The Effect of Customized Insole Pads on Plantar Pressure Distribution in a Diabetic Foot with Neuropathy: Material and Design Study Using Finite Element Analysis Approach

Muhammad Nouman 1, Desmond Y. R. Chong 2, Satta Srewaradachpisal 3 and Surapong Chatpun 4,5,*

Abstract: To reduce the trial and error in a real clinical scenario, the finite element analysis (FEA) can be effectively used to simulate various effective pad designs and a material selection to reduce and redistribute peak plantar pressure in a diabetic foot with neuropathy. The aim of this study was to investigate the effect of pad design and material stiffness on the reduction in plantar pressure in a diabetic foot with neuropathy using FEA. Three-dimensional foot models with a customized insole (CMI) were created to study the peak contact pressure. Ethylene vinyl acetate, Nora® Lunelastike, and thermoplastic polyurethane were assigned to the top, middle, and base layers of the CMI, respectively. Two types of pads were proposed: a heel pad and a heel–forefoot pad. Four different materials with different stiffnesses were assigned as pad materials including a void pad. The FEA revealed that pads with soft materials reduced peak plantar pressure more effectively than stiffer pads. The use of a softer heel–forefoot pad reduced the peak plantar pressure at the midfoot and forefoot compared with other pads. The findings suggest that the material and design selection for the fabrication of CMIs with pads are important factors in reducing plantar pressure and may be useful in the management of a neuropathic diabetic foot.

Keywords: custom-made insole; finite element analysis; material stiffness; pad design; plantar pressure

1. Introduction

Approximately 20 million people with diabetes have diabetic foot ulceration and another 130 million are at risk to develop diabetic foot ulcers [1,2]. Diabetic foot ulceration and re-ulceration are leading causes of prolonged hospitalization and are associated with a socio-economic burden and a high rate of mortality [3]. Foot complications are commonly seen with increased plantar pressure, especially in a diabetic foot with neuropathy causing non-traumatic lower extremity amputation [4,5]. Foot complications resulting in amputation begin with elevated plantar pressure and shear stresses that are directly associated with ulceration [6]. The occurrence of diabetic foot ulcers resulting from abnormal peak plantar pressure are found under the metatarsal heads and hindfoot, with a recurrence rate of more than 80% within three years after recovery [7]. More than 80% of all lower limb amputations in diabetes are led by long-term ulcerations and re-ulcerations [8].

In-shoe plantar pressure is usually measured to evaluate the plantar pressure distribution and sites of high plantar pressure. However, the plantar pressure measurement is time-consuming with prolonged trial and error procedures [9]. Furthermore, the cost of
the measuring instruments and evaluation procedure is high. The finite element analysis (FEA) provides reliable results to evaluate various protocols without a patient’s direct involvement. It also helps to understand the foot biomechanics and the effects of various interventions [10]. Researchers so far have focused on the effect of insole stiffness and thickness on plantar pressure distribution [11,12]. Therapeutic footwear with insoles play an important role in the prevention of ulcers [13]. There are several design parameters that can be used to reduce peak plantar pressure in the feet of people with diabetic neuropathy. Shoe design can help to distribute weight more evenly across a foot and reduce the peak plantar pressure [14]. An insole that is designed to provide cushioning and support can help to reduce the forefoot and hindfoot peak plantar pressure [15]. In the case of material selection, different materials can also reduce peak plantar pressure. For example, foam materials may be more effective at absorbing shock than hard materials [16]. It is important to consider all these design parameters in combination when designing footwear or insoles for people with diabetic neuropathy. Insole shapes and material selections are strongly influenced by the experience of a pedorthist. Therefore, insole designs and materials are effective factors in reducing plantar pressure and in the alleviation of heel pain when compared with simulated flat insoles [17,18].

