P <sup>2</sup>	2	20.973	20.943				
3d <sup>6</sup> 3F <sup>2</sup>	2	3d <sup>6</sup> 3F <sup>2</sup>	3	20.232	20.205				
3d <sup>6</sup> 3F <sup>2</sup>	4	3d <sup>6</sup> 1G <sup>2</sup>	4	25.671	25.592				
3d <sup>6</sup> 3F <sup>2</sup>	4	3d <sup>6</sup> 3F <sup>2</sup>	3	21.909	21.857				
3d <sup>6</sup> 1D <sup>2</sup>	2	3d <sup>6</sup> 3P <sup>2</sup>	1	69.307	68.508				
3d <sup>6</sup> 1D <sup>2</sup>	2	3d <sup>6</sup> 3P <sup>2</sup>	2	33.922	33.783				
3d <sup>6</sup> 1D <sup>2</sup>	2	3d <sup>6</sup> 3F <sup>2</sup>	3	32.025	31.905				
3d <sup>6</sup> 1S <sup>0</sup>	0	3d <sup>6</sup> 3P <sup>2</sup>	1	3732.652	2353.561				
3d <sup>6</sup> 3P <sup>2</sup>	1	3d <sup>6</sup> 3P <sup>2</sup>	2	66.443	66.648				
3d <sup>6</sup> 3P <sup>2</sup>	1	3d <sup>6</sup> 3P <sup>2</sup>	0	15.184	15.162				
3d <sup>6</sup> 1G <sup>2</sup>	4	3d <sup>6</sup> 3F <sup>2</sup>	3	149.470	149.753				
3d <sup>6</sup> 3P <sup>2</sup>	2	3d <sup>6</sup> 3F <sup>2</sup>	3	572.500	573.976				
W <sup>49+</sup> (Mn-like)									
3d <sup>7</sup> 4F <sup>3</sup>	9/2	3d <sup>7</sup> 4F <sup>3</sup>	7/2	18.940	18.908	18.880(3)	19.006	18.901	18.943
3d <sup>7</sup> 4F <sup>3</sup>	9/2	3d <sup>7</sup> 4F <sup>3</sup>	9/2	17.138	17.119	17.106(3)	17.149	17.118	17.132
3d <sup>7</sup> 4F <sup>3</sup>	9/2	3d <sup>7</sup> 2H <sup>3</sup>	11/2	15.381	15.371	15.368(3)	15.343	15.372	15.380
3d <sup>7</sup> 4F <sup>3</sup>	9/2	3d <sup>7</sup> 2F <sup>3</sup>	7/2	14.180	14.170	14.166(3)	14.156	14.187	14.063
3d <sup>7</sup> 4F <sup>3</sup>	9/2	3d <sup>7</sup> 2H <sup>3</sup>	9/2	8.434	8.424				
3d <sup>7</sup> 4F <sup>3</sup>	9/2	3d <sup>7</sup> 2F <sup>3</sup>	7/2	8.259	8.250				
3d <sup>7</sup> 2P <sup>3</sup>	3/2	3d <sup>7</sup> 2D <sup>1</sup>	5/2	174.708	174.056				
3d <sup>7</sup> 2P <sup>3</sup>	3/2	3d <sup>7</sup> 4P <sup>3</sup>	3/2	19.753	19.715				
3d <sup>7</sup> 2P <sup>3</sup>	3/2	3d <sup>7</sup> 4P <sup>3</sup>	5/2	19.111	19.081	19.047(3)	19.130	19.037	19.271
3d <sup>7</sup> 2P <sup>3</sup>	3/2	3d <sup>7</sup> 4P <sup>3</sup>	1/2	18.720	18.692	18.670(3)	18.764	18.680	18.733
3d <sup>7</sup> 2P <sup>3</sup>	3/2	3d <sup>7</sup> 2F <sup>3</sup>	5/2	15.597	15.585				
3d <sup>7</sup> 2P <sup>3</sup>	3/2	3d <sup>7</sup> 2D <sup>1</sup>	3/2	12.711	12.700				
3d <sup>7</sup> 2P <sup>3</sup>	3/2	3d <sup>7</sup> 4F <sup>3</sup>	5/2	9.864	9.847				
3d <sup>7</sup> 2P <sup>3</sup>	3/2	3d <sup>7</sup> 4P <sup>3</sup>	3/2	9.561	9.546				
3d <sup>7</sup> 2P <sup>3</sup>	3/2	3d <sup>7</sup> 2P <sup>3</sup>	1/2	9.171	9.157				
3d <sup>7</sup> 2P <sup>3</sup>	3/2	3d <sup>7</sup> 2D <sup>1</sup>	5/2	7.643	7.636				
3d <sup>7</sup> 2P <sup>3</sup>	3/2	3d <sup>7</sup> 2D <sup>1</sup>	3/2	6.060	6.050				
3d <sup>7</sup> 2D <sup>1</sup>	5/2	3d <sup>7</sup> 4F <sup>3</sup>	7/2	27.098	27.043				
3d <sup>7</sup> 2D <sup>1</sup>	5/2	3d <sup>7</sup> 4P <sup>3</sup>	3/2	22.271	22.233				
3d <sup>7</sup> 2D <sup>1</sup>	5/2	3d <sup>7</sup> 4P <sup>3</sup>	5/2	21.458	21.430				
3d <sup>7</sup> 2D <sup>1</sup>	5/2	3d <sup>7</sup> 2F <sup>3</sup>	7/2	18.307	18.294	18.276(3)	18.258	18.274	18.425
3d <sup>7</sup> 2D <sup>1</sup>	5/2	3d <sup>7</sup> 2F <sup>3</sup>	5/2	17.126	17.117				
3d <sup>7</sup> 2D <sup>1</sup>	5/2	3d <sup>7</sup> 2D <sup>1</sup>	3/2	13.709	13.700				
3d <sup>7</sup> 2D <sup>1</sup>	5/2	3d <sup>7</sup> 4F <sup>3</sup>	5/2	10.455	10.437				
3d <sup>7</sup> 2D <sup>1</sup>	5/2	3d <sup>7</sup> 4P <sup>3</sup>	3/2	10.115	10.099				
3d <sup>7</sup> 2D <sup>1</sup>	5/2	3d <sup>7</sup> 2F <sup>3</sup>	7/2	9.507	9.496				
3d <sup>7</sup> 2D <sup>1</sup>	5/2	3d <sup>7</sup> 2D <sup>1</sup>	5/2	7.993	7.986				
3d <sup>7</sup> 2D <sup>1</sup>	5/2	3d <sup>7</sup> 2D <sup>1</sup>	3/2	6.278	6.268				
3d <sup>7</sup> 4F <sup>3</sup>	7/2	3d <sup>7</sup> 4F <sup>3</sup>	9/2	180.107	180.908				
3d <sup>7</sup> 4F <sup>3</sup>	7/2	3d <sup>7</sup> 4P <sup>3</sup>	5/2	103.103	103.259				
3d <sup>7</sup> 4F <sup>3</sup>	7/2	3d <sup>7</sup> 2F <sup>3</sup>	7/2	56.428	56.550				
3d <sup>7</sup> 4F <sup>3</sup>	7/2	3d <sup>7</sup> 2F <sup>3</sup>	5/2	46.537	46.637				
3d <sup>7</sup> 4F <sup>3</sup>	7/2	3d <sup>7</sup> 4F <sup>3</sup>	5/2	17.022	16.998				
3d <sup>7</sup> 4F <sup>3</sup>	7/2	3d <sup>7</sup> 2H <sup>3</sup>	9/2	15.204	15.193				
3d <sup>7</sup> 4F <sup>3</sup>	7/2	3d <sup>7</sup> 2F <sup>3</sup>	7/2	14.645	14.635				

Table 5. Cont.

Label and J for Lower		Label and J for Upper		Present Work		Expt (Ref. [2])	GRASP	RMBPT <sub>g</sub>	RCI <sub>g</sub>
				n = 5	n = 6				
3d <sup>7</sup> 4F <sup>3</sup>	7/2	3d <sup>7</sup> 2D <sup>1</sup>	5/2	11.337	11.332				
3d <sup>7</sup> 4F <sup>3</sup>	9/2	3d <sup>7</sup> 2H <sup>3</sup>	11/2	150.021	150.559				
3d <sup>7</sup> 4F <sup>3</sup>	9/2	3d <sup>7</sup> 2F <sup>3</sup>	7/2	82.173	82.265				
3d <sup>7</sup> 4F <sup>3</sup>	9/2	3d <sup>7</sup> 2H <sup>3</sup>	9/2	16.606	16.586				
3d <sup>7</sup> 4F <sup>3</sup>	9/2	3d <sup>7</sup> 2F <sup>3</sup>	7/2	15.942	15.923				
3d <sup>7</sup> 4P <sup>3</sup>	3/2	3d <sup>7</sup> 4P <sup>3</sup>	5/2	587.816	593.270				
3d <sup>7</sup> 4P <sup>3</sup>	3/2	3d <sup>7</sup> 4P <sup>3</sup>	1/2	357.969	360.283				
3d <sup>7</sup> 4P <sup>3</sup>	3/2	3d <sup>7</sup> 2F <sup>3</sup>	5/2	74.127	74.387				
3d <sup>7</sup> 4P <sup>3</sup>	3/2	3d <sup>7</sup> 2D <sup>1</sup>	3/2	35.657	35.693				
3d <sup>7</sup> 4P <sup>3</sup>	3/2	3d <sup>7</sup> 4F <sup>3</sup>	5/2	19.704	19.673				
3d <sup>7</sup> 4P <sup>3</sup>	3/2	3d <sup>7</sup> 4P <sup>3</sup>	3/2	18.530	18.506				
3d <sup>7</sup> 4P <sup>3</sup>	3/2	3d <sup>7</sup> 2P <sup>3</sup>	1/2	17.118	17.100				
3d <sup>7</sup> 4P <sup>3</sup>	3/2	3d <sup>7</sup> 2D <sup>1</sup>	5/2	12.467	12.462				
3d <sup>7</sup> 4P <sup>3</sup>	3/2	3d <sup>7</sup> 2D <sup>1</sup>	3/2	8.742	8.729				
3d <sup>7</sup> 4P <sup>3</sup>	5/2	3d <sup>7</sup> 2F <sup>3</sup>	7/2	124.648	125.014				
3d <sup>7</sup> 4P <sup>3</sup>	5/2	3d <sup>7</sup> 2F <sup>3</sup>	5/2	84.823	85.051				
3d <sup>7</sup> 4P <sup>3</sup>	5/2	3d <sup>7</sup> 2D <sup>1</sup>	3/2	37.960	37.978				
3d <sup>7</sup> 4P <sup>3</sup>	5/2	3d <sup>7</sup> 4F <sup>3</sup>	5/2	20.388	20.347				
3d <sup>7</sup> 4P <sup>3</sup>	5/2	3d <sup>7</sup> 4P <sup>3</sup>	3/2	19.133	19.101				
3d <sup>7</sup> 4P <sup>3</sup>	5/2	3d <sup>7</sup> 2F <sup>3</sup>	7/2	17.070	17.052				
3d <sup>7</sup> 4P <sup>3</sup>	5/2	3d <sup>7</sup> 2D <sup>1</sup>	5/2	12.737	12.729				
3d <sup>7</sup> 4P <sup>3</sup>	5/2	3d <sup>7</sup> 2D <sup>1</sup>	3/2	8.874	8.860				
3d <sup>7</sup> 4P <sup>3</sup>	1/2	3d <sup>7</sup> 2D <sup>1</sup>	3/2	39.602	39.618				
3d <sup>7</sup> 4P <sup>3</sup>	1/2	3d <sup>7</sup> 4P <sup>3</sup>	3/2	19.542	19.508				
3d <sup>7</sup> 4P <sup>3</sup>	1/2	3d <sup>7</sup> 2P <sup>3</sup>	1/2	17.978	17.952				
3d <sup>7</sup> 4P <sup>3</sup>	1/2	3d <sup>7</sup> 2D <sup>1</sup>	3/2	8.961	8.946				
3d <sup>7</sup> 2H <sup>3</sup>	11/2	3d <sup>7</sup> 2H <sup>3</sup>	9/2	18.673	18.639				
3d <sup>7</sup> 2F <sup>3</sup>	7/2	3d <sup>7</sup> 2F <sup>3</sup>	5/2	265.490	266.061				
3d <sup>7</sup> 2F <sup>3</sup>	7/2	3d <sup>7</sup> 4F <sup>3</sup>	5/2	24.375	24.303				
3d <sup>7</sup> 2F <sup>3</sup>	7/2	3d <sup>7</sup> 2H <sup>3</sup>	9/2	20.812	20.774				
3d <sup>7</sup> 2F <sup>3</sup>	7/2	3d <sup>7</sup> 2F <sup>3</sup>	7/2	19.779	19.745				
3d <sup>7</sup> 2F <sup>3</sup>	7/2	3d <sup>7</sup> 2D <sup>1</sup>	5/2	14.187	14.173				
3d <sup>7</sup> 2F <sup>3</sup>	5/2	3d <sup>7</sup> 2D <sup>1</sup>	3/2	68.707	68.619				
3d <sup>7</sup> 2F <sup>3</sup>	5/2	3d <sup>7</sup> 4F <sup>3</sup>	5/2	26.839	26.746				
3d <sup>7</sup> 2F <sup>3</sup>	5/2	3d <sup>7</sup> 4P <sup>3</sup>	3/2	24.706	24.634				
3d <sup>7</sup> 2F <sup>3</sup>	5/2	3d <sup>7</sup> 2F <sup>3</sup>	7/2	21.371	21.328				
3d <sup>7</sup> 2F <sup>3</sup>	5/2	3d <sup>7</sup> 2D <sup>1</sup>	5/2	14.988	14.970				
3d <sup>7</sup> 2F <sup>3</sup>	5/2	3d <sup>7</sup> 2D <sup>1</sup>	3/2	9.911	9.890				
3d <sup>7</sup> 2D <sup>1</sup>	3/2	3d <sup>7</sup> 4F <sup>3</sup>	5/2	44.043	43.830				
3d <sup>7</sup> 2D <sup>1</sup>	3/2	3d <sup>7</sup> 4P <sup>3</sup>	3/2	38.579	38.430				
3d <sup>7</sup> 2D <sup>1</sup>	3/2	3d <sup>7</sup> 2P <sup>3</sup>	1/2	32.925	32.828				
3d <sup>7</sup> 2D <sup>1</sup>	3/2	3d <sup>7</sup> 2D <sup>1</sup>	5/2	19.169	19.147				
3d <sup>7</sup> 2D <sup>1</sup>	3/2	3d <sup>7</sup> 2D <sup>1</sup>	3/2	11.581	11.555				
3d <sup>7</sup> 4F <sup>3</sup>	5/2	3d <sup>7</sup> 4P <sup>3</sup>	3/2	310.962	311.919				
3d <sup>7</sup> 4F <sup>3</sup>	5/2	3d <sup>7</sup> 2F <sup>3</sup>	7/2	104.893	105.290				
3d <sup>7</sup> 4F <sup>3</sup>	5/2	3d <sup>7</sup> 2D <sup>1</sup>	5/2	33.943	34.000				
3d <sup>7</sup> 4F <sup>3</sup>	5/2	3d <sup>7</sup> 2D <sup>1</sup>	3/2	15.713	15.692				
3d <sup>7</sup> 4P <sup>3</sup>	3/2	3d <sup>7</sup> 2P <sup>3</sup>	1/2	224.661	225.205				
3d <sup>7</sup> 4P <sup>3</sup>	3/2	3d <sup>7</sup> 2D <sup>1</sup>	5/2	38.102	38.159				

Table 5. Cont.

Label and J for Lower		Label and J for Upper		Present Work		Expt (Ref. [2])	GRASP	RMBPT <sub>g</sub>	RCI <sub>g</sub>
				n = 5	n = 6				
$3d^7\ 4P^3$	3/2	$3d^7\ 2D^1$	3/2	16.549	16.524				
$3d^7\ 2P^3$	1/2	$3d^7\ 2D^1$	3/2	17.865	17.832				
$3d^7\ 2H^3$	9/2	$3d^7\ 2F^3$	7/2	398.243	398.611				
$3d^7\ 2F^3$	7/2	$3d^7\ 2D^1$	5/2	50.182	50.215				
$3d^7\ 2D^1$	5/2	$3d^7\ 2D^1$	3/2	29.257	29.143				
W <sup>48+</sup> (Fe-like)									
$3d^8\ 3F$	4	$3d^8\ 3F$	3	19.041	19.009	18.988(3)	19.114	19.007	19.027
$3d^8\ 3F$	4	$3d^8\ 1G$	4	15.531	15.518	15.511(3)	15.503	15.463	15.525
$3d^8\ 1D$	2	$3d^8\ 3F$	3	22.073	22.029				
$3d^8\ 1D$	2	$3d^8\ 3P$	2	18.931	18.902	18.878(3)	18.978	18.888	18.966
$3d^8\ 1D$	2	$3d^8\ 3P$	1	17.548	17.525	17.502(3)	17.548	17.517	17.489
$3d^8\ 1D$	2	$3d^8\ 3F$	2	9.664	9.648				
$3d^8\ 3P$	0	$3d^8\ 3P$	1	24.268	24.236				
$3d^8\ 3F$	3	$3d^8\ 3P$	2	132.993	133.189				
$3d^8\ 3F$	3	$3d^8\ 1G$	4	84.240	84.489				
$3d^8\ 3F$	3	$3d^8\ 3F$	2	17.190	17.167				
$3d^8\ 3P$	2	$3d^8\ 3P$	1	240.207	240.600				
$3d^8\ 3P$	2	$3d^8\ 3F$	2	19.742	19.707				
$3d^8\ 3P$	1	$3d^8\ 3F$	2	21.510	21.465				
$3d^8\ 3P$	1	$3d^8\ 1S$	0	15.102	15.082				
W <sup>47+</sup> (Co-like)									
$3d^9\ 2D$	5/2	$3d^9\ 2D$	3/2	18.615	18.586	18.567(3)	18.671	18.586	18.580

#### 4. Conclusions

The present study has shown that the inclusion of core correlation effects improves the accuracy of theoretical transition wavelengths for M1 transitions in  $3d^k$  configurations of tungsten ions. Omitted in our work were correlation effects arising from the  $1s^2$  core. Further studies are needed to determine whether the discrepancy with observation arises from the limited orbital set for core correlation or from the inactive  $1s^2$  shell in our present work.

**Acknowledgments:** Computations were performed on resources at the High Performance Computing Center “HPC Sauletekis” in Vilnius University Faculty of Physics (Lithuania). Per Jönsson acknowledge support from the Swedish Research Council under contract 2015-04842.

**Author Contributions:** All authors have participated in the development of the programs that made these calculations possible and in preparation of this manuscript.

**Conflicts of Interest:** The authors declare no conflict of interest.

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# Calculation of Rates of 4p–4d Transitions in Ar II

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Academic Editor: Joseph Reader

Received: 29 December 2016; Accepted: 9 February 2017; Published: 21 February 2017

**Abstract:** Recent experimental work by Belmonte et al. (2014) has given rates for some 4p–4d transitions that are significantly at variance with the previous experimental work of Rudko and Tang (1967) recommended in the NIST tabulations. To date, there are no theoretical rates with which to compare. In this work, we provide such theoretical data. We have undertaken a substantial and systematic configuration interaction calculation, with an extrapolation process applied to ab initio mixing coefficients, which gives energy differences in agreement with experiment. The length and velocity forms give values that are within 10%–15% of each other. Our results are in sufficiently close agreement with those of Belmonte et al. that we can confidently recommend that their results are much more accurate than the early results of Rudko and Tang, and should be adopted in place of the latter.

**Keywords:** E1 transitions; configuration interaction calculation; transition rates

## 1. Introduction

Some years ago, we [1–3] studied transitions among Ar II levels arising from configurations  $3s^23p^5$ ,  $3s3p^6$ ,  $3p^43d$ ,  $3p^44s$ , and  $3p^44p$ . That work was prompted by a range of conflicting experimental results and a limited amount of theoretical work. We found that our calculations gave transition rates in close agreement with the experimental values recommended by Vujnović and Wiese [4], and gave much closer agreement between length and velocity forms of transition rates than were obtained by the only other major theoretical work, conducted by Luyken [5]. The values cited in the NIST tabulations [6] are taken from Bennett et al. [7] where possible, in agreement with the recommended values given in [4], but for other 4p–4d transitions, it is the data of Rudko and Tang [8] which are quoted.

Recently, Belmonte et al. [9]—building on the work of Aparicio et al. [10]—extended the experimental study to 4p–4d (and a few other) transitions. They also included results for some transitions between the lower-lying levels previously studied in [2–4], and found that they were in much closer agreement with the experimental values recommended by Vujnović and Wiese [4], and with our previous calculations, than with other experimental work. By contrast, they found that their results differed by up to a factor of five from the experimental values of Rudko and Tang [8]. The purpose of the present work is to provide some theoretical corroboration (or otherwise) of the new experimental results.

## 2. Method of Calculation

The calculations in this work have been undertaken using the code CIV3 [11,12].

### 2.1. Basic Theory

We express the wave functions in terms of configuration interaction (CI) expansions:

$$\Psi(J) = \sum_{i=1}^M a_i \Phi_i(\alpha_i L_i S_i J) \quad (1)$$

where  $\{\Phi_i\}$  are single-configuration functions (configuration state functions—CSFs) and the expansions in general include summations over  $L_i$  and  $S_i$ . For a specific choice of  $\{\Phi_i\}$ , the expansion coefficients  $\{a_i\}$  are the eigenvector components of the diagonalized Hamiltonian with matrix elements  $H_{ij} = \langle \Phi_i | H | \Phi_j \rangle$ . In this work, we take the Hamiltonian  $H$  to be the Schrödinger Hamiltonian plus the mass correction and Darwin terms, together with a modified spin-orbit term

$$H_{so} = \frac{1}{2} \alpha^2 \sum_{i=1}^N \frac{Z\zeta_l}{r_i^3} \mathbf{l}_i \cdot \mathbf{s}_i \quad (2)$$

In (2), the sum is over the electrons, and the parameters  $\{\zeta_l\}$  depend on the  $l$ -value of the electrons involved in the interaction (Hibbert and Hansen 1989) [2].

The ordered eigenvalues  $\{E_i\}$  of the Hamiltonian matrix are upper bounds to the similarly-ordered energy levels:

$$E_i \geq E_i^{\text{exact}} \quad (3)$$

Hence, any of the eigenvalues may be used as the variational functional for optimisation of the radial parts of the one-electron orbitals from which the  $\{\Phi_i\}$  are constructed. We express these radial functions as sums of normalised Slater-type orbitals (STOs):

$$P_{nl}(r) = \sum_{j=1}^k C_{jnl} \chi_{jnl}(r) \quad (4)$$

where the STOs are of the form

$$\chi_{jnl}(r) = \left[ \frac{(2\zeta_{jnl})^{2I_{jnl}+1}}{(2I_{jnl})!} \right]^{1/2} r^{I_{jnl}} \exp(-\zeta_{jnl}r) \quad (5)$$

Being integers, the  $\{I_{jnl}\}$  are kept fixed, but the exponents  $\{\zeta_{jnl}\}$  and the coefficients  $\{C_{jnl}\}$  may be treated as variational parameters in (3), subject to the orthonormality conditions:

$$\int_0^\infty P_{nl}(r) P_{n'l}(r) dr = \delta_{nn'}; \quad l < n' \leq n \quad (6)$$

## 2.2. Radial Function Parameters

Since we were adding to earlier work [3], we were able to use many of the radial functions we used previously. However, that work did not include 4d levels. The radial function parameters are determined by optimising the energy associated with different states; the optimisation is undertaken in LS coupling. The radial function parameters used in this work were optimised as displayed in Table 1. We comment here on the reasons underpinning the choice of procedure used for the functions new to this work.

- The 6p function was newly introduced in this calculation. While retaining the 4p and 5p functions from previous work, the parameters for 6p were optimised on the ground state to improve the capture of the electron correlation effect in the  $n = 3$  shell, and thereby improve the calculated separation between the ground and excited states.
- We retained the previous 3d and 4d functions, but reoptimised 5d and 6d. We considered the lowering of the energy of several different states brought about by the introduction of 5d. The effect was largest for the  $3p^4 4d^4 \text{ } ^4\text{F}$  state. Similarly, the lowering of the energy of several different doublet states through the introduction of 6d was noted. There was a substantial difference in the mixings between doublet states, depending on the final LS symmetry chosen for the optimisation. As a consequence, we selected those obtained during the optimisation of the  $3p^4 ({}^3\text{P}) 4d^2 \text{ } ^2\text{D}$  state.

- We reoptimised the 6s function on the  $5s^4P$  state, since the energy of that state lay in the region of those of the 4d states.

The set of parameters for all the radial functions used here is displayed in Table 2.

**Table 1.** Method of determining the radial functions.

Orbital	Process of Optimisation	
1s, 2s, 2p, 3s	Hartree–Fock orbitals of $3p^4\ ^1D$ of Ar III (Clementi and Roetti (1974)) [13]	
3p	Exponents taken from the Hartree–Fock orbital of $3p^4\ ^1D$ of Ar III; coefficients reoptimised on $3p^4 4s\ ^4P$ of Ar II	
	Eigenvalue minimised	Configurations
3d	$3s3p^6\ ^2S$	$3s3p^6, 3s^23p^43d$
4s	$3p^4 4s\ ^4P$	$3p^4 4s$
4p	$3p^4 4p\ ^4D^o$	$3p^4 4p$
4d	$3p^4 3d\ ^4D$	$3p^4 3d, 3p^4 4d$
4f	$3p^4 3d\ ^4P$	$3p^4 4s, 3p^4 3d, 3p^4 4d, 3p^3 3d 4f$
5s	$3p^4 4p\ ^4D^o$	$3p^4 4p, 3p^3 4s 5s$
5p	$3p^4 4p\ ^4P^o$	$3p^4 4p, 3p^4 5p$
5d	$3p^4 4d\ ^4F$	$3p^4 3d, 3p^4 4d, 3p^4 5d$
5f	$3p^4 4p\ ^4D^o$	$3p^4 4p, 3p^4 4f, 3p^4 5f$
6s	$3p^4 5s\ ^4P$	$3p^4 4s, 3p^4 5s, 3p^4 6s$
6p	$3p^5\ ^2P^o$	$3p^5, 3p^4 4p, 3p^4 5p, 3p^4 6p$
6d	$3p^4 4d(^3P)\ ^2D$	$3p^4 3d, 3p^4 4d, 3p^4 5d, 3p^4 6d$

### 2.3. Choice of Configurations

In our previous work [3], we included a limited range of configurations aimed at capturing the main correlation effects in the  $3p^4 3d/4s/4p$  states. This led to some difficulties, primarily that the degree of correlation included in the ground state was substantially greater than for the excited states, and the order of some 3d and 4s levels was incorrect.

