Experiments on the Drag and Lift Coefficients of a Spinning Sphere

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Abstract: The drag and lift coefficients are important parameters that affect the particle motion in a viscous fluid. In the present study, the drag and lift coefficients of a spinning sphere in a water tank were studied experimentally using a high-speed camera. To this end, 22 cases were studied to cover a wide range of dimensionless angular speeds (0.149 < Rr < 3.471) and Reynolds numbers (610 < Re < 3472). Based on the present experimental data and the results obtained from the literature, expressions were developed to calculate the lift and drag coefficients. The performed analyses on lift coefficient show that there is a critical Reynolds number (Re_c) at each dimensionless angular speed. When 0 < Re < Re_c, the lift coefficient decreases with increasing the Reynolds number, while it is constant when Re_c < Re < 3500. The constant lift coefficient corresponding to different spin speeds was defined as the limit value of the lift coefficient. It is found that when 1 < Rr < 12, the limit value of the lift coefficient is 0.37, while the limit value of the lift coefficient increases with increasing dimensionless angular speed at 0 < Rr < 1. It is found that the spin increases the drag coefficient of a spinning sphere only when 0 < Rr < 10. Moreover, the performed analyses show that the drag coefficient of a spinning sphere is less than that of a non-spinning sphere when 10 < Rr < 25.

Keywords: spinning sphere; lift coefficient; drag coefficient; Reynolds number; angular speed

1. Introduction

Drag and lift forces are loads that affect particle motion. The lift force can often be significant and can even approach the magnitude of the drag force in some circumstances for surface spin velocities on the order of the translational particle velocity. Saffman [1] and Magnus [2] pointed out that the lift force is especially important for lateral migration in tubes and particle deposition in boundary layers. Yang and Leeming [3] and Barkla and Auchterlonie [4] called the lift force originating from rotating of particles the Magnus lift force. The drag and lift coefficients have been studied by researchers using theoretical analysis, experimental tests, and numerical simulations.

Theoretical studies provide exact results but are limited to special geometries and low Reynolds numbers. In this regard, Rubinow and Keller [5] derived an analytical solution for the spin-lift force in the Stokes regime through matched asymptotic expansions. It was found that the lift coefficient depends on the dimensionless angular speed at Rr << 1 and Re << 1. Dimensionless angular speed is defined as Rr = DΩ/ur, where D is the sphere diameter, Ω is the angular speed, and ur is the relative velocity between the particle and fluid. Moreover, the Reynolds number is defined as Re = urD/ν, where ν is the kinematic viscosity.

However, the results of theoretical studies are not reliable beyond the Stokes regime, and the lift coefficient should be obtained experimentally or numerically. In terms of experimental studies, Tusji et al. [6] analyzed the trajectories of an impinging and bouncing
sphere on an inclined plate and obtained the Magnus lift force on a rotating sphere at
550 < Re < 1600 and 0 < Rr < 1.4. Oesterle and Dinh [7] used stroboscopic photography
technology to study the lift force of a rotating sphere moving at a constant linear and
angular velocity in a viscous fluid. A mathematical expression was proposed to estimate
the lift coefficient in the range 10 < Re < 140 and 2 < Rr < 12. Macoll [8] performed
experiments at 46,000 < Re < 110,000 and reported that the lift coefficient was negative
for 0 < Rr < 0.4. Davis [9] performed experiments at a Reynolds number Re = 90,000. Tri
et al. [10] and Taneda [11] carried out experiments and studied problems with very large
Reynolds numbers.

