Machinability of MoS$_2$ after Oxygen Plasma Treatment under Mechanical Scanning Probe Lithography

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Abstract: The surface of molybdenum disulfide (MoS$_2$) underwent oxygen plasma treatment to enhance its machinability and mitigate the tearing effects commonly associated with mechanical forces on 2D materials. This treatment led to the oxidation of the atoms on the top 1–3 layers of MoS$_2$, resulting in the formation of MoO$_3$ on the surface. During mechanical scanning probe lithography (m-SPL), only the surface oxide layer was uniformly removed, with material accumulation occurring predominantly on one side of the machined area. The resolution of the machining process was significantly enhanced via dynamic lithography while maintaining atomic-level smoothness in the machined area. Importantly, these techniques only removed the surface oxide layer, preserving the integrity of the underlying MoS$_2$ surface, which was pivotal in avoiding damage to the original material structure. This study provided valuable insights and practical guidance for the nanofabrication of transition metal dichalcogenides (TMDCs) nanodevices, demonstrating a method to finely tune the machining of these materials.

Keywords: atomic force microscopy; machinability; TMDCs; scanning probe lithography; oxygen plasma

1. Introduction

In recent years, 2D transition metal dichalcogenides (TMDCs) have gained significant attention for their use in nanoelectronics, optoelectronics, biosensing and other applications, due to their excellent optical, electrical, and mechanical properties [1–4]. However, a challenge in device fabrication involving these 2D materials is the difficulty in removing photoresists or electron beam lithography resists. These residues impaired the performance of the fabricated devices [5–7]. To address this, post-lithography methods like thermal annealing, solvent rinsing or plasma cleaning were employed to remove resist residues, enhance surface passivation, and improve metal–semiconductor contacts [8–10]. It remains challenging to develop techniques that effectively prevent the accumulation of surface residues on 2D material surfaces.

Within this context, scanning probe nanolithography (SPL) has emerged as a potent and resist-free lithographic technique, providing precise nanoscale accuracy and direct patterning capabilities on TMDCs [11–15]. Notably, mechanical scanning probe lithography (m-SPL), the fundamental method of SPL, involved directly applying force to remove material from a surface. A few defects were formed on molybdenum disulfide (MoS$_2$) surfaces under nano-scratching, especially around the edges of the nanogrooves [16]. Consequently, two distinctive types of cracks were observed on the MoS$_2$ surfaces [17]: semi-circular cracks at the fracture front and periodical zigzag cracks in the middle.
anisotropic nature of these cracks during their formation and propagation contributed to a reduction in the quality of the nanofabrication process, posing challenges for the integrity and performance of the resultant nanodevices. On the basis of ensuring nanofabrication resolution, it is particularly important to further enhance the machinability of mechanical scanning probe lithography.

The objective of this letter is to explore the machinability of MoS$_2$ after oxygen plasma treatment when subjected to mechanical scanning probe lithography. After the application of an oxygen plasma treatment, a uniform oxide layer is formed on MoS$_2$ flake. We will employ atomic force microscopy (AFM) for nano-scratching and dynamic lithography on these oxide-coated flakes. Our aim is to elucidate the characteristics of material removal, thereby contributing valuable insights to nanofabrication techniques for TMDC surfaces. This understanding is crucial for developing nanomachining processes tailored to these materials for the advancement of nanoscale devices.

2. Materials and Methods

2.1. Oxygen Plasma Treatment

In this study, few-layer flakes of MoS$_2$ (SPI supplies, West Chester, PA, USA) were produced, which were mechanically exfoliated using adhesive tape and subsequently transferred onto SiO$_2$/Si substrates, as depicted in Figure 1a. For this transfer, commercially available viscoelastic polydimethylsiloxane (PDMS) films (Gelfilm, Gel-Pak, Hayward, CA, USA) were employed. After the preparation of few-layer MoS$_2$ flakes, the flakes were treated by oxygen plasma under a low-pressure plasma system (Tetra, Diener electronic GmbH, Ebhausen, Germany), with an applied power of 200 W for a duration of 1 min, as shown in Figure 1b.

