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Novel Combined Load Frequency Control and Automatic Voltage Regulation of a 100% Sustainable Energy Interconnected Microgrids

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Abstract: Frequency and voltage deviations are two main problems in microgrids, especially with the increase in the penetration level of renewable energies. This paper presents novel techniques to apply combined the load frequency control and automatic voltage regulation of two interconnected microgrids. The two microgrids are operated by solar energy and bioenergy technologies and include energy-storage facilities. The control is applied using a novel accelerating PID controller (PIDA), which is compared to state-of-the-art control schemes. The controllers are designed using a new doctor and patient optimization technique (DPO), which is compared to state-of-the-art techniques. The combined design of load frequency controllers and automatic voltage regulators is also compared to a standalone design. The comparisons are carried out by testing the system performance at each operation condition in addition to indicators such as integral absolute error for frequency and voltage and integral time absolute error for frequency and voltage. The results show that a combined DPO–PIDA design of LFC–AVR schemes for fully sustainable microgrids has better performance than other standalone designs and other control and optimization alternatives.

Keywords: 100% renewables; automatic voltage regulator; load frequency control; accelerating PID; doctor and patient optimization; bioenergy; solar energy

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1. Introduction

There has been a considerable interest in turning grids to 100% renewable energies. Many countries in Asia and Africa are working towards creating a high penetration level of renewables through solar energy and bioenergy technologies [1,2]. The idea behind using solar and bioenergy technologies is the presence of the high amount of waste in those countries in addition to the high solar potential [3–5].

Automatic voltage regulation (AVR) is highly important in a power system to avoid under- and over-voltage occurrences [6]. AVR offers optimal power system operation by minimizing active and reactive power losses. The AVR is implemented by tracking a steady reference through controllers and actuators [7].

Load frequency control (LFC) is very important in terms of power system security. Most historical blackouts resulted from under/over-frequency events. LFC schemes gives the chance to minimize frequency oscillations and deviations from spreading among power system areas [8].

Many controllers are used either in LFC or AVR such as the proportional integral derivative (PID) control scheme [9], nonlinear PID (NPID) [10], and fractional order PID (FOPID) [11]. The comparison between those controllers proved that the increase in the

control variables leads the system to better performance. In [12], the nonlinear FOPID (NFOPID) control scheme is presented as a hybrid controller between NPID and FOPID.

Microgrids are considered as the most applicable solution in places where there is difficulty in reaching the national or regional power systems. It is a hot research topic to operate microgrids with only renewable energies, due to the variability that could affect system frequency and voltage. In [12,13], the authors applied load frequency control on 100% renewable energy interconnected microgrids using novel nonlinear fractional order PID control. In [14], the authors applied automatic generation control in a fully sustainable marine microgrid, using tidal supplementary control in the form of fractional integrators. In [12–14], the research did not consider the voltage problems and did not afford any solutions to it. In [15], the authors applied secondary voltage control in a power system with fully renewable power generation using a neural network and a genetic algorithm, but the research did not consider possible ways to control the frequency.

With the increase in the penetration level of renewables, there are the problems of voltage and frequency deviations that may lead to a blackout, so the coupling between LFC and AVR increases due to the high degree of uncertainty and nonlinearity [16]. In [17], the authors proposed the design of a nonlinear threshold accepting PID, based on a combined AVR–LFC scheme for a conventional multi-area power system. The results proved that the applied technique behaves better than other optimization techniques. In [18], the authors presented particle swarm PID based on a combined LFC–AVR scheme for a multi-area system. In [19], the authors applied lightning search FOPID based on a combined LFC–AVR scheme for a multi-area system. The multi-area system includes conventional and renewable resources. The results proved that lightning search FOPID drives the system to better performance than other techniques. In [20], authors presented a novel technique to control a multi-area power system with coupled LFC–AVR, but the system consisted of conventional and renewable energy technologies. In [21], authors compared the performance of the load frequency control with and without the presence of AVR, but the application was applied in a conventional generation system.

All the previous research papers [12–21] highlight solutions to optimally design load frequency controllers and/or automatic voltage regulators in the presence of different penetration levels of renewable energies. None of them studied the combined design of LFC and AVR in interconnected microgrids with a 100% penetration level of renewable energies.

In [22], Mohammad Dehghani et al. proposed a new doctor and patient algorithm (DPO) optimization technique. The new technique for state-of-the-art optimization techniques proved better performance than, namely the particle swarm (PSO) algorithm [23], the grasshopper optimization (GOZ) algorithm [24], and the socio evolution & learning optimization (SELO) algorithm [25].

The main contributions of this paper are:

1. Application of an LFC–AVR scheme on a multi-area system with 100% renewable energy.
2. Proposal of a novel controller, which is an accelerating PID (PIDA), in comparison with the state-of-the-art control schemes, namely FOPID, NPID, and PID.
3. Application of DPO as a new optimization technique in comparison with the state-of-the-art techniques.
4. Comparison between separate and combined designs of LFC and AVR.
5. Proposal of a new cost function for the controllers' design.

The rest of the paper is organized as follows: Section 2 describes the configuration of the studied 100% renewable energy multi-area system. Section 3 discusses the LFC–AVR scheme and PIDA controller. Section 4 illustrates the optimization problem and the novel optimization technique. Section 5 presents the simulation results, while Section 6 presents a discussion on the results, and Section 7 illustrates the main conclusion.

2. 100% Renewable Energy Interconnected Microgrids

Many locations in Africa have no electricity access, yet are rich with waste and sun as resources for energy transformation. Therefore, Africa is a cultivated land for demonstrating fully renewable energy microgrids in agriculture and industrial communities. Marine communities are also particularly good candidates to employ 100% renewable energy, since seas and oceans are rich with marine biomass, and the sun is also always present there. In this research, each microgrid is consisting of three bioenergy technologies and two solar energy facilities in addition to storage. The bioenergy technologies are a combined biomass heat and power unit, a biogas unit, and a micro-hydro turbine unit. The solar energy units are a photovoltaic unit and a parabolic dish unit. Battery energy storage technology is used to store and generate electricity. Figure 1 shows the two interconnected microgrids used in agriculture and marine communities, including the LFC–AVR combined model of the interconnected system. All the names of the parameters and variables that are written in Equations (1)–(21) are illustrated in Table 1.