Numerical simulations do not have most of the experimental challenges, such as
measuring uncertainties. Ben Salem and Oesterle [12] performed a numerical investigation,
applied different expressions for the lift and drag forces, and calculated the torque in a flow
at 0 < Re < 20. Kurose and Komori [13] performed numerical simulations and studied the
drag and lift forces acting on a spinning rigid sphere in a homogeneous linear shear flow at
1 ≤ Re ≤ 500. Niazzmand and Renksizbulut [14] studied transient wake flow patterns and
dynamic forces acting on a spinning spherical particle with non-uniform surface blowing
for different Reynolds numbers Re up to 300 and different dimensionless angular speeds
Rr up to 1. Kim [15] numerically investigated laminar flow passing a sphere rotating
in the transverse direction at Re = 100, 250, and 300 and dimensionless angular speeds
of 0 ≤ Rr ≤ 2.4. Poon and Ooi [16] simulated the flow passing a transversely rotating
sphere at different Reynolds numbers in the range 500 ≤ Re ≤ 1000 using an unstructured
finite volume collocated code. Citro et al. [17] performed direct numerical simulations and
three-dimensional global stability analyses in the ranges 150 ≤ Re ≤ 300 and 0 ≤ Rr ≤ 2.4.
Leal [18], Drew [19], Magnaudet and Eames [20], Tomiyama and Tamai [21], Loth [22],
and Shi and Rzehak [23] analyzed experimental and numerical results under different
conditions and drew meaningful conclusions.

The drag coefficient is another important parameter that affects the motion of particles.
Based on theoretical analyses, Stokes [24] derived an expression to calculate the drag force.
Swamee and Chandra [25] derived an empirical expression to calculate the drag coefficient.
Song et al. [26] considered the effect of particle shape and settling orientation and develop-
ed a correlation between the drag coefficient and the Reynolds number for spherical
and non-spherical particles. Amin and Umut [27] proposed a drag coefficient as a function
of nominal particle diameter, gravitational acceleration, ambient fluid kinematic viscosity,
and particle shape. Flemmer and Banks [28] and Kelessidis [29] proposed expressions
to estimate the drag coefficient of non-spinning particles in a uniform fluid. Cheng [30]
performed a review study and compared different expressions for the drag coefficient
of spherical particles. Malhotra and Sharma [31] performed an experimental study on
the drag coefficient of spherical particles in unbounded and confined surfactant-based
shear-thinning viscoelastic fluids. Wang et al. [32] studied the drag coefficient of natural
particles with highly irregular shapes. It is worth noting that the drag coefficient of spin-
nining particles differs from that of non-spinning ones. For a particle that spins at a small
Reynolds number with linearized inertia terms, Rubinow and Keller [5] showed that the
spin does not affect the drag coefficient of a spinning sphere. Kurose and Komori [13],
Niazzmand and Renksizbulut [14], Kim and Choi [15], Dobson and Poon [33], and Gia-
cobello and Balachandar [34] studied the drag coefficient of spinning particles at high
Reynolds numbers.

Reviewing the literature indicates that there have been few experiments on the lift and
drag coefficients, and only a few expressions have been proposed to calculate the lift-to-drag
ratio of a spinning sphere in the range of 500 < Re < 3000. Therefore, further experiments are
required to study the lift and drag coefficients in this range of Reynolds numbers. The main
purpose of the present study was to evaluate the drag and lift coefficients of a spinning
sphere with an angular speed in the range of 0.149 < Rr < 0.471 and a Reynolds number in
the range of 610 < Re < 3472 in a water tank using a high-speed camera. It was intended to
develop expressions to calculate the lift and drag coefficients. Furthermore, the lift-to-drag ratio of a spinning sphere was calculated.

2. Materials and Methods
2.1. Experimental Setup

The experiments were conducted in a 0.2 m long, 0.2 m wide, and 0.5 m high plexiglass water tank. The velocities and spin speeds of settled spheres were obtained by adjusting the release height of spheres on the orbit. The vertical distance between the top of the tank and the end of the orbit was 50 mm. A high-speed camera system was used to analyze the motion of spinning spheres. The camera system mainly consists of a high-speed camera (EoSens®3CXP, Mikrotron, Unterschleißheim, Germany), a memorizer (AQ8-CXP6D, Mikrotron, Unterschleißheim, Germany), and image processing software (Stream Pix, Norpix, Montréal, Canada). The image resolution was set to 1690 × 1710 pixels. The recording rate of the camera was set to 400 frames per second (FPS) to ensure clear images. The images were analyzed in the image processing software. Figure 1 shows the schematic view of the experimental setup.