Consequently, in this work, we have included all possible configurations that can be obtained by one- and two-orbital replacements from the  $3l$  and  $4l$  subshells to the full set of orbitals shown in Table 2, from the configurations of the following reference sets.

Odd  $3p^5; 3p^4 4p$   
 Even  $3s3p^6; 3p^4 4s, 3p^4 5s, 3p^4 6s; 3p^4 3d, 3p^4 4d, 3p^4 5d, 3p^4 6d$

The configurations of the reference sets were those with a significant CI coefficient in a relatively small CI calculation. For each possible  $LS\pi$  symmetry, all CSFs were then constructed and combined to give a set of CSFs for each allowed  $J\ \pi$  symmetry, resulting in Hamiltonian matrices of the following sizes.

	J = 0.5	J = 1.5	J = 2.5	J = 3.5	J = 4.5
Odd	13,082	18,144	17,603	9148	
Even	44,149	75,383	75,964	61,072	28,854

**Table 2.** Radial function parameters.

<i>nl</i>	$C_{jnl}$	$I_{jnl}$	$\xi_{jnl}$	<i>nl</i>	$C_{jnl}$	$I_{jnl}$	$\xi_{jnl}$	
1s	0.926 94	1	17.332 10	2p	−0.011 17	3	3.102 81	
	0.058 91	1	25.455 00		0.004 97	3	2.011 93	
	0.007 82	2	7.657 68		0.145 75	3	5.190 03	
	0.017 65	2	15.623 20		0.824 78	2	6.928 92	
	0.000 90	3	3.237 31		0.087 03	2	13.042 40	
	−0.000 47	3	2.296 92					
	−0.003 17	3	6.726 86	3p	0.530 23	3	3.102 81	
			0.583 91		3	2.011 93		
			−0.074 28		3	5.190 03		
2s	−0.277 90	1	17.332 10		−0.272 24	2	6.928 92	
	−0.008 62	1	25.455 00		−0.025 06	2	13.042 40	
	0.816 64	2	7.657 68	4p	0.744 05	4	0.995 10	
	−0.127 59	2	15.623 20		0.297 40	4	0.775 02	
	0.013 06	3	3.237 31		−0.296 30	3	2.508 00	
	−0.003 71	3	2.296 92		0.082 76	2	7.360 60	
0.331 25	3	6.726 86						
3s	−0.094 80	1	17.332 10	5p	4.629 07	4	0.861 89	
	−0.001 41	1	25.455 00		−4.686 80	4	1.000 00	
	0.289 14	2	7.657 68		0.735 21	3	3.221 66	
	−0.043 25	2	15.623 20		−0.403 55	2	3.473 69	
	−0.640 52	3	3.237 31					
	−0.494 62	3	2.296 92		6p	6.828 07	5	0.937 15
0.216 65	3	6.726 86	−8.463 99	4		0.892 84		
			3.198 41	4		1.697 71		
			−1.193 75	3		2.716 06		
			0.308 57	2		8.508 55		
4s	0.487 62	4	1.299 90	3d	0.249 70	3	3.465 62	
	0.569 47	4	1.016 95		0.821 57	3	1.684 33	
	−0.384 57	3	2.931 16		4d	0.216 25	3	2.817 41
	0.157 04	2	6.149 39			0.300 37	3	1.891 60
	−0.042 15	1	14.064 49			−1.104 59	4	0.964 72
						0.067 82	4	0.570 20
5s	1.133 28	5	1.364 91	5d	0.438 75	3	2.189 96	
	−2.125 95	4	2.019 60		−1.653 12	3	0.717 04	
	1.487 29	3	2.884 30		1.981 83	4	0.612 62	
	−0.468 68	2	5.897 16		6d	0.594 56	3	2.112 65
	0.113 37	1	14.178 86			−3.249 46	3	0.719 43
						4.546 89	4	0.699 99
			−2.054 58	4		0.429 47		
6s	1.293 76	5	0.685 92					
	1.084 37	4	2.019 36					
	−1.350 12	4	1.180 83					
	−0.458 59	3	2.844 45					
	0.120 74	2	5.635 72					
	−0.026 11	1	14.432 79					
4f	1.000 00	4	2.154 77					
5f	0.522 16	4	2.573 22					
	−1.044 69	5	1.224 76					

**2.4. Relativistic Effects**

As in our earlier work [3], relativistic effects are included using the Breit–Pauli approximation, retaining in the Hamiltonian the mass correction and Darwin terms and a modified spin-orbit term as given in (2). The parameters  $\zeta_l$ —which depend only on the  $l$ -value of the electrons—were chosen to give the best fit to matrix elements of the full spin-orbit plus spin-other-orbit operators with respect to key CSFs. This led to the values 0.0, 0.856, 1.0, 1.0 for  $l = 0, 1, 2, 3$ , respectively. The d- and f-orbitals contribute little to the fine structure, most of which comes from configurations containing  $3p^4(^3P)$ .

### 3. Results

In our earlier work [3], we found that our choice of configurations resulted in the ground state being around  $12,000\text{ cm}^{-1}$  too low when compared with the excited states. In the present work, with our more systematic choice of configurations, we find that our ab initio energy separations are in much better agreement with the experimental work of Minnhagen [14] and Saloman [15], given in the tabulations of NIST [6]. Most of the energy separations agree to within  $1000\text{ cm}^{-1}$  with these experimental results, the exceptions being a few of the levels associated with states containing a  $3p^4\ ^1D$  core (within  $3000\text{ cm}^{-1}$ ) and those of  $3p^4\ ^1S\ 3d$  (about  $4000\text{ cm}^{-1}$ ). Moreover, the difficulty we encountered earlier with a very strong mixing between the  $3p^4(^1D)4s$  and  $3p^4(^3P)3d\ ^2D_{3/2}$  levels is now sufficiently removed to clearly define the lower of the two as belonging to the  $4s$  state, in agreement with experiment.

Before calculating the electric dipole transition rates between all these levels, we refined the CI mixing coefficients by making small adjustments to some diagonal elements of the Hamiltonian matrices, and then re-diagonalising the adjusted matrices. In this way, we were able to bring the calculated eigenvalue differences into agreement with the experimental energy separations. From past experience, we have found that, while the mixing coefficients are improved by this process, there is a tendency for the coefficients to be somewhat over-corrected. However, since most of the matrix corrections are quite small, and many of the levels are spectroscopically fairly pure, the principal effect of this fine-tuning process will be to allow the use of experimental energy separations, with some modifications to the interactions between levels in a limited number of cases.

In Table 3, we present our calculated transition rates in both length and velocity gauges for those  $4p\text{--}4d$  transitions for which experimental values are given by [9]. The corresponding results from the experimental determinations of [7,8] are also listed. Belmonte et al. [9] also give estimates of the uncertainties in their results, which they obtain not only from the customary standard deviation of experimental measurements, but also from a detailed and careful analysis of a range of other factors which could lead to uncertainties. As a result of this analysis, they are able to provide uncertainties, most of which lie in the 10%–20% range, with a small proportion having higher uncertainties. Table 3 quotes those uncertainties.

**Table 3.** A-values ( $10^8\text{ s}^{-1}$ ) for  $4p\text{--}4d$  transitions in Ar II.

Transition		This Work				
4p *	4d	Wavelength (nm)	$A_l$	$A_v$	[9]	[7] [8]
$4p^0_{5/2}$	$4F_{3/2}$	319.423	0.074	0.066	$0.086\ (12\%)^{\dagger}$	0.236
$4p^0_{1/2}$	$4F_{3/2}$	326.357	0.105	0.094	0.13 (11%)	0.155 0.348
$4p^0_{5/2}$	$4F_{7/2}$	326.899	0.0031	0.0026	0.002 (84%)	
$4p^0_{5/2}$	$4P_{5/2}$	313.902	0.625	0.551	0.49 (18%)	0.52 1.00
$4p^0_{3/2}$	$4P_{5/2}$	316.967	0.524	0.455	0.43 (18%)	0.49 0.817
$4p^0_{5/2}$	$4P_{3/2}$	318.104	0.469	0.421	0.36 (12%)	0.37 0.627
$4p^0_{3/2}$	$4P_{1/2}$	324.369	1.18	1.05	1.07 (11%)	1.1 1.99
$4p^0_{1/2}$	$4P_{3/2}$	324.980	0.763	0.678	0.60 (14%)	0.63 1.00
$4p^0_{1/2}$	$4P_{1/2}$	328.170	0.459	0.405	0.41 (11%)	0.42 0.733
$4D^0_{3/2}$	$4D_{1/2}$	384.152	0.258	0.235	0.19 (12%)	0.269 0.267
$4D^0_{5/2}$	$4D_{7/2}$	384.473	0.051	0.046	0.049 (17%)	0.048 0.047
$4D^0_{5/2}$	$4D_{5/2}$	382.681	0.325	0.297	0.30 (15%)	0.281 0.345
$4D^0_{5/2}$	$4D_{3/2}$	379.938	0.221	0.199	0.22 (13%)	0.17 0.23
$2D^0_{3/2}$	$2P_{3/2}$	320.432	0.176	0.171	0.24 (12%)	0.402
$2D^0_{3/2}$	$2P_{1/2}$	327.332	0.172	0.158	0.20 (16%)	0.371
$2D^0_{5/2}$	$4D_{1/2}$	403.138	0.039	0.033	0.07 (60%)	0.075
$2D^0_{5/2}$	$2D_{5/2}$	295.539	0.325	0.297	0.19 (13%)	

Table 3. Cont.

Transition		This Work					
$2D_{5/2}^o$	$2D_{5/2}$	301.448	0.036	0.034	0.039 (19%)		
$2P_{3/2}^o$	$4F_{3/2}$	383.017	0.0008	0.0009	0.042 (27%)		
$2P_{3/2}^o$	$2F_{5/2}$	365.528	0.326	0.316	0.37 (13%)		0.232
$2P_{3/2}^o$	$2P_{3/2}$	329.364	0.899	0.847	0.59 (17%)		1.73
$2P_{1/2}^o$	$2P_{1/2}$	330.723	1.44	1.38	1.43 (11%)		3.35
$2P_{3/2}^o$	$2P_{1/2}$	336.658	0.271	0.255	0.24 (15%)		0.409
$2S_{1/2}^o$	$2P_{3/2}$	338.853	0.761	0.795	0.81 (12%)		1.91
$2S_{1/2}^o$	$2D_{3/2}$	316.137	0.370	0.368	0.35 (45%)		1.837
$4p'$	$4d'$	Wavelength (nm)	$A_l$	$A_v$	[9]	[7]	[8]
$2F_{5/2}^o$	$2F_{5/2}$	335.092	0.929	0.815	0.90 (13%)		1.48
$2F_{7/2}^o$	$2F_{5/2}$	336.552	0.073	0.066	0.075 (18%)		0.131
$2F_{7/2}^o$	$2F_{7/2}$	337.644	0.860	0.764	0.74 (13%)		1.49
$2P_{3/2}^o$	$2P_{3/2}$	366.044	0.741	0.693	0.73 (11%)		2.22
$2P_{3/2}^o$	$2P_{1/2}$	367.101	0.199	0.191	0.23 (31%)		0.709
$2P_{1/2}^o$	$2D_{3/2}$	368.006	0.031	0.007	0.59 (19%)		1.15
$2P_{3/2}^o$	$2S_{1/2}$	302.675	0.600	0.679	1.03 (21%)		
$2D_{3/2}^o$	$2D_{5/2}$	379.659	0.141	0.132	0.18 (23%)		0.250
$2D_{5/2}^o$	$2D_{5/2}$	380.317	0.978	0.902	0.89 (12%)		1.53
$2D_{3/2}^o$	$2P_{3/2}$	381.902	0.244	0.172	0.15 (49%)		0.0036
$2D_{5/2}^o$	$2P_{3/2}$	382.567	0.384	0.356	0.33 (55%)		0.756

\*  $nl$  denotes  $3p^4(^3P)nl$ ;  $nl'$  denotes  $3p^4(^1D)nl$ ; † estimated uncertainty.

#### 4. Discussion

The accuracy of theoretical energy differences and transition rates can only be estimated: there is no monotonic convergence of these quantities, even as the wave functions are systematically improved. Instead, it is necessary to refer to a number of indicators of accuracy, as explained in [16]. These indicators include a comparison between calculated and experimental energy levels, the convergence of results as the wave functions are improved, the degree of agreement between different forms of the transition rates (typically length and velocity), comparison with other calculations, and of course, comparison with experiment.

In this work, we have adopted our fine-tuning process, which ensures that we are using accurate transition energies and that the CI mixing coefficients are as accurate as we can obtain within the limitations of our finite configuration lists. We have not undertaken a sequence of calculations of different complexity, as would be necessary if we were to establish the degree of convergence of the results, but as many of the levels are fairly pure spectroscopically, we do not believe that this would have a major influence on the level of accuracy achieved. There are no other theoretical transition rates available in the literature for these transitions. That leaves two major factors to be taken into account in assessing the accuracy of our calculations.

It can be observed from Table 3 that the length and velocity forms of our calculated transition rates differ fairly consistently by about 10%–15%, the length form mostly giving the larger of the two. This discrepancy is an indication of either insufficient treatment of electron correlation in the  $3p^4$  core, or (given the strong state-dependency of the valence orbitals) insufficient flexibility in the form of the radial functions of the valence orbitals; that is, there may be too few basis functions in the expansions (4).

However, in spite of these limitations, the important thing to note is the comparison between our calculated  $A$ -values and the experimental values recently determined by Belmonte et al. [9]. For most transitions listed in Table 3, our results lie quite close to the experimental values of [9], bearing in mind the uncertainty of both sets of results. Similar good agreement is found with the experimental results of [7], which are the values recommended in the critical compilation of [4].

By contrast, the experimental results of Rudko and Tang [8] are substantially different from both the recent experimental values and our calculations.

In view of these considerations, we would anticipate that for most of the transitions listed in Table 3, our results are accurate to about 20%–25%, or better.

## 5. Conclusions

We have undertaken a substantial calculation of 4p–4d transitions in Ar II, using a systematic configuration interaction process. These results provide the only theoretical corroboration with which the recent experimental results given in [9] and in other earlier work may be compared. It is clear that our calculations substantially support the results of Belmonte et al. [9], and of Bennett et al. [7] (where comparison is possible), but are in substantial disagreement with the experimental data of Rudko and Tang [8] for many of the transitions considered here. However, until the recent work of [9], the only available data for the doublet transitions was that of [8], and for those transitions, it is the values of [8] which are quoted in the NIST tabulations [6]. We therefore recommend that—where possible—the transition rates of [9] are adopted instead.

**Conflicts of Interest:** The author declares no conflict of interest.

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Review

# Multiconfiguration Dirac-Hartree-Fock Calculations with Spectroscopic Accuracy: Applications to Astrophysics

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Academic Editor: Joseph Reader

Received: 31 January 2017; Accepted: 7 April 2017; Published: 14 April 2017

**Abstract:** Atomic data, such as wavelengths, spectroscopic labels, broadening parameters and transition rates, are necessary for many applications, especially in plasma diagnostics, and for interpreting the spectra of distant astrophysical objects. The experiment with its limited resources is unlikely to ever be able to provide a complete dataset on any atomic system. Instead, the bulk of the data must be calculated. Based on fundamental principles and well-justified approximations, theoretical atomic physics derives and implements algorithms and computational procedures that yield the desired data. We review progress and recent developments in fully-relativistic multiconfiguration Dirac–Hartree–Fock methods and show how large-scale calculations can give transition energies of spectroscopic accuracy, i.e., with an accuracy comparable to the one obtained from observations, as well as transition rates with estimated uncertainties of a few percent for a broad range of ions. Finally, we discuss further developments and challenges.

**Keywords:** transition energies; lifetimes; transition rates; multiconfiguration Dirac-Hartree-Fock

**PACS:** 31.15.am; 32.30.Jc; 32.70.Cs

## 1. Introduction

Atomic data, such as wavelengths, spectroscopic labels, broadening parameters, excitation and transition rates, are necessary for many applications, especially in plasma diagnostics, and for interpreting laboratory and astrophysical spectra [1,2]. Plasma diagnostics are commonly applied to



measure the physical state of the plasma, e.g., temperatures, densities, ion and chemical abundances. Atomic databases, such as CHIANTI [3,4], are widely used for such diagnostic purposes. Their accuracy relies on a range of atomic rates, the main ones being electron collision rates and transition rates. For the solar corona, lines from highly charged iron ions, emitted in the extreme ultraviolet (EUV) and soft X-ray region, are commonly used for diagnostics, together with those from all other abundant elements. Atomic data and line identifications involving states of the lowest configurations of an ion are now relatively well known and observed. However, much less data are available for lines from higher configurations; one example is the lack of line identifications and rates for transitions from  $n = 4$  iron ions in the soft X-rays [5].

Line identification from observed spectra is a very difficult and challenging task. Different methods such as isoelectronic interpolation and extrapolation, perfected by Edlén [6], can be used, but the work is nowadays mostly done with the aid of calculated transition energies and simulated spectra. For calculated transition energies, or wavelengths, to be of practical use, they need to be very accurate with uncertainties of just a few mÅ, placing high demands on computational methodologies.

Transition rates and line ratios are needed for diagnostic purposes. Due to the almost complete lack of accurate experimental data for atoms a few times ionized or more, the bulk of the transition rates must be calculated. Not only the rates themselves should be provided, but also uncertainty estimates that can be propagated in plasma models for sensitivity analysis. Both accurate rates and uncertainty estimates pose a challenge, calling for methods for which computed properties can be monitored as the wave functions are systematically improved.

This review summarizes the results from recent accurate relativistic multiconfiguration calculations for lowly charged ions or more of astrophysical importance. Focus is on the transition energies and their uncertainties, but transition rates and the associated uncertainty estimates are also discussed. The astrophysical background is provided in the individual papers covered by the review. Neutral atoms and ions in the lowest charge states are not covered in the review.

## 2. Multiconfiguration Methods

Multiconfiguration methods are versatile and can, in principle, be applied to any atomic or ionic system [7]. Multiconfiguration methods generate approximate energies and wave functions for the each of the targeted states in a system. The wave functions can then be used to compute measurable quantities, such as transition rates, hyperfine structures or Landé  $g$ -factors [8]. Looking at strengths and weaknesses, multiconfiguration methods capture near degeneracies and valence-valence electron correlation very efficiently. They are however less good at accounting for core-core correlation, and here, perturbative methods relying on a complete orbital basis have advantages. Work has been done to combine multiconfiguration and perturbative methods in different ways [9–12], a development that will open up accurate results also for more complex systems [13].

The relativistic multiconfiguration method, to be described below, is implemented in the GRASP2K program package [14]. The package is generally available and utilizes a message passing interface (MPI) for the most time-consuming programs, allowing for large-scale computing on parallel computers.

### 2.1. Multiconfiguration Dirac-Hartree-Fock

Atomic calculations are based on a Hamiltonian. In the relativistic multiconfiguration Dirac-Hartree-Fock (RMCDHF) method [7,15], as implemented in the GRASP2K package, the Hamiltonian is taken as the Dirac-Coulomb Hamiltonian:

$$H_{DC} = \sum_{i=1}^N \left( c \boldsymbol{\alpha}_i \cdot \mathbf{p}_i + (\beta_i - 1)c^2 + V_{\text{nuc}}(r_i) \right) + \sum_{i>j}^N \frac{1}{r_{ij}}, \quad (1)$$

where  $V_{\text{nuc}}(r_i)$  is the nuclear potential modelled from an extended nuclear charge distribution,  $r_{ij}$  is the distance between electrons  $i$  and  $j$  and  $\alpha$  and  $\beta$  are the Dirac matrices. Wave functions  $\Psi(\gamma PJM_J)$  for fine-structure states labelled by parity,  $P$ , and angular quantum numbers,  $JM_J$ , are expanded in antisymmetrized and coupled configuration state functions (CSFs):

$$\Psi(\gamma PJM_J) = \sum_{j=1}^{N_{\text{CSF}}} c_j \Phi(\gamma_j PJM_J). \quad (2)$$

The labels  $\{\gamma_j\}$  denote the information of the CSFs, such as orbital occupancy and subshell quantum numbers in the angular momentum coupling tree. The CSFs are built from products of one-electron orbitals, having the general form:

$$\psi_{n\kappa,m}(\mathbf{r}) = \frac{1}{r} \begin{pmatrix} P_{n\kappa}(r)\chi_{\kappa,m}(\theta, \varphi) \\ iQ_{n\kappa}(r)\chi_{-\kappa,m}(\theta, \varphi) \end{pmatrix}, \quad (3)$$

where  $\chi_{\pm\kappa,m}(\theta, \varphi)$  are two-component spin-orbit functions and where the radial functions are numerically represented on a logarithmic grid. The selection of the CSFs depends on the atomic system at hand and is described in Section 3.

In applications, one often seeks to determine energies and wave functions for a number, sometimes up to a few hundred, of targeted states. This is most conveniently done in the extended optimal level (EOL) scheme [16]. Given initial estimates of the radial functions, the energies  $E$  and expansion coefficients  $c = (c_1, \dots, c_M)^t$  for the targeted states are obtained as solutions to the relativistic configuration interaction (RCI) problem:

$$Hc = Ec, \quad (4)$$

where  $H$  is the RCI matrix of dimension  $M \times M$  with elements:

$$H_{ij} = \langle \Phi(\gamma_i PJM_J) | H_{\text{DC}} | \Phi(\gamma_j PJM_J) \rangle. \quad (5)$$

Once the expansion coefficients have been determined, the radial functions  $\{P_{n\kappa}(r), Q_{n\kappa}(r)\}$  are improved by solving a set of differential equations that results from applying the variational principle on a weighted energy functional of the targeted states together with additional terms needed to preserve the orthonormality of the orbitals. Appropriate boundary conditions for the radial orbitals exclude undesired negative-energy solutions [15]. The RCI problem and the solution of the differential equations are iterated until the radial orbitals and the energy are converged to a specified tolerance.

## 2.2. Configuration Interaction

The RMCDHF calculations are used to generate an orbital basis. Given this basis, the final wave functions for the targeted states are obtained in RCI calculations based on the frequency dependent Dirac-Coulomb-Breit Hamiltonian:

$$H_{\text{DCB}} = H_{\text{DC}} - \sum_{i < j}^N \left[ \alpha_i \cdot \alpha_j \frac{\cos(\omega_{ij} r_{ij}/c)}{r_{ij}} + (\alpha_i \cdot \nabla)(\alpha_j \cdot \nabla) \frac{\cos(\omega_{ij} r_{ij}/c) - 1}{\omega_{ij}^2 r_{ij} / c^2} \right], \quad (6)$$

where  $\nabla$  is the gradient operator involving differentiation with respect to  $\mathbf{r}_{ij} = \mathbf{r}_i - \mathbf{r}_j$  and  $r_{ij} = |\mathbf{r}_{ij}|$  [17]. In the RCI calculations leading quantum electrodynamic (QED) effects, vacuum polarization and self-energy are also taken into account. RCI calculations require less computational effort than do RMCDHF calculations, and currently, expansions with millions of CSFs can be handled. The relativistic multiconfiguration and configuration interaction calculations go together and are referred to as RMCDHF/RCI calculations.

### 2.3. Managing Large Expansions

To manage large expansions, CSFs can a priori be divided into two groups, referred to as a zero- and first-order partitioning. The first group,  $P$ , with  $m$  elements ( $m \ll M$ ) contains CSFs that account for the major parts of the wave functions. The second group,  $Q$ , with  $M - m$  elements contains CSFs that represent minor corrections. Allowing interaction between CSFs in group  $P$ , interaction between CSFs in groups  $P$  and  $Q$  and diagonal interactions between CSFs in  $Q$  gives a matrix:

$$\begin{pmatrix} H^{(PP)} & H^{(PQ)} \\ H^{(QP)} & H^{(QQ)} \end{pmatrix}, \quad (7)$$

where  $H_{ij}^{(QQ)} = \delta_{ij} E_i^Q$ . The restriction of  $H^{(QQ)}$  to diagonal elements results in a huge reduction in the total number of matrix elements and the corresponding time for RCI calculations [12]. A similar reduction in computational time is obtained when constructing and solving the differential equations obtained from the weighted energy functional. Different computational strategies apply: RMCDHF calculations with limited interactions followed by RCI calculations with full interactions or RMCDHF calculations with limited interactions followed by RCI calculations with limited interaction, possibly with more CSFs in group  $P$ .

### 2.4. Labelling

In fully-relativistic calculations, quantum labels for the targeted states are obtained in  $jj$ -coupling. Most often, this wave function representation is not pure, i.e., there is no dominant CSF whose quantum numbers can be used to label a state in a proper way. Using the methods developed by Gaigalas and co-workers [18], the wave function representation in  $jj$ -coupling is transformed to an approximate representation in  $LSJ$ -coupling. This representation is normally more pure and better suited for labelling. One should be aware of the fact that even in  $LSJ$ -coupling, the labelling is not straight forward, and several components in the  $LSJ$ -coupling representation must be used in a recursive way to find unique labels [19,20]. Programs for transforming wave functions and assigning unique labels are important parts of the GRASP2K package [21].

### 2.5. Transition Properties

Given wave functions from RMCDHF/RCI calculations, transition properties, such as rates,  $A$ , line strengths,  $S$ , and weighted oscillator strengths,  $gf$ , between two states  $\gamma PJ$  and  $\gamma' P' J'$  are computed in terms of reduced matrix elements:

$$\langle \Psi(\gamma PJ) \| T^{(\text{EMK})} \| \Psi(\gamma' P' J') \rangle, \quad (8)$$

where the operator  $T^{(\text{EMK})}$  depends on the multipolarity, E1, M1, E2, M2, etc., of the transition. By including Bessel functions in the definition of the operator, GRASP2K accounts for more high-order effects than the usual transition operator used in non-relativistic calculations with Breit–Pauli corrections [15]. Inserting the CSF expansions for the wave functions, the reduced matrix element reduces to a sum over reduced matrix elements between CSFs. Using Racah algebra techniques, these matrix elements are finally obtained as sums over radial integrals [22,23]. The above procedure assumes that the two states  $\gamma PJ$  and  $\gamma' P' J'$  are built from the same set of orbitals. When this is not the case, e.g., when separate calculations have been done for the even and odd parity states, the representation of the wave functions are changed in such a way that the orbitals become biorthonormal [24,25], in which case the calculation continues along the lines above. For electric transitions, parameters can be computed in both length and velocity gauge [26], where the results in the length gauge are the preferred.

### 3. General Computational Methodology: The SD-MR Approach

Systematic calculations using multiconfiguration methods follow a determined scheme as described below. Details of the scheme are determined by the shell structure of the atom, the number of targeted states, the desired accuracy of the final results and the available computational resources. The atomic Hamiltonian is invariant with respect to space inversions, and there are no interactions between odd and even parity states. The odd and even parity states are thus often treated in separate sets of calculations. After validation for selected ions and states, computed transition energies and rates can be used to aid the analysis of unknown spectra.

