

# Critical Shear Rate of Polymer-Enhanced Hydraulic Fluids

Pawan Panwar,<sup>†</sup> Paul Michael,<sup>‡</sup> Mark Devlin,<sup>¶</sup> and Ashlie Martini<sup>\*,†</sup>

<sup>†</sup>*Department of Mechanical Engineering, University of California Merced, Merced, California, USA*

<sup>‡</sup>*Fluid Power Institute, Milwaukee School of Engineering*

<sup>¶</sup>*Afton Chemical, Richmond, VA*

E-mail: [amartini@ucmerced.edu](mailto:amartini@ucmerced.edu)

## Supporting Information

### Instruments

A Cannon StressTech HR Oscillatory Rheometer was used to measure dynamic viscosity at low shear rates and the PCS Ultra Shear viscometer was used to measure the dynamic viscosity at high shear conditions. Schematics of these devices are shown in Fig. S1.

### Force Field Parameters

The TraPPE-UA forcefield was used to describe the chemistry of molecules. In the TraPPE-UA force field, the nonbonded interactions are described by pairwise-additive Lennard-Jones 12-6 potentials, electrostatic interactions by the Ewald summation, bonded atoms are considered to have fixed bond lengths, bond angles are governed by harmonic potential, and the motion of the dihedral

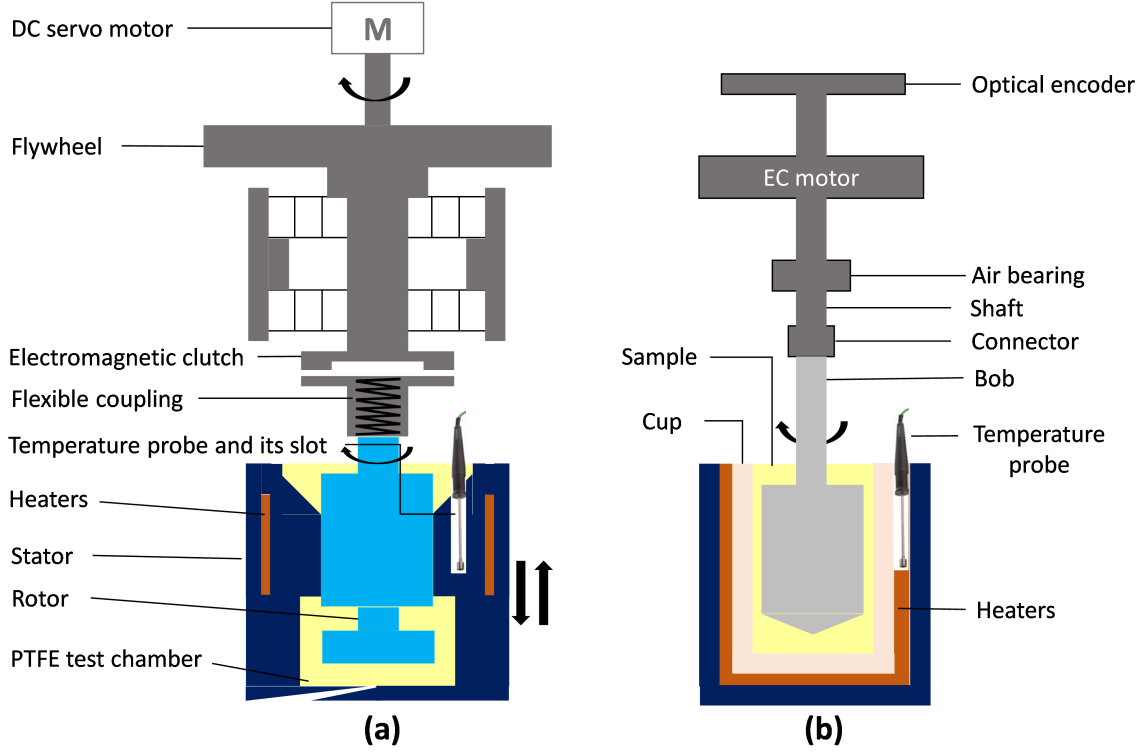


Figure S1: Schematics of (a) PCS Ultra Shear Viscometer and (b) Cannon StressTech HR Oscillatory Rheometer used for measuring high and low shear viscosity, respectively.