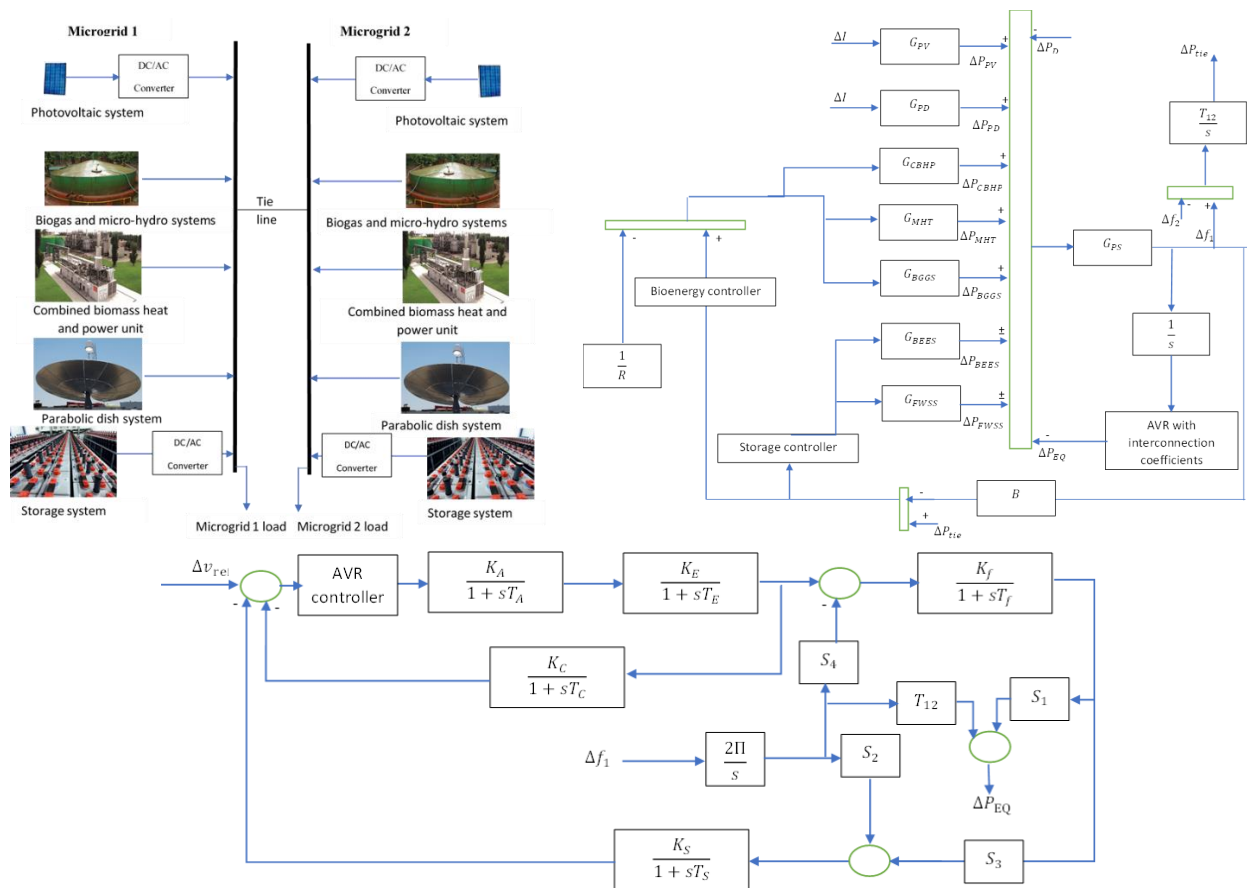


Figure 1. Combined LFC–AVR model for two identical interconnected microgrids with 100% renewables.

Table 1. System parameters values [13,16,17].

Parameter	Nomenclature	Value
T_{PV}	PV time constant	1.8 s
K_{PD}	Parabolic dish gain	1
T_T	Parabolic dish time constant	0.3 s
K_{BC}	Participation factor of CBHP	0.33
T_{BC}	Time constant of speed governor	0.2 s
K_R	Turbine gain	0.3
T_R	Time constant of turbine	10 s
T_{BCT}	Time constant of reheat	0.3 s
K_{MG}	Participation factor of MHT	0.33
T_{HG}	Transient droop	0.2 s
T_{RS}	Governor delay	5 s
T_{RH}	Reset	28.75 s
T_{HT}	Turbine delay	1 s
K_{BGGs}	Participation factor of BG	0.33
T_{CR}	Combustion reaction delay	0.01 s
T_{BG}	Biogas delay	0.23 s
X_c	Lead time	0.6 s
Y_c	Lag time	1 s
b_B	Valve actuator	0.05
T_{BT}	Discharge time constant	0.2 s
K_{BESS}	Battery gain	0.0033
T_{BESS}	Battery time constant	0.1 s
K_{FWSS}	Flywheel gain	0.01
T_{FWSS}	Flywheel time constant	0.1 s
M_{eq}	System inertia	0.2 s
D	Damping constant of the power system	0.012
B	Frequency bias factor	18.4
T12	Synchronized power	1.9
$\Delta f_1, \Delta v_1$	Change in microgrid 1 frequency and voltage	
Δf_2 and Δv_2	Change in microgrid 2 frequency and voltage	
S_1, S_2, S_3 and S_4	Coupling coefficients of AVR	0.2, -0.1, 0.5, and 1.4
$\Delta P_{EQ}, \Delta E_f, \Delta E_e$ and ΔE_u	Deviation in equivalent power due to AVR, field response, exciter response, error in voltage	
ΔO_1 and ΔO_2	Combined effect and controller action of AVR	
$K_A, T_A, K_E, T_E, K_f, T_f,$ K_C, T_C, K_s and T_s	Amplifier, exciter, field, compensator, sensor gains, and time constants of the AVR	40, 0.05 s, 1.0, 0.55 s, 0.8, 1.4 s, 0.5, 0.715 s, 1.0, and 0.05 s.
K_p, K_i and K_D	PID controller gains	
λ and μ	Integral and derivative powers in FOPID controller	
G	Nonlinear gain in NPID	
$K_{C1}, K_{C2}, K_{C3}, K_{C4},$ K_{C5}, K_{C6} and K_{C7}	PIDA controller gains	

2.1. Bioenergy Technologies

Bioenergy technologies are mainly focusing on converting different types of wastes to electrical energy.

2.1.1. Combined Biomass Heat and Power Unit (CBHP)

The unit converts solid waste into electricity through the following transfer function (1), which includes a steam turbine, reheater, and speed governor.

$$G_{CBHP} = \frac{K_{BC}}{1+sT_{BC}} \frac{1+sK_R T_R}{1+sT_R} \frac{1}{1+sT_{BCT}} \quad (1)$$

where K_{BC} is the participation factor of CBHP, T_{BC} is time constant of the speed governor, K_R is turbine gain, T_R is time constant of the turbine, and T_{BCT} is time constant of the reheater.