Figure 1. Schematic view of experimental setup.

2.2. Experimental Methods
2.2.1. Measuring Procedure

The motion of spinning spheres was recorded from the tank side. The camera focused on the vertical plane that was located at the tank centerline. Then, a sufficient number of images were selected using image processing software, and the selected images were further processed by CAD software to calculate the velocity and spinning speed of spheres. To better observe the angular speed of spheres, the surfaces of the spheres were marked. Then, the connection line between the marked dots and the center of gravity of particles was obtained. The angular speed of spheres was calculated by measuring the angle change between the connection line and the gravity over time.

The diameter of spheres $D$ varied from 2.5 mm to 8.0 mm. The densities of the spheres and the fluid were 2390 kg/m$^3$ and 1000 kg/m$^3$, respectively. The velocity of spinning spheres $u_s$ was in the range of 0.244 m/s to 0.434 m/s. The velocity of the fluid $u = 0$. The relative velocity between the particle and fluid was in the range of 0.244 m/s to 0.434 m/s. The range of angular speed $\Omega$ was from 13.956 rad/s to 223.29 rad/s. The range
of dimensionless angular speed $R_r$ was from 0.149 to 3.471. The range of the Reynolds number $Re$ was from 610 to 3472. Table 1 presents the experimental conditions.

### Table 1. Experimental conditions.

<table>
<thead>
<tr>
<th>No.</th>
<th>$D$ (mm)</th>
<th>$u_s$ (m/s)</th>
<th>$\Omega$ (rad/s)</th>
<th>$R_r$</th>
<th>$Re$</th>
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Note: $D$ is the diameter of spheres, $u_s$ is the velocity of spinning spheres, $\Omega$ is the angular speed, $R_r$ is the dimensionless angular speed, $Re$ is the Reynolds number.

### 2.2.2. Data Processing Procedure

In order to describe the motion of the spinning sphere, the coordinate system was defined, as shown in Figure 1. The position of the onset of the sphere moving at a constant velocity was taken as the origin of the coordinate system. The positive direction of the $x$-axis is the same as the direction of the particle velocity component on the horizontal plane. Moreover, the positive direction of the $y$-axis is along the opposite direction of gravity. Figure 2 presents the trajectory of a 6 mm sphere as an example.

Figure 2. The trajectory of a 6 mm sphere.
The trajectory of the sphere can be approximated to 18.77 mm. The angle between the velocity vector of the sphere and the gravity vector can be obtained by fitting the data of the trajectory of spheres corresponding to a constant velocity. For the sphere presented in Figure 2, this angle and the corresponding angular speed are $\beta = 24.552^\circ$ and $\Omega = 34.889 \text{ rad/s}$, respectively. Since the fluctuation of sphere velocity is less than 1%, it can be considered uniform. Figure 3 shows that the velocity of a spinning sphere $u_s$ is 0.417 m/s.

The motion of spinning spheres is mainly affected by submerged weight, drag force, and lift force, as shown in Figure 4. Since the fluid is stationary, the velocity of the fluid $u = 0$. Therefore, the relative velocity between the particle and fluid $u_r$ is equal to the velocity of the spinning sphere $u_s$. The drag force is in the opposite direction of the sphere’s motion.

