Advanced Electrochemical Degradation of Organic Pollutants from Water Using Sb-Doped SnO₂/Ti Anode and Assisted by Granular Activated Carbon

Anamaria Baciu 1, Corina Orha 2, Radu Nicolea 1, Mircea Nicolaescu 1,2, Sorina Ilies 3 and Florica Manea 1,*

1 Department of Applied Chemistry and Engineering of Inorganic Compounds and Environment, Politehnica University of Timisoara, Blv. Vasile Parvan No. 6, 300223 Timisoara, Romania; anamaria.baciu@upt.ro (A.B.); radu.nicolea2@student.upt.ro (R.N.); mircea.nicolaescu@student.upt.ro (M.N.)
2 Condensed Matter Department, National Institute for Research and Development in Electrochemistry and Condensed Matter, 1 P. Andronescu Street, 300254 Timisoara, Romania; orha.corina@gmail.com
3 “Coriolan Drăgulescu” Institute of Chemistry, Romanian Academy, 24 Mihai Viteazu Blvd., 300223 Timisoara, Romania; sorinailies@acad-icht.tm.edu.ro
* Correspondence: florica.manea@upt.ro

Abstract: In this paper, mesoporous electrodes consisting of Sb-doped SnO₂ deposited onto Ti plates that had undergone controlled corrosion under acidic medium were synthesized via a spin-coating method and morpho-structurally characterized via X-ray diffraction (XRD) and scanning electron microscopy (SEM). The electrodes were electrochemically tested to examine their degradation/mineralization through electrooxidation (EO) of doxorubicin (DOX) as a single component and multi-component, together with capecitabine (CCB) from the cytostatic class and humic acid (HA) from the natural organic matter (NOM) class in the absence/the presence of activated carbon (AC) as a particulate electrode. The best mineralization efficiency of 67% was achieved for DOX mineralization using Sb-doped SnO₂ deposited onto a Ti plate that had undergone controlled corrosion with oxalic acid during the electrooxidation process. The presence of AC within the electrolysis process generated a synergistic effect of 52.75% for total organic carbon (TOC) parameter removal, which is in accordance with and significantly better than the results reported in the literature. The aspects related to the complex mechanism of DOX degradation and mineralization are discussed. The superiority of AC assisted electrooxidation, as electrochemical filtering (EF), was proved, considering simultaneous degradation and mineralization of mixture of doxorubicin, capecitabine, capetabimic and humic acid.

Keywords: advanced water treatment; electrochemical filtering; doxorubicin; mesoporous Sb-doped SnO₂ electrode; activated carbon; particulate electrode

1. Introduction

The presence of pharmaceuticals in water is continuously growing and should exhibit possible negative effects on the ecology status of the surface water in both the short and long term. One of the main sources is industrial pharmaceuticals wastewaters. Cytostatic drugs are classified as hazardous waste due to their carcinogenic, teratogenic, and mutagenic properties, and they have a very negative impact on water quality and human health.

Considering their xenobiotic and refractory character, the researchers investigating their removal are focused on the application of advanced oxidation processes (AOPs), which are based on in situ production of hydroxyl radical (OH) for their mineralization [1–4]. Among the AOPs, electrochemical advanced oxidation processes (EAOPs) have been extensively studied for treating various types of pharmaceutical wastewaters, due to their high versatility, efficiency, and environmental compatibility [1].

Considering the key role of the electrode in the performance of electrochemical processes, various types of electrodes, such as graphite [5], platinum (Pt) [6], carbonaceous
matrix, boron-doped diamond (BDD) [7] and dimensionally stable anodes (DSA) [8,9], have been studied.

Dimensionally stable electrodes (DSA) consist of metal oxide films deposited on titanium or other substrates and have been used to replace the conventional electrodes in advanced wastewater treatment [8]. DSA electrodes have been widely investigated in the field of water electrolysis, electro chlorination, cathodic protection, and wastewater treatment [9] due to their advantages of stable size, long service life, high electrocatalytic activity, and low cost [10]. They have a large specific surface area and desired mechanical and chemical properties, e.g., good stability, low resistivity and excellent resistance to corrosion at high currents [11]. Typically, Ti foil is used as the substrate, and the primary chemical composition of the coating is transition metal oxide, e.g., RuO$_2$, IrO$_2$, TiO$_2$, SnO$_2$, PbO$_2$, MnO$_2$, and Ta$_2$O$_5$. DSA exhibit high electroactive surface areas due to their cracked mud-like morphology, allowing the direct oxidation of organic pollutants on the electrode surface at low potentials, and are able to promote the formation of active intermediates (Cl$_2$, ClO$^-$, OH, O$_3$) to perform the indirect oxidation of pollutants [12].

Antimony-doped tin dioxide deposited onto a Ti substrate (Ti/SnO$_2$-Sb) electrode is considered one of the most promising DSA type anode materials used for the electrooxidation process in wastewater treatment due to its advantages of relatively high oxygen evolution potential (OERP), high electrooxidation activity, low cost and low toxicity [13–16]. Several synthesis methods have been reported for its preparation, e.g., dip coating [17], electrolytic deposition [18], spin coating [19] and pyrolysis spray [20].

A traditional two-dimensional (2D) electrode reactor is commonly used for electrochemical processes, including advanced electrooxidation, but there are some disadvantages, e.g., the small electrode surface area, low current efficiency, limited mass transfer, temperature rise during processing and short lifetime of electrodes [21]. To solve these disadvantages, recently, the 3D electrochemical process has attracted much attention as a variant of a 2D electrochemical reactor because of its unique properties and advantages regarding the high current efficiency and the high space–time yield. It is well known that the 3D electrochemical process is similar to the 2D electrochemical process, except for the porous surface of the anode and/or the presence of the third electrode based on filtering/sorption material and named particulate electrode [22]. Properties including high specific area for good adsorption capacity, high electrocatalytic activity, and stability for the coating substrate or good conductivity that can increase the current efficiency are required for good particulate electrode materials. Granular activated carbon (AC) has been tested as a composition of the particulate electrode to enhance the efficacy of the electrochemical system in various wastewater treatments [23–25]. The pollutant degradation is improved due to the AC particles under voltage application becoming the micro-electrolysis cells, which are able to generate hydrogen peroxide and, subsequently, the hydroxyl radicals [23,26–29]. Additionally, AC exhibits the sorption ability for many types of pollutants, enhancing the mass transfer, and as consequence, the pollutant degradation efficiency is higher [30].