2.1.2. Micro-Hydro Turbine Unit (MHT)

The unit converts wastewater into electric energy, modeled through the transfer function in (2), which includes a penstock speed regulator and a micro-hydro turbine.

$$G_{MHT} = \frac{K_{MG}}{1+sT_{HG}} \frac{1+sT_{RS}}{1+sT_{RH}} \frac{1-sT_{HT}}{1+0.5sT_{HT}} \quad (2)$$

where K_{MG} is the participation factor of MHT, T_{HG} is transient droop, T_{RS} is governor delay, T_{RH} is reset, and T_{HT} is turbine delay

2.1.3. Biogas Unit (BG)

The unit converts the animal wastes to electricity, modeled through the transfer function in (3), which includes an inlet valve, combustor, and turbine.

$$G_{BGGs} = K_{BGGs} \frac{1+sX_c}{(1+sY_c)(1+s b_B)} \cdot \frac{1+sT_{CR}}{1+sT_{BG}} \cdot \frac{1}{1+sT_{BT}} \quad (3)$$

K_{BGGs} is the participation factor of BG, T_{CR} is combustion reaction delay, T_{BG} is biogas delay, X_c is lead time, Y_c is lag time, b_B is valve actuator, and T_{BT} is discharge time constant.

2.2. Solar Energy Technologies

Solar energy technologies have a high growing rate among other renewable energy systems. The most two famous technologies are photovoltaics (PV) and concentrated solar power (CSP). A parabolic dish (PD) is one of the types of CSP.

2.2.1. PV Unit

A PV unit converts the solar radiation into electricity. The unit is modeled using the transfer function in (4), which includes radiation, temperature, area, and efficiency.

$$G_{PV} = \frac{\Delta P_{PV}}{\Delta I} = \frac{1}{1+T_{PV}s} \quad (4)$$

where T_{PV} is PV time constant.

2.2.2. PD Unit

A PD unit concentrates solar energy at a point with 40% to 60% efficiency. The unit is modeled using the transfer function in (5).

$$G_{PD} = \frac{\Delta P_{PD}}{\Delta I} = \frac{K_{PD}}{1+T_{PD}s} \quad (5)$$

where K_{PD} is PD gain, and T_{PD} is PD time constant.

2.3. Energy Storage Systems

Each microgrid has two storage technologies, namely a battery storage system and a flywheel storage system. The transfer function of the battery energy and flywheel energy systems is shown in (6) and (7), respectively.

$$G_{BESS} = \frac{K_{BESS}}{1+T_{BESS}s} \quad (6)$$

$$G_{FWSS} = \frac{K_{FWSS}}{1+T_{FWSS}s} \quad (7)$$

where K_{BESS} and T_{BESS} are the battery system's gain and time constant, respectively, while K_{FWSS} and T_{FWSS} are the flywheel system's gain and time constant, respectively.

2.4. Microgrids Equations

The following equations illustrate the microgrids generation, demand and interconnection powers.

$$\Delta P_e = P_{PV} + P_{DG} + P_{MHT} + P_{BG} + P_{CBHP} \pm P_{BESS} \pm P_{FWSS} - P_D \pm \Delta P_{tie} \quad (8)$$

$$\Delta P_{tie} = \frac{T_{12}}{s} (\Delta f_1 - \Delta f_2) \quad (9)$$

$$G_{PS} = \frac{\Delta f}{\Delta P_e} = \frac{1}{D + M_{eq}s} \quad (10)$$

$$B = \frac{1}{R} + D \quad (11)$$

where M_{eq} is the microgrid inertia, D is the damping constant of the microgrid, B is the frequency bias factor, and T_{12} is the synchronized power.

3. System Control

3.1. LFC and AVR Interconnection

In large power grids, it is very rare to find a considerable relation between the change of voltage and the change in frequency, so it is neglected. In microgrids, the voltage and frequency changes are considered and modeled as shown in (12–18)

$$\Delta P_{EQ} = T_{12}\Delta\delta + S_1\Delta E_f \quad (12)$$

$$\Delta v = S_2\Delta\delta + S_3\Delta E_f \quad (13)$$

$$\Delta E_f = \frac{K_f}{1+sT_f} (-S_4\Delta\delta + \Delta E_e) \quad (14)$$

$$\Delta E_e = \frac{K_A}{1+sT_A} \frac{K_E}{1+sT_E} \Delta O_1 \quad (15)$$

$$\Delta E_u = \Delta v_{ref} - \frac{sK_C}{1+sT_C} \Delta E_e - \frac{K_S}{1+sT_S} \Delta v_1 \quad (16)$$

$$\Delta O_1 = (K_{P1} + \frac{K_{I1}}{s} + K_{D1}s) \Delta E_u \quad (17)$$

$$\Delta O_2 = ((K_{P2} + \frac{K_{I2}}{s} + K_{D2}s) - \frac{1}{R}) \Delta f \quad (18)$$

where S_1 , S_2 , S_3 , and S_4 are coupling coefficients of AVR, K_A , T_A , K_E , T_E , K_f , T_f , K_C , T_C , K_S , and T_S are amplifier, exciter, field, compensator, sensor gains, and time constants of the AVR, respectively. ΔP_{EQ} , ΔE_f , ΔE_e , and ΔE_u are deviation in equivalent power due to AVR, field response, exciter response, and error in voltage, respectively.

3.2. Control Schemes

Different control schemes are applied to the system to control frequency, voltage and tie-line power. PID is used in previous work such as [12]. In [13], the authors applied control using FOPID and NPID controllers. The FOPID and NPID controllers transfer functions shown in (19) and (20). This paper presents a novel control scheme which is accelerating PID (PIDA). The controller has a transfer function shown in (21). The PIDA controller has 7 parameters which increase the flexibility if the controller which may drive the system to better performance.

$$G_{FOPID} = K_P + \frac{K_I}{s^\lambda} + K_D s^\mu \quad (19)$$

$$G_{NPID} = (K_P + \frac{K_I}{s} + K_D s) \frac{e^{(GxE)} + e^{-(GxE)}}{2} \quad (20)$$

$$G_{PIDA} = \frac{K_{C1}s^3 + K_{C2}s^2 + K_{C3}s + K_{C4}}{K_{C5}s^2 + K_{C6}s + K_{C7}} \quad (21)$$

where K_P , K_I , and K_D are PID controller gains, λ and μ are integral and derivative powers in the FOPID controller, respectively. G is nonlinear gain in NPID, while K_{C1} , K_{C2} , K_{C3} , K_{C4} , K_{C5} , K_{C6} , and K_{C7} are PIDA controller gains.