A reduction in peak plantar pressure, foot stability, arch support, foot comfort, and shock absorption are some of the key criteria to design and prescribe customized insoles (CMIs) for people with different needs [19–22]. Painful heels are addressed by providing a soft heel cup orthosis that provides comfort and a better reduction in the peak contact pressure under painful heels [23]. However, these soft heel cups are unable to provide stability for the foot. Additionally, adding dome-shaped metatarsal pads to an insole could reduce the forefoot peak contact pressure [24]. However, an addition of such a structure causes discomfort, and an inappropriate placement might result in adverse consequences with increased plantar contact pressure, especially in a diabetic foot with neuropathy [25]. The addition of a heel cup and metatarsal pads to a CMI to appropriately capture the heel morphology and the addition of a void in the base layer at the hindfoot and foot that can be filled with a softer material might be better to reduce and redistribute the pressure from the hindfoot and forefoot.

To estimate plantar pressure distribution, the FEA provides a better understanding of the interaction of a foot with a CMI. Furthermore, the FEA can be effectively used to simulate various effective designs and material combinations to study peak plantar pressure reduction and redistribution. However, limited studies have been focused on design parameters that provide a better reduction in peak plantar pressure at the forefoot and hindfoot in combination with the materials that are best suited to substantially lower peak plantar pressure in diabetic neuropathic feet [26,27]. Metatarsal pads are mostly applied to an insole to reduce and redistribute peak plantar pressure under the metatarsal heads. Moreover, these pads are in a dome-shape that might cause irritation or flatten out due to a poor selection of material, and prolonged use by the subject might be a secondary cause. The approach to reduce and redistribute the peak contact pressure by varying materials and designs in a diabetic foot is by placing padding at the base layer. The inclusion of padding at the base layer eliminates the difficulty of the proper placement of padding, and it strengthens the soft material surrounded and sandwiched by the stiffer material to prolong its durability. Therefore, the aim of this study was to computationally evaluate the effect of pad shape and material stiffness on plantar pressure distribution and the reduction in diabetic neuropathic foot using the FEA. Selecting an appropriate design and material for an insole pad will help to reduce and redistribute peak plantar pressure under pressure-sensitive foot regions.

2. Materials and Methods
2.1. Foot Model Reconstruction

The current study employed a validated FEA methodology developed by Nouman et al. [28,29]. A model of a foot with a CMI was developed to investigate various parameters
affecting the plantar pressure distribution in a diabetic neuropathic foot. The subject’s foot geometry was acquired after approval from the institutional human research ethics committees (EC-63-219-25-2). The foot model is based on the unloaded left foot Digital Imaging and Communications in Medicine (DICOM) data of a 57-year-old male subject with an 84 kg weight. The foot bones and soft tissue geometries were segmented manually from computed tomography scan images of the left foot to acquire a three-dimensional (3D) foot model using Mimics software version 20 (Materialise, Leuven, Belgium). To reduce the computational modeling cost, the bones were merged to form a single body surrounded by soft tissues [28,29].

2.2. Pad Designs and Materials

A three-layer CMI as a control CMI with the top layer as ethylene vinyl acetate (EVA), the middle layer as Nora® Lunalastike, and the base layer as thermoplastic polyurethane (TPU) was designed. A void was designed under the anatomical regions of high peak plantar pressure to reduce the peak plantar pressure under the heel and forefoot (Figure 1). Two types of insole pads, a heel pad and heel–forefoot pad with an overall 3 mm thickness, were embedded in the base layer. The length and width of the heel pad were 60.67 mm and 53.87 mm, respectively (Figure 1a). Moreover, the heel–forefoot pad was designed from heel to forefoot with a heel width of 56.90 mm and a forefoot width of 112.04 mm, with a total length of 190.16 mm (Figure 1b).

Figure 1. The pad designs. (a) Heel pad and (b) heel–forefoot pad added to the base layer.

The pad was embedded in the base layer of the CMI with varying material properties (Table 1). Ansys SpaceClaim (ANSYS Inc., Canonsburg, PA, USA) was used to create a 3D foot model with the CMI and with various pad designs for a diabetic foot with neuropathy.
The pad was embedded in the base layer of the CMI with varying material properties ... is reconstructed with fixed points and applied load, and (b) the 3D foot model is meshed with tetrahedral elements.