Considering our previously reported results achieved for the degradation and mineralization of doxorubicin (DOX), a common cytostatic used for cancer therapy, which can be found in water, using a Ti-based SnO$_2$ anode in electrooxidation process characterized by low electrochemical mineralization efficiency of 0.147 mg C/C cm$^2$ [31], this work aims to enhance the electrochemical performance for DOX degradation and mineralization. Two approaches are considered: one is to improve the anode properties through its composition and morphology and the other is to introduce granular activated carbon in suspension as particulate electrode. The synthesis via spin-coating method of the mesoporous Sb-doped SnO$_2$ films onto controlled corroded Ti plates, their characterization and electrochemical testing are studied in relation to the degradation/mineralization of DOX as a single component and as a multi-component in the presence of capecitabine (CCB) from the cytostatic class and humic acid (HA) from the natural organic matter (NOM) class in both 2D and AC particulate electrode-based 3D electrochemical processes.
2. Materials and Methods

2.1. DSA Electrode Synthesis

A three-stage procedure consisting of the titanium substrate pretreatment via controlled corrosion, sol–gel preparation from precursors and sol–gel spin coating subsequent calcination process was used to obtain Ti/SnO$_2$-Sb electrodes (Figure 1).

Figure 1. Schematic diagram of preparation of Ti/SnO$_2$-Sb electrodes.

Two corrosion processes based on oxalic or fluorhidric acids were applied to Ti substrates (2.5 × 2.5 cm) that were previously polished and degreased. The etching process in oxalic acid (10%) was described in detail in our previous work [31]. The etching of the Ti plate in fluorhydric acid consisted of a Ti plate maintained in 0.5 M HF for 2 h, followed by the process of thermal oxidation carried out in a tubular furnace in a controlled atmosphere of a mixed gas flow of Ar and O$_2$ at a temperature of 500 °C for 4 h.

Ti/SnO$_2$-Sb electrodes were prepared via a spin-coating method using corroded Ti plate and uncorroded Ti plate. Thus, Sb doped SnO$_2$ was deposited onto Ti plate corroded with HF (Ti/SnSb-S1) and, respectively, with oxalic acid (Ti/SnSb-S2). For comparison, Sb-doped SnO$_2$ was deposited onto an uncorroded Ti plate (Ti/SnSb-S0).

The preparation process consisted of mixing 5 mL SnCl$_4$, 250 µL SbCl$_3$ in 10 mL distilled water. Additionally, 1.5 g Pluronic P-123 was added to 15 mL ethanol, which was mixed with aqueous solution for 4 h to obtain sol–gel. This transparent gel was left standing to age at least 24 h at 60 °C before coating. Ti/SnO$_2$-Sb electrodes were achieved via the spin-coating method (WS-400-6NPPB Spin Coater-Laurell Technology Corporation, Lansdale, PA, USA) through the deposition of 6 layers of SnO$_2$-Sb thin films on Ti plates, according to the protocol described in our previous work [31].
2.2. Physicochemical Characterization

The crystalline structure of the Ti/SnO$_2$-Sb electrodes was characterized by X-ray diffraction (XRD, PANalytical X’Pert PRO MPD Diffractometer, Almelo, The Netherlands) with Cu-Kα radiation ($\lambda = 1.5418$ Å) in the range $2\theta = 10–80^\circ$. The morphology of the layers was examined using scanning electron microscopy (SEM, FEI Inspect S model, Eindhoven, The Netherlands).

2.3. Electrochemical Characterization and Degradation

The electrochemical characterizations and testing of the Ti/SnO$_2$-Sb electrodes were performed via cyclic voltammetry (CV) and chronoamperometry (CA) using the classical three-electrode cell system and GPES 4.9 software controlled Autolab potentiostat/galvanostat PGSTAT 302 (Eco Chemie, Utrecht, The Netherlands). The three-electrode cell system consisted of saturated calomel reference electrode (SCE), a platinum plate counter electrode, and a Ti/SnO$_2$-Sb working electrode, considering all types of above-presented antimony-doped tin oxides coated onto un-corroded/corroded Ti substrates (Ti/SnSb-S0-S2 electrodes). The electrochemical testing of all three electrodes was carried out in 0.1 M Na$_2$SO$_4$ and a mixture of 0.05 M Na$_2$SO$_4$ + 0.05 M NaCl supporting electrolytes for the degradation and mineralization of doxorubicin (DOX), a cytostatic considered as an emerging pollutant in water. Additionally, for optimal conditions, the degradation and mineralization of mixture of doxorubicin (DOX), capecitabine (CCB) as another commonly used cytostatic and humic acid (HA) as a main component of natural organic matter (NOM) was assessed.

DOX, CCB and HA concentrations were determined based on UV-VIS spectra recorded with Agilent Cary 100 UV/VIS spectrophotometer (Santa Clara, CA, USA) at specific wavelengths. Spectrophotometrically, DOX concentrations were assessed at wavelengths of 486 nm, 290 nm, 253 nm and 232 nm, while the CCB concentration was determined at the wavelengths of 302 nm, 240 nm and 213 nm and HA concentration at 254 nm (Figure S1).

The organics degradation degree ($\eta$) and electrochemical degradation degree (E$_{org}$) were determined based on Equations (1) and (2):

$$\eta_{org} = \left(\frac{C_{org,i} - C_{org,f}}{C_{org,i}}\right) \cdot 100\% \quad (1)$$

$$E_{org} = \left(\frac{C_{org,i} - C_{org,f}}{C}\right) \cdot S \cdot V_s \left(\frac{mg}{C \cdot cm^2}\right) \quad (2)$$

where: $C_{org,i} - C_{org,f}$ represents the change in the organics (DOX, CCB and HA) concentration, determined via spectrophotometry at each absorbance during electrochemical experiments; C is the charge consumption corresponding to various electrolysis times, $V_s$ is the sample volume (20 cm$^3$) and S is the area of the anode surface (3 cm$^2$).