4. Optimization Problem

4.1. Optimization Problem Definition

In this work, the objective is to reduce the frequencies, voltages, and tie-line power deviation. A new multi-objective function is developed to drive the system to better performance in terms of frequency and voltage. The function is the multiplication of time with the sum of derivatives of frequencies, voltages, and tie-line power.

$$F = \min\left(t\left(\frac{\partial \Delta f_1}{\partial t} + \frac{\partial \Delta f_2}{\partial t} + \frac{\partial \Delta P_{tie}}{\partial t} + \frac{\partial \Delta v_1}{\partial t} + \frac{\partial \Delta v_2}{\partial t}\right)\right) \quad (22)$$

The variables of the optimization problem are the controller's parameters. The system includes six controllers, which are the AVR controller, bioenergy controller, and energy storage controller of each area. If a PIDA control scheme is going to be applied to the system, the number of variables is 42 compared to 30 in an FOPID control scheme and 24 in an NPID control scheme.

The constraints of the optimization process are the boundaries of each parameter of each controller. In an FOPID control scheme, the constraints are $0 \leq \lambda \leq 1$ and $0 \leq \mu \leq 1$, while in an NPID controller, the constraint that must be considered is $0 \leq G \leq 1$.

4.2. DPO Design

DPO is inspired from the treatment of patients at this time of uncertainty. The optimization method is a virtual representation of the stages of patients' treatment. The three steps are vaccination, treatment, and surgery. The patients should be vaccinated to prevent infection in the first stage. The second step is that the patient takes medicine to deal with the virus or the infection. The third stage is surgery for patients in serious conditions.

The population of patients who need to be treated is represented in (23).

$$P = \begin{bmatrix} P_1 & P_1^1 & \dots & P_1^m \\ \vdots & \vdots & P_i^d & \vdots \\ P_N & P_N^1 & \dots & P_N^m \end{bmatrix} \quad (23)$$

where P is the patient population, P_i is the i^{th} patient, and P_i^d is the d^{th} feature of the i^{th} patient. N is the number of patients, and m is the number of variables.

There are three stages to process and update. The updating takes place through (24)–(27).

$$dosage_i = 2 - \frac{F_i^N}{F_{Best}^N} \quad (24)$$

$$F_i^N = \frac{fit_i - f_{worst}}{\sum_{j=1}^N (fit_j - f_{worst})} \quad (25)$$

$$f_{worst} = \max(fit) \ \& \ P_{worst} = P(location(f_{worst})) \quad (26)$$

$$f_{best} = \min(fit) \ \& \ P_{best} = P(location(f_{best})) \quad (27)$$

where $dosage_i$ is the vaccine dosage of patient i , F_i^N is the patient normalized fitness, F_{Best}^N is the best patient normalized fitness, and f_{worst} and f_{best} are the worst and best patients' objective function, respectively, while P_{worst} and P_{best} are the worst and the best patients' positions, respectively.

4.2.1. Stage 1: Vaccination Stage

Community health protection is applied through vaccination, and the modeling of this stage is illustrated in (28).

$$v_i^d = rand \times (dosage_i \times P_i^d - P_{worst}^d) \quad (28)$$

where v_i^d is the i th patient, d is the dimension of vaccine, $rand$ is a randomly selected number between 0 and 1, and P_{worst}^d is the worst patient d dimension.

4.2.2. Stage 2: Drug Administration

In this stage, the doctor selects the suitable pharmaceuticals according to the patient state. The stage can be modeled as shown in (29) and (30).

$$d_i^d = rand \times (P_{best}^d - dosage_i \times P_i^d) \quad (29)$$

$$P_i = \begin{cases} P_i + d_i, & fit(P_i + d_i) \leq fit_i \\ P_i, & else \end{cases} \quad (30)$$

where d_i^d is the dimension d of a drug nominated to patient number I , while P_{best}^d is the best patient d dimension.

4.2.3. Stage 3: Surgery

For late conditions, vaccination and drugs are not enough, and the only way to let the patient improve is surgery. The stage is modeled in (31)

$$P_i = \begin{cases} P_i \times 0.6 + P_{best} \times 0.4, & F_{Best}^N - F_i^N \leq 0.9F_{Best}^N \\ P_i, & else \end{cases} \quad (31)$$

4.3. Indicators

Integral absolute error for frequency and voltage (IAE), in addition to integral time absolute error for frequency and voltage (ITAE), are used as indicators to compare between controllers, tuning methods, and optimization techniques.

$$IAE = \int_0^T \Delta f_1 + \Delta f_2 + \Delta P_{tie} + \Delta v_1 + \Delta v_2 \, dt \quad (32)$$

$$ITAE = \int_0^T t * (\Delta f_1 + \Delta f_2 + \Delta P_{tie} + \Delta v_1 + \Delta v_2) \, dt \quad (33)$$

5. Simulation Results

5.1. Test 1: Comparison between Different Optimization Techniques

In this test, a comparison between different optimization techniques, namely DPO, PSO, GOZ, and SELO, is performed. A load increase by 1% is simulated 1 s after starting the simulation of the system. The parameters of all PID controllers in the combined LFC–AVR model are calculated using each optimization technique. Figure 2 shows the performance of the change in the frequencies, powers, and voltages of the system for each optimization technique. The results show that DPO drives the two interconnected microgrids to better performance. Figure 3 shows that novel DPO leads the system to a better objective function result, with less IAE and ITAE having a smaller number of iterations.