![Figure 1](image-url)  
**Figure 1.** (a) Mechanical exfoliation of MoS$_2$ flakes from bulk crystal. (b) MoS$_2$ flakes treated by oxygen plasma. (c) Mechanical scanning probe lithography on MoS$_2$ flakes after oxygen plasma treatment, including nano-scratching and dynamic lithography.

2.2. Mechanical Scanning Probe Lithography

The scanning probe lithography experiments were conducted using a commercial AFM system (Dimension Icon, Bruker Corporation, Billerica, MA, USA). The equipped Nanoman module in the AFM system is utilized for the scratching process in this study. Figure 1c illustrates the schematic of the lithography processes. To carry out the nanomachining on MoS$_2$ flakes, a silicon tip (MPP-11120, Bruker Corporation, Billerica, MA, USA) with a nominal spring constant of 40 N/m was utilized. During the nano-scratching process in contact mode, the cantilever deformation was regulated by the voltage of the laser on the photodetector ($V_{\text{setpoint}}$), influencing the applied normal load. In tapping mode, the driven amplitude $V_r$ (reading voltage) was obtained by actuating the cantilever at its resonant frequency. For dynamic lithography, the cantilever of the AFM tip was driven to $V_w$ (writing voltage). The driven amplitude ratio $V_w/V_r$ was maintained in the range of 5–25 under dynamic lithography. The direction of m-SPL was perpendicular to the long axis of the cantilever. Post-nanogroove fabrication, a new silicon tip was used to assess the morphology of the generated nanogroove under tapping mode. The scan rate was set at
1 Hz with each scan line comprising 256 pixels. The resulting AFM images were processed using Nanoscope Analysis 1.90 software (Version) provided by Bruker Company.

3. Results and Discussion
3.1. MoS₂ Nanosheets under Oxygen Plasma Treatment

The optical microscope was initially used to locate the position of the flakes, followed by precise positioning using the AFM tip. After the preparation of few-layer MoS₂ flakes through mechanical exfoliation, one flake surface was analyzed, as illustrated in Figure 2a. Subsequently, the surface was treated with oxygen plasma, resulting in the oxidized surface depicted in Figure 2b. An essential step in this process was measuring identical flakes along the same cross-sections. By comparing AFM images before and after oxygen plasma treatment, as shown in Figure 2a,b, it is indicated that the surface height of MoS₂ flakers increased in the range from 4 to 5 nm, according to cross-sections of the pristine flakes of the surface with plasma treatment in Figure 2d, which confirms that the oxidation layer formed was MoO₃ [18,19]. To measure the thickness of the oxidation layer, the produced oxidation was soluble in water, as indicated in Figure 2c. The resulting flake was about 1–2 nm thinner than the pristine flake, based on the heights of the flake after immersion in water for 30 s, as shown in Figure 2d. The same processes were performed on 19 flakes, and it was found that after being treated in oxygen plasma, 1 to 3 layers of MoS₂ were oxidized based on statistics data in Figure 2e, corresponding to the Raman spectroscopy analysis [20]. The oxygen plasma treatment process produced reactive particles, which resulted in thinning the surface through physical bombardment. Note that the oxygen plasma treatment process produced an oxidation phenomenon in this study. The surface, after the oxygen plasma treatment, was relatively flat, which is suitable for mechanical scanning probe lithography.

![AFM images of a MoS₂ flake: (a) pristine flake obtained from mechanical exfoliation, (b) after oxygen plasma treatment, and (c) after immersion in water for 30 s. (d) Cross-sections of the flakes in (a–c) marked in white. (e) Removal layers of MoS₂ flakes treated with oxygen plasma and DI water.](image)