Without a pad (Figure 2a). Conversely, with the heel–forefoot void, the maximum frictional stress increased by 4.52% with the heel–forefoot pad fabricated from a firm material compared with the CMI only fabricated from Plastazote® PE. However, the frictional stress with the heel–forefoot pad was reduced by 6.01% as compared with the heel pad only fabricated from Plastazote® PE. However, the frictional stress shifted from the medial forefoot to the medial midfoot (Figure 3b). The maximum frictional stress increased when the stiffness of the pad was higher for the heel–forefoot pad.

<table>
<thead>
<tr>
<th>Components</th>
<th>Young’s Modulus (MPa)</th>
<th>Poisson’s Ratio $v$</th>
<th>References</th>
</tr>
</thead>
<tbody>
<tr>
<td>Bone</td>
<td>7300</td>
<td>0.3</td>
<td>[30]</td>
</tr>
<tr>
<td>Soft tissue</td>
<td>0.19</td>
<td>0.49</td>
<td>[31]</td>
</tr>
<tr>
<td>Plantar fascia</td>
<td>350</td>
<td>0.35</td>
<td>[32]</td>
</tr>
<tr>
<td>Plastazote® PE</td>
<td>0.45</td>
<td>0.38</td>
<td>[33]</td>
</tr>
<tr>
<td>Nora® Lunalastike</td>
<td>1.04</td>
<td>0.25</td>
<td>[33]</td>
</tr>
<tr>
<td>EVA</td>
<td>5</td>
<td>0.40</td>
<td>[34]</td>
</tr>
<tr>
<td>TPU</td>
<td>11</td>
<td>0.45</td>
<td>[35]</td>
</tr>
<tr>
<td>Firm insole</td>
<td>1000</td>
<td>0.40</td>
<td>[12]</td>
</tr>
<tr>
<td>Ground</td>
<td>21,000,000</td>
<td>0.3</td>
<td>[36]</td>
</tr>
</tbody>
</table>

Note: PE—polyethylene, EVA—ethylene vinyl acetate, TPU—thermoplastic polyurethane.

2.3. Boundary and Loading Conditions

Ansys SpaceClaim was used to build the finite element (FE) foot model with the CMI along with a ground (Figure 2). The fused foot bones as one lump encapsulated by the soft tissues were assigned to be bonded. The foot–insole interaction and the insole–ground interface had a frictional coefficient of 0.3 [24] and 0.6 [25], respectively. The ends of the tibia and fibula were assigned to be fixed. A load of 420 N was regarded as a ground reaction force representing half of the body weight during balanced standing. In addition, based on earlier research, an upward-directed force of about 50% of Achilles tendon force during balanced standing was prescribed in the FE model [28]. To mimic the plantar fascia, 5 tension-only link segments were employed, and origin and insertion locations were determined by their anatomical location in accordance with an anatomy atlas [29]. A mesh convergence study was conducted for five different element sizes, and a tetrahedral 5 mm element size was used as a computationally optimal mesh for further analysis [28,29].

Figure 2. (a) The 3D foot model is reconstructed with fixed points and applied load, and (b) the 3D foot model is meshed with tetrahedral elements.

3. Results

3.1. Frictional Stress

The peak frictional stress occurred under the first metatarsal head with the CMI without a heel pad and with a heel-to-forefoot pad and heel pad fabricated from various materials (Figure 3). The frictional stress with the heel–forefoot pad was reduced by 6.01% as compared with the heel pad only fabricated from Plastazote® PE. However, the frictional stress with the heel–forefoot pad with a firm material was increased by 4.08% as compared with the heel pad with a similar material. The maximum frictional stress increased by 4.52% with the heel–forefoot pad fabricated from a firm material compared with the CMI without a pad (Figure 2a). Conversely, with the heel–forefoot void, the maximum frictional stress shifted from the medial forefoot to the medial midfoot (Figure 3b). The maximum frictional stress increased when the stiffness of the pad was higher for the heel–forefoot pad.
However, this observation could not be found for the heel pad only. The heel–forefoot pad made with Plastazote® PE reduced the maximum frictional stress by 27.18% compared with the heel–forefoot void. A similar effect was found with the heel void, where the frictional stress at the medial forefoot was increased by 9.40% compared with the heel pad fabricated from Plastazote® PE.