Additionally, the organics mineralization degree ($\eta_{TOC}$) and electrochemical mineralization degree (E$_{TOC}$) were determined considering the change in TOC concentration instead of organics concentration, based on Equations (3) and (4):

$$\eta_{TOC} = \left(\frac{TOC_i - TOC_f}{TOC_i}\right) \cdot 100\% \quad (3)$$

$$E_{TOC} = \left(\frac{TOC_i - TOC_f}{C \cdot S}\right) \cdot V_s \left(\frac{mg TOC}{C \cdot cm^2}\right) \quad (4)$$

The total organic carbon (TOC) parameter was analyzed using Shimadzu TOC analyzer (Columbia, MD, USA).
For a more accurate assessment of the mineralization process efficacy taking into account the energy consumption, the mineralization current efficiency (MCE) is determined in accordance with Equation (5) [32]:

\[
MCE = \frac{n \cdot F \cdot V_s \cdot (\text{TOC}_i - \text{TOC}_f)}{4.32 \times 10^7 \cdot 10^4 \cdot m \cdot 100\%}
\]  

(5)

where \( n \) is the number of electrons consumed in the mineralization process of DOX, \( F \) is the Faraday constant (=96,487 C \cdot \text{mol}^{-1}), \( V_s \) is the solution volume (dm³), \( \Delta \text{TOC}_{\text{exp}} \) is the experimental TOC decay (mg \cdot dm⁻³), \( 4.32 \times 10^7 \) is a conversion factor for units homogenization (=3600 s h⁻¹ \cdot 12,000 mg of carbon mol⁻¹), \( m \) is the number of carbon atoms in organic, \( I \) is the applied current (A) and \( t \) is time (h). The number of electrons consumed is determined based on the overall mineralization reaction of organics to CO₂.

The mineralization reactions of organics are considered based on Equations (6) for DOX, (7) for HA and (8) for CCB:

DOX : \( \text{C}_{27}\text{H}_{29}\text{NO}_{11} + 46\text{H}_2\text{O} \rightarrow 27\text{CO}_2 + 121\text{H}^+ + \text{NO}_3^- + 120\text{e}^- \)  

(6)

HA : \( \text{C}_9\text{H}_9\text{NO}_6 + 15\text{H}_2\text{O} \rightarrow 9\text{CO}_2 + \text{NO}_3^- + 39\text{H}^+ + 38\text{e}^- \)  

(7)

CCB : \( \text{C}_{15}\text{H}_{22}\text{FN}_3\text{O}_6 + 33\text{H}_2\text{O} \rightarrow 15\text{CO}_2 + 88\text{H}^+ + \text{F}^- + 3\text{NO}_3^- + 84\text{e}^- \)  

(8)

The energy consumption was assessed per gram of TOC removed (SEC) and per litre of the water treated (Wsp) using Equations (9) and (10), respectively:

\[
\text{SEC} = \frac{U \cdot I \cdot t \cdot \text{TOC}_i}{V_s \cdot (\text{TOC}_i - \text{TOC}_f)} \left( \text{Wh} \cdot \text{g}^{-1} \cdot \text{TOC} \right)
\]

(9)

\[
\text{Wsp} = \frac{U \cdot I \cdot t}{V_s} \left( \text{Wh} \cdot \text{dm}^{-3} \right)
\]

(10)

where: \( U \) is the cell voltage (V), \( I \) indicates the applied current (A), \( t \) is the electrochemical oxidation time (h), \( V_s \) is the volume of the cell (dm³) and \( \text{TOC}_i \) and \( \text{TOC}_f \) are the initial and final TOC concentration (mg C \cdot dm⁻³) at time \( t \), respectively.

3. Results and Discussion

In the first stage, all electrodes of Sb-doped SnO₂ deposited onto uncorroded/corroded Ti plates were characterized morpho-structurally by XRD and SEM.

3.1. Morphostructural Characterization

The crystal structures of the electrodes were studied using X-ray diffraction (XRD). Figure 2 shows that the diffraction peaks of the electrodes were observed at \( 2\theta = 26.6^\circ, 33.9^\circ \) and \( 51.8^\circ \), which were assigned to the (110), (101) and (211) planes of SnO₂. It is noticed that no peaks corresponding to antimony oxides were detected, mostly because of trace amount of antimony added in sol–gel or because the element Sb might have entered into the lattice of SnO₂ crystal through substitution [33]. The presence of a few small Ti peaks at \( 2\theta = 38.41^\circ, 40.19^\circ, 53.11^\circ \) and \( 70.62^\circ \), which were assigned to the (002), (101), (102) and (103) planes, indicates the existence of some cracks on the electrodes surface.
After the corroded Ti plate was coated with Sb-SnO$_2$ sol–gel precursor, the electrodes would seriously affect the electrochemical activity and stability[35–37]. Through these cracks could mitigate the binding force between the film coating and the substrate, which would seriously affect the electrochemical activity and stability[35–37].

In the electrochemical processes, the penetration of electrolyte into the substrate calcinations process and the solvent evaporation[34]. It is well known that during their application in the electrochemical processes, the penetration of electrolyte into the substrate through these cracks could mitigate the binding force between the film coating and the substrate, which would seriously affect the electrochemical activity and stability[35–37].

When the gel was deposited onto a non-corroded Ti plate, the compact morphology containing “mud-like cracks” which corresponds to a classical 2D smooth surface was observed. The phenomenon of “cracked-mud” production was assumed to be related to the expansion properties between the Sn-Sb active layer and titanium substrate during calcinations process and the solvent evaporation[34]. It is well known that during their application in the electrochemical processes, the penetration of electrolyte into the substrate through these cracks could mitigate the binding force between the film coating and the substrate, which would seriously affect the electrochemical activity and stability[35–37].

After the corroded Ti plate was coated with Sb-SnO$_2$ sol–gel precursor, the electrodes showed a more compact surface, proving that Ti corrosion in an acidic medium allowed mesoporous surface characteristics to be obtained on the 3D electrode surface.
3.2. Electrochemical Characterization

Oxygen evolution reaction potential (OERP) and capacitive component as the background current give information about oxygen evolution activity and the electroactive surface area of the electrode. It is well known that oxygen evolution reaction is a major side reaction during advanced electrooxidation, at the potential corresponding to the hydroxyl radicals generation in accordance with Equations (11) and (12):

\[
2H_2O \rightarrow O_2 + 4H^+ + 4e^- \tag{11}
\]

\[
H_2O \rightarrow OH + H^+ + e^- \tag{12}
\]

In addition, within the anodic process, ozone, chlorine and persulphate are generated, in addition to hydroxyl radicals based on the aqueous supporting electrolyte composition, in accordance with Equations (13)–(16). These can act as a supplementary oxidizing agent during electrolysis.

\[
3H_2O \rightarrow O_3 + 6H^+ + 6e^- \tag{13}
\]

\[
2Cl^- \rightarrow Cl_2 + 2e^- \tag{14}
\]

\[
Cl_2 + H_2O \rightarrow HClO + Cl^- + H^+ \tag{15}
\]

\[
2SO_4^{2-} \rightarrow S_2O_8^{2-} + 2e^- \tag{16}
\]

On the other hand, a higher rate of oxygen evolution mitigates the current efficiency and increases the energy consumption. Additionally, the background current is directly proportional to the electroactive surface area, which is enhanced by the surface porosity increasing. The larger the electroactive surface area, the better the electrochemical activity of the electrode surface.