#### 3.1. Multireference and Gross Features of the Wave Functions

For highly ionized systems, a natural starting point is the multireference set (MR). In this review, we define the MR as the set of configurations associated with the targeted states of a given parity together with important closely degenerate configurations. Applying rules for the coupling of angular momenta, the configurations in the MR give rise to a set of CSFs that account for the most important gross features of the wave functions. The expansion coefficients of the CSFs and the orbitals are determined in an initial RMCDHF calculation. The orbitals for the initial calculation are called spectroscopic orbitals. They are required to have the same node structure as hydrogenic orbitals, i.e., the node structure is determined by the principal quantum number. The spectroscopic orbitals are kept frozen in all subsequent calculations.

#### 3.2. Including Electron Correlation and Determining an Orbital Set

The initial approximation of the wave functions is improved by adding CSFs that account for electron correlation. Guided by a perturbative analysis, the CSFs are generated by the single (S) and double (D) multireference (SD-MR) active space method in which a number of configurations is obtained by SD substitutions of orbitals in the configurations of the MR with orbitals in an active set [7,8]. Again, applying rules for the coupling of angular momenta, the generated configurations give rise to the CSFs. Not all of these CSFs are important, and the CSFs are further required to be such that they interact (have non-zero Hamiltonian matrix elements) with the CSFs of the MR. The expansion coefficients of the CSFs and the radial parts of the orbitals in the active set are determined in RMCDHF calculations where, for large expansions, limited interactions are used.

The active set, often denoted by the number of orbitals with a specified symmetry, so that  $\{4s3p2d1f\}$  is a set with four  $s$  orbitals, three  $p$  orbitals, two  $d$  orbitals and one  $f$  orbital, is systematically enlarged one orbital layer at the time until the computed excitation energies and transition rates have converged to within some predetermined tolerance. For small systems, SD substitutions are done from all subshells of the configurations in the MR, and the generated CSFs account for valence-valence, core-valence and core-core electron correlation. For larger systems, it becomes necessary to define a core for which restrictions on the substitutions apply. In many cases, the SD-MR substitutions are restricted in such a way that there are only S substitutions from subshells that define a so-called active core. There may also be subshells deep down in the core for which there are no substitutions at all. CSFs obtained from S-MR substitutions from the active core together with SD-MR substitutions from the valence subshells account for valence-valence and core-valence correlation.

#### 3.3. Final Configuration Interaction Calculations Including the Breit Interaction and QED Effects

The frequency dependent Breit (transverse photon) interaction and leading QED effects are included in final RCI calculations. To account for higher order correlation effects, the MR is sometimes enlarged at this final step leading to larger expansions. Full interaction is normally used, although limited interactions have been shown effective for including core-valence and core-core effects in larger systems [12,27].

4. Excitation Energies

In this section, RMCDHF/RCI excitation energies are compared with observations for a range of systems in order to illustrate the predictive power of highly accurate calculations. Generally, there are enough observations to validate computational methodologies and to distinguish between different approaches.

4.1. Energies for  $2s^2 2p^n$ ,  $2s 2p^{n+1}$  and  $2p^{n+2}$  States in the B-, C-, N-, O- and F-Like Sequences

Excitation energies and E1, M1, E2, M2 transition rates between  $2s^2 2p^n$ ,  $2s 2p^{n+1}$  and  $2p^{n+2}$  states of ions in the B-, C-, N-, O- and F-like sequences were calculated using the RMCDHF/RCI and SD-MR method [28–32]. The range of ions, as well as the details of the calculations are summarized in Table 1. Calculations of Landé  $g_J$  factors, hyperfine structures and isotope shifts were done separately for ions in the Be-, B-, C- and N-like sequences [33,34].

**Table 1.** Multireference (MR), active set, number of generated configuration state functions (CSFs) ( $N_{CSFs}$ ) and the range of ions for the relativistic multiconfiguration Dirac-Hartree-Fock (RMCDHF) and relativistic configuration interaction (RCI) calculations of the boron-, carbon-, nitrogen-, oxygen- and fluorine-like sequences.

Configuration	MR for RMCDHF	MR for RCI	Active Set	$N_{CSFs}$
boron-like, N III to Zn XXVI				
$1s^2 2s^2 2p$	$1s^2 \{2s^2 2p, 2p^3\}$	$1s^2 \{2s^2 2p, 2p^3, 2s 2p 3d, 2p 3d^2\}$	$\{9s 8p 7d 6f 5g 3h 1i\}$	200 100
$1s^2 2p^3$	$1s^2 \{2s^2 2p, 2p^3\}$	$1s^2 \{2s^2 2p, 2p^3, 2s 2p 3d, 2p 3d^2\}$	$\{9s 8p 7d 6f 5g 3h 1i\}$	360 100
$1s^2 2s 2p^2$	$1s^2 2s 2p^2$	$1s^2 \{2s 2p^2, 2p^2 3d, 2s^2 3d, 2s 3d^2\}$	$\{9s 8p 7d 6f 5g 3h 1i\}$	300 100
carbon-like, F IV to Ni XXIII				
$1s^2 2s^2 2p^2$	$1s^2 \{2s^2 2p^2, 2p^4\}$	$1s^2 \{2s^2 2p^2, 2p^4, 2s 2p^2 3d, 2s^2 3d^2\}$	$\{8s 7p 6d 5f 4g 2h\}$	340 100
$1s^2 2p^4$	$1s^2 \{2s^2 2p^2, 2p^4\}$	$1s^2 \{2s^2 2p^2, 2p^4, 2s 2p^2 3d, 2s^2 3d^2\}$	$\{8s 7p 6d 5f 4g 2h\}$	340 100
$1s^2 2s 2p^3$	$1s^2 2s 2p^3$	$1s^2 \{2s 2p^3, 2p^3 3d, 2s^2 2p 3d, 2s 2p 3d^2\}$	$\{8s 7p 6d 5f 4g 2h\}$	1 000 100
nitrogen-like, F III to Kr XXX				
$1s^2 2s^2 2p^3$	$1s^2 \{2s^2 2p^3, 2p^5\}$	$1s^2 \{2s^2 2p^3, 2p^5, 2s 2p^3 3d, 2s^2 2p 3d^2\}$	$\{8s 7p 6d 5f 4g 1h\}$	698 100
$1s^2 2p^5$	$1s^2 \{2s^2 2p^3, 2p^5\}$	$1s^2 \{2s^2 2p^3, 2p^5, 2s 2p^3 3d, 2s^2 2p 3d^2\}$	$\{8s 7p 6d 5f 4g 1h\}$	382 100
$1s^2 2s 2p^4$	$1s^2 2s 2p^4$	$1s^2 \{2s 2p^4, 2p^4 3d, 2s^2 2p^2 3d, 2s 2p^2 3d^2\}$	$\{8s 7p 6d 5f 4g 1h\}$	680 100
oxygen-like, F II to Kr XXIX				
$1s^2 2s^2 2p^4$	$1s^2 \{2s^2 2p^4, 2p^6\}$	$1s^2 \{2s^2 2p^4, 2p^6, 2s 2p^4 3d\}$	$\{8s 7p 6d 5f 4g 3h\}$	709 690
$1s^2 2p^6$	$1s^2 \{2s^2 2p^4, 2p^6\}$	$1s^2 \{2s^2 2p^4, 2p^6, 2s 2p^4 3d\}$	$\{8s 7p 6d 5f 4g 3h\}$	67 375
$1s^2 2s 2p^5$	$1s^2 2s 2p^5$	$1s^2 \{2s 2p^5, 2p^5 3d, 2s^2 2p^3 3d\}$	$\{8s 7p 6d 5f 4g 3h\}$	702 892
fluorine-like, Si VI to WLXVI				
$1s^2 2s^2 2p^5$	$1s^2 2s^2 2p^5$	$1s^2 2s^2 2p^5$	$\{8s 7p 6d 5f 4g 3h 2i\}$	73 000
$1s^2 2s 2p^6$	$1s^2 2s 2p^6$	$1s^2 2s 2p^6$	$\{8s 7p 6d 5f 4g 3h 2i\}$	15 000

A trend for all atomic structure calculations, including RMCDHF/RCI, is that the accuracy of the excitation energies is, relatively speaking, lower for lowly charged ions and that the accuracy then increases as the effects of electron correlation diminish. For the highly charged ions, the situation is less clear. Often experimental excitation energies are associated with large uncertainties or missing altogether. The situation is illustrated in Tables 2 and 3 for the O-like sequence [31].

In Table 2, excitation energies in Ne III and Fe XIX from different calculations are compared with energies from observations. The most accurate calculations are the RMCDHF/RCI calculation [31] and the multireference second-order Möller-Plesset calculation (MRMP). For Ne III, the relative differences with observation for these two calculations are in the range of 0.2–0.4% (slightly worse for MRMP). For Fe XIX the relative errors go down by an order of magnitude, and now, the calculated energies are accurate enough to detect misidentifications or errors in observational data, but also to serve as a valuable tool for identifying new lines. The usefulness of computed energies is illustrated in Table 3 for Br XXVIII, where the RMCDHF/RCI and MRMP calculations clearly discriminate between

observed energies [35] and energies from semiempirical fits [36], being in better agreement with the latter. This suggests that there may be some calibration problems in relation to the observed energies [35].

**Table 2.** Excitation energies in  $\text{cm}^{-1}$  for O-like Ne and Fe from observations and different calculations. Relative errors in % for the calculated energies are shown in parenthesis.  $E_{obs}$  observation NIST [37],  $E_{RCI}$  energies from RMCDHF/RCI [31],  $E_{MRMP}$  energies from Möller-Plesset calculation (MRMP) [38],  $E_{MBPT}$  energies from many-body perturbation theory [39],  $E_{BP}$  energies from multiconfiguration Hartree-Fock-Breit-Pauli [19],  $E_{SS}$  energies from super structure [40],  $E_{MCDF}$  energies from RMCDHF [41] and  $E_{FAC}$  energies from RCI with the FAC code [42].

Ne III							
Level	J	$E_{obs}$	$E_{RCI}$	$E_{MRMP}$	$E_{MBPT}$	$E_{BP}$	$E_{SS}$
$2s^2 2p^4 \ ^3P$	2	0	0 (0.00)	0 (0.00)	0 (0.00)	0 (0.00)	0 (0.00)
	1	643	645 (0.31)	638 (0.77)	645 (0.31)	628 (2.33)	744 (15.70)
	0	921	923 (0.21)	912 (0.97)	926 (0.54)	899 (2.38)	1 069 (16.06)
$2s^2 2p^4 \ ^1D$	2	25 841	25 954 (0.43)	26 097 (0.99)	25 573 (1.03)	25 759 (0.31)	29 219 (13.07)
$2s^2 2p^4 \ ^1S$	0	55 753	56 058 (0.54)	55 772 (0.03)	55 459 (0.52)	55 382 (0.66)	72 484 (30.00)
$2s 2p^5 \ ^3P^o$	2	204 290	204 608 (0.15)	204 718 (0.20)	200 686 (1.76)	204 635 (0.16)	215 348 (5.41)
	1	204 873	205 200 (0.15)	205 297 (0.20)	201 276 (1.75)	205 236 (0.17)	216 008 (5.43)
	0	205 194	205 603 (0.19)	205 617 (0.20)	201 598 (1.75)	205 539 (0.16)	216 367 (5.44)
$2s 2p^5 \ ^1P^o$	1	289 479	290 315 (0.28)	290 703 (0.42)	288 219 (0.43)	291 659 (0.75)	315 511 (8.99)
Fe XIX							
Level	J	$E_{obs}$	$E_{RCI}$	$E_{MRMP}$	$E_{MBPT}$	$E_{MCDF}$	$E_{FAC}$
$2s^2 2p^4 \ ^3P$	2	0	0 (0.000)	0 (0.000)	0 (0.00)	0 (0.00)	0 (0.00)
	0	75 250	75 313 (0.083)	75 218 (0.042)	74 742 (0.67)	75 446 (0.26)	75 198 (0.06)
	1	89 441	89 434 (0.007)	89 251 (0.212)	87 559 (2.10)	88 791 (0.72)	88 821 (0.69)
$2s^2 2p^4 \ ^1D$	2	168 852	168 985 (0.078)	168 792 (0.035)	167 881 (0.57)	170 847 (1.18)	170 578 (1.02)
$2s^2 2p^4 \ ^1S$	0	325 140	325 417 (0.085)	324 949 (0.058)	321 124 (1.23)	326 536 (0.42)	325 421 (0.08)
$2s 2p^5 \ ^3P^o$	2	922 890	923 044 (0.016)	922 855 (0.003)	917 435 (0.59)	933 081 (1.10)	929 231 (0.68)
	1	984 740	984 920 (0.018)	984 791 (0.005)	978 242 (0.65)	995 006 (1.04)	991 246 (0.66)
	0	1030 020	1030 199 (0.017)	1029 992 (0.002)	1022 753 (0.70)	1039 692 (0.93)	1036 058 (0.58)
$2s 2p^5 \ ^1P^o$	1	1267 600	1268 093 (0.038)	1267 771 (0.013)	1258 927 (0.68)	1287 773 (1.59)	1282 914 (1.20)
$2p^6 \ ^1S$	0	2134 180	2134 958 (0.036)	2132 810 (0.064)	2120 211 (0.65)	2175 645 (1.94)	2160 701 (1.24)

**Table 3.** Excitation energies in  $\text{cm}^{-1}$  for O-like Br. Comparison between calculations, observations and semiempirical estimates.  $E_{obs}$  observation NIST [37] with original data from Kelly [35],  $E_{SE}$  semiempirical fit [36] and  $E_{RCI}$  energies from RMCDHF/RCI [31],  $E_{MRMP}$  energies from MRMP [38];  $\Delta E_1$ , difference between calculated energies and  $E_{obs}$ ;  $\Delta E_2$ , difference between calculated energies and  $E_{SE}$ . The calculations support energies from the semiempirical fit.

Level	J	$E_{obs}$	$E_{SE}$	$E_{RCI}$	$\Delta E_1$	$\Delta E_2$	$E_{MRMP}$	$\Delta E_1$	$\Delta E_2$
$2s^2 2p^4 \ ^3P$	2	0	0	0	0	0	0	0	0
	1	218 800	153 478	151 954	-66 846	-1524	15 2035	-66 765	-1443
	1	379 800	371 663	371 606	-8 194	-57	37 1858	-7 942	195
$2s^2 2p^4 \ ^1D$	2	483 040	470 699	470 643	-12 397	-56	47 0804	-12 236	105
$2s^2 2p^4 \ ^1S$	0	944 150	912 501	911 968	-32 182	-533	91 2282	-31 868	-219
$2s 2p^5 \ ^3P^o$	2		1 579 903	1 579 537		-366	1 580 945		1042
	1		1 755 028	1 755 196		168	1 756 684		1656
	0		1 986 274	1 985 784		-490	1 987 396		1122
$2s 2p^5 \ ^1P^o$	1		2 229 358	2 230 149		791	2 231 636		2278
$2p^6 \ ^1S$	0		3 573 416	3 575 415		1999	3 579 486		6070

Summarizing the mean relative errors in the excitation energies for the  $2s^2 2p^n$ ,  $2s 2p^{n+1}$  and  $2p^{n+2}$  states of B-, C-, N-, O- and F-like Fe from RCI calculations [28–32], we have 0.022% for B-like, 0.022% for C-like, 0.050% for N-like, 0.042% for O-like and 0.011% for F-like Fe.

#### 4.2. Energies of the $2s^2 2p^6$ and $2s^2 2p^5 3l$ States in the Ne-Like Sequence

The transitions connecting the  $2s^2 2p^5 3l$ ,  $l = 0, 1, 2$  configurations in Ne-like ions give rise to prominent lines in the spectra of many high temperature light sources. Some of these lines are considered for diagnostics of fusion plasmas. Excitation energies and E1, M1, E2, M2 transition rates between states of the above configurations in Ne-like Mg III and Kr XXVII sequences were calculated using the RMCDHF/RCI and SD-MR method [43]. The calculations were done based on expansions from SD substitutions from the  $2s^2 2p^6$  and  $2s^2 2p^5 3l$  configurations to active sets  $\{7s6p5d4f3g2h1i\}$ . The  $1s^2$  was kept as a closed core. Some triple substitutions were allowed to capture higher order electron correlation effects. In Table 4, the RMCDHF/RCI excitation energies are displayed for Ca XI and Fe XVII. In the same table, the energies are compared with energies from NIST, as well as from MRMP calculations by Ishikawa et al. [44]. Again, the table illustrates the situation when it comes to experiments. For many ions, the excitation energies of the lower states are known from experiments. For other ions, such as Ca XI, energies are only known for a few states. The correlation model from the RMCDHF/RCI calculations predicts the excitation energies extremely well for all of the calculated ions. For Fe XVII, the relative differences with observations are around 0.005%. Calculated energies with this accuracy aid line identification in spectra and can be used to validate previous observations. As can be seen from the table, the RMCDHF/RCI and MRMP calculations both do very well, but the latter lose some of the accuracy at the neutral end of the sequence.

In Table 4, also the *LSJ* composition is shown for each state. There are many states that are heavily mixed, with terms of almost the same weight. In these cases, labelling becomes difficult, and for many ions in the sequence, there are states that have the same leading term. Labeling is a general problem that needs considerable attention [21].

#### 4.3. Energies for Higher States in the B-, C-, N-, O-, F- and Ne-Like Sequences

In plasma modelling and diagnostics, it is important to provide atomic data for more than just the states of the lowest configurations. To meet this demand, the RMCDHF/RCI and SD-MR calculations for the B-, C-, N-, O-, F- and Ne-like sequences have been extended to hundreds of states in what we refer to as spectrum calculations [45–52]. The range of ions, the targeted configurations and the number of studied states for each sequence are summarized in Table 5. Calculations were done by parity, i.e., odd and even parity states were treated in separate sets of calculations. The targeted configurations define the MR, and the expansions were obtained by SD-MR substitutions from all subshells to increasing active sets of orbitals. In addition to excitation energies, E1, M1, E2 and M2 transition rates were calculated.

Spectrum calculations are challenging for different reasons. The active sets of orbitals often have to be large, since many states with different charge distributions should be represented. The large active sets lead to large CSF expansions, and typically, the number of CSFs are a few millions for each parity. Another challenge is to handle the labelling. With closely degenerate configurations, the states are often not pure, but need to be described by the leading *LSJ* composition. However, the *LSJ* composition depends on the details of the calculation and different calculation may lead to different compositions. Thus, it is not unusual that there are inconsistencies in labelling, making comparisons between different sets of calculations, as well as with observations difficult and time consuming.

**Table 4.** Excitation energies in  $\text{cm}^{-1}$  for Ne-like Ca and Fe from observations and different calculations. Relative errors in % for the calculated energies are shown in parenthesis.  $E_{obs}$  observation NIST [37],  $E_{RCI}$  energies from RMCDFH/RCI [43] and  $E_{MRMP}$  energies from MRMP [44].

Level	LSJ	Composition	$E_{obs}$	$E_{RCI}$	$E_{MRMP}$
Ca XI					
$2p^6$	$1S_0$	1.00	0	0	0
$2p^5 3s$	$3P_2^o$	0.99		2 801 989	2 801 819
$2p^5 3s$	$3P_1^o$	$0.62 + 0.38 \ ^1P_1^o$	2 810 900	2 810 834 (0.0023)	2 810 588 (0.011)
$2p^5 3s$	$3P_0^o$	0.99		2 831 800	2 831 670
$2p^5 3s$	$1P_1^o$	$0.62 + 0.38 \ ^3P_1^o$	2 839 900	2 839 662 (0.0084)	2 839 386 (0.018)
$2p^5 3p$	$3S_1$	0.92		2 953 791	2 953 594
$2p^5 3p$	$3D_2$	$0.68 + 0.24 \ ^1D_2$		2 978 410	2 977 968
$2p^5 3p$	$3D_3$	1.00		2 978 650	2 978 276
$2p^5 3p$	$3D_1$	$0.43 + 0.36 \ ^1P_1 + 0.20 \ ^3P_1$		2 986 908	2 986 513
$2p^5 3p$	$3P_2$	$0.65 + 0.34 \ ^1D_2$		2 993 760	2 993 336
$2p^5 3p$	$3D_1$	$0.54 + 0.40 \ ^1P_1$		3 007 301	3 006 932
$2p^5 3p$	$3P_0$	0.98		3 009 345	3 009 000
$2p^5 3p$	$1D_2$	$0.41 + 0.31 \ ^3D_2 + 0.27 \ ^3P_2$		3 016 749	3 016 378
$2p^5 3p$	$3P_1$	$0.68 + 0.24 \ ^1P_1$		3 017 175	3 016 845
$2p^5 3p$	$1S_0$	0.98		3 101 166	3 098 308
$2p^5 3d$	$3P_0^o$	0.99		3 196 075	3 195 830
$2p^5 3d$	$3P_1^o$	0.95	3 199 300	3 199 045 (0.0080)	3 198 902 (0.012)
$2p^5 3d$	$3P_2^o$	0.85		3 205 278	3 205 169
$2p^5 3d$	$3F_4^o$	1.00		3 208 351	3 208 165
$2p^5 3d$	$3F_3^o$	$0.72 + 0.23 \ ^1F_3^o$		3 212 392	3 212 144
$2p^5 3d$	$3F_2^o$	$0.53 + 0.29 \ ^1D_2^o + 0.18 \ ^3D_2^o$		3 219 655	3 219 428
$2p^5 3d$	$3D_3^o$	$0.55 + 0.41 \ ^1F_3^o$		3 224 394	3 224 078
$2p^5 3d$	$3D_1^o$	0.89	3 239 700	3 239 502 (0.0061)	3 239 308 (0.012)
$2p^5 3d$	$3F_2^o$	$0.47 + 0.38 \ ^1D_2^o + 0.14 \ ^3D_2^o$		3 244 348	3 244 161
$2p^5 3d$	$3D_2^o$	$0.58 + 0.27 \ ^1D_2^o + 0.14 \ ^3P_2^o$		3 248 017	3 247 805
$2p^5 3d$	$3D_3^o$	$0.40 + 0.35 \ ^1F_3^o + 0.24 \ ^3F_3^o$		3 248 345	3 248 099
$2p^5 3d$	$1P_1^o$	0.91	3 284 300	3 284 444 (0.0044)	3 283 473 (0.025)
Fe XVII					
$2p^6$	$1S_0$	1.00	0	0	0
$2p^5 3s$	$3P_2^o$	1.00	5 849 490	5 849 108 (0.0065)	5 848 891 (0.0102)
$2p^5 3s$	$1P_1^o$	$0.54 + 0.45 \ ^3P_1$	5 864 760	5 864 469 (0.0049)	5 864 138 (0.0106)
$2p^5 3s$	$3P_0^o$	1.00	5 951 478	5 951 003 (0.0079)	5 950 877 (0.0100)
$2p^5 3s$	$3P_1^o$	$0.54 + 0.45 \ ^1P_1$	5 961 022	5 960 633 (0.0065)	5 960 410 (0.0102)
$2p^5 3p$	$3S_1$	$0.80 + 0.17 \ ^3P_1$	6 093 568	6 093 573 (0.0000)	6 093 209 (0.0058)
$2p^5 3p$	$3D_2$	$0.58 + 0.30 \ ^1D_2 + 0.12 \ ^3P_2$	6 121 756	6 121 769 (0.0002)	6 121 253 (0.0082)
$2p^5 3p$	$3D_3$	1.00	6 134 815	6 134 794 (0.0003)	6 134 360 (0.0074)
$2p^5 3p$	$1P_1$	$0.51 + 0.25 \ ^3D_1 + 0.19 \ ^3P_1$	6 143 897	6 143 898 (0.0000)	6 143 431 (0.0075)
$2p^5 3p$	$3P_2$	$0.67 + 0.32 \ ^1D_2$	6 158 540	6 158 481 (0.0009)	6 158 010 (0.0086)
$2p^5 3p$	$3P_0$	0.94	6 202 620	6 202 542 (0.0012)	6 202 238 (0.0061)
$2p^5 3p$	$3D_1$	$0.67 + 0.31 \ ^1P_1$	6 219 266	6 219 185 (0.0013)	6 218 795 (0.0075)
$2p^5 3p$	$3P_1$	$0.63 + 0.17 \ ^1P_1 + 0.13 \ ^3S_1$	6 245 490	6 245 346 (0.0023)	6 245 018 (0.0075)
$2p^5 3p$	$3D_2$	$0.41 + 0.38 \ ^1D_2 + 0.21 \ ^3P_2$	6 248 530	6 248 390 (0.0022)	6 248 024 (0.0080)
$2p^5 3p$	$1S_0$	0.93	6 353 356	6 353 605 (0.0039)	6 351 136 (0.0349)
$2p^5 3d$	$3P_0^o$	0.99	6 464 095	6 463 913 (0.0028)	6 463 611 (0.0074)
$2p^5 3d$	$3P_1^o$	0.91	6 471 233	6 471 519 (0.0044)	6 471 317 (0.0012)
$2p^5 3d$	$3P_2^o$	$0.72 + 0.18 \ ^3D_2^o$	6 486 440	6 486 166 (0.0042)	6 485 977 (0.0071)
$2p^5 3d$	$3F_4^o$	1.00	6 487 000	6 486 745 (0.0039)	6 486 514 (0.0074)
$2p^5 3d$	$3F_3^o$	$0.65 + 0.29 \ ^1F_3^o$	6 492 924	6 492 689 (0.0036)	6 492 387 (0.0082)
$2p^5 3d$	$1D_2^o$	$0.41 + 0.35 \ ^3F_2^o + 0.24 \ ^3D_2^o$	6 506 808	6 506 561 (0.0037)	6 506 276 (0.0081)
$2p^5 3d$	$3D_3^o$	$0.64 + 0.34 \ ^1F_3^o$	6 515 479	6 515 276 (0.0031)	6 514 936 (0.0083)
$2p^5 3d$	$3D_1^o$	$0.74 + 0.20 \ ^1P_1^o$	6 552 221	6 552 697 (0.0072)	6 552 491 (0.0041)
$2p^5 3d$	$3F_2^o$	$0.63 + 0.29 \ ^1D_2^o$	6 594 617	6 594 260 (0.0054)	6 594 099 (0.0078)
$2p^5 3d$	$3D_2^o$	$0.50 + 0.27 \ ^3P_2^o + 0.21 \ ^1D_2^o$	6 601 210	6 600 855 (0.0053)	6 600 688 (0.0079)
$2p^5 3d$	$1F_3^o$	$0.37 + 0.33 \ ^3F_3^o + 0.30 \ ^3D_3^o$	6 605 469	6 605 078 (0.0059)	6 604 858 (0.0092)
$2p^5 3d$	$1P_1^o$	$0.78 + 0.18 \ ^3D_1^o$	6 660 894	6 661 101 (0.0031)	6 660 232 (0.0099)



**Table 5.** Sequence, ions and targeted configurations for the RMCDFH/RCI calculations.  $N$  is the number of studied states for each ion. In the table,  $l = 0, 1, 2, l' = 0, 1, 2, 3, l'' = 0, \dots, n - 1$ .