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Figure 3. (a) The maximum frictional stress obtained for CMI with pad materials ranging from soft to hard compared with CMI without pad; (b) frictional stress distribution with the highest maximum frictional stress, especially with a heel void (H-void) and a heel–forefoot void (H-F-void) compared with CMI without pad.

#### 3.2. Plantar Pressure Distribution with Heel Pad

The softest heel pad (CMI-A) provided better planar pressure distribution, especially at the medial forefoot and hindfoot compared with the CMI with a stiffer heel pad and the CMI without pad (Figure 4). The results showed that the heel had the highest plantar contact pressure compared with the other foot regions, except for the model of the insole with a void heel (CMI-F). Furthermore, the area of high plantar contact pressure became larger when using a high-stiffness material for the heel pad. CMI-A had the softest heel pad, and the peak contact pressure was 9.02% lowered with CMI-A compared with the CMI without a heel pad (CMI-D). Moreover, there was a maximum reduction in the peak contact pressure by 12.41% with CMI-A compared with the firm material pad (CMI-E). On the contrary, the peak contact pressure increased by 7.06% with the heel void (CMI-F) and shifted from the hindfoot to the forefoot, followed by the midfoot, compared with CMI-A. In addition, the plantar pressure distribution at the midfoot was highest with CMI-F, followed by the first metatarsal head, compared with CMI-E, CMI-D, and CMI-A.
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Figure 4. The plantar pressure obtained from FEA models using heel (H) pad made from various materials from soft to hard (CMI-A to CMI-E), without heel pad (CMI-D), and with void (CMI-F).

3.3. Plantar Pressure Distribution with Heel–Forefoot Pad

The heel–forefoot pad fabricated from a softer material provided a better distribution of plantar pressure at the medial forefoot and hindfoot compared with stiffer materials and the insole without a pad (Figure 5). In contrast with stiffer materials, the soft material heel–forefoot pad reduced the peak contact pressure at the hindfoot. The maximum peak contact pressure was reduced by 20.84% with the softest heel pad (CMI-G) compared with the insole without a heel pad (CMI-J). Moreover, the reduction in the peak contact pressure was 23.24% with CMI-G compared with the firm heel–forefoot pad (CMI-K). On the other hand, the peak contact pressure using the heel–forefoot void (CMI-L) was increased by 34.80% and shifted from the hindfoot to the medial midfoot compared with CMI-G. The regions of high contact pressure under the 1st to 5th metatarsal heads were shifted to a distal part of the metatarsal heads with CMI-L.
The regions of high contact pressure under the 1st to 5th metatarsal heads were shifted to a distal part of the metatarsal heads with CMI-L.

Figure 5. The plantar pressure obtained from FEA models using the heel–forefoot pad fabricated from soft to hard material properties (CMI-G to CMI-K), without heel–forefoot pad (CMI-J), and with a void (CMI-L).

3.4. The Influence of Pad Design on Each Region of the Foot

The peak contact pressure was reduced using heel–forefoot and heel pads with softer materials at the hindfoot area (Table 2). The heel–forefoot pad made from Plastazote® PE (CMI-G) reduced the peak contact pressure by 6.98% compared with the heel pad only fabricated from the same material (CMI-A). However, the heel–forefoot void (CMI-L) had a negative effect with an increased medial forefoot peak contact pressure of 16.18% and 11.00% compared with the softer heel–forefoot pad (CMI-G) and the CMI without a pad, respectively. Moreover, the central forefoot peak contact pressure was reduced with the Plastazote® PE heel pad (CMI-A) compared with the heel–forefoot pad (CMI-G) and that with voids.