Cyclic voltammograms (CVs) were recorded in 0.1 M Na$_2$SO$_4$ solution and a mixture of 0.05 M Na$_2$SO$_4$ and 0.05 M NaCl solution to evaluate the oxygen evolution activity for all synthesized Ti/SnO$_2$-Sb electrodes in comparison with Ti plate (Figure 4). Additionally, the comparative electrochemical behavior of doxorubicin (DOX) on all electrodes was studied via CV (Figure 5).

![Figure 4.](image-url) Comparative cyclic voltammograms recorded in 0.1 M Na$_2$SO$_4$ (solid line) and mixture of 0.05 M Na$_2$SO$_4$ with 0.05 M NaCl (dot line) supporting electrolyte at the electrodes: Ti plate (curves 1, 1'); Ti/SnSb-S0 (curves 2, 2'); Ti/SnSb-S1 (curves 3, 3'); Ti/SnSb-S2 (curves 4, 4').
The presence of Cl\textsuperscript{2−} ion in the solution has a polarization effect for all Ti/SnO\textsubscript{2}-Sb electrodes in contrast with the Ti plate, for which a depolarization effect with a significant increase in the current corresponding to chlorine generation is noticed (Figure 4). The presence of DOX exhibited a depolarization effect with increasing current density due to the DOX direct oxidation process occurring (Figure 5).

In addition to OERP, the oxygen evolution activity can be evaluated based on the current density value that represents the oxygen evolution reaction rate, which is directly proportional to the amount of electric charge [38]. As shown in Figure 4, the Ti plate exhibited the lowest OERP that is characteristic of the “active” electrodes [39] but with very low current density in both the capacitive component and the Faradaic response for the oxygen evolution as reaction rate. Ti/SnSb-S2 electrode exhibited the highest current density and, as a consequence, a higher reaction rate, and an OERP value lower than the other Ti/SnSb electrodes but higher than the Ti plate. This type of electrode is included in the “non-active” category of the electrode, but all dimensionally stable anode types electrode can have mixed behavior during the electrooxidation process, in accordance with Equations (17)–(20) [40]:

\begin{align}
 MO_{\text{II}} + H_2O &\rightarrow MO_{\text{II}}(HO\cdot) + H^+ + e^- \quad (17) \\
 MO_{\text{II}}(HO\cdot) &\rightarrow MO_{\text{II}+} + H^+ + e^- \quad (18) \\
 MO_{\text{II}+} + R &\rightarrow MO_{\text{II}} + RO \quad (19) \\
 MO_{\text{II}}(HO) + R &\rightarrow MO_{\text{II}} + CO_2 + H_2O + H^+ + e^- \quad (20)
\end{align}

where R represents the organic pollutants.
\[
\text{MO}_x + \text{H}_2\text{O} \rightarrow \text{MO}_x(\text{HO}^-) + \text{H}^+ + e^- \quad (17)
\]
\[
\text{MO}_x(\text{HO}^-) \rightarrow \text{MO}_{x+1} + \text{H}^+ + e^- \quad (18)
\]
\[
\text{MO}_{x+1} + R \rightarrow \text{MO}_x + \text{RO} \quad (19)
\]
\[
\text{MO}_x(\text{HO}) + R \rightarrow \text{MO}_x + \text{CO}_2 + \text{H}_2\text{O} + \text{H}^+ + e^- \quad (20)
\]

where \( R \) represents the organic pollutants.

3.3. Electrochemical Oxidation of DOX

Electrooxidation was carried out at constant potential through chronoamperometry (CA) running for one hour using all synthesized Ti/SnO_{2-Sb} electrodes. Chronoamperograms were recorded in both 0.1 M Na_2SO_4 solution and a mixture of 0.05 M Na_2SO_4 and 0.05 M NaCl solution supporting electrolyte at the potential value of +3.0 V/SCE for the electrooxidation of 5 mg·L^{-1} DOX (Figure 6a). The highest current densities were recorded for the Ti/SnSb-S2 electrode in both supporting electrolytes and the chloride ions, with a slight decrease in the current densities, which is in accordance with the CVs results.

![Chronoamperograms recorded in 0.1 M Na_2SO_4 solution and a mixture of 0.05 M Na_2SO_4 and 0.05 M NaCl solution supporting electrolyte at the potential value of +3.0 V/SCE for the electrooxidation of 5 mg·L^{-1} DOX.](image)

**Figure 6.** (a) Time evolution of chronoamperograms recorded at the potential value of +3.00 V vs. SCE for electrooxidation of 5 mg·L^{-1} DOX in 0.1 M Na_2SO_4 (solid lines) and mixture of 0.05 M Na_2SO_4 with 0.05 M NaCl (dotted lines) supporting electrolyte recorded with Ti/SnSb-S0 (curves 1, 1'); Ti/SnSb-S1 (curves 2, 2'); Ti/SnSb-S2 (curves 3, 3'); (b) Time evolution of chronoamperograms recorded in 0.1 M Na_2SO_4 supporting electrolyte and 5 mg·L^{-1} DOX with Ti/SnSb-S2 electrode at the different potential values: +2.00 V vs. SCE (curve 1), +3.00 V vs. SCE (curve 2) and +4.00 V vs. SCE (curve 3).

Additionally, the chronoamperometry was running at the potential value of +2.00, +3.00 and +4.00 V/SCE to determine the effect of the potential value on the DOX degradation and mineralization efficiency (Figure 6b). As was expected, the current densities increased at a higher potential value. Better degradation and mineralization degrees were reached for the potential value of +3.00 V/SCE, which was considered the optimal one (the results are not shown here).