The submerged weight can be calculated using the following expression:

$$G = \frac{\pi D^3}{6} (\rho_s - \rho) g$$  \hspace{1cm} (1)
where \( G \) is submerged weight, \( g \) is gravitational acceleration, and \( \rho_s \) is the density of particles, \( \rho \) is the density of fluid. Moreover, the lift force of a spinning sphere can be obtained from the following expression:

\[
F_{L\Omega} = C_{L\Omega} \pi D^2 \frac{1}{2} \rho (u - u_s)^2
\]  

(2)

where \( F_{L\Omega} \) is the lift force of a spinning sphere, and \( C_{L\Omega} \) is the lift coefficient of a spinning sphere. The drag force of a spinning sphere can be mathematically expressed in the form below:

\[
F_{d\Omega} = C_{d\Omega} \pi D^2 \frac{1}{2} \rho (u - u_s)^2
\]  

(3)

where \( F_{d\Omega} \) is the drag force of a spinning sphere, and \( C_{d\Omega} \) is the drag coefficient of a spinning sphere.

According to Newton’s second law of motion-force and acceleration, when a particle moves at a constant velocity along a straight line, the acceleration of the particle is zero. Accordingly, the equation of motion of a spinning sphere that moves perpendicular to the velocity of the spinning sphere can be expressed as follows:

\[
F_{L\Omega} - G \sin \beta = 0
\]  

(4)

Meanwhile, the equation of motion of the spinning sphere can be expressed as follows:

\[
F_{d\Omega} - G \cos \beta = 0
\]  

(5)

By rearranging Equation (4), the lift coefficient can be expressed in the form below:

\[
C_{L\Omega} = \frac{4D}{3} \frac{\rho_s - \rho}{\rho} g \left( \frac{\sin \beta}{(u - u_s)^2} \right)
\]  

(6)

By rearranging Equation (5), the drag coefficient is expressed as follows:

\[
C_{d\Omega} = \frac{4D}{3} \frac{\rho_s - \rho}{\rho} g \left( \frac{\cos \beta}{(u - u_s)^2} \right)
\]  

(7)

Substituting the measured values of \( u, D, u_s, \) and \( \beta \) into Equations (6) and (7), the lift and drag coefficients of a spinning sphere can be calculated. It is noted that \( u = 0 \).

3. Results and Discussion

3.1. Lift Coefficient

The experimental results are presented in Table 2, indicating that the lift coefficients of a spinning sphere vary from 0.098 to 0.449.

The lift coefficients of the spinning sphere have been studied by other researchers. In this regard, Oesterle and Dinh [7] used stroboscopic photography technology to study the lift force of a spinning sphere moving in a viscous fluid. Kurose and Komori [13] performed three-dimensional numerical simulations and studied the lift force acting on a spinning rigid sphere in a homogeneous linear shear flow. Niazmand and Remksizbulut [14], Dobson and Poon [33], and Giacobello and Balachandar [34] investigated the lift coefficient through numerical simulation. The experimental and simulated results of the previous studies are summarized in Figure 5. They are represented by different symbols in Figure 5.

The correlation between the ratio of the lift coefficient to the dimensionless angular speed and the Reynolds number indicates that the ratio is a variable quantity that depends on the Reynolds number.

By fitting the experimental data in Figure 5, the following expression can be established for the lift coefficient of particles in a flow with a Reynolds number and dimensionless angular speed in the ranges \( 0 < Re < 3500 \) and \( 0 < Rr < 12 \):
The calculated results corresponding to different angular speeds are presented in Figure 5. Moreover, the correlation between the present experimental data and the calculated results using Equation (8) is shown in Figure 6. It is observed that the calculated values are consistent with the present measured ones.

Table 2. Experimental results.

<table>
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<tr>
<th>No.</th>
<th>( D ) (mm)</th>
<th>( u_s ) (m/s)</th>
<th>( \Omega ) (rad/s)</th>
<th>( Rr )</th>
<th>( Re )</th>
<th>( C_{\Omega} )</th>
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Note: \( D \) is the diameter of spheres, \( u_s \) is the velocity of spinning spheres, \( \Omega \) is the angular speed, \( Rr \) is the dimensionless angular speed, \( Re \) is the Reynolds number, \( C_{\Omega} \) is the lift coefficient of a spinning sphere, \( C_{d\Omega} \) is the drag coefficient of a spinning sphere.