The medial and lateral peak contact pressures at the midfoot increased with the voids as compared with the heel and heel–forefoot pads and the insole without a pad. Moreover, the peak contact pressure was increased by 34.42% at the medial midfoot with the heel–forefoot void compared with the insole without a pad. A similar increased trend was found with the heel pad compared with the insole without a pad.
Table 2. Regional peak contact pressure of the foot with heel pad and heel–forefoot pad with varying materials.

<table>
<thead>
<tr>
<th>Foot Region</th>
<th>Peak Contact Pressure (kPa)</th>
</tr>
</thead>
<tbody>
<tr>
<td></td>
<td>Plastazote® PE</td>
</tr>
<tr>
<td>Whole foot</td>
<td>H</td>
</tr>
<tr>
<td>Forefoot</td>
<td>35.5</td>
</tr>
<tr>
<td>Medial forefoot</td>
<td>34.1</td>
</tr>
<tr>
<td>Central forefoot</td>
<td>34.1</td>
</tr>
<tr>
<td>Lateral forefoot</td>
<td>24.6</td>
</tr>
<tr>
<td>Medial midfoot</td>
<td>32.2</td>
</tr>
<tr>
<td>Lateral midfoot</td>
<td>34.0</td>
</tr>
<tr>
<td>Hindfoot</td>
<td>35.5</td>
</tr>
<tr>
<td>Medial hindfoot</td>
<td>34.2</td>
</tr>
<tr>
<td>Lateral hindfoot</td>
<td>35.5</td>
</tr>
</tbody>
</table>

Note: H—heel pad, H-F—heel–forefoot pad, and w/o—without.

4. Discussion

This study proposed to computationally evaluate the effect of pad shape and material stiffness on plantar pressure distribution and the reduction in diabetic foot with neuropathy using the FEA. The current study found a softer material used in the heel–forefoot pad tends to reduce the frictional stresses at the forefoot and hindfoot compared with the heel pad and the insole without a pad. The heel pad designed from a softer material distributed the plantar pressure from the hindfoot compared with stiffer materials and the heel–forefoot pad fabricated from soft to stiff materials. Likewise, the peak contact pressure at the medial and central forefoot was reduced by the soft heel–forefoot pad compared with the soft heel pad only and the insole without a pad. The principles of the reduction in peak contact pressure in a diabetic foot with neuropathy require the consideration of various designs and material selections with the inclusion of frictional stress.

A CMI is beneficial for a diabetic neuropathic foot for the reduction in peak plantar pressure, especially at the forefoot [37–40]. However, some patients require a further reduction in peak plantar pressure either at the forefoot or hindfoot to prevent ulceration and to reduce the occurrence of pain. Experimental and FEA studies have highlighted the heel as one of the most frequently encountered regions with pain in all populations, including athletes and diabetic patients with a high risk of foot ulceration [41,42]. Metatarsal pads and small plugs are used to reduce the peak plantar pressure under metatarsal heads [37,43]. Using a CMI causes comfort in the foot due to the reduction and uniform distribution of the plantar pressure [44]. A previous experiment indicated that the CMI material and its modifications significantly lowered peak contact pressure at the forefoot and hindfoot, including shifting contact pressure to the midfoot [45]. A similar trend was found in this current study with a reduced peak plantar pressure with the use of softer pads compared with the insole without a pad, firm pads, and voids.

Appropriate CMI material selection and pad design play a major impact on contact pressure reduction and redistribution under the hindfoot, and forefoot compared with a flat insole and no insole. The thickness and stiffness of the CMI material reduced the plantar pressure distribution in [46]. In our work, a softer material sandwiched between stiffer materials in addition to varying pad designs fabricated from a low Young’s modulus material could further reduce the peak contact pressure, especially at the heel. A similar trend of reduction was found with an appropriate selection of CMI material and thickness for people with prolonged standing at work [15,17,42]. By changing the designs of CMIs including pads, we can further reduce and redistribute the peak contact pressure in a diabetic neuropathic foot. Evidence suggests using a CMI with a metatarsal pad and a metatarsal bar can redistribute the plantar pressure. However, whether the metatarsal pad...
is positioned proximal or distal to the metatarsal heads influences the plantar pressure
distribution at the forefoot [25,47]. Our study also demonstrated that the heel–forefoot pad
made from a softer material reduced the medial forefoot peak contact pressure compared
with using a heel pad only. However, a heel pad made from softer material reduced the
central forefoot peak contact pressure as compared with the heel–forefoot pad and one
with voids. A similar plantar pressure reduction was found with low- and medium-density
CMIs fabricated from polyurethane and EVA [48].