The DOX degradation and mineralization degrees reached at the potential value of +3.00 V/SCE are gathered in Table 1, which also presents the OERP and the current densities for all tested electrodes. Ti/SnSb-S2 obtained after controlled corrosion with oxalic acid exhibited the lowest OERP and the highest current density as the reaction rate.
<table>
<thead>
<tr>
<th>Electrode</th>
<th>Supporting Electrolyte</th>
<th>$E_{O2}$/V vs. SCE</th>
<th>Current Densities, mA cm$^{-2}$</th>
<th>Mineralization Degree ($\eta_{TOC}$), %</th>
<th>$\lambda = 486$ nm</th>
<th>DOX Degradation Degree ($\eta_{DOX}$), %</th>
<th>$\lambda = 290$ nm</th>
<th>$\lambda = 253$ nm</th>
<th>$\lambda = 232$ nm</th>
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</thead>
<tbody>
<tr>
<td>Ti/SnSb-S0</td>
<td>0.1 M Na$_2$SO$_4$</td>
<td>1.75</td>
<td>2.2</td>
<td>5</td>
<td>70</td>
<td>23</td>
<td>12</td>
<td>9.5</td>
<td></td>
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<tr>
<td></td>
<td>0.05 M Na$_2$SO$_4$ + 0.05 M NaCl</td>
<td>1.72</td>
<td>1.4</td>
<td>4</td>
<td>80</td>
<td>- *</td>
<td>9.4</td>
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<tr>
<td>Ti/SnSb-S1</td>
<td>0.1 M Na$_2$SO$_4$</td>
<td>1.80</td>
<td>2.9</td>
<td>16</td>
<td>90</td>
<td>44</td>
<td>64</td>
<td>67</td>
<td></td>
</tr>
<tr>
<td></td>
<td>0.05 M Na$_2$SO$_4$ + 0.05 M NaCl</td>
<td>1.77</td>
<td>3.1</td>
<td>28</td>
<td>93</td>
<td>- *</td>
<td>74</td>
<td>47</td>
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<tr>
<td>Ti/SnSb-S2</td>
<td>0.1 M Na$_2$SO$_4$</td>
<td>1.65</td>
<td>7.7</td>
<td>42</td>
<td>99</td>
<td>88</td>
<td>95</td>
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<tr>
<td></td>
<td>0.05 M Na$_2$SO$_4$ + 0.05 M NaCl</td>
<td>1.58</td>
<td>6.1</td>
<td>67</td>
<td>98</td>
<td>- *</td>
<td>98</td>
<td>87</td>
<td></td>
</tr>
</tbody>
</table>

* Could not be read due to chlorine discharge (see Figure 7c).
where: \( j_{\text{lim}} \) is the limiting current density for organics mineralization (mA cm\(^{-2}\)), \( z \) is the number of electrons involved in organics mineralization reaction, \( F \) is the Faraday constant (96,487 C mol\(^{-1}\)), \( k_d \) is the mass transfer coefficient (m s\(^{-1}\)) and \( C_R \) is the concentration of organics in the bulk solution (mol m\(^{-3}\))

\[
\frac{\text{TOC}_i}{\text{TOC}_f} = \exp \left( - \frac{S}{V_s} \cdot k_d \cdot t \right)
\]

where: \( \text{TOC}_i \) and \( \text{TOC}_f \) is the initial concentration of total organic carbon of compounds and at time \( t \), respectively, \( S \) is the anodic active surface area (in m\(^2\)), \( V_s \) is the volume of the treated solution (in dm\(^3\)), and \( t \) is the electrolysis time (seconds).

Additionally, the best degradation and mineralization degrees were achieved using the Ti/SnSb-S2 electrode, which allowed a complete decolorization (\( \lambda = 232 \) nm), the aromatic ring and the quinonoid structure (\( \lambda = 253; 290 \) nm) [31]. This is also supported by Figure 7a, which displays the comparative UV-VIS spectrum recorded after one hour of electrolysis using all three electrodes. Additionally, the Ti/SnSb-S2 electrode accomplishes a 42% mineralization degree, while the Ti/SnSb-S0 electrode was not able to mineralize DOX under tested conditions. The presence of chloride enhanced the overall performance of the electrode, but the UV-VIS spectrum shape was modified through increasing absorbance at a wavelength of about 290 nm due to the increased concentration of hypochlorite during electrolysis (Figure 7b).

Additionally, from the kinetics point of view, a comparative evaluation of the effect of both supporting electrolytes (0.1 M Na\(_2\)SO\(_4\) and a mixture of 0.05 M Na\(_2\)SO\(_4\) and 0.05 M NaCl) on the mineralization current efficiencies determined based on Equation (5) was followed and the results are gathered in Table 2. Additionally, the limiting current density (\( j_{\text{lim}} \)) and the mass transfer coefficient for mineralization (\( k_d \)) were determined based on Equations (21) and, respectively, (22) [41]:

\[
j_{\text{lim}} = z \cdot F \cdot k_d \cdot C_R
\]
Table 2. Kinetics parameters and energy consumption-based efficacy for electrochemical oxidation of 5 mg L\(^{-1}\) DOX at Ti/SnSb-S2 electrode in 0.1 M Na\(_2\)SO\(_4\) and mixture of 0.05 M Na\(_2\)SO\(_4\) and 0.05 M NaCl.

<table>
<thead>
<tr>
<th>Supporting Electrolyte</th>
<th>Time, (sec)</th>
<th>(k_d), (m \cdot s(^{-1})) (10^6)</th>
<th>(j_{lim}), mA cm(^{-2})</th>
<th>MCE, %</th>
<th>(E_{TOC}), mg TOC/cm(^2)</th>
<th>(W_{sp}), kWh dm(^{-3})</th>
<th>SEC, kWh g(^{-1}) TOC Removed</th>
</tr>
</thead>
<tbody>
<tr>
<td>0.05 M Na(_2)SO(_4) + 0.05 M NaCl</td>
<td>600</td>
<td>34.2</td>
<td>0.364</td>
<td>6.9</td>
<td>0.960</td>
<td>0.525</td>
<td>0.434</td>
</tr>
<tr>
<td></td>
<td>1200</td>
<td></td>
<td></td>
<td>5.1</td>
<td>0.840</td>
<td>1.10</td>
<td>0.582</td>
</tr>
<tr>
<td></td>
<td>1800</td>
<td></td>
<td></td>
<td>3.4</td>
<td>0.501</td>
<td>1.80</td>
<td>0.887</td>
</tr>
<tr>
<td></td>
<td>3600</td>
<td></td>
<td></td>
<td>1.5</td>
<td>0.231</td>
<td>4.35</td>
<td>1.98</td>
</tr>
<tr>
<td>0.1 M Na(_2)SO(_4)</td>
<td>600</td>
<td>10.5</td>
<td>0.112</td>
<td>1.7</td>
<td>0.179</td>
<td>0.35</td>
<td>1.25</td>
</tr>
<tr>
<td></td>
<td>1200</td>
<td></td>
<td></td>
<td>1.9</td>
<td>0.178</td>
<td>0.62</td>
<td>1.56</td>
</tr>
<tr>
<td></td>
<td>1800</td>
<td></td>
<td></td>
<td>1.3</td>
<td>0.123</td>
<td>1.12</td>
<td>2.25</td>
</tr>
<tr>
<td></td>
<td>3600</td>
<td></td>
<td></td>
<td>1.3</td>
<td>0.116</td>
<td>2.61</td>
<td>2.37</td>
</tr>
</tbody>
</table>

Considering the current densities corresponding to the applied potential value of +3.00 V/SCE (Table 1), it is obvious that the electrooxidation process occurred under the mass transfer control for all tested operation conditions of water discharge generating O\(_2\) evolution involving hydroxyl radicals and other oxidants linked to the supporting electrolyte composition (e.g., chlorine, in accordance with Equations (14) and (15)).