Figure 5. The correlation between the rate of the lift coefficient to dimensionless angular speed and the Reynolds number [7,13,14,33,34].
Figure 6. Correlation between the lift coefficient and the Reynolds number.

Figure 6 shows that there is a critical Reynolds number ($Re_c$) at each dimensionless angular speed. Until the Reynolds number is less than the critical value (i.e., $0 < Re < Re_c$), the lift coefficient decreases with the increase in the Reynolds number, while it is approximately constant when $Re_c < Re < 3500$. The constant lift coefficient corresponding to different spin speeds is defined as the limit value of the lift coefficient, which is 0.37 when $1 < Rr < 12$. When $0 < Rr < 1$, the limit value increases with the increase in the dimensionless angular speed. Figure 7 shows the correlation among the calculated values using Equation (8), the previously measured data, and previous simulation results. It is observed that the calculated values are consistent with the previous measured data and simulation results.

Figure 7. Distribution of the measured lift coefficient against the calculated values [7,13,14,33,34].

Loth [22], Shi and Rzehak [23] proposed expressions to calculate the lift coefficient in flows with a Reynolds number $0 < Re < 1000$. It should be noted that the proposed expression in the present study (i.e., Equation (8)) can be applied to calculate the lift coefficient in flows with a Reynolds number up to 3500. In this section, the root mean square relative error ($RMSRE$) is applied as an appropriate index to evaluate the accuracy of different expressions. The $RMSRE$ index can be mathematically expressed in the form below:

$$RMSRE = \sqrt{\frac{C_{L\Omega c} - C_{L\Omega m}}{C_{L\Omega m}}}$$

where $C_{L\Omega c}$ and $C_{L\Omega m}$ are the calculated and measured lift coefficients, respectively.
The RMSRE indices reported by present paper, Loth [22] and Shi and Rzehak [23] are 0.069, 0.073, and 0.121, respectively. When the Reynolds number is in the range of 500 < \( Re \) < 3500, the RMSRE indices reported by present paper, Loth [22] and Shi and Rzehak [23] are 0.014, 0.122, and 0.116, respectively. Meanwhile, when the Reynolds number 0 < \( Re \) < 500, these indices are 0.081, 0.063, and 0.122, respectively. It is concluded that the proposed expression is reliable and can be applied to estimate the lift coefficient in high-Reynolds flows.

3.2. Drag Coefficient
3.2.1. Drag Coefficient of a Non-Spinning Sphere

The total drag force of a non-spinning sphere settling in the fluid can be decomposed into pressure and viscosity components. The correlation among the total drag force, viscosity-related drag force, and pressure-related drag force can be expressed as follows:

\[
F_d = C_d \frac{\pi}{4} D^2 \frac{1}{2} \rho u_r^2 = F_{dv} + F_{dp}
\]  

(10)

where \( F_d \) is the total drag force of a non-spinning sphere, \( F_{dv} \) is the viscosity-related drag force of a non-spinning sphere, \( F_{dp} \) is the pressure-related drag force of a non-spinning sphere, \( C_d \) is the total drag coefficient of a non-spinning sphere.

The pressure-related drag force can be calculated through the following expression:

\[
F_{dp} = C_{dp} \frac{\pi}{4} D^2 \frac{1}{2} \rho u_r^2
\]  

(11)

where \( C_{dp} \) is the pressure-related drag coefficient of a non-spinning sphere. Similar to the pressure-related drag force, the viscosity-related drag force can be expressed in the form below:

\[
F_{dv} = C_{dv} \frac{\pi}{4} D^2 \frac{1}{2} \rho u_r^2 = 3 \pi \mu D u_r
\]  

(12)

where \( C_{dv} \) is the viscosity-related drag coefficient of a non-spinning sphere,

\[
C_{dv} = \frac{24}{Re}
\]  

(13)

Substituting Equations (12) and (11) into Equation (10) yields the following expression:

\[
C_d = C_{dv} + C_{dp}
\]  