Sequence	Ions	Configurations	$N$	Ref.
B-like	Si, Ti-Cu	$2s^2 2p, 2s 2p^2, 2p^3, 2s^2 3l, 2s 2p 3l, 2p^2 3l, 2s^2 4l', 2s 2p 4l', 2p^2 4l'$	291	[45]
B-like	Na	$2s^2 2p, 2s 2p^2, 2p^3, 2s^2 3l, 2s 2p 3l, 2p^2 3l, 2s^2 4l', 2s 2p 4l'$	133	[46]
C-like	Ar-Zn	$2s^2 2p^2, 2s 2p^3, 2p^4, 2s^2 2p 3l, 2s 2p^2 3l, 2p^3 3l, 2s^2 2p 4l'$	262	[47]
N-like	Cr, Fe, Ni, Zn	$2s^2 2p^3, 2s 2p^4, 2p^5, 2s^2 2p^2 3l, 2s 2p^3 3l, 2p^4 3l$	272	[48]
N-like	Ar-Zn	$2s^2 2p^3, 2s 2p^4, 2p^5, 2s^2 2p^2 3l, 2s 2p^3 3l, 2p^4 3l, 2s^2 2p^2 4l'$	359	[49]
O-like	Cr-Zn	$2s^2 2p^4, 2s 2p^5, 2p^6, 2s^2 2p^3 3l, 2s 2p^4 3l$	200	[50]
F-like	Cr-Zn	$2s^2 2p^5, 2s 2p^6, 2s^2 2p^4 3l, 2s 2p^5 3l, 2p^6 3l, 2s^2 2p^4 4l'$	200	[51]
Ne-like	Cr-Kr	$2s^2 2p^6, 2s 2p^6 3l, 2s^2 2p^5 4l, 2s 2p^6 4l, 2s^2 2p^5 5l'', 2s^2 2p^5 6l''$	201	[52]

For many ions, excitation energies for lower lying states are known from observations. Going higher, comparatively less data are available, and these are often associated with large uncertainties. The situation is well illustrated for C-like Fe, and in Table 6, the RMCDFH/RCI excitation energies by Ekman et al. [47] are compared with observations. Due to near degeneracies, many states have the same leading  $LSJ$  term. In these cases, labelling can be done either by giving the leading terms in the composition or, more simply, introducing an additional index  $A$  and  $B$  to separate the states. For the 20 first states belonging to the  $n = 2$  configurations, observations are available from the NIST [37] and CHIANTI databases [3,4]. There is an agreement between the RMCDFH/RCI and relativistic many body calculations (RMBPT) by Gu [53] and observations at the 0.028–0.032% level (slightly worse for RMBPT). The RCI calculation using the Flexible Atomic Code (FAC) [42] is less accurate. For the higher lying states, experimental data are sparse. In many cases, there is excellent agreement between observations and calculations also for these states, but in some cases, there are obvious disagreements. For State Number 36, the excitation energy from NIST and CHIANTI disagree, and the calculations by Ekman et al. and Gu support the energy from the CHIANTI database. For State 54, all calculations agree, but differ markedly from the energies given by NIST and CHIANTI.

**Table 6.** Energies in  $\text{cm}^{-1}$  for levels in Fe XXI.  $E_{RCI}$  energies from RMCDFH/RCI calculations [47],  $E_{RMBPT}$  energies from RMBPT [53],  $E_{FAC}$  energies from RCI calculations with FAC [42],  $E_{NIST}$  NIST recommended values [37] and  $E_{CHI}$  observed energies from the CHIANTI database [3,4].

No.	Level	$E_{RCI}$	$E_{RMBPT}$	$E_{FAC}$	$E_{NIST}$	$E_{CHI}$
1	$2s^2 2p^2 \ ^3P_0$	0	0	0	0	0
2	$2s^2 2p^2 \ ^3P_1$	73 864	73 867	73 041	73 851	73 851
3	$2s^2 2p^2 \ ^3P_2$	117 417	117 372	117 146	117 354	117 367
4	$2s^2 2p^2 \ ^1D_2$	244 751	244 581	245 710	244 561	244 568
5	$2s^2 2p^2 \ ^1S_0$	372 137	372 261	373 060	371 980	371 744
6	$2s 2p^3 \ ^5S_2$	486 584	487 683	479 658	486 950	486 991
7	$2s 2p^3 \ ^3D_1$	776 775	777 005	779 724	776 690	776 685
8	$2s 2p^3 \ ^3D_2$	777 404	777 655	779 963	777 340	777 367
9	$2s 2p^3 \ ^3D_3$	803 618	803 869	805 768	803 540	803 553
10	$2s 2p^3 \ ^3P_0$	916 444	916 773	920 272	916 330	916 333
11	$2s 2p^3 \ ^3P_1$	925 074	925 408	928 822	924 920	924 920
12	$2s 2p^3 \ ^3P_2$	942 621	942 986	946 135	942 430	942 364
13	$2s 2p^3 \ ^3S_1$	1 096 019	1 095 820	1 105 578	1 095 670	1 095 679
14	$2s 2p^3 \ ^1D_2$	1 127 672	1 127 460	1 137 533	1 127 240	1 127 250
15	$2s 2p^3 \ ^1P_1$	1 261 577	1 261 240	1 272 627	1 261 140	1 260 902
16	$2p^4 \ ^3P_2$	1 646 437	1 646 467	1 657 411	1 646 300	1 646 409
17	$2p^4 \ ^3P_0$	1 735 823	1 735 813	1 747 301	1 735 700	1 735 715
18	$2p^4 \ ^3P_1$	1 740 623	1 740 707	1 750 848	1 740 500	1 740 453
19	$2p^4 \ ^1D_2$	1 817 786	1 817 362	1 832 102	1 817 100	1 817 041
20	$2p^4 \ ^1S_0$	2 048 512	2 047 850	2 066 463	2 048 200	2 048 056
21	$2s^2 2p 3s \ ^3P_0$	7 663 283	7 664 054	7 654 119		
22	$2s^2 2p 3s \ ^3P_1$	7 671 971	7 672 703	7 663 398		7 661 883

Table 6. Cont.

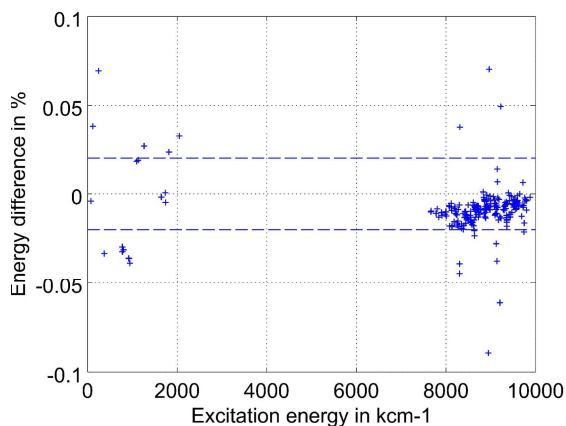
No.	Level	$E_{RCI}$	$E_{RMBPT}$	$E_{FAC}$	$E_{NIST}$	$E_{CHI}$
23	$2s^2 2p 3s^3 P_2$	7 780 298	7 781 147	7 770 895		
24	$2s^2 2p 3s^1 P_1$	7 803 764	7 804 419	7 796 397		
25	$2s^2 2p 3p^3 D_1$	7 841 903	7 842 922	7 834 847		
26	$2s^2 2p 3p^3 P_1 : A$	7 898 154	7 898 974	7 891 978		
27	$2s^2 2p 3p^3 D_2$	7 901 553	7 902 378	7 895 497		
28	$2s^2 2p 3p^3 P_0$	7 914 849	7 915 811	7 909 434		7 915 463
29	$2s^2 2p 3p^3 P_1 : B$	7 983 446	7 984 350	7 977 011		
30	$2s^2 2p 3p^3 D_3$	7 994 588	7 995 388	7 987 318		
31	$2s^2 2p 3p^3 S_1$	8 004 987	8 005 793	7 998 341		
32	$2s^2 2p 3p^3 P_2$	8 007 326	8 008 319	8 002 052		
33	$2s^2 2p 3p^1 D_2$	8 068 537	8 069 071	8 065 382		
34	$2s^2 2p 3d^3 F_2$	8 078 540	8 079 119	8 072 911		8 074 160
35	$2s 2p^2 (4P) 3s^5 P_1$	8 080 551	8 082 001	8 070 805		
36	$2s^2 2p 3d^3 F_3$	8 116 048	8 116 480	8 111 336	8 101 400	8 118 008
37	$2s^2 2p 3d^3 P_2 : A$	8 121 922	8 122 529	8 118 025		8 124 085
38	$2s^2 2p 3p^1 S_0$	8 128 645	8 129 396	8 126 192		8 143 710
39	$2s 2p^2 (4P) 3s^5 P_2$	8 131 973	8 133 460	8 121 258		
40	$2s^2 2p 3d^3 D_1$	8 139 290	8 140 735	8 135 992	8 140 000	8 141 785
41	$2s 2p^2 (4P) 3s^5 P_3$	8 181 331	8 182 599	8 170 876		
42	$2s 2p^2 (4P) 3s^5 P_0$	8 182 172	8 182 844	8 179 292		8 180 254
43	$2s^2 2p 3d^3 F_4$	8 202 073	8 202 670	8 195 771		
44	$2s^2 2p 3d^1 D_2$	8 208 705	8 209 597	8 204 329		
45	$2s 2p^2 (4P) 3s^5 P_1$	8 222 156	8 222 948	8 217 390		
46	$2s^2 2p 3d^3 D_3$	8 230 918	8 231 868	8 227 144	(8 195 000)	8 229 642
47	$2s^2 2p 3d^3 P_2 : B$	8 245 453	8 246 428	8 241 436	8 230 900	8 229 642
48	$2s^2 2p 3d^3 P_1$	8 245 737	8 247 075	8 241 557		
49	$2s^2 2p 3d^3 P_0$	8 247 732	8 249 164	8 243 033		
50	$2s 2p^2 (4P) 3p^5 D_0$	8 267 963	8 269 220	8 259 742		
51	$2s 2p^2 (4P) 3p^5 D_1$	8 270 558	8 272 088	8 262 373		
52	$2s 2p^2 (4P) 3s^5 P_2$	8 274 704	8 275 427	8 270 235		
53	$2s^2 2p 3d^1 F_3$	8 300 618	8 301 128	8 301 379	8 313 600	
54	$2s^2 2p 3d^1 P_1$	8 303 730	8 307 428	8 305 376	8 293 900	8 293 791
55	$2s 2p^2 (4P) 3p^5 D_2$	8 305 917	8 309 162	8 297 457		
56	$2s 2p^2 (4P) 3p^5 S_1$	8 312 499	8 309 359	8 300 070		
57	$2s 2p^2 (4P) 3p^5 P_1$	8 349 456	8 350 857	8 342 324		8 350 731
58	$2s 2p^2 (4P) 3p^5 D_3$	8 351 775	8 353 277	8 342 522		
59	$2s 2p^2 (4P) 3p^5 P_2$	8 352 117	8 353 731	8 343 801		
60	$2s 2p^2 (4P) 3p^5 D_1$	8 379 967	8 380 890	8 373 689		8 376 741
61	$2s 2p^2 (4P) 3p^5 P_3$	8 388 634	8 390 292	8 380 281		
62	$2s 2p^2 (4P) 3p^5 D_4$	8 399 557	8 401 039	8 390 478		
63	$2s 2p^2 (4P) 3p^5 D_2$	8 410 077	8 411 182	8 404 386		
64	$2s 2p^2 (2D) 3s^5 D_1$	8 420 588	8 421 426	8 420 569		
65	$2s 2p^2 (2D) 3s^5 D_2$	8 428 405	8 429 248	8 428 172		
66	$2s 2p^2 (2D) 3s^5 D_3$	8 440 926	8 441 758	8 437 725		
67	$2s 2p^2 (4P) 3p^5 P_0$	8 442 813	8 443 776	8 438 241		
68	$2s 2p^2 (4P) 3p^5 S_2$	8 443 646	8 445 037	8 440 027		
69	$2s 2p^2 (4P) 3p^5 D_3$	8 462 365	8 463 510	8 456 502		
70	$2s 2p^2 (4P) 3p^5 P_1$	8 467 690	8 468 680	8 462 413		
71	$2s 2p^2 (4P) 3p^5 P_2$	8 470 871	8 471 913	8 466 158		
72	$2s 2p^2 (4P) 3d^5 F_1$	8 480 620	8 481 735	8 471 575		
73	$2s 2p^2 (4P) 3d^5 F_2$	8 488 782	8 489 971	8 479 898		8 486 331
74	$2s 2p^2 (2D) 3s^5 D_2$	8 496 990	8 497 512	8 498 660		
75	$2s 2p^2 (4P) 3d^5 F_3 : A$	8 506 111	8 507 343	8 497 311		8 511 385
76	$2s 2p^2 (4P) 3d^5 F_4$	8 544 575	8 545 928	8 534 831		
77	$2s 2p^2 (2P) 3s^5 P_1$	8 545 485	8 546 507	8 544 603		
78	$2s 2p^2 (2P) 3s^5 P_0$	8 553 885	8 554 716	8 545 420		
79	$2s 2p^2 (4P) 3d^5 D_0$	8 554 798	8 555 918	8 546 365		
80	$2s 2p^2 (4P) 3d^5 D_1$	8 555 297	8 556 534	8 547 553		
81	$2s 2p^2 (4P) 3d^5 D_2$	8 555 491	8 556 850	8 558 611		
82	$2s 2p^2 (4P) 3d^5 F_3 : B$	8 561 662	8 562 969	8 552 789		8 564 535
83	$2s 2p^2 (4P) 3d^5 P_2$	8 581 274	8 582 755	8 576 965		8 575 780

Table 6. Cont.

No.	Level	$E_{RCI}$	$E_{RMBPT}$	$E_{FAC}$	$E_{NIST}$	$E_{CHI}$
84	$2s2p^2(4P)3d^5F_5$	8 586 636	8 588 014	8 577 151		
85	$2s2p^2(4P)3d^5D_4$	8 597 735	8 599 106	8 588 388		
86	$2s2p^2(2D)3p^3F_2$	8 606 110	8 606 654	8 607 148		8 605 427
87	$2s2p^2(4P)3d^3F_2$	8 611 432	8 611 843	8 608 283		
88	$2s2p^2(4P)3d^5P_3$	8 619 312	8 620 847	8 611 148		
			:			
228	$2p^3(^2P)3d^3F_4$	9 735 480	9 736 111	9 746 771		
229	$2p^3(^2P)3d^3P_1$	9 740 645	9 742 719	9 754 847		
230	$2p^3(^2P)3d^3P_0$	9 748 184	9 749 774	9 758 859		
231	$2p^3(^2P)3d^3P_2 : B$	9 757 890	9 758 107	9 770 963		
232	$2p^3(^2P)3d^3D_1$	9 765 663	9 766 056	9 781 499		
233	$2p^3(^2P)3d^3D_3$	9 780 738	9 781 044	9 794 389		
234	$2p^3(^2P)3d^1F_3$	9 800 368	9 800 742	9 819 206		
235	$2p^3(^2P)3d^3D_2$	9 800 852	9 801 738	9 819 939		
236	$2p^3(^2P)3d^1P_1$	9 879 471	9 879 655	9 902 175		
237	$2s^22p4s^3P_0$	10 368 077		10 362 393		
238	$2s^22p4s^3P_1$	10 371 121		10 365 585	10 380 000	
239	$2s^22p4p^3D_1$	10 442 616		10 437 633		
240	$2s^22p4p^3P_1$	10 466 102		10 460 676		
241	$2s^22p4p^3D_2$	10 468 322		10 462 978		
242	$2s^22p4p^3P_0$	10 470 990		10 465 993		
243	$2s^22p4s^3P_2$	10 485 597		10 479 693		
244	$2s^22p4s^1P_1$	10 492 966		10 487 317		
245	$2s^22p4d^3F_2$	10 532 099		10 526 459		
246	$2s^22p4d^3P_2 : A$	10 548 542		10 542 323	(10 547 000)	10 547 249
247	$2s^22p4d^3F_3$	10 549 480		10 543 488	10 548 000	10 548 160
248	$2s^22p4d^3D_1$	10 554 447		10 548 345	10 553 000	10 553 955
249	$2s^22p4p^1P_1$	10 568 810		10 563 327		
250	$2s^22p4p^3D_3$	10 574 912		10 569 412	10 664 000	
251	$2s^22p4p^3P_2$	10 575 111		10 569 433		
252	$2s^22p4p^3S_1$	10 578 203		10 572 657		
253	$2s^22p4p^1D_2$	10 597 862				
254	$2s^22p4p^1S_0$	10 619 563				
255	$2s^22p4d^3F_4$	10 652 979				
256	$2s^22p4d^1D_2$	10 653 631			10 675 000	
257	$2s^22p4d^3D_3$	10 660 593				
258	$2s^22p4d^3P_2 : B$	10 666 807				
259	$2s^22p4d^3P_1$	10 666 946			10 688 000	
260	$2s^22p4d^3P_0$	10 667 948				
261	$2s^22p4d^1F_3$	10 683 984			10 681 000	
262	$2s^22p4d^1P_1$	10 687 400				

One should note the excellent agreement between the energies from RMCDHF/RCI and RMBPT, the mean difference being less than 0.013%. Although the energies are in very good agreement, there seems to be a small systematic shift for the higher states, as depicted in Figure 1. The reason for this shift is not known, and further research is needed to shed light on this. To further access the accuracy of the excitation energies, calculations for the N-, O-, F- and Ne-like sequences [49–52] were done using both the RMCDHF/RCI and RMBPT methods. Cross-validations show that the mean energy differences for N-like, O-like, F-like and Ne-like Fe are 0.023%, 0.011%, 0.01% and 0.029%, respectively. The energy differences increase for the ions closer to the neutral end, where the RMBPT method is less efficient in capturing correlation effects.

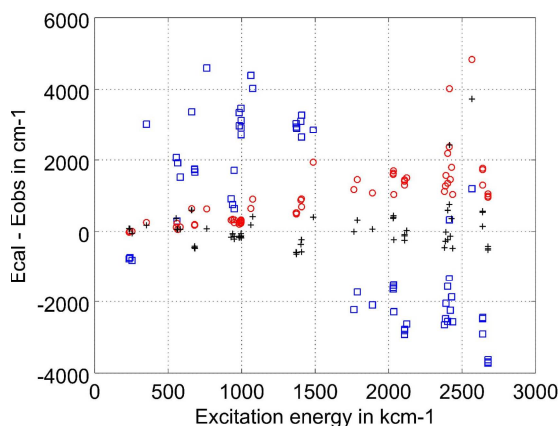
Obviously, calculations with high accuracy that also give the leading *LSJ* compositions are indispensable tools for analysing astrophysical observations.



**Figure 1.** Difference between RMCDHF/RCI and MBPT excitation energies in percent for C-like Fe as a function of the excitation energy in  $\text{cm}^{-1}$ . The dashed lines show the 0.02 % levels.

#### 4.4. Energies for Higher Lying States in the Mg-, Al- and Si-Like Sequences

For larger atomic systems, one needs to think in terms of a core and a number of valence electrons. In many calculations, only valence-valence (VV) correlation is included. More accurate results are obtained when accounting for the interactions with the core through the inclusion of core-valence correlation (VV + CV). The final step is to include core-core correlation (VV + CV + CC). The situation has been analysed by Gustafsson et al. [12] for  $3l3l'$ ,  $3l4l'$ ,  $3s5l$  states in Mg-like Fe where  $1s^22s^22p^6$  is taken as the core. The results of the analysis can be inferred from Figure 2 that shows the difference between the computed excitation energies and the observed energies from the NIST database as a function of the excitation energies for the three computational models: VV, VV + CV and VV + CV + CC.



**Figure 2.** Difference between observed and RMCDHF/RCI excitation energies in  $\text{cm}^{-1}$  for Mg-like Fe [12] as a function of the excitation energy in  $\text{cm}^{-1}$ . valence-valence (VV) (blue squares), VV + core-valence (CV) (red circles) and VV + CV + CC (black+).

From the figure, we see that the differences between the RMCDHF/RCI energies and observed energies are quite large, of the order of several thousand  $\text{cm}^{-1}$ , for the VV model. For many of

the low lying states, calculated energies are too high, whereas for the more highly lying states, calculated energies are too low. Adding core-valence correlation (VV + CV) substantially improves the calculated energies. To explain the difference in behaviour, as shown in the figure, between the low lying states and the more high lying states when core-valence correlation is added, we note that core-valence correlation is a combination of core polarization, an electrostatic long range rearrangement and an electron-electron cusp correcting effect [7,8]. The cusp correcting effect lowers all energies with an amount that depends on the overlap of the valence electron charge distribution and the core. The charge distributions of the low lying states from the  $3l3l'$  configurations are to a larger extent overlapping the core region compared to the charge distributions from the higher states of the  $3l4l'$  and  $3l5l'$  configurations, leading to a more pronounced energy lowering for the former states. The core polarization, in turn, lowers all energies except the  $3s^2\ ^1S_0$  ground state for which the valence electron charge density is spherically symmetric. In total, these two effects explain the observed behaviour. Whereas the low lying states are now in very good agreement with observations, the high lying states are still a little high compared to observations. The effect of the core-core correlation (VV + CV + CC) is small for the low lying states, but brings down the more highly states that are now in perfect agreement with observations.

The increased accuracy comes with a price. For an orbital set  $\{8s7p6d5f4g3h2i\}$ , the valence-valence (VV) expansions sizes are less than 3000 CSFs for each parity. Including the core-valence correlation (VV + CV) increases the expansions sizes to around 650,000 CSFs for each parity. Finally, including also core-core (VV + CV + CC) make the expansion sizes grow to around 6,000,000 CSFs for each parity. For these large expansions, it becomes necessary to use a zero- and first-order partition of the CSFs and include part of the interactions perturbatively as described in Section 2.3.

Based on the valence-valence and core-valence model (VV + CV), RMCDFH/RCI and SD-MR calculations have been done for the Mg-, Al- and Si-like sequences [54–56]. The range of ions, the targeted configurations and the number of studied states for each sequence are summarized in Table 7. Calculations were done by parity, i.e., odd and even parity states were treated in separate sets of calculations. The targeted configurations define the MR, and the expansions were obtained by SD-MR substitutions to increasing active sets of orbitals with the restriction that only one substitution is allowed from the  $2s^22p^6$  core.  $1s^2$  is treated as an inactive core and is always closed.

**Table 7.** Sequence, ions and targeted configurations for the calculations.  $N$  is the number of studied states for each ion. In the table,  $l = 0, \dots, n - 1$ ,  $l' = 0, \dots, n - 1$ .

Sequence	Ions	Configurations	$N$	Ref.
Mg-like	Ca-As, Kr	$3l3l', 3l4l', 3s5l$	146	[54]
Al-like	Ti-Kr, Xe, W	$3s^2\{3l; 4l; 5l\}, 3p^2\{3d; 4l\}, 3s\{3p^2; 3d^2\}, 3s\{3p3d; 3p4l; 3p5s; 3d4l'\}, 3p3d^2, 3p^3, 3d^3$	360	[55]
Si-like	Ti-Ge, Sr, Zr, Mo	$3s^23p^2, 3s3p^3, 3s^23p3d$	27	[56]

To illustrate the accuracy of the RMCDFH/RCI calculation accounting for valence-valence and core-valence effects, we look at Si-like Fe [56]. In Table 8, the computed excitation RMCDFH/RCI energies are compared with observed energies from Del Zanna [57], as well as with energies by Vilks and Ishikawa [58] using the MRMP method. The mean deviation is 0.076% for RMCDFH/RCI and only 0.034% for MRMP. The expansions for the even and odd states contained 1,500,000 and 4,500,000 CSFs, respectively.

The mean energy deviations for Mg-like, Al-like and Si-like iron from RMCDFH/RCI calculation accounting for valence-valence and core-valence effects are 0.051%, 0.039% and 0.076%, respectively. To improve the energies for the RMCDFH/RCI calculations, core-core correlation effects can be included as perturbative corrections, and work is in progress to develop tractable computational methods. For systems with five and more valence electrons, the expansions grow rapidly, and it

may be necessary to start with valence-valence correlation and include core-valence effects as perturbative corrections.

**Table 8.** Comparison of calculated and observed excitation energies in  $\text{cm}^{-1}$ .  $E_{RCI}$  RMCDHF/RCI energies from [56],  $E_{MRMP}$  MRMP energies from [58] and  $E_{DZ}$  observed energies from [57]. Relative errors in % for the calculated energies are shown in parenthesis.

Fe XIII			
Level	$E_{RCI}$	$E_{MRMP}$	$E_{DZ}$
$3s^2 3p^2 \ ^3P_0$	0	0	0
$3s^2 3p^2 \ ^3P_1$	9281 (0.237)	9295 (0.086)	9303.1
$3s^2 3p^2 \ ^3P_2$	18553 (0.048)	18576 (0.075)	18561.7
$3s^2 3p^2 \ ^1D_2$	48236 (0.344)	47985 (1.077)	48069.7
$3s^2 3p^2 \ ^1S_0$	91839 (0.357)	91508 (0.003)	91511.0
$3s 3p^3 \ ^5S_2^o$	214152 (0.220)	214540 (0.039)	214624.0
$3s 3p^3 \ ^3D_1^o$	287123 (0.028)	287199 (0.002)	287205.0
$3s 3p^3 \ ^3D_2^o$	287270 (0.029)	287348 (0.002)	287356.0
$3s 3p^3 \ ^3D_3^o$	290095 (0.029)	290179 (0.000)	290180.0
$3s 3p^3 \ ^3P_0^o$	328974 (0.014)	328980 (0.016)	328927.0
$3s 3p^3 \ ^3P_1^o$	329689 (0.015)	329702 (0.019)	329637.0
$3s 3p^3 \ ^3P_2^o$	330323 (0.012)	330334 (0.015)	330282.0
$3s 3p^3 \ ^1D_2^o$	362482 (0.020)	362416 (0.002)	362407.0
$3s 3p^3 \ ^3S_1^o$	415577 (0.027)	415519 (0.013)	415462.0
$3s^2 3p 3d \ ^3F_2^o$	430277 (0.035)	430129 (0.001)	430124.0
$3s^2 3p 3d \ ^3F_3^o$	437064 (0.033)	436905 (0.003)	436919.0
$3s 3p^3 \ ^1P_1^o$	438365 (0.063)	438005 (0.018)	438086.0
$3s^2 3p 3d \ ^3F_4^o$	447134 (0.029)	446959 (0.009)	447001.0
$3s^2 3p 3d \ ^3P_2^o$	486542 (0.037)	486403 (0.009)	486358.0
$3s^2 3p 3d \ ^3P_1^o$	495102 (0.032)	495242 (0.060)	494942.0
$3s^2 3p 3d \ ^1D_2^o$	499060 (0.038)	498925 (0.011)	498870.0
$3s^2 3p 3d \ ^3P_0^o$	501676 (0.032)	501667 (0.030)	501514.0
$3s^2 3p 3d \ ^3D_1^o$	506661 (0.030)	506681 (0.034)	506505.0
$3s^2 3p 3d \ ^3D_3^o$	509303 (0.024)	509479 (0.059)	509176.0
$3s^2 3p 3d \ ^3D_2^o$	509394 (0.028)	509441 (0.037)	509250.0
$3s^2 3p 3d \ ^1F_3^o$	557432 (0.093)	557303 (0.070)	556911.0
$3s^2 3p 3d \ ^1P_1^o$	571376 (0.110)	571187 (0.077)	570743.0

## 5. Transition Probabilities

Whereas there are enough observations to validate calculated excitation energies, the situation is very different for transition rates. For highly charged ions, there are few experimental methods available to determine transition rates. Lifetimes for long-lived states of the ground configuration or the lowest excited configurations have been determined in accurate storage-ring and trapping experiments (see for example, the review by Träbert [59]) and are used for benchmarking. Lifetimes for a large range of short-lived states have been determined using beam-foil spectroscopy [60]. However, even if these beam-foil data are very valuable, they are in general not accurate enough to discriminate between different computational approaches. In addition, lifetimes are dominated by the strong decay channels down to the lower configurations, and the lack of experimental transition rates, including weak transitions, between states of the excited configurations is of a major concern.