The FEA technique allows an efficient analysis of the peak contact pressure that is
frequently shown in cases of foot complications. The FEA approach highlights some of the
important parameters that play an important role, especially in subjects prone to frequent
ulceration and re-ulceration. However, frictional stress measurement, which is useful to
be evaluated in clinical practice using in-shoe pressure sensors, is rarely reported and
remains difficult in actual clinical settings in diabetic foot with neuropathy. Researchers
attached sensors to the callus site to determine the forces that trigger callus formation, and
it was found that in-shoe shear stresses are a causative factor for foot disorders [49,50].
The unique aspect of our study was using the FEA to evaluate the frictional stress that
occurred with pads fabricated from various materials and those with voids in comparison
with insoles without any pads. In our current study, the maximum frictional stress was
much higher at the forefoot than at the hindfoot. This higher frictional stress at the forefoot
might help in the development of ulceration and re-ulceration [51,52]. The results of
this current study showed, similarly, a trend of maximum frictional stress under the first
metatarsal head with pads and without pads compared with at the hindfoot. However,
the maximum frictional stress shifted to the midfoot while using a heel–forefoot void. The
secondary component causing ulceration can be detected as differences in the peak contact
pressure and maximum frictional stress [53]. Recently, many researchers applied artificial
intelligence for the purpose of diabetic foot screening and a future advancement [54,55].
Further improvement can be achieved by combining the FEA approach with artificial
intelligence.

There were several limitations in this FEA study while investigating the CMI with two
types of pads in comparison with that without a pad. Firstly, the soft tissues and insole
material were simplified as linear elastic material properties to reduce the computational
load acquired by the FEA. Therefore, the material properties in the current models were
assigned as linear elastic, as our focus was to forecast the pattern of plantar pressure distri-
bution while changing the pad designs and materials for a diabetic foot with neuropathy.
Moreover, to identify the exact values it would be recommended to investigate more CMI
designs wherein hyperelastic material properties could be assigned to the soft tissues and
insoles during a gait cycle. Secondly, the current FEA study assumed a balanced standing
with a ground reaction force, representing half of the body weight. The application of force
following the center of pressure might represent a more realistic condition during gait.
Thirdly, the bones were fused together as one entity to represent the bones to reduce the
complexity of the foot model, as the region of interest was the plantar surface of the foot,
rather than the bones in the foot. Lastly, the results are based on a single model of foot.
Therefore, future studies are necessary to focus on types of foot and the effectiveness of
CMIs. For further FE foot model development, the load bearing condition during different
phases of the gait cycle requires muscle loading input. In addition, the motion within foot
joints during walking might give more insight into the diabetic foot with the use of CMIs
with different interventions.

5. Conclusions

It was demonstrated that the pad design and material selection had an impact on
the plantar pressure reduction and distribution, especially in the forefoot and hindfoot
regions. It was observed that the use of a heel–forefoot void further reduced the hindfoot
and forefoot maximum frictional stresses compared with a heel–forefoot pad with softer
materials. Using a softer material as a heel–forefoot pad and heel pad reduced the peak
plantar pressure compared with the stiffer material and the insole without a pad. Our results suggest that the employment of the FEA while designing and selecting materials to fabricate a CMI is able to minimize prolonged clinical trial and error to reduce abnormal peak contact pressure in a diabetic foot with neuropathy.


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**Informed Consent Statement:** Informed consent was obtained from a subject involved in the study.

**Data Availability Statement:** Not applicable.

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**Conflicts of Interest:** The authors declare no conflict of interest.

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