(14)

The measured total drag coefficient was summarized by Kelessidis [29] and Cheng [30]. Substituting the calculated \( C_{dv} \) and measured \( C_d \) into Equation (14), the coefficient \( C_{dp} \) can be obtained. The correlation between the pressure-related drag coefficient and the Reynolds number can be expressed as follows:

\[
C_{dp} = \frac{2.5}{\sqrt{Re}} + 0.4 \quad (R = 0.93)
\]  

(15)

Substituting Equations (13) and (15) into Equation (14), the total drag coefficient in the ranges 0 < \( Re \) < 100,000 can be expressed in the form below:

\[
C_d = \frac{24}{Re} + \frac{2.5}{\sqrt{Re}} + 0.4 \quad (R = 0.93)
\]  

(16)

Figure 8 shows the variation in the total drag coefficient against the Reynolds number, indicating that the calculated results are consistent with the experimental data. It is observed that as the Reynolds number increases, the total drag coefficient, viscosity-related drag coefficient, and pressure-related drag coefficient decrease. The total drag coefficient is approximately equal to the viscosity-related drag coefficient at \( Re < 1 \). The viscosity-related
drag coefficient can be negligible, and the total drag coefficient is approximately equal to the pressure-related drag coefficient for $Re > 500$.

![Figure 8. Variation in the drag coefficient against the Reynolds number [30].](image)

3.2.2. Drag Coefficient of A Spinning Sphere

The drag coefficient of the spinning sphere has been studied by other researchers. Barkla and Auchterlonie [4] measured the drag coefficient of the spinning sphere by suspending it as a pendulum. Niazmand and Reksizbulut [14], Kim [15], Dobson and Poon [33], and Giacobello and Balachandar [34] performed numerical investigations and studied the effect of spin on the drag coefficient. The ratio of the drag coefficient of a spinning sphere to the total drag coefficient of a non-spinning sphere $C_d/\Omega$ is equal to the ratio of the measured or simulated drag coefficient of a spinning sphere to the calculated total drag coefficient of a non-spinning sphere using Equation (16). The previous results are shown in Figure 9.

![Figure 9. Distribution of the drag coefficient against the dimensionless angular velocity [4,14,15,33,34].](image)
Compared with the total drag coefficient of a non-spinning sphere, a spinning sphere has higher drag coefficient at $1 < Rr < 10$. In this region, the ratio $C_{d\Omega}/C_d$ varies from 1 to 1.6. However, the drag coefficient of a spinning sphere is less than the total drag coefficient of a non-spinning sphere for $10 < Rr < 25$. When $0 < Rr < 2.5$, the ratio $C_{d\Omega}/C_d$ increases as $Rr$ increases. Beyond this range, the ratio $C_{d\Omega}/C_d$ decreases as $Rr$ increases. To interpret this phenomenon, two empirical correlations were developed to simulate the effect of particle’s spin on the drag coefficient based on the present experimental data and the results of Barkla and Auchterlonie [4]. When $0 < Rr < 2.5$ and $0 < Re < 3500$, the correlation can be expressed as follows:

$$C_{d\Omega} = \left(0.989 + 0.482Rr - 0.093Rr^2\right)C_d \quad (R = 0.86) \quad (17)$$

When $2.5 < Rr < 25$ and $0 < Re < 3500$, the correlation is given by

$$C_{d\Omega} = 2.117Rr^{-0.33}C_d \quad (R = 0.823) \quad (18)$$

Figure 9 compares the calculated results with the previous results. It is observed that the present results are consistent with the previous ones for $0.5 < Rr < 25$. The previous results show that the spin significantly affects the drag coefficient of a spinning sphere when $0 < Rr < 0.5$. It is concluded that the developed equations can be successfully applied to accurately predict the small effects of spin on the drag coefficient of a spinning sphere at low Reynolds numbers.