### 5.1. Internal Validation and Uncertainty Estimates

Due to the almost complete lack of experimental transition rates for highly charged ions, internal validation becomes important. For RMCDHF/RCI calculations, the convergence of the transition rates should be monitored as the active set is increased. Then, based on the same logic, the convergence of the transition rates should be monitored as the more involved correlation models are used, e.g., VV, VV + CV and VV + CV + CC. Considering the fact that there often are tens of thousands of transitions for extended spectrum calculations, this validation method is impractical,

and only smaller numbers of selected transitions can be monitored. Another internal validation method is based on the accuracy of the transition energy and the agreement between the computed line strength  $S$  in the length and velocity gauge. Along these lines, Froese-Fischer [61] has suggested that the uncertainties  $\delta A'$  of the calculated transition rates for  $LS$  allowed transitions can be estimated according to:

$$\delta A' = (\delta E + \delta S)A', \tag{9}$$

where  $A'$  is the energy-scaled transition rate computed from the observed transition energy ( $E_{obs}$ ),  $\delta E = |E_{calc} - E_{obs}|/E_{obs}$  is the relative error in the transition energy and  $\delta S = |S_{len} - S_{vel}|/\max(S_{len}, S_{vel})$  is the relative discrepancy between the length and velocity forms of the line strengths. In cases where the transition energies are not known, the expression reduces to:

$$\delta A = (\delta S)A. \tag{10}$$

Based on a statistical analysis of large datasets of accurate E1 transition rates from many independent calculations, Ekman et al. [62] found that the estimated errors from Equation (10) are correlated with and very close to the presumed actual errors. A validation of the method extended to intercombination lines reveals a smaller correlation in the statistical analysis and suggests that the uncertainty estimate in this case should only be used if averaging over a larger sample. The analysis further confirms the well-known fact that the uncertainty is large for weaker transitions, the general explanation being cancellations between the contributions to the matrix elements from different pairs of CSFs [63] or cancellations in the integrands of the transition integrals.

### 5.2. Transition Rates for the B- to Si-Like Sequences

The RMCDHF/RCI and SD-MR method has been used to compute tens of thousands of E1, M1, E2, M2 transitions rates for the B- to Si-like sequences [28–32,43,45–52,54–56]. The E1 and E2 rates are internally validated by giving  $\delta A/A$  along with  $A$ . The results for C-like Fe [29], shown in Table 9, illustrate the typical uncertainties. The table displays computed transition energies along with relative uncertainties obtained by comparing with observations from NIST. The uncertainties for the transition energies are all well below 1%, and many of them are around 0.1%, which is highly satisfactory. The transition rates in the length form are given together with the uncertainty estimate  $\delta A/A$ . The uncertainties for the transition rates are a few percent or less for the strong transitions, but go up to around 20% for some of the weak intercombination transitions. To further shed light on the situation, we compare the RMCDHF/RCI rates for Ne-like S [43] with rates from accurate MCHF-BP calculations [19] and with CI calculations using CIV3 [64] in Table 10. From the table, we see that there is in general a very good agreement between the rates from the different calculations. It is clear that the largest differences are for the weak transitions.

**Table 9.** Transition energies in  $\text{cm}^{-1}$  and E1 rates  $A$  in  $\text{s}^{-1}$  in the length gauge for Fe XXI from RMCDHF/RCI calculations [29]. Relative errors in % for the calculated transition energies and rates are shown in parenthesis. For the transition energies, the relative errors were obtained by comparison with observations from NIST. For the transition rates, the relative errors are estimated from Equation (10).

Upper	Lower	$\Delta E_{\text{calc}}$	$A$
Fe XXI			
$2s2p^3\ ^3D_1^o$	$2s^22p^2\ ^3P_0$	776750 (0.049)	1.156E+10 (0.00)
$2s2p^3\ ^3P_1^o$	$2s^22p^2\ ^3P_0$	925023 (0.120)	4.213E+09 (0.07)
$2s2p^3\ ^3S_1^o$	$2s^22p^2\ ^3P_0$	1096012 (0.089)	9.460E+09 (0.16)
$2s2p^3\ ^1P_1^o$	$2s^22p^2\ ^3P_0$	1261529 (0.205)	2.850E+07 (1.82)
$2s2p^3\ ^5S_2^o$	$2s^22p^2\ ^3P_1$	412701 (0.293)	3.597E+07 (8.72)

Table 9. Cont.

Upper	Lower	$\Delta E_{\text{calc}}$	A
$2s2p^3\ ^3D_1^0$	$2s^22p^2\ ^3P_1$	702930 (0.049)	7.606E+08 (1.64)
$2s2p^3\ ^3D_2^0$	$2s^22p^2\ ^3P_1$	703550 (0.048)	9.240E+09 (0.66)
$2s2p^3\ ^3P_0^0$	$2s^22p^2\ ^3P_1$	842581 (0.122)	2.200E+10 (0.31)
$2s2p^3\ ^3P_1^0$	$2s^22p^2\ ^3P_1$	851203 (0.119)	1.602E+10 (0.12)
$2s2p^3\ ^3P_2^0$	$2s^22p^2\ ^3P_1$	868735 (0.120)	3.820E+08 (1.85)
$2s2p^3\ ^3S_1^0$	$2s^22p^2\ ^3P_1$	1022191 (0.133)	2.533E+10 (0.11)
$2s2p^3\ ^1D_2^0$	$2s^22p^2\ ^3P_1$	1053811 (0.089)	3.907E+08 (1.68)
$2s2p^3\ ^1P_1^0$	$2s^22p^2\ ^3P_1$	1187709 (0.205)	4.909E+09 (0.34)
$2s2p^3\ ^5S_2^0$	$2s^22p^2\ ^3P_2$	369157 (0.293)	3.272E+07 (11.61)
$2s2p^3\ ^3D_1^0$	$2s^22p^2\ ^3P_2$	659387 (0.050)	8.335E+07 (6.39)
$2s2p^3\ ^3D_2^0$	$2s^22p^2\ ^3P_2$	660006 (0.050)	4.535E+06 (22.51)
$2s2p^3\ ^3D_3^0$	$2s^22p^2\ ^3P_2$	686197 (0.050)	6.105E+09 (0.80)
$2s2p^3\ ^3P_1^0$	$2s^22p^2\ ^3P_2$	807659 (0.120)	2.681E+09 (1.30)
$2s2p^3\ ^3P_2^0$	$2s^22p^2\ ^3P_2$	825192 (0.121)	2.038E+10 (0.04)
$2s2p^3\ ^3S_1^0$	$2s^22p^2\ ^3P_2$	978647 (0.134)	6.104E+10 (0.24)
$2s2p^3\ ^1D_2^0$	$2s^22p^2\ ^3P_2$	1010267 (0.090)	8.020E+09 (0.39)
$2s2p^3\ ^1P_1^0$	$2s^22p^2\ ^3P_2$	1144165 (0.206)	2.491E+08 (0.16)
$2s2p^3\ ^5S_2^0$	$2s^22p^2\ ^1D_2$	241853 (0.714)	1.307E+06 (19.51)
$2s2p^3\ ^3D_1^0$	$2s^22p^2\ ^1D_2$	532083 (0.048)	1.808E+08 (6.63)
$2s2p^3\ ^3D_2^0$	$2s^22p^2\ ^1D_2$	532703 (0.048)	3.827E+07 (6.27)
$2s2p^3\ ^3D_3^0$	$2s^22p^2\ ^1D_2$	558894 (0.049)	9.767E+08 (3.61)
$2s2p^3\ ^3P_1^0$	$2s^22p^2\ ^1D_2$	680356 (0.051)	2.577E+08 (2.44)
$2s2p^3\ ^3P_2^0$	$2s^22p^2\ ^1D_2$	697888 (0.052)	1.435E+08 (4.80)
$2s2p^3\ ^3S_1^0$	$2s^22p^2\ ^1D_2$	851344 (0.084)	3.607E+08 (3.16)
$2s2p^3\ ^1D_2^0$	$2s^22p^2\ ^1D_2$	882963 (0.037)	4.485E+10 (0.37)
$2s2p^3\ ^1P_1^0$	$2s^22p^2\ ^1D_2$	1016862 (0.170)	6.583E+10 (0.15)
$2s2p^3\ ^3D_1^0$	$2s^22p^2\ ^1S_0$	404698 (0.165)	4.070E+07 (2.97)
$2s2p^3\ ^3P_1^0$	$2s^22p^2\ ^1S_0$	552971 (0.014)	1.492E+08 (7.10)
$2s2p^3\ ^3S_1^0$	$2s^22p^2\ ^1S_0$	723959 (0.008)	6.511E+08 (2.13)
$2s2p^3\ ^1P_1^0$	$2s^22p^2\ ^1S_0$	889477 (0.147)	1.727E+10 (0.52)
$2p^4\ ^3P_2$	$2s2p^3\ ^5S_2^0$	1159940 (0.180)	1.422E+09 (2.39)
$2p^4\ ^3P_1$	$2s2p^3\ ^5S_2^0$	1254085 (0.181)	2.381E+08 (3.65)
$2p^4\ ^1D_2$	$2s2p^3\ ^5S_2^0$	1331255 (0.201)	5.282E+07 (2.48)
$2p^4\ ^3P_2$	$2s2p^3\ ^3D_1^0$	869710 (0.102)	3.455E+09 (0.75)
$2p^4\ ^3P_0$	$2s2p^3\ ^3D_1^0$	959080 (0.137)	3.474E+10 (0.43)
$2p^4\ ^3P_1$	$2s2p^3\ ^3D_1^0$	963855 (0.102)	1.434E+10 (0.27)
$2p^4\ ^1D_2$	$2s2p^3\ ^3D_1^0$	1041025 (0.103)	4.033E+06 (20.67)
$2p^4\ ^1S_0$	$2s2p^3\ ^3D_1^0$	1271738 (0.137)	2.331E+08 (1.32)
$2p^4\ ^3P_2$	$2s2p^3\ ^3D_2^0$	869090 (0.103)	1.335E+10 (0.00)
$2p^4\ ^3P_1$	$2s2p^3\ ^3D_2^0$	963235 (0.104)	2.124E+10 (0.28)
$2p^4\ ^1D_2$	$2s2p^3\ ^3D_2^0$	1040406 (0.106)	7.878E+08 (0.20)
$2p^4\ ^3P_2$	$2s2p^3\ ^3D_3^0$	842899 (0.137)	2.822E+10 (0.53)
$2p^4\ ^1D_2$	$2s2p^3\ ^3D_3^0$	1014215 (0.260)	5.622E+09 (0.85)
$2p^4\ ^3P_1$	$2s2p^3\ ^3P_0^0$	824204 (0.038)	4.813E+09 (0.02)
$2p^4\ ^3P_2$	$2s2p^3\ ^3P_0^0$	721437 (0.039)	3.678E+09 (0.32)
$2p^4\ ^3P_0$	$2s2p^3\ ^3P_1^0$	810807 (0.040)	1.827E+10 (0.93)
$2p^4\ ^3P_1$	$2s2p^3\ ^3P_1^0$	815582 (0.043)	1.273E+08 (3.29)
$2p^4\ ^1D_2$	$2s2p^3\ ^3P_1^0$	892752 (0.085)	1.241E+09 (1.85)
$2p^4\ ^1S_0$	$2s2p^3\ ^3P_2^0$	1123465 (0.233)	4.222E+09 (1.30)
$2p^4\ ^3P_2$	$2s2p^3\ ^3P_2^0$	703905 (0.039)	3.629E+09 (0.88)
$2p^4\ ^3P_1$	$2s2p^3\ ^3P_2^0$	798050 (0.040)	1.598E+10 (0.75)
$2p^4\ ^1D_2$	$2s2p^3\ ^3P_2^0$	875220 (0.085)	2.512E+09 (1.79)
$2p^4\ ^3P_2$	$2s2p^3\ ^3S_1^0$	550450 (0.021)	6.005E+09 (0.76)
$2p^4\ ^3P_0$	$2s2p^3\ ^3S_1^0$	639819 (0.020)	1.733E+10 (0.28)
$2p^4\ ^3P_1$	$2s2p^3\ ^3S_1^0$	644594 (0.049)	1.290E+10 (0.00)
$2p^4\ ^1D_2$	$2s2p^3\ ^3S_1^0$	721764 (0.059)	7.002E+06 (0.68)
$2p^4\ ^1S_0$	$2s2p^3\ ^3S_1^0$	952477 (0.060)	5.111E+09 (0.25)
$2p^4\ ^3P_2$	$2s2p^3\ ^1D_2^0$	518830 (0.065)	7.538E+08 (1.85)
$2p^4\ ^3P_1$	$2s2p^3\ ^1D_2^0$	612975 (0.124)	3.767E+08 (3.31)
$2p^4\ ^1D_2$	$2s2p^3\ ^1D_2^0$	690145 (0.311)	3.182E+10 (0.28)
$2p^4\ ^3P_2$	$2s2p^3\ ^1P_1^0$	384932 (0.274)	8.409E+07 (3.44)
$2p^4\ ^3P_0$	$2s2p^3\ ^1P_1^0$	474302 (0.271)	9.885E+06 (20.99)
$2p^4\ ^3P_1$	$2s2p^3\ ^1P_1^0$	479076 (0.265)	6.387E+08 (1.58)
$2p^4\ ^1D_2$	$2s2p^3\ ^1P_1^0$	556247 (0.139)	4.499E+09 (1.15)
$2p^4\ ^1S_0$	$2s2p^3\ ^1P_1^0$	786959 (0.156)	7.549E+10 (0.09)



**Table 10.** Transition rates for Ne-like S.  $A_{RCI}$  transition rates from RMCDHF/RCI [43],  $A_{BP}$  transition rates from multiconfiguration Hartree-Fock-Breit-Pauli [19] and  $A_{CIV3}$  transition rates from CI calculations using CIV3 [64].

States		$\Delta E$ (cm <sup>-1</sup> )	Type	$A_{RCI}$	$A_{BP}$	$A_{CIV3}$
Upper	Lower					
S VII						
$2p^5 3s^3 P_2^o$	$2p^6 1S_0$	1371667	M2	7.638E+02	7.617E+02	
$2p^5 3s^3 P_1^o$	$2p^6 1S_0$	1376084	E1	1.855E+10	1.816E+10	1.989E+10
$2p^5 3s^1 P_1^o$	$2p^6 1S_0$	1388242	E1	8.421E+10	8.507E+10	8.777E+10
$2p^5 3p^3 D_2$	$2p^6 1S_0$	1484530	E2	3.021E+06	2.964E+06	
$2p^5 3p^3 P_2$	$2p^6 1S_0$	1492576	E2	8.028E+06	8.008E+06	
$2p^5 3d^3 P_2^o$	$2p^6 1S_0$	1624769	E1	2.160E+09	2.182E+09	2.312E+09
$2p^5 3d^3 P_1^o$	$2p^6 1S_0$	1627240	M2	1.710E+04	1.728E+04	
$2p^5 3d^1 P_1^o$	$2p^6 1S_0$	1644545	E1	6.122E+10	6.206E+10	6.230E+10
$2p^5 3d^1 P_1^o$	$2p^6 1S_0$	1662346	E1	9.452E+11	9.448E+11	9.087E+11
$2p^5 3s^3 P_1^o$	$2p^6 1S_0$	4417	M1	1.587E+00	1.601E+00	
$2p^5 3s^3 P_2^o$	$2p^6 1S_0$	16575	M1	1.849E+01	1.867E+01	
$2p^5 3s^3 P_2^o$	$2p^5 3s^3 P_2^o$	95373	E1	6.393E+08	6.504E+08	6.480E+08
$2p^5 3s^3 P_2^o$	$2p^5 3s^3 P_2^o$	111609	E1	1.566E+09	1.608E+09	1.594E+09
$2p^5 3s^3 P_2^o$	$2p^5 3s^3 P_2^o$	112863	E1	6.439E+08	6.627E+08	6.418E+08
$2p^5 3p^3 D_2$	$2p^5 3s^3 P_2^o$	116432	E1	1.994E+08	2.060E+08	2.023E+08
$2p^5 3p^3 D_1$	$2p^5 3s^3 P_2^o$	120909	E1	1.000E+09	1.031E+09	1.006E+09
$2p^5 3p^3 P_2$	$2p^5 3s^3 P_2^o$	124214	E1	7.124E+07	7.315E+07	6.807E+07
$2p^5 3p^3 P_1$	$2p^5 3s^3 P_2^o$	127448	E1	2.464E+08	2.501E+08	2.832E+08
$2p^5 3p^1 D_2$	$2p^5 3s^3 P_2^o$	78797	E1	1.188E+07	1.206E+07	1.253E+07
$2p^5 3p^3 S_1$	$0.81 + 0.18^3 P_1^o$	96287	E1	6.945E+06	7.197E+06	5.508E+06
$2p^5 3p^3 D_2$	$0.81 + 0.18^3 P_1^o$	99856	E1	3.825E+06	4.290E+06	4.536E+06
$2p^5 3p^3 D_1$	$0.81 + 0.18^3 P_1^o$	104333	E1	2.932E+08	2.977E+08	3.152E+08
$2p^5 3p^3 P_2$	$0.81 + 0.18^3 P_1^o$	107638	E1	7.415E+08	7.625E+08	7.557E+08
$2p^5 3p^1 P_1$	$0.81 + 0.18^3 P_1^o$					

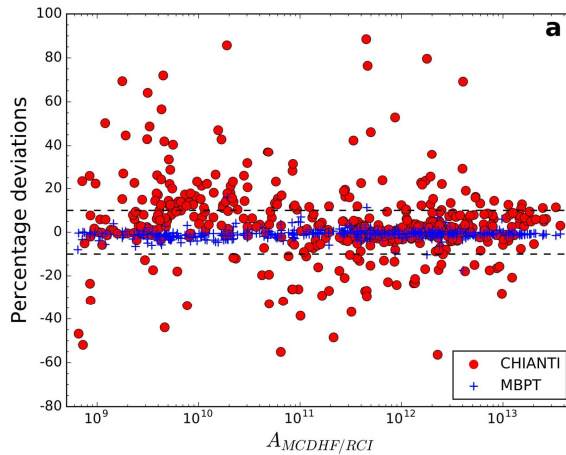


Table 10. Cont.

States		$\Delta E$ (cm <sup>-1</sup> )	Type	A <sub>RCI</sub>	A <sub>BP</sub>	A <sub>CIV3</sub>
Upper	Lower					
2p <sup>5</sup> 3p <sup>3</sup> P <sub>0</sub>	2p <sup>5</sup> 3s <sup>1</sup> P <sub>0</sub> <sup>o</sup>	110460	E1	1.908E+08	1.974E+08	2.006E+08
2p <sup>5</sup> 3p <sup>1</sup> D <sub>2</sub>	2p <sup>5</sup> 3s <sup>1</sup> P <sub>1</sub> <sup>o</sup>	110872	E1	1.206E+09	1.243E+09	1.199E+09
2p <sup>5</sup> 3p <sup>3</sup> P <sub>1</sub>	2p <sup>5</sup> 3s <sup>1</sup> P <sub>1</sub> <sup>o</sup>	112070	E1	7.082E+08	7.307E+08	7.000E+08
2p <sup>5</sup> 3p <sup>3</sup> P <sub>1</sub>	2p <sup>5</sup> 3s <sup>1</sup> P <sub>1</sub> <sup>o</sup>	112070	M2	1.139E-01	1.191E-01	
2p <sup>5</sup> 3p <sup>1</sup> S <sub>0</sub>	2p <sup>5</sup> 3s <sup>1</sup> P <sub>0</sub> <sup>o</sup>	165149	E1	5.082E+09	5.118E+09	5.073E+09
2p <sup>5</sup> 3d <sup>3</sup> P <sub>0</sub>	2p <sup>5</sup> 3p <sup>1</sup> D <sub>2</sub>	125654	E1	1.229E+08	1.235E+08	1.323E+08
2p <sup>5</sup> 3d <sup>3</sup> P <sub>0</sub>	2p <sup>5</sup> 3p <sup>1</sup> D <sub>2</sub>	128125	E1	3.010E+08	3.017E+08	3.358E+08
2p <sup>5</sup> 3d <sup>3</sup> P <sub>0</sub>	2p <sup>5</sup> 3p <sup>1</sup> D <sub>2</sub>	128125	M2	1.161E-01	1.175E-01	
2p <sup>5</sup> 3d <sup>3</sup> F <sub>2</sub>	2p <sup>5</sup> 3p <sup>1</sup> D <sub>2</sub>	132832	E1	1.471E+06	1.472E+06	1.078E+06
2p <sup>5</sup> 3d <sup>3</sup> F <sub>2</sub>	2p <sup>5</sup> 3p <sup>1</sup> D <sub>2</sub>	136157	E1	1.190E+06	1.370E+06	1.643E+06
2p <sup>5</sup> 3d <sup>1</sup> F <sub>3</sub>	2p <sup>5</sup> 3p <sup>1</sup> D <sub>2</sub>	138763	E1	1.511E+08	1.519E+08	1.131E+08
2p <sup>5</sup> 3d <sup>3</sup> D <sub>1</sub>	2p <sup>5</sup> 3p <sup>1</sup> D <sub>2</sub>	145430	E1	3.071E+06	3.159E+06	1.717E+06
2p <sup>5</sup> 3d <sup>1</sup> D <sub>2</sub>	2p <sup>5</sup> 3p <sup>1</sup> D <sub>2</sub>	145447	E1	6.172E+08	6.286E+08	6.276E+08
2p <sup>5</sup> 3d <sup>3</sup> D <sub>2</sub>	2p <sup>5</sup> 3p <sup>1</sup> D <sub>2</sub>	146716	E1	4.030E+09	4.093E+09	4.183E+09
2p <sup>5</sup> 3d <sup>3</sup> D <sub>2</sub>	2p <sup>5</sup> 3p <sup>1</sup> D <sub>2</sub>	146716	M2	1.029E+00	1.054E+00	
2p <sup>5</sup> 3d <sup>3</sup> D <sub>2</sub>	2p <sup>5</sup> 3p <sup>1</sup> D <sub>2</sub>	147358	E1	1.521E+08	1.531E+08	1.489E+08
2p <sup>5</sup> 3d <sup>1</sup> P <sub>1</sub>	2p <sup>5</sup> 3p <sup>1</sup> D <sub>2</sub>	163231	E1	4.854E+07	4.851E+07	5.550E+07

### 5.3. Systematic Comparisons between Methods

Wang and co-workers have systematically compared large sets of transition rates from accurate RMCDHF/RCI and RMBPT calculations [49–52]. These comparisons show that the rates from the two methods agree within a few percent for the strong transitions and that the agreement gets slightly worse for the weak intercombination and the two-electron, one photon transitions<sup>1</sup>. The comparisons also show that the differences between the methods are large for transitions for which there are large differences between the rates in the length and velocity form, thus confirming the usefulness of  $\delta A/A$  as an uncertainty estimate. In Figure 3, we show the results of a comparison between methods for O-like Fe [31]. The figure clearly shows the consistency of the RMCDHF/RCI and RMBPT transition rates, but also the comparatively large differences with rates from the CHIANTI database. These types of comparisons point to the fact that transition rates can be computed with high accuracy, but that much effort remains in order to make data practically available for astronomers and astrophysicist in updated databases.



**Figure 3.** Results of a comparison between methods for O-like Fe [31]. Deviation in percent between RMCDHF/RCI and RMBPT transition rates as a function of the transition rate in  $s^{-1}$ . Deviations from the values of the CHIANTI database [3,4] are given in red. The dashed lines give the 10% levels.

## 6. Conclusions

Current computational methodologies make it possible to compute excitation and transition energies to almost spectroscopic accuracy for many ionized systems. In an astrophysical context, this means that calculated transition energies can be used to unambiguously identify new lines from spectra or correct old identifications. Transition data are lacking for many ions, and calculated values fill this gap. Whereas many of the calculations have been done for systems with relatively few electrons with a full RCI matrix, zero- and first-order methods, allowing for parts of the interactions to be treated perturbatively, have extended the range of applicability, and many calculations with high accuracy are in progress for isoelectronic sequences starting from the third and fourth row of the periodic table.

Accurate and consistent transition rates are essential for collisional and radiative plasma modelling and for diagnostic purposes. Very few experimental data are available for the rates, and thus, the bulk of the data must be computed. The lack of experimental data means that internal validation of

<sup>1</sup> Transitions between two states for which the configurations differ by more than one electron. These transitions are zero in the lowest approximation and are induced by CSFs that enter the calculation to correct for electron correlation effects.

computed data becomes important. For accurate calculations that predict the energy structure at the per mille level, the differences between E1 rates in the length and velocity forms can be used to estimate the uncertainties. Internal validation based on convergence analysis and agreement between rates in length and velocity, as well as systematic comparisons of rates from RMCDHF/RCI and RMBPT calculations show that the uncertainties of the E1 rates are at the level of a few percent for the strong transitions. For the weakest transitions, the uncertainties are higher and come with a more irregular pattern.

## 7. Further Developments and Outlook

The time for angular integration is a limiting factor for very large RCI calculations. This time can be cut down by regrouping CSFs from SD-MR expansions in blocks that can be represented symbolically. For example, in non-relativistic notation,  $1s^2nsm p^3P$  and  $1s^2n p m d^3P$  with  $n = 2, \dots, 12$  and  $m = 2, \dots, 12$  represent two blocks where the angular integration between CSFs in the blocks, as well as between CSFs in the different blocks is independent of the principal quantum numbers or can be reduced to only a few cases. For large  $n$  and  $m$ , the reduction in computing time is substantial. Discussed already decades ago [65], it seems essential that these ideas are now broadly implemented in the generally available computer codes.