angle is governed by Fourier potential. The original TraPPE uses fixed bond lengths, but to model fully flexible bonds, a harmonic potential was implemented by taking the corresponding force constants from the CHARMM<sup>1,2</sup> force field, as suggested by Siepmann.<sup>3</sup> This fully flexible model can be described by Equation S1.

$$\begin{aligned}
 U_{total} &= U_{bond}(r) + U_{bend}(\theta) + U_{torsion}(\phi) + U_{NB}(r_{ij}) \\
 &= \sum_{bond} \frac{k_l}{2} (r - r_0)^2 + \sum_{bend} \frac{k_\theta}{2} (\theta - \theta_{eqm})^2 + \sum_{torsion i=1}^m c_i [1 + \cos(n_i \phi - d_i)] \\
 &\quad + \sum_{i < j} 4\epsilon_{ij} \left[ \left( \frac{\sigma_{ij}}{r_{ij}} \right)^{12} - \left( \frac{\sigma_{ij}}{r_{ij}} \right)^6 \right] + \frac{q_i q_j}{4\pi\epsilon_0 r_{ij}}
 \end{aligned} \tag{S1}$$

Here,  $r$  is the bond length,  $r_0$  is the equilibrium bond length,  $k_l$  is the bond length force constant,  $\theta$  is the bond angle,  $\theta_{eq}$  is the equilibrium bond angle,  $k_\theta$  is the bond angle force constant,  $r_{ij}$  is the site-site separation,  $\epsilon_{ij}$  is the LJ well depth and diameter and  $q_i$  and  $q_j$  are the partial charges

on sites  $i$  and  $j$ , respectively. For LJ interactions between two different atom types, the standard Lorentz-Bethelot empirical combining rules were used to compute parameters using Equation S2.

$$\sigma_{ij} = \frac{1}{2} (\sigma_{ii} + \sigma_{jj}) \quad \varepsilon_{ij} = (\varepsilon_{ii}\varepsilon_{jj})^{1/2} \quad (\text{S2})$$

For the saturated and unsaturated hydrocarbons, all pseudo-atoms were connected to pseudo-atoms formed from heavy atoms of the same electronegativity; thus, partial charges are not needed here for the TraPPE-UA potential.

The potential parameters that are used to fully describe these molecules are given in Tables S1, S2, S3, and S4.

Table S1: UA force field parameters for non-bonded interactions .<sup>3-5</sup>

Pseudo/United atom	$\varepsilon/k_B$ [K]	$\sigma$ [Å]	$q$ [e]
CH <sub>3</sub> (sp <sup>3</sup> )	98.0	3.750	0.0
CH <sub>2</sub> (sp <sup>3</sup> )	46.0	3.950	0.0
CH <sub>2</sub> (sp <sup>2</sup> )	85.0	3.675	0.0
CH (sp <sup>3</sup> )	10.0	4.680	0.0
C (sp <sup>3</sup> )	0.5	6.400	0.0
C (sp <sup>2</sup> )	20.0	3.850	0.0

Table S2: UA force field parameters for 1-2 bonded interactions .<sup>1-6</sup>

Bond	$r_0$ [Å]	$k_l/k_B$ [K/Å <sup>2</sup> ]
CH <sub>x</sub> -CH <sub>y</sub>	1.54	452900
CH <sub>x</sub> =CH <sub>y</sub>	1.33	825280

Table S3: UA force field parameters for 1-3 bonded interactions .<sup>3-5</sup>

Bond	$\theta_0$ [Å]	$k_\theta/k_B$ [K/rad <sup>2</sup> ]
CH <sub>x</sub> -CH <sub>2</sub> -CH <sub>y</sub>	114.0	62500
CH <sub>x</sub> -CH-CH <sub>y</sub>	112.0	62500
CH <sub>x</sub> -C-CH <sub>y</sub>	109.5	62500
CH <sub>x</sub> =C-CH <sub>y</sub>	119.7	70420

Table S4: UA force field parameters for 1-4 bonded interactions .<sup>3-5</sup>

Bond	$c_0/k_B$ [K]	$c_1/k_B$ [K]	$c_2/k_B$ [K]	$c_3/k_B$ [K]
CH <sub>x</sub> -CH <sub>2</sub> -CH <sub>2</sub> -CH <sub>y</sub>	0.00	355.03	-68.19	791.32
CH <sub>x</sub> -CH <sub>2</sub> -CH-CH <sub>y</sub>	-251.06	428.73	-111.85	441.27
CH <sub>x</sub> -CH <sub>2</sub> -C-CH <sub>y</sub>	0.00	0.00	0.00	461.29
CH <sub>x</sub> -CH <sub>2</sub> -C=CH <sub>y</sub>	688.50	86.36	-109.77	-282.24