### 3.3. Lift-to-Drag Ratio

The lift-to-drag ratio of a spinning sphere ($k_{ld}$) can be expressed in the form below:

$$k_{ld} = \frac{C_L\Omega}{C_{d\Omega}} \quad (19)$$

Substituting Equations (8), (17) and (18) into Equation (19) yields the calculated lift-to-drag ratio of a spinning sphere. The previous lift-to-drag ratio of a spinning sphere can be obtained by substituting the simulated lift and drag coefficients from the previous literature into Equation (19). The previous results are compared with the calculated results in Figure 10.

---

**Figure 10.** The distribution of the lift-to-drag ratio against the Reynolds number [13,33,34].
It is observed that when $0 < \text{Re} < 100$, $k_{ld}$ increases with increasing dimensionless angular speed at a certain Reynolds number. At $100 < \text{Re} < 3500$ and $0 < Rr < 0.85$, $k_{ld}$ increases with increasing dimensionless angular speed at a certain Reynolds number and increases with increasing Reynolds number at a certain angular speed. At $100 < \text{Re} < 3500$ and $0.85 < Rr < 6$, $k_{ld}$ increases with increasing Reynolds number at a certain angular speed and can be approximated as a constant value with increasing dimensionless angular speed at a certain Reynolds number. The present equations were preliminarily verified by the previous results.

4. Conclusions

In the present study, the motion of a spinning sphere in a viscous fluid was measured using a high-speed camera. The drag and lift coefficients of a spinning sphere were evaluated through experiments in a water tank using a high-speed camera. Measurements were performed in the ranges of dimensionless angular speed $0.149 < Rr < 3.471$ and Reynolds number $610 < \text{Re} < 3472$. The lift and drag coefficients were obtained by analyzing the motions of the spinning sphere.

1. The obtained experimental data reveal that the lift coefficient is related to the Reynolds number and dimensional angular speed. There is a critical Reynolds number ($R_{c}$) at each dimensionless angular speed. When $0 < \text{Re} < R_{c}$, the lift coefficient decreases as the Reynolds number increases, while it is constant when $R_{c} < \text{Re} < 3500$. The constant lift coefficient corresponding to different spin speeds was defined as the limit value of the lift coefficient. This coefficient is 0.37 when $1 < Rr < 12$, while the limit value of the lift coefficient increases with the increase in dimensionless angular speed for $0 < Rr < 1$.

2. Compared with the total drag coefficient of a non-spinning sphere at a certain dimensionless angular speed, the drag coefficient of a spinning sphere is higher when $1 < Rr < 10$. When $1 < Rr < 10$, the ratio of the drag coefficient of a spinning sphere to the total drag coefficient of a non-spinning sphere $C_{d(\Omega)}/C_{d}$ is between 1 and 1.6. However, the drag coefficient of a spinning sphere is less than the total drag coefficient of a non-spinning sphere when $10 < Rr < 25$. The ratio $C_{d(\Omega)}/C_{d}$ increases with increasing dimensionless angular speed in the range of $0 < Rr < 2.5$, while the ratio $C_{d(\Omega)}/C_{d}$ decreases with an increase in $Rr$ beyond this range. To interpret this phenomenon, two empirical correlations were developed to describe the effect of particle spin on the drag coefficient based on the experimental data and the results from the literature.

3. When $0 < \text{Re} < 100$, the lift-to-drag ratio of a spinning sphere $k_{ld}$ increases with increasing dimensionless angular speed at a certain Reynolds number. At $100 < \text{Re} < 3500$ and $0 < Rr < 0.85$, $k_{ld}$ increases with increasing dimensionless angular speed at a certain Reynolds number and increases with increasing Reynolds number at a certain angular speed. At $100 < \text{Re} < 3500$ and $0.85 < Rr < 6$, $k_{ld}$ increases with increasing Reynolds number at a certain angular speed and can be approximated as a constant value with increasing dimensionless angular speed at a certain Reynolds number.

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