In comparison with our previously reported paper related to Ti/SnO\(_2\) that allowed electrochemical DOX conversion without mineralization at the potential of +3.00 V/ESC [31], Ti/SnSb-S2 exhibited a significant enhanced performance for DOX degradation and mineralization. Additionally, higher mineralization current efficiency was achieved in the presence of chloride due to its supplementary action as an oxidant of chlorine and other chlorine-based species. The electrochemical efficiency related to the DOX mineralization determined based on Equation (4) showed better results in the presence of a mixture of 0.05 M Na\(_2\)SO\(_4\) and 0.05 M NaCl. The energy consumption reported per liter of the water treated is better in the absence of chloride, probably due to a part of the energy being consumed to generate chlorine, from which a main part is wasted.

3.4. Activated Carbon-Based Sorption-Assisted Electrochemical Oxidation of DOX Using Ti/SnSb-S2

Considering the principles of the electrochemical filtration, 1 g L\(^{-1}\) activated carbon, which is well known as mature technology in water treatment technology, was added with the role of the particulate electrode in the electrochemical system using 0.1 M Na\(_2\)SO\(_4\) supporting electrolyte and Ti/SnSb-S2 electrode. The results are presented in Table 3.

Table 3. Kinetics parameters and energy consumption-based efficacy for electrochemical oxidation of 5 mg L\(^{-1}\) DOX using EF process in 0.1 M Na\(_2\)SO\(_4\) supporting electrolyte.

<table>
<thead>
<tr>
<th>Supporting Electrolyte</th>
<th>Time, (sec)</th>
<th>(k_d), (m \cdot s(^{-1})) (10^6)</th>
<th>(j_{lim}), mA cm(^{-2})</th>
<th>MCE, %</th>
<th>(E_{TOC}), mg TOC/cm(^2)</th>
<th>(W_{sp}), Wh dm(^{-3})</th>
<th>SEC, Wh g(^{-1}) TOC Removed</th>
</tr>
</thead>
<tbody>
<tr>
<td>0.1 M Na(_2)SO(_4)</td>
<td>600</td>
<td>19.1</td>
<td>0.203</td>
<td>7.1</td>
<td>0.980</td>
<td>0.515</td>
<td>0.420</td>
</tr>
<tr>
<td></td>
<td>1200</td>
<td></td>
<td></td>
<td>5.5</td>
<td>0.870</td>
<td>1.05</td>
<td>0.610</td>
</tr>
<tr>
<td></td>
<td>1800</td>
<td></td>
<td></td>
<td>6.5</td>
<td>0.518</td>
<td>1.32</td>
<td>0.840</td>
</tr>
<tr>
<td></td>
<td>3600</td>
<td></td>
<td></td>
<td>5.6</td>
<td>0.590</td>
<td>3.25</td>
<td>1.16</td>
</tr>
</tbody>
</table>

It is obvious that the AC improved the process performance through mass transfer enhancement and the sorption of DOX in the electrochemical system. Additionally, under the electric field application, AC particles can be converted into charged microelectrodes exhibiting the electro-sorption of DOX and the ability to degrade and mineralize adsorbed DOX [26–29].

Thus, the mechanism for DOX removal of pollutants in activated carbon-based sorption-assisted electrooxidation of DOX is very complex. The presence of activated carbon particulate electrode should influence the DOX degradation/mineralization mechanism through a potential sorbent role. The electrochemical reactions on the non-active anode should be similar to electrochemical oxidation [42]. The question that arises is related
to the global effect of both processes regarding DOX degradation and mineralization. To elucidate these aspects, each process was applied individually for DOX removal through sorption on AC (S), degradation and mineralization through both electrooxidation (EO) and activated carbon-based sorption-assisted electrooxidation (EF). The presence of activated carbon increased the diffusion constant related to mineralization, which is expected due to its presence in the solution bulk. Additionally, the limiting current density increased in the presence of the activated carbon. A great enhancement is noticed for the mineralization current efficiency (MCE). Moreover, the synergic effect of the hybrid process of activated carbon—assisted electrooxidation (EF) is proved based on the kinetics constants expressed as \( \ln(C_0/C_t) = k(t) \), considering the pseudo-first-order model that fit well (correlation coefficient > 0.9) for each individual and each hybrid process (Table 4) using Equation (23):

\[
\text{Synergy (\%)} = \frac{k_{EF} - k_{EO} - k_S}{k_{EF}} \cdot 100
\]

where \( k_{EF}, k_{EO} \), and \( k_S \) are the kinetic coefficient of pollutant removal in EF, the electrochemical degradation system without AC and the sorption AC system.

Table 4. Kinetics coefficients are determined for each process using pseudo-first order model.