With angular integration being a negligible part of the computation comes the possibility to extend the orbital set to higher  $n$ . Currently, the orbitals are variationally determined on a grid in RMCDHF calculations. The variational determination is computationally costly, and it would be valuable to augment the variationally-determined orbitals with analytical orbitals or orbitals determined in simplified and fast procedures. Work along these lines is in progress.

Among the targeted systems for improved computer codes are the  $\alpha$ -elements, including Mg, Si, Ca and the iron group elements Sc, Ti, Cr, Mn, Fe at lower ionization states. These elements are of key importance for stellar and galactic evolution studies [66].

**Acknowledgments:** Per Jönsson, Henrik Hartman, Jörgen Ekman and Tomas Brage acknowledge support from the Swedish Research Council under Contract 2015-04842. Laima Radziute is thankful for the high performance computing resources provided by the Information Technology Open Access Center of Vilnius University. Michel R. Godefroid acknowledges support from the Belgian F.R.S.-FNRS Fonds de la Recherche Scientifique under CDR J.0047.16.

**Author Contributions:** All authors contributed equally to the work presented here.

**Conflicts of Interest:** The authors declare no conflict of interest.

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Article

# Wavelengths of the Self-Photopumped Nickel-Like $4f\ ^1P_1 \rightarrow 4d\ ^1P_1$ X-ray Laser Transitions

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Academic Editor: Joseph Reader

Received: 31 January 2017; Accepted: 27 June 2017; Published: 13 July 2017

**Abstract:** The energies for the lower  $3d_{3/2}4d_{3/2} [J = 1]$  and upper  $3d_{3/2}4f_{5/2} [J = 1]$  working levels in the self-photopumped X-ray laser are analyzed along the Ni-like sequence. We have found some irregularities in these energy levels in the range  $Z = 42\text{--}49$ . The causes of the irregularities are studied. The list of elements that lase on the self-photopumped transition can be extended much further than originally known. We calculate the wavelengths of this transition in Ni-like sequence to  $Z = 79$  using the relativistic perturbation theory with a zero approximation model potential. We estimate the wavelength accuracy for  $Z > 50$  as  $\Delta\lambda/\lambda \leq 0.005$ .

**Keywords:** X-ray lasers; spectroscopy of multicharged ions; self-photo pumped lasers

## 1. Introduction

Self-photo pumped (SPP) X-ray lasers (XRL) in Ni-like ions were presented in 1996 [1] as an alternative approach to the standard radiative collisional scheme for inversion creation. We use the term SPP following the name given in literature. This is really a collisionally pumped laser assisted by radiation trapping. Both schemes for Ni-like ions are shown in Figure 1. This new class of SPP in Ni-like XRL was first investigated theoretically in [2], where high gain was predicted for the  $4f\ ^1P_1\text{--}4d\ ^1P_1$  transition in  $\text{Mo}^{14+}$  at 22.0 nm. It was supposed that preplasma was created by a nanosecond pulse followed by a picosecond pulse to control the temperature and density in plasma, and to achieve high gain. This wavelength was calculated using the multiconfiguration Dirac-Fock atomic physics code by Grant and co-workers in the extended average level mode [3]. In the experiment [4], the Ni-like SPP XRL on the  $4f\ ^1P_1\text{--}4d\ ^1P_1$  transition was demonstrated in Zr, Nb, and Mo, and the measured wavelengths for these ions were presented. For  $\text{Mo}^{14+}$  a gain of  $13\text{ cm}^{-1}$  was measured at 22.6 nm for a target up to 1 cm long [4]. The wavelengths of this transition for ions from  $Z = 36$  to 54 were predicted in [4] using the experimental data of this work to provide small corrections to their calculations. In the experiment [5], the progress in the optimization and understanding of the collisional pumping of X-ray lasers using an ultrashort subpicosecond heating pulse was reported. Time-integrated and time-resolved lasing signals at the standard  $4d\ ^1S_0\text{--}4p\ ^1P_1$  XRL line in Ni-like Ag were studied in detail. Under specific irradiation conditions, strong lasing was obtained on the SPP  $4f\ ^1P_1\text{--}4d\ ^1P_1$  transition at 16.1 nm. The strong lasing on the SPP transition in  $\text{Mo}^{14+}$  was also observed with very modest (less than 1 J) pump energy at a high repetition rate [6]. Recently, lasing on the SPP  $3d\ ^1P_1\text{--}3p\ ^1P_1$  laser line has been observed for Ne-like V, Cr, Fe, and Co, as well as for Ni-like Ru, Pd, and Ag [7]. A strong dependence on the delay between the main and second prepulse was found: the optimum delay shifts towards smaller delays with increasing atomic number  $Z$ . Accurate wavelength measurements and calculations were shown to be in excellent agreement. The experiment [7] demonstrated that the list of elements that lase on the SPP transitions can be extended much further than originally known.



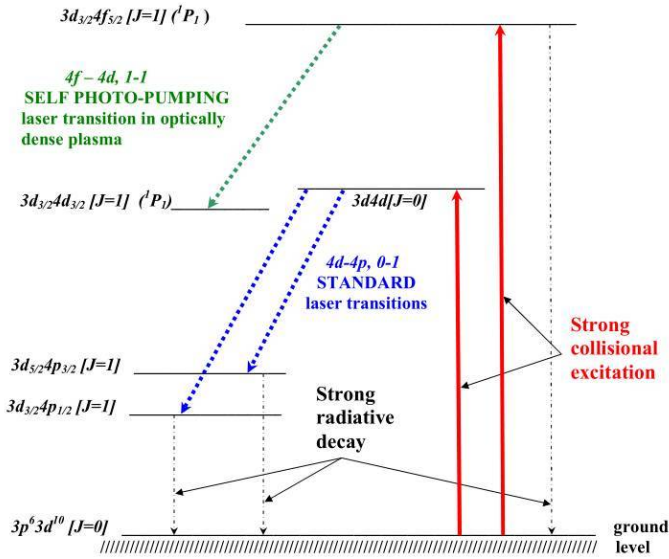


Figure 1. Schematic diagram of three low XRL transitions in Ni-like ions.

Many authors have investigated the spectra of Ni-like ions using vacuum sparks, laser produced plasma and electron beam ion traps as light sources [8–14]. The  $3d^9 4d$  and  $3d^9 4f$  configurations have been analyzed in the Rb X–Mo XV sequence [10,11]. In [10,11], these configurations were investigated using parameter extrapolations within the Generalized-Least-Squares (GLS) method. This method was used in [12,13] to predict for  $3d^9 4d$ ,  $3d^9 4f$  configuration energy levels in Cd XXI and Ag XX. GLS predictions of  $3d^9 4d$ ,  $3d^9 4f$  energy levels in the Zr XIII–Pd XIX sequence are tabulated in [14].

Note that lasing wavelength ( $\lambda_{las}$ ) in  $Mo^{14+}$  was determined theoretically [2] and in the experiment [4] using one and the same atomic physics code [3], but results for  $\lambda_{las}$  were somewhat different (by 4 Å). The  $3d_{3/2} 4f_{5/2} [J = 1]$  upper working level has the largest oscillator strength and radiative transition probability to the  $3d^{10}$  ground level. This fact allows it to achieve high precision in this level energy measurement along the Ni-like sequence up to high  $Z \sim 84$ ; in some ions, the energy of the transition to the ground state was accurate up to the fourth significant digit. The wavelengths of resonant radiative transitions in heavy Ni-like ions were calculated by us to  $Z = 83$  in [15]. Moreover, in [15], the wavelengths (for Z within 79–82) were predicted with the same accuracy, although they have not yet been measured experimentally.

In the present paper, we analyze the smoothness of the working energy levels of SPP XRL along the Ni-like sequence. We found some irregularities in Ni-like sequence energies in the region  $Z = 42$  ( $Mo^{14+}$ ) and in the region  $Z = 49$  ( $In^{21+}$ ) for the upper  $3d_{3/2} 4f_{5/2} [J = 1]$  working level. The causes of the irregularities are studied.

The principle purpose of this paper is to predict the wavelengths of SPP XRL lines in Ni-like ions with  $Z \leq 79$ . The calculations are performed by the Relativistic Perturbation Theory with Model Zero Approximation, (RPTMP). The fundamental principles of the RPTMP approach are given in [16]. Energy levels of the  $3p^6 3d^9 4l$ ,  $3p^5 3d^{10} 4l$ , ( $l = 0, 1$ ) configurations and radiative transition rates to the  $3p^6 3d^{10}$  ground state in the Kr IX ion are calculated by this method in [16]. The stability of calculations on the approximation used is shown in [16].

## 2. Features of Lower and Upper Working Levels of SPP XRL along the Ni-Like Sequence

The schematic diagram of three strong XRL transitions is shown in Figure 1: two of them are standard  $3d4d [J = 0] - 3d_{5/2}4p_{3/2} [J = 1]$  and  $3d4d [J = 0] - 3d_{3/2}4p_{1/2} [J = 1]$  transitions. The classifications of lower working levels in Figure 1 are valid for  $Z > 42$ . The  $3d_{5/2}4p_{3/2} [J = 1]$  level is the lower working level of an XRL for the entire nickel isoelectronic sequence, the  $3d_{3/2}4p_{1/2} [J = 1]$  level is the lower working level for heavy ions starting with  $Z = 62$ . The third  $3d_{3/2}4p_{3/2} [J = 1]$  level decays to a ground state significantly weaker than the two mentioned above, and does not provide a significant gain. In our recent work [17], the energies of standard XRL transitions in ions of the Ni-like sequence with  $Z \leq 79$  are refined by RPTMP calculations. The calculated energies of the two standard  $4d-4p$ ,  $J = 0-1$  XRL transitions are corrected by extrapolation of the experimental differentials of XRL transition energies  $dE_Z^{las} = E_Z^{las} - E_{Z-1}^{las}$ , i.e., the differences between transition energies of neighboring ions, which weakly depend on  $Z$  (especially in the region  $Z \leq 50$ ). It is proven that the accuracy for the final results for large  $Z$  is within the experimental error.

The  $3d_{3/2}4f_{5/2} [J = 1] - 3d_{3/2}4d_{3/2} [J = 1]$  transition is optically self-photopumped XRL in all Ni-like ions, the positions of working levels vary with respect to other levels along the sequence. Based on our previous studies of XRL [18–20], it can be argued that there are at least four principal differences between standard and self photo-pumped mechanisms:

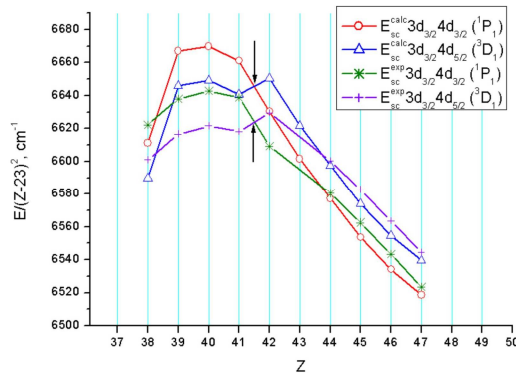
- (1) In the standard scheme, the upper working level is populated by strong monopole electron collisions: in the SPP scheme it is populated by strong dipole electron collisions, which means high oscillator strength and effective photoabsorption.
- (2) Effective SPP XRL is possible only in optically thick plasma (large electron density  $n_e$  and diameter  $d$ ), while the standard XRL is possible both in optically thick and in optically thin plasma over a wide range of  $n_e$  and  $d$ .
- (3) In the SPP, the upper working level is quickly emptied due to the large radiative decay rate. Therefore, in this scheme, a laser effect is short-lived; maximum XRL duration may be a few tens of picoseconds. A standard XRL can operate in quasi-continuous mode (under certain conditions).
- (4) In the SPP, the lower and upper working levels do not change their classification along the Ni-like sequence; in the standard scheme the upper working level changes its classification: the  $3d_{5/2}4d_{5/2} [J = 0]$  state is dominant in the classification of the upper working level at  $Z \leq 51$ , and the  $3d_{3/2}4d_{3/2} [J = 0]$  state is dominant for  $Z > 51$  [17].

Below, we demonstrate the irregularities in the sequence of both the lower and the upper working levels of SPP XRL. Crossing of each working level with another level causes these irregularities. Level crossing is accompanied by a strong interaction at certain  $Z$  points. Figure 2a shows the scaled energies along  $Z$  of the  $3d_{3/2}4d_{3/2} [J = 1]$  lower working level and the  $3d_{3/2}4d_{5/2} [J = 1]$  level close to it. In addition to the energy levels calculated here, Figure 2a also shows the corresponding experimental values [14]. Reference [14] does not indicate classification of  $3d4d [J = 1]$  levels, their classification was made earlier in [11]. Note that theoretical and experimental classifications are identical. There are some differences between theoretical and experimental energies, typically a few units in the 4th–5th digits. These differences are conditioned by the shift of the theoretical list of energy levels as a whole, but this shift does not affect the accuracy of  $\lambda_{las}$ . The energy levels in Figure 2a are scaled by dividing by  $(Z-23)^2$ , so that the behavior of the third and fourth significant digits can be observed. At the beginning of the sequence, the  $3d_{3/2}4d_{3/2} [J = 1]$  level is above the  $3d_{3/2}4d_{5/2} [J = 1]$  level. The crossing of these levels is in the range  $41 < Z < 42$  (shown by arrows). The crossing of the corresponding experimental energy levels occurs at exactly the same  $Z$  values. At  $Z = 42$ , one can observe the “repulsion” of levels caused by their interaction; the “repulsion” is a feature of theoretical and experimental data. Note, that repulsion can be seen due to energy scaling; in fact, the repulsion value is approximately a few thousand  $\text{cm}^{-1}$ , i.e., a few units in the fourth digit for the  $3d_{3/2}4d_{5/2} [J = 1]$  level.

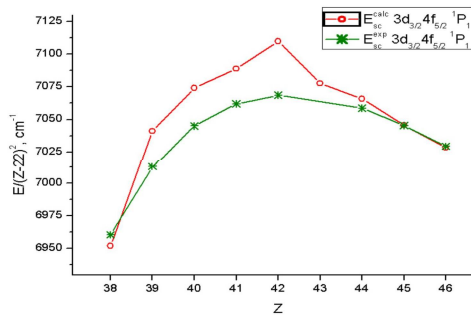
In Figure 2b, we can see hard-to-explain behavior of the  $3d_{3/2}4f_{5/2} [J = 1]$  upper working level in the region of  $Z = 42$ . The features of this level will be considered below in more detail; however,

it is important to note, here, that the energy structure of odd states in the range  $Z = 40\text{--}49$  exhibits extremely high instability caused by the interaction of levels with each other, which rapidly changes with  $Z$ . In the case at hand, we understand the instability as the ambiguity of the calculation of eigenvectors and eigenenergies. As a result, the calculation in the same approximation leads to different energies at a certain level. The deviation from the smooth curve in Figure 2a is  $\sim 10,000\text{ cm}^{-1}$ ; however, such a value leads to a sufficiently large deviation from the corresponding experimental values of  $\lambda_{\text{las}}$  shown in Figure 3.

At the point  $Z = 42$ ,  $\lambda_{\text{las}}$  calculated here is  $\sim 222\text{ \AA}$ , which is smaller than the experimental and theoretical values of [4] by  $4\text{ \AA}$ . In a recent experiment [7], the delay time between preliminary and main pump pulses was optimized to achieve the maximum yield of the X-ray laser. In fact, the electron density was optimized in [7]. X-ray lasing occurs in the Ni-like ion ionization mode, so that the lasing times on both transitions were restricted to the ionization time of Ni-like ions to the Co-like state. Time-resolved measurements in [7] allowed high-accuracy wavelength measurements of the SPP and standard X-ray laser lines. Thus, the calculations of the previous work [4] were confirmed:  $\lambda_{\text{las}} \approx 22.61\text{ nm}$  in Ni-like molybdenum ( $\text{Mo}^{14+}$ ,  $Z = 42$ ). Our calculations are performed for an isolated atom. Based on the studies performed, it can be argued that the interaction of levels at the point  $Z = 42$  is so strong that the energy levels  $3d_{3/2}4d_{3/2} [J = 1]$ ,  $3d_{3/2}4d_{5/2} [J = 1]$  in dense hot plasma can differ significantly from the corresponding energy levels in an isolated atom.

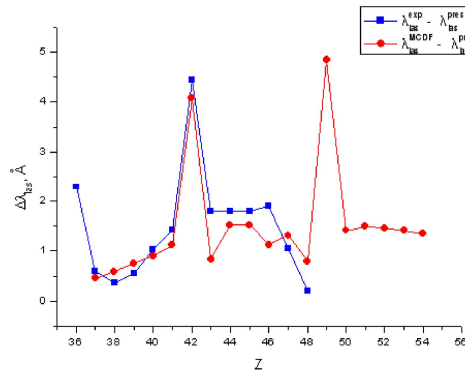


(a)



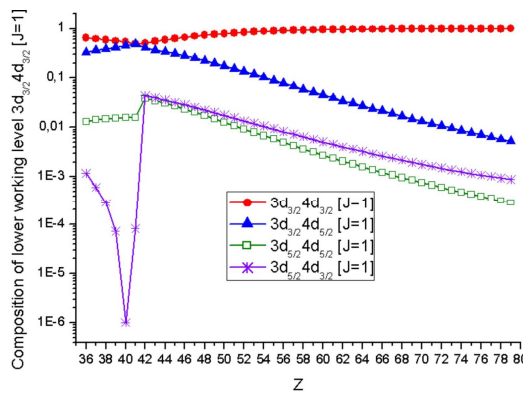
(b)

**Figure 2.** (a) Theoretical and experimental crossing of low working  $3d_{3/2}4d_{3/2} [J = 1]$  energy level with  $3d_{3/2}4d_{5/2} [J = 1]$  energy level in Ni-like sequence, shown by scaled energy values along  $Z$ ; (b) Features of theoretical upper working level  $3d_{3/2}4f_{5/2} [J = 1]$ , shown by scaled energy along  $Z$  in comparison with correspondent experimental data.



**Figure 3.** Difference between experimental, predicted from [4] and calculated here,  $\lambda_{las}$  of SPP XRL transitions in Ni-like ions.

The problem is the composition of the  $3d_{3/2}4d_{3/2} [J = 1]$  working level, which indicates the strength of level interaction. It is shown in Figure 4 for all  $3d4d [J = 1]$  levels in Ni-like ions with  $Z = 36-79$ . Figure 4 shows that contributions of the  $3d_{3/2}4d_{3/2} [J = 1]$  and  $3d_{3/2}4d_{5/2} [J = 1]$  levels are almost equal at  $Z = 42$ , which could lead to levels' misidentification. Theoretical energies of these levels at  $Z = 42$  are  $2,393,554 \text{ cm}^{-1}$  and  $2,400,846 \text{ cm}^{-1}$  (51% and 41%, respectively, are the contributions to the  $3d_{3/2}4d_{3/2} [J = 1]$  low working level). The contributions of these levels in [11] are 45% and 34%, and the energies are  $2,385,902 \text{ cm}^{-1}$  and  $2,393,229 \text{ cm}^{-1}$  respectively. (We note that the theoretical list of energies of Ni-like ions in the range of small  $Z$  is shifted as a whole by  $5000-8000 \text{ cm}^{-1}$ ). Figure 4 demonstrates the rapid restructuring of lower working level compositions: so that the  $3d_{5/2}4d_{3/2} [J = 1]$  level contribution increases by five orders of magnitude in the range  $Z = 40-42$ .



**Figure 4.** Composition of lower working level  $3d_{3/2}4d_{3/2} [J = 1]$  along Ni-like sequence on a logarithmic scale.

Figure 5 shows the scaled energies along  $Z$  of the  $3d_{3/2}4f_{5/2} [J = 1]$  upper working level and the close  $3p_{3/2}4s_{1/2} [J = 1]$  level. Crossing of these levels occurs in the range  $48 < Z < 49$ . At  $Z = 49$  one can see the “repulsion” of levels caused by their interaction; the “repulsion” is a feature of theoretical data. In Figure 5, the corresponding experimental energies for the  $3d_{3/2}4f_{5/2} [J = 1]$  level are shown [14]. Unfortunately, we have no available data on the experimental  $3p_{3/2}4s_{1/2} [J = 1]$  levels in the  $Z$  region under consideration. The value  $Z = 49$  is the point of an abrupt jump (irregularity) in spectroscopic

constants of the  $3d_{3/2}4f_{5/2} [J = 1]$  upper working level and the  $3p_{3/2}4s_{1/2} [J = 1]$  level crossing it, caused by the strong interaction of these levels at this value of  $Z$ . This interaction is shown in Figure 6, where we can see the  $3d_{3/2}4f_{5/2} [J = 1]$  level composition. The interaction of levels at the point  $Z = 49$  leads to the so-called effect of oscillator strength transfer we considered in [21] for the Ne-like sequence. At this point, the rate of radiative processes abruptly changes: the probabilities of the transition from the  $3d_{3/2}4f_{5/2} [J = 1]$  level to the ground state and to the state of the lower working level slightly decrease. At the same time, these probabilities for the  $3p_{3/2}4s_{1/2} [J = 1]$  level increase by an order of magnitude and become almost equal in magnitude to the corresponding values of the  $3d_{3/2}4f_{5/2} [J = 1]$  level. It can be assumed that there was an incorrect identification at the point  $Z = 49$  when extrapolating the upper working level in [4], and the  $3p_{3/2}4s_{1/2} [J = 1]$  level that is close to the  $3d_{3/2}4f_{5/2} [J = 1]$  level in energy was used as the upper working level (see Figure 5). If this assumption is correct,  $\lambda_{las} \sim 144.7 \text{ \AA}$  for  $Z = 49$ , which is identical to [4]. When using our value for  $3d_{3/2}4f_{5/2} [J = 1]$ ,  $\lambda_{las} \sim 140.0 \text{ \AA}$  (here the energy jump shown in Figure 5 is taken into account). Another argument in favor of the incorrect identification in [4], are large jumps of the differential  $d\lambda_{las}(Z) = \lambda_{las}(Z) - \lambda_{las}(Z-1)$  in the range  $Z = 47-50$ .

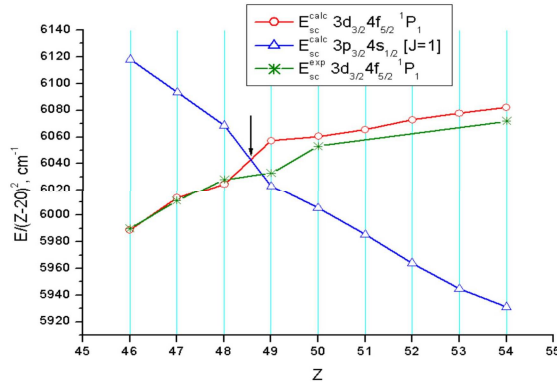


Figure 5. Crossing of upper working  $3d_{3/2}4f_{5/2} [J = 1]$  energy level with  $3p_{3/2}4s_{1/2} [J = 1]$  energy level in Ni-like sequence, shown by scaled energy values along  $Z$ . The corresponding experimental values for  $3d_{3/2}4f_{5/2} [J = 1]$  energies are also shown.

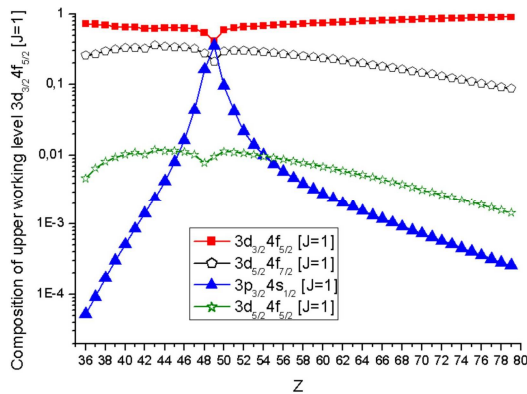


Figure 6. Composition of upper working level  $3d_{3/2}4f_{5/2} [J = 1]$  along Ni-like sequence on a logarithmic scale.

### 3. Wavelengths of the Self-Photopumped Nickel-Like $4f^1P_1 \rightarrow 4d^1P_1$ X-ray Laser Transitions

A comparison of the wavelengths of the self-photopumped nickel-like  $4f^1P_1 \rightarrow 4d^1P_1$  X-ray laser transitions, calculated using the RPTMP method with corresponding experimental values and shown in Figure 3, exhibits a deviation of  $\leq 1\%$  in the range  $Z = 37\text{--}46$ . For  $Z \geq 48$  Å, our results are identical to experimental data, with an accuracy of several units in the fourth significant digit. Two values of  $Z$  are exceptions: (i) the calculation instability point at  $Z = 42$ ; and (ii) the point  $Z = 49$ , where the  $3d_{3/2}4f_{5/2} [J = 1]$  and  $3p_{3/2}4s_{1/2} [J = 1]$  states are probably incorrectly identified in the calculation by the MCDF method in [4]. We estimated the accuracy of the calculation of the energies of the upper and lower working states for high  $Z$  using experimental measurements of various studies. As an example, we compared the experimental energies for  $Z = 74$  ( $W^{46+}$ ), obtained using the Super EBIT (electron beam ion trap) [22,23], presented in Table 1. There are also listed the theoretical results calculated using the MCDF method called Grasp92 [24]. Here, we do not present earlier calculations of other authors. We also note the impossible comparison to the other calculations [25] in view of the level identification entanglement in this paper.

**Table 1.** Energy levels ( $10^3 \text{ cm}^{-1}$ ) of W XLVII. Comparison of present calculations with experimental data [22,23] and with calculations by GRASP92 [24].

Configuration	Term	J	Experiment	Present Work	GRASP92
$3p^63d^{10}$	$^1S_0$	0	0.0	0.0	0.0
$3p^63d^94s$	$(5/2,1/2)$	3	12,601.5	12,600.1	
		2	12,616.44	12,615.2	12,591.1
$3p^63d^94s$	$(3/2,1/2)$	1	13,138.66	13,137.8	13,110.8
		2	13,148.2	13,147.4	13,120.7
$3p^63d^94p$	$(5/2,1/2)$	2	13,379.05	13,357.5	
		3	13,388.20	13,366.3	
$3p^63d^94p$	$(3/2,1/2)$	2	13,916.27	13,894.8	
		1	13,940.6	13,922.4	13,930.6
$3p^63d^94p$	$(5/2,3/2)$	1	14,229.0	14,234.9	14,221.0
$3p^63d^94p$	$(3/2,3/2)$	1	14,751.0	14,756.2	14,741.1
$3p^63d^94d$	$(3/2,3/2)$	1		15,935.9	15,924.2
$3p^63d^94d$	$(5/2,5/2)$	1	15,556.1	15,561.3	15,550.2
		2	15,610.2	15,614.9	15,605.0
$3p^53d^{10}4s$	$(3/2,1/2)$	1	16,247.0	16,258.9	
$3p^63d^94d$	$(3/2,3/2)$	0	16,256.2	16,284.7	16,282.9
$3p^63d^94f$	$(5/2,7/2)$	1	17,045.9	17,042.2	17,030.6
			17,574.7		
$3p^63d^94f$	$(3/2,5/2)$	1	17,580.3 *	17,586.5	17,585.6
$3p^53d^{10}4s$	$(1/2,1/2)$	1	18,727	18,726.4	18,724.4
$3p^53d^{10}4d$	$(3/2,3/2)$	1	19,044.4	19,041.8	19,057.5
$3p^53d^{10}4d$	$(3/2,5/2)$	1	19,244.5	19,234.8	19,244.1
$3p^53d^{10}4f$	$(3/2,7/2)$	2	20,589.0	20,600.1	20,613.8
$3p^53d^{10}4d$	$(1/2,3/2)$	1	21,561.0	21,547.0	21,614.6

\* Data from [23].