3.2. Comparison between Nano-Scratching and Dynamic Lithography

Following the oxygen plasma treatment on the MoS₂ surface, nano-scratching was conducted in AFM contact mode with the voltage bias from 1 to 3 V. As shown in Figure 3a, it was found that the nanogrooves were processed under the mechanical load, and the
removed surface materials were accumulated around the nanogrooves. The fabrication results indicated that the process led to plastic deformation without causing any cracks. The width and depth of the nanogrooves were measured to be about 55 nm and 0.88 ± 0.17 nm, respectively. And the machined depth remained consistent even as the mechanical load increased. This process effectively removed the oxide layer, exposing the original MoS$_2$ flake. An additional shallower groove surrounding the main grooves may have resulted from a defect in the AFM tip. To further enhance the resolution of m-SPL, a dynamic lithography technique was employed. As depicted in Figure 3b, the nanogrooves were produced when the driven amplitude ratio varied from 5 to 25. The cyclic extrusion of the tip not only removed the oxide layer but also led to the formation of material pileups. The machined depth was around 1.30 ± 0.47 nm, and it remained stable across different driven amplitude settings. The month width was roughly 23 nm, showcasing the capability of dynamic lithography in achieving high-resolution nanofabrication on TMDCs surfaces. Therefore, the application of the oxidation treatment enhanced the machinability of the MoS$_2$ surface, effectively preventing the formation of uncontrolled cracks [17] due to mechanical stress. And the tearing of the 2D surface [21] was prevented during dynamic lithography. The treated surface also exhibited isotropic properties, as discussed in [20], enhancing the overall quality and consistency of the nanofabrication process. In the future, it is worth further investigating methods to eliminate material pileups.

![AFM images and corresponding cross-sections](image)

**Figure 3.** AFM images and the corresponding cross-sections of nanogrooves marked in white on a MoS$_2$ flake with oxygen plasma treatment under (a) nano-scratching and (b) dynamic lithography.

### 3.3. Characterization on Nanofabrication Quality of Dynamic Lithography

Dynamic lithography was utilized for high-resolution nanomachining. The nanofabrication quality should be further assessed. Figure 4 displays the surface morphologies and the corresponding cross-sections of the machined areas via dynamic lithography at the driven amplitude ratio of 10, 15 and 20. The results showed uniform material removal from the surface, with minimal material debris remaining at the edges. Most of the removed material accumulated at the end of the tip trace. The machined depth varied from 0.96 to 2.21 nm, corresponding to approximately 1 to 3 layers of MoS$_2$ thickness. Additionally, Figure 4 includes phase images of the machined areas, which could be employed to explore
the influence on the mechanical properties of 2D materials at the nanoscale through contact stiffness measurements [22]. To verify that the observed phase contrast was not due to topographic changes, the phase measurements were taken in both forward and backward scanning directions. The consistency in these measurements across both directions confirmed the material contrast, indicating successful removal of the surface oxidation layer and exposure of the pristine MoS$_2$ surface. The surface roughness of both the machined area and the original surface was quantified, as shown in Table 1. It was observed that the surface roughness of the machined area was marginally higher than that of the original surface. Nevertheless, the resulting surface was atomically flat, demonstrating that the dynamic lithography technique yielded high-quality surface nanomachining.

Table 1. Roughness of unmachined surface and machined surface after dynamic lithography with varied driven amplitude ratio.

<table>
<thead>
<tr>
<th>$V_w/V_r$</th>
<th>Unmachined Surface $R_a$ (nm)</th>
<th>Machined Surface $R_a$ (nm)</th>
</tr>
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<tbody>
<tr>
<td>10</td>
<td>0.13</td>
<td>0.17</td>
</tr>
<tr>
<td>15</td>
<td>0.20</td>
<td>0.31</td>
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<tr>
<td>20</td>
<td>0.19</td>
<td>0.21</td>
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4. Conclusions

This study has investigated the material removal capabilities of MoS$_2$ after oxygen plasma treatment under mechanical scanning probe lithography. Oxygen plasma treatment enhanced the MoS$_2$ surface’s machinability. Under this condition, the surface material could be precisely removed using techniques like nano-scratching and dynamic lithography. Notably, dynamic lithography demonstrated superior machining resolution and maintained surface integrity more effectively. The surface oxide layer was selectively removed by nanomachining, exposing the untouched MoS$_2$ surface without causing any damage.
This resulted in a machined surface with atomic-level smoothness for the fabrication of subsequent nanodevices.

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**References**


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