<table>
<thead>
<tr>
<th>Process</th>
<th>Parameter</th>
<th>( \lambda_{DOX} = ) nm</th>
<th>( k, \text{ min}^{-1} )</th>
<th>( R^2 )</th>
<th>( k_{E,F}^{C}, \text{ C}^{-1} )</th>
<th>( R^2 )</th>
</tr>
</thead>
<tbody>
<tr>
<td>S</td>
<td>( \lambda_{DOX} = 486 \text{ nm} )</td>
<td>0.004</td>
<td>0.937</td>
<td>-</td>
<td>-</td>
<td></td>
</tr>
<tr>
<td></td>
<td>( \lambda_{DOX} = 290 \text{ nm} )</td>
<td>0.0011</td>
<td>0.911</td>
<td>-</td>
<td>-</td>
<td></td>
</tr>
<tr>
<td></td>
<td>( \lambda_{DOX} = 253 \text{ nm} )</td>
<td>0.0018</td>
<td>0.969</td>
<td>-</td>
<td>-</td>
<td></td>
</tr>
<tr>
<td></td>
<td>( \lambda_{DOX} = 232 \text{ nm} )</td>
<td>0.0015</td>
<td>0.966</td>
<td>-</td>
<td>-</td>
<td></td>
</tr>
<tr>
<td></td>
<td>TOC, mg L^{-1}</td>
<td>0.0011</td>
<td>0.95</td>
<td>-</td>
<td>-</td>
<td></td>
</tr>
<tr>
<td>EO</td>
<td>( \lambda_{DOX} = 486 \text{ nm} )</td>
<td>0.07</td>
<td>0.998</td>
<td>4.724</td>
<td>0.99</td>
<td></td>
</tr>
<tr>
<td></td>
<td>( \lambda_{DOX} = 290 \text{ nm} )</td>
<td>0.02</td>
<td>0.999</td>
<td>1.524</td>
<td>0.999</td>
<td></td>
</tr>
<tr>
<td></td>
<td>( \lambda_{DOX} = 253 \text{ nm} )</td>
<td>0.034</td>
<td>0.999</td>
<td>2.535</td>
<td>0.999</td>
<td></td>
</tr>
<tr>
<td></td>
<td>( \lambda_{DOX} = 232 \text{ nm} )</td>
<td>0.032</td>
<td>0.999</td>
<td>2.545</td>
<td>0.999</td>
<td></td>
</tr>
<tr>
<td></td>
<td>TOC, mg L^{-1}</td>
<td>0.0084</td>
<td>0.96</td>
<td>0.555</td>
<td>0.999</td>
<td></td>
</tr>
<tr>
<td>EF</td>
<td>( \lambda_{DOX} = 486 \text{ nm} )</td>
<td>0.04</td>
<td>0.976</td>
<td>3.01</td>
<td>0.993</td>
<td></td>
</tr>
<tr>
<td></td>
<td>( \lambda_{DOX} = 290 \text{ nm} )</td>
<td>0.02</td>
<td>0.952</td>
<td>0.55</td>
<td>0.944</td>
<td></td>
</tr>
<tr>
<td></td>
<td>( \lambda_{DOX} = 253 \text{ nm} )</td>
<td>0.021</td>
<td>0.967</td>
<td>1.461</td>
<td>0.998</td>
<td></td>
</tr>
<tr>
<td></td>
<td>( \lambda_{DOX} = 232 \text{ nm} )</td>
<td>0.023</td>
<td>0.966</td>
<td>1.624</td>
<td>0.991</td>
<td></td>
</tr>
<tr>
<td></td>
<td>TOC, mg L^{-1}</td>
<td>0.02</td>
<td>0.900</td>
<td>2.721</td>
<td>0.986</td>
<td></td>
</tr>
</tbody>
</table>

The synergy in the EF process of 52.75% was calculated for TOC parameter removal. This is in accordance with the literature [43–45] reported for various configurations of GAC sorption-assisted electrooxidation using different DSA-type anodes and higher than the one reported for graywater treatment by Garcia et al., 2018 [46]. The presence of activated carbon under the electric field between anode and cathode within undivided cell ensure the creation of a double electric layer that is able to adsorb organic pollutant via an electro sorption mechanism [47]. Additionally, AC particles are polarized as anode and as a cathode depending on their position, generating a large number of micro-electrolysis cells, which should generate oxidant species (e.g., hydroxyl radicals) able to oxidize and mineralize the organic pollutant adsorbed onto its surface [30,48].

For the EO and EF processes, the apparent rate was determined using relation \( \ln(C_0/C_t) = k_E(C) \), in which C represents the electrical charge passed during EO and EF processes applied for DOX degradation and mineralization [49]. The results gathered in Table 4 show the superiority of EF in comparison with EO (2.72 vs. 0.555 C^{-1}), regarding the mineralization process.

The effective mineralization rate assessed as the ratio between the apparent mineralization rate constant calculated for the TOC analysis and the apparent degradation rate constant calculated based on UV analysis (\( k_{E,TOC}^{C}/k_{E,UV}^{C} \)) [49] showed the superiority of EF (\( k_{E,TOC}^{C}/k_{E,UV}^{C} = 0.90 \)) in comparison with EO (\( k_{E,TOC}^{C}/k_{E,UV}^{C} = 0.12 \)).
The synergic effect of the combination of electrooxidation and sorption processes operating at high voltage may be attributed to both indirect and direct electrochemical oxidation of DOX improving the transfer stage through DOX sorption onto AC and its further oxidation via the direct transfer of electrons and via hydroxyl radicals generated at the Ti/SnSb-S2 electrode surface and AC microanodes.

Considering the results related to the rate constants for DOX degradation and mineralization by EO using Ti/SnSb-S2 electrode, the tendency is similar to that reported by our group for DOX degradation using 3-D Ti/SnO$_2$ [31]. However, better mineralization current efficiency was achieved using the Ti/SnSb-S2 electrode due to its better electrochemical activity for radicals generation. The degradation and mineralization process imply the electron transfer at the solution–electrode surface interface that assured the DOX decolorization as direct electrolysis followed by the attack of the hydroxyl radicals and/or other oxidants (e.g., Cl$_2$) generated and adsorbed on the electrode surface through their diffusion into the bulk solution in according with the Equations (24) and (25):

$$\text{H}_2\text{O} + \text{Ti/SnSb} - \text{S}_2 \rightarrow \text{Ti/SnSb} - \text{S}_2(\cdot\text{OH}) + \text{H}^+ + \text{e}^- \quad (24)$$

$$\text{Ti/SnSb} - \text{S}_2(\cdot\text{OH}) + \text{C}_{27}\text{H}_{29}\text{NO}_{11} + 46\text{H}_2\text{O} \rightarrow \text{Ti/SnSb} - \text{S}_2 + 27\text{CO}_2 + 121\text{H}^+ + \text{NO}_3^- + 120\text{e}^- \quad (25)$$

The presence of AC in the EF process further complicates the mechanism considering the reduction in the O$_2$ as H$_2$O$_2$ that generates the hydroxyl radicals acting in the mineralization process of DOX adsorbed onto AC surface in according with Equations (26) and (27):

$$\text{O}_2 + 2\text{H}^+ + 2\text{e}^- \rightarrow \text{AC}(\text{H}_2\text{O}_2) \rightarrow \text{AC}(\cdot\text{OH}) \quad (26)$$

$$\text{AC}(\cdot\text{OH}) + \text{C}_{27}\text{H}_{29}\text{NO}_{11} + 46\text{H}_2\text{O} \rightarrow \text{AC} + 27\text{CO}_2 + 121\text{H}^+ + \text{NO}_3^- + 120\text{e}^- \quad (27)$$

This mechanism is proved by the above-discussed kinetics aspects presented in Table 4, especially considering the low rate constants for DOX removal when AC acted as simple sorbent material in comparison with the AC under voltage field application, which improved DOX mineralization kinetics but not degradation ones. This behavior explains the synergic effect of the combination of EO with the S process into the EF one for the mineralization process.