## Viscosity Simulation Details

The low-shear or Newtonian viscosity of fluids was modeled using the GreenKubo (GK) approach which relate the shear viscosity to the integral over time of the pressure tensor autocorrelation function <sup>7,8</sup>

$$\eta_0 = \frac{V}{k_B T} \int_0^\infty \langle P_{\alpha\beta}(t) P_{\alpha\beta}(0) \rangle dt \quad (\text{S3})$$

Here,  $V$  is the system volume,  $k_B$  is the Boltzmann constant,  $T$  is the temperature,  $P_{\alpha\beta}$  denotes the element  $\alpha\beta$  of the pressure or stress tensor, and the angle bracket indicates the ensemble average.

The high shear viscosity  $\eta$  in the non-equilibrium molecular dynamics simulation was determined by computed the ratio of shear stress  $P_{xz}$  to the shear rate  $\dot{\gamma}$ .

$$\eta = -\frac{P_{xz}}{\dot{\gamma}} \quad (\text{S4})$$

## Governing Equations

**Rouse Model:** The Rouse model <sup>9-11</sup> provides the relaxation times as a function of density  $\rho$  and viscosity  $\eta_0$  of fluid, and the molecular weight  $M$  of polymer as

$$1/\lambda = \frac{\pi^2 \rho R_g T}{12 \eta_0 M} \quad (S5)$$

**Bird et al. Model:** This model <sup>12,13</sup> provides the relaxation times as a function of density  $\rho$  and viscosity  $\eta_0$  of fluid, and the molecular weight  $M$  and concentration  $c_p$  of polymer. In addition to this, it consider the viscosity  $\eta_{0s}$  of solvent which is base oil in this case.

$$1/\lambda = \frac{c_p \rho R_g T}{(\eta_0 - \eta_{0s}) M} \quad (S6)$$

**Kendall-Monroe:** The kinematic viscosity of blend of polymer and base oil was determined by the Kendall-Monroe equation which calculate the viscosity of a blend as the cubic-root average of the viscosity of its components,

$$\mu^{1/3} = x_p \mu_p^{1/3} + x_s \mu_s^{1/3} \quad (S7)$$

Here,  $\mu$ ,  $\mu_p$ , and  $\mu_s$  are the kinematic viscosity of blend, polymer, and base oil or solvent,  $x_p$  and  $x_s$  are the mole fraction of polymer and base oil in he blend, respectively.

**William-Landel-Ferry (WLF):** The Newtonian viscosity of polyisobutylene (PIB) as a function of its molecular weight was calculated using an empirical model. This empirical model has been extracted from a large set of experimental data to provide viscosity in mPa·s at 25°C . <sup>14,15</sup>

$$\eta_{0p} = 4.69 \times 10^{-9} M^{3.43} \quad (S8)$$

The viscosity of PIB at any temperature  $T$  can be obtained by a temperature shift factor which is described by the WLF equation as

$$\log(a_T) = \log(\eta_{0p}(T)/\eta_{0p}(T_0)) = -\frac{c_1(T - T_0)}{c_2 + (T - T_0)} \quad (\text{S9})$$

Here,  $T_0$  is the reference temperature of 25°C and empirical parameters  $c_1 = 8.61$  and  $c_2 = 200$  K<sup>14,15</sup>

## Carreau Model

Parameter of the Carreau fit to experiment and simulation viscosity data are tabulated in Table S5.

Table S5: Parameter of the Carreau fit to experiment and simulation viscosity data.

2*Temperature	2*Fluid ID	Parameters			
		$\eta_0$ [mPa·s]	$\eta_\infty$ [mPa·s]	$\lambda$ [s]	n [-]
3*50°C	Fluid 1	40.149	0.000	$1.898 \times 10^{-6}$	0.763
	Fluid 2	61.917	1.564	$3.592 \times 10^{-6}$	0.712
	Fluid 3	35.451	0.000	$3.693 \times 10^{-8}$	0.671
3*80°C	Fluid 1	15.837	0.000	$4.143 \times 10^{-7}$	0.793
	Fluid 2	22.260	0.000	$7.742 \times 10^{-7}$	0.790
	Fluid 3	13.483	0.000	$9.932 \times 10^{-9}$	0.662

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