Good agreement between experimental and theoretical results for the energy levels in Table 1 may be noted: the maximum deviation is two units in the fourth significant digit. For the problem under study, it is important to ascertain the high accuracy of the calculation of the upper and lower working levels. For the experimental energy of the  $3d_{3/2}4f_{5/2} [J = 1]$  level, Table 1 gives two values: one obtained in the experiments [22], and the other later [23]. The difference with our calculation is 6 units in the fifth significant digit. We did not find the experimental energy of the  $3d_{3/2}4d_{3/2} [J = 1]$  lower working level for high  $Z$  in the literature. The energies of two other states of the  $3d4d$  configuration with  $J = 1, 2$ , given in Table 1, also agree with high accuracy, which indirectly confirms the calculation

reliability. Wavelengths of the  $3d_{3/2}4f_{5/2} (^1P_1) - 3d_{3/2}4d_{3/2} (^1P_1)$  SPP laser transitions in Ni-like sequence calculated by RPTMP are listed in Table 2.

**Table 2.** Wavelengths ( $\lambda_{las}$ , Å) of the  $3d_{3/2}4f_{5/2} (^1P_1) - 3d_{3/2}4d_{3/2} (^1P_1)$  SPP laser transitions in Ni-like sequence calculated by RPTMP.

Z	$\lambda_{las}$
50	134.08
51	128.12
52	122.54
53	117.39
54	112.66
55	108.36
56	104.295
57	100.51
58	96.98
59	93.68
60	90.57
61	87.65
62	84.89
63	82.28
64	79.81
65	77.47
66	75.23
67	73.08
68	71.06
69	69.11
70	67.25
71	65.47
72	63.75
73	62.10
74	60.51
75	58.97
76	57.48
77	56.04
78	54.64
79	53.23

#### 4. Conclusions

The data on  $\lambda_{las}$  (see Table 2) were obtained a priori, no fittings were used. The error could be several units in the fourth significant digit. The precision wavelengths of laser transitions are necessary, in particular, to determine ions in which intense laser emission is possible at wavelengths for which multilayer mirrors (MM) with high reflectance are developed. At least three values of  $\lambda_{las}$  are of interest from the viewpoint of the development of XRL-based sources for nanolithography.

- (i) For  $Z = 50$ ,  $\lambda_{las} \sim 134.1$  Å. For this wavelength region, MMs for nanolithography were developed as early as in 1993 [26]. The maximum normal incidence reflectivity achieved that time was 66% for a Mo/Si MM at  $\lambda = 13.4$  nm, the reflectivity can be increased to 70%.
- (ii) For  $Z = 54$   $\lambda_{las} \sim 11.3$  nm. A series of normal-incidence reflectance measurements at just longer than the beryllium K-edge (11.1 nm) from Mo/Be MM was reported in [27]. The highest peak reflectance was  $68.7 \pm 0.2\%$  at 11.3 nm obtained from a MM with 70 bilayers ending in beryllium. Our model of the high efficient monochromatic radiation sources near  $\lambda = 13.5$  at 11.3 nm obtained in  $Xe^{26+}$ , intended for commercial nanolithography, was presented in our recent work [28].
- (iii) In Ni-like Ytterbium ( $Z = 70$ ),  $\lambda_{las} \approx 67.25$  Å. MM for wavelengths of 6.71–6.89 nm were developed in [29]. Summary of measured and calculated reflectivity of La/B MM for these wavelengths is listed in Table 1 of [29]. The largest reflectivity was observed and calculated for  $\lambda = 6.71$ –6.74 nm.

The crossing region of each working level with another level is characterized by their strong effect on each other, which can cause strong instability of the energy structure in the crossing region. In such regions, jumps in functions of energy levels and probabilities of radiative transition on  $Z$  are possible (see Figure 2a). The authors of [30], where the level crossing in the Ni-like sequence and associated irregularities in the functions of energies and probabilities of radiative transitions in the range  $Z = 74\text{--}84$  were studied, arrived at the same conclusion. From this, the conclusion regarding the possible incorrect identification of levels in their crossing regions follows.

The SPP XRL can be very sensitive to external fields. It is implied that even an insignificant change in the plasma density can affect the emission spectrum. The remarkable phenomenon (see Figure 4) where a rapid increase in the contribution of the  $3d_{5/2}4d_{3/2} [J = 1]$  level to the composition of the lower working level is demonstrated could be an indirect confirmation of this. In the interval  $Z = 40\text{--}42$ , the contribution of this level increases by five orders of magnitude. A similar pattern is observed in Figure 6, where the contribution of  $3p_{3/2}4s_{1/2} [J = 1]$  also rapidly increases to  $Z = 49$ , where this level strongly interacts with the upper working level. In this case, the oscillator strength is transferred from the upper working level to the  $3p_{3/2}4s_{1/2} [J = 1]$  level.

**Conflicts of Interest:** The authors declare no conflict of interest.

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Article

# Configuration Interaction Effects in Unresolved $5p^6 5d^{N+1} - 5p^5 5d^{N+2} + 5p^6 5d^N 5f^1$ Transition Arrays in Ions $Z = 79-92$

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Academic Editor: Joseph Reader

Received: 12 April 2017; Accepted: 12 May 2017; Published: 21 May 2017

**Abstract:** Configuration interaction (CI) effects can greatly influence the way in which extreme ultraviolet (EUV) and soft X-ray (SXR) spectra of heavier ions are dominated by emission from unresolved transition arrays (UTAs), the most intense of which originate from  $\Delta n = 0$ ,  $4p^6 4d^{N+1} - 4p^5 4d^{N+2} + 4p^6 4d^N 4f^1$  transitions. Changing the principle quantum number  $n$ , from 4 to 5, changes the origin of the UTA from  $\Delta n = 0$ ,  $4p^6 4d^{N+1} - 4p^5 4d^{N+2} + 4p^6 4d^N 4f^1$  to  $\Delta n = 0$ ,  $5p^6 5d^{N+1} - 5p^5 5d^{N+2} + 5p^6 5d^N 5f^1$  transitions. This causes unexpected and significant changes in the impact of configuration interaction from that observed in the heavily studied  $n = 4 - n = 4$  arrays. In this study, the properties of  $n = 5 - n = 5$  arrays have been investigated theoretically with the aid of Hartree-Fock with configuration interaction (HF-CI) calculations. In addition to predicting the wavelengths and spectral details of the anticipated features, the calculations show that the effects of configuration interaction are quite different for the two different families of  $\Delta n = 0$  transitions, a conclusion which is reinforced by comparison with experimental results.

**Keywords:** configuration interaction (CI); unresolved transition array (UTA); Cowan code

## 1. Introduction

Laser produced plasmas (LPPs) from tin droplet targets have been adopted as the optimum extreme ultraviolet (EUV) light sources for next generation lithography for high-volume manufacturing (HVM) of semiconductor circuits with feature sizes of 10 nm or less [1,2]. Transitions of the type  $4p^6 4d^{N+1} - 4p^5 4d^{N+2} + 4p^6 4d^N 4f^1$  in  $\text{Sn}^{8+} - \text{Sn}^{13+}$  merge to form an unresolved transition array (UTA) [3] which contains thousands of individual lines and emits strongly in such a plasma at an electron temperature of  $\sim 30$  eV in a narrow wavelength range around 13.5 nm [4,5]. This value coincides with the wavelength of peak reflectance of  $\sim 70\%$  of the Mo/Si multilayer mirrors (MLMs) that are used in the scanning tools [6] and tin plasmas are the brightest sources at this wavelength. Other recent research has concentrated on investigating future-generation lithographic sources at shorter wavelengths, in particular at 6.75 nm where an intense UTA is emitted by gadolinium and terbium plasmas with an electron temperature of close to 100 eV [7–9], and where  $\text{LaB}_4\text{C}$  and  $\text{LaNB}_4\text{C}$  MLMs have a peak theoretical reflectivity of close to  $\sim 80\%$  [10]. Once more the transitions responsible are predominantly of the type  $4p^6 4d^{N+1} - 4p^5 4d^{N+2} + 4p^6 4d^N 4f^1$ .

Moving to shorter wavelengths, we encounter the “water window” (2.3–4.4 nm) spectral region lying between the K-edges of carbon and oxygen, where carbon K-edge absorption is strong, but oxygen L edge absorption is weak, and where sources are being developed for in vivo single shot imaging

and tomography of biological samples in aqueous environments with nm resolution [11,12]. Initially, sources in this region used strong quasi-monochromatic emission at wavelengths of  $\lambda = 2.879$  nm and  $\lambda = 2.478$  nm arising from the  $1s^2-1s\ 2p$  line in  $N^{5+}$  and the  $1s-2p$  doublet in  $N^{6+}$  respectively [13]. However more recently  $4d-4f$  transitions of the  $4p^6 4d^{N+1} - 4p^5 4d^{N+2} + 4p^6 4d^N 4f^1$  UTA in  $Bi^{37+}-Bi^{46+}$  have been proposed, and a Bi source based on a plasma heated to a sufficient temperature ( $T_e > 500$  eV) to generate these ion stages is under development for water window imaging [14].

The dominant emission in all of these sources arises from  $4p^6 4d^{N+1} - 4p^5 4d^{N+2} + 4p^6 4d^N 4f^1$  transitions and due to the near degeneracy of the  $4p^5 4d^{N+2}$  and  $4d^N 4f$  configurations, it is well known that it is necessary to allow for configuration interaction (CI) in the upper state [4,15,16]. The effects of CI in any particular ion stage have been shown to cause a strong spectral narrowing and concentrate the available emission intensity at the high energy end of the array. Moreover, although the  $4p^5 4d^{N+2}$  configuration must be included in order to obtain the correct energy eigenvalues and eigenvectors, the latter remain sufficiently pure while the emission is dominated by the valence  $4p^6 4d^{N+1} - 4p^6 4d^N 4f^1$  transitions and there is little evidence in any spectrum of a sizable contribution in emission from  $4p^6 4d^{N+1} - 4p^5 4d^{N+2}$  lines until  $N = 1$ . This is presumably due to the electron impact excitation rates for valence and sub-valence excitation responsible for populating the upper states being very different. Based on a simple line strengths comparison, the ratio of total lines strengths for  $p-d$  transitions to that for  $d-f$  should scale as  $9-N/N+1$  times the ratio of their respective dipole matrix elements [17]. So one would expect the  $p-d$  contribution to overtake that for  $d-f$  with increasing ionization around  $n = 3$  [17]. Moreover, if one allows for spin orbit splitting of the  $4p$  and  $4d$  subshells, for  $N > 4$  the lowest configuration will be  $4p^2_{1/2} 4p^4_{3/2} 4d^4_{3/2} 4d^{N-4}_{5/2}$ . Thus if it is easier to collisionally excite outer electrons, for  $N > 4$  the dominant excitation will involve  $4d_{5/2}$  electrons and the transitions expected are:  $4p^2_{1/2} 4p^4_{3/2} 4d^4_{3/2} 4d^{N-4}_{5/2} - 4p^2_{1/2} 4p^3_{3/2} 4d^4_{3/2} 4d^{N-3}_{5/2} + 4p^2_{1/2} 4p^4_{3/2} 4d^4_{3/2} 4d^{N-5}_{5/2} 4f^1$ .

For  $N < 4$ , the lowest configuration will be  $4p^2_{1/2} 4p^4_{3/2} 4d^N_{3/2}$  and transitions can now take place to  $4p^2_{1/2} 4p^4_{3/2} 4d^N_{3/2} - 4p^2_{1/2} 4p^3_{3/2} 4d^{N+1}_{3/2} + 4p^1_{1/2} 4p^4_{3/2} 4d^{N+1}_{3/2} + 4p^2_{1/2} 4p^4_{3/2} 4d^{N-1}_{3/2} 4f^1$  with the  $4p_{1/2}-4d_{3/2}$  contribution appearing on the short wavelength side of the UTA, or, if the  $4p$  spin orbit splitting is sufficiently large, forming a second UTA at a shorter wavelength.

However, both sets of transitions are responsible for absorption by ions in the plasma periphery which is the major problem that must be overcome to attain the maximum conversion efficiency of laser to spectral emission energy in EUV source development. Theoretical studies of the effects of CI in ions from  $Z = 50 - Z = 89$  have been reported which showed that CI effects in general diminish as  $Z$  increases as the upper state arrays separate in energy [18,19] and recently the corresponding UTA emission in a number of elements at the higher  $Z$  end of this sequence has been observed [20,21].

In the absence of CI, according to the UTA formalism, for  $4p^6 4d^{N+1} - 4p^6 4d^N 4f^1$  transitions the position of the line strength weighted mean of an array is shifted from the position of the differences in average energies by an amount [22]

$$\delta E = \frac{35}{9}(N) \left[ \sum_{k \neq 0} f_k F^k(4d, 4f) + g_k G^k(4d, 4f) \right] \tag{1}$$

where  $F^k(4d, 4f)$  and  $G^k(4d, 4f)$  are Slater Condon direct and exchange integrals respectively and the coefficients  $f_k$  and  $g_k$  result from integrals over polar and azimuthal angles that, in general, decrease with increasing  $k$  [23]. Here  $g_1 = 137/2450$  has the largest numerical value and the above formula can be roughly approximated as  $\delta E = \frac{2}{9} N G^1(4d, 4f)$  [24] so that the position of the emission peak is determined by the degree of  $4d$  and  $4f$  overlap. In higher ion stages (beyond  $\sim 4+$ ) of the rare earths, where  $G^1(4d, 4f)$  is almost constant for different ion stages of a given element, the effect of CI is to essentially remove this  $N$  dependence and the array is narrowly peaked at around  $2G^1(4d, 4f)$  above the difference between the average energies of the ground and upper state configurations. Thus the UTAs in successive ion stages overlap with each other to yield a very intense, relatively narrow ( $\Delta E \sim 10$  eV), emission band in a low opacity plasma, whose shape is completely modified by increasing opacity [25].

In performing calculations for low ion stages of the lighter lanthanides and the elements preceding them in the periodic table, it is necessary to expand the excited state basis to include higher  $nf$  orbitals or reduce the effective exchange interaction. This is achieved by scaling the  $G^1(4d, 4f)$  parameter, as is done in calculations with the Cowan code, in order to obtain good agreement between calculated and observed results. Mixing of  $4f$  and  $nf$  orbitals essentially increases the mean radius of the  $4f$  wave function and so leads to a reduction in the size of both direct and exchange integrals [26]. The photoionization spectra of low ion stages of these elements are well known to be dominated by  $4f$  contraction effects and the correct estimation of the  $4f$  radial wave function is essential if good agreement between theory and experimental spectra is to be obtained [27].

For the elements from Ag to La,  $4f$  contraction increases with ion stage due to the interplay between the attractive Coulomb and centrifugal repulsion  $\left(\frac{l(l+1)}{2\mu r^2}\right)$  terms in the effective radial potential, where  $l$  is the orbital angular momentum quantum number and  $\mu$  is the reduced mass of the electron. In the neutral atom, the effective potential is bimodal with an inner well close to the nucleus, whose depth rapidly increases from  $Z = 47$  (silver), where it first appears, to  $Z = 58$  (cerium), where it first supports a bound state leading to the formation of the lanthanides [27,28]. This inner well is separated by a centrifugal barrier from a broad outer well with a minimum near the hydrogenic value of  $16a_0$ . The EUV absorption spectrum of these elements is dominated by a large  $4d$ - $\epsilon f$  shape resonance [29] since depending on  $Z$ ,  $4d$ - $\epsilon f$  excitation can only occur when the  $\epsilon f$  photoelectron has sufficient energy to surmount the centrifugal barrier, or the lowest state of the inner well is autotomizing. Due to the lack of any appreciable overlap between the  $4d$  wave function, which lies in the core, and the bound  $nf$  wave functions which are eigenstates of the outer well,  $4d$ - $4f$  transitions have vanishing oscillator strength. With increasing ionization, the inner well deepens, the potential barrier decreases, and the outer-well  $nf$  functions gradually contract into the inner well region. As they do, the  $4d, 4f$  overlap increases and the intensity of  $4d$ - $4f$  transitions increases and the oscillator strength, associated with  $4d$ - $\epsilon f$  in the neutral is effectively transferred to  $4d$ - $4f$  excitation [30].

In contrast to the situation for  $\Delta n = 0, n = 4 - n = 4$  transitions, no systematic study of the equivalent  $\Delta n = 0, n = 5 - n = 5$  transitions has been reported. From studies of the photoionization cross-sections of neutral elements past  $Z = 79$  (gold) it is known that the spectra display strong  $5d$ - $\epsilon f$  resonances and that any difference from their  $4d$ - $\epsilon f$  counterparts can be attributed to the increased influence of spin-orbit effects [30–33]. UTAs due to  $5p^6 5d^{N+1} - 5p^5 5d^{N+2} + 5p^6 5d^N 5f^l$  transitions in LPPs of Th and U have been observed and some of the simpler transitions identified [34,35]. Compared to the  $4p^6 4d^{N+1} - 4p^5 4d^{N+2} + 4p^6 4d^N 4f^l$  UTAs observed under identical experimental conditions in the homologous elements Ba and Ce, the  $n = 5 - n = 5$  UTAs were broader [36]. Spectra from ionized uranium that were recorded following impurity injection into the TEXT Tokamak were found to contain two distinct UTAs which were assigned primarily to  $5p_{1/2} - 5d$  and  $5d - 5f$  component groups of  $5p^6 5d^{N+1} - 5p^5 5d^{N+2} + 5p^6 5d^N 5f^l$  transitions in U XV –U XXXI [37]. However, apart from this work, no calculations were performed to elucidate and explore CI effects.

In this paper, we report on the results of calculations for  $5p^6 5d^{N+1} - 5p^5 5d^{N+2} + 5p^6 5d^N 5f^l$  transitions in elements from  $Z = 79$  to  $Z = 92$  to predict the positions and spectral properties of the corresponding UTAs and in particular to compare the effects of CI between  $\Delta n = 0, n = 5 - n = 5$  transitions in these elements and  $n = 4 - n = 4$  transitions in their homologous, lower  $Z$  counterparts.

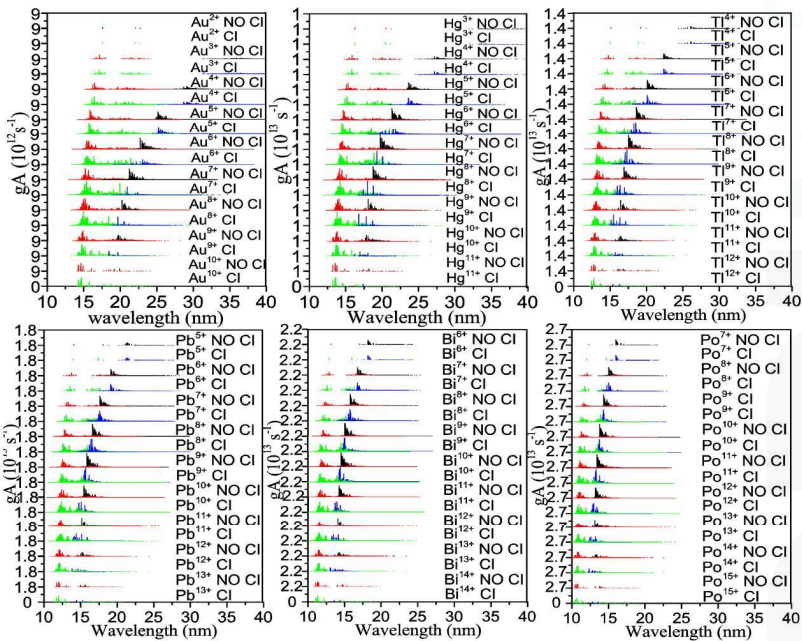
## 2. Results

### 2.1. $5p - 5d$ and $5d - 5f$ Unresolved Transition Arrays of Ions with $Z = 79 - 92$

Calculations were performed using the Hartree-Fock with Configuration Interaction (HFCI) suite of codes written by Cowan [17]. Because of the high  $Z$  of the atoms and ions of interest, relativistic effects which are the mass-velocity and Darwin contributions to the energy were included. The Slater Condon  $F^k, G^k,$  and  $R^k$  parameters were scaled to 90% of their *ab initio* values while the spin orbit parameters were unchanged. Energies and wavelengths were determined for  $5p^6 5d^{N+1} - 5p^5 5d^{N+2} + 5p^6 5d^N 5f^l$

transitions both with and without CI for all ions with  $N = 0-8$  of the elements considered. For the CI calculations, the eigenvectors percentage compositions were used to assign  $5d-5f$  and  $5p-5d$  lines within the overall arrays.

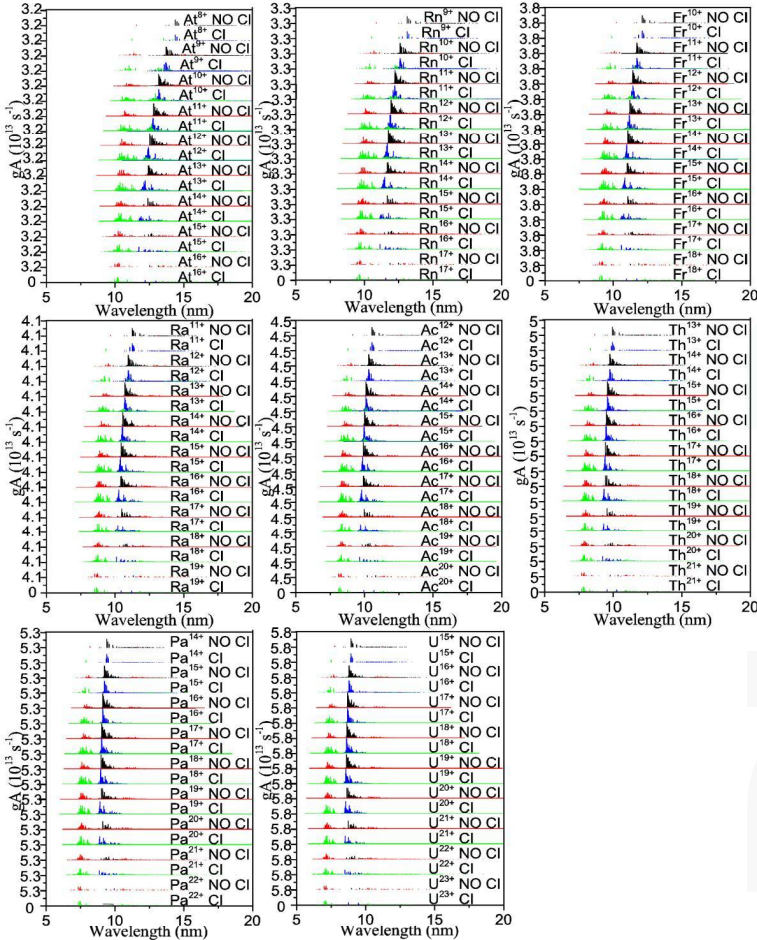
The results of these calculations are presented in Figures 1 and 2. Figure 1 shows the calculated spectra for ions of the elements from Au ( $Z = 79$ ) to Po ( $Z = 84$ ), while Figure 2 contains the corresponding data for ions from At ( $Z = 85$ ) to U ( $Z = 92$ ). For each element, the green and red line distributions denote  $5p-5d$  transitions with and without CI included, respectively, while blue and black denote  $5d-5f$  transitions with and without CI included. In the case of Au, the most obvious feature of the spectra is that with increasing ion stage, the  $5p-5d$  transition arrays move slowly towards shorter wavelength while the  $5d-5f$  transition arrays move more rapidly towards higher energy with increasing ion stage. The arrays never overlap and so CI effects are almost non-existent up to  $Au^{5+}$  and from  $Au^{6+}$  onwards, CI mainly affects the  $5d-5f$  transitions where they dramatically alter the line distributions. It should be noted that most or all of the  $5p-5d$  transitions are autoionizing until we reach  $Au^{7+}$  and even if the upper states are populated, they will never appear in emission. The near absence of CI for  $5d-5f$  transitions in lower stages and the closeness in energy of the  $5d-5f$  sub-arrays in the higher stages would suggest that the intensity weighted mean positions of these arrays should be given by Equation (1). The fact that the arrays move to shorter wavelength so dramatically is due to the  $5f$  wave function contraction which leads to both an increase in the separation of average energies of the upper and lower configurations and also a rapid increase in  $G^1(5d, 5f)$ . Similar behavior, in the case of  $4d-4f$  transitions has been found in Sn spectra [38].



**Figure 1.** (Color online) Ir-like through Tm-like spectra of Au-Po calculated with the Cowan Code both including Configuration interaction (CI) (green denotes  $5p-5d$  and blue denotes  $5d-5f$ ) and excluding CI (red denotes  $5p-5d$  and black denotes  $5d-5f$ ).

In the case of Hg and Tl, CI effects again become important for  $5d-5f$  spectra at  $Hg^{6+}$  and  $Tl^{6+}$ . For Pb and Bi the effects of CI on  $5d-5f$  transitions are predicted to become noticeable at  $Pb^{7+}$  and  $Bi^{7+}$ , while in all cases the changes in the  $5p-5d$  sub-arrays only become noticeable when they begin to

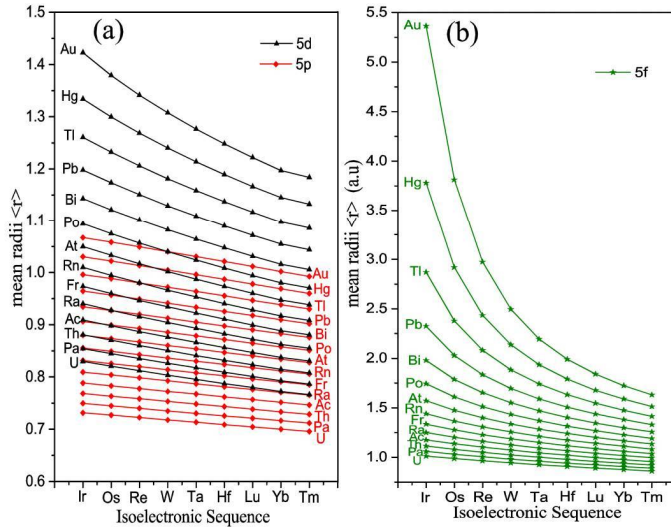
overlap with the  $5d-5f$  sub-arrays and where a redistribution of intensity towards the higher energy end of the overall arrays become visible. With increasing  $Z$ ,  $5f$  contraction effects diminish as the transitions now involve significantly higher charge state ions. As can be seen from Figure 2, the  $5p-5d$  and  $5d-5f$  sub-arrays become closer and CI effects cause subtle changes to the spectral profiles of both sub-arrays for situations where the  $5p^6 5d^{N+1}$  ground configuration has  $N > 3$  and more dramatic effects when  $N \leq 3$ .