3.5. Comparative Simultaneous Mineralization of DOX, Capecitabine (CCB) and Humic Acid (HA) by EO and EF

Considering the common presence of humic acid (HA) as a main component of natural organic matter in surface water and the potential presence of other cytostatic such as capecitabine (CCB), Ti/SnSb-S2-based EO was tested for each individual pollutant (5 mg·L$^{-1}$ DOX, 5 mg·L$^{-1}$ CCB and 10 mg·L$^{-1}$ HA) and for their mixture (5 mg·L$^{-1}$ DOX + 5 mg·L$^{-1}$ CCB + 10 mg·L$^{-1}$ HA) mineralization. The activated carbon-based sorption-assisted electrochemical oxidation using Ti/SnSb-S2 (EF) process was tested for the same mixture composition. The UV-VIS spectra recorded for initial solutions and after treatment by EO are shown in Supplementary Materials, Figure S2.

The degradation of each pollutant occurred through EO. Additionally, the degradation of the mixture is proved by UV-VIS spectra using both EO and EF. Mineralization degrees, electrochemical efficiencies and mineralization current efficiencies for each pollutant and for their mixture are presented in Figure 8.
degrees, electrochemical efficiencies and mineralization current efficiencies for each pollutant and for their mixture are presented in Figure 8.

Figure 8. The comparative mineralization degrees and electrochemical mineralization efficiency of Ti/SnSb-S2 electrode after one hour of chronoamperometry running at +3.00 V/SCE in 0.1 M Na$_2$SO$_4$ supporting electrolyte for different individual pollutants (DOX, CCB, HA) and their mixture in the absence and the presence of 1 g·L$^{-1}$ AC. Inset: Mineralization current efficiency determined for similar operating conditions.

There is obviously enhanced efficiency for EF in comparison with EO. Additionally, better efficacy in terms of the energy consumed per g of TOC is provided by EF in comparison with EO. SEC of 0.653 kWh·g$^{-1}$ TOC was determined for EF in comparison with 1.128 kWh·g$^{-1}$ TOC for EO. These results clarify the superiority of EF for enhanced removal of the mixture of the pollutants.

4. Conclusions

The controlled corrosion of the Ti plate under acidic medium using hydrofluoric acid and oxalic acid allowed us to obtain mesoporous Sb-doped SnO$_2$ deposited onto Ti via a spin-coating method. A more uniform deposition of Sb-doped SnO$_2$ which mitigated the “mud-like cracks” was achieved through controlled corrosion of the Ti substrate in comparison with the uncorroded Ti plate.

Sb-doped SnO$_2$ deposited onto the Ti plate corroded with oxalic acid, named the Ti/SnSb-S2 electrode, exhibited the lowest potential value and the highest rate of oxygen evolution reaction. The best mineralization efficiency was achieved for doxorubicin (DOX) mineralization using the Ti/SnSb-S2 electrode at the potential value of +3.00 V/SCE. The presence of Cl$^-$ in the supporting electrolyte enhanced the mineralization efficiency in the presence of Cl$^-$, 67% vs. 42% in the absence of Cl$^-$. The energy consumption reported per liter of the water treated is mitigated in the absence of chloride, probably due to a part of
the energy being consumed to generate chlorine, from which a main part is wasted, while the reduced energy consumption reported for the removed TOC was achieved in chloride containing solution.

The presence of activated carbon within the electrolysis process increased the mass transport, enhancing the global mineralization process. Additionally, the mineralization current efficiency was improved substantially, and the effective mineralization was proved considering the apparent mineralization rate constant reported to the apparent degradation mineralization constant. Moreover, a synergic effect was proved considering the kinetics aspects of all electrooxidation, sorption and activated carbon-assisted electrooxidation named electrochemical filtering processes. A synergy of 52.75% was determined for TOC removal, which is in accordance with the result reported by [46–48].

The mechanism of DOX degradation and mineralization is very complex, involving both direct and indirect electrolysis-generating hydroxyl radicals and other oxidants (e.g., Cl2 in the presence of Cl−) at mesoporous Sb-doped SnO2 deposited onto Ti plate that had undergone controlled corrosion with oxalic acid. In addition, activated carbon micro-electrolysis cells configured under applied voltage enhanced the hydroxyl radicals concentration, with the consequence of improved general process performance.

The superiority of EF was proved considering simultaneous degradation and mineralization of a mixture of doxorubicin, capecitabine and humic acid, which shows the great potential of the hybrid process to be used in advanced treatment of water either solely or integrated in the finishing step of the water treatment technology.

Supplementary Materials: The following supporting information can be downloaded at: https://www.mdpi.com/article/10.3390/coatings13061127/s1, Figure S1: UV-VIS spectra in 0.1 M Na2SO4 supporting electrolyte and in the presence of different initial pollutants: 5 mg·L−1 DOX (curve 1), 5 mg·L−1 CCB (curve 2), and 10 mg·L−1 HA (curve 3), Figure S2: UV-VIS spectra in 0.1 M Na2SO4 supporting electrolyte, in the presence of an initial mixture of 5 mg·L−1 DOX, 5 mg·L−1 CCB and 10 mg·L−1 HA (curve 1) and after treatment by EO (curve 2), and after treatment by EF (curve 3) at an applied potential of +3.00 V vs. SCE.

Author Contributions: F.M.; methodology, F.M and C.O.; investigation, A.B., R.N., C.O., M.N. and S.I.; writing—original draft preparation, F.M., C.O. and A.B.; writing—review and editing, F.M. and A.B.; supervision, F.M. All authors have read and agreed to the published version of the manuscript.

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References
1. Sirés, I.; Brillas, E. Remediation of water pollution caused by pharmaceutical residues based on electrochemical separation and degradation technologies: A review. Environ. Int. 2012, 40, 212–229. [CrossRef]


25. Lei, S.; Song, Y. Comparative study on electrochemical treatment of cyanide wastewater. *Front. Chem.* 2021, 9, 598228. [CrossRef]


27. McQuillan, R.V.; Stevens, G.W.; Mumford, K.A. The electrochemical regeneration of granular activated carbons: A review. *J. Hazard Mater.* 2018, 355, 34–49. [CrossRef]


31. Orha, C.; Bandas, C.; Lazau, C.; Popesco, M.I.; Baciuc, A.; Manea, F. Advanced electrodegradation of doxorubicin in water using a 3-D Ti/SnO$_2$ anode. *Water* 2022, 14, 821. [CrossRef]


47. Ratiu, C.; Manea, F.; Lazau, C.; Grozescu, I.; Radovan, C.; Schoonman, J. Electrochemical oxidation of p-aminophenol from water with boron-doped diamond anodes and assisted photocatalytically by TiO₂-supported zeolite. *Desalination* 2010, 260, 51–56. [CrossRef]