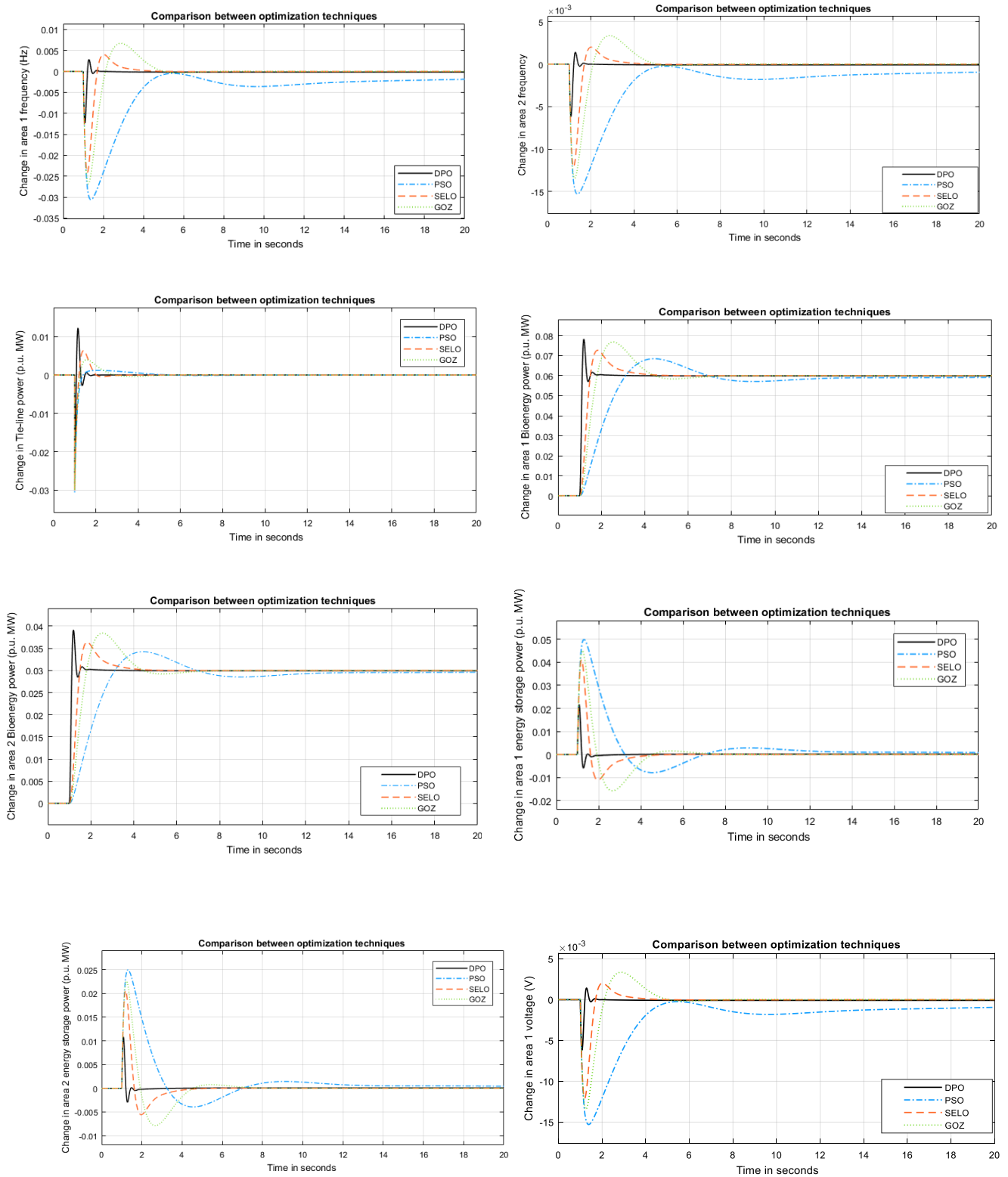


Figure 2. Change in frequencies, power, and voltages using different optimization techniques.

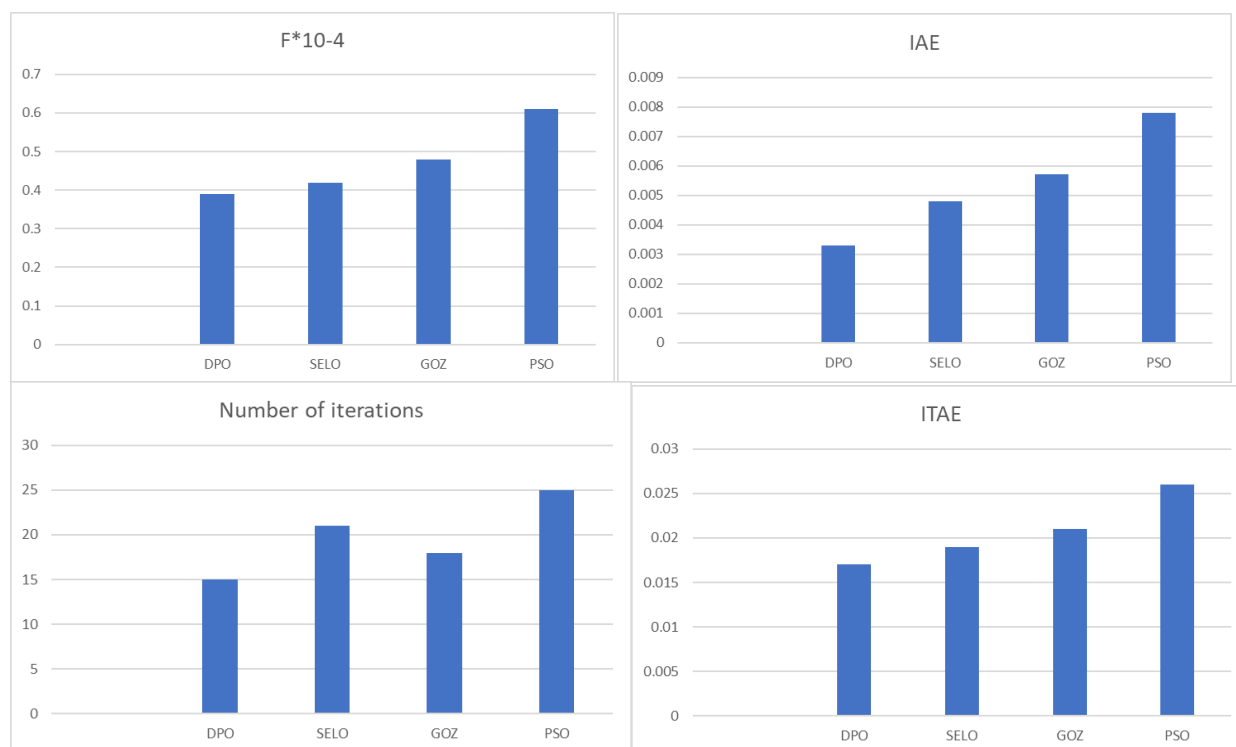


Figure 3. Comparison between different optimization techniques using objective function, ITAE, IAE, and number of iterations.

5.2. Test 2: Comparison between Different Control Schemes

In this test, a comparison between different controllers, namely PIDA, FOPID, and PID is performed by subjecting the two microgrids to a 10% increase in demand. The parameters of all controllers are calculated using the DPO optimization technique. Figure 4 shows the performance of the change in frequencies, powers, and voltages of the system at each optimization technique. The results show that DPO leads the two interconnected microgrids to better performance. Figure 5 shows that novel PIDA leads the system to a better objective function result, with better IAE and ITAE than the other state-of-the-art control schemes.