**Figure 2.** (Color online) Ir-like through Tm-like spectra of At-U calculated with the Cowan Code both including CI (green denotes  $5p-5d$  and blue denotes  $5d-5f$ ) and excluding CI (red denotes  $5p-5d$  and black denotes  $5d-5f$ ).

To explore the effects of wave function contraction with increasing ion stage, the radial wave functions  $P_{n,l}(r)$  were extracted for  $5p$ ,  $5d$ , and  $5f$  electron orbitals for each ion considered. From these the mean radius  $\langle r \rangle$  was computed using  $\langle r \rangle = \int_0^\infty P_{n,l}^2 r dr$  and the results are presented in Figure 3. It is clear from this figure that the mean radii of the  $5p$  and  $5d$  functions decrease slowly with  $Z$  and charge state. The situation for the  $5f$  wave function is very different. In Au, for example,  $\langle r \rangle$  contracts from  $5.4a_0$  in  $Au^{2+}$  to  $1.5a_0$  in  $Au^{10+}$ . With increasing  $Z$ , the effect is less dramatic and past Ra, the  $5f$

contacts with increasing ionization much like the  $5p$  and  $5d$ . This is mirrored in the spectra by the fact that separation of the  $5p-5d$  and  $5d-5f$  arrays becomes essentially constant as the  $5d-5f$  array does not dramatically move to higher energy with increasing charge.



**Figure 3.** (Color online) mean radii of  $5p$ ,  $5d$ , and  $5f$  eigenfunctions for ions of the Ir (ground state  $5d^9$ ) through Tm (ground configuration  $5d^1$ ) for all elements from Au-U.

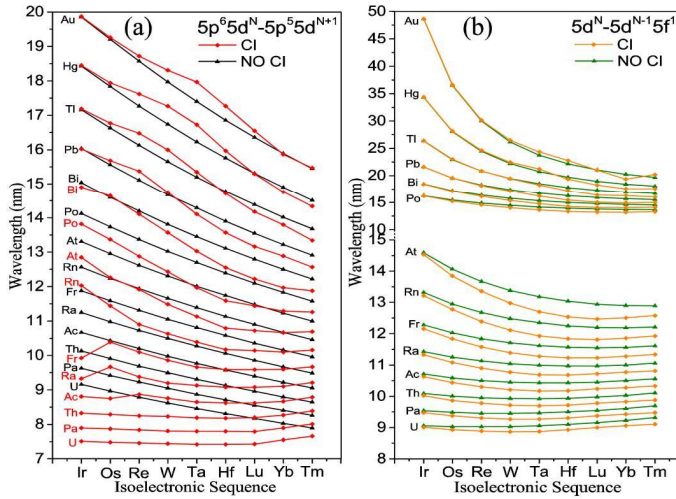
2.2.  $5p-5d$  and  $5d-5f$  UTA Statistics of Ions with  $Z = 79-92$

In general, the complexity of arrays with  $1 < N < 8$ , the UTA formalism is suitable for the parameterization of the calculated wavelength data [3,21]. The general  $n$ th-order moment for a set of  $N$  values  $\lambda_i$  with line strengths  $\omega_i$  reads

$$\mu_n = \sum_{i=1}^N \omega_i \lambda_i^n / W \tag{2}$$

where  $W = \sum_{i=1}^N \omega_i$  is the total line strength. The first-order moment  $\mu_1$  gives the intensity weighted average wavelength. The centered second-order moment  $\mu_2^c = \mu_2 - \mu_1^2$  gives the variance,  $\nu$ , which is obtained by the above expression after replacing  $\lambda_i$  by  $\lambda_i - \mu_1$ . For a Gaussian-shaped distribution, its full width at half maximum (FWHM) is given by  $2(2 \ln 2)^{1/2} \sigma = 2.355\sigma$ , where  $\sigma = (\mu_2^c)^{1/2}$ . Thus the variance is related to the width of the array. Using the UTA formalism described above, the  $gA$  weighted UTA positions and widths for the  $5d-5f$  and  $5p-5d$  component sub-arrays of the  $5p^6 5d^{N+1} - 5p^5 5d^{N+2} + 5p^6 5d^N 5f^1$  array were calculated and the results are presented in Figure 4 and Tables 1 and 2. Separate UTAs for  $5p-5d$  and  $5d-5f$  transitions were identified from their eigenvector compositions and UTA statistics were computed for both sets of transitions with and without CI effects included for comparison. From this figure it is clear that in the case of  $5d-5f$  transitions, which will be observed in emission from a plasma, the effect of CI is to shift the corresponding sub-array towards higher energy especially for the higher  $Z$  elements. This trend is also clear from Tables 1 and 2. Interestingly, unlike the corresponding  $4-4$  arrays, where spectral narrowing is the dominant effect observed, the effect of CI is actually to increase the width of the UTAs. Again, during the rapid contraction phase of the  $5f$  wave function in lower ion stages of the lighter elements, CI effects are

noticeably absent as can be seen from the coincidence in energies in both cases. For  $5p-5d$  transitions, CI effects are somewhat different also for lighter and heavier elements. For the elements past francium, the mean energies are shifted by CI towards higher values in lower ion stages and gradually converge towards their non-CI value at the highest ion stage.



**Figure 4.** (Color online) Mean wavelength of transition arrays  $5p^6 5d^{N+1} - 5p^5 5d^{N+2}$  and of  $5p^6 5d^{N+1} - 5p^6 5d^N 5f^1$  Ir-like through Tm-like ions of gold through uranium (a)  $5p^6 5d^{N+1} - 5p^5 5d^{N+2}$  including CI (red) and excluding CI (black); (b)  $5p^6 5d^{N+1} - 5p^6 5d^N 5f^1$  including CI (orange) and excluding CI (green).

**Table 1.** Calculated mean wavelength  $\bar{\lambda}_{gA}$  (nm) and spectral width  $\Delta\lambda_{gA}$  (nm) for the UTA of gold through astatine ions: Ir-like to Tm-like ions for the  $5d-5f$  arrays without and with the effect of configuration interaction.

$5d-5f$ (No CI)	Au		Hg		Tl		Pb		Bi		Po		At	
Ion	$\bar{\lambda}_{gA}$	$\Delta\lambda_{gA}$	$\bar{\lambda}_{gA}$	$\Delta\lambda_{gA}$	$\bar{\lambda}_{gA}$	$\Delta\lambda_{gA}$	$\bar{\lambda}_{gA}$	$\Delta\lambda_{gA}$	$\bar{\lambda}_{gA}$	$\Delta\lambda_{gA}$	$\bar{\lambda}_{gA}$	$\Delta\lambda_{gA}$	$\bar{\lambda}_{gA}$	$\Delta\lambda_{gA}$
Ir-like	48.62	5.99	34.33	3.11	26.40	1.97	21.59	1.47	18.45	1.23	16.23	1.08	14.59	0.98
Os-like	36.54	3.83	28.09	2.39	22.96	1.80	19.58	1.51	17.21	1.34	15.44	1.22	14.06	1.13
Re-like	29.99	2.77	24.48	2.09	20.84	1.77	18.27	1.57	16.36	1.43	14.87	1.32	13.67	1.24
W-like	26.17	2.35	22.23	1.98	19.45	1.76	17.37	1.61	15.75	1.48	14.46	1.38	13.38	1.30
Ta-like	23.77	2.16	20.74	1.91	18.48	1.74	16.72	1.60	15.31	1.49	14.15	1.40	13.18	1.32
Hf-like	22.17	2.00	19.70	1.82	17.79	1.67	16.25	1.55	14.99	1.45	13.94	1.37	13.04	1.29
Lu-like	21.05	1.80	18.96	1.65	17.29	1.53	15.91	1.43	14.77	1.35	13.79	1.28	12.94	1.21
Yb-like	20.25	1.48	18.42	1.37	16.92	1.29	15.67	1.21	14.61	1.15	13.69	1.10	12.90	1.05
Tm-like	19.67	0.87	18.03	0.83	16.67	0.80	15.51	0.78	14.52	0.76	13.65	0.75	12.89	0.74
$5d-5f$ (CI)	Au		Hg		Tl		Pb		Bi		Po		At	
Ion	$\bar{\lambda}_{gA}$	$\Delta\lambda_{gA}$	$\bar{\lambda}_{gA}$	$\Delta\lambda_{gA}$	$\bar{\lambda}_{gA}$	$\Delta\lambda_{gA}$	$\bar{\lambda}_{gA}$	$\Delta\lambda_{gA}$	$\bar{\lambda}_{gA}$	$\Delta\lambda_{gA}$	$\bar{\lambda}_{gA}$	$\Delta\lambda_{gA}$	$\bar{\lambda}_{gA}$	$\Delta\lambda_{gA}$
Ir-like	48.64	6.00	34.36	3.16	26.43	2.10	21.60	1.69	18.43	1.45	16.19	1.25	14.53	1.10
Os-like	36.62	3.90	28.17	2.60	23.02	2.17	19.58	2.00	17.09	1.90	15.24	1.56	13.85	1.30
Re-like	30.15	2.99	24.63	2.69	20.86	2.66	18.16	2.51	16.13	2.07	14.55	1.61	13.36	1.36
W-like	26.48	2.89	22.47	3.18	19.43	3.05	17.12	2.58	15.33	2.03	14.00	1.59	12.98	1.37
Ta-like	24.34	3.15	21.21	3.46	18.24	3.00	16.18	2.35	14.75	1.85	13.62	1.55	12.70	1.39
Hf-like	22.79	3.29	19.36	3.60	17.19	2.64	15.46	2.03	14.26	1.68	13.33	1.50	12.54	1.43
Lu-like	21.01	3.24	18.25	2.88	16.35	2.08	15.02	1.73	14.06	1.61	13.20	1.51	12.47	1.43
Yb-like	19.37	2.34	17.60	1.79	16.25	1.42	14.92	1.70	14.06	1.53	13.18	1.37	12.51	1.37
Tm-like	20.19	0.16	17.56	0.12	15.99	1.05	14.98	1.00	14.09	0.97	13.29	0.94	12.58	0.92

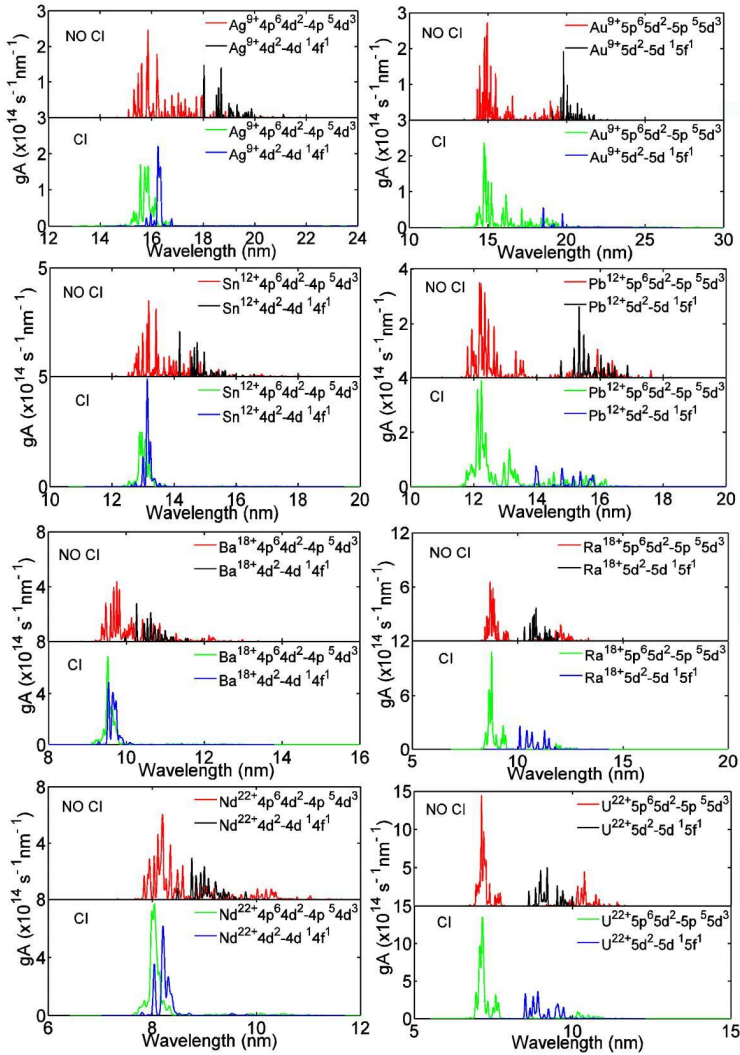


**Table 2.** Calculated mean wavelength  $\bar{\lambda}_{gA}$  (nm) and spectral width  $\Delta\lambda_{gA}$  (nm) for the UTA of radon through uranium ions: Ir-like to Tm-like ions for the  $5d-5f$  arrays without and with the effect of configuration interaction.

$5d-5f$ (No CI)	Rn		Fr		Ra		Ac		Th		Pa		U	
Ion	$\bar{\lambda}_{gA}$	$\Delta\lambda_{gA}$	$\bar{\lambda}_{gA}$	$\Delta\lambda_{gA}$	$\bar{\lambda}_{gA}$	$\Delta\lambda_{gA}$	$\bar{\lambda}_{gA}$	$\Delta\lambda_{gA}$	$\bar{\lambda}_{gA}$	$\Delta\lambda_{gA}$	$\bar{\lambda}_{gA}$	$\Delta\lambda_{gA}$	$\bar{\lambda}_{gA}$	$\Delta\lambda_{gA}$
Ir-like	13.32	0.91	12.28	0.85	11.43	0.80	10.71	0.77	10.09	0.73	9.54	0.71	9.06	0.68
Os-like	12.95	1.06	12.03	1.00	11.25	0.95	10.59	0.90	10.01	0.86	9.49	0.83	9.03	0.80
Re-like	12.68	1.16	11.84	1.10	11.13	1.04	10.50	1.00	9.95	0.95	9.46	0.92	9.03	0.88
W-like	12.48	1.22	11.71	1.16	11.04	1.10	10.45	1.05	9.93	1.01	9.46	0.97	9.03	0.94
Ta-like	12.35	1.25	11.62	1.18	10.99	1.13	10.43	1.08	9.92	1.04	9.47	1.00	9.06	0.97
Hf-like	12.25	1.23	11.57	1.17	10.97	1.12	10.43	1.08	9.94	1.04	9.50	1.00	9.10	0.97
Lu-like	12.20	1.16	11.55	1.11	10.97	1.07	10.45	1.03	9.98	1.00	9.55	0.97	9.16	0.94
Yb-like	12.19	1.01	11.56	0.98	11.00	0.95	10.50	0.92	10.03	0.90	9.61	0.88	9.23	0.86
Tm-like	12.21	0.73	11.61	0.72	11.06	0.72	10.56	0.71	10.11	0.71	9.70	0.71	9.32	0.71
$5d-5f$ (CI)	Rn		Fr		Ra		Ac		Th		Pa		U	
Ion	$\bar{\lambda}_{gA}$	$\Delta\lambda_{gA}$	$\bar{\lambda}_{gA}$	$\Delta\lambda_{gA}$	$\bar{\lambda}_{gA}$	$\Delta\lambda_{gA}$	$\bar{\lambda}_{gA}$	$\Delta\lambda_{gA}$	$\bar{\lambda}_{gA}$	$\Delta\lambda_{gA}$	$\bar{\lambda}_{gA}$	$\Delta\lambda_{gA}$	$\bar{\lambda}_{gA}$	$\Delta\lambda_{gA}$
Ir-like	13.22	0.99	12.16	0.84	11.33	0.77	10.63	0.71	10.02	0.68	9.48	0.65	9.01	0.63
Os-like	12.78	1.11	11.84	0.98	11.08	0.90	10.44	0.83	9.87	0.79	9.38	0.77	8.93	0.74
Re-like	12.39	1.19	11.58	1.06	10.90	0.99	10.30	0.94	9.78	0.90	9.31	0.87	8.89	0.85
W-like	12.11	1.22	11.39	1.15	10.77	1.09	10.21	1.05	9.72	1.01	9.27	0.98	8.87	0.96
Ta-like	11.93	1.29	11.28	1.24	10.69	1.19	10.17	1.14	9.70	1.11	9.27	1.01	8.88	1.05
Hf-like	11.84	1.36	11.23	1.30	10.68	1.27	10.18	1.23	9.72	1.18	9.31	1.15	8.93	1.12
Lu-like	11.81	1.38	11.23	1.32	10.72	1.29	10.24	1.26	9.78	1.22	9.38	1.18	9.00	1.14
Yb-like	11.86	1.27	11.28	1.22	10.77	1.17	10.28	1.12	9.83	1.08	9.43	1.06	9.06	1.04
Tm-like	11.93	0.90	11.34	0.89	10.81	0.87	10.33	0.86	9.88	0.85	9.48	0.84	9.11	0.83

**3. Comparison of  $5p^65d^{N+} - 5p^55d^{N+2} + 5p^65d^N5f^1$  with  $4p^64d^{N+1} - 4p^54d^{N+2} + 4p^64d^N4f^1$  Arrays**

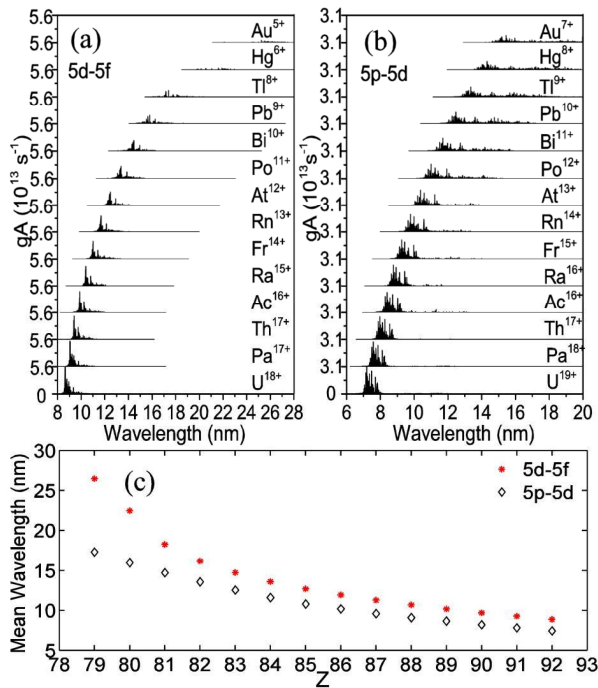
In the case of  $4p^64d^{N+1} - 4p^54d^{N+2} + 4p^64d^N4f^1$  transitions, as already discussed, configuration interaction leads to a strong spectral narrowing and redistribution of oscillator strength towards the high energy end of the resulting UTA. Here, the opposite is true and the widths of the predicted  $5d-5f$  UTAs is in general slightly greater when CI effects are accounted for. In order to directly compare the results of CI on the spectral distribution rearrangement of  $n = 4 - n = 4$  UTA and  $n = 5 - n = 5$  UTA, calculations were performed for  $4p^64d^2 - 4p^54d^3 + 4p^64d4f^1$  transitions in Sr-like  $Ag^{9+}$ ,  $Sn^{12+}$ ,  $Ba^{18+}$ , and  $Nd^{22+}$  and  $5p^65d^2 - 5p^55d^3 + 5p^65d5f^1$  transitions in the homologous ions  $Au^{9+}$ ,  $Pb^{12+}$ ,  $Ra^{18+}$ , and  $U^{22+}$  of the Yb-isoelectronic sequence. The results are shown in Figure 5. From this figure it is clear that for  $n = 4 - n = 4$  transitions, CI completely reallocates the intensity of the  $4d-4f$  component transitions as well as the lower energy  $4p-4d$  lines to the higher energy end of the array and that with increasing ionization the resulting spectrum narrows until its FWHM becomes less than 0.5 nm. For  $n = 5 - n = 5$  transitions, in the absence of CI the  $5p-5d$  array splits with increasing  $Z$  due to spin orbit interaction into  $5p_{1/2}-5d$  and  $5p_{3/2}-5d$  sub-arrays. The  $5d-5f$  sub array overlays the longer wavelength  $5p_{3/2}-5d_{5/2}$  sub-array in  $Au^{9+}$  and  $Pb^{12+}$ , and lies between the  $5p_{1/2}-5d$  and  $5p_{3/2}-5d$  sub-arrays in  $Ra^{18+}$  and  $U^{22+}$ . The effect of CI is to narrow the spectral width of the  $5p_{1/2}-5d$  sub-array while leaving its mean position essentially unchanged, while mixing the  $5d-5f$  and  $5p_{3/2}-5d$  sub-arrays to produce a broader spectral profile that in some instances contains fewer strong individual lines, that is shifted to shorter wavelength by the interaction. Thus, the effect of CI is less dramatic for  $5-5$  transitions though it still leads to major redistribution of intensity both between and within the resulting two sub arrays.



**Figure 5.** (Color online) Gaussian convolved spectra of  $4p^6 4d^2 - 4p^5 4d^3 + 4p^6 4d^1 4f^1$  transitions in Sr-like  $\text{Ag}^{9+}$ ,  $\text{Sn}^{12+}$ ,  $\text{Ba}^{18+}$ , and  $\text{Nd}^{22+}$  and  $5p^6 5d^2 - 5p^5 5d^3 + 5p^6 5d^1 5f^1$  transitions in the homologous ions  $\text{Au}^{9+}$ ,  $\text{Pb}^{12+}$ ,  $\text{Ra}^{18+}$ , and  $\text{U}^{22+}$  of the Yb-isoelectronic sequence.

From the CI calculations, the normalized  $gA$  ( $gA/\Sigma gA$ ) distributions for  $5d-5f$  and  $5p-5d$  transitions were extracted for each ion stage, i.e., for  $0 \leq N \leq 8$  of each of the elements considered here and summed to give an overall profile for both sets of transitions. The results are shown in Figure 6. As in the rare earths, the  $d-f$  lines are expected to contribute to the emission spectra from hot plasmas of these elements whilst both sets of transitions may be observed in absorption. It is interesting to compare the positions of the strong UTAs observed in LPPs of Th and U [34,35] with the predictions of the present calculations. In the Th spectrum, recorded under essentially optically thin conditions, a UTA extending from approximately 9.5–11.5 nm and peaking near 10.3 nm was observed while in the U spectrum the same feature lay between approximately 9.0 and 10.5 nm and

peaked near 9.5 nm. From Table 2, the peak positions are predicted to lie near 9.8 and 9 nm respectively indicating a wavelength shift of approximately 0.5 nm between observed and calculated data for  $5p^6 5d^{N+1} - 5p^6 5d^N 5f^1$  transitions. No shorter wavelength UTA corresponding to  $5p^6 5d^{N+1} - 5p^5 5d^{N+2}$  was observed. However, the maximum ionization stages produced in these experiments were around 16 or 17 times ionized and some contribution from  $5d^{10} 5f^N - 5d^9 5f^{N+1}$  transitions in lower ion stages is also present. When first reported it was assumed that the increased widths of these  $5p^6 5d^{N+1} - 5p^6 5d^N 5f^1$  UTAs relative to their  $4p^6 4d^{N+1} - 4p^6 4d^N 4f^1$  counterparts in the spectra of the homologous species Ce and Nd was due to increased spin orbit interaction effects [34]. From this work it is clear that the  $5p$  spin orbit splitting essentially limits the interaction to the  $5p_{3/2} - 5d$  sub-array and this interaction results in a broadening of the  $5d - 5f$  array. In the more highly ionized spectra of U recorded from the TEXT Tokamak, two distinct UTAs were observed with peaks near 7 and 9 nm which are in excellent agreement with the results obtained in this work. However, the shorter wavelength observed peak also contains a contribution from  $5p^n - 5p^{n-1} 5d$  transitions, which may dominate over  $5p^6 5d^{N+1} - 5p^5 5d^{N+2}$  emission.



**Figure 6.** (Color online) Summed peak emission from (a)  $5d-5f$  and (b)  $5p-5d$  UTAs including CI in elements with  $Z = 79-92$ . (c) Dependence of UTA transition energies on atomic number  $Z$ ,  $5d-5f$  (red stars) and  $5p-5d$  (black diamonds).

#### 4. Conclusions

Unresolved transition arrays (UTAs) of the type  $\Delta n = 0$ ,  $4p^6 4d^{N+1} - 4p^5 4d^{N+2} + 4p^6 4d^N 4f^1$  have been extensively studied because their intensity and emission bandwidth makes them ideal candidates for applications as radiation sources for a variety of technological applications in the EUV and SXR region. In contrast, the corresponding  $\Delta n = 0$ ,  $5p^6 5d^{N+1} - 5p^5 5d^{N+2} + 5p^6 5d^N 5f^1$  UTAs have not been studied in detail. In this paper, the properties of these arrays have been studied theoretically with the aid of Hartree-Fock with configuration interaction (CI) calculations. We report on calculations for  $5p-5d$  and

$5d-5f$  transitions in elements from  $Z = 79$  to  $Z = 92$  and predict the positions and spectral properties of the corresponding UTAs. We compared the effects of CI between  $\Delta n = 0$ ,  $n = 5-n = 5$  transitions in these elements and  $n = 4-n = 4$  transitions in their homologous, lower  $Z$  counterparts and found that the strong spectral narrowing, which is a feature of  $\Delta n = 0$ ,  $n = 4-n = 4$  transitions is not expected to be important in these spectra but shifts the position of  $5d-5f$  arrays to slightly shorter wavelengths and results in a broadening of their spectral profiles. This broadening points to their potential usefulness in the development of broadband sources for future EUV and soft X-ray metrology applications.

**Acknowledgments:** Luning Liu acknowledges support from UCD and from a Chinese Scholarship Council (CSC) scholarship and from the Fundamental Research Funds for the Central Universities under grant No. HUST: 2016YXMS028. DK acknowledges funding from the Irish Research Council and the Marie Curie Actions ELEVATE fellowship.

**Author Contributions:** Luning Liu and Gerry O' Sullivan performed the calculations; Gerry O' Sullivan, Deirdre Kilbane, Pdraig Dunne, Luning Liu and Xinbing Wang analyzed the data; Gerry O'Sullivan, Deirdre Kilbane and Luning Liu wrote the paper.

**Conflicts of Interest:** The authors declare no conflict of interest. The founding sponsors had no role in the design of the study; in the collection, analyses, or interpretation of data; in the writing of the manuscript, and in the decision to publish the results.

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ISBN 978-3-03842-870-1