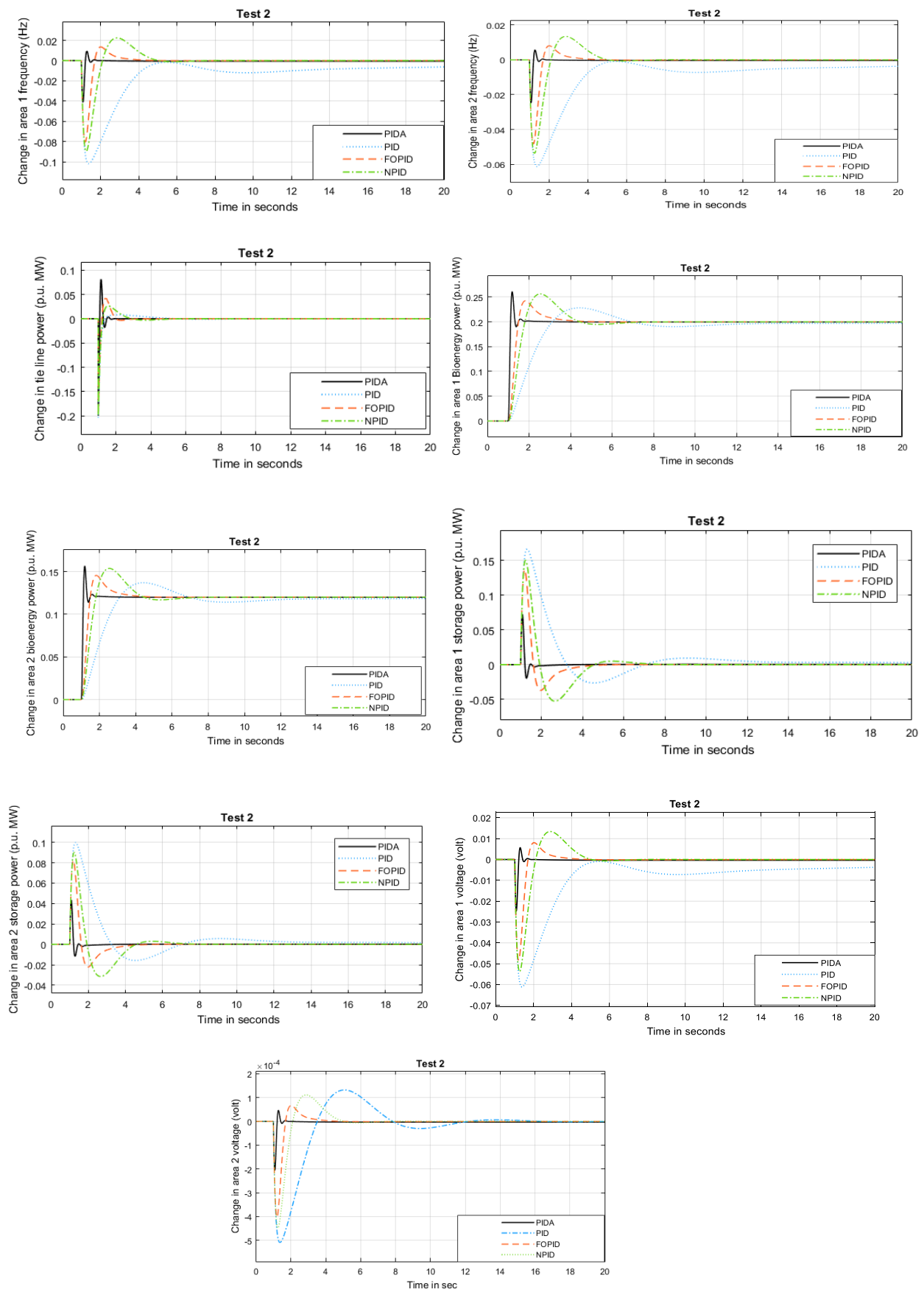


Figure 4. Change in frequencies, power, and voltages using different control schemes.

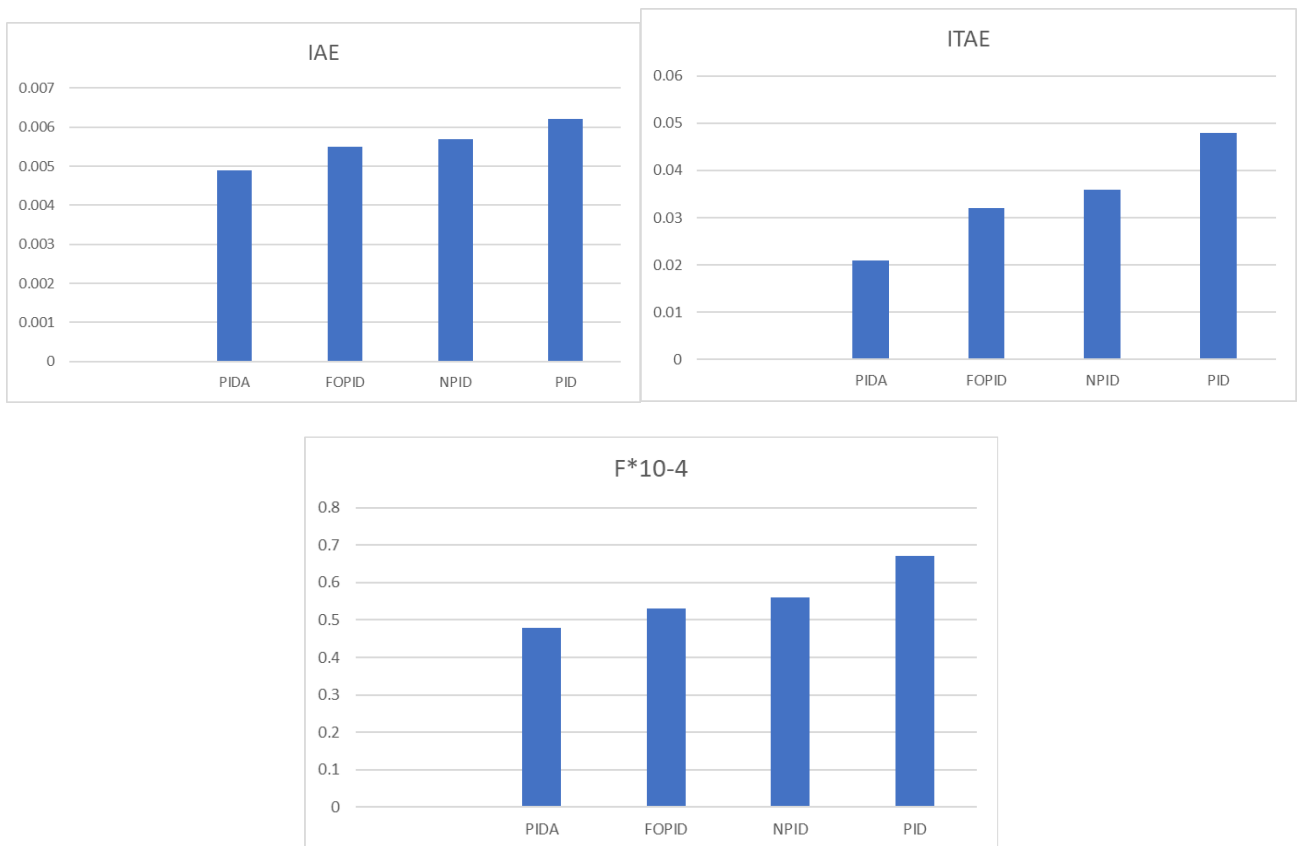


Figure 5. Comparison between different control schemes using objective function, ITAE, and IAE.

5.3. Test 3: Comparison between Combined Design of AVR-LFC Controllers and Standalone Design of AVR and LFC Controllers

In this test, a comparison between the design of AVR and LFC controllers at the same time (combined) and a standalone design for AVR and LFC controllers (AVR controllers are designed, then LFC controllers are designed), when the two areas are subjected to the same real change in demand and solar power. The case study used in this test is SEKEM farm in ElWahat [26,27]. The parameters of all controllers are calculated using the DPO optimization technique. Figure 6 shows the performance of the change in frequencies, powers, and voltages of the system using combined PIDA, standalone PIDA, combined FOPID, and standalone FOPID controllers. The results show that combined PIDA controllers led the two interconnected microgrids to better performance than other alternatives. Figure 7 shows that using PIDA in a combined LFC–AVR model led the system to a better objective function result, with better IAE and ITAE than standalone models of AVR and LFC, plus the combined model is better than the standalone model in the case of using FOPID.

The results proved that applying a combined LFC–AVR design for PIDA using DPO will lead to better system performance in terms of frequency and voltage than the other alternatives and scenarios.

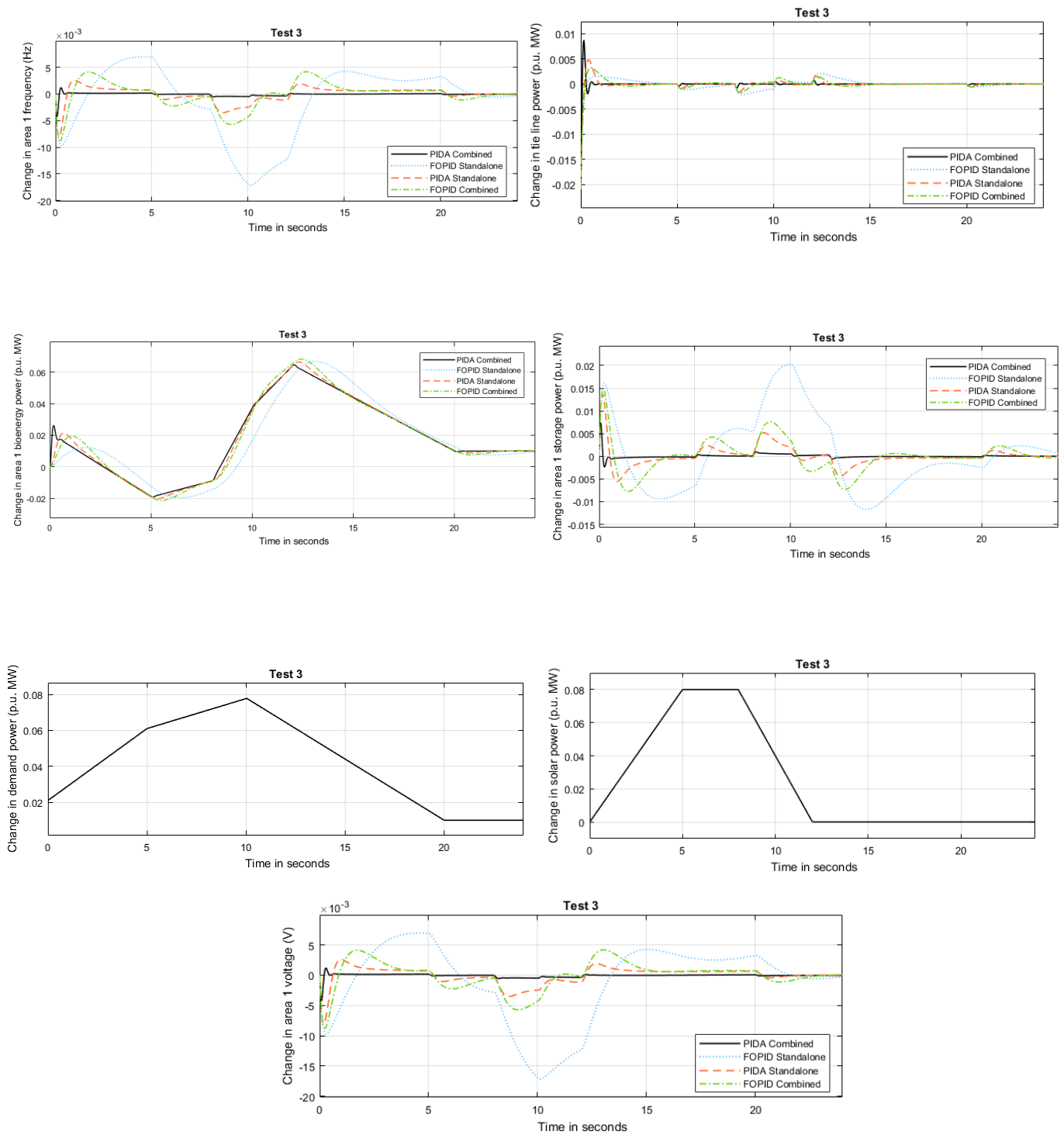


Figure 6. Change in frequencies, power, and voltages using standalone and combined designs of PIDA and FOPID controllers.

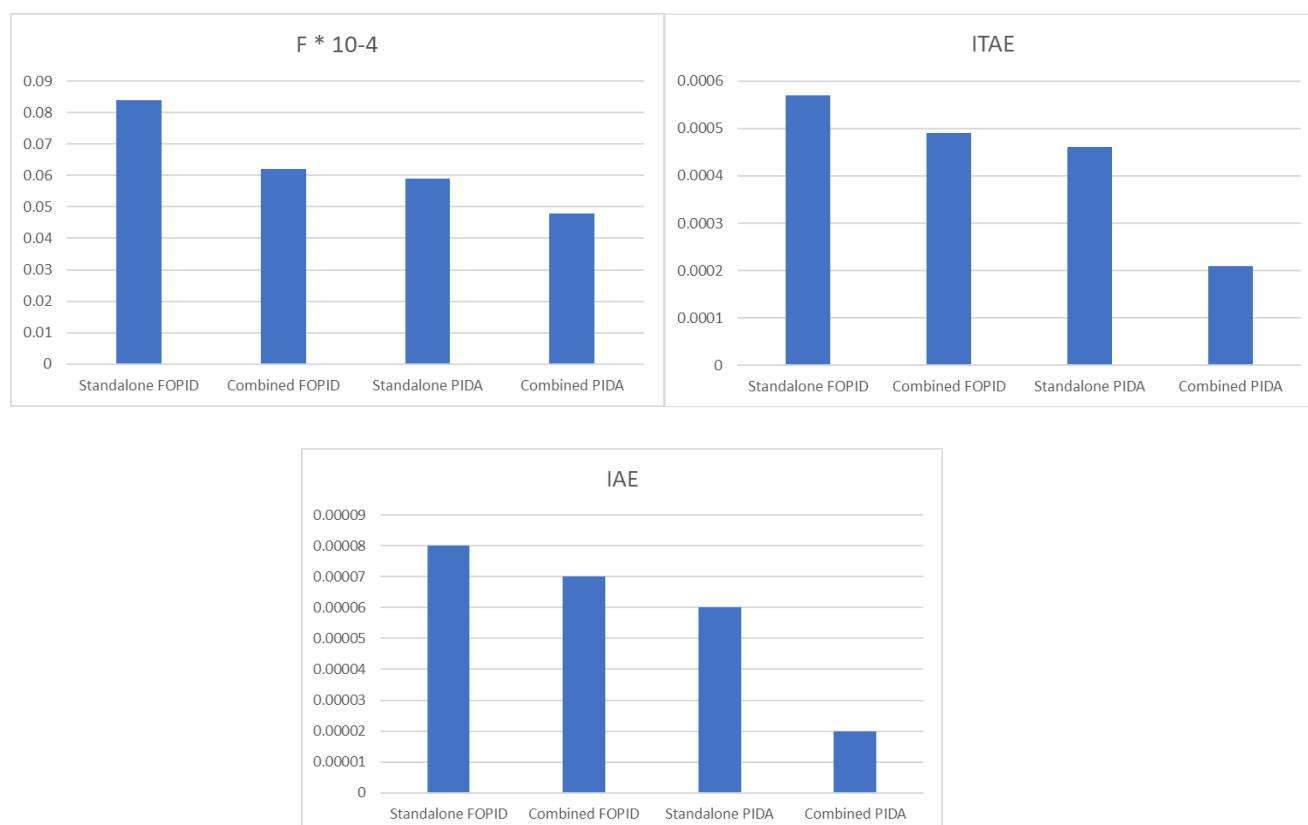


Figure 7. Comparison between standalone and combined designs of PIDA and FOPID control schemes using objective function, ITAE, and IAE.

6. Discussions

The paper presented a combined model for LFC–AVR to improve the performance of two interconnected identical microgrids operated by 100% renewable energy technologies. The whole system is simulated according to Equations (1)–(21) in MATLAB SIMULINK version 2017A. The system is subjected to different case studies to compare between different control schemes and optimization techniques. The system is also examined in a real-case scenario.

The system is subjected to a 1% increase in demand in the two microgrids to compare between different optimization algorithms, namely DPO, which is a new algorithm, PSO, GOZ, and SELO. The results show that DPO is better than SELO, GOZ, and PSO in achieving the objective function, by 10%, 19%, and 37%, respectively. In terms of achieving less ITAE, DPO is better than SELO, GOZ, and PSO, by 11%, 18%, and 31%, respectively. The results also show that DPO is better than SELO, GOZ and PSO in achieving less ITAE, by 10%, 19%, and 37%, respectively. In terms of achieving less IAE, DPO is better than SELO, GOZ, and PSO, by 29%, 44%, and 62%, respectively.

The system is subjected to a 10% increase in the demand of each microgrid, to compare between different control schemes, namely PIDA, FOPID, NPID, and PID. The results show that PIDA drives the system to less objective function than FOPID, NPID, and PID, by 9%, 16%, and 29%, respectively. The results also show that PIDA drives the system to less IAE than FOPID, NPID and PID, by 13%, 17%, and 21%, respectively. The results show that PIDA drives the system to less ITAE than FOPID, NPID, and PID, by 34%, 39%, and 59%, respectively.

The system is subjected in test three to the real change in radiation and demand in SEKEM farm in ElWahat, which is located in western Egypt. The aim of this test is to compare the standalone design and the combined design of LFC–AVR. The results show that combined design led the system to better performance than the standalone design, by

18%, 58%, and 67%, in terms of objective function, ITAE, and IAE, respectively. The results also proved that the combined design of PIDA drives the system to better performance than the combined design of FOPID.

The simulated system is now turning to be implemented in the interconnected Egyptian farms in west Egypt, as a model for the whole of Africa to operate their farms using 100% sustainable energy technologies, employing sun and wastes as the main resources. The system is also valid for application in marine-isolated communities, since there is sun and marine wastes that can produce 100% green electricity, and by applying combined PIDA to LFC–AVR, the system reliability and performance will highly improve, to ensure a high quality of green electricity. The study will even help in achieving a 42% penetration level of renewable energies in Egypt by 2035, as planned by the government [28].

7. Conclusions

The paper studied the role of combined LFC–AVR on interconnected microgrids operated by fully sustainable energy solutions. The results proved that the design of combined AVR–LFC controllers drives the system to better performance than a standalone LFC and a standalone AVR, in terms of ITAE and IAE. The results also proved that a novel PIDA control scheme leads the system to better performance than FOPID, NPID, and PID control schemes, in terms of microgrids' frequencies, powers, and voltages. The results also proved that the DPO optimization algorithm has better performance than other state-of-the-art algorithms, in terms of achieving better objective value, IAE, and ITAE, with a lower number of iterations during the control-scheme design process. The study also proved that biomass energy converters cover the changes in the demand and solar power more than energy storage systems.

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